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MODEL-INDEPENDENT STELLAR AND PLANETARY MASSES FROM MULTI-TRANSITING EXOPLANETARY SYSTEMS

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ABSTRACT

Precise exoplanet characterization requires precise classification of exoplanet host stars. The masses of host stars are commonly estimated by comparing their spectra to those predicted by stellar evolution models. However, spectroscopically determined properties are difficult to measure accurately for stars that are substantially different from the Sun, such as M-dwarfs and evolved stars. Here, we propose a new method to dynamically measure the masses of transiting planets near mean-motion resonances and their host stars by combining observations of transit timing variations with radial velocity (RV) measurements. We derive expressions to analytically determine the mass of each member of the system and demonstrate the technique on the Kepler-18 system. We compare these analytic results to numerical simulations and find that the two are consistent. We identify eight systems for which our technique could be applied if follow-up RV measurements are collected. We conclude that this analysis would be optimal for systems discovered by next-generation missions similar to TESS or PLATO, which will target bright stars that are amenable to efficient RV follow-up.

Key words: methods: analytical - planets and satellites: fundamental parameters - stars: fundamental parameters

1. INTRODUCTION

With modern radial velocity (RV) techniques and the phenomenal success of space-based transit surveys, exoplanetary science has moved from a "stamp-collecting" era of finding individual systems to an era where hundreds of planetary systems are discovered simultaneously (Borucki et al. 2011). Despite these successes, accurate characterization of planets still presents a challenge. In general, uncertainties in the radii and masses of planets are dominated by uncertainties in the radii and masses of their host stars (e.g., Muirhead et al. 2012). Difficulties in characterizing the physical properties of planets are particularly acute for systems discovered by the Kepler space telescope. For many systems, the ratio between the radius of the planet and the radius of its host star is known to within 1 part in 1000 (Batalha et al. 2012). Yet the stellar radii are often not known to better than 10%, meaning that much of the precision of Kepler is lost when estimating planetary properties (Lissauer et al. 2012; Johnson et al. 2012a).

In general, measuring the masses of exoplanet host stars is a model-dependent procedure. For nearby stars with trigonometric parallaxes, one compares the luminosity, effective temperature, and metallicity of a star to stellar evolution model grids (Valenti & Fischer 2005; Johnson et al. 2012b). For stars without measured parallaxes, the stellar density can be measured from the transit light curve and used in place of the luminosity. However, this relies on either the assumption that the planet's orbit is circular—a poor assumption for periods larger than 10 days—or an RV orbital solution (Sozzetti et al. 2007; Dawson & Johnson 2012). The atmospheres and interior structures of stars are also poorly understood for stars that differ substantially from the Sun, complicating their analyses further. Thus, model-independent methods of measuring stellar masses are extremely valuable.

Agol et al. (2005) suggest that in a system with transiting planets, a precise measurement of the transit duration, which depends on stellar density, coupled with RV information and

precise measurements of the scatter in transit times, can provide a unique measurement of the stellar mass. Unfortunately, this strategy requires precise knowledge of the inclination of the system, which from a transit light curve is degenerate with limb-darkening coefficients (Jha et al. 2000), especially for low signal-to-noise transit detections.

The method described by Agol et al. also breaks down for resonant systems, as it assumes that the relative positions of the planets change from transit to transit. Moreover, outside of resonance, transit timing effects are small for all but the largest planets, so this method is not ideal for studying rocky planets. This strategy is successful when the perturbing object is massive, as is the case in circumbinary planets (Doyle et al. 2011; Welsh et al. 2012), but is less promising for studying solar-type systems. It has also been suggested that in a system containing a transiting planet and an exomoon detected through transit timing and duration variations, the stellar mass and radius can be determined directly through dynamical effects (Kipping 2010). While this technique holds future promise, the exomoons required to test this procedure have not yet been detected.

Recently, transit timing variations (TTVs) caused by mutual gravitational interactions of bodies in multiple-planet systems have been detected (Holman et al. 2010; Ford et al. 2012a). These deviations from a linear transit ephemeris allow for an estimate of the ratio of the mass of the perturbing planet to the mass of its star. In cases where multiple planets transit, the ratio of the masses of each planet to the mass of the host star can be estimated (Fabrycky et al. 2012; Steffen et al. 2012b).

In this paper, we propose a method to directly measure stellar and planetary masses for multi-transiting systems by combining an analysis of the transit timing signal caused by planet–planet interactions with Doppler RV measurements. Unlike the technique developed by Agol et al. (2005), our method requires the observed transiting planets to lie near a mean-motion resonance, where transit timing effects are strongest. In Section 2, we explain how TTVs can be combined with RV information to estimate stellar and planetary masses. In Section 3, we apply our process to the well-studied Kepler-18 planetary system and compare the result to both numerical integrations of the system and published stellar evolution models. We find that the scheme is viable, but at present the RV data are insufficient to place meaningful constraints on stellar parameters. In Section 4, we discuss uncertainties and limitations to our method, as well as its applications to systems discovered by *Kepler* and its eventual successors.

2. UNIQUE MASSES AND ERRORS

2.1. Mass Determination from TTVs

Consider a system of two coplanar planets orbiting near (but not exactly at) a first-order mean-motion resonance. The planets have periods P and P' (here and throughout, the unprimed quantity refers to the inner planet and the primed quantity to the outer planet) and orbit their star such that the inner planet completes approximately *j* orbits in the time the outer planet completes j - 1. A nearly edge-on observer will detect both planets transiting their host star. Because of the near commensurability of their periods, the inner planet will pass its companion at nearly the same location each orbit, driving small gravitational interactions that add coherently, inducing a small forced eccentricity on each object. The two planets will therefore not transit their star in an exactly periodic fashion. Instead, a small, sinusoidal departure from periodicity, termed a TTV, will be observed (e.g., Nesvorný et al. 2012). TTVs have been used to detect the presence of nontransiting planets (Ballard et al. 2011; Dawson et al. 2012) and to fully characterize systems when multiple planets transit (Holman et al. 2010; Lissauer et al. 2011). The period of the TTV signal is related to the periods of the planets such that

$$P_{\rm TTV} = \frac{1}{|j/P' - (j-1)/P|}.$$
 (1)

In most cases, the superb photometry provided by the *Kepler* mission allows this quantity to be precisely estimated.

An analytic form for the amplitude of the TTV signal is derived by Lithwick et al. (2012, hereafter L12). The amplitude of the signal depends strongly on the free eccentricity of the system. Here, free eccentricity refers to the component of the eccentricity caused by the initial dynamical conditions of the system, not the component driven by resonant interactions. Without observing a secondary transit, for small planets the free eccentricity is difficult to constrain precisely via photometry. However, many TTV signals have been detected in systems in which the planets have orbital periods of days to weeks.

In this case, the estimated ages of the planets are larger than the expected tidal circularization timescale at their present locations, so their orbits can be expected to have negligible free eccentricity. This can be verified by analyzing the phase of the TTV signal. If the zero points of the TTV signal occur when the longitude of conjunction is parallel to the line of sight, L12 suggest that the free eccentricity can be neglected. In this case, the amplitudes of the TTV signals, V and V', are

$$V = \frac{m'}{M} \left| \frac{f}{\Delta} \right| \frac{P}{\pi j^{2/3} (j-1)^{1/3}}$$
(2)

$$V' = \frac{m}{M} \left| \frac{g}{\Delta} \right| \frac{P'}{\pi j},\tag{3}$$

where *m* and *M* are the planet and stellar mass, Δ is the fractional distance from commensurability, typically of order 0.01, and *f* and *g* are the appropriate coefficients of the disturbing function, which characterize the interactions between the planets. These sums of Laplace coefficients can be calculated by using the information found in Appendix B of Murray & Dermott (1999). Additionally, the values of *f* and *g* for common resonances are listed in L12. To first order, these coefficients are of order unity and depend only weakly on Δ . For systems with TTVs, Equations (2) and (3) enable a unique determination of the planet–star mass ratio, but normally one must rely on stellar models to separate stellar and planetary properties. However, if RV measurements are available, the amplitude of the Doppler signal can be used in conjunction with the TTV information to estimate the masses of the planets and the star.

2.2. Including Radial Velocities

The semiamplitude of an RV Doppler signal is

$$K = \left(\frac{2\pi G}{P}\right)^{1/3} \frac{m}{(M+m)^{2/3}} \frac{\sin i}{\sqrt{1-e^2}},\tag{4}$$

with *i* and *e* being the inclination and eccentricity, respectively (Paddock 1913). Despite the lack of free eccentricity, we may expect a small forced eccentricity as a result of threebody interactions. The magnitude of this forced eccentricity is ≤ 0.05 , so neglecting it will induce an error of $\leq 0.1\%$ in our semiamplitude calculation. An error of the same magnitude but in the opposite direction is induced by assuming $i = 90^\circ$, since a strong constraint on the inclination is provided by our requirement of a transit.

Thus, neglecting eccentricity and assuming an edge-on orbit, in the limit where $m \ll M$ the RV semiamplitude can be approximated as

$$K = \left(\frac{2\pi G}{P}\right)^{1/3} \frac{m}{M^{2/3}},$$
 (5)

and the RV can be modeled as

$$v(t) = -K \sin\left(\frac{2\pi(t-t_c)}{P}\right),\tag{6}$$

with t_c being the time of transit center. Again, a degeneracy exists between the planet and stellar mass, so stellar models must be invoked. However, the degeneracy is different from the one recovered from TTVs, so these two expressions taken together can be used to solve for the planet and stellar masses individually. This allows for two independent measurements of the mass of the star and one unique measurement of the mass of each planet. The mass of the star is

$$M = \left[\frac{P P^{3} g^{3}}{2\pi^{4} G \Delta^{3} j^{3}}\right] \frac{K^{3}}{V^{3}}$$
(7)

$$= \left[\frac{P'P^3f^3}{2\pi^4 G\Delta^3 j^2(j-1)}\right] \frac{K'^3}{V^3},$$
 (8)

and the mass of each planet is

$$m = \frac{P^3}{2\pi G} \left(\frac{P'g}{\Delta \pi j}\right)^2 \frac{K^3}{V'^2} \tag{9}$$

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$$m' = \frac{P'^3}{2\pi G} \left(\frac{Pf}{\Delta \pi j^{2/3} (j-1)^{1/3}}\right)^2 \frac{K'^3}{V^2}.$$
 (10)

Simply put, for a given system of two coplanar planets, the constants $M^{1/3}V'K^{-1}$ and $M^{1/3}VK'^{-1}$ depend only on the system architecture. Thus, by precisely measuring the RV semiamplitude and magnitude of the TTV signal, the stellar mass can be directly estimated. Because of *Kepler*'s exceptional photometry, the periods of each planet and terms derived from these (such as Δ) are well known. Thus, we expect the errors in the mass estimates to be dominated by the errors in V and K and neglect the errors caused by other terms. In this case,

$$\left(\frac{\delta M}{M}\right)^2 = \left(3\frac{\delta K}{K}\right)^2 + \left(3\frac{\delta V'}{V'}\right)^2$$
$$= \left(3\frac{\delta K'}{K'}\right)^2 + \left(3\frac{\delta V}{V}\right)^2 \tag{11}$$

$$\left(\frac{\delta m}{m}\right)^2 = \left(3\frac{\delta K}{K}\right)^2 + \left(2\frac{\delta V'}{V'}\right)^2 \tag{12}$$

$$\left(\frac{\delta m'}{m'}\right)^2 = \left(3\frac{\delta K'}{K'}\right)^2 + \left(2\frac{\delta V}{V}\right)^2,\tag{13}$$

where we expect the covariant terms to be zero since K and V are independently measured quantities. Here, the fractional uncertainties depend quite sensitively on the ability to measure K and V. Typically for systems of multi-transiting planets, only one of these quantities is well measured. Therefore, we would expect to only weakly constrain the stellar masses at present; with more observations the constraints will tighten considerably. In the limit where $m \gg m'$, K and V' are much larger than their counterparts and can be more easily constrained. Thus, when one planet is substantially more massive than its companion, one stellar mass measurement will be considerably more precise than the other and the mass of the more massive planet will be better constrained than that of the less massive planet. In the case where $m \approx m'$, both measurements are expected to have similar uncertainties.

3. EXAMPLE

Kepler-18 (KOI 137, KIC 8644288) is a planetary system containing three nearly coplanar planets with 3.5, 7.6, and 14.9 day periods orbiting a 0.97 M_{\odot} star (Cochran et al. 2011, hereafter C11). These planets (137.03, 137.01, and 137.02, or Kepler-18 b, c, and d, respectively) were confirmed by a combination of transit timing and RV measurements. The star has been observed using the *Kepler* short-cadence mode nearly continuously for two years, allowing for precise measurements of transit times over dozens of transits. Moreover, 18 RV measurements of this $K_p = 13.5$ star, where K_p is the apparent magnitude in the *Kepler* bandpass, have been collected over the past three years by the California Planet Search team with the Keck 1 High Resolution Echelle Spectrometer (HIRES). Thus, enough data exist to attempt to determine the mass of each member of this system dynamically.

We first fit a limb-darkened light curve to a series of phasefolded transits to estimate the observable transit parameters, such as the impact parameter and limb-darkening coefficients, following the OCCULTQUAD routine developed by Mandel & Agol (2002). Because of the high signal-to-noise ratio of these observations and the one-minute integration times, transit parameters can be easily measured from individual transits: we find no significant difference in these parameters or their uncertainties when fitting one individual transit instead of fitting a phase-folded transit.

Once the shape of the light curve is modeled, we fit a curve of this shape to each individual transit, allowing only the time of transit center to vary. Each individual transit light curve consists of over 200 in-transit data points, allowing for measurements of the transit center time to sub-minute precision. We remove from our data set transits that occur simultaneously with the transit of another planet. As expected, the transits follow a sinusoidal deviation from a linear ephemeris; these deviations, as shown in Table 1, appear to be anti-correlated between the two planets.

For our method to provide meaningful mass estimates, the primordial (free) eccentricity of the system must be damped on a timescale shorter than the age of the system. As explained in L12, if the zero points of the TTVs occur at the times at which the longitude of conjunction of the planets is equal to 0° or 180° , then the system is likely to have negligible free eccentricity. We check the phase of these TTVs by fitting each TTV curve independently to a sinusoid. We determine parameters of this sinusoid and their uncertainties by minimizing the χ^2 statistic through a Levenberg-Marquardt algorithm. Additionally, we allow for a vertical offset to the sine function in the fit (indicative of a miscalculated time of transit center t_c) and also a linear trend (indicative of a miscalculated orbital period). The results of this minimization can be found in Table 2. Both planets are consistent with having zero free eccentricity and anticorrelated TTV signals. From these parameters, we measure a fractional distance from commensurability $\Delta = -2.776 \times 10^{-2}$ and find the coefficients of the disturbing function to be f = -1.251 and g = 0.5308. The amplitude of the TTV signals for Kepler-18 c and d can be measured to within 3.3% and 6.8%, respectively.

These results can then be combined with RV measurements in order to uniquely constrain the stellar and planetary masses. C11 used 14 RV measurements to confirm this system; we analyze these data plus four additional observations collected between 2012 July 1 and 2012 August 1, all of which are provided in Table 3.

The large uncertainties in each individual observation, coupled with the small number of observations relative to the number of observed transits, suggest that our mass uncertainties will be dominated by uncertainties in the RV semiamplitude. In fact, many different solutions fit the RV data satisfactorily. As an example, C11 fit a larger RV semiamplitude for planet d than c, despite the fact that they find planet c to be both more massive and nearer the star than planet d. The analysis is complicated by the existence of the much smaller planet b orbiting inside the other two planets. In this case, we invoke one additional piece of information. Equations (2) and (3) can be combined to solve for the mass ratio of the resonant planets,

$$\frac{m'}{m} = \frac{P}{P'} \frac{f}{g} \frac{V'}{V} \left(\frac{j}{j-1}\right)^{1/3},$$
(14)

which in this case implies $m'/m = 1.22 \pm 0.09$, where m' refers to planet c and m to planet d. This can be applied as an additional constraint in the RV fit. In the case where $\sigma_{RV} \ll \sigma_{TTV}$, an equivalent mass ratio constraint, derived from the RV semiamplitude ratio, can be applied to the TTV fit.

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633.8837

641.5253

664.4500

672.0915

679.7331

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-0.0028

-0.0042

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-0.0025

-0.0029

-0.0029

-0.0004

 Table 1

 Transit Times for Kepler Transiting Planet Candidates

Table 1

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$\begin{split} BID = -2.45.900 & (days) & (days) \\ IPS. 3142 & -0.0006 & 0.0012 & I37.01 & 71 & 740.8657 & 0.0006 & 0.0014 \\ 215.3973 & 0.0019 & 0.0018 & I37.01 & 72 & 748.507 & 0.0006 & 0.0014 \\ 215.3973 & 0.0019 & 0.0018 & I37.01 & 73 & 756.1488 & 0.0014 & 0.0017 \\ 228.5820 & 0.0014 & 0.0015 & I37.01 & 74 & 763.794 & 0.0049 & 0.0017 \\ 228.522 & 0.0014 & 0.0015 & I37.01 & 75 & 771.4320 & 0.0013 & 0.0012 \\ 24.6520 & 0.0031 & 0.0011 & I37.01 & 76 & 779.0755 & 0.0033 & 0.0012 \\ 254.522 & 0.0034 & 0.0011 & I37.01 & 77 & 786.7151 & 0.0021 & 0.0011 \\ 254.052 & 0.0030 & 0.0011 & I37.01 & 78 & 794.3567 & 0.0033 & 0.0012 \\ 257.083 & 0.0055 & 0.0018 & I37.01 & 78 & 794.3567 & 0.0033 & 0.0012 \\ 257.083 & 0.0055 & 0.0018 & I37.01 & 78 & 890.6398 & 0.0029 & 0.0046 \\ 247.0546 & 0.0028 & 0.0012 & I37.01 & 80 & 890.6398 & 0.0029 & 0.0016 \\ 297.0546 & 0.0028 & 0.0012 & I37.01 & 81 & 817.2814 & 0.0038 & 0.0012 \\ 297.0546 & 0.0028 & 0.0011 & I37.02 & 2 & 24.6011 & -0.0025 & 0.0016 \\ 312.3977 & 0.0026 & 0.0011 & I37.02 & 3 & 239.4600 & -0.0037 & 0.0010 \\ 328.2209 & 0.0018 & 0.0011 & I37.02 & 4 & 243.189 & -0.0029 & 0.0010 \\ 328.2209 & 0.0018 & 0.0011 & I37.02 & 7 & 298.8958 & -0.0040 & 0.0011 \\ 351.564 & 0.0001 & 0.0011 & I37.02 & 7 & 298.8958 & -0.0040 & 0.0011 \\ 352.6763 & 0.0003 & 0.0011 & I37.02 & 13 & 338.4754 & -0.0023 & 0.0012 \\ 358.7871 & -0.0027 & 0.0014 & I37.02 & 13 & 338.4754 & -0.0023 & 0.0012 \\ 364.287 & -0.0027 & 0.0014 & I37.02 & 12 & 373.1905 & 0.0017 & 0.0023 \\ 364.6287 & -0.0027 & 0.0011 & I37.02 & 12 & 373.1905 & 0.0017 & 0.0023 \\ 364.6287 & -0.0027 & 0.0011 & I37.02 & 12 & 373.1905 & 0.0013 & 0.0012 \\ 374.073 & -0.0033 & 0.0011 & I37.02 & 12 & 373.1905 & 0.0013 & 0.0012 \\ 364.636 & -0.0033 & 0.0011 & I37.02 & 12 & 373.1905 & 0.0013 & 0.0012 \\ 364.636 & -0.0033 & 0.0011 & I37.02 & 12 & 373.1905 & 0.0013 & 0.0012 \\ 442.5444 & -0.0019 & 0.0012 & I37.02 & 13 & 356.638 & -0.0033 & 0.0010 \\ 364.6354 & -0.0028 & 0.0011 & I37.02 & 12 & 556.5567 & -0.0033 & 0.0011 \\ 374.073 & -0.0035 & 0.0011 & I37.02 & 25 & 566.5567 & -0.0033 &$	t _n	TTV _n	σ_n	KOI	n	t_n	TTV _n	σ_n	
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228.8804 0.0021 0.0017 137.01 75 771.4320 0.0011 0.0012 226.5220 0.0014 0.0011 137.01 77 778.751 0.0031 0.0011 251.6052 0.0037 0.0012 137.01 78 794.3567 0.0031 0.0012 259.4467 0.0037 0.0012 137.01 79 801.9982 0.0039 0.0012 274.7299 0.0041 0.0012 137.01 80 899.6398 0.0029 0.0011 280.0130 0.0037 0.0012 137.01 82 824.9229 0.0016 0.0012 290.0130 0.0037 0.0018 137.02 1 209.7421 -0.0012 0.0011 305.2961 0.0034 0.0011 137.02 3 239.4600 -0.0037 0.0010 312.9377 0.0026 0.0011 137.02 7 298.858 -0.0032 0.0011 313.764 -0.0025 0.0012 137.02 7 298.858 </td <td>221.2389</td> <td>0.0017</td> <td>0.0010</td> <td>137.01</td> <td>74</td> <td>763.7904</td> <td>0.0049</td> <td>0.0017</td>	221.2389	0.0017	0.0010	137.01	74	763.7904	0.0049	0.0017	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	228.8804	0.0021	0.0017	137.01	75	771.4320	0.0011	0.0016	
244,1636 0.0031 0.0011 137.01 77 786,7151 0.0021 0.00011 251,8052 0.0030 0.0012 137.01 78 794,3557 0.0033 0.0012 267,0883 0.0050 0.0012 137.01 80 809,6398 0.0029 0.0014 274,729 0.0041 0.0012 137.01 81 817.2814 0.0038 0.0011 290,0130 0.0035 0.0018 137.02 1 209,7421 -0.0012 0.0010 290,6130 0.0034 0.0011 137.02 2 224,6011 -0.0037 0.0016 312,9377 0.0026 0.0011 137.02 3 239,4600 -0.0037 0.0016 312,9377 0.0026 0.0011 137.02 7 298,8958 -0.0040 0.0011 351,1456 0.0001 0.0012 137.02 11 358,315 -0.0008 0.0012 374,070 -0.0033 0.0014 137.02 14 402,9	236.5220	0.0014	0.0015	137.01	76	779.0735	0.0033	0.0012	
251 0.0030 0.0011 137.01 78 794.3567 0.0031 0.00012 259.4467 0.0037 0.0012 137.01 80 809.6398 0.0029 0.0014 247.0883 0.0050 0.0012 137.01 81 817.2814 0.0038 0.0011 252.3714 0.0037 0.0018 137.02 0 194.8832 0.0000 0.0010 297.654 0.0034 0.0011 137.02 2 224.6011 -0.0025 0.0010 312.9377 0.0066 0.0011 137.02 4 254.3189 -0.0037 0.0010 320.5793 0.0013 0.0011 137.02 7 298.8958 -0.0040 0.0011 351.862 0.0008 0.0012 137.02 9 328.6168 -0.0033 0.0011 351.871 -0.0001 0.0011 137.02 14 343.4726 -0.0005 0.0017 358.7871 -0.0033 0.0011 137.02 15 417.7673 </td <td>244.1636</td> <td>0.0031</td> <td>0.0011</td> <td>137.01</td> <td>77</td> <td>786.7151</td> <td>0.0021</td> <td>0.0011</td>	244.1636	0.0031	0.0011	137.01	77	786.7151	0.0021	0.0011	
259,4467 0.0037 0.0012 137.01 79 801.9982 0.0039 0.0012 267.0883 0.0050 0.0012 137.01 80 809.6398 0.0029 0.0014 274.7299 0.0041 0.0012 137.01 81 817.2814 0.0038 0.0012 290.0130 0.0035 0.0018 137.02 1 209.7421 -0.0012 0.0011 305.2961 0.0034 0.0011 137.02 2 224.6001 -0.0025 0.0016 312.9377 0.0026 0.0011 137.02 4 254.3189 -0.0029 0.0011 351.455 0.0008 0.0015 137.02 7 298.8958 -0.0040 0.0011 351.455 0.0001 0.0011 137.02 9 323.6136 -0.0023 0.0012 374.0703 -0.0033 0.0014 137.02 13 388.014 -0.0036 0.0017 39.353 -0.0025 0.0011 137.02 14 402.9083	251.8052	0.0030	0.0011	137.01	78	794.3567	0.0031	0.0012	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	259.4467	0.0037	0.0012	137.01	79	801.9982	0.0039	0.0012	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	267.0883	0.0050	0.0012	137.01	80	809.6398	0.0029	0.0014	
282.3714 0.0037 0.0018 137.01 82 824.9229 0.0016 0.0012 290.0130 0.0035 0.0018 137.02 0 194.8832 0.0000 0.0011 305.2961 0.0034 0.0011 137.02 2 224.6011 -0.0025 0.0010 312.9377 0.0026 0.0011 137.02 3 239.4600 -0.0025 0.0010 320.5793 0.0018 0.0012 137.02 4 254.3189 -0.0029 0.0011 355.8624 0.0008 0.0011 137.02 7 288.988 -0.0040 0.0013 355.8624 0.0006 0.0011 137.02 9 328.6136 -0.0023 0.0023 358.7871 -0.0025 0.0014 137.02 11 358.8315 0.0008 0.0017 364.4287 -0.0025 0.0011 137.02 13 388.0494 0.0036 0.0017 381.7119 -0.0024 0.0011 137.02 14	274.7299	0.0041	0.0012	137.01	81	817.2814	0.0038	0.0011	
290.0130 0.0035 0.0018 137.02 0 194.8832 0.0000 0.0010 297.6546 0.0028 0.0011 137.02 1 209.7421 -0.0012 0.0011 305.2961 0.0034 0.0011 137.02 2 224.6011 -0.0025 0.0013 305.2961 0.0013 0.0011 137.02 4 254.3189 -0.0029 0.0010 328.2209 0.0018 0.0012 137.02 6 284.0368 -0.0032 0.0011 351.456 0.00001 0.0011 137.02 8 313.7547 -0.0013 0.0011 356.4287 -0.0027 0.0014 137.02 11 358.315 0.0008 0.0017 374.0703 -0.0025 0.0011 137.02 13 388.0494 0.0020 0.0017 389.3534 -0.0025 0.0011 137.02 14 402.9083 0.0029 0.0011 404.6366 -0.0036 0.0013 137.02 15<	282.3714	0.0037	0.0018	137.01	82	824,9229	0.0016	0.0012	
297.6546 0.0028 0.0012 137.02 1 209.7421 -0.0012 0.0011 305.2961 0.0034 0.0011 137.02 2 224.6011 -0.0025 0.0010 312.9377 0.0026 0.0011 137.02 3 239.4600 -0.0037 0.0012 328.2209 0.0018 0.0012 137.02 7 298.8958 -0.0040 0.0013 355.8624 0.0006 0.0011 137.02 7 298.8958 -0.0040 0.0013 358.7871 -0.00050 0.0012 137.02 9 328.6136 -0.0033 0.0014 37.02 10 343.4726 -0.0005 0.0011 37.02 12 37.3105 0.0017 0.0013 381.719 -0.0024 0.0011 137.02 13 388.0494 0.0036 0.0010 396.9950 -0.0033 0.0011 137.02 14 402.9083 0.0029 0.0011 404.6366 -0.0036 0.001	290.0130	0.0035	0.0018	137.02	0	194.8832	0.0000	0.0010	
305.2961 0.0034 0.0011 137.02 2 224.6011 -0.0025 0.0010 312.9377 0.0026 0.0011 137.02 3 239.4600 -0.0037 0.0010 320.5793 0.0013 0.0011 137.02 4 254.3189 -0.0029 0.0013 335.8624 0.0008 0.0015 137.02 7 298.8958 -0.0013 0.0011 351.1456 0.0001 0.0011 137.02 8 313.7547 -0.0013 0.0012 366.4287 -0.0027 0.0014 137.02 10 343.4726 -0.0005 0.0011 374.0703 -0.0024 0.0011 137.02 13 388.0494 0.0036 0.0017 389.3534 -0.0025 0.0011 137.02 14 402.9083 0.0029 0.0011 412.2781 -0.0046 0.0012 137.02 16 432.6262 0.0008 0.0012 419.9197 -0.0038 0.0015 137.02 <	297 6546	0.0028	0.0012	137.02	1	209 7421	-0.0012	0.0011	
312.937 0.0026 0.0011 137.02 3 239.4600 -0.0037 0.0010 320.5793 0.0018 0.0011 137.02 4 254.3189 -0.0029 0.0010 328.229 0.0018 0.0012 137.02 6 228.40368 -0.0023 0.0011 358.787 -0.0005 0.0012 137.02 8 313.7547 -0.0013 0.0012 358.787 -0.0005 0.0012 137.02 9 328.6136 -0.0023 0.0023 366.4287 -0.0027 0.0014 137.02 10 343.4726 -0.0005 0.0011 374.0703 -0.0033 0.0011 137.02 13 388.0494 0.0036 0.0012 381.7119 -0.0024 0.0011 137.02 14 402.9083 0.0029 0.0011 396.995 -0.0036 0.0013 137.02 17 447.4852 0.0008 0.0012 412.917 -0.0037 0.011 137.02 17 447.4852 0.0008 0.0011 425.5028 -0.0039 <td>305 2961</td> <td>0.0034</td> <td>0.0011</td> <td>137.02</td> <td>2</td> <td>224 6011</td> <td>-0.0025</td> <td>0.0010</td>	305 2961	0.0034	0.0011	137.02	2	224 6011	-0.0025	0.0010	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	312 9377	0.0026	0.0011	137.02	3	239 4600	-0.0023	0.0010	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	320 5793	0.0013	0.0011	137.02	4	254 3189	-0.0029	0.0010	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	328.2200	0.0015	0.0011	137.02	6	284.0368	-0.0022	0.0010	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	335 8624	0.0008	0.0012	137.02	7	204.0500	-0.0040	0.0011	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	351.1456	0.0008	0.0013	137.02	8	298.8958	-0.0040	0.0011	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	259 7971	0.0001	0.0011	137.02	0	228 6126	-0.0013	0.0010	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	266 1297	-0.0003	0.0012	137.02	9	242 4726	-0.0023	0.0023	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	300.4287	-0.0027	0.0014	137.02	10	343.4720	-0.0003	0.0011	
381.7119 -0.0024 0.0011 137.02 12 373.1905 0.0017 0.0017 389.3534 -0.0025 0.0011 137.02 14 402.9083 0.0029 0.0011 404.6366 -0.0036 0.0011 137.02 15 417.7673 0.0020 0.0011 412.2781 -0.0046 0.0012 137.02 16 432.6262 0.0008 0.0011 419.9197 -0.0037 0.0011 137.02 18 462.3441 0.0008 0.0011 425.813 -0.0038 0.0013 137.02 19 477.2030 -0.0001 0.0011 435.2028 -0.0013 0.0011 137.02 20 492.0620 0.00020 0.0011 435.2028 -0.0013 0.0011 137.02 23 536.6388 -0.0024 0.0016 450.4860 -0.0017 0.0011 137.02 25 566.3567 -0.0033 0.0016 473.4107 0.0005 0.0013 137.02 27 $596.$	3/4.0/03	-0.0033	0.0014	137.02	11	336.3313	0.0008	0.0009	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	381./119	-0.0024	0.0011	137.02	12	373.1905	0.0017	0.0012	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	389.3534	-0.0025	0.0011	137.02	13	388.0494	0.0036	0.0010	
404.6366 -0.0036 0.0013 137.02 15 417.1673 0.0020 0.0012 412.2781 -0.0046 0.0012 137.02 16 432.6262 0.0008 0.0011 427.5613 -0.0038 0.0015 137.02 17 447.4852 0.0008 0.0011 427.5613 -0.0039 0.0013 137.02 18 462.3441 0.0008 0.0011 435.2028 -0.0039 0.0012 137.02 19 477.2030 -0.0001 0.0011 442.8444 -0.0019 0.0012 137.02 20 492.0620 0.00022 0.0012 450.4860 -0.0017 0.0011 137.02 22 521.7799 -0.0024 0.0016 455.6919 -0.0008 0.0015 137.02 23 536.6388 -0.0038 0.0016 473.4107 0.0005 0.0013 137.02 24 551.4977 -0.0033 0.0016 488.6938 0.0026 0.0014 137.02 26 581.2156 -0.0033 0.0016 496.3354 0.0027 0.0013 137.02 31 655.5103 0.0022 0.0016 511.6186 0.0038 0.0011 137.02 32 670.3693 0.0015 0.0016 519.2501 0.0032 0.0014 137.02 34 700.0871 -0.0011 0.0016 549.433 0.0034 0.0010 137.02 36 729.8050 -0.0019 0.0016 </td <td>396.9950</td> <td>-0.0033</td> <td>0.0011</td> <td>137.02</td> <td>14</td> <td>402.9083</td> <td>0.0029</td> <td>0.0011</td>	396.9950	-0.0033	0.0011	137.02	14	402.9083	0.0029	0.0011	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	404.6366	-0.0036	0.0013	137.02	15	417.7673	0.0020	0.0010	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	412.2781	-0.0046	0.0012	137.02	16	432.6262	0.0008	0.0012	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	419.9197	-0.0037	0.0011	137.02	17	447.4852	0.0008	0.0011	
435.2028 -0.0039 0.0013 137.02 19 477.2030 -0.0001 0.0001 442.8444 -0.0019 0.0012 137.02 20 492.0620 0.0002 0.0011 450.4860 -0.0013 0.0011 137.02 21 506.9209 -0.0023 0.0011 458.1276 -0.0017 0.0010 137.02 22 521.7799 -0.0024 0.0010 465.7691 -0.0008 0.0015 137.02 23 536.6388 -0.0038 0.0010 473.4107 0.0005 0.0013 137.02 24 551.4977 -0.0035 0.0010 481.0523 0.0016 0.0011 137.02 25 566.3567 -0.0033 0.0011 486.6938 0.0026 0.0014 137.02 27 596.0746 -0.0013 0.0015 503.9770 0.0030 0.0014 137.02 23 670.3693 0.0015 0.0015 511.6186 0.0038 0.0011 137.02 31 655.5103 0.0032 0.0014 519.2601 0.0032 0.0013 137.02 33 685.2282 0.0026 0.0009 534.5433 0.0055 0.0013 137.02 35 714.9461 0.0008 0.0010 549.8264 0.0025 0.0014 137.02 37 744.6640 -0.0012 0.0011 577.4680 0.0049 0.0021 137.02 37 744.6640 -0.0027 0.0011 580.3927	427.5613	-0.0038	0.0015	137.02	18	462.3441	0.0008	0.0011	
442.8444 -0.0019 0.0012 137.02 20 492.0620 0.0002 0.0010 450.4860 -0.0013 0.0011 137.02 21 506.9209 -0.0023 0.0011 458.1276 -0.0017 0.0010 137.02 22 521.7799 -0.0024 0.0010 455.7691 -0.0008 0.0015 137.02 23 536.6388 -0.0038 0.0010 473.4107 0.0005 0.0013 137.02 24 551.4977 -0.0035 0.0010 481.0523 0.0016 0.0011 137.02 25 566.3567 -0.0033 0.0011 488.6938 0.0026 0.0014 137.02 26 581.2156 -0.0033 0.0016 496.3354 0.0027 0.0015 137.02 29 625.7924 0.0020 0.0016 503.9770 0.0030 0.0014 137.02 31 655.5103 0.0032 0.0014 511.6186 0.0032 0.0013 137.02 32 670.3693 0.0015 0.0014 526.9017 0.0052 0.0013 137.02 34 700.0871 -0.0011 0.0014 542.1848 0.0034 0.0010 137.02 35 714.9461 0.0008 0.0016 557.4680 0.0049 0.0021 137.02 37 744.6640 -0.0012 0.0011 557.4680 0.0035 0.0011 137.02 37 744.6640 -0.0034 0.0016 <td>435.2028</td> <td>-0.0039</td> <td>0.0013</td> <td>137.02</td> <td>19</td> <td>477.2030</td> <td>-0.0001</td> <td>0.0011</td>	435.2028	-0.0039	0.0013	137.02	19	477.2030	-0.0001	0.0011	
450.4860 -0.0013 0.0011 137.02 21 506.9209 -0.0023 0.0011 458.1276 -0.0017 0.0010 137.02 22 521.7799 -0.0024 0.0010 465.7691 -0.0008 0.0015 137.02 23 536.6388 -0.0038 0.0010 473.4107 0.0005 0.0013 137.02 24 551.4977 -0.0035 0.0010 481.0523 0.0016 0.0014 137.02 25 566.3567 -0.0033 0.0016 496.3354 0.0027 0.0015 137.02 27 596.0746 -0.0013 0.0015 503.9770 0.0030 0.0014 137.02 29 625.7924 0.0020 0.0016 511.6186 0.0038 0.0011 137.02 31 655.5103 0.0032 0.0014 512.69017 0.0052 0.0013 137.02 32 670.3693 0.0015 0.0016 544.5433 0.0055 0.0013 137.02 34 700.0871 -0.0011 0.0011 542.98264 0.0025 0.0014 137.02 35 714.9461 0.0008 0.0012 57.4680 0.0049 0.0021 137.02 37 744.6640 -0.0012 0.0011 572.7511 0.0035 0.0011 137.02 39 774.3818 -0.0030 0.0012 580.3927 0.0017 0.0016 137.02 40 789.2408 -0.0034 0.0012 <td>442.8444</td> <td>-0.0019</td> <td>0.0012</td> <td>137.02</td> <td>20</td> <td>492.0620</td> <td>0.0002</td> <td>0.0010</td>	442.8444	-0.0019	0.0012	137.02	20	492.0620	0.0002	0.0010	
458.1276 -0.0017 0.0010 137.02 22 521.7799 -0.0024 0.0010 465.7691 -0.0008 0.0015 137.02 23 536.6388 -0.0038 0.0010 473.4107 0.0005 0.0013 137.02 24 551.4977 -0.0035 0.0010 481.0523 0.0016 0.0011 137.02 25 566.3567 -0.0033 0.0011 488.6938 0.0026 0.0014 137.02 26 581.2156 -0.0033 0.0015 496.3354 0.0027 0.0015 137.02 27 596.0746 -0.0013 0.0015 503.9770 0.0030 0.0014 137.02 29 625.7924 0.0020 0.0014 511.6186 0.0038 0.0011 137.02 31 655.5103 0.0032 0.0014 519.2601 0.0032 0.0013 137.02 32 670.3693 0.0015 0.0011 526.9017 0.0052 0.0013 137.02 33 685.2282 0.0026 0.0009 534.5433 0.0055 0.0013 137.02 34 700.0871 -0.0011 0.0016 549.8264 0.0025 0.0014 137.02 35 714.9461 0.0008 0.0016 557.4680 0.0049 0.0021 137.02 38 759.5229 -0.0027 0.0011 572.7511 0.0035 0.0012 137.02 40 789.2408 -0.0034 0.0016 <	450.4860	-0.0013	0.0011	137.02	21	506.9209	-0.0023	0.0011	
465.7691 -0.0008 0.0015 137.02 23 536.6388 -0.0038 0.0010 473.4107 0.0005 0.0013 137.02 24 551.4977 -0.0035 0.0010 481.0523 0.0016 0.0011 137.02 25 566.3567 -0.0033 0.0011 486.6938 0.0026 0.0014 137.02 25 566.3567 -0.0033 0.0010 496.3354 0.0027 0.0015 137.02 27 596.0746 -0.0013 0.0016 503.9770 0.0030 0.0014 137.02 29 625.7924 0.0020 0.0014 511.6186 0.0038 0.0011 137.02 31 655.5103 0.0032 0.0014 519.2601 0.0032 0.0013 137.02 32 670.3693 0.0015 0.0011 526.9017 0.0052 0.0013 137.02 34 700.0871 -0.0011 0.0011 542.1848 0.0034 0.0010 137.02 35 714.9461 0.0008 0.0016 549.8264 0.0025 0.0014 137.02 37 744.6640 -0.0012 0.0011 577.4680 0.0035 0.0011 137.02 38 759.5229 -0.0027 0.0011 580.3927 0.0017 0.0012 137.02 39 774.3818 -0.0030 0.0012 580.3927 0.0017 0.0016 137.02 40 789.2408 -0.0034 0.0016 <	458.1276	-0.0017	0.0010	137.02	22	521.7799	-0.0024	0.0010	
473.4107 0.0005 0.0013 137.02 24 551.4977 -0.0035 0.0010 481.0523 0.0016 0.0011 137.02 25 566.3567 -0.0033 0.0011 488.6938 0.0026 0.0014 137.02 26 581.2156 -0.0033 0.0016 496.3354 0.0027 0.0015 137.02 27 596.0746 -0.0013 0.0015 503.9770 0.0030 0.0014 137.02 29 625.7924 0.0020 0.0016 511.6186 0.0038 0.0011 137.02 31 655.5103 0.0032 0.0014 519.2601 0.0032 0.0013 137.02 32 670.3693 0.0015 0.0014 526.9017 0.0052 0.0013 137.02 33 685.2282 0.0026 0.0009 534.5433 0.0055 0.0013 137.02 34 700.0871 -0.0011 0.0016 549.8264 0.0025 0.0014 137.02 35 714.9461 0.0008 0.0016 557.4680 0.0049 0.0021 137.02 37 744.6640 -0.0012 0.0011 572.7511 0.0035 0.0011 137.02 38 759.5229 -0.0027 0.0016 580.3927 0.0017 0.0016 137.02 40 789.2408 -0.0034 0.0016 580.343 0.0034 0.0016 137.02 41 804.0997 -0.0052 0.0016 <td>465.7691</td> <td>-0.0008</td> <td>0.0015</td> <td>137.02</td> <td>23</td> <td>536.6388</td> <td>-0.0038</td> <td>0.0010</td>	465.7691	-0.0008	0.0015	137.02	23	536.6388	-0.0038	0.0010	
481.0523 0.0016 0.0011 137.02 25 566.3567 -0.0033 0.0011 488.6938 0.0026 0.0014 137.02 26 581.2156 -0.0033 0.0016 496.3354 0.0027 0.0015 137.02 27 596.0746 -0.0013 0.0015 503.9770 0.0030 0.0014 137.02 29 625.7924 0.0020 0.0016 511.6186 0.0038 0.0011 137.02 31 655.5103 0.0032 0.0014 519.2601 0.0032 0.0013 137.02 32 670.3693 0.0015 0.0015 526.9017 0.0052 0.0013 137.02 33 685.2282 0.0026 0.0009 534.5433 0.0055 0.0013 137.02 34 700.0871 -0.0011 0.0011 542.1848 0.0034 0.0010 137.02 35 714.9461 0.0008 0.0010 557.4680 0.0049 0.0021 137.02 37 744.6640 -0.0012 0.0011 565.1095 0.0035 0.0011 137.02 38 759.5229 -0.0027 0.0011 572.7511 0.0030 0.0012 137.02 39 774.3818 -0.0034 0.0010 580.3927 0.0017 0.0016 137.02 40 789.2408 -0.0034 0.0016 595.6758 0.0013 0.0011 137.02 41 804.0997 -0.0052 0.0013 <td>473.4107</td> <td>0.0005</td> <td>0.0013</td> <td>137.02</td> <td>24</td> <td>551.4977</td> <td>-0.0035</td> <td>0.0010</td>	473.4107	0.0005	0.0013	137.02	24	551.4977	-0.0035	0.0010	
488.6938 0.0026 0.0014 137.02 26 581.2156 -0.0033 0.0010 496.3354 0.0027 0.0015 137.02 27 596.0746 -0.0013 0.0015 503.9770 0.0030 0.0014 137.02 29 625.7924 0.0020 0.0010 511.6186 0.0038 0.0011 137.02 31 655.5103 0.0032 0.0014 519.2601 0.0032 0.0013 137.02 32 670.3693 0.0015 0.0011 526.9017 0.0052 0.0013 137.02 33 685.2282 0.0026 0.0009 534.5433 0.0055 0.0013 137.02 34 700.0871 -0.0011 0.0011 542.1848 0.0034 0.0010 137.02 35 714.9461 0.0008 0.0010 549.8264 0.0025 0.0014 137.02 36 729.8050 -0.0019 0.0010 557.4680 0.0049 0.0021 137.02 37 744.6640 -0.0012 0.0011 565.1095 0.0035 0.0011 137.02 38 759.5229 -0.0027 0.0011 572.7511 0.0030 0.0012 137.02 40 789.2408 -0.0034 0.0010 580.3927 0.0017 0.0016 137.02 41 804.0997 -0.0052 0.0016 595.6758 0.0013 0.0011 137.02 42 818.9587 0.0003 0.0013 <td>481.0523</td> <td>0.0016</td> <td>0.0011</td> <td>137.02</td> <td>25</td> <td>566.3567</td> <td>-0.0033</td> <td>0.0011</td>	481.0523	0.0016	0.0011	137.02	25	566.3567	-0.0033	0.0011	
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610.9590 -0.0006 0.0012 618.6005 -0.0019 0.0012 626.2421 0.0015 0.0016	595 6758	0.0013	0.0011	137.02	42	818 9587	0.0003	0.0013	
618.6005 -0.0019 $0.0012626.2401$ 0.0015 0.0016 With this additional constraint, we model the PVs as the sum	610 9590	-0.0006	0.0012			0100000	0.0000	0.0015	
226 2411 0.0015 0.0016 With this additional constraint, we model the DVs as the sum	618 6005	-0.0019	0.0012						
	626 2421	_0.0015	0.0012	With t	his additid	onal constraint we ma	odel the RVs a	s the sum	

With this additional constraint, we model the RVs as the sum of three sinusoids of the form of Equation (6), with three free parameters: the semiamplitude of one of the resonant planets (c or d; here, we fit c), the semiamplitude of the innermost planet b, and an offset term, γ . We find the best-fitting parameters to be $K_c = 6.89 \pm 1.40$ m s⁻¹, $K_b = 4.18 \pm 2.14$ m s⁻¹, and $\gamma = 1.30 \pm 1.45$ m s⁻¹. From the mass ratio above, this implies a semiamplitude for planet d of $K_d = 4.52\pm0.97$ m s⁻¹. We now have enough information to estimate the stellar and planetary masses; these results are shown in Table 4.

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	Table 2		
TTV Fitting	Results	for Ke	pler-18

Planet	Phase (deg)	Amplitude (minutes)	Period (day)	T_c (BJD -2,454,900.0)	TTV Period (day)
18-c	184.5 ± 4.1	5.54 ± 0.18	7.6415716(5)	68.4071(2)	265.1 ± 2.5
18-d	3.2 ± 8.8	4.46 ± 0.30	14.858941(1)	61.1531(1)	265.9 ± 5.3

 Table 3

 Keck HIRES Relative Radial Velocity Measurements of Kepler-18

BJD -2,440,000	RV (m s ⁻¹)	σ (m s ⁻¹)
15076.009	7.750	2.539
15076.927	6.950	2.487
15081.024	8.617	4.214
15082.007	-1.007	2.381
15084.984	-7.320	2.977
15318.066	3.388	2.625
15322.029	-10.093	2.303
15373.004	12.189	2.150
15403.019	24.983	2.915
15405.909	-11.692	2.350
15406.881	0.340	2.195
15413.011	-10.788	2.498
15432.970	0.205	2.233
15436.782	-6.675	2.256
16109.905	-14.919	2.261
16111.845	4.123	2.642
16115.973	-0.326	2.434
16140.839	-8.153	2.730

When both the RV and TTV amplitudes are measured without invoking the extra constraint of Equation (14), two independent measurements of the stellar mass can be calculated, one through *K* and *V'*, and one through *K'* and *V*. However, since our value for *K'* is found by assuming a value for *K*, we only calculate one independent measure of the stellar mass. We find a stellar mass of $0.83 \pm 0.51 M_{\odot}$, consistent with that found by C11. We find the masses of planets c and d to be 18.6 ± 11.6 and $15.4 \pm 9.5 M_{\oplus}$, respectively.

It is somewhat disappointing that the uncertainties in the stellar mass are so large in this example, but this should be considered a shortcoming in the available data, not in the potential of our technique. Because most Kepler Objects of Interest (KOIs) are considerably fainter than typical stars probed by RV surveys, follow-up RV measurements are often carried out only to a level necessary to confirm the planetary nature of a transiting system, if any observations are collected at all. Thus, for most systems that exhibit TTVs, RV measurements alone are rarely precise to within even 20%. Better constraints

on *K* are regularly achieved for stars targeted in RV surveys, and with more follow-up observations these mass estimates will be greatly improved. This is discussed more fully in Section 4.

We can confirm the validity of our method by comparing our analytic result to results obtained through numerical integrations of this system. To accomplish this task, we make use of the Systemic Console developed by Meschiari et al. (2009). This program is designed to simultaneously fit Doppler and transit timing measurements. The Console contains several built-in integrators, including an eighth-order Runge-Kutta scheme employed in this work. The Console is not designed to enable the user to solve for the stellar mass as a free parameter. We circumvent this problem by first assuming a stellar mass. We fix the period and mean anomaly at BJD = 2,455,128.0 so that they are consistent with values found in Table 7 of C11; we then allow the planet masses, inclinations, and eccentricities to vary and minimize the χ^2 of the system. Once χ^2 is calculated, we vary the stellar mass slightly and repeat this procedure. With this technique, we can map the likelihood space in both M and m. As shown in Table 4, both the best-fitting parameters and their uncertainties are consistent with the analytic result, suggesting that our method is viable and that dynamical techniques can be used in conjunction with our analytic result to further constrain the stellar and planetary parameters.

In all cases, our uncertainties are dominated by our 20% errors in the RV semiamplitudes. The uncertainty in the RV semiamplitude will decrease considerably with more RV observations. We prove this claim by simulating observations placed randomly between the months of June and October, when the Kepler field is visible at night. We first find the true RV of the system at that time, assuming $K_c = 7.0 \text{ m s}^{-1}$. A statistical uncertainty σ is randomly drawn from the observed errors in previous HIRES measurements, and a Gaussian random number is drawn from a distribution $\mathcal{N}(0, \sigma)$. The RV measurement is shifted by an amount equal to this random number, and the statistical uncertainty is recorded as σ . Finally, to simulate the effects of RV "jitter" caused by stellar pulsations, a random number is drawn from $\mathcal{N}(0, 3 \text{ m s}^{-1})$; this value is also added to the RV measurement. The observations are fitted to a combination of sinusoids as described above, and the stellar and planetary masses are estimated. The fractional error in the semiamplitudes for the largest planet as a function of the number of observations is shown in Figure 1 (solid line).

Table 4						
Mass Estimates for Kepler-18 System						

Object	C11	L12	Analytic Result ^a	Dynamical Estimateb
$\overline{\text{Star}(M_{\odot})}$	0.972 ± 0.042	Assumed C11	0.83 ± 0.51	$0.92^{+0.61}_{-0.40}$
Planet c (M_{\oplus})	17.3 ± 1.8	20.2 ± 1.9	18.6 ± 11.6	$14.8^{+9.4}_{-6.0}$
Planet d (M_{\oplus})	16.4 ± 1.4	17.4 ± 1.2	15.4 ± 9.5	$15.4^{+11.0}_{-7.0}$

Notes.

^a Result derived by applying Equations (11)–(13).

^b Result determined from numerical integrations.



Figure 1. Derived fractional errors in the Doppler semiamplitude measurement as a function of number of radial velocity observations taken, for various values of *K*, the Doppler semiamplitude. For all observations, the same statistical uncertainties and RV jitter levels are assumed. The jitter level is 3 m s⁻¹, a reasonable estimate for all but the youngest dwarf stars. From top to bottom, these curves represent semiamplitudes of [7, 11, 15, 19, 23] m s⁻¹. For a system like Kepler-18, where $K \approx 7$ m s⁻¹, many more measurements would be required to constrain *K* to 5% (and thus the stellar mass to 15%). However, for a system with either larger planets or a smaller star, this level of precision could be reached with fewer observations.

We find that, with 30 more RV observations, the uncertainty in our calculation drops by nearly a factor of two, from the current 61% to 33%. To provide substantially better than 33% uncertainties without obtaining 50 RV measurements, we can target a less massive star. As stated in Section 1, this method will be optimal for stars for which evolutionary models are less able to constrain stellar parameters precisely, such as F-type stars, subgiants, and M-dwarfs. Since M-dwarfs are less massive than their G-type counterparts, a given mass planet around an M-dwarf produces a comparatively larger RV signal. Since the mass uncertainties will generally be dominated by the Doppler uncertainty, focusing on low-mass stars will enhance the observed signal, allowing for more meaningful mass constraints to be set. As proof, we again simulate observations of orbiting planets, but with larger values for K, corresponding to a less massive star or more massive planets. By sampling at the same times and assuming the same statistical errors and jitter levels, the fractional error in K decreases significantly for a fixed number of observations. These results are also shown in Figure 1 (dashed lines). For example, a planet identical to Kepler-18 c orbiting a star of mass $M = 0.33 M_{\odot}$ would produce a semiamplitude K = 15 m s⁻¹; with only 20 observations the RV semiamplitude could be constrained to within 8% and the stellar mass to within 30%. It is worth noting that these observations are all simulated assuming similar levels of statistical noise as the Kepler-18 observations. This is a reasonable approximation for the stars hosting KOIs, but these stars are considerably fainter than the average Doppler planet search target. If TTVs are detected around a considerably brighter star, as one would expect from next-generation spacebased planet-finding missions, RV observations could be carried out to considerably higher precision, decreasing the number of observations required to precisely measure the stellar RV semiamplitude.

4. SUMMARY AND DISCUSSION

We present a method of measuring stellar and planetary masses dynamically by combining TTVs measured from transit light curves and follow-up RV measurements. Our method can be used as an alternative to relying on stellar evolutionary models, which can be poorly constrained for non-solar-type stars such as M-dwarfs, subgiants, and F stars. By analyzing the Kepler-18 system and confirming our expressions with dynamical simulations of this system, we show the potential of our method.

While we show our method to be viable, especially for lowmass stars, using our method requires a somewhat specific set of circumstances. The system must contain two planets with masses large enough to force a detectable Doppler signal and observable TTVs on circular orbits near a first-order commensurability. *Kepler* data suggest that planets near resonance are common: more than 12% of planet systems show evidence for detectable TTVs (Ford et al. 2012b), and dozens of planets near resonance have been confirmed through TTVs (Steffen et al. 2012a). Both the TTV and Doppler signals can be measured for super-Earth planets with periods less than 30 days; short-period systems such as these are extremely common (Howard et al. 2012). Thus, it is likely that despite the specific requirements needed to use our system, it can be applied to a considerable number of *Kepler* planetary systems.

As shown in Equations (14) and (15) of L12, the amplitude of the TTV signal is given such that

$$|V| \sim |V_{\text{damped}}| \left(1 + \frac{|Z_{\text{free}}|}{|\Delta|} \right), \tag{15}$$

with $|V_{\text{damped}}|$ being the amplitude of the TTV signal if the system were damped of its free eccentricity. The quantity Z_{free} is defined such that $Z_{\text{free}} = f z_{\text{free}} + g z'_{\text{free}}$, where z is the complex eccentricity of the planet, $z = e \exp(i\omega)$. Thus, our method as described will break down unless $|Z_{\text{free}}| \ll |\Delta|$. This is a reasonable assumption for planets with periods under 10 days. In theory, even if a non-negligible amount of free eccentricity remains in the system, a detailed RV orbital solution and light-curve analysis could be used to calculate Z_{free} and determine the stellar and planetary masses.

As a projection of the utility of this method, consider KOI 1241, a system containing two planets with periods of 10.5 and 21.4 days orbiting a giant star ($R = 3.14 R_{\odot}$; Steffen et al. 2012a). From the transit timing signal, there is evidence that this system has not dissipated its free eccentricity, meaning that it is not optimal for our study. However, with nine quarters of public Kepler data, we can constrain the TTV signal caused by the larger planet in this system to 8.2%. Moreover, with only nine RV observations, the RV semiamplitude of the larger planet can be measured to 5.3%. Thus, from our method alone, if a system existed that was nearly identical to KOI 1241 but damped of free eccentricity, by Equations (11)–(13), we expect we could determine the stellar mass to 29% and the mass of the larger planet to within 22%. Our method could also be applied to KOI 1241 in the future if enough RV data are collected to determine the magnitude of Z_{free} for the system. The uncertainties in the TTV signal of KOI 1241 are larger than the uncertainty in the RV semiamplitude. The transit timing errors will decrease as more *Kepler* data are released: decreasing the TTV error to 5% without including any additional RV observations will reduce the uncertainty in the stellar mass to 20%. Thus, our method could provide significant constraints on stellar masses in regimes where stellar atmospheres are less well understood, such as subgiants and cool stars. For these cases, our method will be able to compliment asteroseismology results as an independent measure on the mass of the star. Moreover,

our method can be used to find systems where the analytic stellar mass is substantially different than the Kepler Input Catalog values, which can then be followed up with dynamical modeling, asteroseismology, or high-resolution spectroscopy to better characterize the star and orbiting planets.

Our method of estimating the stellar mass of a planet host star requires many high-precision RV measurements and observations of enough measurements to measure TTVs. Traditionally, for RV searches the stellar mass is estimated by interpolating spectroscopic properties such as the stellar effective temperature and metallicity onto stellar evolution model grids (e.g., Sozzetti et al. 2007). From a careful analysis of transit light curves, one can measure the ratio a/R_* and the duration of the transit event, which provide an estimate of the stellar density. However, stellar evolution models are still required to break the degeneracy between stellar radius and mass. While these traditional methods allow for precise measurements of stellar masses, the results are model dependent and may be subject to systematic errors induced by the stellar models. This is particularly true for stars very different from the Sun. Our method has the advantage of providing an accurate, model-independent stellar mass, albeit with a trade-off in precision. However, even in cases for which the precision of our method is poor, the resulting mass estimate can be used as a prior in the more traditional model-grid interpolation.

With present data our technique is only viable as an alternative to stellar modeling in the most exceptional cases. TTVs have been detected to remarkable precision by *Kepler*, but very few KOIs have been followed up with RV measurements. In the cases where RV data exist, only enough measurements were collected to confirm the planetary nature of the system, not to independently measure the planetary masses (Holman et al. 2010). Our routine will become more useful for systems around brighter stars, when more RV measurements can be efficiently collected and the RV semiamplitude can be better constrained.

Despite the faintness of the Kepler planet candidate host stars, there are a few stars that would be ideal candidates for applications of our method. From the collection of KOIs, we searched for stars hosting at least two transiting planets each with P < 25 days. We required at least one planet to be larger than 2 R_{\oplus} and the planet periods to lie within 5% of a first-order mean-motion resonance. To ensure that all targets were optimized for RV follow-up, we eliminated all targets fainter than $m_{\rm Kp} = 13.0$. After making these cuts, we find eight candidate systems to which this technique can be applied: KOI 85, 111, 115, 117, 244, 304, 1241, and 1930. As stated earlier in this section, KOI 1241 is not an ideal target because it has not been fully damped of its primordial eccentricity and there is not enough RV information to uniquely determine the eccentricity of both planets. Of the remaining seven systems, the CPS team has collected more than 10 RV measurements only on one, KOI 244. Additional RV measurements of any or all of the above systems would enable further validation of our

procedure, as well as additional constraints on the masses of each of the stars and their planets. Moreover, next-generation planet-finding missions, such as TESS (Brown & Latham 2008) and PLATO (Catala et al. 2010), will target bright stars, making detailed RV follow-up observations of systems exhibiting TTVs a much more practical possibility.

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