

Second, the effect of initial imperfections is enormous for circumferential mode buckling according to incremental theory (curve 1A compared to Eq. (4), Fig. 2). Circumferential buckling according to deformation theory, however, is not very sensitive to initial imperfection (curve 3A compared to curve 3, Fig. 1). These results are now in agreement with those of Onat and Drucker for the imperfection sensitive cruciform.<sup>6</sup>

On the basis of the preceding remarks and the fact that the axisymmetric mode is not greatly affected by initial imperfections,<sup>2,3</sup> what was originally conjectured by Gerard<sup>3</sup> can now be considered firmly established. Cylinders fail in the diamond-shaped circumferential mode pattern in the proportional limit region of the shell material, because the presence of small unavoidable imperfections in shape lowers the circumferential mode buckling stress below the corresponding axisymmetric mode value. However, above the proportional limit region, the axisymmetric mode will be observed, because the spread in predictions between circumferential mode and axisymmetric mode buckling will be too great to be overcome by initial imperfections acting in conjunction with a circumferential mode.

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## Errata: "Effect of Heterogeneity on the Stability of Composite Cylindrical Shells under Axial Compression"

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THE left-hand side of the second and third equations in Eqs. (10) should be  $[B]$  and  $[D]$ , respectively. In Table 2 the value of  $v_{12}$  for S994 glass-epoxy composite should be 0.3.

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## Errata: "Observations of Turbulent Reattachment behind an Axisymmetric Downstream-Facing Step in Supersonic Flow"

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IN Fig. 4c, only the data for  $h = 0.25$  and  $1.02$  are for  $M_s = 3.90$ , as labeled; the data for  $h = 1.68$  actually correspond to  $M_s = 4.37$ . This error is repeated in Fig. 8. The data corresponding to  $M_s = 3.90$ ,  $h = 1.68$  may be found in Fig. 9.

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