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A Model for the Control of Dissolved Manganese in the Interstitial Waters of Chesapeake Bay  
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Recent interest in the origin of marine and fresh water ferro-manganese deposits has resulted in a number of investigations of the distribution of dissolved manganese in recent sediments (1-6). Attempts to model the observed manganese distribution have been made by several investigators.

Michard (7) devised a model to describe the concentration of manganese as a function of depth in the sediment by dividing the sediment into three chemically distinct zones and by using a partition coefficient,  $\alpha$ , to describe the distribution of manganese between the solid and solution phases. The differential equations were developed independently for each zone, and, then, they were coupled at the boundaries between the different zones in order to maintain continuity in the calculated profiles. Calvert and Price (8) developed a qualitative model to describe the profiles of manganese in the sediments of Loch Fyne, Scotland. Unfortunately, their sample spacing was too large to delineate the fine structure of the dissolved manganese profile typically found in the top few centimeters of an estuarine sediment. Also, analyses of chemical parameters other than the trace metals were not done, and so, they could only presume that the chemical controls in Loch Fyne were the same as have been found in other systems. Robbins and Callendar (9) developed a model, purportedly continuous over the depth of the sediment column, to describe the diagenesis of manganese in Lake Michigan sediments. This model, however, requires that a point source of manganese exist at some arbitrary depth in the sediment and that the concentration of dissolved manganese slowly approach equilibrium with some elusive detrital manganese phase at greater depths. While a qualitative fit is obtained for their field data, very little is actually known about the chemical nature of these interstitial waters, and, thus, the operative equilibrium controls in this system are again left to conjecture.

Other models have been developed to explain the frequently observed enrichment of manganese in the solid phases of surface sediments. Bender (10), Anikonchine (11), and Lynn and Bonatti

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(12) have developed diffusion models to describe this phenomena. The emphasis of these works has been to investigate if upward diffusion of manganese could supply the metal required to explain the observed enrichment. In light of this goal, no attempts were made to describe the specific diagenetic reactions involved in the control of manganese in these sediment systems.

In this paper, we explore possible chemical and physical mechanisms that may control the distribution of manganese in the Chesapeake Bay estuarine sediments. Interstitial waters of the bay sediments contain greater concentrations of dissolved manganese than have been reported in any other marine or brackish water sediment system (1-4). It is not uncommon to find manganese concentrations that exceed 400  $\mu\text{M}$  ( $\sim 20$  ppm) and concentrations as high as 950  $\mu\text{M}$  (52.5 ppm) have been observed. Based on these observations and the general chemical composition of the interstitial waters, we develop a model to describe profiles of manganous ion in the Chesapeake Bay sediments.

### Field Study and Methods

A two phase field program was initiated to investigate the spatial and temporal variability in the pore water composition of Chesapeake Bay sediments. Figure 1 shows the location of some of our standard sampling stations. The problems involved in relocating at any particular stations in the bay and the attendant sampling errors have been discussed (13).

Temporal changes were investigated by sampling monthly at a mid-bay station for the period June 1971 to August 1972. This station, 858-8, is located at  $38^{\circ}58'20''\text{N}$  x  $76^{\circ}23'\text{W}$ , east of the mouth of the Severn River and is located in about 33 m of water. Three gravity cores were collected each month using a Benthos gravity corer. The sediment was held in cellulose-acetate-butyrate plastic coreliners. A plastic butterfly valve was used to retain the sediment during retrieval. The water trapped above the sediment in the core liners during this operation was siphoned off, filtered and saved for chemical analysis. Pre-determined sections of the sediment were extruded directly into Reeburgh-type sedimentsqueezers (14). The pore waters to be used for chemical analysis were expressed through Whatman filter paper and 0.22  $\mu\text{m}$  Millipore membrane filters by 150 psi pressure exerted by nitrogen gas against a rubber diaphragm in the squeezer.

Aliquots of these samples were analyzed for carbonate alkalinity, chloride, ammonia, reactive phosphate, ferrous iron, pH,  $\text{pS}^{\ominus}$  and Eh onboard ship. The remainder of the sample was returned to the lab for analysis of silica and sulfate. A complete description of both the analytical techniques and the sample handling procedures are found elsewhere in this symposium (13).

In the second phase of the field program, the spatial variability of the pore water composition in the bay was investigated.

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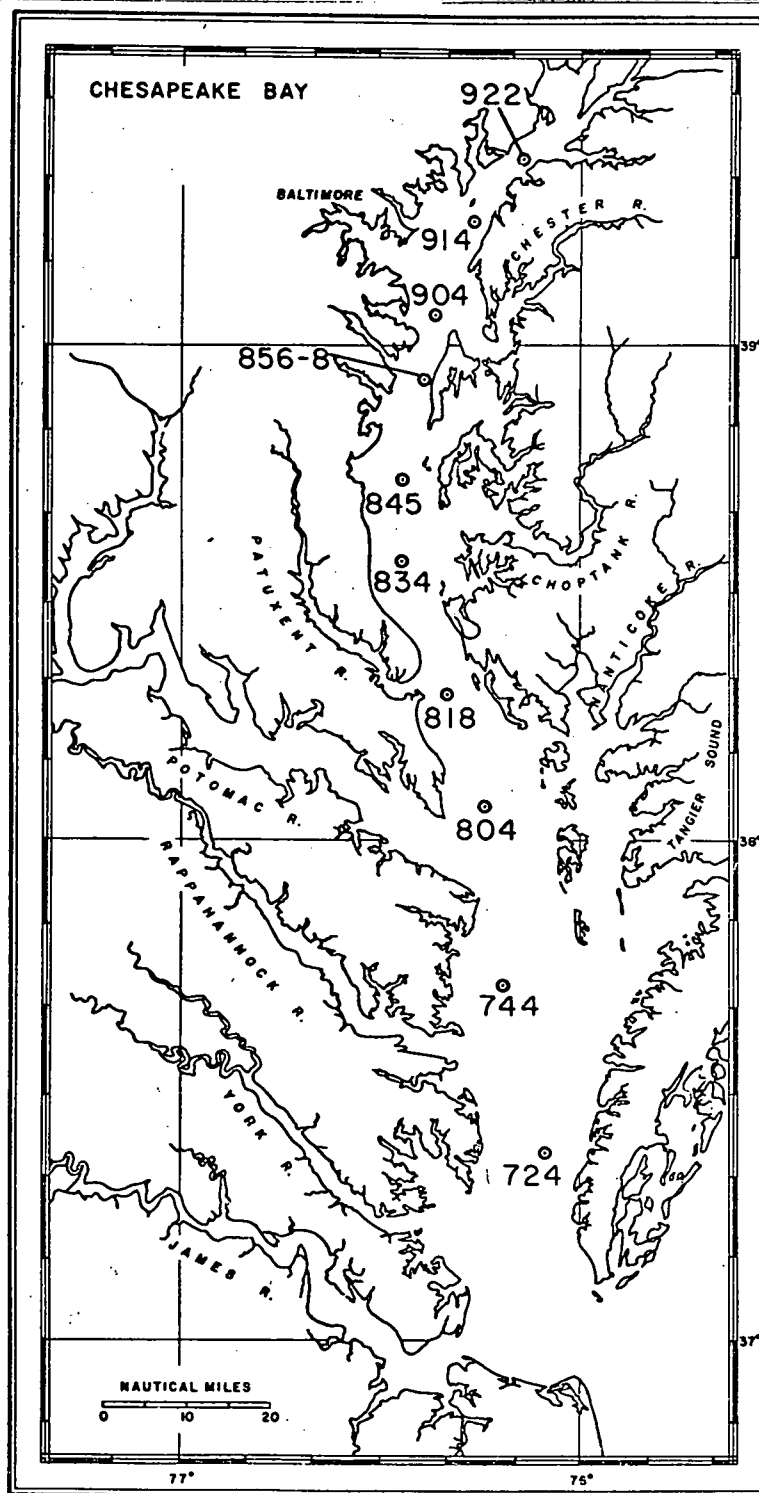


Figure 1. The Chesapeake Bay and the locations of our sampling stations along its central axis. Stations occupied during this study, but not shown on the map, are cross-bay transects at the latitude of the stations shown.

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50 Six cruises conducted between August 1972 and December 1974  
 49 allowed us to collect over 700 individual interstitial water  
 48 samples along with the associated sediment. Sampling locations  
 47 ranged from station 935, located at the mouth of the Susquehanna  
 46 River near Havre de Grace, Md., to station 724R, located between  
 45 the York and Rappahannock Rivers in Virginia. During this phase  
 44 of the program, all sample handling operations were done in a  
 43 glove box under an inert nitrogen atmosphere to avoid the loss  
 42 of trace metals and phosphate (15). Otherwise, all onboard and  
 41 laboratory analytical techniques remained unchanged. In addition  
 40 to the above analyses, dissolved manganese was determined on  
 39 acidified subsamples of the pore water collected during this  
 38 phase of the study by direct aspiration of the sample into an  
 37 atomic absorption spectrophotometer. Typically, samples were  
 36 diluted by a factor of between 5 and 100 with 0.01 NHCl to lower  
 35 the concentration of manganese into the linear range of detection  
 34 for our instrument. A detail description of the techniques is  
 33 found elsewhere in this symposium (13).

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### 32 Results and Discussion

30 Physical Influences on Transport: Chloride Data. The  
 29 Chesapeake Bay estuary is a very productive area, biologically.  
 28 This is reflected in the organic content of the sediments in the  
 27 estuary which is typically 2 to 3% on a dry weight basis. A  
 26 large infaunal benthic community is supported by these organics.  
 25 The resulting activity mixes the upper portion of the sediment  
 24 and enhances the exchange of material between the sediments and  
 23 the overlying water. To investigate the magnitude of this mixing  
 22 effect, along with other physical processes such as diffusion, we  
 21 have studied the time dependent changes that occur in pore water  
 20 chloride concentration with depth beneath the sediment/water  
 19 interface.

18 Chloride is an ideal tracer to study these effects in an  
 17 estuary such as the bay. It is essentially inert in terms of  
 16 chemical reactivity in the estuarine environment. Thus, only  
 15 the changing physical environment affects its distribution.  
 14 Because of the seasonal variations in the fresh water input to  
 13 the bay, the chloride distribution in the bottom waters is con-  
 12 stantly changing. This produces a continually varying concentra-  
 11 tion gradient between bottom waters and interstitial waters. By  
 10 following the response of the chloride profile in the sediment to  
 9 changes in the chlorinity of the overlying waters, an estimate  
 8 of the net rate of transport in the sediment can be made.

7 Figure 2 shows the results of our study at station 858-8.  
 6 Easily measurable changes occur in the chloride profile on a  
 5 month-to-month basis. The surface sediments respond most quickly  
 4 and, with increasing depth, the magnitude of the changes decreases  
 3 until at a depth of about 20 cm, variations are essentially within  
 2 the analytical limits of the measurements. The mean concentration  
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50 of chloride in the upper  
49 20 cm of the profile is  
48 considerably more dilute  
47 than the concentrations  
46 deeper in the sediment.  
45 This is a result of the  
44 year-to-year fluctuations  
43 in the mean discharge of  
42 the Susquehanna River  
41 which supplies between  
40 90 and 97% of the fresh  
39 water to this portion  
38 of the bay.

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37 If the primary  
36 mechanism for the trans-  
35 port of chloride is dif-  
34 fusalional in nature, the  
33 diffusion equation should  
32 adequately describe the  
31 shapes of the measured  
30 profiles. Lateral con-  
29 centration gradients of  
28 chloride in the sediments  
27 are small compared to  
26 the vertical gradients,  
25 and so the situation is  
24 reduced to a one dimen-  
23 sional diffusion problem.  
22 Several models for dif-  
21 fusion in modern sedi-  
20 ments have appeared in  
19 the recent literature

18 (16-19). Only one of these was designed specifically to deal  
17 with a boundary condition which is oscillatory in nature (17).  
16 However, for our purposes in this paper, the numerical approach  
15 used by Scholl et al., is too involved.

14 One other may be important in setting up this diffusion  
13 model for chloride. Sediment deposition in the Chesapeake Bay  
12 is on the order of 1 cm/yr (20). The sediment is derived from  
11 both shoreline erosion and suspended sediment discharge from the  
10 inflowing rivers and streams. While this probably does not  
9 significantly alter the chloride distribution in the sediment  
8 over the period of one year, provisions should be made in the  
7 model to account for any long term effects resulting from the  
6 sediment accumulation on the chloride distribution.

5 The equation, incorporating a sedimentation term, is:

$$\frac{dC_1}{dt} = D \frac{d^2 C_1}{dx^2} - W \frac{dC_1}{dx} \quad (1)$$

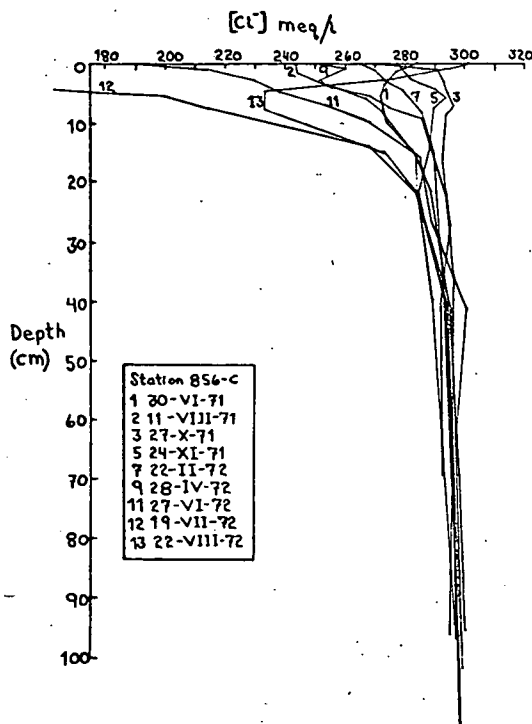
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Figure 2. Interstitial water chloride profiles collected at station 856-8 (C) over a one-year period. Only about half of the profiles are shown here. Sampling date for each profile is given in the legend.

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50 With the boundary conditions:

$$49 \quad C1(0,t) = C1_0 + C1_1 \cos(\lambda_1 t) + C1_2 \cos(\lambda_2 t) \quad (2)$$

$$47 \quad \left. \frac{dC1}{dx} \right|_{x \rightarrow \infty} = 0 \quad (3)$$

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44 Equation (1) is the standard one-dimensional form of the diffusion equation with an advective term ( $-W \frac{dC1}{dx}$ ) to describe the effects of sediment deposition. The boundary conditions are based on the physical observation made for the system.

43 The first boundary condition describes the chloride concentration in the overlying water as a function of time. The first term on the right hand side of the equation is the long term mean chlorinity. The second term accounts for the seasonal fluctuations in the chloride concentration. These are the variations observed in the month-to-month changes in the chloride profiles. The last term describes the long term changes in the mean annual chlorinity. It is this term which accounts for the skewing of the upper portion of the profile toward more dilute concentrations relative to the deeper pore waters.

42 The second boundary condition simply states that there is no net diffusional flux of chloride at great depth in the sediment. This is equivalent to saying that the estuary is "lined" by impermeable bedrock beneath the sediment.

41 For constant  $D$  and  $W$  the solution to this equation is found in Carslaw and Jaeger (21):

$$23 \quad C1(X,t) = C1_0 + C1_1 \cos\{\lambda_1 t - X a_1^{1/2} \sin \frac{1}{2} \phi_1\} \exp \left| \frac{WX}{2D} - X a_1^{1/2} \cos \frac{1}{2} \phi_1 \right|$$

$$22 \quad + C1_2 \cos\{\lambda_2 t - X a_2^{1/2} \sin \frac{1}{2} \phi_2\} \exp \left| \frac{WX}{2D} - X a_2^{1/2} \cos \frac{1}{2} \phi_2 \right| \quad (4)$$

$$21 \quad \text{where} \quad a_1 = \left| \frac{W^4}{16 D^4} + \frac{\lambda_1^2}{D^2} \right|^{1/2}$$

$$20 \quad \text{and} \quad \phi_1 = \tan^{-1} (4D\lambda_1/W^2)$$

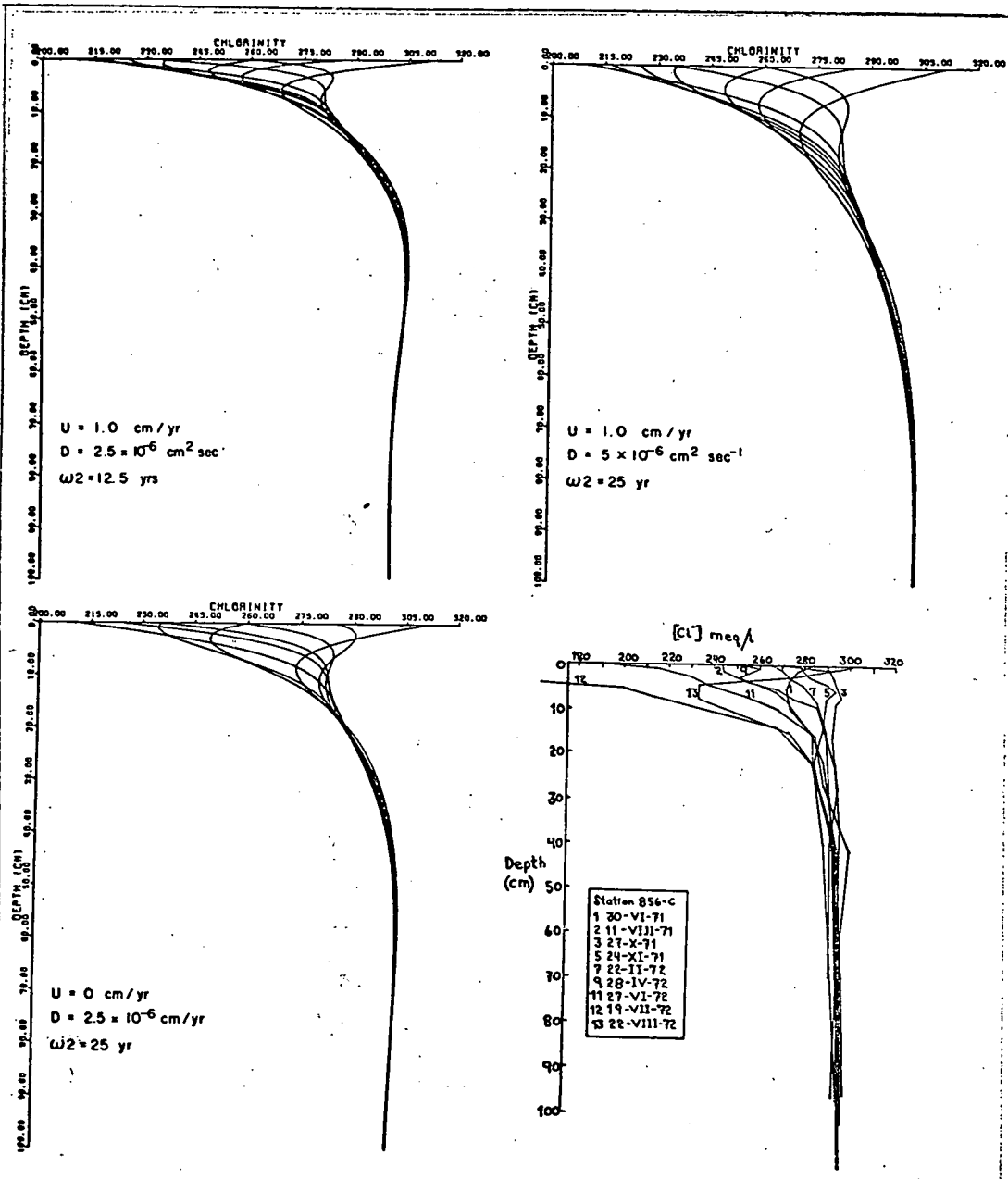
19 By picking values for  $W$ ,  $D$ , and  $\lambda_2$  ( $\lambda_1 = 2\pi/\text{year}$ ), theoretical, time dependent chloride profiles can be calculated. The range of the values for  $W$  and  $\lambda_2$  are available from independent sources (20, 22). Therefore, an estimate of the diffusion coefficient typical of bay sediments can be made by matching calculated profiles to the field data.

18 The results of some representative calculations are shown in figure 3a-c. All three parameters,  $D$ ,  $W$  and  $\lambda_2$ , were varied in the calculations to determine the net effect of each on the profiles. Results indicate that reasonable rates of sedimentation has very little effect on the chloride profiles. It makes little difference whether  $W$  is  $3 \times 10^{-5}$  cm/yr or 3 cm/yr in the final results. Changes in  $\lambda_2$  has only a slightly greater effect.

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Figure 3. a-c. Vertical profiles of chloride calculated by the diffusion model. These plots show the effect of varying  $D$ ,  $W$  and  $\lambda_2$  on the profiles. d. For comparison to the model profiles, the field data is replotted.

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Changes in the diffusion coefficient,  $D$ , had the greatest effect of these three parameters. Comparison of the calculated profiles to the field data indicate that the best value for a constant  $D$  is  $5 \times 10^{-6}$   $\text{cm}^2/\text{sec}$ . This is in good agreement with values that have been reported in other sediment systems (23,24). Results of the model indicate that the diffusion coefficient is not strictly a constant with depth. We have a numerical model which calculates chloride concentration profiles through time for any arbitrary functional form of  $D$ . However, the purpose here is not to generate exact replicates of the observed chloride profiles in the bay sediments, but rather is to obtain a feeling for the magnitude of the combined effects of diffusion, broturbation and sedimentation on the distribution of any dissolved component of the interstitial waters. The simple model described above accomplishes this goal.

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Manganese: Field Data. The next step in determining the overall diagenetic behavior of dissolved manganese in anoxic pore waters is to identify which, if any, specific reactions or apparent equilibria may be involved in controlling the manganese cycle. To do this it first helps to examine the concentration profiles of manganese. Figure 4 shows some typical profiles of dissolved manganese for stations located along the axis of the bay. These samples were collected in the summer of 1973.

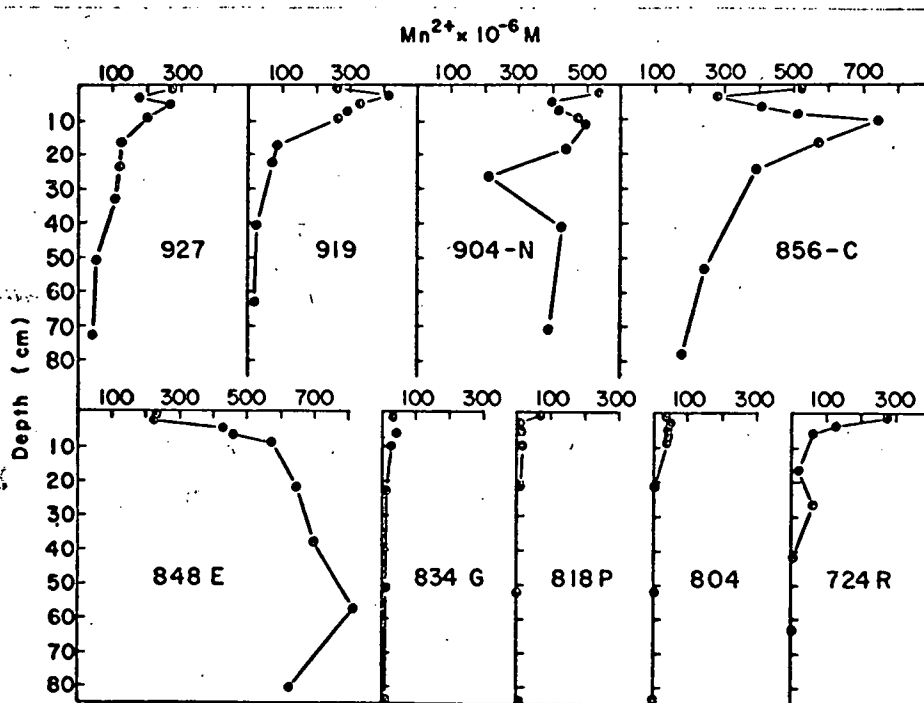


Figure 4. Profiles of dissolved manganese in the interstitial waters of the sediments obtained along the central axis of the bay. These are typical summer profiles.

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50 Several features of these profiles should be noted. The  
49 concentration of dissolved manganese in the overlying waters  
48 never exceeded 6  $\mu\text{M}$  on this cruise. These values, which are  
47 relatively concentrated by open water standards, are probably  
46 the result of the resuspension and subsequent mixing of the top  
45 few millimeters of sediment which occurred during the coring  
44 operation. Within the sediment, concentrations of dissolved  
43 manganese increase quickly below the sediment/water interface.  
42 Commonly, the concentration in the top two centimeters of the  
41 sediment column is the highest in the core. Concentration of  
40 dissolved manganese usually decreases with depth. Samples col-  
39 lected at other times of the year exhibit the same gross features.  
38 However, during colder periods, the maximum concentration is  
37 reached five or ten centimeters below the sediment/water inter-  
36 face.

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35 To determine whether any heterogeneous equilibrium con-  
34 straints are being imposed on the concentration of dissolved  
33 manganese by the pore water composition, activity calculations  
32 were made on each sample. These calculations were checked for  
31 possible saturation of a number of common sedimentary manganese  
30 minerals including rhodochrosite ( $\text{MnCO}_3$ ), reeddingite ( $\text{Mn}_3(\text{PO}_4)_2 \cdot$   
29  $3\text{H}_2\text{O}$ ) and albandite ( $\text{MnS}$ ). The calculation used a modified form  
28 of the Garrels and Thompson model for sea water (25) to describe  
27 the ionic medium and determine ionic strengths. Activity coef-  
26 ficients were estimated from the extended form of the Debye-Hückel  
25 equation. An ion pairing model was then used to calculate activi-  
24 ties of manganous ion from the composition of the pore waters.  
23 Free energy data used in calculations were obtained from several  
22 sources (26, 27).

21 The results of these calculations indicate that rhodochrosite  
20 is the only mineral for which the pore waters exceed saturation.  
19 This supersaturation exists at all stations and for most levels  
18 within the sediments of the bay. In the northern bay, the pore  
17 waters are between 1.5 and 2.5 orders of magnitude supersaturated  
16 and in the southern bay, the pore waters are generally in the  
15 range of 0.5 to 1.5 orders of magnitude supersaturated with  
14 respect to rhodochrosite.

13 Albandite is the only other mineral that even approaches  
12 saturation in the pore water system. This situation occurs in  
11 the southern portion of the bay where pore water sulfide values  
10 are generally higher because of the greater sulfate concentrations  
9 in the overlying water.

8 To describe manganese profiles in the bay, the interaction  
7 between manganese and carbonate must be further investigated.  
6 To this end it is helpful to understand the behavior and genesis  
5 of bicarbonate in the pore waters of the bay.

4  
3 Carbonate. At pore water pH's, bicarbonate ion concentration  
2 is essentially equal to the carbonate alkalinity. Figure 5 shows  
1 some profiles of carbonate alkalinity measured at stations.

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located along the axis of the bay. Concentrations of bicarbonate ion in surface sediments and overlying waters rarely exceed 1.5 meq/l. The concentration generally increases with depth; however, individual profiles can be quite complex.

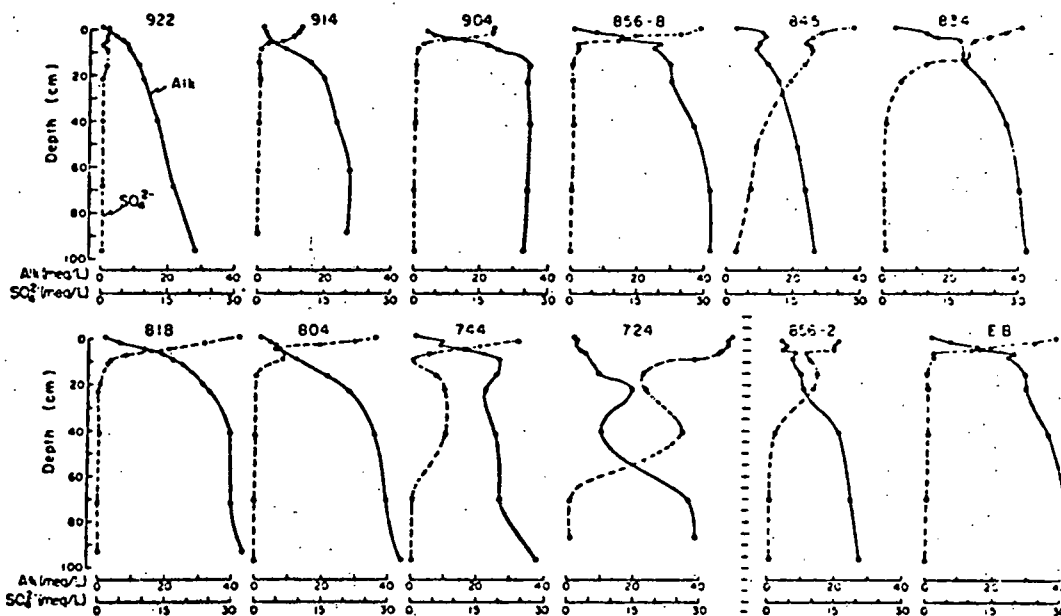
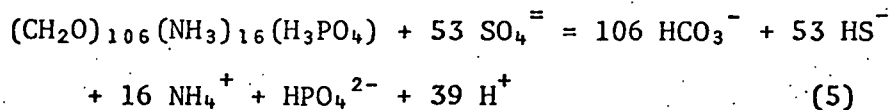
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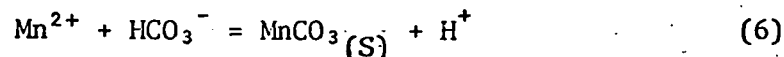
Figure 5. Sulfate and alkalinity data for the interstitial waters along the axis of the bay. These are typical profiles.

Bicarbonate ion is a byproduct of bacterial oxidation of organic matter in the sediment. In an anoxic marine environment, sulfate is used by the bacteria as an oxygen source. The general equation for this oxidation is written:



For every equivalent of sulfate reduced, one equivalent of bicarbonate is generated, along with lesser amounts of ammonia, phosphate and sulfide. Measured profiles of sulfate in the bay sediments are shown in figure 5. The one-to-one correspondence between the amount of sulfate reduced and the amount of bicarbonate generated as predicted by (5) does not hold true. However, as can be seen in figure 5, a nearly linear relation does exist.

Bicarbonate Ion Control of Manganese. The reaction of bicarbonate ion with manganous ion can be expressed as:

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50 As indicated by the activity calculations, this is the reaction  
49 which controls the concentration of manganese in the sediment.  
48 The ion activity product (IAP) of the reaction components of (6)  
47 calculated from pore water compositions usually exceeds the  
46 thermodynamically derived solubility product of rhodochrosite.  
45 This occurs for two reasons.

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44 First, one of the assumptions made in setting up the ion  
43 pairing model to calculate manganese ion activities was that only  
42 inorganic ion pairs need be considered. No attempt was made to  
41 account for organic complexes of manganese. The interstitial  
40 waters of the Chesapeake Bay contain up to 70 ppm dissolved  
39 organic carbon. Others (28) have shown that manganese can  
38 complex strongly with naturally occurring organics. Because  
37 the association constants for reactions of this type are not well  
36 known, they cannot be included in the equilibrium calculations.  
35 This exclusion results in calculated activities which are larger  
34 than actually occur.

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33 The second reason apparent supersaturation exists in the bay  
32 sediments is that the IAP we calculate is compared to the solu-  
31 bility of pure rhodochrosite. It is highly likely that the  
30 rhodochrosite in the sediments is not a pure phase, but a solid  
29 solution with an enhanced solubility compared to that of pure  
28 rhodochrosite.

27 To incorporate the effects of these two factors, we calculated  
26 an "apparent stability constant",  $K'_{sp}$ , to describe the reaction  
25 between the dissolved components and the solid sedimentary car-  
24 bonate phase. pH, alkalinity and manganese data from the deepest  
23 sample from each core was used for this purpose. We felt that  
22 these samples had had the greatest opportunity to attain equilib-  
21 rium with the solid phase. This calculation yields a Gibbs free  
20 energy for the manganese carbonate phase of -193.1 kcal/mole.  
19 These combined effects reduce the apparent stability of the  
18 sediment phase by about 2 kcal compared to the free energy of  
17 pure rhodochrosite which lies in the range -195.05 (29) to -195.7  
16 kcal/mol (30).

15 If the pH and bicarbonate concentration are known, the con-  
14 centration of manganese can be determined from the mass action  
13 relation for (6).

$$12 \quad \text{Mn}^{2+} = \frac{K'_{sp} \cdot [\text{H}^+]}{[\text{HCO}_3^-]} \quad (7)$$

9 Sample by sample adjustments of pH could be made in applying (7)  
8 to the calculated manganese profiles. However, because variations  
7 in pH with depth in any one core are generally small, and in  
6 order to maintain continuity, the mean value of the measured pH  
5 within a core is used for all depths in that core.

4 Similarly, bicarbonate concentrations on a point by point  
3 basis could be used in the calculation. However, to expedite  
2 the computational process and again for sake of continuity in the  
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profiles, we chose to use a simple model to describe the generation of bicarbonate. Because of the observed relation between sulfate and bicarbonate, a modification of Berner's model for sulphur diagenesis was used (31) to calculate the bicarbonate distribution in the sediment. Bicarbonate concentration is described as a function of depth by the equation:

$$\text{HCO}_3^- = \text{HCO}_3^-(\text{I}) + \frac{W^2 G_0}{W^2 + K_1 D} [1 - \exp(-K_1 X/W)] \quad (8)$$

where  $\text{HCO}_3^-(\text{I})$  = bicarbonate in the overlying water

W = the sedimentation rate

D = the diffusion coefficient for bicarbonate

$G_0$  = the organic content of surface sediments

$K_1$  = the first order rate constant for bicarbonate generation

and X = distance below sediment/water interface (cm)

There are several assumptions in this model. W and D must be constants through time and space, respectively. Generation of bicarbonate is assumed to be a first order reaction with respect to the amount of available organic material in the sediment. Finally the bicarbonate profile is assumed to have reached steady state. Since we are simply fitting this model to the bicarbonate data, these assumptions are of little concern to us.

Estimates for W and D are obtained by independent means. By adjusting the values of  $K_1$  and  $G_0$  the model can be fit to the data. The results of this method of calculating the bicarbonate concentrations are shown in figure 7 for several of our stations. The values of pH, W,  $K_1$ , and  $G_0$  used for each station are listed in table I.

TABLE I

Station	W	pH	$K_1$	$G_0$	$K_2$	$(\text{MnO}_2)_0$
	cm/yr		year <sup>-1</sup>	mmoles l <sup>-1</sup>	year <sup>-1</sup>	moles l <sup>-1</sup>
904D	1.0	7.5	0.0133	0.091	0.0173	0.010
834G	0.5	7.65	0.0385	0.265	0.0173	0.0025
914Q	1.0	7.2	0.0345	0.082	0.0173	0.012
848F	0.5	7.7	0.0198	0.179	0.0173	0.005
919T	1.0	7.0	0.0277	0.105	0.0173	0.015

$D = 3 \times 10^{-6}$  cm<sup>2</sup>/sec. for all stations.

By using (8), concentrations of dissolved manganese can be calculated for most of the sediment column. However, the results of the calculation in the top few centimeters of the sediment are inconsistent with the field data. This portion of the profile must be controlled by some other process.

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Oxidation and Diffusion of Manganese. The concentration of dissolved manganese in the waters immediately overlying the sediment are generally small. The concentration jumps to as high as 857  $\mu\text{M}$  within the top two centimeters of the sediment. To maintain such a large concentration gradient over a small distance for any length of time, a sink for dissolved manganese must exist at the sediment/water interface. Manganese is sensitive to the oxidation potential of the environment. Upon diffusing from the anoxic mud into a zone containing free molecular oxygen, manganese would precipitate as a hydrous-oxide phase. Then, upon burial, this metal would be available for remobilization.

The concentration of dissolved manganese in the zone immediately beneath the oxic layer is dependent on two factors: 1) how fast the metal is released from the solid phase, and 2) how quickly it diffuses away from its source. The rate a material is released from a solid depends on many parameters. The surface area of the solid is one of the major factors (32, 33). The hydrous oxide phase is present essentially as a two dimensional coating on clay particles. For this reason, the amount of solid manganese is roughly proportional to the surface area of the solid available for dissolution. If we assume that the rate of dissolution of manganese is first order relative to the amount of available solid phase, the rate of production will be expressed as

$$\frac{d \text{Mn}^{2+}}{dt} = -K_2(\text{MnO}_2) \quad (9)$$

To apply this expression to bay sediments, we must assume that for any station the supply of solid manganese to the surface sediments is constant with time. Since this surface zone rarely extends more than about 5 cm into the sediment, representing a maximum period of about 10 years, this is a reasonable assumption.

Finally, the balance between the rate of dissolution and subsequent upward diffusion of the manganous ion must be established. If we assume the system is in steady state, this balance can be written

$$D \frac{d^2 \text{Mn}^{2+}}{dx^2} - W \frac{d \text{Mn}^{2+}}{dx} + K_2(\text{MnO}_2) = 0 \quad (10)$$

with the boundary conditions

$$\text{Mn}^{2+}(0, t) = 0$$

$$\text{and } \text{Mn}^{2+}(\infty, t) = \text{Mn}^{2+}_f$$

The solution to this equation is

$$\text{Mn}^{2+} = \frac{W^2 (\text{MnO}_2)_0}{W^2 + K_2 D} [1 - \exp(-K_2 X/W)] \quad (11)$$

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where  $W$  = the sedimentation rate  
 $D$  = the diffusion coefficient for  $Mn^{2+}$   
 $K_2$  = the first order rate constant for the dissolution  
of the hydrous manganese oxide phase.  
and  $(MnO_2)_0$  = the amount of solid manganese in the surface  
sediments.

$X$  = distance below sediment/water interface (cm)  
This solution is similar to (8). The values of  $(MnO_2)_0$  and  $K_2$   
are listed in table I.

The two processes that dominate manganese chemistry have now  
been described. They must be integrated into a unified model in  
order to predict the distribution of dissolved manganese over  
the whole sediment column. Each reaction is limiting over that  
part of the sediment where it is dominant. This is to say, in  
the upper part of sediment, there is only a limited rate at which  
 $Mn^{2+}$  is produced. It cannot attain concentrations large enough  
to become saturated with respect to any mineral because it simply  
diffuses to the sediment/water interface too quickly. At greater  
depths, the amount of dissolved  $Mn^{2+}$  which can be maintained by  
dissolution is greater than that which is allowed by the solu-  
bility of the manganese carbonate. Precipitation of the carbo-  
nate then becomes the limiting factor in the observed concentra-  
tion of the metal. Therefore, by calculation the concentration  
of manganese using both (7) and (11), the observed concentration  
will be the lesser of the two values at any particular depth.

Results of Model Calculations. Figure 6 shows the results  
of our calculations. The second in each set of graphs shows the  
concentration of dissolved manganese as a function of depth in  
the sediment at several northern and mid-bay stations.

The solid line is the concentration of dissolved manganese  
predicted by the model. Remember that this single line is the  
combined result of two competing processes. The portion of the  
curve increasing with depth is the result of the dissolution and  
upward diffusion of manganous ion. The lower portion of the  
profile is the part controlled by equilibrium with the carbonate  
phase.

### Conclusion

We have developed a model for the prediction of dissolved  
manganese distribution in the anoxic pore waters of the sediments  
of the Chesapeake Bay. The model requires knowledge of the pH of  
the pore waters, the distribution of bicarbonate ion with depth  
in the sediment, the amount of manganese oxide in the surface  
sediment and the rate of release of manganous ion from those  
solids. In the calculations presented, a modification of Berner's  
model for sulphur diagenesis was used to describe bicarbonate ion  
distribution. This model was fit to the observed profiles. Other

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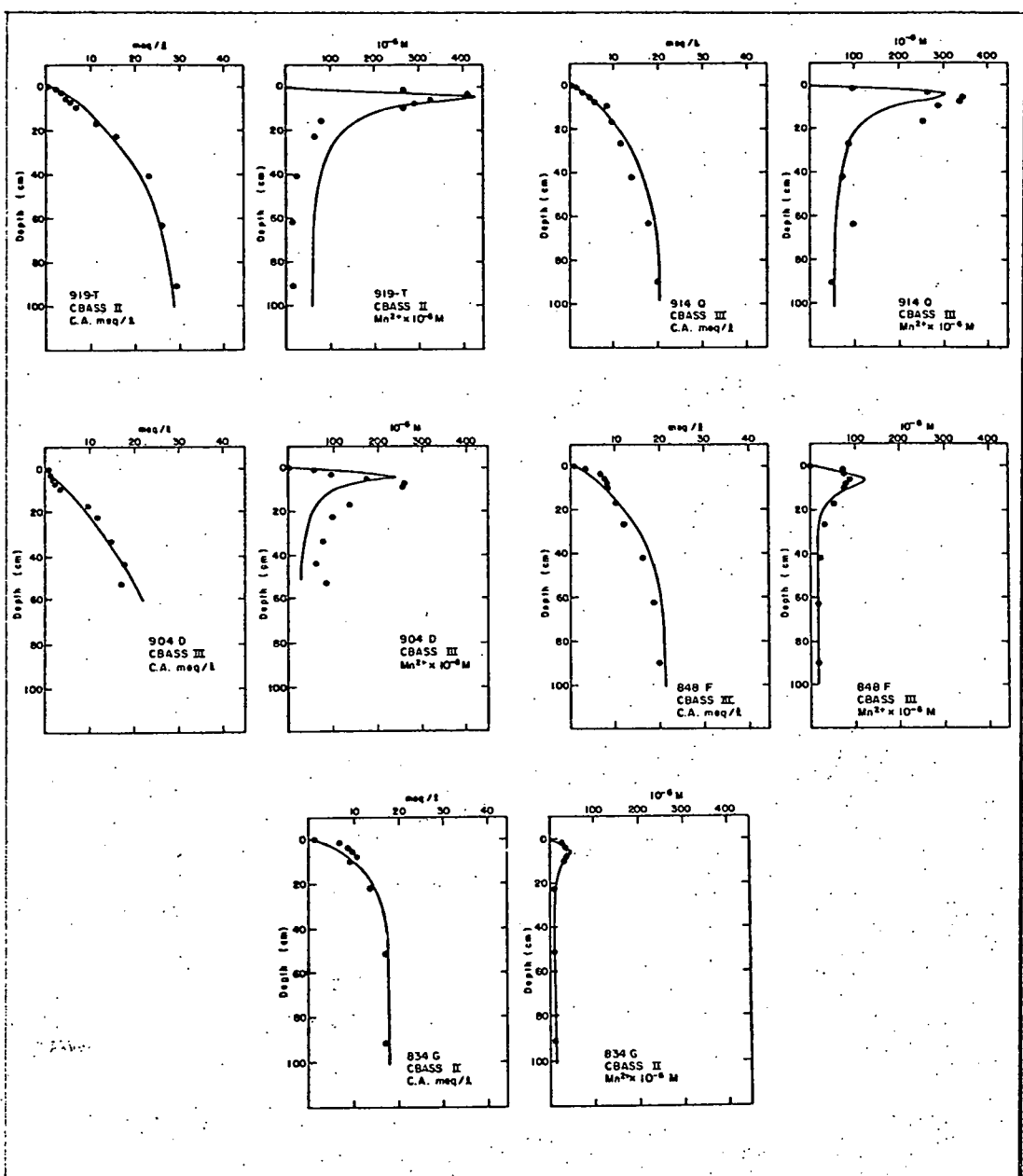


Figure 6. These are plots of the carbonate alkalinity and dissolved manganese profiles at five upper and mid-bay stations. The alkalinity plots show the field data (circles) and the model representation of that data used in the calculation of the manganese profiles (line). The second graph in each set contains the dissolved manganese profile at each station (circles). The concentration profiles predicted by our model using the pH and alkalinity data are shown by the line.

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50 techniques, however, such as fitting a power series to the data,  
49 could equally serve this purpose.

48 There were several assumptions used in the model. The  
47 diffusion coefficient and sedimentation rates were assumed to be  
46 constant through space and time, respectively. We assumed that  
45 steady state had been reached in the system, and that with depth  
44 in the core manganous ion was in equilibrium with a poorly  
43 crystalline carbonate phase.

42 The model was developed from observations on the pore water  
41 composition. The model describes the results of two independent  
40 competing reactions. Both reactions are continuous over the whole  
39 sediment column, and the final calculated concentration of dis-  
38 solved manganese at any particular depth is dictated by the  
37 process most limiting that concentration at that depth.

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36 Agreement between the model and the field data is generally  
35 good. This suggests that the processes controlling the distribu-  
34 tion of dissolved manganese in the bay sediments are basically  
33 understood. The results of the model are qualitatively the same  
32 as reported profiles of dissolved manganese in other marine sedi-  
31 ment systems (1, 3, 9). It would be most interesting to see if  
30 the model can describe these interstitial water systems with the  
29 same accuracy as was obtained in Chesapeake Bay sediments.

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