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EFFLUENT TREATMENT FACILITY TRITIUM EMISSIONS MONITORING

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ABSTRACT

An Environmental Protection Agency (EPA) approved sampling and analysis protocol was developed and executed to verify atmospheric emissions compliance for the new Savannah River Site (SRS) F/H area Effluent Treatment Facility. Sampling equipment was fabricated, installed, and tested at stack monitoring points for filtrable particulate radionuclides, radioactive iodine, and tritium. The only detectable anthropogenic radionuclides released from Effluent Treatment Facility stacks during monitoring were iodine-129 and tritium oxide. This paper only examines the collection and analysis of tritium oxide.

INTRODUCTION

The SRS Effluent Treatment Facility was brought on line in late October, 1988. This fulfilled a Resource Conservation and Recovery Act (RCRA) mandate that banned the use of SRS seepage basins after November 8, 1988. The facility was designed to collect and treat water previously discharged to the F- and H- area seepage basins. The facility receives routine process wastewater, reactor fuel reprocessing cooling water, and waste tank storm runoff water. It removes radioactive and nonradioactive contaminants, except tritium, from process effluents. This allows the water to be discharged to Upper Three Runs Creek, which empties into the Savannah River. The process eliminates the use of seepage basins, which adversely impact the quality of groundwater. The EPA construction/operation approval for

the Effluent Treatment Facility required a series of stack effluent tests within 90 days of facility startup. The sampling protocol included in this report was first defended through Department of Energy (DOE) review and was then approved by the EPA.

Two stacks of the Effluent Treatment Facility were monitored during December, 1988 through January, 1989. The control building stack, which handled laboratory hood exhausts, was designed with one Kurz® isokinetic sampling port and was monitored first for tritium and iodine-129. The treatment building stack, which managed process gas exhaust was monitored simultaneously through two Kurz isokinetic sampling ports for particulate radionuclides. Each stack was monitored continuously for three weeks by each sampling system.

PROCEDURES

Residual moisture from the manufacturing process was removed from commercial molecular sieve, Davison type 4A, by heating batches of sieve to 500°C. Dryness was verified by adding an accurately known weight of water to the sieve and then quantitatively recovering the water at the conclusion of the drying process. If the weight of the recovered water was not within 5% of the water added, the sieve was rejected and detained for another drying cycle.

Dry adsorbent was sealed in furnace glassware and stored in a low humidity, tritium free area until use. Samplers were filled with dry adsorbent inside this low humidity, tritium free area. Atmospheric tritium was removed from the air supplied to the room by passing building air in series through a water scrubber, activated molecular sieve beds, and finally HEPA filters. Relative humidity, typically 7%, was monitored continuously to verify equipment operation. The air stream conducted into the room was sampled during all sieve material transfers to verify background conditions. The filled collection canisters were sealed to prevent intrusion of ambient tritium oxide during transport to the collection site.

Isokinetic sampling systems designed by Kurz were installed in the exhaust systems of the control and treatment buildings at the Effluent Treatment Facilities. Portable collection equipment for tritium oxide was connected as shown in Figure 1 to the Kurz sampling system to insure that the collected samples adequately represented facility releases. The tritium oxide sampler, shown schematically in Figure 1, required a flow rate of only 1 liter per minute (lpm). The tritium collection system had little effect on the full flow (nominally 85 lpm) through

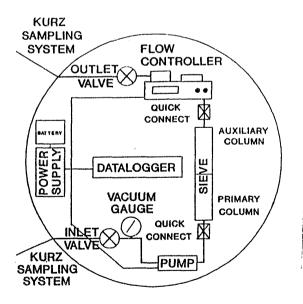


Fig. 1. Flow schematic of the Effluent Treatment Facility Tritium Monitoring System. the Kurz sampling system. After passing through the collection systems, the sampled air streams were redirected to the exhaust stack.

The molecular sieve adsorbed water vapor containing tritium oxide, HTO, from the sampled air stream. A downstream auxiliary column also containing molecular sieve was used to collect any water that persisted in the air stream leaving the primary column. The 1 lpm sampling rate was regulated by a mass flow controller. The flow rate was continuously recorded in a data logger to provide accurate air volumes over the duration of the 24 hour collection period.

The collection canister was a double chambered stainless steel cylinder. The primary adsorbent column was in the first chamber and the backup adsorbent was immediately downstream in the adjacent chamber. The two chambers were separated by a screen to prevent mixing of adsorbent.

The collection canister was changed daily. To change the adsorbent column, air flow through the tritium collection system was first valved off at the inlet and outlet valves of the system. The used column was removed and then sealed to preserve sample integrity during transport to the analysis lab. Sample collection parameters accumulated by the data logger were transferred to tape for later retrieval.

After installation of a new collection canister, the system was checked for air leaks by first opening the inlet and outlet valves and allowing the system vacuum to stabilize, indicated by a vacuum gauge mounted downstream of the system inlet valve. The system inlet and outlet valves were then closed to isolate the vacuum in the sampling system. If the isolated vacuum remained constant for one minute, the system was considered leak free. The system was then opened for collection and the data logger was initiated. After the collection period, the leak check was repeated to verify the integrity of the collected sample.

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Canisters were returned to the laboratory and the sieve material was unloaded into clean, dry sample specific glass vessels. These vessels containing sieve material with physically adsorbed sample were transferred to a furnace, connected to a vacuum manifold and evacuated to 500 microns. The furnace temperature was raised slowly from an initial 300°C to 500°C and held constant there for 24 hours. The entrained water slowly desorbs. After several hours at 500°C, three grams of tritium free water were introduced into the vessels to aid desorbtion of the original sample. Freeze traps, immersed in an ethylene glycol solution and maintained at -40°C or colder, were downstream of the furnace. The desorbed sample water and the additional three grams of expurgating water were crystallized onto the cold surface of a connected trap. After 24 hours, the freeze traps were removed, capped, and allowed to warm to room temperature. Recovered sample water weights were then carefully recorded and the trap contents transferred to sample vials. The original sample weight was the

total recovered weight less the freeze trap weight and the three grams of additional water.

A three gram subsample of the recovered sample was diluted into a scintillation vial containing liquid scintillation cocktail mix. The tritium concentration was measured by counting the aliquot in a Tri-Carb® 2000 CA/LL liquid scintillation analyzer. The analyzer was calibrated as needed with NIST and NIST traceable standards. Appropriate calibration standards and blanks were analyzed with each suite of samples to verify calibrations and background.

RESULTS

Tables 1 and 2 list the daily releases of tritium oxide through the monitored stack. The releases shown in the tables reflect the combined values from the primary and auxiliary adsorbent columns. Typically, greater than 99% of the total tritium in the combined sample was collected on the primary column.

TABLE 1

EFFLUENT TREATMENT FACILITY CONTROL BUILDING STACK

ON	OFF	CONCENTRATION	MILLICURIES RELEASED
DATE	DATE	pCi/m3	PER COLLECTION PERIOD
14DEC88	15DEC88	237.29	0.078
15DEC88	16DEC88	429.76	0.144
16DEC88	17DEC88	141.39	0.046
17DEC88	18DEC88	478.47	0.161
18DEC88	19DEC88	411.04	0.139
19DEC88	20DEC88	137.59	0.046
20DEC88	21DEC88	809.86	0.271
21DEC88	22DEC88	421.35	0.142
22DEC88	23DEC88	94.27	0.031
23DEC88	24DEC88	1010.41	0.338
24DEC88	25DEC88	279.86	0.093
25DEC88	26DEC88	1000.13	0.336
26DEC88	27DEC88	111.97	0.039
27DEC88	28DEC88	101.44	0.033
28DEC88	29DEC88	499.16	0.165
29DEC88	30DEC88	124.17	1).042
30DEC88	31DEC88	255.14	0.084
31DEC88	01JAN89	230.86	0.077
01JAN89	02JAN89	1657.45	0.554
02JAN89	03JAN89	349.70	0.117
03JAN89	04JAN89	1567.26	0.524

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TABLE 2

EFFLUENT TREATMENT FACILITY TREATMENT BUILDING STACK

ON DATE	OFF	CONCENTRATION	
	DATE	pCi/m3	PER COLLECTION PERIOD
04JAN89	05JAN89	1639	2.454
05JAN89	06JAN89	922	1.455
06JAN89	07JAN89	973	1.477
07JAN89	08JAN89	969	1.495
08JAN89	09JAN89	1431	2.219
09JAN89	10JAN89	395	0.559
10JAN89	11JAN89	452	0.725
11JAN89	12JAN89	437	0.667
12JAN89	13JAN89	787	1.255
13JAN89	14JAN89	677	0.987
14JAN89	15JAN89	466	0.714
15JAN89	16JAN89	1378	2.175
16JAN89	17JAN89	2111	3.239
17JAN89	18JAN89	1555	2.579
18JAN89	19JAN89	1057	1.736
19JAN89	20JAN89	20746	30.390
20JAN89	21JAN89	1743	2.731
21JAN89	22JAN89	2612	3.744
22JAN89	23JAN89	1878	2.838
23JAN89	24JAN89	2042	3.046
24JAN89	25JAN89	1872	2.770

Tritium releases ranged from 0.03 to 0.55 millicuries per day from the Control building stack and from 0.56 to 30.39 millicuries per day from the Treatment building stack. The total tritium released from the Control building stack during the three week monitoring period was 3.5 millicuries. The total tritium released from the Treatment building stack was 69.3 millicuries during the second three week monitoring period. On all monitoring days except one, the releases from the Treatment building stack fell in the range of 0.56 to 3.74 millicuries per day. On the single exception day, the release was 30.39 millicuries. The fluctuation cannot be attributed to a known anomaly in the process. Tritium emissions, through the treatment building stack, averaged 20 times higher than those through the control building stack during sampling. These data are shown graphically in Figures 2 and 3.

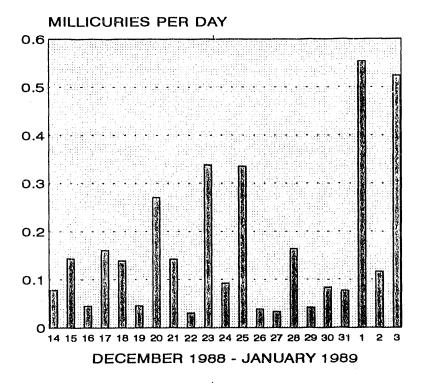


Fig. 2. Control Building Stack Monitoring Results

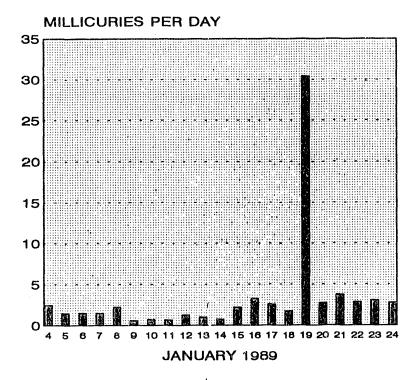


Fig. 3. Treatment Building Stack Monitoring Results

DISCUSSION

The Effluent Treatment Facility uses a series of water treatment processes including pH adjustment, microfiltration, organic removal, reverse osmosis, and ion exchange. Secondary liquid wastes are concentrated by evaporation. The evaporated vapor is released through the building stacks after treatment by ion exchange.

A major design criterion for the Effluent Treatment Facility was secondary waste minimization. The reverse osmosis unit, for example was designed to produce 90% permeate for ion exchange and evaporation. Successful startup of the Effluent Treatment Facility required confirmation of effectual ion exchange cleanup of the stack releases of high separation permeate.

All sampling and analysis for tritium oxide occurred without incident or procedural discrepancy.

CONCLUSIONS

The SRS F/H area Effluent Treatment Facility met or bettered the radionuclide emissions requirements of applicable NESHAP licensing permits at facility startup.

ACKNOWLEDGMENTS

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The Environmental Technology Section and the Environmental Sciences Section of the Savannah River Laboratory conduct ongoing environmental management and research programs in support of the Effluent Treatment Facility as well as other Independent SRS operations. environmental studies of post-operational characteristics of Upper Three Runs Creek waters and fish populations are being conducted by the Savannah River Ecology Laboratory, operated by the University of Georgia under contract with DOE. The Environmental Monitoring Section of the **Environmental Protection Department** conducts extensive sampling programs in support of SRS environmental compliance activities.

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