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ESTIMATING THE ENVIRONMENTAL COSTS OF THE HYDRO FUEL CYCLE USING LIFE CYCLE ASSESSMENT TECHNIQUES AND ECONOMIC VALUATION

BY

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DISSERTATION

Submitted to the University of New Hampshire in Partial Fulfillment of the Requirements for the Degree of

> Doctor of Philosophy In Natural Resources

> > December, 2001

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 $\frac{12/12/2001}{2001}$

ACKNOWLEDGMENT

I am sincerely grateful to Professor Richard England for his sustained support throughout my long stay at UNH. Professor England has been a valuable source of knowledge and an important mentor ever since I took his Ecological Economics course, and his patience and direction as thesis advisor were critical to the completion of this project. Professor England is an inspirational educator, and I am fortunate to have been his student.

I am indebted to Dr. Greg Norris at Sylvatica, who developed and donated the LCNetBase software and provided ongoing technical and moral support for this thesis. I am impressed by Dr. Norris' experience modeling complex systems and I appreciate his friendship, as well as his continuous help throughout my research.

For their support and help throughout my UNH experiences, I am especially grateful to Professors Mike Merenda, Gregory Theyel and John Aber. They are excellent educators who have helped shape my world view, and I am lucky to have studied in their classrooms.

Many thanks to my wife, Shannon Shuptrine, for patience and love, to Sandy Shuptrine for good questions and help with editing, and to many other family members and friends, whose contributions to this project are less tangible, but without whom completion of this project would not have been possible.

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ABSTRACT

ESTIMATING THE ENVIRONMENTAL COSTS OF THE HYDRO FUEL CYCLE USING LIFE CYCLE ASSESSMENT TECHNIQUES AND ECONOMIC VALUATION

By

Benjamin Ellis

University of New Hampshire, December, 2001

A Life Cycle Assessment model, with an integrated impact assessment, is used to estimate average external economic damages from the hydro fuel cycle. Aggregated average damage assessments of the hydro fuel cycle are complementary to marginal and site specific assessments, and are useful for general energy policy planning. For the upstream inventory assessment, detailed material input data from the Morrow Point Dam is used to estimate material inputs at 174 New England, and 4 Quebec, concrete hydroelectric projects. LCNetBase input-output life cycle assessment software, developed by Dr. Gregory Norris at Sylvatica, is used to estimate upstream emissions associated with material inputs and construction activities. Operations-phase emissions assessed include methane (CH4), carbon dioxide (CO2) and methyl mercury (MeHg), which are primarily associated with microbial activity in reservoirs. In the impact assessment, economic valuation is used to estimate the environmental impact associated with emissions from the hydro fuel cycle. Estimates of average externalities are as follows: small NE dams = \$.0343/kWh, medium NE dams = \$.0202/kWh, large NE dams = \$.0193/kWh, Hydro Quebec, La Grande Complex = \$.0461/kWh. Results indicate that the average external impacts from the hydro fuel cycle are less than, but similar to, the external costs from fossil fuel cycles. However, more

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detailed assessment of individual projects shows that emissions from the majority of hydro projects are very small as compared to fossil fuel cycles. In contrast, site specific characteristics at a small handful of hydro projects greatly exceed emissions per unit of energy for the coal fuel cycle, and increase the average estimates for small, medium and large New England dams.

EXECUTIVE SUMMARY

ES.1 Introduction

The hydro fuel cycle is an important part of the electricity generation mix in the U.S. and throughout the world. In New England, hydroelectricity is responsible approximately 30 percent of electricity consumed, much of which is imported from Quebec. With growing environmental concerns, hydro is increasingly seen as a clean alternative to fossil fuel electricity generation.

However, the environmental burdens associated with the hydro fuel cycle, particularly those burdens that are not included in the price of power, are complex, difficult to quantify, and difficult to compare to other fuel cycles. Some of these impacts are commonly understood, even if scope of the impact is not typically quantified. For example, many New England residents are aware that dams affect Atlantic salmon migration and spawning habitat.

Other impacts from the hydro fuel cycle are not commonly recognized, such as air pollution associated with materials and construction activities of the dam, or greenhouse-gas emissions from reservoirs. These burdens can have significant environmental impacts, the costs of which are not included in the price of power.

As many states move toward deregulating the electricity industry, quantifying the full costs of energy production is an important factor in making good decisions about energy. This thesis documents a quantitative analysis of the external costs of the hydro fuel cycle, or those costs born by society that are not included in the private costs of business. Externalities are a common measure of environmental and social damages from a product or process. The purpose of this study is to provide average, baseline estimates of hydro externalities that extend previous quantitative analysis of the fuel cycle by including previous ignored emissions. To that end, we quantify the external costs of emissions from the construction and operations-phase of the fuel cycle that are generally applicable to all hydro facilities. These include air and water pollutants from construction activities and greenhouse-gas emissions from the operations-phase. We do not quantify external costs that are typically site specific, such as wildlife habitat impacts or land use changes associated with new hydro projects.

Results from this study are unique, and they provide new insights into hydro electricity's role in pollution and global warming. We find that, on average, externalities from New England projects are approximately \$24 per megawatt hour, and externalities from Hydro Quebec projects are approximately \$44 per megawatt hour. Of these average estimates, greenhouse-gases from the reservoir account for more than half of total emissions. However, a handful of small and large projects have very high emissions per unit of energy that increase the total average externalities, suggesting that project size has little to do with per unit of energy externalities, and that the majority of New England projects have very low externalities per unit of energy.

It is important to note that this report is intended to be used as a starting point for further research rather than an endpoint for valuing the environmental impacts of the hydro fuel cycle. Expanded scope of study to include North America, improved material input data, and quantitative estimates of error would improve the accuracy of our findings.

ES.2 Objectives

The primary objectives of this study were to:

- Use affordable modeling techniques and existing data to develop, within time and resource constraints, an assessment of the external emissions from the hydro fuel cycle, including greenhouse-gas emissions from reservoirs.
- Develop a range of estimates of average externalities associated with selected impacts.
- Explore the relationship between material inputs, reservoir emissions and hydroelectric project size for the representative projects.
- Explore the role of time in quantitative life cycle assessment models.

ES.3 Methods

The damage function approach (DFA) was chosen as the basic methodology. DFA is a methodology which combines natural science and economics to model incremental changes in baseline conditions. An economic valuation process was used to estimate the average environmental damages and average externality costs associated with the quantified emissions. Specifically, input-output life cycle assessment (IO-LCA) was used to estimate the emissions associated with construction materials and construction activities. Conventional life cycle assessment was used to estimate emissions from reservoirs, such as carbon dioxide and methane, that occur during the operation of a hydroelectric project. Economic valuation was used to interpret the impact of emissions on human and environmental systems.

This application of DFA using LCA and economic valuation has not been applied to the hydro fuel cycle and the methodology has afforded a broader scope of study. For example, inputoutput life cycle assessment utilizes data from economic interactions throughout the entire U.S.

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economy, allowing us to estimate emissions from all upstream activities for over 1000 of the direct materials used in constructing dams. Materials assessed in this study include everything from concrete and structural steel to waterproofing materials, paints and explosives¹. Previous assessments of the hydro fuel cycle considered only the three primary inputs, concrete, steel and copper. These studies assumed that other material inputs were inconsequential, because the volume of these materials used to construct hydro projects are typically small.

In addition, previous assessments of the hydro fuel cycle have not included emissions from the operations-phase, or those activities associated with generating power once project construction is completed. Operations-phase emissions include estimates of greenhouse-gas emissions that form in the reservoir as a result of microbial decomposition of flooded organic materials.

Another typical assumption in previous hydro fuel cycle assessments is that the technology is mature and the fuel cycle emits no emissions in the operations-phase, thus limiting the time period for assessment to the present. The nature of our modeling techniques provides a dynamic data set, where emissions in any given year of the fuel cycle's life differ from the previous year. Rather then restrict the assessment to the present, this study utilizes discounting at different rates to explore the dynamic relationship between hydro and coal externalities over time.

Our methodology is a departure from previous assessments of the hydro fuel cycle. Although DFA has been applied utilizing life cycle assessment modeling, our application, with a mix of IO-

¹ In this study, we refer to these activities as "upstream" as it relates to the business supply chain. Building the materials and components for a hydro project are necessary activities that take place before the operation of a dam to produce electricity. Our use of "upstream" should not be confused with "further up a river."

LCA, conventional LCA and economic valuation, has only recently been developed and has not been applied to the hydro fuel cycle.

ES.4 Scope & Data

The study utilizes data published by the Federal Energy Regulatory Commission (FERC) and the Army Corps of Engineers (Corps) for concrete hydro projects with the primary purpose of electricity generation. Our scope was limited to 174 New England dams and 4 Hydro Quebec dams that are part of the La Grande project. The FERC and the Corps publish data that characterize certain physical descriptions of existing projects, such as annual average generation, dam size, powerhouse characteristics, generator characteristics, installed power capacity, and reservoir details.

Table ES.1 summarizes structural characteristics of the projects assessed in this study. Column C shows that the structural size of the dams ranges from 12,500 cubic yards to over 6.8 million cubic yards. Likewise, average annual generation ranges from 2,000 to 6 million megawatt hours per year.

Detailed material input data, a necessary minimum for estimating emissions associated with constructing dams, is not publicly available for these projects. In order to estimate the materials used in constructing each of these dams, data was taken from one project, the Morrow Point Dam, from which a detailed list of material quantities and costs was published by the Corps. The Morrow Point Dam was completed in 1968 on the Gunnison River in Colorado and is a large, concrete, arch-type dam. We separated the material into categories (Dam, Powerhouse, Transmission Lines, and Roads) and estimated the materials needed for a cubic yard of Dam and Powerhouse, and a meter of Transmission Line and Road. We then multiplied these data by

structural characteristics for the 178 dams in the study in order to estimate materials used at each of our study sites.

a) Group size	b) Model Number	c) Average Dam Volume (y ³)	d) Average Annual Electricity Generation (MWh/year)	e) Average Reservoir Volume (f ^d)	f) Average Reservoir Surface Area (acres)	g) Number of Dams in Each Model
	1	12,500	2,003	4.E+07	324	27
	2	29,186	2,355	4.E+07	198	29
	3	51,178	4,705	4.E+08	571	23
	4	67,551	8,974	2.E+07	61	15
7	5	92,062	12,315	4.E+07	84	6
Small	6	109,818	13,606	3.E+07	99	7
	7	124,980	19,574	4.E+07	183	5
	8	150,940	19,320	6.E+07	157	5
	9	173,213	11,878	4.E+07	96	3
	10	190,796	27,445	3.E+07	93	4
	11	239,445	54,558	4.E+08	710	12
	12	350,824	86,435	2.E+08	603	11
	13	444,124	34,605	4.E+09	4,545	4
E.	14	536,410	64,700	3.E+08	1,022	2
Meditum	15	668,321	104,984	1.E+09	1,747	5
	16	769,542	30,644	3.E+08	399	2
	17	871,704	16,850	5.E+09	4,183	2
	18	905,072	228,042	3.E+10	29,270	1
	19	1,335,549	51,517	2.E+09	2,518	5
	20	2,162,999	148,850	2.E+09	3,100	1
Large	21	3,554,953	105,200	1.E+07	300	1
•	22	6,800,742	277,800	5.E+09	2,292	2
	23	8,018,947	356,064	9.E+09	3,240	1,1
Hydro Duebec	24	87,000,000	6,800,000	3.E+12	3,376,045	4

Table ES.1 Structural characteristics of hydro projects assessed in this study

Estimates of the quantity of greenhouse-gas emissions at each dam were developed from recent studies of Canadian reservoirs. These studies measured greenhouse-gas emissions from experimental lakes and have demonstrated that lands flooded by dams yield high levels of carbon dioxide and methane where previously they had been neutral, or slight net sinks for carbon. Other work has measured emissions at Hydro Quebec's La Grande complex. Using this data,

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estimates were made for greenhouse-gas emissions for a square meter of reservoir surface area and applied to the projects in the study.

ES.5 Results

Table ES.2 summarizes the average emissions per megawatt hour quantified in this study. For most emissions categories, the largest projects, those associated with Hydro Quebec, have the lowest emissions. Notable exceptions are for methane (CH_4), carbon dioxide (CO_2) and methyl mercury (MeHg), where the Hydro Quebec projects produce approximately ten times the emissions of the New England projects.

	VOCs (ST)	NOx (ST)	CO (ST)	SO2 (ST)	PM10 (ST)
Small NF	1.88E-05	6.22E-05	1.01B-04	1.23E-04	1.80E-05
Medium NE	3.11E-05	1.03E-04	1.66E-04	2.03E-04	2.98E-05
Large NE	5.17E-05	1.71E-04	2.76E-04	3.37E-04	4.94E-05
Hydro Quebec	3.04E-05	9.30E-05	1.52E-04	1.84E-04	2.69E-05
	Fossil CO2 (MT)	TRI Air (lbs)	TRI Water (lbs)	TRI UnGnd (lbs)	TRI Land (lbs)
Small NE	2.67E-02	1.26E-02	1.30E-03	4.95E-03	6.78E-03
Medium NE	4.42E-02	2.08E-02	2.14E-03	8.17E-03	1.12E-02
Large NE	7.34E-02	3.46E-02	3.56E-03	1,36E-02	1.86E-02
Hydro Quebec	4.04E-02	2.01E-02	2.04E-03	7.72E-03	1.06E-02
	TRI POTW (lbs)	TRI Off-Site(lbs)	Cost D&T (\$K)	CO2 Equiv (ST)	MeHg (ST)
Small NE	2.84E-03	5.38E-02	4.09E-05	1.55E-01	4.70E-03
Medium NE	4.69E-03	8.88E-02	6.76E-05	2.66E-01	2.24E-02
large NE	7.80E-03	1.48E-01	1.12E-04	6.67E-02	6.83E-03
Hydro Quebec	4.45E-03	8.44E-02	6.30E-05	1.82E+00	1.56E-01

Table ES.2 Normaliz		

Viewing the average emissions data in Table ES2 provides some information about the normalized releases from different hydro projects, but it does not allow for comparisons between emission categories or for estimates of total impacts. For example, knowing that the Hydro Quebec projects are the largest projects, but that they emit less pollutants in most emission

categories is not enough information to understand what these emissions mean to those affected by the pollutants.

Table ES.3 summarizes the results from externality assessments of the emissions data, which allowed us to quantify disparate emissions data into a common measure of social and environmental damage. Column A shows the average externalities for the upstream activities assessed in this study. Hydro Quebec projects have the smallest upstream externalities of those projects considered in this study, with approximately 48 cents per megawatt hour of generation. Column B summarizes operations-phase emissions, the majority of which represent greenhouse-gas emissions from the reservoirs (refer to Table ES.2). Column B indicates that Hydro Quebec projects have the highest externalities of the projects assessed in this study, on the order of \$43 per megawatt hour. In total, column C shows that New England projects have average externalities that range from \$12 to \$28 per megawatt hour and Hydro Quebec projects are approximately \$44 per megawatt hour

	A) Total Upstream Emissions	B) Total Operations Emissions	C) Total Impact	D) Total Impact 5% Discount	E) Total W/O 3 Outliers	F) Total W/O 10 Outliers
Small NE Dams	\$5.27	\$22.42	\$27.70	\$21.40	\$9.85	\$5,56
Medium NE Dams	\$3.09	\$13.26	\$16,35	\$12.62	\$4.78	\$5.52
Large NE Dams	\$6.04	\$5.75	\$11.79	\$9.96	\$11.79	\$4.47
Average NE Dams	\$4.82	\$19.39	\$24.22	\$18.76	\$13.66	\$5.53
HQ	\$0,48	\$43.14	\$43.62	\$31.66	\$43.62	\$43.62

Column C in Table ES3 suggests that large New England dams have the lowest average externalities of the projects assessed in this study. However, a more detailed look at the underlying data shows that a few outliers exaggerate the average externalities from the New England projects. For example, one small project has total externalities over \$2,000 per megawatt, while the median externality for the entire New England pool is only \$3.63, indicating

that the average externality estimates are highly skewed by a few projects. Column D shows our results without the three highest outliers, or those that exceed \$200 per megawatt. Column E shows our results without the ten highest outliers, or those that exceed \$50. With the outliers removed, total externalities per megawatt hour for the New England projects range from \$4.47 to \$5.56.

Commonly referenced results from other externality studies of the hydro fuel cycle range from \$0 to \$.1 per megawatt (Pace 1990, DOE 1995). Our average estimates are significantly higher than previous hydro assessments, particularly for the Hydro Quebec projects.

Discounted results from externality studies of the coal fuel cycle range from \$1.3 to \$64 per megawatt. Our estimates of externalities for Hydro Quebec are generally at the higher end of the coal externality studies.

ES.6 Conclusions

Total externalities assessed in this study are driven by relationships between average annual generation and structural characteristics of the project. Upstream emissions per unit of energy are associated with the size of the dam and powerhouse, and the length of the transmission lines and access roads. Operations-phase emissions are related to the surface area of the impoundment and the total volume of water stored in the reservoir. In general, the projects with the lowest emissions have small reservoirs, short roads and transmission lines, and small dams and powerhouses relative to the average annual generation.

Previous studies of the hydro fuel cycle conclude that a major advantage of hydroelectricity over fossil fuel cycles are the negligible total externalities. In general, we find that a majority of New

England hydro projects assessed in this study have low externalities as compared to fossil fuel cycles. However, our findings suggest that a small handful of New England hydroelectric projects, and the Hydro Quebec projects assessed in this study, may have significant externalities that are of similar magnitude to coal fuel cycles.

A second key finding of previous studies is that there is essentially no risk of climate change from hydroelectricity as a result of greenhouse-gas emission. However, this study suggest that, on average, greenhouse-gas emissions from the operations-phase account for approximately half of total externalities for New England projects and the majority of externalities from the Hydro Quebec projects.

This assessment provides insight into planning and siting new hydro facilities, and it is helpful in identifying pathways from emission to impact on the environment to include in marginal externality studies. Insofar as public utilities and federal agencies are considering ways to internalize the external damages from the electricity generation mix, our findings conflict with previous understandings and suggest the need for more quantitative assessments of the hydro fuel cycle. Extending this study with improved data and with an expanded scope that covers North America would help in understanding the effects of the hydro fuel cycle and assist in planning an electric generation mix to minimize environmental impacts.

The scope of this study was limited by a set of resource and time constraints. The study findings are based on a number of assumptions that suggest the need for more research. Important assumptions in this study include:

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- The materials used in the Morrow Point Dam are generally representative of the materials used in New England and Hydro Quebec concrete hydroelectric projects.
- Greenhouse-gas emissions measured at the La Grande complex in northern Quebec are reasonably transferable to temperate reservoirs.
- Reservoir greenhouse-gas emissions generally follow Fernside's (1995) emission curve decay rate model.

Error in our results is magnified because of embedded assumptions in the three primary data manipulation steps, including estimates of material inputs at study sites, input-output life cycle assessment of upstream emissions, and economic valuation of emissions data to estimate impacts on society. We qualitatively describe our assumptions and inconsistencies in the data, but we provide no quantitative estimates of uncertainty. One published study on the hydro fuel cycle utilizes Monte Carlo modeling to develop quantitative estimates of uncertainty (DOE 1995). Monte Carlo simulation would be possible with the data we collected, but we felt it was beyond the scope and charter of the project.

The study could be expanded in a number of ways to address these limitations. First, with little increased effort, the model could be expanded to include all regions of the U.S., Mexico and Canada, which would improve regional, average estimates of externalities and provide insight into marginal damages at proposed sites. Second, more detailed, site-specific infrastructure data would enhance the accuracy of the model. Third, additional site-specific environmental impacts and external benefits could be included, such as long-term impacts on anadromous fish, degraded water quality, increased recreation activity or increased real-estate value. Last, improved estimates of error utilizing sensitivity analysis or Monte Carlo modeling, would provide more accurate and useful results.

PART I

LIFE CYCLE INVENTORY OF THE EXTERNAL EMISSIONS FROM THE HYDRO FUEL CYCLE

CHAPTER I

INTRODUCTION TO THE HYDRO LIFE CYCLE

1.1 Introduction

This paper represents the first of three describing our work in valuing hydro externalities. Our primary concern in this paper is to use affordable modeling techniques to quantify some of the emissions that are often excluded from LCA models of the hydro fuel cycle. To that end, we use input-output life cycle assessment (IO-LCA) to quantify upstream and construction phase emissions, and we use conventional life cycle assessment (LCA) to model some operations-phase emissions. We introduce methods to include some of the impacts typically ignored in hydro LCA studies, specifically greenhouse-gas emissions from the impoundment and methyl-mercury mineralization associated with the flooding of new reservoirs. Our model is based on a case study of 174 concrete hydroelectric dams in New England and four Hydro Quebec projects associated with the La Grande project. The results are presented in emissions per unit of energy for a size-graduated profile of the individual hydro projects. We use the model and results presented in this paper as baseline data for valuing hydro externalities in the following paper.

A secondary purpose of this study is to explore the relationship between material inputs, emissions, and hydroelectric project size in a New England and Hydro Quebec cases study. We hypothesized that small New England hydroelectric projects emit less energy per unit than larger

projects. Our hypothesis is based on the assumption that small projects require the least infrastructure and smallest impoundment for the available power potential of a given site. Additional rationale for this assumption comes from previous studies, where it is commonly held that small hydro has fewer impacts than large hydro (American Rivers 1998, Wiser & Pickle 1997, Holt 1997). To test this hypothesis we calculated baseline estimates for a set of air, water and land emissions on a per-unit of energy basis for small, medium and large projects.

The structure of the paper follows the Society of Environmental Toxicology and Chemistry (SETAC) recommendations for reporting LCA results (SETAC 1996). SETAC is a scientific association that has played a leading role in the documentation and dissemination of guidance for LCA methodology and practice. We first define the scope and boundary of the hydro fuel cycle considered in the model. Next, we review LCA studies of the hydro fuel cycle. We include a review of economic externality studies of hydro because they are among the most comprehensive studies of the fuel cycle, and they utilize methods that are similar to ours for estimating the quantity of emissions. In addition, externality studies assess the impacts emissions have on social and environmental communities, which is a primary purpose of this study and the subject of the following papers. Following the literature review, we describe the data and methods used in the modeling process. Finally, we present the results of the LCA model and a discussion of the importance of our findings.

We find that hydro power leads to direct and indirect air, water and land emissions, and that emissions per unit of energy are poorly correlated with project size. Our model suggests that certain small and certain large projects have equally high emissions per unit of energy. In testing our hypothesis, we find that three simple ratios are useful predictors of emissions. These ratios can be used to compare emissions from proposed projects with regional averages.

1.2 Study Boundary and Scope

Figure 1 summarizes the scope of quantified and assessed emissions from the hydro fuel cycle. We quantify and model emissions from processes within the indicated study boundary, including upstream emissions associated with building materials and design activities, emissions from construction, and mercury and greenhouse-gas emissions from the operations-phase. Figure 1 also shows that we excluded numerous emissions and impacts from the construction and operations-phase. We find that the emissions excluded from our analysis tend to be site-specific and beyond the scope of our assessment.

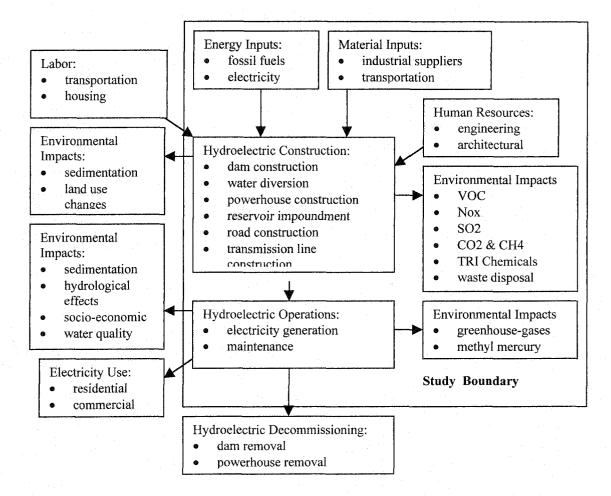
1.3 Hydro Life cycle

The hydro life cycle has similarities to other electricity generation fuel cycles in that the primary product, electricity, is highly consumable, applied to disparate forms of work, and the environmental impacts tend to be site specific. Beyond these, however, comparisons become difficult. The hydro fuel cycle is relatively simple. The "fuel", which is water, is renewable and does not undergo chemical changes during electricity generation. The operation phase of the hydro life cycle does not include many of the external industrial inputs necessary for other fuel cycle, such as mining, refining and fuel processing, and fuel transportation. Many of the impacts affect the immediate surrounding environment, including local water quality, aquatic habitats and land-use changes, which are more typically associated with damages to the environment rather than damages to human health or well being (DOE 1995).

The hydro life cycle starts with architectural, engineering, planning and accounting activities. Following the planning phase, energy and products are combined with labor to divert the river, clear the impounded area, and construct the superstructures, access roads, and transmission lines. In this study, we refer to this combination of activities as the upstream and construction phase.

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Figure 1 Study boundary



We define "upstream emissions"² as those emissions from the chain of processes necessary to produce any of the materials used in constructing the dam. For example, steel, a primary material input, requires a set of mining, manufacturing and transportation activities, each of which result in emissions and has environmental consequences. IO-LCA allows us to model the many industrial linkages necessary to produce every material used in dam construction. We can then estimate the upstream emissions embodied in the construction materials in order to develop a comprehensive profile of impacts from the fuel cycle. We further aggregate upstream emissions

² Upstream is used in a process rather than hydrologic sense.

into six supply tiers, in which the first tier represents the emissions from constructing and supplying the direct materials purchased to construct the dam, and the second tier represents the emissions produced to supply the first tier, and so on.

The operations-phase consists of those activities necessary to run and maintain the hydroelectric facility. These include facilities management, ongoing maintenance to the moving and non-moving systems, and licensing. We assume that the primary product of the facility is electricity generated during the operations-phase, although secondary internal and external benefits may exist at individual projects, such as increased flat-water recreation on the impoundment, shoreline real-estate development opportunities, or irrigation.

In this study, we assume that the working life of a hydroelectric facility is 50 years. This assumption is undoubtedly somewhat arbitrary, given that many facilities have been in operation for more than 100 years. We chose the 50-year life for four reasons. First, 50 years is the longest license issued by the Federal Energy Regulatory Commission (FERC) in the U.S. to private hydroelectric facilities. FERC is the regulatory agency with jurisdiction over private electricity generation. Fifty years was considered by the commissioners to be a reasonable time for hydroelectric facilities to recapture environmental mitigation costs assessed during the licensing process (FERC 1998).

Second, a literature review of hydroelectric fuel cycle studies indicate that the majority of studies assume a 50-year life (PACE 1990, DOE 1995, BPA 1984, Meyers et al. 1986, Rudd et al. 1993). This time-period assumption is somewhat institutionalized in academic research of the hydro fuel cycle and the use of a 50-year life cycle in this study allows direct comparison to the results of other studies.

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Third, it is reasonable to assume that meaningful predictions about the role of hydroelectric facilities beyond 50 years from today are not possible. Changes in technology, improvements in conservation and efficiency, and demand for electricity products by residential and industrial users have proven difficult to predict with certainty even 10 years in advance (DOE 1995). Consider, by way of example, the long-term contracts signed in the early 1980s between New England PUCs and renewable energy generators to supply electricity at prices well beyond market values (PURPA 1999). These contracts were based on assumptions about rapid and sustained increases in electricity demand that did not materialize.

Finally, major renovations are typically required at hydroelectric facilities as they reach 50 years in age (FERC 1998, ExternE 1998). These retrofits are site specific, but may include overhaul and rewinding of the generators, reconstruction of spillways and dam superstructures, improvements for recreation access and other environmental mitigation, and major maintenance to buildings.

The decommissioning phase includes a number of possible outcomes, primarily driven by the site and politics. Outcomes include total removal of all buildings and dams, partial breaching of the project with no removal of the associated infrastructure, in-place abandonment of the project assets, and full renovation of existing facilities (FERC 1998). Because these decisions are sitespecific, we do not assess emissions from the decommissioning phase.

1.4 Environmental Impacts from the Hydro Fuel Cycle

Construction and operation of hydroelectric facilities can affect ecological systems, cultural and recreation resources, safety, and economic systems through a variety of impact pathways. The primary environmental impact pathways are changes in hydrology and water quality, changes in land use, and interference with fish and wildlife movement through construction of barriers

(Rosenberg et al. 1997). Other primary impacts, which may have both positive and negative external results, include affects on recreation and commercial opportunities (Medsker 1982, PACE 1990, DOE 1995). Secondary impacts can come from emissions associated with building, transporting and installing construction materials, as well as emissions from reservoirs. Appendix I provides a qualitative summary of emissions and other impacts from the hydro fuel cycle in a table format.

Land-use changes are initiated through building of dam superstructures, cutting and maintaining transmission lines, and flooding of reservoirs (PACE 1990). Sediments and nutrients in unaltered river basins are typically flushed through the rivers during periods of high flows. In altered systems, sediments settle in the reservoirs and can contribute to eutrophication. Sediment-free waters below dams can increase shoreline erosion, reduce downstream agricultural fertility and reduce the productivity of aquatic organisms (Bodaly et al. 1984).

Water quality in reservoirs can degrade in response to thermal stratification, which takes place when dense, cool waters settle on the bottom of the impoundment and resists mixing with warmer, upper-level waters (Bodaly et al. 1984, PACE 1990). In upper-level waters, aerobic decomposition of flooded organic matter can lead to releases of CO2, which is thought to be a primary factor in global warming (Rudd 1995, Tathy et al. 1992). Flooding of new reservoirs has been demonstrated to initiate natural mercury mineralization, which leads to the highly toxic and persistent form of methyl mercury (Kelly et al. 1997). In the cold, deeper waters, dissolved oxygen content can decrease to the point where decomposition of flooded organic materials becomes anaerobic. Many of the by-products of anaerobic decomposition are toxic to aquatic life, including ammonia and hydrogen sulfide. In addition, anaerobic biological activity produces methane, which is a particularly potent greenhouse-gas (Galy-Lacauz et al. 1997). Water released from the depths of an impoundment can require many miles of travel to re-oxygenate (FERC 1995).

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Biological communities, including fish, wildlife and macro invertebrates, are affected by hydro projects, although many of these impacts are poorly understood (DOE 1995, PACE 1990). At a minimum, flooding reservoirs causes changes in biological communities as natural riparian and wetland areas are covered and lake environments are created. Fish and other aquatic species are affected by changes in flow, reduced spawning grounds, reduced food, increased temperature, decreased water quality, increased mortality, and restricted mobility caused by the dam structures (FERC 1995). Hydroelectric projects are known to cause extinction in certain fish species in certain regions of the U.S. and Canada (Meyer 1986).

Safety concerns can exist with the possible, but improbable, result of dam failure and catastrophic flooding (FERC 1999). Safety concerns are typically minimal, as dam construction and licensing is subject to significant and comprehensive review by the FERC.

Damming and flooding rivers can affect recreation and commercial activities, as well as cultural resources. There are numerous examples of lost whitewater boating and fishing opportunities, as well as the flooding of important Native American cultural sites in the Southwest U.S. exist (see RIMS database maintained by FERC). Recreational and cultural impacts, though at times significant and external to project operations, are site-specific and beyond the scope of this study.

Many of these environmental impacts are internalized in the price of power. For example, new standards for minimum and flushing flows downstream of a dam may be required during the FERC relicensing process (see FERC License Application for Kennebec p-2143, Mokelumne p-137, Feather p-1963). The goal of such an action would be to improve water quality, habitat and sediment transport. The utility may have to forego electricity generation or install special floodgates to provide such flows, which increases the price of power and internalizes the costs of

the mitigation measure. However, many other environmental impacts are not captured in the price of power, including upstream and operations-phase emissions.

With the exception of upstream and operations-phase emissions, most of hydro's environmental impacts are site specific. Quantifying these site-specific impacts at all New England and Hydro Quebec projects is beyond the scope of this analysis. As indicated in Figure 1, we focused our attention on assessing upstream and operations-phase emissions that are common to the concrete hydroelectric projects assessed in this study.

CHAPTER II

REVIEW OF QUANTITATIVE ASSESSMENTS OF THE HYDRO FUEL CYCLE

2.1 Introduction

In this study, we use input-output life cycle assessment to quantify upstream emissions, which are the emissions associated with providing the construction materials for the hydro projects in question. We use conventional LCA methods to assess greenhouse-gas and methyl mercury emissions from the operations-phase. IO-LCA is distinguished from conventional LCA in both the method and scope of the study (Lave 1997). IO-LCA is a particularly affordable and powerful modeling tool in that it captures detailed upstream emissions not only for each individual material used in new dam construction, but also emissions for material extraction and construction for each part used in the dam. IO-LCA software provides a method to assess emissions from all tiers in the supply chain for each product used in new dam construction (Norris 1996). In this study, we assessed more than 1000 individual material inputs. Certain products, such as explosives, waterproofing, or paints, may be used in very small quantities as compared to other materials, such as concrete and steel, but their damages to the environment and human health may be disproportionately large to the volume of the material used. Ignoring upstream material inputs, or focusing on only a few materials used in construction, could obfuscate the overall impacts from the hydro fuel cycle.

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In this section, we compare our study methods and scope to hydro LCA studies and other quantitative assessments of the hydro fuel cycle. We find that no other studies utilize the IO-LCA methodology for assessing upstream emissions and no other studies assess the greenhousegas or methyl mercury emissions for individual projects from the operations-phase of the hydro fuel cycle. We conclude that our methods are unique and that we capture broader range of emissions as compared to other quantitative assessments of the hydro fuel cycle.

2.2 Hydro LCA Studies and Databases

We reviewed fuel cycle LCA studies to identify methods used, inventory results, and valuation outcomes. In general, previous LCA studies of the hydro fuel cycle defined a narrow scope around operations-phase emissions, and typically conclude that the hydro fuel cycle has zero emissions. LCA has been extensively developed in Europe and there are at least two publicly available LCA studies of hydroelectricity, but they are not published in English (ETH 1994, Norsk Hydro 1998). In addition, the product and process focus of LCA has led to many privately commissioned studies, the results of which are not generally available. Finally, many private firms and quasi-public organizations have established proprietary databases that are available for a fee. The user manuals, often available in marketing materials, do not provide sufficient information on the sources, scope and quality of the background data to reconstruct detailed LCA methodology of the hydro fuel cycle (SimaPro 4.0, Umberto)

Nonetheless, a number of LCA studies have been conducted on hydroelectricity, and most databases available for use in conventional LCA modeling assess the environmental impacts of hydro to some level. In 1995, the Society for the Promotion of LCA Development (SPOLD) published a directory of life cycle inventory data (SPOLD 1995). The directory was published in an attempt to overcome the limitations of data location and formatting, and the report lists details of the sources, geographic boundary, data quality and price of the majority of conventional LCA

databases. All of the data listed in the SPOLD directory follows the SETAC, or an adapted SETAC methodology. Many of the data sources are not independent assessments. For example, the "Ecobalance of Packaging Materials" (BUWAL 250 1995) study uses ETH energy data for hydroelectricity.

Many other databases utilize BUWAL as a primary source of data. Table 1 summarizes the material inputs from which emissions were quantified in this and other LCA studies. Detailed descriptions of our methods are located in Section 4, and detailed descriptions of our results are located in Section 5.

Table 1 Summary of inpu	ts assessed in h	ydro LCA stu	dies	
	Ellis	ETH	Franklin	EcoBalance
Upstream Emissions				
Cement	V V CARA	1		
Concrete	V	N		Ń
Steel	1	4		\checkmark
Copper	V	1		V
Aluminum	. √	staria -		
Explosives	V	V		
Paints & Waterproofing	√			
Other metals	V			
Construction Fuel	\mathcal{A}			
All other material inputs	V			
	i	labativet i j		
Operations Emissions				
CO2	- √			. *
CH4	V			

The SPOLD report lists four sources of independently constructed hydroelectric LCA data: ETH-ESU (Switzerland), Franklin Associates, Ltd. (USA), EcoBalance (USA), and IVAM Environmental Research (Netherlands). Of this data, the ETH-ESU is general recognized at the most comprehensive source of LCA fuel cycle data, (Personal discussion with Greg Norris, Sylvatica; Keith Weitz, RTI; Jim Wasla, SCS; Bob Hunt, Franklin Associates) . The database, developed from existing infrastructure in European countries, is publicly available, but the supporting materials describing study methods and scope are only available in German. Part of

this literature review is an effort to translate the hydropower section into English in order to compare the results, methodology and scope of the study to the results of this paper. We used German to English translation software with 90 percent accuracy. Our translated text, however, did not preserve any of the formatting, so it is inadequate to ascertain the true intent, scope or results of the study. The translated text from the ETH study is located in Appendix J.

From what we can understand from the translated text, the ETH study appears to be extremely comprehensive. It estimated first-tier air, water, and toxic chemical emissions from explosives, cement, aluminum, copper and steel, the primary materials by volume used in hydro projects. ETH considered the operational life of various facility components, including turbines, powerhouses and dam structures. It identified large and small projects based on hydraulic head and estimated annual energy production. ETH concluded that hydro has low emissions per unit of energy, primarily because there are no greenhouse-gases emitted from the operations-phase. In its summary tables, ETH allocated emissions to units of energy, although we have been unable to translate the tables into English.

Franklin Associates, Ltd. (FAL) has a long history of conducting LCA studies in the U.S. for private firms (Hunt 1996). FAL sells and supports its their database directly to customers and through their LCA software package EcoManager. FAL quantified the environmental impacts of other fuel cycles, but did not quantify the impacts of hydro. FAL assumed that the emissions from operations were negligible or not quantifiable, and it followed SETAC guidelines by ignoring capital goods and equipment. As a result, the database has "zero" values in all emission categories for the hydro fuel cycle (FAL 1998).

EcoBalance, a consulting firm based in Rockville, Maryland, developed the DEAM inventory database with independent assessments of the environmental impacts of hydroelectricity. Its operations emissions data comes from Chamberland's (1996) article on hydroelectricity.

EcoBalance estimated average reservoir size and depth and average annual electricity generation from data published by the FERC for all US hydroelectric projects. Its model includes first-tier assessments of four construction materials. EcoBalance further assessed the greenhouse-gas emissions released during operations. Details of how these assessments were made, the life cycle of the facility, and the construction materials assessed are not publicly available, and have not been made available by the staff at EcoBalance. The results of this model: 1 MJ of hydroelectricity results in .0042 g of CO2 & .00057 g of CH4 (personal correspondence with Vince Camobreco).

IVAM, a private research, consulting and software development firm in the Netherlands, has developed an independent, peer-reviewed database for 700 processes that lead to more than 250 materials (IVAM 1999). Its database has been constructed from internal LCA studies in combination with BUWAL, ETH and other publicly available data. Hydroelectric data appears to have come from a Dutch fuel cycle study, which was a subsidiary study of the ETH study (van Heijningen 1992).

We conclude that our methodology, which considers upstream as well as operations emissions using IO-LCA techniques, is more comprehensive than the methods described above. Our results, as described in following sections, consider many additional impact pathways and result in a substantially higher inventory of emissions.

2.3 Hydro Externality Cost Studies

Methods used in externality cost studies are similar to conventional LCA studies in their calculation of upstream and operations emissions data, and their assessment of human and environmental impacts from these emissions. We reviewed the methods, scope and results of three commonly cited and comprehensive hydro externality studies, including "Estimating

Externalities of the Hydro Fuel Cycle" conducted by the DOE Oak Ridge Laboratory (DOE 1995), the "The Environmental Costs of Electricity" conducted by Pace University (PACE 1990), and the "Sultan River Study" conducted by the Bonneville Power Authority (BPA 1984).

Some of the data underlying the final results is similar to the inventory data used in LCA studies, however we conclude that the IO-LCA methodology provides a more comprehensive assessment of upstream emissions than the externality cost method. Of the externality studies reviewed, only the DOE study includes any upstream emissions from construction materials.

As with the LCA studies reviewed above, the externality cost studies devote little attention to operations-phase emissions. All of the externality cost studies identify the avoidance of greenhouse-gases and heavy metals in the operations-phase as a significant external benefit of the hydro fuel cycle. In contrast, we found that greenhouse-gas emissions from reservoirs are a quantifiable and significant environmental impact pathway.

2.3.1 Estimating externalities of the hydro fuel cycle - Department of Energy, 1995.

The DOE sponsored a comprehensive study of fuel cycles with the primary goal of estimating environmental externalities through application of cost-benefit methodology. The DOE reviewed the externality cost literature in order to construct a range of estimates of the marginal damages from certain impacts of new hydro projects. The study considers two U.S. reference sites with a total of 12 hydroelectric projects. The two sites are a hydroelectric retrofit of an existing water diversion project in the Southeast, and a proposed new construction of a diversion project in the Northwest.

For upstream damages, the DOE assessed the indirect emissions resulting from the use of four primary construction materials: concrete, steel, copper and aluminum. The scope of the upstream assessment was limited to the first tier in the supply chain. No assessment was made of raw material extraction or transport of building materials to the manufacturer.

Estimated quantities of construction materials per cubic yard of dam construction were provided by the Army Corps of Engineers. Steel in the dam and diversion structures was estimated to be 120 lbs/cubic yard of concrete, which is the value used by the DOE for estimating steel in all concrete-reinforced structures. The DOE assumed that all of the turbine, and all but 8 percent of the generators' gross weight, is steel. It assumed that remaining 8 percent of the generator weight is copper. By treating the generator and turbine as raw material, the study disregarded emissions associated with energy and material inputs that result from manufacturing these complex products. The study assumed that powerhouse structures would a.ll be 30x60 feet, and explicitly excluded other building materials, such as waterproofing, roofing, paints and explosives, arguing that they are negligible as compared to concrete and steel.

DOE estimates of aluminum input requirements are based exclusively on transmission line cable at the weight of 1/3 pound per linear foot. The study ignored steel, rubber and other circuitry necessary for transmission lines. No effort was made to assess the emissions from access road construction or transportation of construction materials to the site.

In order to convert the inventory of steel, concrete, copper and aluminum into estimates of atmospheric emissions, the DOE utilized data from the TEMIS database. TEMIS was developed by Meridian Corporation from LCA emissions data for Germany and Western Europe. The DOE utilized this data in place of data developed in the U.S. because TEMIS was comprehensively collected and the U.S. and European manufacturing practices are similar. Table 2 summarizes the emission factors from the TEMIS database.

Table 2 Emission	factors for m	aterials manufac	ture (lb/ton)
Steel	Concrete	Aluminum	Copper
CO2 6,000	1,800	50,000	17,600
SQ ₂ 6	10	50	8
NO _x 10	30	40	10
PM 1	2	10	2

The DOE study was unable to quantify impacts and emissions from changes in water quality, flow alterations, air quality, or land-use changes initiated during the construction or operations-phase.

Two operations-related impacts were quantified: loss of fish from suspended sediment load and loss of fish spawning habitat as a result of altered hydrology. Data for the estimate of impacts to fish from suspended sediments was collected from site-specific details in the FERC license application, including estimated annual sediment load associated with each project, risk factors for catastrophic collapse of the diversion structures, and the number of anadromous fish downstream of each project.

Data for the assessed losses to fish and fish habitat from altered flows was taken from the FERC license application and was highly site-specific. At each of the reference sites, in-stream flow studies were conducted as part of the license application, indicating the percent of fish habitat available before and after project development. These percentages were multiplied by the estimated number of spawning fish in each reach.

Despite the fact that numerous impacts were not quantified, the DOE study concludes that the hydro fuel cycle has smaller environmental impacts than other fuel cycles because it does not produce greenhouse-gas emissions and impacts to road from transporting heavy fuels are not present. The final results calculated for the diversion project were .1 mill/kWh for reduced fishing benefits.

2.3.2 Environmental Costs of Electricity – Pace University, 1990.

The primary purpose of the Pace study was to conduct a comprehensive review of the environmental externalities literature as it relates to electricity generation, and to present best estimates of externalities per unit of energy. A secondary purpose of the Pace study was to use the literature reviewed to prepare damage estimates for typical pollutants released during the generation of the fuel cycle.

Pace reviewed two studies on the environmental impacts and costs of hydroelectricity, including "Methods for Valuation of the Environmental Costs and Benefits of Hydroelectric Facilities: A Case Study for the Sultan River Project," and "Calculation of Environmental Costs and Benefits Associated with Hydropower Development in the Pacific Northwest." Both studies were prepared for the Bonneville Power Authority (BPA) in the late 1980s in an attempt to quantify external impacts of BPA operations.

Pace prepared an overview of small hydroelectric facilities, as defined as less then 80 MW capacity. Pace concluded that the potential impacts from small hydropower are generally the same as large hydropower on a kilowatt-hour basis, and that the magnitude of impacts per unit of energy can be smaller or larger than large hydropower. On a project-by–project basis, the impacts from small hydro tend to be less than large hydro. However, the stacking effects of numerous small hydro projects built in succession along a river tend to increase the impacts of these facilities on a unit of energy basis. Pace found no environmental cost studies of small hydropower, so the study provides only a qualitative description of the possible impacts of project size.

Pace was unable to estimate the externality value of hydroelectricity. However, it pointed to a number of factors that make hydropower attractive as compared to energy generated from fossil

fuel. Pace argues that there are many important positive externalities, including avoided greenhouse-gas emissions, avoided acid rain precursor emissions, avoided trace metal emissions, and no cooling water impacts. Pace reprints a table from a DOE white paper that indicates that on a kilowatt-hour basis hydro CO2 emissions are 10 times higher than fossil fuel CO2 emissions during the construction phase (A-12). During the operations-phase, the table indicates that hydro CO2 emissions are zero and coal plant CO2 emissions are over 1000 tons per GWH. In total, the study claims that CO2 emissions from hydropower are 100 times less than those from coal plants.

Two shortcomings in the Pace study make the results somewhat controversial (DOE 1995, BPA 1991). First, the scope of the Pace study included operations emissions only. Those direct and indirect emissions associated with construction and maintenance activities were ignored. Second, Pace assumed that electricity generation is the primary social purpose for hydroelectric projects. Pace assigned all external impacts to electricity production, ignoring for simplicity purposes the parts responsible for flood management, irrigation and recreation. Despite problems with the hydro fuel cycle analysis, the Pace study is often cited in the literature and is considered a seminal study on the environmental costs of electricity (DOE 1995).

2.3.3 Sultan River Study- Bonniville Power Administration, 1984.

The Sultan River Study (BPA 1984) was developed to test the merit of applying cost valuation methodologies to site-specific environmental attributes. The study argues that environmental costs of hydropower are unique to each site and that calculating generic costs per unit of energy for the hydro fuel cycle may not be possible. The study also suggests that economic valuation methods may not be necessary or sufficient for quantifying the environmental externalities of hydropower.

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The Sultan River study used three methods to quantify numerous, site-specific estimates of impacts, including hedonic pricing, willingness to pay, and willingness to be compensated. Impact areas quantified include: old growth, deer, whitewater, extreme kayaking, commercial timber, and general recreation. The study used a 3 percent discount rate and presented the results in mills/ kWh. The final results are 10.87 to 12.31 mills/kWh for total external costs. These results are considerably higher than other externalities estimates, which range from zero (Pace 1990) to .01 mills/kWh (DOE 1995).

The study has been criticized for using methodologies that overestimate certain impacts (DOE 1995, PACE 1990). The study, for example, calculated that 30 deer are valued at \$6200, class V kayaking at \$1886 per day, and commercial timber at \$32,628 per acre. The Pace reviewers criticized the study on three accounts. First, they noted the study's dependence on willingness to be compensated methodologies that Pace asserts are "seriously biased." Second, Pace noted flaws in the survey instrument that could have led to biased answers. Third, the method used for calculating loss of old-growth forest is misleading because old growth "confounds equity and efficiency considerations." The DOE points out that the study does not develop and document uncertainty surrounding the value estimates.

2.3.4 Other externality studies.

Numerous valuation studies have been conducted that quantify the value of recreation, fisheries and other biological attributes of river ecosystems. Andrews and Dolcine (1990) contains a bibliography of 117 valuation studies. These studies, though useful in the economic valuation of the inventory assessment, provide little insight into assessing the life cycle impacts from the hydro fuel cycle.

2.4 Lessons from the Literature Review

We emphasize three points from our review of the literature. First, each study utilized a unique methodology, with a unique scope and disparate results. Our approach, using IO-LCA for assessing upstream emissions and conventional LCA for assessing operations emissions, considerably extends the scope of previously conducted studies. We were able to include all upstream material inputs, and some of the operations emissions, such as greenhouse-gas and methyl mercury emissions from reservoirs, that have not been included in previous assessments. New science indicates that greenhouse-gas emissions from hydroelectric reservoirs may be significant, and we were able to model these emissions at all 178 case study sites.

Second, our methodology, relying primarily on publicly available data and IO-LCA techniques, is an affordable and transferable approach to assessing upstream emissions. In addition, our model allowed us to utilize data from all hydroelectric projects in our study region, a total of 178, rather than a handful of representative projects. This allows us to consider both marginal damages from a proposed project against regional averages, and average damages for small and large projects.

Third, we concur with the position taken, or implied, in all of the reviewed studies that current scientific understanding of most of the hydro impacts is inadequate to assist in quantitative modeling of the fuel cycle. Impacts, such as degraded water quality and reduced fish habitat, must be modeled for each site and requires assessment of other projects in a given watershed, as well as other land uses within the watershed. Such an assessment was beyond the scope of this study. Quantitative analysis in our study, as with other studies reviewed, is limited to emissions associated with construction and, in our case, a few operations-related emissions.

CHAPTER III

METHODS AND DATA

3.1 Introduction

Data necessary for running the model was compiled, aggregated and adjusted in a number of steps. Each data set required considerable adjustment for use in the model. Table 3 summarizes our modeling activities and Appendix G describes our assumptions and adjustments for each data set. In this section we summarize our modeling steps, the data used, and the data conversions necessary for use in our model.

3.2 Step 1: Model Material Inputs

First, we calculated material inputs in dollars per cubic yard of concrete hydroelectric dam from detailed construction data for the Morrow Point Dam (BOR 1983). The Morrow Point Dam is the only project in the U.S. for which extensive construction details are available to the public. The Army Corps of Engineers finished construction of the dam in 1968 and published an extensive report on every detail of dam construction. The report lists all material and labor purchase orders in dollars, and the quantity of materials used in various units. The line-item data was reported as the aggregated cost of direct material, labor, profit and service inputs into the project. Approximately 1000 product line items were entered into a spreadsheet (Appendix A).

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Next, the total reported value of each line item was reduced by the percentage of contractor profit, labor, and on-site transportation costs in order to derive actual costs of materials used in the dam. Percentage adjustments were developed using RS Means construction cost data (RS Means 1998). RS Means develops an annual detailed average construction cost database for concrete construction, heavy construction, site-work and landscaping, and building construction.

Step	Modeling Activity	Hours
Step 1: Calculate material inputs	Hydro LCA literature review	200
to new dam construction	Hydro cost benefit literature review	200
	Input quantities and dollar value for all materials used at Morrow Point Dam from the Army Corps of Engineers (CORPS) data	160
	Assign commodity code for each material line item using BEA descriptions	25
	Create construction category for excavation, transportation and road construction using RS Means percentages	10
	Allocate materials to Dam, Powerhouse, Switchyards, Transmission lines, Roads using CORPS data	7
	Remove profit & labor using RS Means	8
	Convert dollar value to 1992 using CPI	5
Step 2: Model emissions for	IO-LCA literature review	100
cubic yard of new dam	Input dollar value per commodity into LCNetBase	1
	Model emissions using LCNetBase per cubic yard of dam.	15
Step 3: Model New England & Hydro Quebec profile of concrete	Input average annual generation, and operation regime for 174 NE dams from FERC data	25
hydroelectric projects	Input structural information for 174 dams from CORPS data: year of construction, height, length, number & type of generators, nameplate rating, impoundment surface area, impounded area volume,	25
	Estimate structural volume of dam, length of roads, length of transmission lines	10
	Convert CORPS identifying numbers to FERC	1
	Hydro Quebec Literature review	30
	Convert disparate Hydro Quebec literature descriptions into structural and average generation for the La Grande	10
Step 4: Model emissions for all NE and HQ projects	Apply emissions from LCNetBase output to structural aspects of all assessed dams	35
Step 5: Model greenhouse-gas	Literature review	75
& methyl mercury emissions	Estimate greenhouse-gas (GHG) residence time and turnover rate from Fernside	10
	Estimate GHG emissions per square meter of impoundment surface areas from empirical Hydro Quebec data	30
	Estimate methyl mercury residence time and turnover rate	8
	Estimate methyl mercury residence time and tanover rate Estimate methyl mercury emissions per cubic meter of impounded water	10
	Frivolous time that can't be allocated to a real task, but was somehow necessary for completing this project	ť
	Total Hours	1025

Table 3	Summary	of modeling	activities

The database lists more than 40,000 component installation line-items with unit costs, labor, installation materials, and profit estimates for an average installation. Labor and profit were removed entirely from the calculus. For products where RS Means percentages were not available, the average of all percentages used for labor, profit and transportation were used to

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reduce those products and materials by labor, profit and transportation. A new category, "on-site transportation," was created and the residual fuel costs from activities such as excavation and landscaping were summed and placed in the new category cell.

Each line item was assigned a product sector code number that corresponds to the Bureau of Economic Analysis (BEA) input-output tables. LCNetBase software publishes a search table of 485 industries and close to 12,000 products produced by those industries (Norris 1998). We matched the Corps descriptions with product descriptions (Appendix A). The data was then subtotaled under each BEA product sector code. Using annual changes in the Consumer Price Index (CPI), subtotaled dollars were converted to 1992 dollars in order to correspond with the 1992 input-output tables.

Morrow Point Dam data was not reported in discrete segments, such as transmission line costs, road construction costs, or powerhouse costs. We separated the data into four material input categories: powerhouse and switchyard, dam, transmission lines, and roads. We used data from the Morrow Point Dam to estimate the dollar of inputs from each industry sector for a generic, cubic yard of dam construction, cubic yard of powerhouse and switchyard construction, meter of road construction, and meter of transmission line construction. We assumed that material inputs scale linearly within these categories.

3.3 Step 2: Model Upstream Emissions Using LCNetBase IO-LCA Software

In step 2, we used LCNetBaseTM software developed by Greg Norris at Sylvatica (1997) to run the input-output LCA model and calculate emissions for new dam construction. Wassily Leontief developed input-output analysis to capture economy-wide economic interdependencies based on the assumptions that complicated interactions between industries can be simulated with proportionality relationships (Leontief 1996, Miller et al. 1995). For example, if 3 tons of copper

is required to build one industrial electric generator, then 6 tons would be required to build two generators. In addition, an increase in demand for industrial electric generators would require increased output by hundreds of other industry sectors, including electricity, steel, petroleum, plastics, and engineering services, to name a few. Based on a change in final demand, the inputoutput analysis models the change in output for all of the direct and indirect supplies to an industry.

Figure 2 Steps in Input-Output LCA (adapted from Joshi 1998)

Step 1) Estimate direct output for changes in sector (f)

Step 2) Estimate direct and indirect economic change (x) with input output matrix (a)

Step 3) Estimate environmental discharges from industry sector output (e)

Step 4) Add all industry sector discharges to find total emissions

Recent work in life cycle assessment has combined pollution discharge data for industry sectors with input-output estimated change in final demand for each sector, producing an input-output life cycle assessment model for the entire economy (Lave et al. 1996, Horvath 1997, Joshi 1998). Figure 2 shows the IO-LCA modeling process in which change in final demand (f) for a product leads to an assessment of direct and indirect economic change (x) for all industry sectors within the I/O matrix (a) necessary to produce the product. Equations 1) shows that final demand (f) plus intermediate demand (ax) equals the change in total output of a given sector³:

³ More detailed descriptions of input-output analysis, including underlying assumptions about the economy and detailed mathematical descriptions, can be found in Miller 1985.

(1)
$$x - ax = f$$
.

However, equation 1 does not calculate sectoral input requirements because it does not include the actual indirect inputs from other sectors in the supply chain. The industry sector output to meet final demand is calculated by pre-multiplying equation (1) by $[I-a]^{-1}$:

(2)
$$x = (I-a)^{-1} f$$

where x = total output of a vector, a = the matrix of direct requirements, f = the vector of final demand, and I= is the identity matrix for sectoral interactions. Equation (2) can be expanded to represent the infinite transactions between industry sectors:

(3)
$$x = (I + a + a^2 + a^3 + a^4 + \dots)f$$

In step 3, we expand the input-output model to assess the pollution discharges to the environment associated with changes in final demand. If (r) represents a matrix of emission coefficients associated with a dollar change of output from each industrial sector, and if (e) represents the vector of total direct and indirect emissions, then the total environmental effects associated with a change in the demand vector (f) is:

•
$$e_{total} = rx = r(I-a)^{-1}f$$
,

and the direct discharges are:

(5)
$$e_{direct} = r(I+a)f$$

Input-output tables are developed and used by many countries for economic planning (Miller et al. 1985), and comprehensive input-output tables are maintained by the Department of

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Commerce. U.S. economy input-output data used in LCNetBase is from the Bureau of Economic Analysis (BEA 1997). The economic tables are compiled from survey and Economic Census data and are reported on the national level by the commodity and industry sectors. Data for more than 500 commodities and nearly 500 industries are catalogued and used in developing the input-output tables. When we ran the model, the most recent set of input-output data available was from 1992.

The environmental emissions matrix (r) can include vectors for any pollutant with sufficient data to be included in the model. Environmental emissions data, such as raw material consumption, energy use, and emission releases, is reported annually to various federal agencies. When combined with the input-output matrices in the LCNetBase software, we can model the emissions profile for a product, process, service, or the entire economy. Environmental matrixes used in LCNetBase are from the EPA's Toxic Release Inventory (TRI), Emission Trends Inventory, Aerometric Information Retrieval System (AIRS), and Resource Conservation and Recovery Act (RCRA) (Norris 1997). These matrices provide sufficient data to estimate toxic chemical releases to air, water and land, the emissions of conventional air pollutants, and greenhouse-gas emissions from fuel and electricity consumption.

3.4 Step 3: Material Inputs and Emissions at NE and HQ Projects

In this study, we assume that concrete hydroelectric projects utilize similar materials in similar proportions. In order to model emissions for individual hydro projects, we combined emissions data from LCNetBase for a cubic yard of construction material for the four categories previously described to detailed structural data for the individual projects. Data for the size, structure and average annual generation for the New England hydroelectric projects was calculated from data published by the Army Corps of Engineers (CORPS 1996) and from the Federal Energy

Regulatory Commission (FERC 1999). Structural data for the Hydro Quebec La Grande project was compiled from the literature.

Army Corps data, as reported in the National Inventory of Dams (NID) (CORPS 1996), provides structural information for every U.S. dam, including structural height and length, reservoir size, hydraulic head, year of construction, and materials used (Appendix C). Appendix K summarizes categories in the NID database. Column 13 includes the primary purpose of the facility, including: Irrigation; Hydroelectric; Flood Control; Navigation; Water Supply; Recreation; Fire/Farm Pond; Fish andWildlife; Debris Control; Tailings; Other. Column 23 indicates which federal agency has regulatory oversight of the project. Column 27 identifies the NID code for the type of dam construction for each project, including: RE = Earth; ER = Rockfill; PG =Gravity; CB = Buttress; VA = Arch; MV = Multi-Arch; CN = Concrete; MS = Masonry; ST = Stone; TC= Timber Crib; OT = Other. We sorted the database for New England, hydroelectric projects overseen by the FERC, and further sorted for those dams constructed of concrete in a similar manner to the Morrow Point Dam project FERC project numbers were assigned to the hydro facilities and subtotals of structural details were calculated. Of more than 400 New England dams, we were left with 174 individual projects that fit our criteria.

Army Corps data included structural length and height of dams, but did not report the dam width or the volume of materials in FERC-licensed projects. Although "volume" appears in the NID data fields, no data was entered in any of the concrete hydroelectric projects in New England. In order to estimate volume for the New England projects, we developed a multiplier from Morrow Point Dam data that scaled with the height of the dam. The structural height of Morrow Point Dam is 469 feet, ranging in width from 10 feet at the top of the impoundment structure, to 52 feet at the bottom of the structure. We assumed a linear decrease in dam width from the foot to the top of the structure. This multiplier was used to estimate dam width for the New England projects.

The FERC database (FERC 1999) presented kilowatt output in both capacity and annual average generation for each project as organized under FERC licensing and project ownership. FERC and Army Corps data sets were combined in a metafile to reflect average annual generation in kilowatt hours relative to volume of structural materials used, surface area of the impoundment, average head for each development, and year of damming for all New England hydroelectric projects that were constructed primarily of concrete (Appendix D).

A similar methodology was used for estimating the material inputs for the Hydro Quebec La Grande complex. Data on the size of the impoundment, volume of superstructure development, length of new roads constructed, length of high-tension transmission lines, and average annual generation are from Ludwig et al., (1980), Amyot et al., (1976), and Duchemin et al. (1995). Structural profile data was combined with the detailed material inputs for the Morrow Point dam project in order to estimate total upstream emissions for the La Grande complex.

3.5 Step 4: Calculate Emissions per MWh at NE and HQ Projects

In order to calculate upstream emissions at the 174 dams, we allocated upstream emissions per cubic yard of material to the total structural materials used in each project. Emissions for each project were then divided by the annual average generation for the assumed 50-year project life. We used one megawatt hour as the functional unit (the basis for comparison) for the study.

3.6 Step 5: Estimate Greenhouse-gas and Methyl Mercury Emissions

We derived our estimates of greenhouse-gas emissions and methyl mercury mineralization from a literature review of empirical studies conducted in Canada and at the Hydro Quebec La Grande complex. Details of this review, and further discussion of the strengths and weaknesses of the studies, as well as a discussion of how we derived greenhouse-gas estimates are in Appendix G.

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3.6.1 Greenhouse-gas emissions.

Over the last decade, research has led to the conclusion that artificial reservoirs are sources of greenhouse-gases (Rudd et al, 1993, Chamberland 1993, Kelly et al. 1994, Duchemin et al. 1995, Fernside 1995, Galy-Laxaux et al. 1997). Decomposition of flooded vegetation leads to the release of carbon stored in the biomass. Where decomposition tends toward aerobic conditions, CO2 is typically released to both the water column and the atmosphere. Where anoxic conditions dominate, methane and hydrogen sulfide are released.

We used Duchemin's estimates of CO2 and CH4 releases for deep and shallow waters (Duchemin et al. 1995 & 1997). We used Chamberland's (1993) estimates of the ratio of deep and shallow waters at the La Grande complex: 10% of the La Grande project lands is shallow (less than 10 meters), and 90 percent is deep. We used Fernside's (1995) estimate of decay rates and release curves for the flooded carbon stock based over a 50-year life. We chose Duchemin's estimates because they are based on direct measurements from the La Grande complex. Other studies of greenhouse-gases, including those of the Freshwater Institute, are also based on direct measurement, but are conducted at other boreal reservoirs. In addition, the Freshwater Institute studies are primarily concerned with flooded peatland, which is thought to release more greenhouse-gases than other forest soils.

Duchemin (1995 & 1997) measured CO2 and CH4 emissions in the La Grande reservoirs at the air-water interface in both shallow and deep regions of the lake. The studies are limited in a number of ways. They assume that there are only 120 days of ice-out conditions and that no greenhouse-gasses will be accumulated or released when the reservoir is frozen. They did not account for the increased contribution of flooded peatland. They did not account for the possible increased biological activity along the riparian borders where lake levels inundate and retreat with

seasonally. In addition, the Duchemin studies did not conduct a mass-balance of carbon emissions from the lands before and after flooding in order to establish an estimate of net greenhouse-gas flux. For these reasons, we conclude that Duchemin's measurements are likely to be conservative underestimates of the total greenhouse-gas emissions from the La Grande project.

All of the studies of boreal reservoirs measure greenhouse-gas emissions at a certain point in time (Rudd, 1993, Duchemin, 1995, Chamberland, 1993). However, these studies made few quantitative estimates of the total flooded carbon stock that would be released as CH4 and CO2, and no estimates of the magnitude of greenhouse-gas flows over time. In contrast, Fearnside (1995) estimated the total carbon stocks associated with three zones in the reservoir: anoxic or fully submerged material, partially aerobic within 3 meters of the surface area, and aerobic organic material flooded by the reservoir but periodically exposed to the air. The zones included deeply submerged organic materials that were assumed to decay very slowly (over 500 years) and produce primarily methane. Fearnside assigned biological decay rates and percent releases of CH4 and CO2 for all the carbon stored in the studied reservoirs and developed release curves associated with different points in time. In order to estimate the greenhouse-gas releases from Canadian and New England reservoirs, we used the measured emissions data at the water-air interface from reservoir studies at theLa Grande complex in years 17 to 22 after flooding. We placed the empirical data from the La Grande complex on the Fearnside emission rate curve in order to assign a total value for greenhouse-gas emissions for each reservoir studied for 50 years following flooding, and to assign relative impacts to each year in the hydro life cycle.

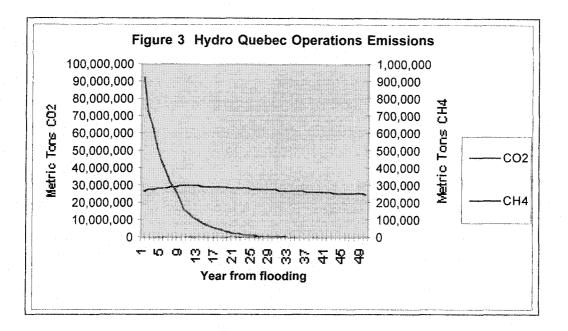
The estimates of greenhouse-gas releases were converted to grams per square meter per year at the water-air interface. Using the same ratio of 10 percent shallow and 90 percent deep, we developed profiles of greenhouse-gas releases for the New England reservoirs. It is likely that these estimates exaggerate actual emissions from New England reservoirs. In contrast to boreal reservoirs, when temperate reservoirs were constructed the timber was typically first harvested

and sold, removing considerable amounts of the carbon stock before flooding lands. In addition, most of these reservoirs were flooded in the late 1800s and early 1900s. Assuming that Fernside's greenhouse-gas release curve is valid, then the CO2 releases are currently reduced to background levels. Also, all of the New England reservoirs are many times smaller than the Hydro Quebec La Grande complex. The profile of the lake tends to have a higher ratio of shallow to deep water than those found at La Grande. As can be seen in Table 4, emissions of both CH4 and CO2 are lower in shallow waters, and the proportion of methane to carbon dioxide is smaller. Both of these factors would lead to lower total greenhouse-gas emissions per unit of energy.

Table 4 Estimated greenhouse-gas emissions from reservoirs (metric tons/m^2/180 days)

	shallow		deep	
	ch4	co2	ch4	co2
Estimated release	0.00000220	0.00579306	0.00000092	0.00695168
CH4 as CO2 equivalent		0.00004615		0.00001923
Total		0.00583922		0.00697091

Figure 3 shows the CO2 and CH4 curves for the La Grande complex. We assumed that ice-in conditions stop greenhouse-gas production. We assumed ice-out conditions of 120 days for the La Grande complex and 180 days for the New England dams.



We adjusted the CH4 impacts into CO2 equivalents by utilizing a multiplier of 21 for the following reasons. The Intergovernmental Panel for Climate Change (IPCC) preferred method for calculating direct impacts from CH4 releases is to consider a 100-year timeframe without discounting (Isaksen et al. 1992). When considering direct impacts only, the IPCC recommends utilizing a CO2 equivalent multiplier of 11. When considering the indirect impacts, the IPCC recommends a CO2 equivalent multiplier of 21. Methane's direct effects are directly related to atmospheric warming, and its indirect effects are due to the production of tropospheric ozone and stratospheric water vapor. CO2 emissions include no indirect effects (IPCC 1996). Because this study is concerned with the cumulative impacts of hydroelectricity, and because many of the methane-related impacts to global warming are indirect, we chose the higher multiplier

3.6.2 Methyl mercury emissions.

Mercury is a known mutagen, tetragen, and carcinogen (FS 1984). At comparatively low levels, mercury absorbed by animals behaves as a neurological toxin, affecting behavior, reproduction and other basic biological functions. At sufficient levels, mercury ingestion is fatal. Mercury has

no known metabolic function, and bio accumulates at higher trophic levels. Many documented examples of mercury poisoning follow its rapid path through the environment, from toxic release, to accumulation at higher levels of the food chain, to toxic impacts on human populations (Eisler 1987).

Ample evidence supports the claim that mercury levels increase significantly in recently flooded reservoirs (Potter et al. 1974, Abernathy & Crumbie 1977). Extensive research in Quebec, Ontario, Manitoba (Bodaly et al. 1983 & 1991), Finland, Sweden (Lodenius et al. 1983) and the Southeast US (Abernathy et al. 1977) indicate that mercury levels in reservoir fish are between two and five times higher than that of fish in unpolluted, natural lakes.

The increase of mercury in newly flooded reservoirs is thought to result from the release of natural and deposited inorganic mercury in the soil (Abernaty & Crumbie 1977, Bodaly 1991). Flooded reservoirs tend to support increased microorganism activity as the flooded biomass becomes an available food source. Chemical speciation of mercury is complex, especially in reservoir environments. However, in newly flooded areas, the toxic characteristics of mercury tends to increase by following path from inorganic forms of Hg, which are most common in soils, to organic methylated forms of mercury, which are more common in water (Trembaly & Lucotte 1997). Anaerobic and aerobic microbial activity converts the various species of inorganic mercury (Hg⁰) to the highly toxic and mobile methyl mercury (CH³Hg⁺).

Methyl mercury is a particularly toxic species of Hg because of its stability and solubility in fats, and its ionic potential tends to move the molecule across cell membranes. Once ingested, it accumulates in fatty tissues. Organisms higher up the food chain, such as predatory fish and fish feeding birds and mammals, tend to have the highest concentrations of methyl mercury. Data collected from the La Grande complex indicates that mercury levels in predatory fish 20 years after flooding remain on average five times higher than marketable levels established by the

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Canadian government (Tremblay & Lucotte 1997). Mercury levels in predatory fish from natural lakes in the region are within marketable thresholds.

Most of the published literature concerning methyl mercury in reservoirs has been conducted in Canada in response to mercury poisoning of the Cree Indians and other indigenous peoples living around the large Canadian reservoirs⁴. The Freshwater Institute at the University of Manitoba created an artificial reservoir and tested the total mercury and methyl mercury content of the natural pond and flooded reservoir before and after flooding in 1992 (Kelly et al. 1997, Rosenberg et al. 1997). Their ongoing studies indicate that northern peat landmasses are small net annual sources of total mercury and methyl mercury. Following flooding, total mercury increases marginally, but the percentage of methyl mercury increased from 4 percent to 79 percent, with a long-term average increase of 37 percent.

Table 5 Measureme	nt of percent c	hange in methyl mercu	ry (Kelly et al. 1997)
(ng/L-1)	Before	After Flooding	Net Change
Total Hg	2.5	2.65	0.15
Methyl mercury	0,1	0,98	0.88

Other findings indicate that methyl mercury concentration in fish and in the water column are more dependent on upstream factors than reservoir factors (Johnston et al. 1991). Two variable models of fish mercury levels from physical characteristics of the flooded reservoirs, utilizing within-lake measures and upstream measures, were able to account for more than 70 percent of the variation in mercury levels. Upstream characteristics accounted for the majority of impacts.

In the US and other sub-arctic temperate countries there has been little empirical work concerning methyl mercury in reservoirs. Elevated mercury levels in natural and artificial lakes have been

⁴ The Cree Regional Authority's successfully 1986 suit against Hydro Quebec and the Quebec government brought international attention to the environmental impacts of Quebec's hydroelectric projects. This suit, along with others, has been a catalyst for scientific research into these impacts.

recorded throughout the US, but it is assumed that these high levels of mercury are related to atmospheric deposition and point-source pollution instead of methyl mercury mobilization from flooding new lands (USFWS 1987). This theory is supported by the fact that most reservoirs in the U.S. are older than 50 years, suggesting that initial impacts from flooding would be mitigated.

Empirical data on the residence time and turnover rate of methyl mercury in reservoirs has yet to be established. Actual methyl mercury loads in reservoirs depend on numerous site-specific factors, including inflow and outflow of the impoundment, acidity, soil substrates, atmospheric deposition, dissolved oxygen content, and the quantity of flooded biomass (Lodenius et al. 1982). Empirical evidence from the Experimental Lake project indicates that methyl mercury in the water column returns to background levels after 10 years (Kelly et al. 1997). Mass balance models of methyl mercury in reservoirs are currently under development by private consulting firms (Manitoba Hydro 1997). These models depend on data collected by the Freshwater Institute and are calibrated to predict mercury levels in fish in specific regions. No estimates of residence time or turnover rate used in the model are publicly available (Literature search and personal correspondence with Dr. Reed Harris). Best-guess estimates of mercury residence time in fish from newly flooded reservoirs vary from five years (Abernathy & Cumbie 1977) to more than 30 years (Maxwell et al. 1997).

Extensive measurements of mercury accumulation in fish do not provide adequate information for assessing the annual production of mercury per liter, residence time, or turnover rate. However, given the persistence of methyl mercury in fish tissue, and the fact that elevated levels tend to peak, stabilize and slowly decline over time, it is hypothesized that methyl mercury formation in newly flooded reservoirs will bloom in the first years of the flooded system. Future impacts and biological accumulation in the biota result from an initial bloom of methyl mercury (personal correspondence with Dr. Drew Bodaly, Freshwater Institute; Dr. Reed Harris). The Freshwater institute is currently using 10 years for average residence time in the water column.

Table 6 summarizes the estimates of methyl mercury contamination used in this study. The net change in methyl mercury in nanograms per liter⁻⁽¹⁾, as measured by Kelly (1997), was multiplied by the total volume of water in each reservoir. We assumed the average turnover time to be one year, and that the measured quantity of methyl mercury declined to background levels over 10 years following a linear curve. We estimated the total methylation of mercury in each reservoir for each year and divided the annual emission by average annual generation. The table includes conversion into total pounds of methyl mercury generated in the entire reservoir each year.

Table 6 Methyl mercury mobilization from flooding at the La Grande Complex

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year	1	2	3	4	5	6	7	8	9	10
Total MeHg	0.980	0.882	0.784	0.687	0.589	0,491	0.393	0.296	0.198	0,100
Net MeHg (ng L ¹)	0.880	0.792	0.704	0.616	0.528	0,440	0.352	0.264	0.176	0.088
Total Reservoir (g/year)	83,877	75,489	67,101	58,714	50,326	41,938	33,551	25,163	16,775	8,388
Total Reservoir (kg/year)	84	75	67	59	50	42	34	25	17	8
Total Reservoir (lbs/year)	185	166	148	129	111	92	74	55	37	18

3.7 Comparison of Our Methods to Other Quantitative Hydro Studies

Our methodology appears to be unique. LCA and externality cost studies of fuel cycles more typically define the major direct materials as the average of a set of "representative" products (ETH 1994, PACE 1990). For hydro projects this typically means the average direct material inputs for, say, zero to 30-megawatts of installed capacity, and 30-100 MW projects. The model would then aggregate impacts to a kilowatt-hour functional output, so that within the tested range impacts would be linearly related.

The problem with this approach is that the quantity of the material inputs into a hydro facility is assumed to be linearly correlated to the megawatt-hour output of the facility. However, we have found that megawatt-hour output is not a good predictor of the size of the impoundment, the size of the dam, the length of the transmission lines or other necessary infrastructure which lead to life

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cycle emissions. In constructing our model, we assumed that most hydroelectric facilities have similar direct materials inputs in similar proportions to the Morrow Point Dam project. But, rather than directly apply impacts to energy output, we assume that the total volume of material inputs to hydro projects is site-specific rather than linearly related to average annual generation. For example, a large dam in a small drainage may have small annual generation, a large reservoir, and a proportionally large upstream burden.

	Coefficients	Standard Error	t -Statistic	p-value	Lower 95%	Upper 95%
Observations	120					
Standard Error	6613808.67	A TOTAL AND	an e rinstanna	2 cm com prosesso		and the state of the state
Adjusted R Square	0,57969225					
R Square	0.58322425					
Multiple R	0.7636912					

In order to assess the variability of material inputs to annual kilowatt output, we regressed the volume of dam materials (dependant variable) into the average annual kilowatt hour output (the independent variable) of all New England concrete hydroelectric facilities. Table 7 summarizes the results of the simple regression model. The model indicated that material inputs explain approximately 58 percent of average annual generation. This suggests that traditional methods of assigning environmental impacts directly to kilowatt-hour output would falsely allocate more than 40 percent of impacts to certain projects.

3.8 Assumptions and Weakness in the Data and Model

We consider our model to provide baseline information about the pool of New England hydroelectric projects. We find that our methods could be useful in assessing baseline information at other hydroelectric sites, or for other fuel cycles, in an efficient and affordable manner.

There are a number of weaknesses in our methods and the data used to model hydroelectric emissions. The scope of our model, though beyond other published assessments of the hydro fuel cycle, is limited to upstream emissions plus two pollutant emissions from the operations-phase. We were unable to model other environmental impacts external to the hydro fuel cycle, such as water-quality effects, or changes in biodiversity. Our research suggests that these impacts are site-specific and often internalized in the cost of operations. Modeling these impacts would require detailed knowledge about the individual projects and other land uses in the watershed. In addition, the scope of our project did not include end-of-life assessments, such as decommission, breaching or retrofitting.

We assume similar material inputs for all concrete dams and associated infrastructure. Many of the dams included in this assessment were constructed more than 100 years ago. The construction methods and materials used are somewhat different than those of today. In addition, we depend on only one set of input data from the Morrow Dam, and we assume that other hydroelectric facilities use materials in similar proportions. Further, we estimated dam volume at our reference sites based on height and width characteristics of the Morrow Point Dam. A more complete methodology would utilize detailed input data from each hydro facility assessed. However, at this time such data is not publicly available in sufficient detail to support such an analysis.

Finally, we qualitatively describe our assumptions and inconsistencies in the data, but we provide no quantitative estimates of uncertainty. One published study on the hydro fuel cycle utilizes Monte Carlo modeling to develop quantitative estimates of uncertainty (DOE 1995). This would

be possible with the data we collected, but we felt it was beyond the scope and charter of this project.

In summary, we have taken a new approach to quantifying emissions from the hydro fuel cycle on a regional basis. Because we assessed every hydroelectric project in New England, our results are necessarily generalized. The number of projects in our assessment reduced our ability to study many of the fuel cycle impacts for which generalized data was not available. Nonetheless, our results provide insight into the environmental impacts of the fuel cycle and provide baseline information from which further site-specific modeling can be done.

CHAPTER IV

INVENTORY OF EMISSIONS FROM THE HYDRO FUEL CYCLE

4.1 Introduction

We theorized that larger projects would have larger impacts when normalized to annual generation. We assumed that smaller projects, as assessed by the volume of the dam superstructure, would be built first in areas with proportionally high head, thus minimizing the materials used and associated environmental impacts when considered on a per unit of energy metric. We find that both small and large projects have profiles that cannot be easily generalized by the small, medium and large criteria. Rather, we have developed three sets of ratios, including dam volume, reservoir size, and reservoir surface area to annual generation, to more easily generalize impacts from individual projects.

The primary purpose of this section is to profile the inventory of emissions released during the upstream, construction and operations-phases. We first look at the emissions from construction of a generic 10,000 cubic yards of new hydroelectric dam. We used LCNetBase to model upstream and construction-phase emissions. LCNetBase output allowed us to consider emissions by chemical, supply chain tier and industry. This assessment is important in identifying emissions from the hydro fuel cycle that are similar by chemical type, rather than quantity or environmental impact, for all hydroelectric projects.

In section 5.2 we present the results of our assessment of upstream emissions from the New England and the La Grande complex hydroelectric projects. The results are normalized by the average annual megawatt hour output of each project over 50 years in order to compare the impacts in a common metric. In section 5.3 we present the results of our assessment of emissions from the operations-phase. In section 5.4 we combine upstream and operations emissions and present the results for small, medium and large dams.

4.2 Upstream Emissions to the Environment from the Hydro Fuel Cycle

In order to assess the upstream and construction-phase emissions of hydroelectric projects we calculated the materials and energy used to create a hypothetical 10,000 cubic yards of hydroelectric dam and associated superstructure. In the New England context, 10,000 cubic yards would represent the smallest hydro projects, with the largest projects extending well over a million cubic yards.

Eight emission categories were used to assess the total upstream environmental impacts of hydro projects. Table 8 summarizes the impact indicators.

Description (total upstream)	Measurement
Volatile organic compounds to air	Short Tons (ST)
Nitrogen oxides to air	Short Tons (ST)
Carbon monoxides to air	Short Tons (ST)
Sulfur dioxides to air	Short Tons (ST)
Particulate matter < 10 microns to air	Short Tons (ST)
Carbon dioxide from fossil fuel combustion to air	Metric Tons (MT)
Toxic releases to air, water, underground, land, public waste treatment, other off-site processes	Pounds (lbs)
Expenditures on freatment and disposal of all wastes	2000 dollars (\$K)
	Volatile organic compounds to air Nitrogen oxides to air Carbon monoxides to air Sulfur dioxides to air Particulate matter < 10 microns to air

Table 8 Upstream emissions from the hydro fuel cycle assessed in this study

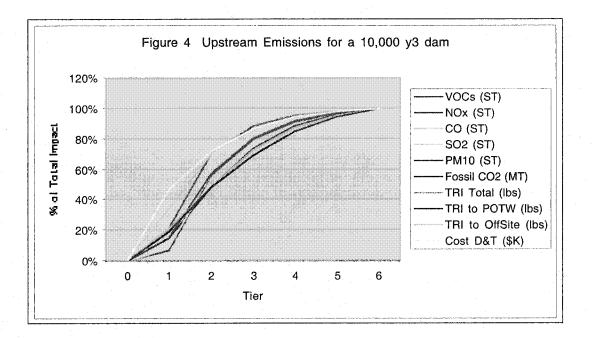
Table 9 summarizes the total upstream and construction-phase emissions associated with the eight indicators for 10,000 cubic yards of new dam construction. In this table, the toxic release inventory is further divided to highlight the direction of the pollutant flows.

Table 9 Upstream inventory	
results	Total
VOCs to air (ST)	1.06566
NOx to air (ST)	3.52334
CO to air (ST)	5.6916
SO2 to air (ST)	6.9435
PM10 to air (ST)	1.01954
Fossil CO2 (MT)	1514.17
TRI to Air (lbs)	713.64
TRI to Water (lbs)	73.397
TRI to UnGnd (lbs)	280.02
TRI to Land (lbs)	383.831
TRI to Total Environment (lbs)	1450.97
TRI to POTW (lbs)	160.841
TRI to OffSite (lbs)	3043.04
Cost D&T (\$K)	2.31648

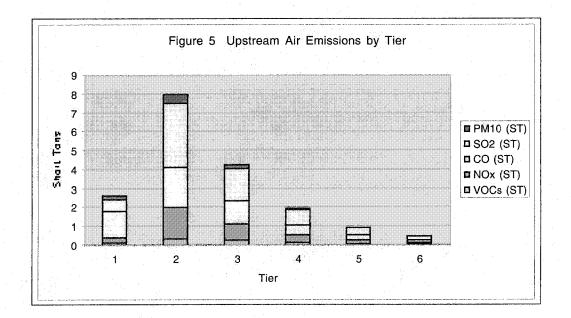
For our hypothetical dam project, upstream emissions range from 1 to 7 short tons of air pollutants. Approximately 1500 metric tons of CO2 would be released at other, off-site facilities along the supply chain and from fossil-fuel combustion during construction.

Figure 4 shows the emissions associated with upstream production tiers. The figure shows that the bulk of emissions, close to 80 percent, are associated with the first three tiers of production.

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Figures 5 through 7 highlight the upstream emissions for conventional air pollutants and CO2 releases for six of the upstream tiers. For all of the environmental impact categories, the majority of impacts occur in the second production tier. For air pollutants, SO₂, CO and NOx comprise the majority of releases and account for more than 7 short tons of emissions.



The second production tier accounts for the majority of upstream CO2 emissions. Figure 6 indicates that more than 550 metric tons of CO2 were released in the second production tier and that approximately 400 metric tons of CO2 were releases in the first production tier.

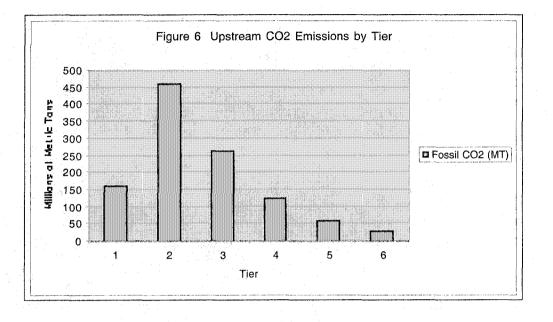
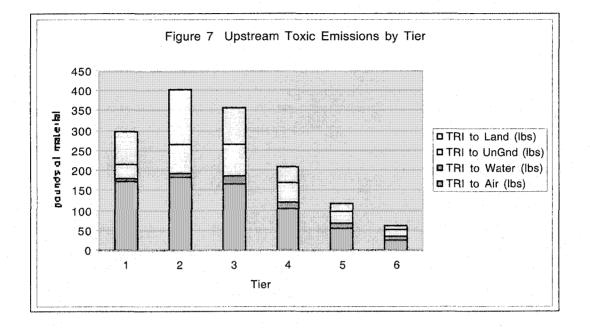


Figure 7 shows the upstream emission of toxic chemicals by tier. As with the other upstream emissions, the second production tier accounts for the majority of TRI releases with a cumulative total of approximately 1500 lbs. For all tiers, toxic emissions to air and land account for the majority of TRI emissions.

4.2.1 Upstream emissions by industry.

We reviewed the upstream impacts from various industries in order to understand which industrial inputs to hydroelectric dam construction contribute the largest environmental emissions. As with other factors assessed in the upstream analysis, the data is modeled in LCNetBase from the BEA "make and use" tables at the 500-commodity/industry level. The figures are presented in Appendix F. We considered the upstream emissions of pollutants associated with the 15 largest industrial producers of the emissions in the supply chain. No industry dominates all emission categories , however a number of industries are in the top five

producers of many of the pollutants, including blast furnaces, industrial inorganic and organic chemicals, and concrete and cement products.



For volatile organic compounds (VOCs) to the air, the top 15 industries account for approximately 75 percent of all VOCs produced from upstream material assembly and facility construction. The four largest emitters of VOCs are industrial inorganic and organic chemicals, petroleum refining, blast furnaces and steel mills, plastics materials and resins. These industries account for approximately 45 percent of all VOC emissions.

For upstream emissions of Nitrogen Oxides (NOx) to the air, the top 15 industries account for more than 95 percent of all NOx produced. The two largest industrial polluters of NOx, electrical services and hydraulic cement, are responsible for more than 65 percent of all upstream NOx releases.

For carbon monoxide (CO) releases to the air, the top 15 industries are responsible for more than 95 percent of upstream CO emissions. Blast furnaces alone accounts for more than 55 percent of these emissions, which is the single highest industrial producer of any of the emissions studied.

For upstream emissions of sulfur dioxide (SO2) to the air, the top 15 industries account for more than 95 percent of all SO2 produced in the cradle-to-gate scenario. The two largest industrial polluters of SO2, electrical services and hydraulic cement, are responsible for more than 65 percent of all upstream SO2 releases.

For upstream emissions of Toxic Release Inventory (TRI) chemicals to the environment, the top 15 industries account for more than 80 percent of all upstream TRI chemicals released. The two largest industrial polluters of TRI chemicals, blast furnaces and petroleum refineries, are responsible for approximately 85 percent of all upstream TRI releases.

For upstream emissions of particulate matter (PM10) to the air, the top 15 industries account for approximately 90 percent of all PM10 produced in the cradle-to-gate scenario. The two largest industrial polluters of PM10, hydraulic cement and blast furnaces, are responsible for more than 40 percent of all upstream PM10 releases.

For upstream emissions of carbon dioxide (CO2) to the air, the top 15 industries account for approximately 90 percent of all CO2 produced in the cradle-to-gate scenario, with two largest industrial polluters of PM10, motor freight and electrical services, responsible for approximately 36 percent of all upstream CO2 releases.

4.2.2 Other upstream inventory questions that could be explored with IO-LCA

Output from LCNetBase allows for a considerably more detailed study of upstream emissions data and results. For example, we could identify industries responsible for each release, to the chemical level, for each tier. We could graph material, product and service inputs for each type of emissions. And, we could categorize the largest emission contributors. However, such a detailed analysis is not pertinent to our research question and is, therefore, beyond the scope of this study.

	Model #	#of Dams in Group	Average Dam Volume (y3)	Average Annual MWh	Increase in Cubic Yards of Material (1000y3)
Small Dams	1	27	12,500	2,003	0-19
	2	29	29,186	2,355	20-39
	3	23	51,178	4,705	40-59
	4	15	67,551	8,974	60-79
	5	6	92,062	12,315	80-99
	6	7	109,818	13,606	100-120
	7	5	124,980	19,574	120-139
	8	5	150,940	19,320	140-159
	9	3	173,213	11,878	160-179
	10	4	190,796	27,445	180-199
Medium Dams	11	12	239,445	54,558	200-299
	12	11	350,824	86,435	300-399
	13	4	444,124	34,605	400-499
	14	2	536,410	64,700	500-599
	15	5	668,321	104,984	600-699
	16	2	769,542	30,644	700-799
	17	2	871,704	16,850	800-899
	18	1	905,072	228,042	900-999
Large Dams	19	5	1,335,549	51,517	Im
nasono (" por del Servero del Com	20	1 1	2,162,999	148,850	2m
	21	1	3,554,953	105,200	4m
an	22	2	6,800,742	277,800	5m
	23	1	8,018,947	356,064	6m
lydro Quebec	24	4	87,000,000	6,800,000	
0.0000000000000000000000000000000000000	Total	178	() NGC MARKAN	i ing shini na sa sa sa	a Maria Attackang

Table 10 Structural characteristics of hydro projects included in this study

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4.3 Upstream Emissions from New England & Hydro Quebec Projects

It is difficult to understand the results of life cycle models outside of a direct comparison between similar products. In this study, we compare upstream emissions between small, medium and large hydroelectric projects in New England normalized to a unit of energy output for each group.

	VOCs to air (ST)	NOx to air (ST)	CO to air (ST)	SO2 to air (ST)	PM10 to air (ST)	Fossil CO2 (MT)	TRI OffSite (lbs)	Cost D&T (\$K)
1	1.11E-04	3.68E-04	5.95E-04	7.26E-04	1.07E-04	1.58E-01	3.18E-01	2.42E-04
2	5.71E-05	1.89E-04	3.05E-04	3.72E-04	5.46E-05	8.11E-02	1.63E-01	1.24E-04
3	7.62E-05	2.52E-04	4.07E-04	4.97E-04	7.29E-05	1.08E-01	2.18E-01	1.66E-04
4	5.52E-05	1,83E-04	2.95E-04	3.60E-04	5.28E-05	7.85E-02	1.58E-01	1.20E-04
5	1.35E-04	4.47E-04	7.22E-04	8.81E-04	1.29E-04	1.92E-01	3.86E-01	2.94E-04
6	4.19E-05	1.39E-04	2.24E-04	2.73E-04	4.01E-05	5.96E-02	1.20E-01	9.11E-05
7	5.91E-05	1.95E-04	3.16E-04	3.85E-04	5.65E-05	8.40E-02	1.69E-01	1.28E-04
8	3.00E-05	9.91E-05	1.60E-04	1.95E-04	2.87E-05	4.26E-02	8.56E-02	6.51E-05
9	3.56E-05	1.18E-04	1.90E-04	2.32E-04	3.40E-05	5.05E-02	1.02E-01	7.73E-05
10	1.97E-05	6.52E-05	1.05E-04	1,28F-04	1.89E-05	2.80E-02	5.63E-02	4.29E-05
11	6.13E-05	2.03E-04	3.27E-04	3.99E-04	5.86E-05	8.71E-02	1.75E-01	1.33E-04
12	1.70E-05	5.64E-05	9.10E-05	1.11E-04	1.63E-05	2.42E-02	4.87E-02	3.71E-05
13	3.79E-05	1.25E-04	2.03E-04	2.471:-04	3.63E-05	5.39E-02	1.08E-01	8.24E-05
14	1.88E-05	6.22E-05	1.00E-04	1.23E-04	1.80E-05	2.67E-02	5.37E-02	4.09E-05
15	1.73E-05	5.73E-05	9.25E-05	1,13E-04	1.66E-05	2.46E-02	4.95E-02	3.77E-05
16	6.71E-05	2.22E-04	3.59E-04	4.37E-04	6.42E-05	9.54E-02	1.92E-01	1.46E-04
17	1.57E-04	5.18E-04	8.37E-04	1.02E-03	1.50E-04	2.23E-01	4.48E-01	3.41E-04
18	8.46E-06	2.80E-05	4.52E-05	5.51E-05	8,09E-06	1.20E-02	2.42E-02	1.84E-05
19	1.15E-04	3.79E-04	6.13E-04	7.47E-04	1.10E-04	1.63E-01	3.28E-01	2.49E-04
20	3.10E-05	1.02E-04	1.65E-04	2.02E-04	2,96E-05	4.40E-02	8.84E-02	6.73E-05
21	7.20E-05	2.38E-04	3.85E-04	4.69E-04	6.89E-05	1.02E-01	2.06E-01	1.57E-04
22	5.25E-05	1.74E-04	2.80E-04	3.42E-04	5.02E-05	7.46E-02	1.50E-01	1.14E-04
23	4.80E-05	1.59E-04	2.56E-04	3.13E-04	4,59E-05	6.82E-02	1.37E-01	1.04E-04
HQ	3.04E-05	9.30E-05	1.52E-04	1.84E-04	2.69E-05	4.04E-02	8.44E-02	6.30E-05

As described in the methods section, New England dams selected for this study were averaged together to represent small, medium and large dams. Within each category, models were developed to capture the gradual increase in superstructure volume, and the associated average

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annual generation for appropriate increases in dam size. Table 10 summarizes the models used throughout this analysis, including the number of dams averaged together in each model, the average volume of superstructure materials, average annual megawatt-hour output, and our trigger points for project size. The volume of superstructure materials and the average annual energy production for the Hydro Quebec model exceeds by an order of magnitude the largest New England projects assessed.

Upstream and construction emissions from New England and Hydro Quebec projects were assessed by multiplying structural material emissions with the structural characteristics of all individual project assessed. The results were normalized by dividing emissions into the average annual kilowatt output for the each project. Table 11 summarizes the upstream conventional air pollutants per megawatt hour. The model numbers listed in Column A correspond to the model numbers in Table 4.4. For each group of small, medium and large, we highlighted the project with the largest upstream emissions in yellow, and the smallest upstream emissions in green.

We found no pattern of emissions per unit of energy based on the size of the project. Some small projects, such as model 5, have large upstream emissions per MWh, while the La Grande project, model 24, has proportionally small upstream emissions.

Project	VOCs to air	NOx to air	CO to air	SO2 to air	PM10 to air	Fossil CO2	TRI OffSite	Cost D&T
Size	(ST)	(ST)	(ST)	(ST)	(ST)	(MT)	(lbs)	(\$K)
small	6.21E-05	2.05E-04	3.32E-04	4.05E-04	5,94E-05	8.83E-02	1.77E-01	1.35E-04
medium	4.81E-05	1.59E-04	2.57E-04	3.13E-04	4.60E-05	6.83E-02	1.37E-01	1.05E~04
large	6.36E-05	2.10E-04	3.40E-04	4.15E-04	6.09E-05	9.04E-02	1,82E-01	1.38E-04
HQ	3.04E-05	9.30E-05	1.52E-04	1.84E-04	2.69E-05	4.04E-02	8,44E-02	6.30E-05

Table 12 shows that with further averaging of the data, large New England dams tend to have slightly higher normalized upstream emissions per megawatt-hour output than smaller dams.

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Hydro Quebec's La Grande complex, though extremely large in scope, has an upstream environmental burden that is less than the New England average.

4.4 Operations Emissions from New England and Hydro Quebec Projects

As indicated in the introduction, numerous operations impacts were not included in this analysis. The limited available data and uncertain methods for quantifying the impacts made assessment of impacts such as bio-diversity losses, changes in sedimentation patterns, or impacts to anadromous fish, both site-specific and difficult to quantify. However, recent discovery of greenhouse-gas emissions and methyl mercury releases from reservoirs provided adequate data to estimate these operations-related impacts for New England and Hydro Quebec. Table 13 summarizes the operations per unit of energy for the assessed projects.

The methyl mercury cycle in new reservoirs is considered to be short (Kelly 1997). The initial bloom of organic mercury is thought to decline to background levels over 10 years following flooding. When amortized over 50 years of electricity generation, the impact of the initial bloom is small compared to other flows assessed in this study. On a per megawatt-hour basis, we found that short tons of methyl mercury emissions from New England dams range from 1*10⁻⁶ to 1*10⁻⁹ per megawatt hour. Methyl mercury per megawatt hour released from New England projects during operations is many times smaller than the toxic chemical emissions that result from construction activities. This is due in part to the small total active and passive volume of water in reservoirs as compared to the lifetime generation of the hydro project.

The mobilization of methyl mercury at the Hydro Quebec La Grande complex is considerably higher on a per megawatt-hour basis than that of the New England projects. We assessed the emissions to be on the order of $1*10^{-1}$ short tons per megawatt hour, approximately 10 times higher than the worst – case New England example. In addition, methyl mercury at the La

Grande complex represents a higher portion of toxic chemical emissions than those released during the construction phase. This can be explained by the relatively large volume of reservoirs to the power generated.

	Model #	CO2 Equivalent Emissions (ST/ MWH)	Methyl Mercury (STMWH)
Small	1	0.599039	0.007001
	2	0.312365	0.005575
	3	0.450178	0.028905
ingener Lingen sold	4	0.025183	0.000613
	5	0.025323	0.001139
fi serie	6	0.026986	0.000790
	7	0.034714	0.000581
	8	0.030140	0.001001
	9	0.030081	0.000959
	10	0.012619	0.000396
ledium	11	0.048233	0.002543
	12	0.025875	0.000908
	13	0.487170	0.034605
	14	0.058558	0.001332
	15	0.061705	0.003563
	16	0.048232	0.002884
	17	0.920742	0.090743
	18	0.476056	0.042660
arge	19	0.181312	0.014916
	20	0.077244	0.005063
	21	0.010577	0.000033
	22	0.030594	0.006086
	23	0.033749	0.008039
	Hydro Quebec	1.822602	0.155703

Table 13 Total operations-phase emissions of CO2 and

Releases of CO₂ equivalent greenhouse-gases during the operation phase of the hydro life cycle represent a large portion of the total emissions from New England and Hydro Quebec projects. In New England, operations-phase greenhouse-gas emissions range from .01 to .92 tons per

megawatt hour. In all cases, greenhouse-gas emissions are many orders of magnitude larger than the greenhouse-gas equivalents released during the construction phase.

Emissions of CO2 equivalent greenhouse-gases from the Hydro Quebec projects assessed in this study represent the largest flow of emissions during the operations-phase of the life cycle. We calculated just under 2 tons of greenhouse-gas emissions per megawatt hour. As with methyl mercury releases during the operations-phase, the large contribution of greenhouse-gas emissions from the Hydro Quebec model can be explained by the large volume of impounded water as compared to annual average generation.

CHAPTER V

DISCUSSION OF RESULTS

5.1 Introduction

In this section we look at methods for assessing individual projects against regional averages using simple ratios. Total emissions from the construction and operations-phases of hydroelectric facilities vary according to certain characteristics described in the previous section. We have found that simple descriptive ratios can provide substantial information about the environmental burdens of individual projects against the regional averages.

Hydroelectric projects with a large volume of construction materials embodied in superstructures and with relatively low electricity generation will produce larger upstream emissions per unit of energy generated from the facility. This suggests that, relative to baseline averages, a low ratio of dam volume to energy produced would be indicative of low upstream environmental emissions.

5.2 Energy Output as a Function of Dam Size

Table 13 appears to suggest that the annual megawatt-hour output of hydroelectric facilities increases with the volume of construction materials used in the superstructures. As discussed in the methods section, this is a common assumption embedded in other quantitative assessments of the hydro fuel cycle. However, generation and total volume of inputs do not appear to be tightly

correlated. In Figure 8, we graph the volume of materials in the superstructure against the average annual kilowatt-hour output for each of the New England hydro projects. The graph shows that average annual energy production increases as dam size increases. However, there is considerable variation in average annual generation for all of the facilities assessed. Some large projects generate small amounts of electricity.

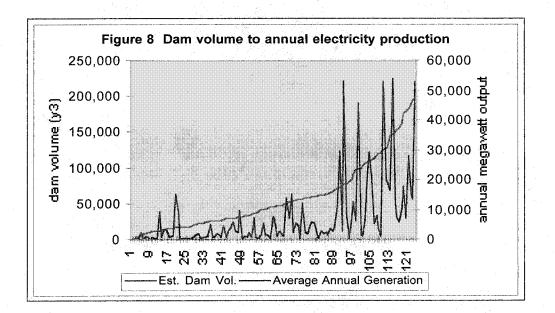
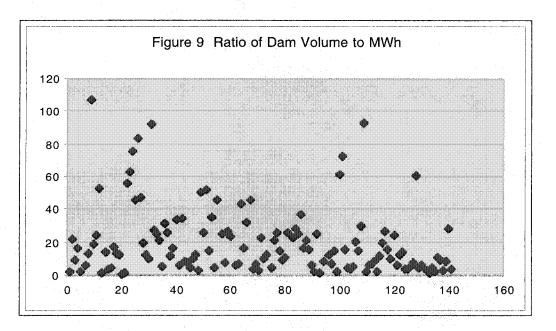
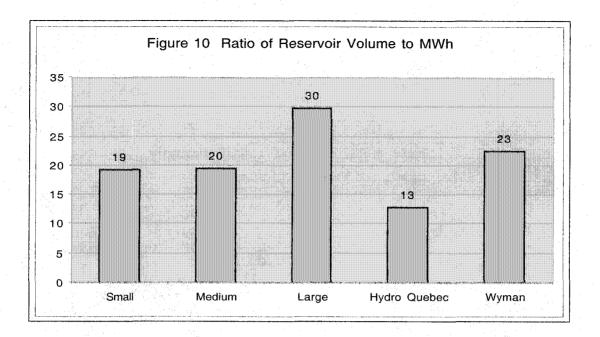


Figure 9 provides another view of the same data. Plotting the ratio of total dam volume to average annual energy production shows that there is little relationship between project size and energy output.

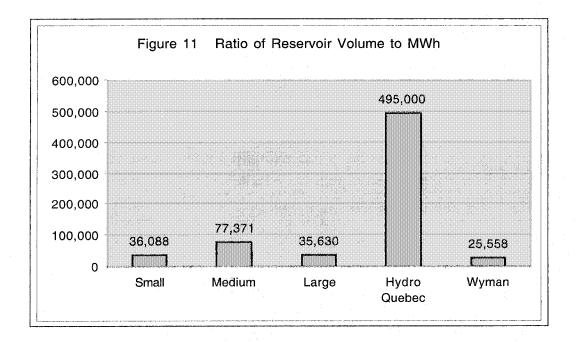


For demonstration purposes, we consider the Wyman Hydroelectric project (FERC # 2329.0101) located on the upper Kennebec River in northern Maine. The Wyman project has the largest dam volume and generates the most electricity of those New England projects assessed in this study. However, the project has a proportionally small reservoir and active generation volume. Ratio analysis, as summarized in Figure 10, indicates that the Wyman project has smaller upstream emissions per unit of energy when compared with other large New England projects. However, the upstream burdens from the Wyman project are marginally larger than small and medium-sized New England projects, and considerably larger than those of the Hydro Quebec projects.

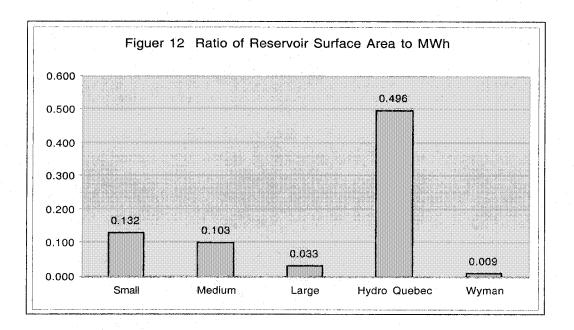


Similar descriptive ratios can be constructed for methyl mercury and greenhouse-gas emissions during the operations-phase. For methyl mercury, the descriptive ratio is the volume of impounded waters per unit of energy for a given project. Figure 11 summarizes mercury emission ratios. The Wyman project has proportionally small operations emissions of methyl mercury as compared to any of the New England baseline averages. Methyl mercury emissions from Wyman are many times smaller than emissions from the La Grande complex, as is the case with all of the New England projects.

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For operations-phase greenhouse-gas emissions, the descriptive ratio is the final flooded surface area per unit of energy. The Wyman impoundment is characterized by a long, thin reservoir that follows the natural channel of the Kennebec River. Steep canyon walls reduced flooded surface area in proportion to the electricity generated. Figure 12 shows that greenhouse-gas emissions from the Wyman project are 10 times less that those associated with large New England projects and more than 100 times less than those of the Hydro Quebec La Grande complex.



CHAPTER IV

CONCLUSIONS

The primary purpose of this paper was to construct a quantitative profile of external upstream and operations emissions from the hydro fuel cycle. The results of this study provide baseline data for further research in the valuation of the external impacts of the hydro fuel cycle. We hypothesized that external emissions are not zero and that small dams would have smaller emissions per unit of energy.

Using IO-LCA methods and LCNetBase software, we were able to profile upstream and construction-phase emissions. Using conventional LCA methods, we included two operations-phase emissions. We included 174 New England concrete hydroelectric dams and the four concrete dams associated with the Hydro Quebec La Grande project. Our model allowed us to consider emissions at both individual facilities as well as averages for the entire collection of hydroelectric facilities within the region.

We were unable to quantify many site-specific environmental impacts from the hydro fuel cycle, including impacts to water quality, fisheries and changes in land use. We determined that these impacts could be considered in site-specific analysis, but insufficient data was available for inclusion in our general profile of regional hydro assets.

We confirmed the first part of our hypothesis: that the emissions from the hydro fuel cycle are not zero. Both upstream and operations-phase activities generate direct and indirect emissions to air, water and land. Table 14 summarizes the emissions from the hydro fuel cycle during upstream and operations-phase activities. This data, and the associated model, provides sufficient detail to estimate societal values of hydro fuel cycle emissions.

Quebec proje	ects (metric/MW	h)	•		·
	VOCs (ST)	NOx (ST)	CO (ST)	SO2 (ST)	PM10 (ST)
Small NE	1.88E-05	6.22E-05	1.01E-04	1.23E-04	1.80E-05
Medium NE	3.11E-05	1.03E-04	1.66E-04	2.03E-04	2.98E-05
Large NE	5.17E-05	1.71E-04	2.76E-04	3.37E-04	4.94E-05
Hydro Quebec	3.04E-05	9,30E-05	1,52E-04	1.84E-04	2.69E-05
	Fossil CO2 (MT)	TRI Air (lbs)	TRI Water (lbs)	TRI UnGnd (lbs)	TRI Land (lbs)
Small NE	2.67E-02	1.26E-02	1.30E-03	4.95E-03	6.78E-03
Medium NE	4.42E-02	2.08E-02	2.14E-03	8.17E-03	1.12E-02
Large NE	7.34E-02	3.4612-02	3.56E-03	1.36E-02	1.86E-02
Hydro Quebec	4.04E-02	2.01E-02	2.04E-03	7.72E-03	1.06E-02
	TRI POTW (lbs)	TRI Off-Site(lbs)	Cost D&T (\$K)	CO2 Equiv (ST)	MeHg (ST)
Small NE	2.84E-03	5.38E-02	4.09E-05	1.55E-01	4.70E-03
Medium NE	4.69E-03	8.88E-02	6.76E-05	2.66E-01	2.24E-02
Large NE	7.80E-03	1.48E-01	1.12E-04	6.67E-02	6.83E-03
Hydro Quebee	4.45E-03	8.44E-02	6.30E-05	1.82E+00	1.56E-01

	rmalized extern			
	ects (metric/MV			

We incorrectly hypothesized that small New England hydroelectric facilities would emit a smaller quantity of emissions per unit of energy than larger projects. We assumed that sites with smallest infrastructure requirements relative to annual inflow and hydraulic head would have been developed first and would have proportionally low emissions compared to annual generation. However, when considered individually, the size and the age of the project have little bearing on the quantity of emissions per unit of energy. Certain small projects and certain large projects have very small emissions per megawatt hour, while other small and large projects have very high emissions per megawatt hour. The unique characteristics of the Hydro Quebec projects assessed

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in this study suggest that the life-cycle emissions per megawatt hour greatly exceed those of the New England pool. The Hydro Quebec operations-phase emissions are on an order of magnitude larger than the New England average.

In testing the second part of our hypothesis, we found that three simple ratios, dam size, reservoir size and reservoir surface area to annual generation, provide quick and simple estimates of the upstream and operations emissions assessed in this study. These ratios can be used to compare individual projects to regional averages, allowing for simple marginal assessments of proposed projects that are similar in size and annual average generation to existing projects.

PART II

LIFE CYCLE IMPACT ASSESSMENT OF THE HYDRO FUEL CYCLE

CHAPTER I

INTRODUCTION

This paper is the second in a series of three describing our Life Cycle Assessment (LCA) model of hydro emissions and externalities. In this paper, we conduct an LCA impact assessment of the hydro fuel cycle using economic valuation.

We have two main objectives. The first objective is to identify assumptions and problems in the application of economic valuation to LCA inventory data that can lead to erroneous results. To address this objective, we review the Craighill and Powell (1996) LCA impact assessment methodology, which borrows per unit economic damages from past studies, in order to understand how assumptions in economic studies are recognized, adjusted, or hidden when combined with LCA. We then consider the appropriate conditions for combining the Damage Function Approach (DFA), which is often used in economic valuation studies, with LCA in order to present more comprehensive impact assessment results. We develop heuristic tests to inform the level of detail needed in combining per unit economic damage values with the quantity of emissions estimated in LCA models. We suggest that the Craighill and Powell methodology is appropriate for average assessments of external impacts, particularly when assumptions embedded in the per unit economic valuation data are made explicit, or adjusted to dovetail with the assumptions in the LCA model. We anticipate that LCA impact assessments conducted using

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DFA will provide additional detail and be appropriate for marginal, site-specific assessments of externalities.

Our second objective is to develop baseline, average externality estimates for the hydro fuel cycle in order to incorporate recent scientific understanding of hydro impacts into estimates of net external damages. In the first paper in this series, we developed an inventory assessment of upstream and operations-phase emissions for 174 New England concrete hydroelectric projects and four projects associated with the La Grande complex in Quebec. In this paper, we develop an impact assessment by combining the results of the inventory assessment with economic valuation. We follow the Craighill and Powell methodology and provide additional detail about our economic valuation step.

We find that the construction and operations-phase emissions assessed in this study are significant and measurable, and that the size of the hydro project is not useful in predicting normalized average emissions. We estimate the following average externality values for the hydro fuel cycle: small NE dams = 0.0343/kWh, medium NE dams = 0.0202/kWh, large NE dams = 0.0193/kWh, Hydro Quebec, La Grande Complex = 0.0461/kWh⁵.

Our results indicate that the average external impacts from the hydro fuel cycle are less than, but similar to, the external costs of fossil fuel cycles. However, more detailed assessment of individual projects shows that emissions from the majority of hydro projects are very small compared to fossil fuel cycles. In contrast, site-specific characteristics, and a handful hydro projects greatly exceed emissions per unit of energy for the coal fuel cycle, and significantly increase our average estimates for small, medium and large New England dams.

⁵ In this paper, all dollar units are reported for the year 2000 cost basis unless otherwise noted.

We conclude that life cycle assessment and economic valuation provide a useful and affordable methodology for assessing some of the external impacts of the hydro fuel cycle. The methodology allows for direct comparison of impact pathways in common units, as well as comparison of individual, site-specific projects against regional baseline estimates.

This paper is divided into six sections. In section 2 we discuss common LCA impact assessment methods with a focus on economic valuation. We present the Craighill and Powell methodology for combining LCA inventory output with economic valuation. We also consider the Damage Function Approach (DFA) used in economics for estimating net externalities at the margin. We identify important assumptions embedded in LCA with economic assessments and discuss the ability to transfer damage values between studies. In section 3 and 4 we present our methods and results for hydro impact assessment with economic valuation. Section 5 we consider our average externality estimates in the context of previous hydro externality studies, and we recommend steps for improving the transparency and validity of IO-LCA with economic valuation. Our conclusions are in section 6.

CHAPTER II

ECONOMIC VALUATION IN THE IMPACT ASSESSMENT

2.1 Introduction

One of the primary purposes of LCA modeling is to provide information for public decisions and policies about the environmental consequences of future actions (Fava 1991). Of concern to decision makers may be the impacts and costs of alternative technologies, the development of methods for designing new technologies that minimize total environmental burdens, or the identification of components within existing technologies that have the greatest external impacts. In LCA modeling, quantifying the emissions from material and energy use in a product or process is known as the inventory assessment. Translating the emissions into social, economic and ecological impacts is referred to as the impact assessment.

The majority of LCA studies conducted in the U.S. do not extend beyond the inventory assessment (Hunt & Franklin 1995). However, as it relates to public decisions and policy, problems arise when LCA studies are restricted to the inventory stage (Powell et al. 1997). Quantifying emissions in the inventory stage of LCA modeling does not inform society about the effect emissions have on the environment, human health, buildings, equipment, and other social factors. As Craighill and Powell (1996) state, "it is not the emissions themselves, but their resulting impact upon the environment with which we are concerned."

LCA impact assessment allows for direct comparison of the impacts from emissions by placing value on emission parameters. The parameters are typically in common metrics such that the associated impacts can be compared between emissions categories, and summed for an assessment of cumulative impacts. When conducted, the impact assessment is often considered a controversial step in LCA methodology, in part because it requires the analyst to weight the relative impacts of unrelated emission flows on society. While the impact assessment allows us to compare emissions in a common metric, analysts must make assumptions about which emission has greater impacts on society and weight the impacts accordingly. The associated controversy has limited the use of LCA modeling in public policy (Shankle and Humphreys 1998).

Another factor that has limited the use of LCA in public policy is its focus on emissions from existing products or processes (see Rafenberg and Mayer 1998, Legarth et al., 2000). From a local, regional and state public policy perspective, emissions and impacts from the life cycle of existing products are only useful in so far as they inform strategies to minimized marginal impacts from future decision within a set of constraints (Mitchell and Carson 1989). LCA models concerned with past emissions are less helpful in making future decisions than assessments focused on the impacts of a proposed action. For example, quantification of the impacts from an existing recycling scheme is less useful to a municipality or a county in deciding what system to adopt than a study that considers the costs and impacts from a number of proposed waste disposal actions.

Also, from a public policy perspective, total impacts from a product or process are of less concern than those impacts that are external to the private costs of operations (Kahneman and Knetch

1992). Many impacts from a product or process may be incorporated in the costs of operations. For example, a hydro facility may reduce access to fishing and other recreation opportunities along a river. Regulation, however, may require the owners to build fishing access facilities. These costs would be included in the costs of operations. In contrast, the facility may reduce populations of anadromous fish, such as salmon, which could have impacts on commercial fisheries and reduce bio-diversity in the watershed. If regulation does not require the owners to mitigate for these costs, then these costs are external to the costs of doing business and are borne by society. From a policy perspective, it is the private costs, plus these costs which are external to private costs, that are of concern. Private costs plus external costs are referred to in this study as the total social costs.

In this section (2), we briefly review LCA impact assessment methodology, with a focus on economic valuation methods currently used. Then we consider problems in the impact assessment step when using economic valuation. Finally, we recommend heuristic measures for choosing the level of detail needed in the economic valuation impact assessment in order to fit within the scope of the LCA study and the type of public policy decisions to be made. We make three primary points in this section. First, of the LCA methods currently used for impact assessment, economic valuation is the most appropriate for policy decisions as it is focused on measures of total social costs, can provide estimates of marginal and average damages, and allows for consideration of externalities. Second, the methods currently used to combine LCA with economic valuation have deeply embedded assumptions, including assumptions about time-value, intergenerational equity and the value of human life. Third, the accuracy and applicability of LCA impact assessments of change at the margin.

2.2 Impact Assessment Using Distance-to-target, Cost Control, and Scoring

Four methods are commonly used in LCA to choose weights for the emissions identified in inventory assessment: distance-to-target, environmental control costs, scoring, and economic valuation⁶ (Powell, et al. 1997). The distance-to-target approach calculates weights for emissions by measuring the extent to which environmental performance exceeds desired standards (SETAC 1996) For example, if the actual level of PCBs in a water body is 11/ppm and the target level is 10/ppm, then a weight of 10 percent would be assigned to the impact. This method works on the assumption that the social and political processes for developing environmental standards represent the best possible action for maximizing social welfare.

The environmental control costs method determines weights for emissions by comparing the expenditures necessary to control the environmental damages for each impact (Powel et al. 1997). If controlling environmental damage requires 100 dollars per unit for one impact and 200 dollars per unit for a second impact, then the second impact would be assigned a weight that is two times larger than first impact.

The scoring method relies on expert testimony, or, in some cases, stakeholders to determine weights for the environmental impacts (Powel et al. 1997). Two stages are required to determine the appropriate weights. First, the panel ranks the extent to which emission flows initiate further damages to the environment. Second, the panel ranks each pollutant relative to all the other pollutants analyzed.

⁶ Economic valuation is not considered part of the SETAC or ISO 14000 methods for calculating environmental impacts in LCA studies. However, the methodology has been established in economic cost-benefit studies, and it is being applied by LCA practitioners.

A number of problems with these three methods have been recognized (Shankle & Humphreys 1998, Powel et al. 1997). Because environmental standards are set through political processes, they do not necessarily represent a scientifically "optimum" solution that utilizes natural and human resources, including ecosystem benefits, to maximize social welfare.

Another problem with these methods is the fact that not all material and energy flows identified in LCA models will have associated standards (Powel et al. 1997). The Society of Environmental Toxicology and Chemistry (SETAC), recommends ignoring impacts from flows with no associated standard, on the assumption that no standard is a statement that society does not value the flows (Fava 1991).

Finally, results from the impact assessment using these methods tend to be irreproducible within or between countries (Powel et al. 1997). In addition, relatively few studies have been conducted, so established ranges for impact assessment weights are not available in peer-reviewed literature.

2.3 Impact Assessment Using Economic Valuation

The guiding principal behind economic valuation is to calculate changes in well-being of those affected by the emissions identified in the inventory assessment (Pearce 1995, Bockstael et al. 2000). LCA models estimate the emissions from a product or process and economists estimate the economic costs of impacts through assessments of willingness-to-pay (WTP) for a change in well being before the change has occurred. Assessing this change is performed through the use of a set of indirect methods, such as travel-cost and hedonic measures, or direct questioning studies, known as contingent valuation. Both direct and indirect methods estimate the amount of money people would be willing to pay, or willing to accept, to avoid the changes in their personal

experience caused by the emissions. The resulting estimate in dollars is used as a proxy for the social and environmental damages caused by the emissions.

One of the first LCA impact assessments with economic valuation was developed as part of a LCA of curbside recycling (Craighill and Powell 1996). The arguments for LCA with economic valuation were further refined in a review of impact assessment methodology conducted for SETAC (Powell, Pearce and Craighill 1997). Extensive research has been conducted using WTP to identify the externality value for numerous impacts. Low, medium and high estimates for numerous emissions categories are available in peer-reviewed literature. New studies verifying past estimates and estimating impacts from previously untested emissions are regularly undertaken (Aldred 1994; EPA 1998, Bockstael et al. 2000).

The methodology for establishing WTP estimates, though controversial, is well established in public policy domains and continues to be refined through academic dialogue. WTP models have been used in these fields for more than 40 years with increasing acceptance. A database maintained by Environment Canadian lists more than 2000 published WTP studies, and more than 50 countries utilizing these methodologies for public policy purposes (Carson 2000). In 1993, Robert Solow and Kenneth Arrow hosted a panel of economists at the National Oceanic and Atmospheric Administration (NOAA) in order to determine the validity of WTP analysis in public policy. The panel recommended guidelines for use in natural resource damage assessments to help ensure the reliability of WTP survey instruments, including the use of inperson interviews, a binary discrete choice question, a careful description of the good and its substitutes, and several different statistical and subjective tests of the survey results. Since the panel issued its report, many empirical tests have been conducted, and many key theoretical issues have been clarified (Carson 1999). Though more work needs to be done in developing

economic valuation methodology, economists continue to refine the methodology, improve the quality of the results, and reduce the level of error.

Of the methods used to assign value in the LCA impact assessment, economic valuation tends to be the most transparent. Brent (1996) points out that one cannot avoid making value judgements when making social decisions. Rather than avoiding subjectivity and value judgements, modeling social impacts involves a question of whether assumptions are implicit or explicit in the model. Assumptions about social values are deeply embedded in any of the methods previously discussed (Powell et al. 1997). Political positions used in crafting policy, or in the personal opinions of experts, make reproducing results from other impact assessment methods difficult to impossible. Understanding what assumptions are at work when an agency or legislative body sets target emissions is, to say the least, difficult. In contrast, the assumptions made in estimating economic parameters are typically identified in the background studies. If assumptions are appropriately presented, analysts can test previous results with similar methods, and explore the relationship between assumptions and the estimated parameters (DOE 1995, Shankle et al. 1998, Frankhauser 1994, EPA 1998).

Finally, economic valuation results, based on willingness-to-pay estimates of damages, are consistent with the general goals of maximizing social welfare, a fundamental tenet of economic thought (Brent 1996). A principal goal of welfare economics is to ensure that society as a whole benefits from policy and regulatory actions, even if some individuals are negatively impacted. Economists argue that external costs affect all members of society and that market prices are not a good substitute for individuals' willingness to pay to avoid the impacts. Economic valuation reflects a social price, or a price that is adjusted to reflect the effects market prices do not capture.

The results of economic valuation impact assessment are tailored for use in actions that maximize social welfare.

In addition to these four benefits of economic valuation over other LCA impact assessment methods, Craighill (1996), Powell (1997) and Pearce (1995) argue that economic valuation is technically easy to apply to inventory assessment output. Results from the inventory assessment are in heterogeneous units for each emissions category, such as SO2 in metric tons, and toxic chemicals in standard pounds. Results for economic valuation studies are typically in dollars per unit. For example, economic valuation results for SO2 are reported in dollars per metric ton. Calculating social and environmental impacts for SO2 is as simple as multiplying the quantity of emissions by the estimated per unit value.

2.4 Uncertainty and Embedded Assumptions

Four types of uncertainty exist with the economic valuation methodology. First, the methodology for combining LCA inventory output with economic valuation is still evolving, and the array of externality estimates available does not cover all impact flows that may be calculated in LCA models. In addition, externality estimates are typically developed as marginal estimates for one location. Transferability of per-unit externality values, without significant adjustment to the local conditions of the LCA study site, is limited (Krewitt 1999).

Second, the combination of externality estimates with LCA output following the Craighill and Powell methodology assumes that each unit of pollutant has the exact same impact as subsequent units. This leads to average assessments of damages (DOE 1995, ExternE 1995&1997). In reality, the impacts are site-specific and can be larger or smaller depending on regional

characteristics, such as population density, critical habitat, and other biological systems that might mitigate, or magnify, the damages caused by the flow of pollutants.

Third, though increasingly rare, some academicians argue that the use of existence values, or value that extend beyond market values, has no place in economic analysis (Aldred 1994). Existence values are not consumed and do not, therefore, fit the economic definition of a preference. However, Krutilla (1967) observed that people do place value on natural resources, and excluding existence values from economic analysis would place a zero, or very low, value on any public good or environmental damage.

Fourth, there are still outstanding technical issues involved in quantifying individuals and societies' willingness-to-pay. Some argue that irreproducibility of results from WTP models is symptomatic of anomalies associated with individual studies (Aldred 1994, Carson 2000). The debate tends to focus on the shortcomings of the various WTP methods and whether they result from the problems of particular methods or reflect deeper problems in WTP models.

Uncertainty with the results requires that the final output of LCA economic valuation should be considered order-of-magnitude estimates of damages (Powell et al. 1997, Krewitt 2001). WTP models are highly simplified pictures of real-world processes. The errors associated with each step in the externality modeling process, as well as those associated with the LCA modeling process, are combined in the final output. In addition, the WTP methodology is still evolving, along with the scientific understanding of the effects emissions have on society. It is probable that certain flows and impacts are left out of the assessment.

2.5 Example of Embedded Assumptions with Economic Valuation

In order to demonstrate how uncertainty is magnified in LCA impact assessment with economic valuation, we take a closer look at the valuation step in the Craighill and Powell (1996) curbside recycling versus waste disposal study. We focus on their valuation of greenhouse-gas emissions in order to identify some of the assumptions that are deeply embedded in their results. Though we focus on greenhouse-gas valuation estimates used in their study, the analysis is applicable to their method of applying other per unit estimates of damages.

Craighill and Powell quantified the greenhouse-gas emissions for each stage of the life cycle and multiplied these total emissions by the cost per unit of emissions estimated in Frankhauser's (1994) externality study in Great Britain. Their report provides no assessment of Frankhauser's externality results and assumptions, or the transferability of his per-unit estimates to the local conditions in rural England. However, to run Frankhauser's model of the marginal costs of greenhouse-gases requires a set of assumptions which are relevant to the question of external impacts calculated in the Craighill and Powell model.

Table 15 summarized the assumptions and sources of data used in Frankhauser's greenhouse-gas study. Each of these micro questions requires a set of assumptions. Frankhauser is explicit in his assumptions, and identifies the source from which his positions are derived. However, there is no way to dismantle and reconstruct Frankhauser's model with different assumptions. If, for example, we assume that the GNP will remain steady or actually decline over the next 200 years, or that the appropriate discount rate is zero for intergenerational projects, then we must reject Frankhauser's results. Frankhauser's assumptions about the structure of populations and economic systems, as well as the behavior of biochemical and ecological systems, are deeply embedded in the Craighill and Powell study.

Table 15 Assumption	is in Frankhauser (1994) that are implicit in Craighill ((1996) and Powell
(1997)		
Micro Question	Assumptions	Source
Ambient Stock of Pollutant	Size of stock based on pre-industrial atmospheric concentrations Non linear decay rates to carbon sinks	Schmalensee (1993)
Source & quantity of future Emissions	Populations growth at 1990 rate Gross national product growth rate 1-2% No policy to reduce GHG emissions Fossil fuel use at 1990 rates Deforestation at 1990 rates	IPCC (1992)
Accumulation of emissions	Nonlinear decay rate Absorption to other stocks	Hasselmann (1987)
Radiative forcing of per unit increases in stock concentrations	Relationship between ozone, total stock and forcing Excludes overall cooling effects of other emissions	IPCC (1990)
Rate of global temperature rise	Temperature rise in atmosphere, upper oceans, deep oceans.	Nordhaus (1992)
Annual damages	Accept optimum gas emissions curve as baseline. Damages increase as populations grow and economies change. Threshold conditions exist where ecosystem is unable to adapt Include market & non market damages	Frankhauser
Discounting	Social time preference rate	Frankhauser

Assumptions for other emissions and environmental damages are equally important to the results of both the per-unit values and the resulting LCA impact assessment conclusions. For example, the assumed value of human mortality, which is necessary data for assessing health effects from emissions or traffic accidents, ranges from \$500,000 to more than \$4,000,000 (Lee 1995). These differences can result in fundamentally different estimates of per-unit value. It is unclear in Craighill and Powell what assumptions are included in their unit values and how these assumptions dovetail with the authors' position.

In economics, a significant issue is the transferability of WTP estimates from one location to another (DOE 1995). The three studies used for per-unit damage estimates were conducted as marginal estimates. The location of populations, environmental attributes and economic activities relative to the site assessed are important in marginal externality studies, to the point that damage estimates are rarely transferable from one study to the next. For example, the value external damages associated from SO2 releases as assessed in the Ohio Valley may not be transferable to

rural Quebec locations In general, economists recommend adjusting WTP estimates to sitespecific marginal impacts.

Although Craighill and Powell's method of multiplying of per-unit damages estimates with the quantity of emissions released is technically easy, their methods embed implicit assumptions and off-site specific attributes in their results.

2.6 Average versus Marginal Assessment

Craighill and Powell use estimates of existing damages from one curbside recycling scheme and one waste disposal scheme to consider which method has the least overall environmental burden. However, from an economic perspective, comparing the impact of existing methods is of less concern than comparing the impacts associated with a proposed project. Economists consider past impacts, including those associated with past capital expenses and emissions, to be sunk. The emissions are released, and the product or process cannot recapture past actions.

What Craighill and Powell have provided is a first cut assessment of average damages from the two systems such that it generally informs communities about future waste versus recycling-related decisions. Estimates of average damages consider the impacts from, ideally, a pool of representative products or processes normalized on an appropriate per-unit metric (PACE 1990).

In contrast, marginal damages are the impact of a one-unit change in the output of a product or process as compared to baseline conditions. Marginal damages are of central concern in economic and policy analysis of the environmental consequences of a product or process. From an economic efficiency perspective, regulators would raise compliance standards for a new project if the new standards would reduce damages more than they would raise the costs of

compliance. Stated in economic terms, regulatory standards should be adopted if the marginal damages avoided exceed the marginal costs.

As it relates to our study, assessments of average damages provide insight into certain characteristics of the hydro fuel cycle, such as facility siting and emissions profiles, that are necessary to understand the impacts from more site-specific assessments related to future decisions. For example, the size of local populations, aesthetic considerations, size and depth of the reservoirs, structure of the dams and materials used may be significant determinants of external costs.

However, average costs are not appropriate for considering the external damages from an individual product or process, because average costs can significantly under or over estimate the environmental costs at the margin. In situations where all components of the environmental impact pathway are linearly related, then marginal damages would equal average damages. But this condition is not supported by scientific understanding of how emissions disperse from a source, which suggests that distance, atmospheric conditions and other factors create nonlinear relationships between emissions and damages (DOE 1995). Under nonlinear conditions, valuation based on average physical damages and average costs will underestimate damages at high pollution levels and overestimate damages at low levels. Ideally, damages from each incremental unit of ambient pollution would be estimated and linked to changes in pollutant emissions, such that marginal damages per unit of emissions could be estimated.

From a state perspective, where externality "adders" are often used to adjust market prices to reflect social damages, marginal assessments of the fuel cycle are of primary concern. State public utility commissions (PUCs), with a charter of maximizing social welfare, typically focus

on delivering power at its least social cost. Before deregulation of electricity markets was initiated in California and Pennsylvania, a majority state-level regulatory efforts included accounting for external damages in all new investment decisions (Lee and Drummer 1994). To achieve this regulatory objective, state PUCs must take the existing pool of generation assets and existing policy controls as an existing condition, such that they are forced to ignore measures of the optimal generation mix and focus instead on choosing technologies with the lowest social costs to meet new electricity demand. Often described as "least costs planning," regulations based on social costs require utilities to accept projects with the lowest social costs, even if the market prices are higher than other choices, but they do not require the utility or rate payers to actually pay the difference between market and social prices.

From a Federal perspective, marginal assessments are also of primary concern. Incentive-based regulation, such as tradable permits, require a detailed understanding of the social costs of pollution so as to quantify the economically efficient level of emissions control and the associated number of permits to be issued. However, technical issues interfere with accurate federal-level estimates of marginal damages (Lazzari 2000). For example, practical federal-level estimates demand ignoring a central tenet of marginal damage analysis: damages are site-specific. In addition, federal policy is typically concerned with larger regions where numerous types of economic activity take place. It is difficult to imagine a social cost study that explicitly estimates damages and benefits at all sites across the continent. The most common method for estimating social costs at the federal level is to ignore the dynamic effects of emission impacts on local economies and generalize with average estimates of damages for some representative or average site (DOE 1995). Simplicity requires accepting the assumption that impacts from pollutants follow linear increases and decreases. Stated another way, average assessments of social costs are the most practical means for assessing external damages on the federal level.

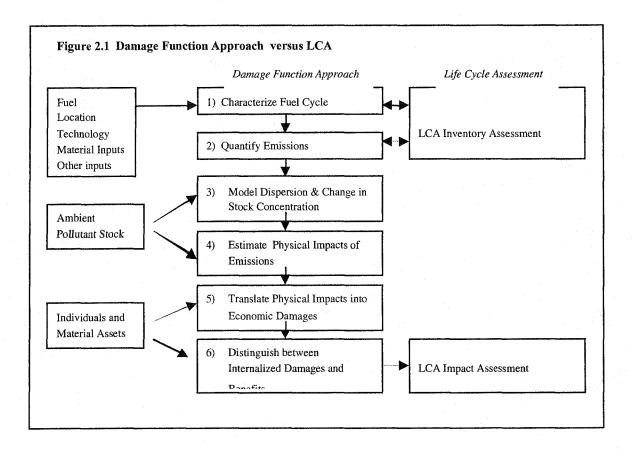
2.7 Economic Damage Function Approach

The economic damage-function approach (EDFA), summarized in Figure 13, was designed for estimating environmental damages at the margin. EDFA was born from the externality valuation literature and applied to fuel cycle analysis in a joint study by the US Department of Energy and the Commission of the European Communities (DOE 1995, ExternE 1997). LCA has traditionally skipped steps 3 through 5, moving from the inventory of pollutants to a single index of damages (Goedkoop 1995). However, more recently, aspects of the EDFA methodology has been applied in LCA modeling, making explicit the impact categories, such as human health, or crop production, that are considered in the analysis (Krewitt 1998, Goedkoop 1999, Hayashi et al. 2000, Itsubo 2000).

EDFA was primarily developed to capture the spatial and temporal marginal impacts of a proposed project. As such, EDFA requires detailed information about engineering, natural and physical sciences, and economics associated with constructing, operating and decommissioning the proposed project. The first two steps of the EDFA method are similar to the LCA inventory assessment, and include a quantification of emissions and other impacts associated with each life cycle state of the project.

In step 3, EDFA requires detailed modeling of emissions transport and deposition. These natural science models are then adjusted to site-specific characteristics, such that a footprint for each chemical emission is developed for the proposed project's local and regional characteristics.

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Step 4 estimates the physical response by human and ecological resources to the marginal change in emission concentration. Dose-response models are typically used to capture changes in the local and regional populations, such as increased health-related incidents and increased mortality from emissions exposure.

Step 5 applies willingness-to-pay models to estimate damages and benefits, either specifically developed for the regional characteristics, or borrowed from other studies and adapted to the regional characteristics.

The final step of the EDFA process estimates the portion of marginal damages and benefits that are external to cost of operations. For example, the federal Clean Air Act and some state

regulations require a tradable permit system in which power plants wishing to increase emissions of a particular pollutant are required to purchase that right from a plant wishing to reduce emissions. If such a transaction is regionally contained, then the net marginal increase in social costs is zero.

EDFA greatly increases the level of detail and data requirements beyond the Craighill and Powell approach. For marginal assessments used to develop an appropriate level of taxation, or other policy-related activities with significant financial costs, the increased scope of work can often be justified by the accuracy of the results. However, in practice, the increased scope of the EDFA approach, even with the best-funded studies, has led to ignoring many impact pathways that may be significant.

We reviewed a number of economic valuation studies of the external impacts from the hydro fuel cycle, including Pace University (PACE 1990), Department of Energy Externality of Fuel Cycles (DOE 1995), Bonneville Power Authority's Sultan River Case Study (BPA 1984), the Generic Hydro Study (Meyers et al. 1986), Extern E National Implementation (ExternE 1997), and Environmental Impacts of Alternative Energy Resources (Thayer et al. 1991). Of these studies, the best funded and most comprehensive in demonstrating and applying EDFA methodology are the DOE and Extern E studies. In their final assessment, the DOE included only the external benefits of jobs, the external costs of lost fish habitat, and reduced recreation access at their representative sites. The ExternE project rejects the damage function approach for hydro and resorts to willingness-to-pay estimates for avoiding the construction of a proposed dam. In all of these studies, upstream emissions were assumed to be inconsequential as compared to operations-phase emissions, and all of these studies concluded that hydro is an environmentally benign source of energy, primarily because it emits no greenhouse-gases.

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2.8 Damage Function and LCA

LCA is moving toward a more generalized application of EDFA with the development of databases that approximate impacts for regions within continents. Such databases significantly reduce the level of original data collection necessary for site-specific analysis, while simultaneously decreasing the accuracy of the marginal assessments. Rather than initiating steps 5 and 6 of the EDFA methodology, LCA with DFA estimates the human and ecological impacts for a set of standard emissions by country, or within grid cells overlaid on a country or region. This simplification of the EDFA methodology allows for first-cut approximations of marginal externalities, but does not capture all of the spatial and temporal impacts from a proposed project (Krewitt 2001). We have come to think of LCA with DFA as an intermediate step between the affordable Craighill and Powell approach and the data-intensive, site-specific EDFA approach.

All of the recent LCA application of DFA includes Steps 1-4 of the EDFA method (Krewitt 1998, Krewitt 2001, Goedkoop 1999, Hayashi et al. 2000). For example, the Eco-indicator 99 methodology includes detailed damage function analysis of category endpoints, such as cancer or decreased biodiversity, in DFA step 4 (Goedkoop 1999). However, the Eco-indicator 99 methodology is not designed to capture the spatial and temporal aspects necessary for marginal analysis. Rather, Eco-indicator 99 estimates impacts for Europe as a whole.

Krewitt (1998) developed LCA methodology to include DFA steps 5 and 6, leading to marginal economic externality estimates. His recent work develops an integrated model for Europe, South America and Asia that assesses the externalities associated with incremental changes in certain pollutants for each cell in a county-wide, 50x50 km grid (Krewitt 2001). Krewitt's work captures many of the spatial and temporal aspects associated with a handful of emissions consider in his

study. However, many of the site-specific impacts and benefits, such as changes in recreation patterns, cannot be assessed with the LCA-DFA methodology.

Krewitt's recent work suggests the future state of LCA with DFA, where more accurate average assessments, and more affordable and rapid, first-cut marginal assessments of externalities, can be made. Such databases have yet to be developed for the U.S., and the complex task of applying the EDFA approach to the hydro fuel cycle can restrict the scope of assessment to the detriment of the analysis. Where those impact pathways that are considered a priority receive comprehensive impact analysis, those impact pathways that are rejected can have untold significance.

2.9 Implications of DFA and Simple Economic Valuation on Hydro Study Methods

IO-LCA with simple economic valuation, as developed by Craighill and Powell, represents an affordable approach to assessing average, or baseline, conditions. Average assessments are useful in considering generalized characteristics of the hydro fuel cycle. In addition, the results are useful in designing and siting new plants such that gross external impacts from new facilities can be minimized in the design phase. Where average externality estimates and baseline conditions for fuel cycle analysis are the primary focus of the study, then the Craighill and Powell methodology appears to represent the most affordable and timely type of assessment.

We find that when economic valuation is used in the Craighill and Powell approach, a certain minimum review of the per-unit valuation data is necessary in order to summarize assumptions that would otherwise be deeply embedded in the impact assessment results. At a minimum, major controlling parameters that are controversial, and for which slight changes could significantly alter per-unit estimates, should be revealed, including discount rates, assumptions

about the value of human life, as well as certain characteristics about the populations and locations for which the per-unit values were estimated.

In a situation with some budget and time constraints, the best case scenario for estimating the external impacts of fuel cycles appears to be the LCA with DFA methodology. As this methodology and the associated data sources develop, LCA will be able to model spatial and temporal marginal externality estimates, as well as provide improved average externality estimates, for some emissions and impacts.

Where the results of a marginal assessment have significant social implications, such as a new tax, and the value non-emissions related damages and benefits are important to the estimates of externalities, then the increased scope of work associated with EDFA methodology may be necessary.

Table 16 summarizes a heuristic test for including economic valuation in LCA impact assessment. Average assessments are appropriate for regional and larger assessments when marginal estimates are impractical. Average assessments are also useful in identifying key parameters and impact pathways to be assessed in marginal studies, as well as design and operations characteristics to be included in future projects.

Table 16 Heuristic	test for level of det	ail needed in economic valua	tion step
Decision / Policy Level	Type of Assessment	Scope	Method
Local	Marginal	Proposed Project	EDFA
State	Marginal or Average	Proposed Project	LCA with DFA
Regional / Federal	Average	Numerous Representative Projects	LCA with Explicit Craighill & Powell

LCA with economic valuation is a useful methodology for capturing external impacts from a product or process. The methodology is currently being improved from the existing state through

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rigorous application of the DFA approach, explicative characterization of embedded assumptions, and focus on marginal assessments.

CHAPTER III

METHODS

3.1 Introduction

We augment the Craighill and Powell methodology described in Section 2.0 with more detailed assessment of the damage estimates, which we borrowed from the literature. Our primary concern is to establish average, baseline estimates of external damages from the hydro fuel cycle for the New England and Quebec regions. Rather than perform site-specific assessments for each site, we combined steps four through six of the EDFA approach (Figure 13), and borrowed externality estimates for three general geographical areas: rural, suburban and urban. Based on regional population characteristics, we label the La Grande projects in northern Quebec rural and the New England sites as suburban.

In this section, we briefly review the results from our inventory assessment in order to present the quantity of emissions per megawatt hour used in our impact assessment. Next, we present the valuation model used in this study. Then we review the damage estimates used in this study. Finally, we describe the parts of the damage estimates used in our assessment of externalities.

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3.2 Life Cycle Inventory

Table 17, reproduced from the first paper in this series, summarizes the emissions from the hydro fuel cycle assessed in our model. In the first paper, we summarized emissions data from three perspectives, including all 178 individual projects, 24 models grouped into graduated size categories, and groupings of small, medium and large projects. We assumed a 50-year project life and developed all underlying data for individual projects.

Table 17 Sur	mmary of inventory	results from Pa	rt I (unit/ MWh)		
Project Size	VOCs to air (ST)	NOx to air (ST)	CO to air (ST)	SO2 to air (ST)	PM10 to air (ST)
Small N.E.	6.21E-05	2.05E-04	3.32E-04	4.05E-04	5.94E-05
Medium N.E.	4.81E-05	1.59E-04	2.57E-04	3.13E-04	4.60E-05
Large N.E.	6.36E-05	2.10E-04	3.40E-04	4.15E-04	6.09E-05
Hydro Quebec	3.04E-05	9.30E-05	1.52E-04	1.84E-04	2.69E-05
Project Size	Fossil CO2 (MMT)	TRI Rel Air (Ibs)	TRI Rel Water (lbs	TRI Rel UnGnd (bs) TRI Rel Land (lbs)
Small N.E.	8.83E-02	4.16E-02	4.28E-03	1.63E-02	2.24E-02
Medium N.E.	6.83E-02	3.22E-02	3.31E-03	1.26E-02	1.73E-02
Large N.E.	9.04E-02	4.2613-02	4,38E-03	1.67E-02	2.29E-02
Hydro Quebec	4,04E-02	2.01E-02	2.04E-03	7.72E-03	1.06E-02
Project Size	TRI TI POTW (lbs)	TRI Tf OffSite (lbs)	Cost D&T (\$K)	CO2 Equiv. (ST)	Methyl Mercury (ST)
Small N.E.	9.38E-03	1.77E-01	1.35E-04	1.55E-01	4.70E-03
Medium N.E.	7.26E-03	1.37E-01	1.05E-04	2.66E-01	2.24E-02
Large N.E.	9.60E-03	1.82E-01	1.38E-04	6.67E-02	6.83E-03
Hydro Quebec	4.45E-03	8.44E-02	6.30E-05	1.82E+00	1.56E-01

In deference to our goal of developing average damage estimates for hydro emissions, many sitespecific emissions and impacts were excluded from the inventory assessment. The scope of our study included upstream emissions for all materials used in constructing hydro projects, as well as energy used for transporting materials to the construction site, and energy needed for building the dams. In addition, we included estimates of greenhouse gasses and methyl mercury released from the impoundment during project operations. We did not include impacts unique to each site, such as effects on anadromous fish, impacts on water quality, or changes in fluvial processes. Our assumptions, the data sources used in our model, the scope and boundary of the study, and the

uncertainty of the underlying data can be reviewed in the inventory assessment paper (Part I of this thesis).

3.3 Damage Calculation

Emissions from the inventory assessment were derived annually for each site. We estimated the annual costs for each emission category at each site by multiplying annual emissions with damage costs for the associated year. When dealing with stock pollutants, such as greenhouse-gases or methyl mercury, the damages in any particular year depend on both the current level of emissions and the size of the accumulated stock already in the environment. Our damage estimates are based on 10-year increments, such that they are adjusted to account for changes in ambient conditions as populations and economies grow.

Equation 3.1:

DamageEstimate(yeary, sitex) = Emission(yeary, sitex) * AnnualDamage(yeary, sitex)

Annual damages for individual projects in dollars per unit of energy were derived by summing the damage estimates for each emission, and dividing by average annual electricity generation for a 50-year life. Equations3.2 summarizes this relationship:

Equation 3.2: $AnnualDamages(yeary, sitex) = \frac{(GHG + CAP + CWP + TOX + DIS)}{(AnnualGeneration)}$

where GHG= greenhouse-gas costs; CAP= conventional air pollutant costs; CWP = conventional water pollutant costs; TOX = costs of toxic releases to air and water; DIS = disposal costs.

Total damage costs per unit of energy for each site are the sum of annual damages and adjusted to reflect cost per megawatt hour. All data is adjusted to the year 2000 basis with changes in the Consumer Price Index (CPI).

Equation 3.3:

 $TotalDamages(site_x) = \sum_{0}^{50} AnnualDamages(site_x)$

Although we allocated external costs to each year in the hydro life cycle, we do not discount the results. SETAC, the primary authority responsible for developing LCA standards, holds that valuation results should be reported without discounting (SETAC 1996). Further discounting can be conducted after non-discounted results are reported. Discounting is controversial in LCA modeling. We consider these issues in the third paper in this series (Part III of this thesis).

Externality cost results were calculated for each emissions category for individual projects. In order to present the results for all 178 dams assessed in this study, we averaged individual projects into 24 models. Table 18 summarizes the structural characteristics of each model leading to our distinction of small, medium and large projects. The models are graduated by the volume of materials used in the dam superstructures, and the model numbers in Column B correspond to the model numbers in all of the results figures. In our conclusions, we further averaged the New England projects into small, medium and large models as summarized in Column A.

3.4 Damage Estimates

Damage estimates used in this study were derived from a review of the literature for each emission category quantified in the inventory assessment. In general, damage estimates are calculated by estimating the value to society of a one-unit increase in the underlying stock of

pollutants. For example, economists ask what is society willing to pay to avoid an additional ton of greenhouse-gas emissions. In this section, we briefly review the damage estimate studies for conventional and toxic air pollutants, greenhouse-gases, conventional and toxic water pollutants, and external costs of solid waste disposal and incineration.

a) Group size	b) Model Number	c) Average Dam Volume (y ³)	d) Average Annual Electricity Generation (MWh/year)	e) Average Reservoir Volume (f ^s)	f) Average Reservoir Surface Area (acres)	g) Number of ns in Each del
	1	12,500	2,003	4.E+07	324	27
	2	29,186	2,355	4.E+07	198	29
	3	51,178	4,705	4.E+08	571	23
	4	67,551	8,974	2.E+07	61	15
I	5	92,062	12,315	4.E+07	84	6
Small	6	109,818	13,606	3.E+07	99	7
	7	124,980	19,574	4.E+07	183	5
	8	150,940	19,320	6.E+07	157	5
	9	173,213	11,878	4.E+07	96	3
	10	190,796	27,445	3.E+07	93	4
	11	239,445	54,558	4.E+08	710	12
	12	350,824	86,435	2.E+08	603	11
	13	444,124	34,605	4.E+09	4,545	4
E.	14	536,410	64,700	3.E+08	1,022	2
Medium	15	668,321	104,984	1.E+09	1,747	5
	16	769,542	30,644	3.E+08	399	2
	17	871,704	16,850	5.E+09	4,183	2
	18	905,072	228,042	3.E+10	29,270	1
	19	1,335,549	51,517	2.E+09	2,518	5
	20	2,162,999	148,850	2.E409	3,100	1
Large	21	3,554,953	105,200	1.E+07	300	1
	22	6,800,742	277,800	5.E+09	2,292	2
	23	8,018,947	356,064	9.E+09	3,240	1
Hydro Duebec	24	87,000,000	6,800,000	3.B+12	3,376,045	4

Table 18 Structural characteristics of hydro projects assessed in this study

3.4.1 Conventional air pollutants.

The Clean Air Act designates six emissions as conventional air pollutants. These include Ozone (O3), particulate matter (PM), nitrogen oxide (NOx), sulfur dioxide (SO2), carbon monoxide

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(CO), lead (Pb), and volatile organic compounds (VOCs). We reviewed six peer-reviewed studies to construct damage estimates for conventional air pollutants. These studies include the DOE Fuel Cycles Study (DOE 1995), EPA Clean Air Act Study (EPA 1998a), the PACE Externality Costing Study (PACE 1990), New England Externality Costing Study, [NE 89], California Externality Study, (CA 1993), and the Minnesota Externality Costing Study, (MN 1994). We reviewed the New England and California externality studies through a recent EPA literature review of economic valuation studies (EPA 1998b).

All of these studies estimate the marginal benefits of per-unit reductions in the emission categories. In order to do so, the studies estimate the direct external costs to human health, including mortality and morbidity. Some of these studies include indirect damages to humans through impacts to the environment, including changes to ecosystem and cropland productivity, and damages to recreation. Some studies include indirect damages to capital equipment, such as buildings, caused by pollution.

In each of the studies reviewed, the underlying data and assumptions are borrowed from other studies on morbidity and mortality. None of these studies conducted independent assessments of local populations' willingness to pay to avoid the external damages. The underlying assumptions in each of these studies greatly affect the estimates of damages for the conventional air emission categories. For example, the EPA Clean Air Act Study estimates the value of human mortality at 1,000,000 for particulate, lead, and SO₂ emissions. The Pace University study estimates the value of a human life at \$4,000,000. In his seminal work, Hohmeyer (1988) estimates the value of life in Germany to be \$500,000. The DOE used \$3.5 million as the value for a statistical life and conducted sensitivity analysis for a range of \$1.6 million to \$8.5 million. Taken on their

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own, variation in estimates of mortality can change estimates of net damages by an order of two or more, especially for marginal estimates in densely populated areas.

Morbidity damages in these studies have an even broader range of cost estimates and quantified categories. For example, the DOE estimates the affects of SO_2 on children's coughs and adult chest discomfort, building and material impacts, on visibility, and on the net benefits from increased cropland fertilization. The DOE concluded that net SO_2 damages are zero. In contrast, the EPA estimated the value of productivity losses from health damages, cleaning, and premature mortality for SO_2 , but did not estimate any benefits of SO_2 emissions.

		VOC	РМ	NOx	SO2	CO	Lead
EPA	Low	\$619			\$6,144		
	Medium	\$1,708	\$13,683		\$9,876		
	High	\$2,797			\$13,608		
PACE			\$3,389	\$2,335	\$5,781		
NE		1. 14 17		\$4,431	\$2,594		
Minnesota	Low		\$648	\$21	\$11	\$0.24	\$463
	Medium		\$816	\$69	\$20	\$0.36	\$489
	High		\$985	\$117	\$29	\$0.48	\$516
CA	South Coast	\$8,946	\$61,637	\$18,746	\$9,611	\$4	
	South East	\$204	\$880	\$568	\$1,942	\$0	
	North Coast	\$605	\$713	\$1,024	\$1,942	\$0	

Table 19 summarized the damage estimates in the reviewed studies. The DOE study and some of the results from the California study are not included in this table because their results are expressed as marginal damages for specific sites in dollars per kilowatt. Despite the various assumptions, methods of assessment and scope, the results provide adequate data for identifying low, medium and high estimates for emission categories.

The EPA recently developed a summary table for conventional air pollutants, with low, midpoint and high damage estimates, based on seven studies, six of which are included in our review (EPA 1998b). Table 20 summarized these results and we use this table for our estimates of external damages in this study. The methodology used to distill the independent studies into Table 20 is not fully developed in the EPA's report. However, the results suggest an assumption of normal distribution and Monte Carlo simulation to define low and high boundaries. The report points out that midpoint estimates for PM, SO2 and NOx are generally equivalent to those estimated in the Pace University study. Midpoint estimates for VOCs are from EPA (1998a) and midpoint estimates for CO are based on the California and Minnesota studies. Estimates for lead are based solely on the CAA study. The EPA suggests considering the low estimates for situations where pollutants impact predominately rural areas and the high estimates where pollutants impact predominately high density, urban areas.

Table 20Conventional air er/MT) (EPA 98)	mission dam	age estimates	s (1992 \$
	Low	Midpoint	High
VOC	\$87	\$1,485	\$7,862
РМК	\$699	\$2,970	\$11,794
NOx	\$175	\$2,009	\$5,242
SO2	\$1,747	\$5,067	\$5,242
CO	\$0	\$2	\$3
Lead	\$174,720	\$742,560	\$1,397,760

In this study we used the midpoint estimates for all New England hydroelectric projects on the assumption that hydro projects are located at a mix of rural and urban sites, and the pollutants would have an average damage effect across the region. For the Hydro Quebec La Grande project, we used the low damage estimates because the site is located in northern Quebec and has a rural character with low populations.

3.4.2 Greenhouse gases.

The suspected impacts of greenhouse gases on global warming have been well established in the literature (IPCC 1990, IPCC 1995, EPA 1995). Secondary impacts of warming include reduced agricultural production, decreased biological diversity, increased sea levels, and increased destructive weather events and human health impacts. However, quantifying damages from global warming is particularly complex. In their review of the literature, the DOE (1995) identified three problems areas that lead to inconsistent and controversial estimates damage costs. First, there are scientific uncertainties about the behavior of greenhouse gases in the atmosphere, including the size and behavior of carbon sinks, reactive chemistry of methane, regional climatic effects, and the effects of stratospheric ozone on warming. Second, the impact pathways of greenhouse-gases on warming tend to be nonlinear. For example, heat trapped in the atmosphere by a unit of gas is a nonlinear function of the stock of that gas, and other gases, which trap the same wavelength. Other nonlinear elements of warming include the physical consequences, such as changes in crop growth, and social consequences, such as rising sea levels. Third, the relationship between emissions and damages are time-dependent, leading to an intergenerational relationship between those who pay for greenhouse-gas reductions and those who benefit. In addition, there appears to be a complex relationship between accumulating stocks and decay rates, such that decay may be a function of the underlying stock levels.

We reviewed three studies to estimate the external costs of greenhouse-gas emissions (Cline 1992, Nordhaus 1994, Frankhauser 1994) The primary methodology used in the three studies include assuming that a specified increase in CO2 concentrations will lead to corresponding temperature increases. The studies model a nonlinear, socially optimal greenhouse-gas emissions curve and estimate the external costs of additional greenhouse-gas emissions. Cline assumes that a doubling of CO2 will lead to 2.5° C increase in global temperatures, and that without significant

policy action, temperatures will rise 10[°] C in 300 years. Other methods used for extrapolating warming into the future include sensitivity assessments based on functional forms such as linear, quadratic, and logarithmic curves (Reilly and Richards 1993). All three studies estimate effects of greenhouse-gas damages on agriculture, electricity demand, and real estate. Cline and Frankhauser also include some non-market damages, such as changes in biodiversity and other effects of warming.

Table 21 summarized the results of these studies. Estimates of damages range from 5.3/Mg (Nordhaus 1994) to 124/Mg (Cline 1992). Variability of the results depend on underlying assumptions about population growth and income, as well as the application of discount rates. The upper values of Cline's results reflect the "no policy" action with a corresponding 10^{0} C increase in global warming.

Table 21 Damage esti	mates for gr	eenhouse-gas	emissions (19	990\$/ MT)	
	9		2001-2010	2011-2020	2021-2030
Nordhaus (1994)	CO2	\$5.3	\$6.8	\$8.6	\$10.0
Cline (1992)	CO2	\$5.8-\$124	\$7.6-\$154	\$9.8-\$186	\$11.8 -\$221
Frankhauser (1994)	CO2	\$20.3	\$22.8	\$25.3	\$27.8
	CH4	\$108	\$129	\$152	\$176
	N20	\$2,895	\$3,379	\$3,901	\$4,489

In a recent report on cost-benefit analysis, the EPA (1998b) uses Frankhauser's estimates of GHG externalities (Frankhauser, 1994), and compares these results and methodologies to other studies (Nordhaus 1991 & 1994, Ayers and Walter 1991, Cline 1992, Madison 1994). Frankhauser's results include more explicit estimates of uncertainty and specify probability distributions for key parameters. The outcome is that Frankhauser's results are somewhat higher than other similar studies, but considerably lower than the highest estimates.

In this study, we use Frankhauser's damage estimates in Table 21 for greenhouse-gas emissions because of the comprehensive nature of their study and general convergence in externality studies to used the Frankhauser estimates. We quantify upstream and operations-phase greenhouse-gas emissions, but because of their size and uncertainty, we do not include our upstream greenhouse-gas emissions in our average estimates.

3.4.3 Disposal and incineration.

Table 22 summarizes external cost estimates for disposal and incineration of solid waste from a Center for Social and Economic Research on the Global Environment study conducted in Great Britain (CSREGE 1993) as cited in EPA 1998. The CSREGE study estimated landfill emissions of CO2 and CH4, as well as traffic accidents and air pollution from the transportation of waste to the facility. The transportation externalities were assessed at an urban and rural landfills, with an average travel distance of 12 and 50 miles respectively. In this study, we assume that disposal activities are primarily at on-site landfill. The Army Corps of Engineers provides little information about how waste materials are typically handled during dam construction. We assume that most waste from the hydro fuel cycle is generated during dam construction and that these materials are disposed in project-owned landfills.

3.4.4 Toxic air and water emissions.

We use damage cost data for toxic air and water emissions as estimated by the EPA (1998b). We report our findings for toxic impacts separately from other emissions. In our final analysis, we reject our estimates of toxic impacts as too uncertain. The EPA based its damage estimates for hundreds of toxic chemicals on detailed analysis of three chemicals. The results have not been tested in other peer-reviewed studies and estimates of uncertainty have not been calculated. In addition, our results of the toxic externalities suggest that these emissions account for 90 percent

of total emissions considered in this study. All recent studies of the Hydro fuel cycle find a level of toxic emissions that is not measurable (DOE 1995, ExternE 1997). Because of this uncertainty, we present our impact results for toxic emissions, but we do not include toxic emissions in our final calculation of impacts per unit of energy.

Table 22 Dama	age estimates	for dispos	al and inci	neration	
(1992\$/MT)	4	,			
Landfill	n in an				
Urban	Rural	Onsite			
4	. 4	3			
Incinerator					
Urban	Regional	Onsite-u	rban	Onsite-rural	
6	6	6		4	

The EPA methodology for estimating external impacts from toxic chemicals is based on estimates of the carcinogenic effects of each chemical on human health and mortality. The EPA analysis does not include other damages associated with toxic chemical emissions, such as losses of biodiversity and other ecosystem damages. Nonetheless, the results have a very high degree of uncertainty.

To calculate damage costs for toxic chemicals, the EPA estimated the carcinogenic effects of three chemicals: chromium, arsenic and cadmium. The study calculated the total emissions of these chemicals from 684 oil- and coal-burning plants in the U.S. and estimated the number of associated cancer cases. The EPA assumed that each cancer case resulted in premature death, and valued each premature death at \$5 million. The study then calculated the cost of emissions for the three chemicals on a per-unit basis.

Using the per-unit estimates of the three chemicals, the EPA derived estimates of the per-unit cost of other carcinogenic chemicals. The study separated the remaining chemicals into two groups:

those for which the EPA had established estimates of the unit cancer risk from inhalation, and those for which reference concentrations (RfC) for non-carcinogenic effects have been established. Sixty-three chemicals have established carcinogenic risk factors for inhalation of the chemical. For these chemicals, the EPA derived an equivalent unit value from the ratio of the chemical's unit risk value to the unit risk value of arsenic, cadmium and chromium. Damage costs estimates were derived for the 64 chemicals by multiplying the ratio value by the unit dollar value for the three equivalent chemicals. The EPA derived final damage estimates by averaging the unit value for the three equivalent chemicals into an average unit value for each chemical.

For non-carcinogenic chemicals with RfC values, the EPA first calculated an arsenic, cadmium and chromium RfC equivalent that estimated the chemical in air that would lead to a lifetime cancer risk of one in 100,000. It calculated equivalent scores for arsenic, chromium and cadmium, applied these equivalents to non-carcinogenic chemicals, and averaged per-unit scores into damage costs. Appendix A summarizes the EPA damage results for each toxic chemical analyzed.

The uncertainty of these estimates is likely to represent order of magnitude calculations of the value of human health damages associated with emissions of each chemical. The EPA suggests that the error is smallest with the estimates for arsenic, chromium and cadmium, but points to a number of factors that increase the uncertainty of these estimates. First, the \$5 million used to approximate the value of human life is within a range of plus or minus \$3 million. Second, uncertainty is compounded by applying the estimates for arsenic, cadmium and chromium to other carcinogens by assuming that the per-unit cancer risk is proportionally the same for each chemical. In addition, the methodology does not account for the environmental path and exposure each chemical follows in the environment. Finally, uncertainty is increased even further

by the assumption that concentrations the non-carcinogenic chemicals, which are three times greater than the RfC, have risks that are equivalent to three out of 100,000 for the carcinogenic chemicals. The EPA states that this relationship is somewhat arbitrary.

3.4.5 Land use and change in hydrology.

Hydroelectric projects can have significant impacts on water resources through impounding water and releasing water through spillways. In addition, flooding at certain projects and development of transmission lines have significant land impacts through inundation of valuable lands used for agriculture, forestry and recreation. Reservoirs often create some mitigating factors, particularly with recreation. Numerous biological studies have identified these impacts to be large and the costs are typically site-specific. We identified no estimates that generically value the land uses and water impacts associated with hydroelectric facilities.

3.5 Externalities

Externalities represent the net damages and benefits that are external to private investment decisions about power plants. Regulatory factors lead utilities to internalize many of the damages caused by hydro projects. For example, licensing through the Federal Energy Regulatory Commission (FERC) requires equal consideration and mitigation for non-power attributes disturbed by a project. Non-power attributes include the effects of hydro development on anadromous fish, reduced gravel recruitment needed for resident fish spawning, shoreline erosion, and recreation access. In licensing, the applicant is required to mitigate for these impacts at the firm's expense.

Technology can also act to internalize external costs. For example, in this study, we assume that the methods for new hydro project construction are similar to those practiced in the recent past.

However, improvements in transportation efficiency, reductions in the strength to weight ratio of concrete and cement products, or the employment of non-toxic paints and waterproofing materials could significantly reduce the emissions from a new project.

In this study, we assume that all emissions quantified in our inventory assessment are external to the price of power. Regulatory efforts by the FERC and the Army Corps of Engineers do not require any extra measures to mitigate for emissions from new construction (BOR 1980). In fact, because operations-phase emissions are commonly assumed zero, the FERC is currently pursuing means to consider the greenhouse-gas emissions avoided by hydro. Additionally, we do not assess external recreation- or employment-related benefits that would have the effect of reducing net externalities.

CHAPTER IV

RESULTS

4.1 Introduction

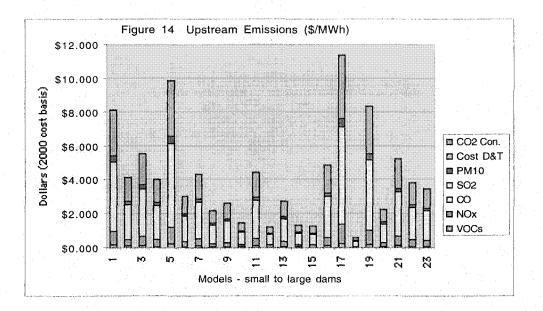
It is possible to develop a simple impact assessment from the inventory results by comparing total emissions for each type of pollutant in LCA modeling. This is known as characterization of inventory results. In Table 17, the highlighted box in each emissions column represents the hydro project size with the largest emissions per unit of energy. Emissions from large New England hydroelectric projects exceed all other models, including Hydro Quebec, for all emissions categories except CO2 and methyl mercury from the impoundment. Hydro Quebec projects have the highest per unit of energy emissions for these two emissions categories.

Characterization of inventory results may lead to the conclusion that large New England hydroelectric projects exceed other examples in New England and Hydro Quebec. If toxic emissions are the analyst's primary concern, then certain factors associated with New England projects, such as large dam structures, could be the target for mitigation. If global warming is the pathway of primary concern, then the large projects associated with Hydro Quebec may become a target for greenhouse-gas mitigation.

For individual emission pathways, characterization of the inventory provides some basis for decision making. However, characterization provides no basis for comparing unrelated impacts, or common impacts that occur at different phases of production for unique products or processes. For example, while we can compare the quantity of VOC emissions between small, medium and large hydro facilities, we cannot compare VOCs to CO2, or assess the impact these emissions have on society. Some methods for weighting the impact categories is necessary before decisions can be made based on the total external impacts of hydroelectricity. Economic valuation provides such a system.

4.2 Economic Valuation Results

We calculated the external economic costs for each of the emission categories in dollars per megawatt hour with the formula described in section 3.0. Figure 14 summarizes the costs of upstream emissions. For the models assessed, the upstream burden ranges from \$1 to \$13 per megawatt hour. SO2 emissions represent the majority of the upstream external costs.



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Figure 14 shows an obvious disconnect between project size and normalized upstream and construction-phase emissions. As Table 17 indicates, the volume of materials used in each model increases from approximately 12,500 cubic yards for the smallest New England dams to more than 85 million cubic yards. Some of the small New England models, such as Model 1 and Model 5, have some of the highest emissions per unit of energy. Hydro Quebec, model 24, has by far the largest dam superstructure, and nearly the lowest upstream external costs of all the projects assessed.

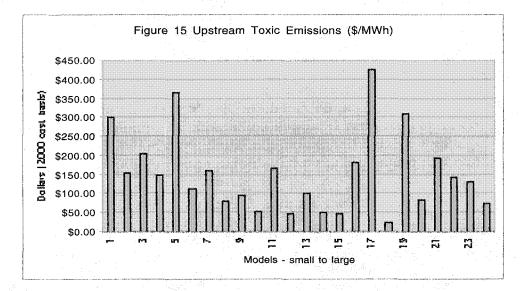
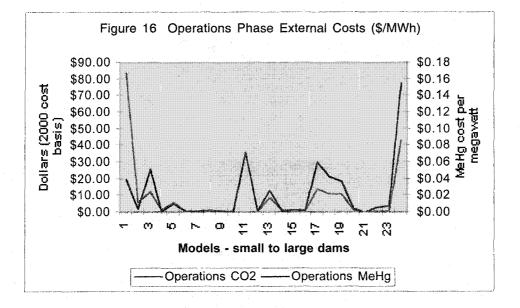


Figure 15 summarized our externality estimates for upstream toxic emissions.

Figure 16 summarizes operations-phase external costs. Operations-phase emissions represent a significant portion of life cycle impacts for some models, and an insignificant portion for other models. For all projects, the cost of methyl mercury mineralization is small, between zero and \$.16 per megawatt hour. Greenhouse-gas emissions range from zero to \$85 per megawatt hour. Mineralization, driven in part by the volume of impounded water, tends to cycle with greenhouse-

gas emissions that are related to the surface area of the impoundment and the ratio of deep to shallow waters.



As with upstream emissions, the size of the project, in terms of the volume of materials used in construction and average annual generation, has no bearing on the expected operations-phase emissions per unit of energy. By any metric, Model #1 represents the smallest hydroelectric project in New England and has the highest per unit of energy emissions of any grouping assessed in this study. Appendix B presents detailed externality costs data for the individual projects. Hydro project FERC # 5274 is one of the smallest projects assessed in the study, but represents the largest operations-phase CO2 emissions per unit of energy of the dams. Though the dam and average annual generation values are small, the impoundment, the primary source of CO2, is proportionally large and shallow.

Figure 17 summarizes total emissions from the hydro fuel cycle. Many of the models, as well as the underlying data, have very low external impacts per unit of energy. However, models 1 and

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11 have anomalous data that significantly increases average impacts for those models, as well as the entire data set.

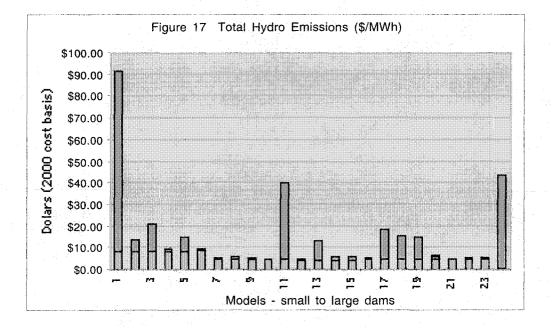


Table 23 summarized descriptive statistics for the entire New England and Hydro Quebec data set. Total emissions average \$23 per megawatt hour and range from \$.16 per megawatt hour to more than \$2000 per megawatt hour for the individual projects. For the New England dams, the median cost per megawatt hour of \$2.66 suggests a significantly skewed data set. The two outliers in models 1 and 11 increase the apparent and average operations-phase emissions per unit of energy for New England averages. For example, one project in model 1 has total external costs more than \$2000 per megawatt hour. With these three anomalies removed, the median external cost estimate is \$2.36, and the mean cost per megawatt hour is \$7.29.

Figure 18 further aggregates total external costs for the hydro fuel cycle to reflect regional averages for small, medium and large New England projects. For these models, upstream impacts range from half to three-quarters of the total external costs. Because of the anomaly in

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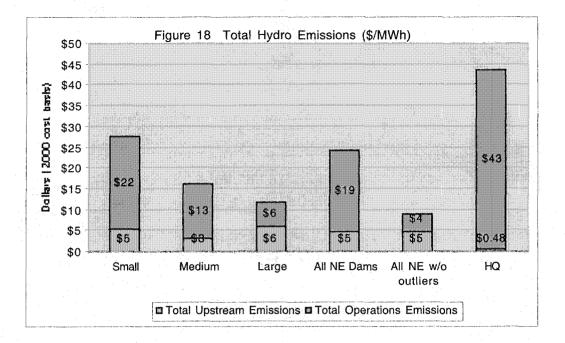
model 1, small projects appear to have the largest total external costs of approximately \$27 per megawatt hour. Average costs for all New England dams are approximately \$24 per megawatt hour. When we remove the three outliers from the analysis, average costs for all dams are approximately \$9 per megawatt hour.

	a se	· · · ·		s s astrona			1.45 - 144 1	e e la	an an stàite an s-
									<i>i</i>
		Upstream	Upstream (no outliers)	Operations CO2	Operations MeHg	Total Operations Emissions	Operations (no outliers)	Total Emissions	Total Emissions (no outliers)
All New	Average	\$3.21	\$3.08	\$19.45	\$0.02	\$19.40	\$4.21	\$22.61	\$7.29
England Projects	Median	\$1.50	\$1.45	\$0.82	\$0.00	\$0.81	\$0.80	\$2.66	\$2.63
	Lowest Value	\$0.11	\$0.11	\$0.01	\$0.00	\$0.01	\$0.01	\$0.16	\$0.16
	Highest Value	\$71.64	\$71.64	\$2,010.35	\$1.07	\$2,002.26	\$168.65	\$2,008.05	\$173.53
Hydro Quebec		\$0.48		\$42.99	\$0.16	\$43		\$43.63	

 Table 23 Total upstream and operations external costs for the hydro fuel cycle

 (\$/MWh)

In contrast, the burdens from Hydro Quebec are concentrated in the operations-phase as CO2 releases to the atmosphere from the reservoirs. We estimate external costs to be \$44 per megawatt hour. On a per unit of energy basis, the Hydro Quebec La Grande complex has the largest average life cycle burden of the projects assessed in this study.



4.4 Comparison of Our Results with Other Assessments

Externality studies of the hydro cycle, summarized in Table 24, indicate that our results are high, but within the range of other findings. When comparing these results, it is important to keep in mind that we used a different methodology to assess externalities and assessed different emissions at 174 dams. The three studies listed in Table 24 considered a small handful of projects, different stages of the hydro life cycle and different emissions. For example, no peer-reviewed study included comprehensive evaluations of upstream emissions, or operations-phase greenhouse-gas or methyl mercury emissions. In addition, the PACE study and the BEA study were average assessments, whereas the DOE study was for a marginal increase new hydro. The DOE estimated their results at a Southwest retrofit of an existing dam, and a Northwest, best technology diversion project. Our higher estimates are partly explained by the extended scope of our analysis.

Our results are also comparable to peer-reviewed externality estimates for the coal fuel cycle. Table 25 summarizes the results of some peer-reviewed coal externality studies. Study estimates

range from \$1.3 to \$64 per megawatt hour and they were discounted at a rate between 3 and 5 percent. Most of these studies concentrate their assessment on operations-phase emissions, suggesting that comprehensive upstream analysis, using IO-LCA would increase estimates. The low estimate (DOE 1995) was developed for marginal increases in 1995 for the best-available clean-coal technology.

Table 24 Study	results in t	he context (of other exter	nality stud	lies of the hy	dro fuel cycle (\$/MWh)	
Ellis, 2000			[PACE 90]	e de la composition Status	[DOE 95]	[BEA 89]	
New England	Hydro Qi	iebec	\$0		\$.1	\$10 - \$12	
\$7 - \$23*							
*non-discounted	results						

Our non-discounted, average estimates for all New England projects are in the lower range, and our estimates for the Hydro Quebec projects are within the upper range of the coal fuel cycle.

Table 25 Externa	ality study resu	its for the coal fu	iel cycle (\$/MW	h)	
[PACE 90] []	DOE 95]	[EC 95]	Bailly, 1995	Private Studies (from k	Crupnik, 1996)
\$25 - \$58 \$	1.3	\$19	\$2.9	\$54-\$64	

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CHAPTER V

DISCUSSION

5.1 Introduction

Hydroelectricity is widely assumed to be an environmentally benign, renewable energy source, especially when compared to other fuel cycles. Unlike fossil fuel cycles, hydro is commonly thought to emit no greenhouse-gases or heavy metals from the operations-phase (DOE 1995, PACE 1990). Proponents of the hydro fuel cycle argue that life cycle emissions per unit of energy are non-existent, or minimal and site-specific (Gagnon and Chamberland 1993, Duchemin et al. 1995, American Rivers 1998, DOE 1995, PACE 1990). Impacts to local hydrology and land-use changes from flooding reservoirs are thought to be small and have few long-term effects (HQ 1990).

Our results suggest that hydro is not as environmentally benign as it is commonly held. We find that external costs per unit of energy for the majority of individual hydro facilities assessed are small as compared to other fuel cycles. However, a small handful of individual hydro facilities greatly exceed average external costs for other fuel cycles, including the coal fuel cycle. The average external costs for New England hydro projects are lower, but comparable with, average external costs from fossil fuel cycles. The projects with the best siting have very low external impacts, considerably lower than the average estimates from the coal fuel cycle. In contrast, Hydro Quebec projects potentially have higher external costs per unit of energy than average emissions from the coal fuel cycle.

In addition to our findings, which are generalized for all hydro projects within our case study region, numerous biological studies suggest that site-specific impacts external to the price per unit of energy can be significant. Impacts to anadromous fish can have significant local and regional effects on recreation and commercial fishing, as well as initiate long-term changes in biodiversity (PACE 1990, Chambers 1992, Hazel 1991). Changes in hydrology tend to mobilize sediments during the construction phase, and restrict sediment and nutrient transport once dams are in place (Rosenberg et al. 1997, DOE 1995). Land-use changes, such as flooding and clearing transmission lines, can affect aesthetic, cultural and biological resources (Maxwell et al. 1997). These impacts tend to be site-specific and difficult to generalize from one plant to another. In many cases, these impacts would be mitigated through regulation, and the associated externality would be internalized in the price of electricity.

5.2 Implications for Public Policy

Because we have conducted an average assessment of the hydro fuel cycle, the direct implications of our study on public policy are limited. Our results do not include the total array of site-specific damages and benefits needed in state-level electricity capacity planning. Rather, detailed marginal assessments are needed for states to minimize incremental changes in social costs resulting from changes in consumer demand for electricity. However, our results do provide some insight into characteristics of the fuel cycle that have not been included in previous quantitative assessments of hydro, and they are, therefore, important in state-level planning and siting of new hydro facilities, as well as identifying impact pathways to include in marginal assessments.

Our results may be more directly applicable to regional and federal-level policy and planning where average assessments are useful for considering incentive-based environmental regulation. Efforts are underway in New England to adopt uniform information disclosure labels for the

deregulated electricity markets. The New England public utility commissioners have received a report from the managers of the National Council that recommends a number of policies and actions for commissions to take in streamlining information disclosure (Austin et al. 1997). At the heart of these recommendations are information standards for emissions release labels that would be published on each electricity bill, and would be made available in marketing materials. Nuclear, coal, oil, gas and renewables are the recommended categories for the fuel mix portion of the label, and average estimates of emissions would be included on the label. Pollutants likely to be included are sulfur dioxides, nitrogen oxides, mercury, particulate, and carbon dioxide releases from the operations-phase. Because the commission assumes that hydro does not emit any of the above listed pollutants, hydro would be lumped in with renewable fuel sources and would not be counted on the emissions portion of the label. The label would present no environmental impacts from any other part of the hydro fuel cycle. Our average assessment of New England hydro provides adequate baseline information for refining the proposed label to include operations-phase emissions from the hydro fuel cycle.

Research indicates that demand for renewable electrical products is likely to increase in deregulated markets (Holt 1997, Austin et al. 1997). Because hydro would be lumped in with renewables, the label under consideration by the New England public utility commissioners would "push" environmentally conscientious electricity consumers toward hydro products and away from fuel cycles that produce the listed air emissions. In addition, considering all hydropower benign allows the largest, lowest-cost hydroelectric generators to dominate the low impact renewable energy market. In New England, this means Hydro-Quebec, with low cost and large quantities of hydropower, would wheel additional electricity into the New England markets. In New England, Hydro Quebec has the lowest market costs, but, as our results indicate, some of the highest external impacts. Significant market shifts toward "green" energy products based on

the information disclosure labels could have the unintended impact of increasing demand for products with some of the highest externality costs and largest social and environmental impacts.

Hydro Quebec is still considering the Great Whale project, which would divert the Great Whale River and three other rivers, into the La Grande watershed (Maxwell et al. 1997). If this project were to proceed, then storage in the La Grande complex would more than double with a one eighth to one quarter increase in power output (Amyot et al. 1976). Our results suggest that increases in capacity would release significant additional greenhouse-gases, an issue of global concern. The Great Whale is one of many Canadian hydro projects of similar scale. Hydro Quebec has currently tabled the project in order to develop more accurate electricity demand projections, including those associated with the New England region. It is possible that the regional labels that combine hydro with renewables could precipitating additional Canadian hydro projects with the unintended effect of increasing globally significant social costs.

From a Federal perspective, our average estimates could be useful to the Federal Electric Regulatory Commission (FERC), the agency with regulatory oversight of private hydroelectric projects in the US. FERC is required to balance the benefits of individual projects against external environmental and social costs. Where social and environmental costs are high, the FERC requires mitigation measures. In some cases, the environmental impacts of a project have been high enough for the FERC to require project decommissioning and removal (Reisner 1998). To date, the FERC does not assess indirect or direct emissions from the hydro fuel cycle. Our model would provide additional, average quantitative information about some of the external costs that are not currently considered in the FERC licensing process. Our methods for estimating average, baseline damages could be adapted to different regions of the country and could be improved through more site-specific estimates of local and regional damages.

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In addition, the FERC is considering methods to assess the greenhouse-gas emissions avoided by individual hydro projects (see Commission Rulings, including Herbert 2000). The FERC position is based on the assumption that hydro emits no operations-phase emissions. Our results refute this position, and our model could be used to study emissions from individual projects in the context of regional baseline averages, and in the context of emissions from other fuel cycles.

5.3 Limitations of Our Model and Economic Valuation

Significant testing of our results is necessary to validate our findings. Our results indicate that a fundamental shift in perspective with regard to the societal impacts of the hydro fuel cycle may be in order. However, there are a number of limitations to our model.

First, life cycle inventory results are known to have problems with data accuracy and quality. We used input-output life cycle assessment techniques that generalize emissions for products by industry sectors. Environmental matrices used to estimate emissions often require voluntary reporting (Lave 1996). It is possible that material inputs could have more or less emissions per unit of energy than we assessed. In addition, we calculated detailed material inputs for one project, and assumed that these materials are the same for all of the projects in our model. It is likely that dams were constructed with various techniques and materials at individual sites. Sensitivity analysis could be used to further study the effects of small changes in both the input data and the externality data.

Second, we based our estimates of greenhouse-gas emissions on recent and ongoing scientific research. Little work has been done to verify greenhouse-gas emissions outside of the boreal regions. Although based on the best available literature, it is possible that our estimates for New

England are significantly inflated, and our decomposition rates are exaggerated. For the Hydro Quebec projects, where these emissions appear to be very significant, assumptions about the emissions profile could inflate the external costs.

Third, economic valuation data used to convert quantified emissions to externality costs are order-of-magnitude estimates.

Fourth, many identified environmental impacts, as well as external benefits, were not quantified in this study. We determined that these impacts are typically site-specific and are often internalized in the price of power through regulatory oversight. Even if one could quantify these impacts at individual sites, few externality estimates are available with which to convert these impacts into damages.

We considered our results order-of-magnitude estimates of external costs for the projects assessed in this study.

CHAPTER VI

CONCLUSIONS

We had two main objectives in this paper. Our first objective was to identify assumptions and problems in the application of economic valuation to LCA inventory data that can lead to erroneous results. We identified a number of deeply embedded assumptions in economic valuation studies that may conflict with the LCA practitioner's results. We recommended explicit descriptions of the underlying economic valuation studies, and, where possible, we recommended adjusting valuation results to comply with LCA assumptions.

We also found that the Damage Function Approach, used in marginal economic valuation studies, could be combined with LCA impact assessment and would be appropriate for assessments of damages at the margin. We found that expanding the scope of LCA with economic valuation methodology as developed by Craighill and Powell (1996) to include dose-response functions and other attributes of the Damage Function Approach would improve the accuracy and transparency of results.

Our second objective was to develop baseline, average damages for the hydro fuel cycle in order to consider impact pathways excluded from previous studies. We presented a case study of hydroelectric facilities in New England and Quebec in order to compare the relative burdens of small, medium and large hydro projects. In the preceding paper, we used input-output life cycle

assessment to quantify the emissions associated with the construction and operations phases of the hydro life cycle. In this paper we used economic valuation to assigned weights to the emissions flows and compared the net external costs from the hydro fuel cycle.

Table 26 summarizes our results. We find that, for the projects assessed, the Hydro Quebec projects have the highest environmental burdens, and that large New England projects have the smallest environmental burdens. We found that CO2 emissions from the operations-phase, and SO2 from the upstream phase, represent the largest external impacts of the fuel cycle.

Table 26 Hy	dro extern	ality est	imates (S	5/MWh)	
	VOCs	NOx	co	CO2 Construction	SO2
Small	\$0,119	\$0.530	\$0,001	\$1.762	\$2.635
Medium	\$0.069	\$0.311	\$0.000	\$1.033	\$1,545
Large	\$0.136	\$0.607	\$0.001	\$2.019	\$3.018
All NE Dams	\$0,108	\$0.485	\$0.001	\$1.613	\$2.411
HQ	\$0.003	\$0.018	\$0.000	\$0.953	\$0.355

	PM10	Solid Waste Disposal	Operations CO2	Operations MeHg
Small	\$0.227	\$0,00016	\$22.50	\$0.02
Medium	\$0.133	\$0.00009	\$13.27	\$0.03
Large	\$0.260	\$0.00018	\$5.75	\$0.02
All NE Dams	\$0.208	\$0.00014	\$19.45	\$0.02
HQ	\$0.021	\$0.08444	\$42.99	\$0.1 6

We included new empirical estimates of greenhouse-gas and methyl mercury external costs resulting from impoundment flooding. Previous studies of the hydro fuel cycle cite the lack of greenhouse-gas emissions as a primary benefit of the fuel cycle (DOE 95; PACE 90; Gagnon, et al, 93). Our findings dispute these results and suggest that greenhouse-gas emissions are contributors to the cumulative external burdens from the hydro fuel cycle.

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Our study could be expanded in a number of ways. First, with little increased effort, the model could be expanded to include all regions of the U.S. and Canada, which would improve regional, average estimates of externalities. Second, more detailed, site-specific infrastructure data would enhance the accuracy of the model. Third, additional site-specific environmental impacts and external benefits could be included, such as long-term impacts on anadromous fish, degraded water quality, increased recreation activity or increased real-estate value. Last, improved estimates of error, such as sensitivity analysis or Monte Carlo modeling, would provide more accurate estimates of the error in our model.

PART III

TIME VALUE, DISCOUNTING AND LIFE CYCLE ASSESSMENT

CHAPTER I

INTRODUCTION

This paper is the third in a series of three describing a life cycle assessment (LCA) model with economic valuation of the hydro fuel cycle. Our main objective in this paper is to explore the role of time in LCA, and consider discounting as a methodology for more explicit handling of time-related assumptions and values for short-term projects (less than 40 years). To that end, we review economic theory on time-value, and identify assumptions about individual preferences and economic growth that lead to the changing value of resources over time. We point out that these assumptions are both theoretically consistent with maximizing social welfare, and empirically expressed in market behavior. We submit that LCA studies with economic valuation, which appear to reject or ignore discounting, actually apply a discount rate of zero, with a set of assumptions about future economic growth and personal preferences that are implicit in the analysis.

We also consider criticisms of discounting, particularly that the mechanics of discounting can lead to favoring projects that have significant future environmental impacts. This is especially true when the benefits of a project are realized early in the project life, and the costs are deferred to the future. These criticisms are primarily concerned with questions of equitable distribution of the benefits and costs of LCA projects so that society has as a whole benefits from public policy

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and regulatory action. We follow the lead of conventional economists and suggest that, for shortterm projects, discounting is concerned with the efficient allocation resources over time rather than equitable distribution of resources to members of society. We point out that discounting provides insight into efficient projects where the benefits outweigh the costs, but that society may choose the less-efficient project when other criteria, such as intergenerational fairness, are considered. For short-term projects, we suggest that questions of equity or fairness in distributing the costs and benefits of regulatory projects should be handled through distributional weights.

As an illustration, we present the discounted and non-discounted results from a LCA study with economic valuation of hydroelectricity, and compare these results to a simple LCA model of a generic U.S. coal-fired plant. We show that private investment decisions and public policy positions can fundamentally shift when different discount rates are used. In our example, high discount rates would suggest that coal-fired electricity has similar impacts to the hydro fuel cycle.

Discounting is methodologically and philosophically complex, and we do not presume to resolve the debate over what discount rate to use. However, we find that when economic valuation is applied in LCA to assess environmental and social impacts from short-term projects, then discounting is an appropriate tool for making explicit values and assumptions that would otherwise remain deeply embedded in the analysis. We suggest that simple sensitivity analysis at different rates would go a long way toward recognizing time-value issues in LCA. A more comprehensive analysis of time-value in LCA, such as explicitly following the steps in calculating a discount rate, would provide deeper insights into embedded values and assumptions about social preferences and economic growth, even if that rate is zero. Discounting, combined with distributional weights, would provide a more equitable and transparent handling of timevalue in LCA models.

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CHAPTER II

TIME-VALUE AND EQUITY FOR SHORT-TERM PROJECTS

There is no doubt that the issue of what rate to use for discounting non-market projects, particularly those with time horizons beyond 40 years, is unresolved in economics (see Portney & Weyant 1999). We explore this debate and the methods for calculating a discount rate in the following sections. However, both mainstream and environmental economists tend toward agreement on the question of when to discount costs and benefits. Economists recommend that, for any economic analysis with temporal aspects that do not exceed 40 years, costs and benefits should be discounted at some positive rate (Arrow 1999, Weitzman 1999, Mann 1999, Schelling 1999).

This position follows from the basic economic tenet that resources are subject to declining value over time. The common adage, "A dollar today is worth more than the same dollar one year from now," has real implications when considering external costs borne by society. Time-value, which is central to the question of discounting in welfare economics, indicates that private firms and government officials achieve economic efficiency when they maximized discounted net benefits and costs. Discounting is simply applying temporal weights that adjust benefits and costs to reflect time-value.

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Three factors go into creating economic time-value effects. First, opportunities for private and public investment allow for compounded returns (Farber & Hammersbaug 1993). By investment, we refer to the economist's definition of spending on productivity enhancing capital goods by firms and government, which will allow increased production of consumer goods and services in future periods.

Second, investment today requires cash out of hand, forgoing the opportunities for spending on purchases today, or taking advantage of higher-yield investments that may arise. Economists argue that, all things equal, people have time preferences, and the time-value is society's way of compensating for forgone consumption opportunities.

Third, economists generally assume that economic growth will occur, thus improving the standard of living of those in the future. It is likely that in the near future, economies of industrialized countries will continue to expand, making future generations wealthier than present generations. This has the effect of further decreasing the value of a dollar in the future.

These three factors, though theoretical, play out in the real world of private and public finance. Regardless of whether the dollar is spent on the cost or benefit side of the equation, and regardless of whether that dollar represents a cost or benefit that is external or internal to the financial markets, that same dollar is less valuable in the future. Discounting is simply a method for adjusting the real difference between present value and future value, and it provides information about the overall economic efficiency of an investment.

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CHAPTER III

CALCULATING THE DISCOUNT RATE

3.1 Introduction

When concerned with external costs borne by society, as we often are in LCA studies, economists recommend discounting at the social discount rate (SDR). Economists define the SDR as the rate at which society as a whole is willing to trade present consumption for future consumption (Sassone & Schaffer 1998). As previously indicated, economists generally agree that discounting is appropriate for short-term projects. However, determination of the appropriate rate for the SDR presents complex methodological problems that are, as of yet, unresolved. We consider these issues in the following section. For our purposes, the question is less about the appropriate rate and more about the assumptions necessary to calculate various rates. Discounting provides a methodological forum for clearly stating assumptions that are otherwise implicit in LCA results.

Brent (1996) defines discounting as temporal weighting of costs and benefits. Net benefits from an investment today are returned over time, and, because the values of these benefits are different at different points in time, they can be weighted with time-dependent parameters relative to the

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investment.⁷ Based on the assumption of time-value, the weights assigned to cost and benefit streams will decline the further they are from the present. This rate of fall in the weights can be thought of as the social discount rate.⁸

Economist advocate two methods for calculating the SDR for near term, present value calculations, the social opportunity cost rate (SOCR), and the social time preference rate (STPR). In general, the SOCR leads to higher discount rates and the STPR leads to lower discount rates.

3.2 Social Opportunity Cost Rate (SOCR)

The SOCR is based on the argument that if public investment could earn a high return, say 10 percent, then accepting projects that would return less would deprive society of more productive investment opportunities. The SOCR is essentially the market rate of return. The SOCR would be the appropriate discount rate if the markets are truly efficient, have no distortions, and future economic conditions are known, conditions that work in theory, but not in practice (Howarth & Norgaard 1993)⁹.

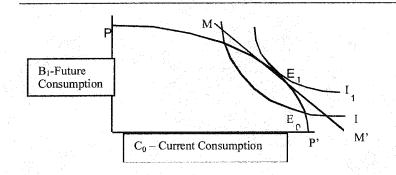
⁷ $B_t = -w_0C_0 + w_1B_1$ Where B_t = total benefits, C_0 = investment in year zero, B_1 = benefits year 1, and w = weights.

⁸ The social discount rate (I) is defined as the falling weights of costs and benefits over time. $i = \frac{w_0 - w_1}{w_1}$ or $\frac{w_1}{w_0} = \frac{1}{1+i}$

⁹Utilizing the market rate of interest as a proxy for the social discount rate is rejected in the literature (Brent 1996). In a perfectly competitive market with no constraints, it is possible that the STPR (slope of social indifference curve I), SOCR (slope of production possibility indifference curve P), and the market rate of return (slope of market indifference curve M)could be equal at point E_1 . However, in the presence of any additional constraints, such as taxes or non-competitive markets, the amount investors are willing to pay and savers are willing to receive are separated. This moves the social indifference curve from I_1 to I_0 . Note that the slope of E_0 is no longer tangential to market, or SOCR curves.

A second weakness with this line of reasoning is that it assumes a fixed budget constraint, where a decision-maker has a fixed amount of money to allocate to the investment with the largest present value. The issue of whether an investment is undervalued relative to consumption is more a shadow price issue than an issue of valuing of future resources against today's resources (Brent 1996). Shadow price is a synonym for social value, where the market price of a resource does not reflect the true value society places on that resource. As this relates to efficiency of an investment, analysts would quantify the shadow price of each cost and benefit in the analysis and recommend changes in behavior to bring market prices in accordance with shadow prices. For projects with time dimensions, this requires estimates of numerous discount rates. The Office of Budget and Management (OMB) suggests that the shadow price method is the analytically preferred approach to assessing the impact of public investment on private-sector resources (as cited in Carson 2000). However, because of the complexity of the shadow price analysis, the OMB recommends that public agencies use a single discount rate for assessing the social value of public investment.

Markandya and Pearce (1991) point to a third weakness with the SOCR methodology. If society consumes public funds rather than invests at the best market rates, then the SOCR becomes an irrelevant metric. There is no opportunity cost for consumption.



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3.3 Social Time Preference Rate (STPR)

Two methods are used to calculate the social time preference rate. The first method is known as the individual time preference methods, where one quantifies through surveys the value individuals place on the consumption rights of living and future generations. Some economists argue that a degree of consideration of future generations exists in the individual time preferences of current generations. Parents are concerned about the welfare of their children, although such concerns require forgoing consumption today for the benefit of future generations. However, others have argued that humans are myopic when it comes to allocating resources over time (Pigou 1920). We choose to consume non-renewable resources at a rate that could preclude a second and third generation's use of these resources. The myopia of the individual time preferences leads to heavy weights for consumption by current generations and light weights for consumption by future generations. When the SDR is calculated using individual time preferences, we reduce the importance of future generations' needs in the consumption decisions made by living generations, arguably not a socially optimal solution.

The myopia of the living generation has led some economist to argue for an authoritarian time preference method where estimates of socially optimum allocation of resources between generations is used to set the discount rate. This method is based on the assumption that society has an equal responsibility to future generations, a relationship that requires a higher responsibility to future generations than the individual time preference indicates (Brent 1996). Equal consideration, however, does not mean equal weight in the time preferences. Theory holds that future generations can expect to be better off than current generations because economic growth will increase their wealth, a reasonable assumption for near-term projects. In addition,

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there is a decreasing marginal value to increased consumption.¹⁰ In other words, a unit of benefits is more valuable to a person with fewer resources than to a person with more resources. Economists argue that multiplying the growth rate of income by the change in marginal utility leads to socially optimum discount rates.

Expressed as an equation, the social time preference rate looks as follows:

 $i = \eta g + z$

Where i = the social time preference rate, η is the percent change in social marginal utility of income, and g is the rate of growth of real future consumption.

Because the individual's time preferences are removed in the authoritarian analysis, other economists advocate the inclusion of the rate of pure time preference, z in the equation above. Brent (1996) suggests that people would want to discount the future simply because it is the future and does not include them. Squire and Van der Tak (1975) recommend "fairly low values (for z), say 0 to 5 percent, on the grounds that most governments recognize their obligation to future generations as well as to the present." Pure time preference has the benefit of allowing the discount rate to be positive when other factors would lead to a zero, or negative SDR.

$$i = \left[\frac{(w_0 - w_1)/w_1}{(Y_1 - Y_0)/Y_0}\right] \left[\frac{(Y_1 - Y_0)}{Y_0}\right]$$

¹⁰ Social discount rate (i) = elasticity of social marginal utility (the first parenthetical statement) times the multi-generation income growth rate (the second parenthetical statement) $(Y_1-Y_0)/Y_0$ is the percent change in income over generations. $(W_0-W_1)/W_1$ is the definition of the social discount rate used in footnote 3 to highlight the declining weights assigned to future generations.

The STPR should equal the SOCR before taxes and other market distortions are included in the assessment. Taxes drive a "wedge" between individual preferences and the opportunity costs for firms (Lind 1982). For example, in order to fulfill a 2 percent discount rate for personal consumption, firms must invest in projects offering a minimum of 2 percent plus the tax rate. If taxes reduce profits by 50 percent, then the firm will need to earn a 4 percent return in order to give shareholders their 2 percent after-tax return. While the SOCR is 4 percent, the STPR is two percent.

3.4 Subjectivity in Calculations of the STPR

Calculations of each variable in the social time preference equation require a certain degree of subjectivity. On the surface, calculating the growth rate of capital income (g) is straightforward. Coefficients for g are generated through time series regressions of per capita consumption. However, environmental economists suggest that the issue is more complicated. They argue that the GDP does not distinguish between production income and natural resource exploitation income, and the GDP does not make a distinction between reparation costs and expenditures that increase wealth. (Serafy & Lutz 1989, Norgaard 1989, Hueting 1991). This suggests that the GDP is generally overvalued, indicating that better accounting could create situations of low, or even negative growth. Further, England (2000) develops a growth model that includes natural capital, which suggests that a significant portion of perceived growth depends, among other things, on unsustainable appropriation of non-renewable resources. If these claims are true, then the 2 to 3 percent growth rates typically used in the U.S. and Canada could greatly inflate the social discount rate.

Calculating the elasticity of the social marginal utility of income (η) requires value judgements about the importance society places on income inequality between economic classes. Benefits

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from a project are often broken into low, medium and high income brackets in order to assess the impact additional benefits will have on each group (Hau, 1986). Economists assume that a unit of benefit leads to higher utility in low-income recipients as compared to high-income recipients. In addition, the allocation a unit of benefit to increase the utility of an income group leads to secondary positive effects on the welfare of society.¹¹ But, quantifying the increase in utility of both the income group and society requires setting distributional weights for both categories (Brent 1996). By "ignoring" the weights in the SDR calculation one is essentially setting the weights at one, and inserting the value judgement that marginal utility is equal among income groups.

Setting the pure time preference rate (z) is also fundamentally a subjective process. Brent states that "there are no theoretically accepted procedures for deriving (z), except for extreme cases . . outside of the extremes, one has little guidance (Brent 1996)." A choice of z=0 assumes that all individuals in society, both future and current are equal, and rejects the notion of allocating a premium to current generations. A choice of $z=\infty$ assumes that the worst-off individual in society is the only one that matters. Society should choose efficient welfare projects that increase the utility of one member at a cost to other members' utility. Some efforts to calculate z have analyzed change in mortality rate, and others simply recommend a value of z=1 or less (Brent 1996, Squire & Tak 1975).

In summary, where capital markets are truly efficient, future economic conditions are "known," and the allocation of wealth between members of society is equitable, then the SOCR is the

$$\eta_{i} = \left[\frac{\Delta Social Welfare}{\Delta UtilityGroup(i)}\right] \left[\frac{\Delta UtilityGroup(i)}{\Delta IncomeGroup(i)}\right] = a_{i}\lambda_{i}$$

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¹¹ The most common way to calculate the social marginal utility of income is to set the change in utility of individuals on social welfare $(a_{i}) = 1$.

appropriate rate for discounting. However, Howarth and Norgaard (1993) point out that these conditions are stringent, and are often considered "first-best," highly theoretical examples, rather than practical conditions from which to derive the SDR.

Lind (1990) and Hanley (1992) consider a "second best" scenario, where taxes and other factors distort the theoretical versus actual return on a capital investment. Under these conditions, with timeframes of 40 years or less, the STPR is the appropriate discount rate.

3.5 Equity

When considering short-term public investment, efficiency is only one part of the economic analysis. Equity, or who pays the costs and who receives the benefits, is an equally important factor in determining whether a policy option is socially viable (Pearce & Markendaya 1991, Norgaard 1997). For example, a policy option may be economically efficient, with the benefits significantly outweighing the costs, while the poorest sectors of society bear the costs and the richest sectors of society receive the benefits. Though this example may be economically efficient, it is unlikely that such a policy would be taken, as the net benefit of the project would reduce society's overall welfare.

Society's overall welfare would be reduced because, as economists argue, the utility of a dollar in the hands of a poorer person exceeds the utility of dollar in the hands of a richer person. A person with a \$1 million annual income is likely to be less concerned with a tax of \$100 in comparison to a person with an annual income of \$20,000. The welfare of society as a whole is improved if efficient policies are adjusted to fairly reflect the disproportionate utility of those affected by a policy.

In a practical sense, equity issues are dealt with in economics by assigning distributional weights to the costs and benefits, a method that is mathematically similar to discounting with a fundamentally different outcome. Distributional weights are used to value resources to different people in each time period, whereas discounting is used to value resources to the same people at different point in time (Brent 1996). The outcome of equitable allocation may lead to the adoption of an economically inefficient policy that distributes costs and benefits in such a way as to increase social welfare.

Conservationists' concerns about discounting are not unfounded. Economic studies of natural resource management often focus on efficiency, and the consequence of an efficient cost-benefit assessment, such as rapid depletion of non-renewable natural resource, appears to reduce society's, particularly future generations', overall welfare. As Markandya and Pearce (1991) point out, a primary criticism of discounting has to do with the outcome of the costs benefit equation; the management of non-renewable natural resources in a discounted analysis can lead toward rapid depletion of stocks and the inability to sustain basic living standards in the future. Without accommodating for factors in income distribution, the analysis of project efficiency can be destructive to the environment.

Nonetheless, economists argue that much of conservationists' concern about discounting appears to confuse economic efficiency with equitable resource distribution. Portney and Weyant (1999) point out that one could reject inequitable projects even when they pass efficiency tests with extreme net benefits. They argue that tinkering with the discount rate to mitigate for equity issues is not defensible, and remind us that efficiency is "hardly the only criterion that matters in policy analysis." For similar reasons, Markandya and Pearce (1991) argue that discounting "should not be tampered with." They propose a method for including sustainability criteria used as weights in

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the cost benefit analysis in order to more equitably allocate costs and benefits without overturning a fundamental neo-classical economic tenet: the time-value of money.

Questions of equity and efficiency become increasingly complex as time periods exceed the living generations. Howarth (1996, 1997 & 1998) and Norgaard (1991, 1993, 1998) make compelling arguments that questions of maximizing efficiency within one generation are fundamentally different from questions of resource allocation over many generations. They suggest that if the allocation of resources between present and future generations is equitable, and follows social welfare functions, then economic cost benefit analysis, using the SDR, improves the efficient allocation of resources between generations. However, they suggest that if equitable conditions are not met, such that the distribution of resources between generations does not maximize the welfare of both generations, then cost-benefit methods may not support efficient transfers of resources. In fact, discounting could serve to exaggerate equity disparities between present and future generations (Howarth & Norgaard 1993). With some similarities to Markandya and Pearce, they suggest methods for allocating stock resources to future generations.

3.6 Discounting in LCA & zero discount rate

To date, LCA studies have not applied discounting in the economic valuation step, despite the observation that impacts from emissions typically have a time dimension (Frankhauser 1994, Rudd et al. 1993). Craighill (1996) and Powell (1997) demonstrated the power of economic valuation in impact assessment of LCA modeling. However, they did not allocate their results to different points in time, and their studies do not include discounting. When discounting is not included in LCA impact assessment, then a unit of emissions in year one of a proposed project has the same impact as a unit in year 40.

The Society of Environmental Toxicology and Chemistry (SETAC) has developed best available practice recommendations for conducting LCA studies (SETAC 1999). These recommendations suggest that the impacts identified in LCA studies integrate over time, and that all impacts, irrespective of when they occur, should be equally weighted. This implies that all environmental impacts have infinite lives with no potential for future mitigation. For impacts that have known environmental effects with long time horizons, such as those greenhouse-gases associated with global warming, SETAC recommends assigning long time periods to the project that imitate infinite time, such as 500 years. SETAC assumes that most of the impacts will have taken place and that we can ignore differences between a long time horizon and infinite time. SETAC recognizes that this is an assumption that has yet to be verified.

We consider both the Powell and Craighill approach and the SETAC recommendations for infinite time to be an implicit assumption of a zero discount rate. On the surface, the idea of a zero discount rate is appealing, since a death today and a death tomorrow are considered on some level equal. However, as we are concerned in this paper with discounting within one or two generations, such an assessment makes little sense. From an individual perspective, we are not indifferent about whether we die today or well in the future. In any economic assessment, the effect of utilizing a zero discount rate is two-fold. First, the outcome of applying a zero discount rate can lead to implausible results that do not reflect current understanding of time value and social preferences. Second, and more importantly to our discussion, assumptions about social preferences and time are deeply embedded in the analysis.

Application of a zero discount rate can lead to internal conflicts in cost-benefit analysis (Farber & Hemmersbaugh 1993). If a discount rate is less than the risk-free rate of return from an investment, such as a bond, then this can lead to contradictory solutions. For example, if the

present value with a zero discount rate for an environmental clean up program cost \$2 million, but society is only willing to pay \$1 million, then a socially agreeable solution would be to invest \$.5 million in government bonds until it reaches the \$2 million value of project. The further the costs occur in the future, the lower the cost of the initial investment. This suggests that the regulatory costs to society are less than the present value of the environmental clean up program, despite the fact that benefits of the investment will outweigh the costs when they occur in the future.

From a private perspective, if a zero discount rate is assumed, then the present value of an investment option equals the value of the same investment in the future. Borrowing capital would be essentially free, and firms would likely borrow to support consumption today rather than in the future.

Calculations of a zero discount rate require a set of assumptions about economic growth and social preferences that are embedded in the LCA valuation step. Although mathematically infinite, in a practical sense, there are numerous combinations that could lead to a zero discount rate, all of which require a set of assumptions about time value and preferences. For $\eta=0$, we assume that 10 dollars of goods and services provides the same utility to the poorest member of society as it does to the richest. For g=0, we must assume that the economy will not grow over the period of time of the analysis. For z=0, we must assume that society allocates no time preferences for a dollar in hand today over a dollar next year. All of these assumptions are imbedded in any economic valuation step that utilizes a zero discount rate.

Economists debate the merits of various methods used to calculate the SDR, and, as previously demonstrated, the outcome of the various calculations leads to significantly different values.

Tresch (1981) wrote "In our view, it would be difficult to mount a decisive case for or against any rate of discount governments might choose over a range of 3 percent to 20 or even 25 percent." A review of discount rates used by U.S. government agencies in the late 1960s indicated that the actual range used in evaluating social welfare projects was between zero percent and 12 percent (Staats 1969). This range is significantly smaller than what Tresch suggested might be acceptable, but still large enough to see that establishing the social discount rate is far from an exact science. The Office of Management and Budget recently revised its recommendations for discounting regulatory cost and benefits from 10 percent to 7 percent (OMB 1992). The OMB estimates a 4-percent rate of time preference. In practical application, most economists advocate a social discount rate in the range of 1 to 3 percent (Lind 1990, Howes 1990, Farber et al. 1996). Those economists that include the tax wedge driven between the opportunity cost methods, and the STPR methods typically recommend discount rates from 3 to 6 percent (Arrow 1999).

Choosing the proper discount rate is a challenge. Calculating the discount rate requires significant knowledge of complex economic concepts, and leading economists are clearly divided on what method to follow. We do not presume to resolve the debate in this paper. However, we feel that ignoring time-value in LCA poses additional problems that should not be dismissed. Applying a zero discount rate requires a set of assumptions that do not generally reflect our empirical understanding of preferences and values. As it relates to practical decisions in LCA, we cannot wait for resolution on which method to choose in calculating discount rates, and we cannot necessarily continue to apply a zero rate with its deeply embedded assumptions.

If we accept that economic valuation is a useful method for considering alternative actions, then the actual discount rate is less important than the assumptions that underlie the development of a given rate. Discounting provides a forum for airing assumptions, and basic assumptions and

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impacts of different rates on time-dependant data can be explored in LCA results through simple sensitivity analysis.

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CHAPTER IV

SIMPLE DISCOUNTED MODEL OF THE HYDRO FUEL CYCLE

4.1 Introduction

In order to demonstrate the power of discounting and the impacts of applying a zero discount rate, we performed an Input-Output LCA study of the upstream emissions and the quantifiable operations emissions associated with the hydro fuel cycle. We report our inventory assessment results and our impact assessment, as well as other background information, in the first and second papers in this series (Reference). We used data from all concrete, hydroelectric dams in New England (174 total dams) and the Hydro Quebec La Grande complex (4 dams). We calculated externality costs for each emission category, including conventional air and water pollutants, and greenhouse-gas emissions. We also assessed the upstream toxic chemical emissions to water and air, but we did not include this data in our model. Despite the small per-unit emissions of toxic materials, the externality cost for toxic materials represented over 90 percent of the total externality costs for the hydro fuel cycle and we were uncomfortable with the transparency and accuracy of toxic externality calculations.

We allocated external costs per unit of energy to the hydro fuel cycle to each year for an assumed 40-year project life. We allocated all upstream costs to year zero and all operations costs to their appropriate year in the project life cycle. We calculated the net present value for each individual

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project at year zero, in year 2000 dollars. The model has change cells for inputting discount rates, allowing us to test the sensitivity of our results to changes in the SDR. Appendix L shows the data included in our model.

4.2 Simple Coal Input-output LCA

For demonstration purposes, we developed simple model of upstream and operations air emissions from a representative coal-fired facility (Appendix M). We used two sources of data for the coal LCA model: facility construction data per kilowatt (DOE 1995), and operationsphase conventional air pollutants and greenhouse-gas emissions per kilowatt . We borrowed coal emissions estimates per unit of energy for New Source Performance Standard (NSPS) plants as cited in PACE 1990. NSPS plants include scrubber control equipment, but do not use clean coal fuel. We used non-discounted, raw data to construct our model and allocate externality cost data to each year of operations. As with the hydro models, we assumed a 50-year project life. Unlike the hydro assessment discussed above, the coal model does not include comprehensive upstream emissions associated with construction of the facility, or upstream emissions from coal mining and transportation of fuel to the generation facility.

Because we developed our coal model for comparison purposes, we were only concerned that our damage estimates fit within the range defined in the literature. A review of the literature indicates that our estimates for coal externalities at \$20/MW are middle range between the low estimate of \$1.3/ MW and the high estimate of \$64/MW. Table 27 summarizes the results of the six studies we consulted in developing our simple LCA of the coal fuel cycle.

Table 27 Extern	nality study resu	lts for the coal f	uel cycle (\$/MW	h)	
[PACE 90]	[DOE 95]	[EC 95]	Bailly, 1995	Private Studies (from k	(rupnik, 1996)
\$25 - \$58	\$1,3	\$19	\$2.9	\$54-\$64	

It is important to note that the studies assessed different impact pathways, considered different site-specific damages, and utilized different methods, making direct comparisons difficult. All of the studies used a 5-percent discount rate and assumed life cycles from 25 to 50 years. The lowest damage estimates are from a comprehensive study conducted by the Department of Energy (DOE 1995) that assessed marginal damages associated with six fuel cycles. The study initially considered all life cycle stages and all pollutant pathways, but reduced the scope of analysis in the face of uncertainty. The highest estimates come from a Pace University study (PACE 1990) and private-sector studies conducted by the Regional Economic Research (RER 1991), and the Triangle Economic Research (TER 1995). Our discounted estimates are consistent with those of the European Commission study (EC1995) which estimated externalities associated with nine fuel cycles located in England and Germany.

In both the hydro and the coal externality models, a number of environmental and health-related impacts are excluded from the analysis. Numerous impacts from the hydro fuel cycle are site-specific and difficult to quantify. These include impacts on water quality, fish and terrestrial resources. We also excluded external benefits, such as increased recreation opportunities and jobs. For both fuel cycles we excluded direct health impacts from operations of the coal facility, including worker fatalities, traffic accidents, and radon poisoning. Neither the hydro nor the coal model includes assessments of the impacts associated with operations, maintenance or decommissioning.

We discounted all future costs to present value and expressed the results in real dollars for the year 2000. We used a 5-percent discount rate and conduct sensitivity assessment with 2 and 10 percent rates. We assumed a 40-year project life for both the hydro and the coal models.

We use externality data from studies of society's willingness to pay to avoid impacts. A review of the externality estimates used in our model is in the second paper in this series (Part II of this thesis). We derived externality estimates using a three-step damage function approach where impacts were estimated, values for the impacts were determined, and the values were summed for each impact pathway.

4.3 Model Results

Net external costs for small, medium and large New England hydro facilities, as well as Hydro Quebec's La Grande project, are summarized in Table 28. Column A shows the results of the externality assessment using a zero discount rate. The results indicate that, though the externalities associated with marginal increases in hydroelectricity are significant, they are not as significant as those associated with the coal fuel cycle. In addition, electricity from a marginal increase in Quebec appears to produce more than twice the emissions of a similar increase in New England.

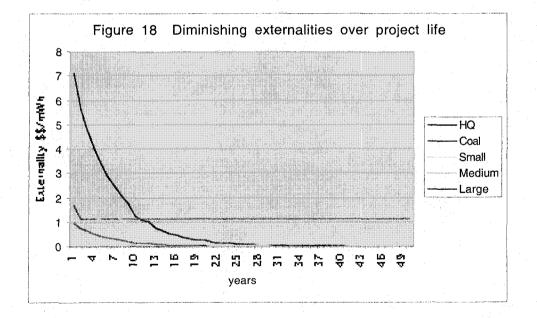
	a) Zero Discount Rate (\$/MWh)	b) 5% discount rate Average NPV/MWh	c) NPV % of zero discount	d) 2% discount rate Average NPV/MWh	e) 10%discount rate Average NPV/MWh
Small N.E. Dams	\$28.37	\$22.03	77.65%	\$25.41	\$18.08
Medium N.E. Dams	\$16.74	\$12.99	77.60%	\$14.99	\$10.66
Large N.E. Dams	\$12.56	\$10.68	85.02%	\$11.70	\$9.44
Hydro Quebec	\$43.78	\$31,63	72.25%	\$37.94	\$24.49
NSPS Coal Plant	\$58.95	\$19.46	33.01%	\$31.71	\$10.79

 Table 28 Discounted externality results for the hydro and coal fuel cycles

However, the results and associated policy conclusions become less clear when we discount the external cost stream. Column B shows the results of applying a 5- percent discount rate to the externality costs. The results are fundamentally different from the zero discount models. A

marginal increase in coal generation capacity appears to have less impact than that of small New England hydro facilities, or that of Hydro Quebec facilities. When we apply a 10-percent discount rate the differences between models is further magnified. Column E indicates that the coal fuel cycle has similar impacts to those of the most environmentally benign hydro models.

The illustrative results in Table 28 highlight the power of compound interest rates, particularly when an analysis has a long time dimension. In our example, one would be more likely to recommend a marginal increase in hydroelectricity for LCA models that utilize zero discount rates. The analysis is less clear when an SDR of between 2 and 5 percent is used. Because the relative external costs per unit of energy are similar for the various hydro and coal models, other factors would play a larger role in distinguishing between alternative projects. When a firm's opportunity cost rate of approximately 10 percent is applied, a marginal increase of coal-fired electricity appears to have the least external costs.



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These contradictory results and policy decisions that change with the discount rates used are due to structural configurations of underlying data. Figure 19 shows the diminishing external costs of the hydro fuel cycle in comparison to the constant emissions associated with coal plants. For the hydro fuel cycle, initial external costs are high due to the effects of upstream emissions and CO2 emissions from flooded reservoirs. In contrast, emissions from the coal fuel cycle are stable throughout the life of the project. When the coal plant is operating, the external costs are uniform. In situations where the majority of costs are borne early in the life cycle, discounting magnifies the relative impact of these burdens. For projects with relatively low initial costs consistent throughout the life of the project, discounting places less weight on the cost side of the equation. As the discount rate increases, projects that defer costs into the future appear attractive to the agency or the firm.

CHAPTER V

CONCLUSIONS

Economic valuation is a powerful methodology for quantifying external costs in the LCA impact assessment. However, LCA, which is often concerned with impacts that accrue over time, must develop methods for handling time-value. In this paper, we consider discounting as a method to more explicitly recognize assumptions about individual preferences and economic growth in the LCA impact assessment.

On the surface, choosing a discount rate appears to be an esoteric process. A brief review of discounting equations is enough to set this opinion. But the technical challenges of calculating a discount rate should not overshadow the purpose of discounting, which is to consider fundamental questions about the economy and philosophical questions about consumption preferences. Answers to these questions have real impacts on time-dependant LCA assessments.

We demonstrated that economic valuation studies that report aggregated results, but do not include discounting, are actually applying at zero discount rate. Discounting at a rate of zero requires a set of assumptions that do not necessarily match social scientists' understanding of time-value and consumption preferences. When we ignore time-value, assumptions about

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preferences and economic growth, which lead to the value of resources over time, are deeply embedded in the LCA analysis and results.

Consequently, we advocate a more transparent method for discounting. Our bias is consistent with conservationists' concerns that future generations receive inadequate attention in calculating the discount rate. In general, we follow economists' recommendation to discount at some positive social discount rate (between 1-3), although we recognize that economists are divided on what rate to use. At a minimum, LCA models should recognize time-value in their results by conducting sensitivity analysis for a number of different discount rates, and providing access to time-dependant data so that other users can adjust the assessment to comply with their values. A more comprehensive model would include justification for the chosen rates by explicitly expressing assumptions, and calculating a social discount rate. If conclusions do not shift with the changing rate, then analysts can make some claims about the efficiency of one project over another. If conclusions do shift, then other criteria are necessary in making a policy decision.

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APPENDICES

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APPENDIX A Material Inputs to the Morrow Point Dam 1 of 13

t	line appndx		SIC		Volume Unit				Equip % Profit	Adjusted Total Truck
481	120 c	Landscaping		12.03	100% lump sum	9,100.00	9,100	0,270	0.215 0.196	2,903
694	318 c	Furnishing and constructing the following 13.Et	2491	20.0800	2 each	560	1,120	0.220	0.217912791	630
695	319 c	Type SS with 40-foot pole t	2491	20.0800	3 each	600	1,800	0.220	0.217912791	1,012
696	320 c	Type SS with 45-foot pole t	2491	20.0800	5 each	630	3,150	0.220	0.217912791	1,771
697	321 c	Type SS with 50-foot pole t	2491	20.0800	12 each	700	8,400	0.220	0.217912791	4,722
698	322 c	Type SS with 55-foot pole t	2491	20.0800	0 each	750	0	0.220	0.217912791	0
699	323 c	Type SS with 60-foot pole 1	2491	20.0800	1 each	960	960	0.220	0.217912791	540
700	324 c	Type SD with 45-foot pole t	2491	20.0800	2 each	725	1,450	0.220	0.217912791	815
701	325 c	Type ST with 40-foot pole it	2491	20.0800	0 each	660	0	0.220	0.217912791	0
702	326 c	Type ST with 45-foot pole t	2491	20.0800	4 each	750	3,000	0.220	0.217912791	1,686
703	327 c	Type ST with 50-foot pole t	2491	20.0800						
					3 each	770	2,310	0.220	0.217912791	1,298
704	328 c	Type ST with 55-foot pole t	2491	20.0800	1 each	800	800	0.220	0.217912791	450
705	329 c	Type SA with 55-foot pole t	2491	20.0800	1 each	750	750	0.220	0.217912791	422
706	330 c	Type SAT with 60-foot pole t	2491	20.0800	1 each	820	820	0.220	0.217912791	461
707	331 c	Terminal type with 50-foot pole and per drawit	2491	20.0800	0 each	610	0	0.220	0.217912791	0
81	84 b	Furnishing and placing 1 inch 1.16520 corkboard joint tiller	2499	20.0903	582 ft2	2	1,165	0.090	0.217912791	806
89	92 0	Furnishing and installing miscellaneous metal work in powerplant	2542	23.0500	93,942 lb	1	50,729	0.345	0.217912791	22,173
107	1101b	installing non-embedded metal work except for powerplant	2542	23.0500	26,936 lb	0	10,745	0.345	0.217912791	4,696
108	111b	installing embedded metalwork except for powerplant	2542	23.0500	5,288 lb	1	2,644	0.345	0.217912791	1,156
468	107 c	Furnishing and installing miscellaneous metalwork for powerplant and		23.0500	65.5 b	1 1	65,500	0.345	0.217912791	28,629
475	114 c	Trimming makeup piece ends	2542	23.0500	4 each	225	900	0.345	0.217912791	20,023
638	262 c	Furnishing and installing miscellaneous metalwork in substation	2542	23.0500	4 each 255.7 lb	\$3.50	895	0.345	0.217912791	393
435	74 c	Furnishing and installing one steel work bench	2599	23.0700	100% lump sum	400	400	0.297208267	0.217912791	194
418	57 c	Furnishing installing and testing filter paper drying	2679	24.0706	100% lump sum	1020	1020	0.297208267	0.217912791	495
380	19 c	Furnishing and applying soil- applied herbicide	2879	27.0300	2,180 yd2	0.22	480	0.297208267	0.217912791	233
80	83 b	Furnishing and placing sponge rubber joint filler	2891	27.0402	3,090 ft2	1	3,091	0.090	0.217912791	2,139
182 6		Furnishing and installing 1 inch type B elastic joint filler	2891	27.0402	68 lb	6	374	0.090	0.217912791	259
183 c		furnishing and installing type B rubber water stop	2891	27.0402	16 lin ft	5	72	0.090	0.217912791	50
37	40 b	Pressure grouting foundations	2899	27.0406	76.644 sack	1	76,644	0,110	0.217912791	51.511
40	43 b	Pressure grouting contract on joints and cooling systems	2899	27.0406	5,228 sack		28,663	0.110	0.217912791	17,920
77	80 b	Furnishing and placing metal grout grooves covers	2899	27.0406	3,269 lin ft	3	8,827	0.110	0.217912791	5,933
85	88 5							0.110	0.217912791	
		Furnishing and applying two- coats concrete floor hardener	2899	27.0408	603 yd2		1,207			811
192 5		Furnishing cement for and grouting rock bolts requiring more than one	2899	27.0406	2 3 sack	5	121	0.110	0.217912791	81
310 (As an adjustment for overrun quantity under schedule item 40	2899	27.0406	1 lump sum	17,344	17,344	0.110	0.217912791	11,657
553	192 c	Furnishing and installing one125-volt, 60-cell, station storage battery	2899	27.0406	100% lump sum	15.000.00	15,000	0.110	0.217912791	
632		Furnishing and handling cement	2899	27.0406	99.4 bbl	9	895	0.110	0.217912791	601
752 (Grouting flat jacks in powerplant100%	2899	27.0406	100% lump sum	234.61	235	0.110	0.217912791	158
829 (Assisting in grouting post- tensioned tendons	2899	27.0406	100% lump sum	240.71	241	0.110	0.217912791	162
212 0		For returning 15.75 tons of type II coal tar patch to manufacture	2821	28.0100	1 lump sum	-802	-802	0.110	0.217912791	-539
501	140 c	Furnishing and installing the following sizes of exposed rigid polyvinyl-		28.0100	863.5 lin ft	1.8	1,554	0,110	0.217912791	1,045
502		1 inch in diameter	2821	28.0100	846 lin ft	2.8	1,692	0.110	0.217912791	1,137
82	85 b	Furnishing and placing type E rubber water stops	2822	28.0200	66 lin ft	4	264	0.370	0.217912791	109
83	86 b	Furnishing and placing type F rubber water stops	2822	28.0200	2,122 lin ft		9,549	0.370	0.217912791	3,935
84	87 b	Furnishing and installing rubber joint strips	2822	28.0200	33 lin ft		68	0.370	0.217912791	
461	100 c	Furnishing and placing urethane foam seals	2822	28.0200	100% lump sum	60.0	600	0.370	0.217912791	
513	152 c	Ozone-resisting butyl rubber,No.6 AWG	2822	28.0200	396 lin ft	0.2	79	0.370	0.217912791	
205 j	b	Furnishing material, cleaning, and painting pier nose protection plates	2851	30.0000	1 iump sum	1,505	1,505	0.588	0.217912791	
235]	b	furnishing materials for and painting the exterior surfaces at the ends	2851	30.0000	1 lump sum	430	430	0.588	0.100	134
247 8		Furnishing and delivering to the Government warehouse at Cimarran.	2851	30.0000	1 Jump sum	540	540	0.588	0.100	168
291 (Painting weather door hoists for the spillways and outlet works	2851	30.0000	1 Jump sum	89	89	0.588	0.217912791	17
296 (Painting metal celling support assemblies	2851	30.0000	1 lump sum	529	529	0.588	0.217912791	103
345 (Prime painting spiral stairways for dam	2851	30.0000	1 lump sum	81	2,437	0.568	0.217912791	473
404	43 c	Painting generators	2851	30.0000	5,145 ft2	0.4	2,058	0.588	0.217912791	399
405	44 c	Painting existing handrails and rolling door No.405	2851	30.0000	100% lump sum	700	700	0.588	0.217912791	
406	45 c	Painting existing rock bolts	2851	30.0000	100% lump sum	3,200.00	3,200	0.588	0.217912791	
407	46 c	Painting existing access tunnel portals	2851	30.0000	100% lump sum	800	800	0.588	0.217912791	155
408	47 c	Painting surfaces of concrete walls in powerplant	2851	30.0000	1,267 ft2	0.6	760	0.588	0.217912791	148
409	48 c	Painting concrete and grout surfaces between generator stator wrapp		30.0000	1,000 ft2	1	1,000	0.588	0.217912791	
480	119 c	Constructing entrance and visitor facilities	2851	30.0000	100% lump sum	108,125.00	108,125	0.297208267	0.217912791	52,428
626 0		Painting existing metal roof arch ceiling and appurtenant Soutters	2851	30.0000	16.496 ft2	0.25	4,124	0.588	0.100	
721 (Repairing and painting access tunnel rolling door	2851	30.0000	100% lump sum	635	635	0.588	0.217912791	123
742 (Cleaning and painting steel supports in cable tunnel	2851	30.0000	100% lump sum	1,472.92	1,473	0.588	0.217912791	286
789 (Furnishing, installing, and painting cover plates for 4 tendons and repai		30.0000	100% lump sum	1,256.79	1,4/3	0.588	0.217912791	
811 (Painting servomotor to shifting ring links	2851	30.0000	100% lump sum	81.14	81	0.588	0.217912791	
812 (Cleaning and painting lighting panels	2851	30.0000	100% lump sum	40.52	41	0.588	0.217912791	
813	(I) c	Painting walls in control room	2851	30,0000	100% lump sum	213.8	214	0.588	0.217912791	41

APPENDIX A Material Inputs to the Morrow Point Dam 2 of 13

count line appndx	Pay Item type	SIC	BEA	Volume (Unit	Unit Cost	Total Cost	% Labor %	Equip 9	6 Profit	Adjusted Total Truck	
814 (k) c	Cleaning and painting gate section of log boom	2851	30.0000		lump sum	113.53	114	0.588		0.217912791	22	
815 (I) c	Repairing damaged paint on transformer cooling water discharge pipin	2851	30.0000	100%	lump sum	20.39	20	0.588		0.217912791	4	. (
451 90 c	Furnishing and installing flexible oil hose	3052	32.0500	5280%	lb.	4	211	0.588		0.217912791	41	1
399 38 c	Constructing brick masonry walls	3251	36.0200	100%	lump sum	20,000.00	20,000	0.580		0.217912791	4,042	1
233 h b	Placing a pneumatically applied mortar protective coating over shear a	3255	36.0400	11	lump sum	12,750	12,750	0.297208267		0.217912791	6,182	
56 59 b	Concrete in dam	3272	36.1100	365,179	yd3	. 13	4,747,334	0.400		0.217912791	1,813,895	
57 60 6	Concrete intake structure	3272	36.1100	7,360	yd3	21	154,566	0.400	1	0.217912791	59,058	
58 61 b	Concrete in trashrack structures	3272	36.1100	254	yd3	180	45,823	0.400		0.217912791	17,508	
59 62 b	concrete in curbs, parapets and miscellaneous structures	3272	36.1100	322	yd3	150	48,317	0.400		0.217912791	18,461	
60 63 b	Second-stage concrete in out et works	3272	36.1100	49	yd3	68	3,356	0.400		0.217912791	1,282	
61 64 b	Concrete backfill in existing foundation tunnels	3272	36.1100	247		53	13,142	0.400		0.217912791	5,022	
62 65 b	Concrete in blockouts	3272	36,1100	219		261	57,102	0.400		0.217912791	21,818	
63 66 b	Concrete in floor of foundation tunnels	3272	36.1100	360	vd3	100	36,058	0.400		0.217912791	13,777	
64 67 b	Concrete in penstock tunnel	3272	36.1100	4,126	vd3	27	111,427	0.400		0.217912791	42,575	
65 68 b	Concrete in stilling basin lining	3272	36.1100	1,916,368		0	306,619	0.400		0.217912791	117,155	
66 69 b	Concrete in stilling basin weir	3272	36.1100	10,619		15	159,248	0.400		0.217912791	60,846	
67 70 b	First stage concrete in powerplant Structure	3272	36,1100	3,538		68	240,601	0.400		0.217912791	91,930	
68 71 b	Concrete in draft tube tunnel linings	3272	36.1100	4,478		75	335,904	0.400		0.217912791	128,345	,
69 72 b	Concrete n draft tube gate structures	3272	36.1100	667		44	29,366	0.400	· ····	0.217912791	11,221	····
70 73 b	Concrete in portals of access cable, and ventilation tunnels	3272	36,1100	557		150	83.621	0.400		0.217912791	31.950	
71 74 b	Concrete in floor of access and cable tunnels	3272	36.1100	110		54		0.400		0.217912791	2,273	
72 75 b	Concrete in bridge	3272	36.1100	214		100	21,491	0.400		0.217912791	8,211	
73 76 b	Cooling concrete	3272	36.1100	364,370		1	437,244	0.400		0.217912791	167,065	
123 126 b	Installing one 3.5- by 40-foot tandem outlet gate for outlet works	3272	36.1100		jump sum	24,500	24,500	0.400		0.217912791	9,361	
135 138 b	Furnishing two 2.500-gallon storage tanks	3272	36,1100		lump sum	4,300	4,300	0.400		0.217912791	1,643	
159 165 b	Constructing foundation deformation wells	3272	36.1100		each	500	1,500	0.400		0.217912791	573	
213 e b	Furnishing and placing concrete for cable tunnel linning between stati	3272	36.1100	176		161	28,355	0,400	···	0.217912791	10.834	
and a second		3272	36,1100	26		167	4,330	0.400		0.217912791	1.654	·
223 o b 243 h b	Furnishing and placing concrete in grouting and drainage tunnel floor.	3272	36.1100	65		151	9,787	0.400		0.217912791	3,739	
	Furnishing and placing concrete in crest road retaining walls		36.1100		lump sum		130,067	0.400		0.217912791	49,697	
	Furnishing and Installing 25 post tensioned tendons and furnishing an		36.1100			130,067	25,360	0.400		0.217912791	9,690	
252 g b	Furnishing and placing concrete for protective wall above penstock if			158		158	13,870	0.400		0.217912791	5,300	
254 i b	Furnishing and placing concrete lining in penstock makeup piece reces		36.1100	88						0.217912791		
258 (a) b	Order for Changes No. 13 Furnishing and placing concrete for retain		36.1100	191		150	28,704	0.400		0.217912791	10,967	
264 (a) b	Constructing concrete center pier support in draft tube gate deck	3272 3272	36.1100		lump sum	3,300 18	3,300 2,767	0.400		0.217912791	1,057	
279 (d) b	Furnishing and placing 12-inchdiameter concrete pipe with bedding	3272	36.1100	of	lin ft	8.465	8,465	0.400		0.217912791	3,234	
287 (e) b	Constructing a concrete protective wall above left abutment parking				lump sum	83,920	83,9201	0.400		0.217912791	32,065	
290 (a) b	Order for Changes No. 17 Constructing a concrete retaining wall on	3272	36.1100		lump sum			0.400		0.217912791		·····
292 (a) b	Order for Changes No. 18 Constructing theodolite piers and collimate		36.1100		lump sum	20,204	20,204			0.217912791	7,720	
333 (b) b	Constructing a concrete buttress at downstream toe of right keyway		36.1100		lump sum	17,800		0.400			6,801	
334 (c) b	Constructing a concrete buttress above and downstream of cable tur		36.1100		lump sum	63,228	63,228	0.400		0.217912791	24,159	
377 16 c	Sand backfill in high-voltage cable trench t	3272	36.1100	1,076.70		10		0.400		0.217912791 0.217912791		
387 26 c	Second-stage concrete in powerplant structure	3272	36.1100	5,950		60		0.400	· · · · · · · · · · · · · · · · · · ·	0.217912791	136,407 8,858	
388 27 c	Concrete in blockouts 77.10	3272	36.1100	77.1		300		0.400		0.217912791	8,858	
389 28 c	Miscellaneous concrete in powerplant structure 15.04	3272	36.1100	15.04			2,256					
390 29 c	Concrete floor fill	3272	36.1100	18.34		200	3,668	0.400		0.217912791	1,402	
391 30 c	Concrete in entrance and visitor facilities	3272	36.1100	974.52		135	131,561	0.400		0.217912791	50,268	
392 31 c	Concrete in switchyard structures	3272	36.1100	88.09		110		0.400		0.217912791	3,702	·····
395 34 c	Furnishing and applying concrete floor hardener in powerplant structu		36.1100	658.7		2		0.400		0.217912791	2,822	
396 35 c	Constructing planter area rock masonry walls	3272	36.1100	738.7		10		0.400		0.217912791		
485 124 c	Furnishing and installing single switch-operatin t	3272	36.1100		each	335		0.400		0.217912791	128	
486 125 c	Furnishing and installing double switch-operativit	3272	36.1100		each	568	568	0.400	(-	0.217912791		
500 139 c	Furnishing and installing nonmetallic conduit 3 inches in diameter	3272	36.1100	54		1.5		0.400		0.217912791	31	
637 260 c	Concrete in substation structures	3272	36.1100	78.72		140		0.400		0.217912791	4,211	
642 266 c	Furnishing and installing single switch-operating platforms in substation		36.1100		each	335	335	0.400	·····	0.217912791	128	
680 304 c	Concrete in transmission line tower footings t	3272	36.1100	32.45		150	4,867	0.400		0.217912791 0.217912791	1,860	
750 (e) c	Placing concrete in overbreak in rock excavation for visitor facilities	3272	36.1100	175.42		70	12,280	0.400		0.217912791	4,692	
<u>397 36</u> c	Furnishing and installing guarry tile for floors	3281	36.1500		lump sum	15,000.00	15,000	0.360		0.217912791	6,331	
398 37 c	Furnishing and installing vinyl- asbestos floor tile and vinyl 3 cove bas		36.1700		lump sum	2.700.00	2,700	0.330			1,221	
459 98 c	Furnishing and installing pipe insulation	3292	36.1700		lump sum	500		0.410		0.217912791	186	2.0
22 24 b	Compacted backfill	3295	36.1900	867		4	3,208	0.180	0.640	0.160	64	
23 25 b	Backfill	3295	36.1900	1,659		<u></u>	1,659	0.180	0.640	0.160	33	1,0
24 26 b	Riprap	3295	36.1900	539		3	1,671	0.180	0.640	0.160	33	1,0
164 170 b	Compacted backfill	3295	36.1900	3,333		5		0.180	0.640	0.160	333	10,6
176 182 b	Gravel or crushed-rock surfacing	3295	36.1900	2,461		5		0.180	0.640	0.160	246	7,8
195 e b	Increased cost of restoping certain reaches of crest access road	3295	36.1900	29,899		2		0.180	0.640	0.160	1,495	47.8
201 f b	Placing rock fill material from required excavation for dam and stilling	3295	36.1900	899	yd3	0	422	0.180	0.640	0.160	8	2

APPENDIX A Material Inputs to the Morrow Point Dam 3 of 13

count	1	line	ppndx	Pay item type	SIC	BEA	Volume	Unit	Unit Cost T	Total Cost	% Labor	%Egulo	% Profit	Adjusted Total	Truck
	249 d			Pay item Itype Furnishing and placing free draining non-compacted backfill downstre	3295	36.1900	225		3	787	0.180	0.640	0.160	and the second second second second second second second	· · · · · · · · · · · · · · · · · · ·
	272 (Furnishing and placing new draming holi-compacted backfill for drop structure	3295	36,1900	2,344		1	2,344	0.180	0.640	0.160	16	1,500
	278 (Furnishing and placing rockfill	3295	36,1900	4,881		2	8,395	0.180	0.640	0.160	168	
	281 (, 	Furnishing and placing locking	3295	36.1900	980		27	26,754	0,180	0.640	0.160	535	
	282 (,	Furnishing and placing backfill concrete in wais of power prant chart Furnishing and placing backfill concrete for support of shear zone A	3295	36.1900		yas luma sum	3.770	26,754	0,180	0.640	0.160		
	366	y) 1 5 (Placing and placing backful concrete for support of shear zone A	3295	36.1900	304	Adventure " to send the st " matterne" and		1.702	0.180	0.640	0.160	75	
	367			Placing and compacting backfill for switchvard t	3295	36.1900	298		5.6		0.180	0.640	0,160	33	
	376	6 (15 (Sand backfill and timber protection for buried it	3295	36.1900	147			1,639 529	0.180		0.160		
	378	17		Gravelfills, except in substation	3295	36.1900	258.48		3.6	3,877	0.180	0.640	0.160	11	
	379	18			3295	36.1900	2,656		15		0.180	0.640	0.160	186	
	629	252		Placing 4-inch-thick gravel surfacing Placing and compacting backfill for substation structures	3295	36.1900	2,050		3.5	9,296 2,116	0.180	0.640	0.160		
	630	252			3295	36.1900	529		4	2,118	0.180	0.640	0.160	42	
	631	253		Sand backfill and timber protection for buried insulated electrical cable	3295	36.1900			14		0.180	0.640	0.160	4	31
	678	302		Graveifills in substation	3295	36.1900	4	yd3	4.5	56 761	0.180	0.640	0.160	16	
	208 r		b	Placing and compacting backfill around transmit Furnishing and installing fiberglass insulation in the five weather doors	3296	36.2000		iump sum	902	902	0.180	0.640	0.160	18	
	401	40		Furnishing and installing suspended acoustical ceilings in powerplant s	3296	36.2000		lump sum	3,000	3.000	0.180	0.640	0.160	60	
	636	259		Insulating intersections of reinforcing bars	3296	36.2000	denne i denne p	each	3,000	4,170	0.180	0.640	0.160	83	
	16	17			3312	37.0101	29,910		0	10,469	0.240	0.020	0.260	5.025	
	19	20		Furnishing and placing permanent steel tunnel supports Furnishing and installing steel bearing plates	3312	37.0101	60.226		0	13,250	0.240	0.020	0.260	6,360	
1	131	134		Furnishing and installing steel bearing plates	3312	37.0101	denne ander som fistersondere	iump sum	560,000	560,000	0.240	0.020	0.260	268,800	
	189 6		ս Ե	Furnishing and installing steel liners and piping complete with accessor	3312	37.0101		each	75	525	0.240	0.020	0.260	200,000	
	190 f		b	Furnishing and constructing end post and brace post structures	3312	37.0101		each	50	800	0.240	0.020	0.260	384	
h	196 8		b	Order for Changes No 4 Furnishing and constructing 8 inch galvanied	3312	37.0101	495		5	2,489	0.240	0.020	0.260	1,195	
F	229 0		b	Relocating B-inch standard pipe drain from elevation 67760 to eleva		37.0101		lump sum	243	243	0.297208267		0.217912791	118	
	251 f		X	Performing corrective works on piping	3312	37.0101		lump sum	243	223	0.297208267		0.217912791	108	
	293 (b	installing plezometer piping for tandem outlet gate	3312	37.0101		lump sum	1,049	1,049	0.297208267		0.217912791	505	
	355 (b	Furnishing and delivering surplus bin-type retaining wall	3312	37.0101		lumo sum	5,812	6,812	0.240	0.020	0.260	3,270	
	374	13		Furnishing and installing steel bearing plates	3312	37.0101	11.562.91		1.7	19,657	0.240	0.020	0.260	9,43	
	452	91		Furnishing and installing cast iron soil pipe	3312	37.0101	14.397.90		0.6	8,639	0.240	0.020	0.260	4,147	
	453	92		Furnishing and installing cast iron bell-and-spigot and flanged pipe and		37.0101	22.714		0.4	9,086	0.240	0.020	0.260	4.36	
	454	93		Furnishing and installing steel pipe, fittings, and valves 2	3312	37.0101	10726.3		2.5	26,816	0.240	0.020	0.260	12.872	
	455	94		Furnishing and installing steel pipe, fittings and valves 2.5	3312	37.0101	110,232,40		1	110.232	0.240	0.020	0.260	52,912	
	457	96		Furnishing and installing stainless steel pipe, fittings.	3312	37.0101	130.3		12	1,564	0.297208267		0.217912791	758	
· · · · · · · · · · · · ·	458	97		Furnishing and installing metal tubing, fittings and valves	3312	37.0101	219.96		4	880	0.240	0.020	0.260		
	633	256		Furnishing and placing the following sizes of reinforcment bars: #2 &	3312	37.0101	159		0.4	64	0.240	0.020	0.260		
	634	257	с	4 and 5	3312	37.0101	3.25		0.35	1,138	0.240	0.020	0.260	546	3 2
	635	258	с.	6 and 7	3312	37.0101	1,496		0.34	509	0.240	0.020	0.260	244	
	675	299		1-inch iron-pipe-size	3312	37.0101	85	lin ft	6	510	0.240	0.020	0.260	24	5 1
	731 (C ·	Relocating, replacing and cleaning pipe sleeves and fittings	3312	37.0101		lump sum	358.76	359	0.297208267		0.217912791	17.	4) 1
	756		c	Removing, cleaning, and V reinstalling filling pipe on unfiltered oil tank	3312	37.0101	100%	lump sum	279.77	280	0.297208267	1	0.217912791	136	5
	762		c	Refabricating cooling water piping	3312	37.0101	100%	lump sum	803.41	803	0.240	0.020	0.260	386	3 1
	765		c	Replacing 0.5-inch-diameter piping with 1-inch-diameter piping in brake		37.0101		iump sum	100.58	101	0.240	0.020	0.260	41	3
	783		C	Furnishing and installing steel bearing plates	3312	37.0101	2817.7	łb	2.02	5,692	0.240	0.020	0.260		
	785		с.,	Order for Changes No7: Cutting, cleaning and rewelding overflow pip	3312	37.0101		lump sum	\$353.37	353	0.297208267		0.217912791	17	
	821 (c	Furnishing bearing plates	3312	37.0101	363	each	0.8	290	0.240	0.020	0.260	13	
-	833		C	Performing miscellaneous modifications to piping systems	3312	37.0101	100%	lump sum	391.59	392	0.297208267		0.217912791	190	
1	844		C	Refabricating piping for 0 turbine grease system	3312	37.0101	100%	lump sum	2,869.72	2,870	0.297208267		0.217912791	1,39	
L	21	22		Furnishing and installing chain-link fabric in underground excavation	3315	37.0103	4,536		3	15,135	0.420		0.280	4,54	
	187 1		b	Furnishing and constructing four-wire, barbed-wire fence with steel p		37.0103	5,425		0	2,712	0.420		0.280		
L	188		b	Furnishing and constructing fence crossing river channel	3315	37.0103	202		3	606	0.420		0.280	18:	
[300	()	b	Removing and reinstalling wire cable for 25-ton gantry crane	3315	37.0103		lump sum	345	345	0.420		0.280		
L	371	10		Furnishing and installing chain link fabric on rock faces	3315	37.0103	12,811.79		5	64,059	0.420		0.280		
· · · ·	487	126	c	Furnishing and erecting switchyard fence t	3315	37.0103	440		46.00	20,240.00	0.420		0.280		
	781		с	Furnishing and installing chain link fabric	3315	37.0103	3,399.97		5.93	20,162	0.420		0.280		
L	819		c	Furnishing chain link fabric	3315	37.0103	12		45.63	548	0.420		0.280		
	35	38		Furnishing and placing metal pipe and fittings for foundation grouting a		37.0105	49,134		- 1	31,937	0.420		0.280		
L	38	41		Furnishing and installing metal tubing and fittings for Grouting contract		37.0105	57,402		1	80,364	0.420		0.280		
I	94	97		Furnishing and installing steel pipe and fittings 2 inches and smaller in i		37.0105	386		2	580	0.420		0.280		
1	95	98		Furnishing and installing steel pipe and fittings 25 inches and larger in		37.0105	7,146		1	8,576	0.420		0.280		
1	132	135		Furnishing and installing steel drain piping and fittings	3317	37.0105	25,477			30,573	0.420		0.280		
	133	136	b	Furnishing makeup pieces complete with supports, bolts and coupling		37.0105		lump sum	20,000	20,000	0.420		0.280		
	240		b	seal welding tandem outlet gate liners	3317	37.0105		lump sum	578	578	0.420		0.280		
L	241		b	Furnishing and Installing 6-nondiamster standard steel pipe drain	3317	37.0105		lump sum	7,829	7,829	0.420		0.280		
	350		b	As an adjustment for overrun in guantity under schedule item 38	3317	37.0105		lump sum	13,314	13,314	0.420		0.280		
	92			Furnishing and installing cast iron soll pipe and fittings including bell tra		37.0200	15,847		1	14,262	0.290		0.197		
1	93	96	b	Furnishing and installing cal iron bell-and-spigot and flanged pipe, wall	3321	37.0200	49,855	lb	1	29,913	0.290		0.197	15,34	5

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APPENDIX A Material Inputs to the Morrow Point Dam 4 of 13

Image: Problem Image:	count line apondx	Pay Item type	SIC	BEA	Volume	Unit	Unit Cost T	otal Cost	% Labor %Equip	% Profit	Adjusted Total Truck
Image: Section of the sectio											
Image: space of the s	122 125 b										
P2:10 C Emblance and teached updated on far value in a product on	125 128 b										
J. 50 Sin Imminison of the firm on 24 km label flag wire wire for 0 frag. Sin Jum sum Bit Bit Control Contro Contro <thcontro< th=""></thcontro<>		Furnishing and installing 4-inch-diameter perforated drain for visitor fa	3321	37.0200							
Image: 1.7. Image: 1.7. <thimage: 1.7.<="" th=""> <thimage: 1.7.<="" th=""></thimage:></thimage:>			3462	37.0300	1	lump sum	900	900	0.190	0.210	
68 95 C Districting and Peter Sign and Sign an			3462	37.0300	0	each	12	0	0.190	0.210	
Bit Dial Proving tempore excitus latifications of an opportunit Bit Dial B			3462		284	each	7	1,988	0.190	0.210	1,193
def 1312 Cancel Cancel 1312 Cancel Cancel 1312 Cancel Cancel 1312 341 1312 Cancel Market 335 30.0000 3,721 in Cancel					100%	lump sum	800	800	0.190	0.210	480
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S17 156 f. 40 AVG 325 f. 32,000 62 f. 0 ft 5,42 f. 37 5,220 5,100 177 S16 121 40,000 crolum mil of relation field and fi											
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P.19 D. Lessing 300 million shufter mill angle conduct (00 or 1) statuted 3357 35.000 2.837 Int 0.6 2.831 0.280 0.155 1.297 178 184.0 Funding and intelling and conduct (00 or 1) 3357 35.100 10.357 10.100 10.357 10.100 10.357 10.100 10.357 10.100 10.357 10.100 10.357 10.100 10.357 10.100 10.101 10.101 10.155											
176 184.0 Funning and trailing the tolowing gates of any conducts 600 via 3357 38.1000 10.887 in ft 0 443 5.260 0.169 127 178 186.0 No 0 AVG 3357 38.1000 10.837 in ft 0 2.172 0.280 0.159 1.748 186 No 0 AVG 3357 38.1000 5.000 10 1.772 0.280 0.159 1.748 186 0 0 0.400 0.197 0.280 0.195 1.537 318 100 0 1.846 0 0 0.280 0.195 1.537 318 100 0 1.846 ft 0.195 1.537 1.337 3.1000 1.947 0.280 0.197 1.38 101 0 0.146 ft ft 1.937 0.8100 0.013 1.027 0.280 0.197 1.38 101 0 0.280 0.195 1.337 3.1000 9.040400 in ft 0.161 0.196<											
178 185 b No 10 AVG 3857 38.1000 10.937 lin it 0 2.167 0.280 0.165 1.146 283 (8) b Order for Change Ho. 13 Function and Installing and U200 iter. 3857 38.1000 0 in it 0 0.286 0.155 0 281 (b) b Function and Installing and Installing and U200 iter. 3877 38.1000 0 iter 0 0.286 0.155 0 293 (c) b Function and Installing Inst											
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1 283 (e) 0 Order for Changes No. 15 Functioning and installing about 2000 (inter et of No. 0. 0											
284 (0) b. Function and installing about 300 lines terr of to: 0.0 387.7 38.1000 0 [in ft] 0 0.280 0.1185 0 283 (0) b. Funnishing and installing bars, store for complete error 337.7 38.1000 600 [in ft] 0 180 0.280 0.195 537. 16.100 19.5 19.3 100 59.5 19.7 10.10 0.280 0.195 537. 16.100 10.10 0.280 0.195 537. 16.100 10.10 0.280 0.195 537. 16.100 19.5 19.3 10.10 0.280 0.195 537. 18.1000 8357. 38.1000 6599.1 31m.ft 0.11 10.12 7.77 0.280 0.195 5.81 510 140 10 AVG 3357. 38.1000 450.01 10.14 1.161 0.280 0.195 5.81 511 150 6 AVG 3357. 38.1000 281.01 10.00 7.00 0.280 0.195 5.81 521 152 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>· · · · · · · · · · · · · · · · · · ·</td> <td></td> <td></td> <td></td> <td></td>							· · · · · · · · · · · · · · · · · · ·				
285 (c) D Furnishing and matering about 3000 fines "feet of No. 8 AVG, ange 318 (10) 3927 38, 1000 11 (ump pain (1, 1)) 100 100 0.280 0.195 93, 301 037 144 c 1 AVG mataling the following aixes of single-concluctor, 600-voit insulated 3357 38, 1000 915 (in ft 0.11 101 0.290 0.195 15, 301 046 142 c 1 AVG 3357 38, 1000 19 (in ft 0.11 0.11 0.290 0.195 16, 301 056 142 c 1 AVG 3357 38, 1000 0569 (i, 3) in in 0.18 727 0.280 0.198 4, 335 1512 152 c 5 AVG 3357 38, 1000 6450, 21 (in ft 0.16 1, 101 0.280 0.198 4316 152 152 conductor No.10 AVG 3357 38, 1000 8561 (in ft 0.6 1, 400 0.280 0.198 160 152 164 (in ft 0.6 1, 400 0.280 0.198 160 152 1650 (in ft<											
318 (d) D Fundahing and installing basis famaled, coper solution (coper solution) 337 39,700 91 (lump pain) 25,335 0.280 0.165 13,301 507 14 d c Installing basis (lample-conducto, 600-voltinual del 3357 39,1000 915 (lin ft) 0.11 10.10 0.290 0.195 1,335 508 142 c 12 AVG 3357 39,1000 0.696 (lin ft) 0.14 4,212 0.280 0.195 4,335 519 146 c 12 AVG 3357 39,1000 6,084 (s) lin ft 0.14 4,212 0.280 0.195 4,135 519 146 c 12 AVG 3357 38,1000 6,084 (s) lin ft 0.14 4,212 0.280 0.195 544 524 164 c 12 AVG 3357 38,1000 1.3 lin ft 0.64 0.280 0.195 1564 524 164 c 1494 (s) AVG 3357 38,1000 2.13 lin ft 0.14 0.280 0.195 1565 525 164 c							0				
507 146 Installing the following sizes of single-conductor, 600-vit invalated 3357 39.1000 915 (in ft 0.111 101 0.290 0.175 52 509 148 c 12 AVG 3357 39.1000 6466.6 (in ft 0.135 7.877 0.280 0.195 6.139 510 148 c 12 AVG 3357 39.1000 60.691.3 (in ft 0.13 7.877 0.280 0.195 6.135 511 150 c AVG 3357 39.1000 64.621 (in ft 0.166 1.099 0.280 0.195 561 524 151 c AVG 3357 39.1000 3161 0.16 1.099 0.280 0.195 561 524 154 c Installing the following mattering mathemature, mathmature, mathemature, mathmature, mathemature, mathmature,					1						
600 147 c 14 AVG 3357 78 1000 1648.6 lin ft 0.12 1.978 0.280 0.195 1.039 510 149 c 10 AVG 3357 38 1000 66691.3 lin ft 0.113 7.777 0.280 0.195 2.211 511 1516 6 AVG 3357 38 1000 6.6811 lin ft 0.16 1.099 0.280 0.195 5.211 512 151 c 6 AVG 3357 38 1000 4540.2 lin ft 0.16 1.099 0.280 0.195 5.611 523 162 c Installing the folowing surround (varificat itser/multiconductor, 600-visit as 1000 1.3 lin ft 0.0 1.040 0.280 0.195 5.66 524 163 c Installing the folowing nuticonductor, 600-visit insulated, copper is 3357 38 1000 2.125 lin ft 0.144 0.280 0.195 5.26 526 164 c 550 sin ft 0.214 sin ft 0.214 sin ft 0.244 0.280 0.195 1.235 527 16100 2.351 sin ft <td></td> <td></td> <td></td> <td></td> <td>915</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>					915						
999 148 12 AVG 9337 38.1000 90.084.50 in ft 0.11 7.777 0.280 0.196 4.135 510 149 C 0.440 3337 38.1000 6.081 in ft 0.146 0.128 0.195 5.211 511 150 C 6.4VG 3337 38.1000 6.681 in ft 0.16 1.161 0.280 0.195 5.61 521 C Instaling the following tamored (vertical rise), multiconductor, 600-verti matalated, coper etc. 3357 38.1000 3.81 ft 0.04 0.040 0.280 0.185 5.46 524 153 C Schoold 27.01 0.16 0.44 0.280 0.185 5.46 524 153 C Schoold 27.01 0.04 0.280 0.195 2.55 526 156 Schoold 27.01 Schoold 27.01 0.04 0.280 0.195 2.55 528 157 156 C-conductor No.10 AVG 3337 35.1000 2.644 int 0.23											
S10 149 c. 10 AVG 3357 38 1000 30,084 50 in ft 0.14 4,212 0.280 0.195 52.11 511 156 c. 6 AVG 3357 38 1000 6.681 in ft 0.16 1,161 0.280 0.195 6.10 523 152 (c. 12 conductor No.10 AVG 3357 38 1000 137 18 100 10.04 0.280 0.195 5.16 524 153 (c. 12 conductor No.10 AVG 3357 38 1000 13.1 in ft 0.8 1.040 0.280 0.195 5.46 525 156 (c. 4-conductor No.10 AVG 3357 38 1000 2.172 lin ft 0.14 3.04 0.280 0.195 1.56 527 156 (c. 4-conductor No 3357 38 1000 2.172 lin ft 0.14 3.04 0.280 0.195 1.52 528 156 (c. 4-conductor No 3357 38 1000 2.66 lin ft 0.23 0.280 0.195 1.52 521 172 (c. 4-conductor No											
612 151 6 6 9357 <td></td> <td>10 AWG</td> <td></td> <td>38.1000</td> <td>30,084.50</td> <td>) lin ft</td> <td>0.14</td> <td></td> <td>0.280</td> <td>0.195</td> <td></td>		10 AWG		38.1000	30,084.50) lin ft	0.14		0.280	0.195	
523 162 c Installing the following tarroned (varied) inser, multiconductor, 600-will 3357 38.1000 13.01 in ft 0.9 720 0.280 0.195 546 524 164 c 50-pair No.19 AWG 3357 38.1000 330 in ft 0.75 28.5 0.280 0.195 546 526 164 c 50-pair No.19 AWG 3357 38.1000 2.172 in ft 0.14 30.4 0.280 0.195 160 527 166 c 4-conductor No 3357 38.1000 2.134 lin ft 0.61 17 0.280 0.195 256 528 168 c 2-conductor No 3357 38.1000 2.664 lin ft 0.61 1.77 0.280 0.195 721 531 177 c 4-conductor No.10 AWG 3357 38.1000 2.666 lin ft 0.317 0.280 0.195 732 531 177 c 4-conductor No.10 AWG 3357 38.1000 2.666 lin ft 0.32 163 lin 2.02.00 0.195 173 533		8 AWG					0.16		0.280		
524 163 12-conductor No.10 AWG 3357 38.1000 1.3 in ft 0.8 1.040 0.280 0.195 546 526 166 60-pair No.19 AWG 3357 38.1000 2.172 in ft 0.14 304 0.280 0.195 150 527 166 4-conductor No 3357 38.1000 2.172 in ft 0.14 304 0.280 0.195 235 528 167 12-conductor No 3357 38.1000 2.528 in ft 0.16 1.112 0.280 0.195 741 530 168 2-conductor No.10 AWG 3357 38.1000 2.664 lin ft 0.3 762 0.280 0.195 741 530 168 3-conductor No.10 AWG 3357 38.1000 2.664 lin ft 0.34 3229 0.280 0.195 541 531 170 d-conductor No.10 AWG 3357 38.1000 2.664 lin ft 0.34 329 0.280 0.195 544 531 173 c-conductor No.10 AWG 3357 38.1000 2.644 lin ft 0.34 329		6 AWG									
S25 164 C. 80-pair No.16 AWG 133 38.000 380 in ft 0.75 285 0.280 0.195 150 S26 165 C. Hostaling the following multiconductor, 600-well isualted, copper ele 3357 38.1000 2.134 lin ft 0.14 304 0.280 0.195 150 S27 166 C. 4-conductor No.10 AWG 3357 38.1000 2.642 lin ft 0.61 1.412 0.280 0.195 158 S29 168 c. 2-conductor No.10 AWG 3357 38.1000 2.666 lin ft 0.14 317 0.280 0.195 322 S11 170 C 4-conductor No.10 AWG 3357 38.1000 2.666 lin ft 0.34 329 0.280 0.195 173 S33 172 L 7-conductor No.10 AWG 3357 38.1000 2.642 lin ft 0.42 1.131 0.280 0.195 173 S33 172 L 7-conductor No.10 AWG 3357 38.1000 5.977 1n ft 0.42 1.131 0.280 <t< td=""><td>523 162 c</td><td>Installing the following tarmored (vertical riser), multiconductor, 600-v</td><td>3357</td><td>38.1000</td><td>878</td><td>3 lin ft</td><td>0.9</td><td>790</td><td>0.280</td><td>0.198</td><td>415</td></t<>	523 162 c	Installing the following tarmored (vertical riser), multiconductor, 600-v	3357	38.1000	878	3 lin ft	0.9	790	0.280	0.198	415
526 168 c Installing the following multiconductor, 600-volt insulated, copper etc. 3357 38.1000 2.172 lin ft 0.14 304 0.280 0.195 120 528 167 c 12-conductor No 3357 38.1000 528 lin ft 0.21 448 0.280 0.195 2351 528 167 c 12-conductor No.10 AWG 3357 38.1000 72.843 lin ft 0.18 1.412 0.280 0.195 732.1 530 169 c 2-conductor No.10 AWG 3357 38.1000 2.664 lin ft 0.33 728.2 0.280 0.195 322.1 531 170 c 4-conductor No.10 AWG 3357 38.1000 2.662 lin ft 0.34 329 0.280 0.195 173 533 172 c 7-conductor No.10 AWG 3357 38.1000 4.642 1.131 0.280 0.195 541 533 172 c 7-conductor No.10 AWG 3357 38.1000 5.97 1n ft 0.42 0.280 0.195 2.197 <td>524 163 c</td> <td>12-conductor No.10 AWG</td> <td></td> <td>38.1000</td> <td>1.3</td> <td>B lin ft</td> <td>0.8</td> <td>1,040</td> <td>0.280</td> <td>0.195</td> <td>546</td>	524 163 c	12-conductor No.10 AWG		38.1000	1.3	B lin ft	0.8	1,040	0.280	0.195	546
527 166 c 4-conductor No. 337 38.1000 2.14 ln ft 0.21 448 0.280 0.195 235 528 168 c 2-conductor No.10 AWG 3357 38.1000 528 ln ft 0.18 1.412 0.280 0.195 741 530 159 c 3-conductor No.10 AWG 3357 38.1000 2.864 ln ft 0.18 1.412 0.280 0.195 322 531 170 c 4-conductor No.10 AWG 3357 38.1000 2.664 ln ft 0.3 722 0.280 0.195 171 533 171 c 5-conductor No.10 AWG 3357 38.1000 2.662 ln ft 0.34 329 0.280 0.195 173 533 172 c 7-conductor No.10 AWG 3357 38.1000 647 ln ft 0.3 2.40 0.280 0.195 1.93 534 174 c 12-conductor No.10 AWG 3357 38.1000 0 0 0 0 2.402 0.195 0.195 0.195 0.19											
528 In 7 c 12-conductor No.1 3357 38.1000 528.1m ft 0.6 317 0.280 0.195 166 530 159 c 2-conductor No.10 AWG 3357 38.1000 2.664 in ft 0.23 513 0.280 0.195 322 531 170 c 4-conductor No.10 AWG 3357 38.1000 2.606 in ft 0.34 329 0.280 0.195 322 531 170 c 5-conductor No.10 AWG 3357 38.1000 2.606 in ft 0.34 329 0.280 0.195 173 532 171 c 5-conductor No.10 AWG 3357 38.1000 2.662 in ft 0.34 2.29 0.280 0.195 173 533 172 c 7-conductor No.10 AWG 3357 38.1000 647 if in ft 0.34 0.280 0.195 0.195 0 535 174 c 12-conductor No.10 AWG 3357 38.1000 0 0 0.44 0 0.280 0.195 0.195 0 </td <td></td>											
529 168 c. 2-conductor No.10 AWG 3357 38.1000 7,843 in t 0.16 1,412 0.280 0.195 741 530 159 6 3-conductor No.10 AWG 3357 38.1000 2,666 in t 0.23 613 0.280 0.195 322 531 170 6 4-conductor No.10 AWG 3357 38.1000 2,606 in t 0.34 329 0.280 0.195 173 533 172 6 -conductor No.10 AWG 3357 38.1000 2,606 in t 0.34 329 0.280 0.195 173 533 172 6 -conductor No.10 AWG 3357 38.1000 6.677 in t 0.53 324 0.280 0.195 0.195 170 535 175 c Installing the following armored multiconductor, 6.00-wolf copper cold 3357 38.1000 778 in t 0.46 6.422 0.280 0.195 3.403 536 1											
530 168 c 3 conductor No.10 AWG 3357 38.1000 2,664 in ft 0.23 613 0.280 0.195 322 531 170 c 4-conductor No.10 AWG 3357 38.1000 2,606 im ft 0.3 782 0.280 0.195 410 532 177 c 5-conductor No.10 AWG 3357 38.1000 2,606 im ft 0.34 229 0.280 0.195 410 533 172 c 7-conductor No.10 AWG 3357 38.1000 2,692 in ft 0.42 1,131 0.280 0.195 594 534 173 c 7-conductor No.10 AWG 3357 38.1000 5,977 in ft 0.42 0.144 0.280 0.195 0.195 0 535 174 c 12-conductor No.10 AWG 3357 38.1000 6.193 in ft 0.74 0.280 0.195 0.195 0 536 177 c Installing 25-pair telephone cable 3357 38.1000 778 in ft 0.28 6.482 0.280 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>											
531 1770 4-conductor No.10 AWG 3357 38.1000 2,606 In t 0.3 762 0.280 0.195 410 532 171 5 5 38.1000 969 in th 0.34 325 38.1000 2,692 in th 0.42 1,131 0.280 0.195 574 533 172 C 7-conductor No.10 AWG 3357 38.1000 2,692 in th 0.42 1,131 0.280 0.195 594 534 173 E-conductor No.10 AWG 3357 38.1000 647 in th 0.5 324 0.280 0.195 170 536 175 Installing the following amored multiconductor,600-volt copper cont 3357 38.1000 0 0 0.44 0 0.280 0.195 3403 538 1776 Installing 2-pair telephone cable 3357 38.1000 771 in th 0.86 617 0.280 0.195 344 538 178 Install											
532 171 c 5-conductor No.10 AWG 3357 38,1000 969 in ft 0.34 329 0.280 0.195 173 533 172 C 7-conductor No.10 AWG 3357 38,1000 2,692 in ft 0.42 1,131 0.280 0.195 594 534 173 C 9-conductor No.10 AWG 3357 38,1000 647 in it 0.42 1,131 0.280 0.195 594 535 174 c I2-conductor No.10 AWG 3357 38,1000 647 in it 0.7 4,184 0.280 0.195 0 535 176 installing the following armored multiconductor,600-volt copper cont 3557 38,1000 0 0 0.4 0.280 0.195 3.402 538 177 installing 5-conductor No.10 AWG 3357 38,1000 778 in it 0.45 350 0.280 0.195 3.402 538 177 installing 5-conductor No.4WG copper cold vol insulated anread to 3357 38,1000 571 in ft 0.45 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>											
533 172 C 7-conductor No.10 AWG 3357 38.1000 2,692 in ft 0.42 1,131 0.280 0.195 594 534 173 c 9-conductor No.10 AWG 3357 38.1000 647 lin ft 0.5 324 0.280 0.195 170 536 174 a 12-conductor No.10 AWG 3357 38.1000 0 0 0.4 0 0.280 0.195 2.197 536 176 c 12-conductor No.10 AWG 3357 38.1000 8.103 lin ft 0.8 6,482 0.280 0.195 3.403 537 176 c 12-conductor No.10 AWG 3357 38.1000 778 lin ft 0.8 6,482 0.280 0.195 3.403 538 177 c instaling 50-pair telephone cable 3357 38.1000 771 lin ft 0.8 617 0.280 0.195 3.10 541 180 c instaliing 3-conduc											
534 173 c 9-onductor No.10 AWG 3357 38.1000 647 lin it 0.5 324 0.280 0.195 170 535 174 c 12-conductor No.10 AWG 3357 38.1000 5.977 in it 0.7 4.184 0.280 0.195 2.197 536 175 c installing the following arroared multiconductor,600-volt copper cont 3357 38.1000 0 0 0 0 0 0 0.44 0 0.280 0.195 3.403 537 176 c Itstalling 25-pair telephone cable 3357 38.1000 771 lin it 0.8 6.482 0.280 0.195 3.403 538 178 c installing 50-pair telephone cable 3357 38.1000 771 lin it 0.8 617 0.280 0.195 324 540 178 c installing 50-conductor No AWG copper 600 volt insulated arroard 3357 38.1000 591 lin it 1 591 0.280 0.195 310 541 180 c installing 36-conductor No AWG arro											
536 174 c 12-conductor No. 10 AWG 3357 38.1000 5.977 In ft 0.7 4,184 0.280 0.195 2.197 536 175 Installing time following armored multiconductor,600-volt copper cont 3357 38.1000 0 0 0.4 0.280 0.195 0 537 176 Installing 25-pair telephone cable 3357 38.1000 778 Ini ft 0.45 350 0.280 0.195 3.403 538 177 Installing 25-pair telephone cable 3357 38.1000 778 Ini ft 0.45 350 0.280 0.195 3.403 548 177 Installing 25-pair telephone cable 3357 38.1000 771 Ini ft 0.45 350 0.280 0.195 314 538 178 Installing 25-pair telephone cable 3357 38.1000 591 Ini ft 1 2.80 0.195 310 541 180 Installing 30-t0 AWG camper 600 volt insulated armored 3357 38											
536 175 c Installing the following amored multiconductor,600-volt copper cont 3357 38,1000 0 0 0.4 0 0.280 0.195 0 537 176 I2-conductor No.10 AWG 3357 38,1000 8.103 init 0.8 6,482 0.280 0.195 34.03 538 177 c Installing 50-pair telephone cable 3357 38.1000 771 in it 0.46 6,482 0.280 0.195 34.03 538 177 c Installing 50-pair telephone cable 3357 38.1000 771 in it 0.46 6.17 0.280 0.195 31.00 541 180 c Installing 15,000-volt insulated more day to opter 4.3357 38.1000 591 11.16 1 2,221 0.280 0.195 11.66 542 181 c Installing 30-00 Volt insulated amore and y to operate 3.3357 38.1000 100% iump sum 196,800.00 196,800 0.195 11.66 521/1 c <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>											
\$37 176 c 12-conductor No. 10 AWG 3357 38.1000 8.103 in ft 0.8 6,482 0.280 0.195 3,403 538 177 c installing 55-pair telephone cable 3357 38.1000 776 in ft 0.45 350 0.280 0.195 184 539 178 c installing 50-pair telephone cable 3357 38.1000 771 in ft 0.45 350 0.280 0.195 184 540 179 c installing 50-pair telephoner cable 3357 38.1000 591 in ft 1 591 0.280 0.195 310 541 180 c Funsiting and installing completely outfited and ready to operate 3 3357 38.1000 2.221 lin ft 1 2.221 0.280 0.195 130 541 181 c Funsiting and installing completely outfited and ready to operate 3 3357 38.1000 400 inft 0.56 224 0.280 0.195 118 <td></td> <td></td> <td></td> <td></td> <td>agentia a la construir en e</td> <td>A REAL PROPERTY OF A REAL PROPER</td> <td></td> <td></td> <td></td> <td></td> <td></td>					agentia a la construir en e	A REAL PROPERTY OF A REAL PROPER					
538 177 c Installing 25-pair telephone cable 3357 38,1000 778 lin ft 0.45 350 0.280 0.195 154 538 178 c installing 3co-pair telephone cable 3357 38,1000 778 lin ft 0.45 350 0.280 0.195 324 538 178 c installing 3conductor No AWG copper 600 volt insulated armored 3357 38,1000 571 lin ft 1 1 0.280 0.195 324 541 180 c Installing 15,000-volt insulated No.IAWG, 3-conductor (auminum) ar 3357 38,1000 2.221 lin ft 1 1 2,280 0.195 1,166 542 181 c Furnishing and installing completely outfitted and ready to operate 3 3357 38,1000 2.001 lin ft 0.196,000 0.80 0.195 133,200 620 i. c installing 3/c-1/0 AWG numti- conductor600-volt insulated copper el 3357 38,1000 435 lin ft 0.51 477 0.280 0.195 250 621 J. c Installing 3/c-1/0 AWG numti- conductor600-volt insulated copper el </td <td></td>											
538 178 c Installing 50-pair telephoner cable 3357 38.1000 771 In ft 0.8 617 0.280 0.195 324 540 178 Installing 50-pair telephoner cable 3357 38.1000 591 In ft 1 591 0.280 0.195 324 541 180 c Installing 15,000-voit insulated monumarial 3357 38.1000 2.221 In ft 1 591 0.280 0.195 310 541 180 c Installing 36:00 AWG starting one potents 3357 38.1000 2.221 In ft 1 2.221 0.280 0.195 311.86 620 L c Installing 36:00 AWG starting one potents 3357 38.1000 400 in ft 0.56 2.280 0.195 118 621 C Installing 36:00 AWG amuti- conductor 600-voit insulated capper ei 3357 38.1000 435 installing 36:00 0.195 115 621 C Installing 36:03 AWG amuti- conductor 600-voit insulated capper											
540 179 c Installing 3-conductor No AWG copper 600 volt insulated armorad c 3357 38.1000 591 in ft 1 591 0.280 0.195 310 541 180 c Installing 15,000-volt insulated No.1AWG, 3-conductor (autimium) ard 3337 38.1000 2.221 lin ft 1 2.221 0.280 0.195 1.166 542 181 c Functionand and ready to operate 3 3357 38.1000 2.021 lin ft 1 2.221 0.280 0.195 1.166 620 L c Installing 30-10 AWG tarmored (vertical riser), mutti- roenductor600 3357 38.1000 400 lin ft 0.56 224 0.280 0.195 118 621 J c Installing 30-10 AWG tarmored (vertical riser), mutti- roenductor600 volt insulated copper et 3357 38.1000 479 lin ft 0.51 477 0.280 0.195 250 622 K. c Installing 70-10 AWG mutti- conductor60-volt insulated copper et 3357 38.1000 479 lin ft 0.42 849											
641 180 Installing 15,000-volt insulated No.J AWG, 3-conductor (aluminum) ar 3357 38,1000 2.221 Im 1 2.221 0.280 0.195 1.166 542 181 c Furnishing and installing completely cultified and ready to operate 3 3357 38,1000 100% iump sum 196,800.00 196,800 0.280 0.195 103,320 6201.i c Installing 3/c-1/0 AWG ammotive conductors00-volt insulated copper 3357 38,1000 400 iin tt 0.56 224 0.280 0.195 116 621.j c Installing 3/c-1/0 AWG mutti- conductors00-volt insulated copper 3357 38,1000 935 iin ft 0.51 477 0.280 0.195 250 622.k c Installing 3/c-1/0 AWG ammored multi-conductors00-volt insulated copper 3357 38,1000 479 iin ft 0.42 849 0.280 0.195 251 623.L c Installing 7/c-10 AWG ammored multi-conductors00-volt insulated copper co 3357 38,1000 2021 iin ft 0.42 849 0.280 0.195 27 </td <td></td>											
542 181 c Furnishing and installing completely outlifted and ready to operate 3: 3357 38.1000 100% lump sum 196,800 0.280 0.195 103,320 620 L c installing 3/c-1/0 AWG tarmored (vertical riser), multi: conductor600 3357 38.1000 400 lin tt 0.56 224 0.280 0.195 118 621 J c installing 3/c-1/0 AWG multi- conductor600 volt insulated copper el 3357 38.1000 935 lin tt 0.511 477 0.280 0.195 151 622 K c Installing 3/c-1/0 AWG multi- conductor600-volt insulated copper el 3357 38.1000 479 lin ft 0.6 287 0.280 0.195 151 623 L c Installing 7/c-10 AWG multi- conductor,600-volt copper cd 3357 38.1000 2.021 lin ft 0.42 849 0.280 0.195 27 653 277 c 8 AWG installing the following size of single-conductor, 600-volt,insulated copper 4 3357 38.1000 92 lin ft 0.15 14 0.280 0.195 27 653							+				
620 L c Installing 3/c-1/0 AWG tarmored (vertical riser), multi- roonductor600 3357 38,1000 400 lin ft 0.56 224 0.280 0.195 118 621 J c Installing 3/c-1/0 AWG tarmored (vertical riser), multi- roonductor600-volt insulated copper e 3357 38,1000 935 lin ft 0.51 477 0.280 0.195 250 622 K. c Installing 3/c-1/0 AWG multi- conductor600-volt insulated copper e 3357 38,1000 479 lin ft 0.6 287 0.280 0.195 415 623 L c Installing 3/c-1/0 AWG aurmored multi-conductor, 600-volt insulated copper ed 3357 38,1000 2.021 lin ft 0.42 848 0.280 0.195 446 652 276 c Installing 7/c-10 AWG aurmored multi-conductor, 600-volt.Insulated c 3357 38,1000 93 lin ft 0.14 52 0.280 0.195 27 653 277 c 8 MvG 3357 38,1000 93 lin ft 0.14 52 0.280 0.195 7 654 278 c 6 AWG							196 800 00				
621 J c Installing 3/c-1/0 AWG mutil- conductor600-volt insulated copper 3357 38.1000 935 lin ft 0.51 477 0.280 0.195 250 622 K. Installing 3/c-1/0 AWG mutil- conductor600-volt insulated copper el 3357 38.1000 479 lin ft 0.6 287 0.280 0.195 151 623 L c Installing 3/c-1/0 AWG >armored mutil- conductor600-volt insulated copper el 3357 38.1000 2021 lin ft 0.42 849 0.280 0.195 446 652 276 G Installing the following sizes of single-conductor, 600-volt, insulated 3357 38.1000 933 lin ft 0.14 52 0.280 0.195 27 653 277 G 6 AWG NG 3357 38.1000 93 lin ft 0.15 14 0.280 0.195 27 654 278 c 6 AWG 3357 38.1000 925 lin ft 0.19 48 0.280 0.195 25 655 280 c 4/0 AWG 3357 38.1000 258 lin ft 0.19 48 0.280 0.195 <td></td>											
622 K c Installing 3/c-3/0 AWG multi- conductor/600-volt insulated copper el 3357 38.1000 479 lin ft 0.6 287 0.280 0.195 151 623 L c Installing 3/c-3/0 AWG multi- conductor/600-volt copper c 3357 38.1000 2.021 lin ft 0.42 849 0.280 0.195 446 652 276 c Installing the following sizes of single-conductor, 600-volt, insulated copper ci 3357 38.1000 373 lin ft 0.14 52 0.280 0.195 247 653 277 c 8 AWG 3457 38.1000 90 lin ft 0.15 14 0.280 0.195 27 654 278 c 6 AWG 3357 38.1000 92 lin ft 0.15 14 0.280 0.195 25 655 279 c 1/c-75,000-circular mil AWG 3357 38.1000 225 lin ft 0.75 194 0.280 0.195 192 656 280 c 4/0 AWG 3357 38.1000 86 lin ft 0.75 194 0.280 0.195 192 656 28											
623 L c Installing 7/c-10 AWG >armored multi-conductor, 600-volt copper cc 3357 38,1000 2.021 Im ft 0.42 849 0.280 0.195 446 652 276 c installing 7/c-10 AWG >armored multi-conductor, 600-volt copper cc 3357 38,1000 373 Im ft 0.14 52 0.280 0.195 27 653 277 c 8 MVG 3357 38,1000 90 (in ft 0.15 14 0.280 0.195 7 654 278 c 6 AWG 3357 38,1000 925 lim ft 0.19 48 0.280 0.195 25 655 278 c 16-750,000-circular mil AWG 3357 38,1000 225 lim ft 0.75 194 0.280 0.195 102 656 280 c 4/0 AWG 3357 38,1000 86 lim ft 0.43 37 0.280 0.195 102											
652 276 Installing the following sizes of single-conductor, 600-volt, insulated c 3357 38.1000 373 in 0.14 52 0.280 0.195 27 653 277 c 8 AWG 3357 38.1000 90 (in ft 0.15 14 0.280 0.195 7 654 278 c 6 AWG 3357 38.1000 92 (in ft 0.19 48 0.280 0.195 7 654 278 c 1/c<750,000-circular mil AWG											
653 277 c 8 AWG 3357 38.1000 90 in ft 0.15 14 0.280 0.195 7 654 278 c 6 AWG 3357 38.1000 225 in ft 0.19 48 0.280 0.195 25 655 279 c 1/c~750,000-circular mil AWG 3357 38.1000 225 lift 0.75 194 0.280 0.195 102 656 280 c 4// AWG 3357 38.1000 86 lin ft 0.43 37 0.280 0.195 19											
664 278 c 6 AWG 3357 38.1000 225 lin ft 0.19 48 0.280 0.195 25 655 278 c 1/c-750,000-circular mil AWG 3357 38.1000 225 lin ft 0.75 194 0.280 0.195 102 656 280 c 4/0 AWG 3357 38.1000 8.6 lin ft 0.43 37 0.280 0.195 19											
655 278 c 1/c-750,000-circular mil AWG 3357 38.1000 258 lin ft 0.75 194 0.280 0.195 102 656 280 c 4/0 AWG 3357 38.1000 86 lin ft 0.43 37 0.280 0.195 194											
656 280 c 4/0 AWG 3357 38.1000 86 lin ft 0.43 37 0.280 0.195 19											
											19
	659 283 c	Complete installation and make connections of control cable	3357	38.1000			1,100.00	1,100			

APPENDIX A Material Inputs to the Morrow Point Dam 5 of 13

count line appndx	Pay Item type	SIC	BEA	Values	Unit	Unit Cost	Total Cont	% Labor 19	(Engla II	N. Durit		
713 337 c	Pay Item type Furnishing and installing suspension-type asser t	3357	38.1000	Volume	each	en an	Total Cost 870	contract in a second se	6Equip			Truck
714 338 c	Furnishing and installing tension-type assemblic t	3357	38.1000		each	30 60	720	0.280		0.195	457	
715 339 c	Furnishing and stringing three No.2 AWG, ACS t	3357	38.1000	1.72		\$7,720.00	13,263	0.280		0.195	6,963	
716 340 c	Furnishing and attaching spiral type vibration d.t	3357	38.1000		each	\$7,720.00	1,764	0.280		0.195	926	
726 (i) c	Furnishing color coded No.10 600-volt, single- conductor, type THW	3357	38.1000		lin ft		240	0.280		0.195	126	
727 (i) c	Furnishing color coded No.12AWG, 600-volt, single- conductor type 1	3357	38,1000	15.000		0.04	600	0.280		0.195	315	
732 (e) c	Mounting and connecting wiring to terminals of transfer switch in trans		38.1000		lump sum	49.61	50	0.280		0.195	26	
738 (k) c	Furnishing and installing 3-inch electrical conduit for telephone cables	3357	38.1000	235.6		10	2,356	0.280	· · · · · · · · · · · · · · · · · · ·	0.195	1,237	
749 (d) c	Installing Government- furnished, 6-pair communications cable	3357	38.1000	2,183		0.45	982	0.280		0.195	516	
760 (g) c	Furnishing additional 230-kilovolt cable	3357	38.1000		lin ft	4	500	0.280		0.195	263	
766 (a) c	Order for Changes No6: Furnishing oil for the 230 kilovolt insulated d	3357	38.1000		bbl	\$81.50	245	0.280		0.195	128	······
471 110 c	Furnishing and installing aluminum covers in switchyard620	3363	38.1100	620	lb	\$2.00	1,240	0.379	······································	0.251	459	
639 263 c	Furnishing and installing aluminum covers in substation	3363	38.1100	486.2	lb	2	972	0.379		0.251	360	
472 111 c	Furnishing and installing aluminum handrail for crest road and service a	3364	38.1300	100%	lump sum	4.900.00	4,900	0.379		0.251	1,813	
836 (o) c	Furnishing and installing service sink in oil purifier room	3431	40.0100	100%	lump sum	585.63	586	0.502		0.282	126	
169 175 b	Furnishing and constructing metal bin-type retaining walls.5.5-loot bas	3441	40.0400	2,106	ft2	10	21,653	0.196	0.065	0.213	11,400	1,40
170 176 b	Furnishing and constructing metal bin-type retaining walls1.75-foot ba	3441	40.0400	746	ft	10	7,466	0.196	0.065	0.213	3,931	48
177 183 b	Furnishing and erecting structural steel for bridge	3441	40.0400	48,556	lb	Ō	9,711	0.196	0.065	0.213	5,113	63
219 k b	For deleting the eight ice prevention system nozzles.associated tubin		40.0400	1	lump sum	-14	-14	0.196	0.065	0.213	-7	
226 a b	Order for Changes No 7 Bonding field joints in rubber series s for pe		40.0400	1	lump sum	587	587	0.196	0.065	0.213	309	3
230 e b	Furnishing and installing modified support jackets on power plant meta		40.0400	102	each	156	15,922	0.196	0.065	0.213	8,383	1,03
250 e b	Furnishing materials for and performing corrective works on power pl		40.0400	1	lump sum	444	444	0.196	0.065	0.213	234	2
253 h b	Furnishing and placing reinforcing steel for protective wall above pen		40.0400	723		0	166	0.196	0.065	0.213	87	1
257 (a) b	Order for changes No. 12 installing the 20 Government furnished fla		40.0400	1	lump sum	22,281	22,281	0.196	0.065	0.213	11,731	1,44
294 (c) b	Straightening Government furnished fixed-wheel gate for spillway No.	3441	40.0400	1	lump sum	338	338	0.196	0.065	0.213	178	2
483 122 c	Furnishing and erecting switchyard steel structures	3441	40.0400	50.029		0.5		0.196	0.065	0.213	13,170	1,62
640 264 c	Furnishing and erecting substation steel structures	3441	40.0400	9,307		0.6	5,584	0.196	0.065	0.213	2,940	36
641 265 c	Moving and reinstalling existing substation steel structures	3441	40.0400		lump sum	1,300.00	1,300	0.196	0.065	0.213	684	8
<u>681 305 c</u>	Furnishing and erecting transmission line steel t	3441	40.0400	52,556		0.47	24,701	0.196	0.065	0.213	13,005	1,60
686 310 c	Furnishing and installing tower leg grounds with t	3441	40.0400		each	65	520	0.196	0.065	0.213	274	3
690 314 c	At Curecanti end of Morrow Point-Curecanti 25 t	3441	40.0400		tump sum	4.000.00	4,000	0.196	0.065	0.213	2,106	26
691 315 c	Furnishing materials for second and third spans t	3441	40.0400		lump sum	2,200.00	2,200	0.196	0.065	0.213	1,158	14
724 (g) c 88 91 b	Modifying pipe jack turbine supports to extend to existing rock	3441	40.0400		iump sum	1,011.95	1,012	0.196	0.065	0.213	533	6
88 91 b 99 102 b	Furnishing and installing metal rolling doors	3442 3442	40.0500		1113	6	5,040	0.101		0.137	3,840	
103 106 b	Furnishing and installing weather doors Furnishing and installing nine industrials-type steel swinging doors	3442	40.0500		lump sum	3,500	18,000 3,500	0.101		0.137	13,716	
104 107 b	Furnishing and installing one steel window	3442	40.0500		lump sum	170	3,500	0.101		0.137	130	
204 i b	Furnishing and installing one additional double steel swinging door in a	3442	40.0500		lump sum	678	678	0.101		0.137	517	
402 41 c	Furnishing and installing steel swinging doors in powerplant structure	3442	40.0500		lump sum	5,100.00	5,100			0.137	3,886	
403 42 c	Furnishing and installing metal- clad fire doors	3442	40.0500		lump sum	1.100.00	1,100		· · · · · · · · · · · · · · · · · · ·	0.137	838	
627 P c	Furnishing and installing four spillway weather door I operators	3442	40.0500		lump sum	10.500	10,500	0.101		0.137	8,001	
818 (o) c	Furnishing and handling electric-operated sliding weather door	3442	40.0500		lump sum	1.322.50	1.323	0.101		0.137	1,008	
105 108 b	installing trashrack and slot closure	3443	40.0600	224,250		1022100	16,819	0.297208267		0.217912791	8,155	
344 (h) b	As an adjustment for underrun in quantity under schedule item 108	3443	40.0600		lump sum	4,500	4,500	0.297208267		0.217912791	2,182	
416 55 c	Installing three aftercoolers	3443	40.0600		lump sum	625	625	0.297208267		0.217912791	303	
417 56 c	Installing six air receivers	3443	40.0600		lump sum	1,520.00	1,520	0.297208267		0.217912791	737	
470 109 c	Furnishing and installing cable trays	3443	40.0600		lump sum	3,018.00	3,018	0.297208267		0.217912791	1,463	
476 115 c	Furnishing and installing penstock filling line	3443	40.0600		lump sum	13,500.00	13,500			0.217912791	6,546	
477 116 c	Furnishing and installing hydropneumatic tank	3443	40.0600		lump sum	3.400.00	3,400			0.217912791	1,649	
478 117 c	Furnishing, testing, and installing all material and equipment for modil		40.0600		lump sum	9,000.00				0.217912791	4,364	
479 118 c	Furnishing and installing engine-generator set	3443	40.0600		lump sum	14,740.00			1	0.217912791	7,147	
718 (a) c	Order for Changes No2: Installing two Government- S furnished 2,50		40.0600	100%	lump sum	\$ 1.300.00	1,300			0.217912791	630	
91 94 b	Furnishing and installing embedded heating and ventilating ducts	3444	40.0700	3,888	B Ib	2	6,999	0.174	0.034	0.165	4,389	23
165 171 b	Furnishing and laying 24-inch- diameter No. 1Cgaugs corrugated-meta	3444	40.0700		lin ft	11		0.174	0.034	0.165	3,173	17
166 172 b	Furnishing and installing 30-inch diameter No. 14 gauge corrugated-m	3444	40.0700		each	85		0.174	0.034	0.165	586	3
167 173 b	Furnishing and erecting 168 Inch diameter No 3 gage multiple-plate c		40.0700		in ft	150	11,400		0.034	0.165	7,148	38
168 174 b	Furnishing and erecting 168inch-diameter No gage multiple plate con		40.0700		s lin ft	1 30			0.034	0.165	8,803	47
175 181 b	Furnishing and installing metal railing for bridge	3444	40.0700		lin ft	6	1,087	0.174	0.034	0.165	682	3
224 p b	Constructing forms for blocks 8. 10. and 12 made obsolete by change		40.0700		lump sum	948	948		0.034	0.165	594	
227 b b	re-fabricating and recalculating leaders and gutters in power plant	3444	40.0700		lump sum	133		0.174	0.034	0.165	83	
228 c b	constructing formed air ducts below elevation 7164.97 in penstock	3444	40.0700		lump sum	4,897	4,897	0.174	0.034	0.165	3,070	16
280 (e) b	For additional costs for furnishing additional metalwork required in po-		40.0700	8,598		0	995		0.034	0,165	624	
97 100 b	Furnishing and installing access stairways	3446	40.0800		lump sum	12,000	12,000		0.016	0.219	6,828	19
98 101 b	Installing spiral stairways in dam	3446	40.0800	129,854		0			0.016	0.219	13,300	37
102 105 b	Fumishing and installing handrall	3446	40.0800		lin ft	15			0.016	0.219	5,644	15
237 b b	As an adjustment for increased cost for f Furnishing and Installing me	3446	40.0800	1 1	lump sum	4,747	4,747	0.196	0.016	0.219	2,701	

APPENDIX A Material Inputs to the Morrow Point Dam 6 of 13

count	line appndx	Pay Item type	SIC	BEA	Volume Unit	Unit Cost	Total Cost	% Labor	%Equip % Profit	Adjusted Total	Truck
	266 (c) b	Furnishing and installing platform and ladder support assemblies in pov	3446	40.0800	9 each	156	1,404	0.196	0.016 0.219	799	22
	267 (d) b	Furnishing and installing additional handrail in powerplant chamber	3446	40.0800	130 lb	1	132	0.196	0.016 0.219	75	2
	465 104 c	Furnishing and installing steel railing for sidewalks and retaining walls	3446	40.0800	11,649 lb	1.5	17,474	0.196	0.016 0.219	9,942	280
	753 (h) c	Installing protective handrail in cable tunnel	3446	40.0800	100% lump sum	109.25	109	0.196	0.016 0.219	62	2
	792 (h) o	Modifying handrailing at a pproach to visitor facilities	3446	40.0800	100% tump sum	48.61	49	0.196	0.016 0.219	28	1
	793 (i) c	Repairing and painting handralling at draft tube gate deck	3446	40.0800	100% lump sum	415.46	415	0.196	0.016 0.219	236	
	808 (e) c 87 90 b	Realining handrail for powerplant access road	3446	40.0800	100% lump sum	218.26	218	0.196	0.016 0.219	124	3
	87 90 b 48 51 b	Furnishing and installing metal ceiling Furnishing and handling cement, except for grouting	3448 3449	40.0901	11,709 ft2 436,265 bbl	3	31,615	0.297208267	0.217912791	15,330	0
	49 52 0	Furnishing and handling sacked cement for grouting foundations and c	3449	40.0902	81,803 sack	5		0.231	0.066 0.450	518,763 35,184	135,329 9,178
	50 53 b	Furnishing and handling special cement for grouting contraction joints	3449	40.0902	4,240 sack	2		0.231	0.066 0.450	1.931	9,176
	51 54 b	Furnishing and handling sacked cement for grouting rock bolts	3449	40.0902	1,289 sack	2		0.231	0.066 0.450	652	170
	52 55 b	Furnishing and placing reinforcement bars of the following sizes No 3	3449	40.0902	137 lb	0		0.231	0.066 0.450	7	2
	53 56 b	No.s 4 and 5	3449	40.0902	117,501 b	0		0.231	0.066 0.450	4,459	1,163
	54 57 b	No.s 6 and 7	3449	40.0902	602,075 lb	0	90,311	0.231	0.066 0.450	22,849	5,961
	55 58 b	No 8 and larger	3449	40.0902	2,225,510 lb	0	333,827	0.231	0.066 0.450	84,458	22,033
	217 i b	furnishing cement for grout and grouting cable tunnel linning voids	3449	40.0902	287 sack	4		0.231	0.066 0.450	316	82
	259 (b) b	Furnishing and installing reinforcement steel for retaining wall betwee		40.0902	10,103 lb	0		0.231	0.066 0.450	588	153
	297 (f) b 351 (g) b	Performing backfill grouting of outlet works steel liner	3449	40.0902	1 lump sum	2,113	2,113	0.231	0.066 0.450	535	139
	351 (o) b 382 21 c	As an adjustment for overrun in guantity under schedule item 52 Furnishing and handling cement	3449 3449	40.0902	1 lump sum 9,268.75 bbl	<u>5,006</u> 9	5,006 83,419	0.231	0.066 0.450	1,267 21,105	330 5,506
	383 22 0	Furnishing and placing the following sizes of reinforcement bars: 2 an	3449	40.0902	4.86 lb	0.3	1,458	0.231	0.066 0.450	21,105	5,506
	384 23 c	4 and 5	3449	40.0902	60.316 lb	0.25		0.231	0.066 0.450	3,815	995
	385 24 c	6 and 7	3449	40.0902	49,297 lb	0.24		0.231	0.066 0.450	2,993	781
	386 25 c	8 and larger	3449	40.0902	361.416 lb	\$0.23	83,126	0.231	0.066 0.450		5,486
1	679 303 c	Furnishing and handling cement t	3449	40.0902	38.38 bbl	9	345	0.231	0.066 0.450		23
	682 306 c	Furnishing and placing the following sizes of ret	3449	40.0902	110 lb	0.4		0.231	0.066 0.450		3
	683 307 c	4 and 5 t	3449	40.0902	597 lb	0.35	209	0.231	0.066 0.450		14
	684 308 c	6 and 7 t	3449	40.0902	2,910 lb	0.35		0.231	0.066 0.450	258	67
	685 309 c	B and t	3449	40.0902	1,877 lb	0.35		0.231	0.066 0.450		43
and the second	816 (m) c 817 (n) c	As an equitable adjustment for substitution of Prostrata junipers in lier Furnishing and installing metal lath for guarry tile installation	3449 3449	40.0902	100% lump sum 100% lump sum	2,500.00		0.231	0.066 0.450		165
and the state	17 18 b	Furnishing and installing grouted rock bolts in powerplant chamber and		41.0100	66,613 lin ft	4		0.517	0.008 0.450		
· · · · · · · · · · · · · · · · · · ·	18. 19 5.	Furnishing and installing ungrouted rock bolts in powerplant chamber a	3452	41.0100	918 lin ft	2		0.517	0.308	289	ŏ
	20 21 b	Furnishing and installing ungrouted rock bolts in open-cut excavation	3452	41.0100	47,488 lin ft	3		0.517	0.308		0
	36 39 b	hookups to foundation grout holes	3452	41.0100	1,684 hookup	20	33,680	0.517	0.308	5,894	0
	39 42 b	Hookups to contraction joint 9"Yf1"8 system	3452	41.0100	196 hookup	45			0.308		0
	100 103 b	installing Government furnished anchor bolts	3452	41.0100	17,463 lb	0		0.517	0.308		0
	101 104 b	Furnishing and installing anchor bolts	3452	41.0100	5,544 lb	1		0.517	0.308		0
	158 164 b	Installing rock boit load cells	3452	41.0100	26 each	250			0.308		0
	185 a b 191 a b	Order for Changes No 2 Furnishing and installing expansion bolts of Order for change # 3 Furnishing and constructing 1-inch diameter pro		41.0100	3,201 each 17,826 ft	4		0.517	0.308		. <u> </u>
	193 c b	Furnishing and constructing 0.75inch-diameter ungrouted rock bolts v		41.0100	19.140 ft	7		0.517	0.308		0
	194 d b	Furnishing and constructing 0.75inch-diameter ungrouted rock bolts	3452	41.0100	3,008 ft	15		0.517	0.308	8,107	0
	207 I b	Furnishing and installing modified rock bolts	3452	41.0100	67,531 lin ft	0			0.308		0
	210 b b	Furnishing and installing grouting rock bolts around portal of ventilatio		41.0100	276 lin ft	10		0.517	0.308		0
	211 c b	Furnishing and Installing groutable rock bolts within ventilation adit	3452	41.0100	36 lin ft	9		0.517	0.308		0
	234 I D	fumishing and installing 148 anchor bars and driling holes for MPBX	3452	41.0100	1 lump sum	49,700		0.517	0.308	8,698	0
L	238 c b	Furnishing and Installing 1375inch hollow core rock bolts	3452	41.0100	1,534 lin ft	31		0.517	0.308		0
1	288 (f) b	As an adjustment for overrun in quantity under schedule item 18	3452	41.0100	1 lump sum	19,209		0.517	0.308		0
I	372 11 c	Furnishing and installing rock bolts	3452	41.0100	736 lin ft 4,500 each	7			0.308		0
	373 12 c 469 108 c	Furnishing and installing expansion bolts Installing generator anchor bolts	3452	41.0100	4,500 leach 100% lump sum	5,500			0.308		
	474 113 c	Installing generator anchor bons Installing penstock makeup pieces complete with supports, bolts and		41.0100	100% lump sum	8,000		0.517	0.308		
	780 (o) c	Furnishing surplus rock bolts	3452	41.0100	8,250 lin ft	0.5			0.308		
	782 (g) c	Furnishing and installing 2-foot expansion bolts	3452	41.0100	1,112 each	11.86		0.517	0.308		
[784 (s) C	Furnishing and installing rock bolts	3452	41.0100	100 lin ft	8.3	830	0.517	0.308	145	
	820 (q) c	Furnishing expansion bolts	3452	41.0100	291 each	3.13		0.517	0.308		0
	400 39 c	Furnishing and installing movable metal partitions	3469	41.0203	100% lump sum	5,400			0.217912791	2,618	0
	449 88 c	Furnishing and installing hose adapters	3429	42.0300	123.3 lb	7		0.297208267	0.217912791	418	0
	74 77 b	Furnishing and pacing 1-Inch- outside-diameter metal pipe or tubing i	3498	42.0800	311,063 lin ft	1	202,191		0.217912791	98,038	0
	124 127 b	Installing one hydraulic control system for the 3.5- by 40-foot tande		42.0800	1 lump sum	2,300			0.265		0
	130 133 b	Furnishing and installing reservoir level gauge well heating system	3492	42.0800	1 lump sum 6 each	400			0.137		U 0
	157 163 b 186 b b	Installing reinforcement meters Furnishing and installing pielometer piping for outlet works	3492 3498	42.0800	1 lump sum	400			0.137		0
	186 b b 197 b b	Furnishing and installing hangers for one or two pipes	3498	42.0800	19 sack	4,479			0.265		0
L	U 10	remaining and mataling nangera to one of two pipes	<u>9129</u>		i o joquin				0.200		·,0

APPENDIX A Material Inputs to the Morrow Point Dam 7 of 13

count line appndx	Pay Item type 1	SIC	BEA	Volume	Unit	Unit Cost	Total Cost	% Labor %	Equip	% Profit	Adjusted Total Truck
198 c b	Furnishing and Installing hangers for three pipes	3498	42.0800	11	each	38	418			0.265	
206 k b	deleting the salt velocity piping and connector for penstock steel line	3498	42.0800	1	lump sum	-1,275	-1,275	0.451		0.265	-362
214 f b	Furnishing and Installing 3-inch pipe for weep holes in cable tunnel lin	3498	42.0800	58	lín ft	6	343	0.451	-	0.265	97
215 g b	Furnishing and Installing 15inch pipe in cab e tunnel lining for back fill g	3498	42.0800	212	lb	2	350	0.451		0.265	99
218 j b	For deleting the 16-inchair vent piping from penstock intake Structur	3498	42.0800	1	lump sum	-1,525	-1,525	0.451		0.265	-433
246 a b	Order for Changes No. 11 Furnishing and Installing additional piping to	3498	42.0800	1	tump sum	76)	76	0.451		0.265	22
255 j b	Furnishing and Installing weep pipe in lining of penstock makeup piece	3498	42.0800	3	lin ft	9	28	0.451		0.265	8
256 k b	Removing tight rock from penstock makeup piece recess	3498	42.0800	1	lump sum	324	324	0.451		0.265	92
260 (c) b	Furnishing and installing weep pipe for retaining wall between stations	3498	42.0800	206	lin ft	2	506	0.451		0.265	144
265 (b) b	Furnishing and installing 1.5inch-diameter standard pipe extensions to	3498	42.0800	1,209	łb	3	3,361	0.451		0.265	955
298 (g) b	As an adjustment for overrun in quantity under schedule item 58	3498	42.0800	1	lump sum	27,578	27,578	0.451		0.265	7,832
420 59 c	Furnishing installing and testing motor-operated valves	3491	42.0800	2,491	lb	4	9,964	0.451		0.265	2,830
425 64 c	Furnishing and installing pressure gages	3492	42.0800	23	each	45	1,035	0.451		0.265	294
426 65 c	Furnishing and installing differential pressure gauges	3492	42.0800	5	each	150	750	0.451		0.265	213
440 79 c	Furnishing and installing air-release valve	3491	42.0800	135		2	270	0.451		0.265	77
441 80 c	and vacuum valves	3491	42.0800	672	lb	2.5	1,680	0.451		0.265	477
442 81 c	Furnishing and installing air- operated butterfly valves	3491	42.0800	1.292		6	7,752	0.451		0.265	2,202
443 82 c	Furnishing and installing relief valves	3491	42.0800	53800%	lb ·	4	2,152	0.451		0.265	611
444 83 c	Furnishing and installing pressure-regulating valves	3491	42.0800	118400%	1b	\$4.50	5,328	0.451		0.265	1,513
445 84 c	Furnishing and installing weight-operated valve	3491	42.0800		lump sum	190	190			0.265	
446 85 c	Furnsihing and installing electro-hydraulic-operated valves	3491	42.0800	6200%		12.5	775			0.265	
447 86 c	Furnishing and installing solenoid valves	3491	42.0800	72.5		10	725			0.265	
460 99 c	Furnishing and installing pipe hangers and supports	3498	42.0800	8,602.60		3	25,808		of the second second second	0.265	
787 (c) c	Furnishing and installing a 2.5l inch gate valve	3491	42.0800		lump sum	188.31	188			0.265	
410 49 c	Installing and testing two 83.000-horsepower hydraulic turbines	3511	43.0100		lump sum	301.755.00	301,755			0.217912791	
411 50 c	Installing and testing two184,000-foot-pound governors for hydraulic	3511	43.0100		lump sum	19.600.00	19,600			0.217912791	
482 121 c	Constructing irrigation system	3523	44.0001		lump sum	2.800.00	2,800			0.217912791	
86 89 b	Furnishing and erecting steel for powerplant crane runway	3531	45.0100	288,957		0	54,902	0.297208267		0.217912791	
106 109 b	Installing 30-ton gantry crane Rack	3531	45.0100	1	lump sum	2,600	2,600			0.217912791	
109 112 b	Installing one 300-ton overhead traveling crane	3531	45.0100	1 i	lump sum	34,000	34,000	0.297208267		0.217912791	
110 113 5	Installing one 30-lon gantry crane	3531	45.0100	1	lumo sum	11,500	11.500	0.297208267		0.217912791	
111 114 b	Installing one 20-ton gantry crane	3531	45.0100	1	lump sum	8,000	8.000			0.217912791	
112 115 b	Installing one 6ton Dingle I-beam crane	3531	45.0100	1	lump sum	850	850	0.297208267		0.217912791	
231 f b	Furnishing and installing pipe sleeves for crane runway column and g	3531	45.0100		each	53	8,111	0.297208267		0.217912791	
466 105 c	Modifying crane girders	3531	45.0100		lump sum	3.000.00	3,000			0.217912791	
643 267 c	Furnishing and installing double switch-operating platforms in substatic	3531	45.0100	100 /8	each	568	568		··· ···	0.217912791	
772 (g) c	Replacing hydraulic brake system on 250-ton traveling crane	3531	45.0100	100%	lump sum	504.41	504			0.217912791	
773 (h) c	Furnishing and installing new rectifiers in hoist motors of 250-ton trave	3531	45.0100		lumo sum	234.98	235		· ···· —···	0.217912791	
778 (m) c	Replacing defective brake coil on auxiliary hoist of 250-ton traveling	3531	45.0100		lump sum	124.97	125			0.217912791	
353 (q) b	installing dam sump pumps and controls	3561	49.0100		lump sum	2,957	2,957			0.217912791	
412 51 c	Installing and testing two sump pumping units	3561	49.0100		lump sum	3,420.00	3,420			0.217912791	
413 52 c	Furnishing, installing and testing three cooling water pumping units	3561	49.0100		lump sum	6,100.00	6,100			0.217912791	
413 32 5 414 53 c	Furnishing, installing, and testing two oil pumping units	3561	49.0100		lump sum	1,720.00	1,720			0.217912791	
414 535 415 54 c	Installing and testing three air compressors	3563	49.0100		lump sum	1,390.00	1,390			0.217912791	
431 70 c	Furnishing and installing sump eductor	3561	49.0100		lump sum	1,100.00	1,100			0.217912791	
431 70 C	Furnishing installing and testing one sump pumping	3561	49.0100		lump sum	3,200.00	3,200			0.217912791	
90 93 5	Furnishing and erecting enclosures for penstock intake structure gate	3569	49.0700	1	lump sum	29,000	29,000		0.012	0.106	
114 117 b	Installing two 13.5 by 1607-foot. fixed-wheel gates for penstock ins	3569	49.0700	+	lump sum	6,400	6,400		0.012		
115 118 b	installing two frames for 13.5 by 1607-foot, fixed-wheel gates for pensiock me	3569	49.0700	+	lump sum	4,500	4,500		0.012	0.106	
116 119 b	Installing two hydraulic hoists for 13.5- by 1601-foot fixed-wheel ge	3569	49.0700		lump sum	4,500	4,500		0.012		
118 121 b	installing four 15- by 1683- foot, fixed-wheel gates for spillways	3569	49.0700		lump sum	12,000	12.000		0.012		
110 121 0 119 122 b	Installing four frames for 15- by 1683-foot, fixed-wheel gates for spinways	3569	49.0700		lump sum	8,500	8,500		0.012		
120 123 0		3569	49.0700		lump sum	8,500			0.012		
120 123 0 127 130 b	Installing four Hoists for 15- by 1683-foat, fixed-wheel gates Installing seats and guides for bulkheads gates for draft tunnel and fo	3569	49.0700	128,430		0,400	17,338		0.012		
128 131 b	Installing lifting frames and fitting beam	3569	49.0700		lump sum	700	700		0.012		
128 131 b		3569	49.0700		lump sum	5,400	5,400		0.012		
129 132 b	Furnishing and installing one reservoir level gauges well and piping	3569	49.0700		each	5,400	5,400		0.012		
	Furnishing and installing extension eter protection assemblies	3569	49.0700			3.380.00	3,380		0.012	0.217912791	
and the second	Installing and testing fixed carbon dioxide fire-extinguishing system	3569	49.0700		lump sum	13000	13,000		0.012		
448 87 c	Fumshing and installing flanged twin strainers				lump sum				0.012		
838 (g) c	Mounting two motor starters f for dam sump pumps	3569	49.0700		lump sum	45.86	46				
450 89 c	Furnishing and installing flexible metal hose	3599	50.0400) lb	10	800		0.012		
547 186 c	Installing main control board CCA and sequential operations recorder	3577	51.0104	100%	lump sum	\$ 8.250.00	8,250			0.217912791 0.129	
134 137 b	Furnishing and installing ice prevention air systems	3585	52.0300		lump sum	26,000	26,000				
463 102 c	Furnishing and installing water coolers in powerplant structure	3585	52.0300		lump sum	720				0.129	
473 112 c	Furnishing and installing heating, ventilating, and air-conditioning syste	3585	52.0300		lump sum	155,000.00	155,000			0.125	
419 58 c	Installing and testing chlorinating equipment	3589	52.0500	100%	lump sum	660	660	0.297208267		0.217912791	<u>1 3201</u>

APPENDIX A Material Inputs to the Morrow Point Dam 8 of 13

count		line appndx	Pay Item type	SIC	BEA	Volume	Unit	Unit Cost	Total Cost	% Labor	%Equip	% Profit	Adjusted Total	Truck
		106 c	Furnishing and installing transformer vault enclosure	3612	53.0200		lump sum	31,000.00	31,000	0.037		0.104		248
		189 c	Installing transformer remote- indicating panel KSA	3612	53.0200	100%	lump sum	600	600	0.037		0.104		
		193 c	Furnishing and installing one9-kilovolt-ampere480/208/120-volt cont	3612	53.0200	100%	tump sum	700	700		0.008	0.104	596	
		203 c	Installing generator voltage isolated-phase bus structure	3612	53.0200		tump sum	13.325.00	13,325	0.037	0.008	0.104	11,340	107
- 1		204 c	Installing generator voltage segregated-phase bus structures with pro		53.0200		lump sum	2,000.00		0.037		0.104	1,702	16
		205 c	Installing two generator neutral grounding transformers resistors, and	3612	53.0200		lump sum	2,000.00	2,000	0.037		0.104	1,702	16
		223 c	Furnishing and installing lighting transformers for dam and appurtenan	3612	53.0200	1.951		3	5,853			0.104	4,981	
	624 M	C	Furnishing and installing three Idifferential relays, one t differential loc		53.0200		lump sum	760	760			0.104	647	
	625 N 720 ©	c	Installing one 150-kilcvolt ampere lighting transformer K2E (formerly	3612	53.0200		lump sum	850	850			0.104	723	
1 · · · · · · · ·	761 (h)) C	type G lighting fixtures in powerplant	3612	53.0200		each	30	780			0.104		
	767 (b)		Moving d-c lighting contactor100%	3612	53.0200		lump sum	210.36	210			0.104		
) c 120 b	Modifying lighting and power panels and transfer switches installing two hydraulic control systems for 13.5- by 1607- foot, fixe	3612 3613	53.0200 53.0300		iump sum	185	185			0.104		
		143 b	Furnishing and installing 600- volt. BO-ampere power receptacles con	3613	53.0300		lump sum each	4,800	4,800 200			0.110	3,902	
		144 b	Furnishing and installing 600 volt 100-ampere power receptacies com		53.0300		each	200	600			0.110	163	
1	427	66 c	pressure switches	3613	53.0300		each	56		0.077		0.110	488	
	428	67 c	switches	3613	53.0300		each	145				0.110		
	430	69 c	Furnishing and installing combination float and pressure switch	3613	53.0300		lump sum	764	764			0.110		
1		144 c	Furnishing and installing 480 volt, 60-ampere power receptacles come		53.0300		each	100	600			0.110		
		145 c	Furnishing and installing 480 volt, 100-ampere power receptacle com	3613	53.0300	1	each	120	120			0.110	98	
		190 c	Installing 480-volt station- service switchgear DCA	3613	53.0300	100%	lump sum	4,000.00	4,000			0.110		
1		195 c	Furnishing and installing 16automatic transfer switches	3613	53.0300		lump sum	8,400.00	8,400			0.110		
		196 c	Furnishing and installing five alternating current distribution boards M1	3613	53.0300	100%	iump sum	8.500.00	8,500			0.110	6,911	C
		197 c	Furnishing and installing two 460-volt alternating-current emergency (3613	53.0300		lump sum	2,785.00	2,785			.0.110		
+		198 c	Furnishing and installing one direct-current distribution board BCA	3613	53.0300		lump sum	3.500.00	3,500			0.110		
		202 c	Installing two 14.4-kilovolt station-type generator switchgear assemb		53.0300		tump sum	4.400.00	4,400			0.110		
		206 c	Installing 230-kilovolt, 3-pole manually gang-operated air switch with 3	3613	53.0300		lump sum	\$2.470.00	2,470			0.110		
		207 c 208 c	Installing 14.4-kilovolt 3-pole, manually gang-operated air switch	3613	53.0300		lump sum	1.000.00	1,000			0.110		
		208 c	Installing 14.4-kilovolt single-pole hook-operated disconnecting fuses Installing 13.2-kilovolt single- phase, 15-kilovolt ampere switchyard of		53.0300		each Iump sum	50	250			0.110		
		213 c	Installing 240/120-volt switchyard station-service distribution panelt		53.0300		each	500	150			0.110		
		214 c	Installing 15-kilovoit current transformer	3613	53.0300		each	200				0.110		
		215 c	Furnishing and installing 1.431,000-circular mid ACSR, strain and jump		53.0300	372.6		1,490.40	200	0.077		0.110		
		216 c	Furnishing and installing No.2AWG, ACSR, jumper bus	3613	53.0300		lin ft	72	<u></u>	0.077		0.110		
		217 c	Furnishing and installing No.4/0 AWG copper jumper bus	3613	53.0300		lin ft	3	6	0.077		0.110	5	
	579	218 c	Furnishing and installing 1-inch iron-pipe-size rigid aluminum bus	3613	53.0300	149	lin ft	6	894	0.077		0.110	727	C
	581	220 c	Furnishing and installing instrument transformer terminal box	3613	53.0300		each	100		0.077		0.110		C
		234 c	Furnishing and installing eight lighting panelboards in dam and appurter	3613	53.0300	100%	lump sum	8,313.00	8,313	0.077		0.110		C
·		235 c	Furnishing and installing time switches in dam and appurtenant structu		53.0300		each	130				0.110		
		236 c	Furnishing and installing miscellaneous electrical equipment items in d		53.0300	8,077.40		7	56,542			0.110		
· · · ·		249 c	Installing recessed-type panelboards L1B L2B, L2C, and LCA in glazed		53.0300		each	110	330			0.110		
		250 c	Removing and reinstalling panelboard fronts on formed concrete reces		53.0300		each	25	75			0.110		
	619 H	C	Removing three single-pole i breakers and furnishing and t installing a		53.0300		lump sum	36				0.110		
1		286 c 287 c	Installing 15-kilovolt, 3-pole,gang-operated air switch	3613	53.0300		each	1,150.00				0.110		
		287 C	Installing 230-kilovolt, 10,000-ampere power circuit breaker Installing 14.4-kilovolt 250-megavoit ampere power circuit breaker	3613 3613	53.0300 53.0300	0	each	0 0 \$3,200.00	0 3.200	0.077		0.110		
1		289 c	Installing 14.4-kilovoit 250-megavoit ampere power circuit breaker Installing 14.4-kilovoit, single- phase, current-limiting reactors	3613	53.0300	A second reaction of the second second second	each	\$3,200.00	3,200	0.077		0.110		
		291 c	Installing 14.4-kilovolt, single prase, current many reactors	3613	53.0300		each	150				0.110		
		293 c	Reinstalling 14.4-kilovolt fused disconnecting switches	3613	53.0300		each	50				0.110		
		294 c	Reinstalling 13.2-kilovolt, 50,1 kilovolt ampere single-phase transform		53.0300		each	210				0.110		
		295 c	Fumishing and installing954.000-circular mid ACSR strain and jumper I		53.0300		lin ft	4				0.110		
		296 c	Furnishing and installing No.2	3613	53.0300		lin ft	3				0.110		
		297 c	Reinstalling 230-kilovolt pedestal insulators, technical reference No.2		53.0300		each	100				0.110		
		300 c	Furnishing and installinginstrument transformer terminal boxes	3613	53.0300		each	105				0.110		
	825 (d)		Installing load and frequency cabinet CCD 100%	3613	53.0300		lump sum	572.47				0.110		
		139 0	Furnishing and installing parapet lighting units	3646	55.0200	28	each	60	1,680			0.200		
		145 b	design, furnish and install lighting in powerplant, access tunnel and ver		55.0200	<u> </u>	lump sum	33,000	33,000			0.200		
	317 (c)		Fabricating and installing mounting brackets for type GG lighting fixtur		55.0200		lump sum	645	645	0.290		0.200		
	319 (e)		As an adjustment for increased costs for furnishing type DD, EE, and	3646	55.0200		lump sum	14,502	14,502	0.290		0.200		
	320 (f)		Providing temporary storage for lighting equipment, materials, and for		55.0200		lump sum	977	977			0.200		
	323 (i)		As an adjustment for changes in lighting system requirements unde		55.0200 55.0200		Jump sum	-7,068	-7,068			0.200		
. <u>-</u>		221 c 224 c	Furnishing and installing switchyard tapered-pole type t lighting units Furnishing and installing lighting system wiring devices in dam and app	3645 3645	55.0200		each each	250 15				0.200		
		225 c	Furnishing and installing lighting system wining devices in dani and ap-		55.0200		each	30				0.200		
1		225 C	Type DB	3645	55.0200		each	42				0.200		
1		227 0	Type DC	3645	55.0200		each	\$30.00				0.200		
Line of				00-0	1 00.0400				420	0.200	· · · · · · · · · · · · · · · · · · ·	0.200	<u> </u>	·

APPENDIX A Material Inputs to the Morrow Point Dam 9 of 13

count line appndx	Pay Item type	SIC	BEA	Volume Unit	Unit Cost	Total Cost	% Labor %Equip	% Profit Adjust	ted Total Truck
589 228 c	Type DE	3645	55.0200	3 each	46			0.200	70 70
590 229 c	Туре DF	3645	55.0200	13 each	25	325		0.200	166
591 230 c	Type DG	3645	55.0200	7 each	55	385		0.200	196
593 232 c	Type DJ	3645	55.0200	4 each	290			0.200	592
594 233 c	Type DK	3645	55.0200	4 each	45			0.200	92
598 237 c	Installing the following types of lighting fixtures for the powerplant: 1	3645	55.0200	3 each	27	81		0.200	41
599 238 c	Type A in second-stage concrete	3645	55.0200	21 each	27	567	0.290	0.200	289
600 239 c	Туре В	3645	55.0200	59 each	20	1,180	0.290	0.200	602
601 240 c	Туре Е	3645	55.0200	6 each	17	102	0.290	0.200	52
602 241 c	Type J	3645	55.0200	8 each	27			0.200	110
603 242 c	Туре	3645	55.0200	8 each	20	160	0.290	0.200	82
604 243 c	Туре М	3645	55.0200	6 each	13	78	0.290	0.200	40
605 244 c	Type N	3645	55.0200	2 each	20	40	0.290	0.200	20
606 245 c	Type AA	3645	55.0200	12 each	26			0.200	159
607 246 c	Туре ВВ	3645	55.0200	7 each	26			0.200	93
608 247 c	Furnishing and installing type T lighting fixtures inside heating and vent	3645	55.0200	6 each	25			0.200	77
609 248 c	Installing lighting system wiring devices	3645	55.0200	80 each	10	800		0.200	408
617 F c	Furnishing and installing type HH lighting fixtures in access tunnel	3645	55.0200	100% lump sum	6.550.00	6,550		0.200	3,341
618 G C 140 146 b	Access tunnel lighting conduit t modification for circuit 6LSB	3645	55.0200	0 lump sum	\$330.00	0		0.200	0
140 146 D 141 147 b	Furnishing and installing embedded electrical rigid metal conduit::0.5 in 0.75 inch in diameter	3644 3644	55.0300 55.0300	1,145 fin ft 7,783 lin ft		1,260		0.269	312
141 147 b 142 148 b	0.75 mch in diameter	3644	55.0300	7,783 lin π 3,648 lin ft	2			0.269	2,896
142 148 b	15 inches in diameter	3644	55.0300	5,487 lin ft	3			0.269	3,402
143 149 b	2 inches in diameter	3644	55.0300	3,925 lin ft	3	11,776		0.269	2.920
145 151 b	25 inches in diameter	3644	55.0300	1,837 lin ft	3	6,431		0.269	1,595
146 152 b	3 inches in diameter	3644	55.0300	2,450 lin ft	5			0.269	2,735
147 153 b	35 inches in diameter	3644	55.0300	2,904 lin ft	5			0.269	3,602
148 154 b	5 inches in diameter	3644	55.0300	12 lin ft	8			0.269	25
149 155 b	4 inches in diameter	3644	55.0300	437 lin ft	6			0.269	650
236 a b	Order for Changes No 8 As an adjustment for increased costs for ins		55.0300	1 jump sum	306			0,269	76
321 (g) ib	As an adjustment for furnishing 480-volt power receptacles in lieu of		55,0300	1 lump sum	215			0.269	53
324 (j) b	Furnishing and installing conduit and grounding system for crest road	3644	55.0300	1 lump sum	2,117		0.483	0.269	525
330 (P) b	Furnishing and installing additional 0.75-inch rigid metal conduit in out	3644	55.0300	1 Jump sum	67	67	0.483	0.269	17
331 (q) b	Furnishing and installing additional 2.5-inch rigid metal condult for inst		55.0300	1 jump sum	295			0.269	73
464 103 c	Furnishing and installing bus enclosure	3643	55.0300	120 lin ft	120			0.269	3,571
492 131 c	Furnishing and installing the following sizes of embedded and/or expo	3644	55.0300	1,207.80 lin ft	1.5	1,812		0.269	449
493 132 c	0.75 inch in diameter	3644	55.0300	8975.4 lin ft	2			0.269	4,452
494 133 c	1 inch in diameter	3644	55.0300	3224.5 lin ft	2.5			0.269	2,123
495 134 c	1.5 inches in diameter	3644	55.0300	3,921.60 lin ft	3.5			0.269	3,404
496 135 c	2 inches in diameter	3644	55.0300	3,163.10 lin ft	4.5			0.269	3,530
497 <u>136</u> c	2.5 inches in diameter	3644	55.0300	1,170.10 lin ft	5.5			0.269	1,596
498 137 c	3 inches in diameter	3644	55.0300	643.3 lin ft	\$6.50	4,181		0.269	1.037
499 138 c	5 inches in diameter	3644 3644	55.0300	88 lin ft 80 each	10			0.269	218 397
503 142 c 504 143 c	Furnishing and installing No.1 cast metal outlet boxes	3644	55.0300 55.0300	50 each	20			0.269	397
543 182 c	Furnishing and installing No.2 cast metal outlet boxes Furnishing and installing fabricated sheet steel boxes and wireways	3644	55.0300	1,360.40 lb	4.5			0.269	1,518
552 191 c	Installing one main lighting board LCA	3644	55.0300	1,300.40 ib 100% lump sum	4.5	800		0.269	198
555 194 c	Installing indoor electronic equipment	3644	55.0300	1 each	750			0.269	186
560 199 c	Furnishing and installing one indoor terminal and cooling control cabine		55.0300	100% lump sum	2.800.00	2,800		0.269	694
572 211 c	Installing 192-kilovolt station class lightning arresters	3644	55.0300	3 each	150			0.269	112
573 212 c	Installing 15-kilovolt intermediate-type lighting s arresters	3644	55.0300	3 each	70			0.269	52
583 222 c	Furnishing and installing outdoor power receptacles	3644	55.0300	0 each	30		A REAL PROPERTY AND A REAL	0.269	0
648 272 c	Furnishing and installing the following electrical rigid metal condult: 5		55.0300	1.005 lin ft	7.5			0.269	1,869
649 273 c	4 inches in diameter	3644	55.0300	7 lin ft	6		0.483	0.269	10
650 274 c	2 inches in diameter	3644	55.0300	11 lin ft	5			0.269	14
651 275 c	1 inch in diameter	3644	55.0300	94 lin ft	4	282		0.269	70
666 290 c	Installing 15-kilovolt,N intermediate class lightning arresters	3644	55.0300	6 each	70			0.269	104
708 332 c	Furnishing and placing plate or cone guy ancho t	3644	55.0300	30 each	90			0.269	670
709 333 c	Furnishing and placing grouted guy anchors t	3644	55.0300	11 each	110			0.269	300
710 334 c	Furnishing and constructing single guys t	3644	55.0300	25 each	75			0.269	465
711 335 c	Furnishing and constructing double guys	3644	55.0300	20 each	115			0.269	570
712 336 c	Furnishing and installing guy protectors	3644	55.0300	7 each	22			0.269	38
763 (i) c	Rewiring current limiting resistors on 250-ton crane	3644	55.0300	100% lump sum	36.5			0.269	9
768 (c) c	Furnishing and installing two 51-pair telephone terminal blocks	3661	56.0300	100% lump sum	845			0.254	259
646 270 c	Processing insulating oil	3663	56.0500	0 gal	0.16			0.21/912/91	18.016
491 130 c	Furnishing and installing all materials for grounding system	3662	57.0300	10899.01 lb		32,697	0.204	0.100	10,0101

APPENDIX A Material Inputs to the Morrow Point Dam 10 of 13

count line appn	ix Pay Item type	SIC	BEA	Volume	Unit	Unit Cost	Total Cost	% Labor %	(E-ula	N/ Deefla	A.I	ruck
561 200 c	Installing two 3-phase 1000 - kilovolt ampere station- service transfor		57.0300		lump sum	3.000.00	3,000		«Еquip	% Profit	and the second sec	ruck o
562 201 c	Installing three single-phase 12.2- to 230-kilovolt.52,000-kilovolt am		57.0300		lump sum	19.500.00	19,500	0.483		0.269	4,836	0
571 210 c	Installing 230-kilovolt coupling b capacitor potential devices	3675	57.0300		each	300	900			0.269	4,636	
660 284 c	Installing 230-kilovolt coupling capacitor potential devices	3675	57.0300		each	300	900	0.483		0.269	223	
75 78 b	Furnishing and installing thermocouples	3823	62.0200	9.039		1	10,576	0.120		0.130	7,932	
222 n b	Installing additional joint meters in dam	3823	62.0200		each	117	3.048	0.120		0.130	2,286	0
225 a b	Order for Changes No. 6 Furnishing all materials labor for work and c		62.0200		lump sum	4,949	4,949	0.120		0.130	3.712	
432 71 c	Furnishing and installing industrial-type thermometers	3823	62.0200		each	80	240	0.297208267		0.217912791	116	0
434 73 c	Furnishing and installing two water-level switches	3823	62.0200		lump sum	250	250	0.297208267		0.217912791	121	
436 75 c	Furnishing and installing gauge boards for miscellaneous instruments	3823	62.0200	1,960	h	0.2				0.217912791	190	0
439 78 c	Furnishing and installing rate-of flow indicators	3823	62.0200		each	500				0.217912791	727	
741 (n) c	Installing Chemonitor CF-1 chemical feeder in dam pump chamber	3823	62,0200		lump sum	325.98	326	0.297208267		0.217912791	158	ů.
150 156 b	Installing sets of thermostats	3822	62.0300		set	160		0.321		0.210	825	0
151 157 b	A groups	3822	62.0300	73	group	395	28,800	0.321		0.210	13,507	0
152 158 b	8 groups	3822	62.0300		group	600	3,600	0.321		0.210	1,688	0
153 159 b	C groups	3822	62.0300	4	group	500	2,000	0.321		0.210	938	0
154 160 b	D group	3822	62.0300	7	group	400	2,800	0.321		0.210	1,313	0
155 161 b	E group	3822	62.0300	8	group	1,000	8,000	0.321		0.210	3,752	0
156 162 b	F groups	3822	62.0300	2	group	1,500	3,000			0.210	1,407	0
2201 b	Installing two groups of eight pore pressure meters in dam block 10	3822	62.0300	2	group	532				0.210	499	0
221 m b	Installing one group of eight pole pressure metals in dam block 10 at		62.0300	1	group	847	847			0.210	397	0
429 68 c	Furnishing and installing two pneumatic liquid level I	3822	62.0300		lump sum	2,480.00				0.210	1,163	0
462 101 c	Processing lubricating and governor oil	3822	62.0300	1116500%		0.15				0.210	785	0
78_81b	Furnishing and placing type Z metal seals	3953	64.0503	22,566		4				0.217912791	41,580	0
79 82 b	Furnishing and placing type N2 metal seals	3953	64.0503		lin ft	3		0.297208267		0.217912791	2,289	. 0
394 33 c	Furnishing and placing type N2 metal seals	3953	64.0503		lin ft	8				0.217912791	1,043	0
433 72 c	Nameplates	3993	64.1100		each	7.5				0.181	1,781	0
488 127 c	Furnishing and installing equipment identification signs	3993	64.1100		each	16				0.181	58	0
489 128 c	Furnishing and installing phase identification signs	3993	64.1100		each					0.181	83	0
490 129 c	Furnishing and installing warning and safety signs	3993	64.1100		each	35			······	0.181	85	0
644 268 c	Furnishing and installing equipment identification signs	3993	64.1100		each	22			2	0.181	281	0
645 269 c	Furnishing and installing phase identification signs	3993	64.1100		i each	11				0.181	100	
687 311 c	Danger signs t	3993	64.1100		each	\$35.00	140			0.181	85	0
688 312 c	Tower number signs t	3993	64.1100	2		24	48			0.181	29	0
422 61 c 423 62 c	Installing hand-portable carbon dioxide fire extinguishers	3999	64.1200		lump sum	360				0.158	801	
	Furnishing and installing firehose reels firehose.	3999 3999	64.1200		tump sum	1,210.00	460			0.158	305	·
424 63 c 437 76 c	Furnishing and installing miscellaneous fire protection equipment Furnishing and installing three wheeled-portable carbon dioxide fire ex		64.1200		lump sum	900				0.158	596	0
857	Onsight Trucking and Excavation	3999	65.030		lump sum	300	900	0.100		0.150	3,711,364	
693 317 c	Clearing land and right-of-way for 13.8-kilovoit t	clear land	clear land		lump sum	5.500.00	5,500	0.392	0.368	0.240	3,711,304	2,024
173 179 b	Removing and disposing of county bridge No. 3	disposal	disposal	1004	lump sum	1,760			0.329		0	579
322 (h) b		disposal	disposal		lump sum	1.076			0.329		Ő.	354
328 (n) b	As an adjustment for extra costs in disposing of excess conduit	disposal	disposal		lump sum	188			0.329		Ō	62
8 9 b	Drilling line holes for opencut rock excavate	drill	drill) lin ft	1			0.395		7	2,709
15 16 b	Drilling line holes for underground rock excavation	drill	drill		7 lin ft	1			0.395		5	1,844
26 28 b	Core drilling NX holes in stage between the depths of: O and 50 feet		drill) lin ft	10			0.395			1,304
27 29 5	50 and 100 feet	drill	drill		3 lin ft	10			0.395			291
28 31 b	Drilling grout Holes in stage between depth of: O and 30 feet	drill	drill	43,25		2			0.395		91	35,879
29 32 b	30 and BO feet	drill	drill	32,37		2			0.395	0.240	65	25,577
30 33 b	60 and 1/O feet	drill	driff	16,899	9 lin ft	2	33,799	0.364	0.395	0.240	34	13,35
31 34 b	110 and 160 feet	drill	drill		3 lín ft	2	9,254	0.364	0.395			3,655
32 35 b	160 and 210 feet	drill	drill		5 lin ft	2	3,692	0.364	0.395			1,458
33 36 b	210 and 260 feet	drill	drill		7 lin ft	3	2,271		0.395			897
34 37 b	260 and 310 feet	drill	drill	25	5 lin ft	5	1,148		0.395			453
41 44 b	Drilling drainage holes in stage between the depths of: O and 25 feet	drisi	drill		5 lin ft	4	23,346		0.395			9,222
42 45 b	25 and 50 feet	drill	drill		7 lin ft	. 4	24,073		0.395		24	9,509
43 46 b	50 and 75 feet	drill	drill		t lin ft	4	17,536		0.395		18	6,92
44 47 b	75 and 100 feet	dril	drill		1 lin ft	4	12,878		0.395			5,087
45 48 b	IO0 and 150 feet	drill	drill		3 lin ft	4	10,812		0.395			4,27
46 49 b	150 and 200 feet	drill	drill		4 lin ft	5	370		0.395			14
47 50 b	Drilling holes for anchor bars and grouting bars in place	drill	drill	28,17		-1	33,804		0.395			13,35
76 79 b	Drilling 10-inch-diametsr cores in concrete	drill	drill	23	7 lin ft	20			0.395			1,877
263 (f) b	As an adjustment for the underrun in quantity under schedule item 16	drill	cirili		lump sum	15,108			0.395			5,96
299 (h) b	Dritting NX drain holes in left abutment of dam	drill	drill		5 lin ft	17			0.395			4,87
302 (a) b	Order for Changes No. 19 Drilling and grouting fan holes in stilling ba	drili	drill		lump sum	12,056			0.395			4,76
303 (b) b	Drilling and grouting horizontal holes in stilling basin	drili	drill	1	t iump sum	15,068	15,068	0.364	0.395	0.240	15	5,95

APPENDIX A Material Inputs to the Mor	row Point Dam 11 of 13
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count	line appndx	Pay item type	SIC	BEA	Volume	Unit	Unit Cost	Total Cost	% Labor	%Equip	% Profit	Adjusted Total	Truck
	304 (c) b	Drilling and grouting horizontal holes in penstock intake structu		drill	1	lump sum	40,169	40,169	9 0.364	0.395	0.240	40	15,86
	306 (b) b	As an adjustment for overrun quantity under schedule item 32		drifi	1	lump sum	22,185	22,18	5 0.364	0.395	0.240	22	
	307 (c) b	As an adjustment for overrun quantity under schedule item 33		drifi	1	lump sum	9,157	9,15	7 0.364	0.395	0.240	9	3,61
	308 (d) b	As an adjustment for overrun quantity under schedule item 36		drill	1	lump sum	313	31:	3 0.364	0.395	0.240	0	12
	309 (e) b	As an adjustment for overrun quantity under schedule item 37		drill	1	lump sum	-6				0.240		-
	311 (g) b	As an adjustment for overrun in quantity under schedule item		drilf	1	lump sum	5,454	5,45			0.240	5	2,15
	312 (h) b	As an adjustment for overrun in quantity under schedule item		drill	1	lump sum	8,093	8,09	3 0.364	0.395	0.240	8	3,19
	313 (i) b	As an adjustment for overrun in quantity under schedule ite		drili	1	lump sum	2,878		8 0.364	0.395	0.240	3	
	314 (a) b	Order for Changes No. 21 Drilling drain holes in powerplant a-		drill	1	lump sum	91,705	91,70	5 0.364	0.395	0.240	92	36,22
	316 (b) b	Performing additional drilling for rock anchors in powerplant ch	amber drill	drill	1	lump sum	1,285	1,28	5 0.364	0.395	0.240	1	50
	329 (o) b	Drilling and tapping power receptacle	drill	drill	1	lump sum	14	1	4 0.364	0.395	0.240	0	1
	337 (a) b	Order for Changes No. 24Performing corrective work on left s	ide tra drili	drili	1	lump sum	188			0.395	0.240	0	7
	381 20 c	Drilling holes for anchor bars and grouting bars in place	drili	drill	1,589	lin ft	2.5	3,97	3 0.364	0.395	0.240	4	1,56
	393 32 c	Drilling 3-inch-diameter holes in reinforced concrete	dritt	driti		lin ft	20				0.240		26
	717 (a) c	Order for Changes No1 : Drilling holes and injecting asphalt int	o left al drill	drill	100%	lump sum	\$67,640.57	67,64	1 0.364	0.395	0.240	68	26,71
	1 <u>2 b</u>	Removal of unstable rock from canyon walls	exc	exc	3,095		18	55,71			0.223		
	2 3 b	Excavation, common, in open cut rock dam, stilling basin, and a	veir exc	exc	135,155		1				0.223		58,92
	3 <u>4</u> b	Excavation, rock, in open cut for dam, stilling basin, and weir	exc	exc	22,675		30				0.223		296,58
	4 5 b	Excavation, common, in open cut for penstock intake structur	exc	exc	1,866		2				0.223		1,38
	5 <u>6</u> b	Excavation, rock, in open cut for penstock inisLB structure	exc	exc	19,185		4	76,74			0.223		33,45
	6 7 b	Excavation, all classes, in open cut far powerplant appurtensno		exc	144,419		3				0.223		173,15
	7 8 b	Excavation. all classes. for channel improvement	exc	exc	23,534		2				0.223	0	18,54
	9 10 b	Excavation, all classes, far access, cable, and ventilation tunne		exc	3,542		23				0.223		35,51
	10 11 b	Excavation, all classes, for drain tube tunnels	exc	exc	9,897	yd3	15	143,50	7 0.341	0.436	0.223	0	62,56
	11 12 b	Excavation, all classes for penstock funnels	exc	exc	9,183		29	266,30			0.223	0	116,11
	12 13 b	Excavation, all classes, for foundation tunnels	exc	exc	2,307	yd3	46	106,12	2 0.341	0.436	0.223	0	46,26
	13 14 b	Excavation, all classes, for powerplant, above elevation 6820		exc	7,135	i yd3	14	99,89			0.223	0	43,55
	14 15 b	Excavation. all classes. for powerplant, below elevation 6820	.00 exc	exc	35,825		17	623,43	8 0.341	0.436	0.223	0	
	160 166 b	Excavation, al classes, for roadway	exc	exc	242,171	yd3	3	726,51	3 0.341	0.436	0.223		316,76
	162 168 b	Excavation, common, for structures	exc	exc	3,179	yd3	2	6,35	8 0.341	0.436	0.223	0	2,77
	163 169 b	Excavation, rock, for structures	exc	exc	298	3 yd3	6		3 0.34	0.436	0.223	3 0	71
	181 a b	Order for Changes No 1 Diversion and care of river during of	onstruc exc	exc	1	lump sum	1,272,239	1,272,23	9 0.341	0.436	0.223	0	554,69
	184 d b	Excavating exploratory tunnels in dam abutments	exc	exc	510	yd3	108	55,17	7 0.34	0.436	0.223	0	24,05
	200 e b	Excavating, hauling, and placing impervious material in upstread	am coffe exc	exc	899	yd3	2	1,49	2 0.341	0.436	0.223	0	65
	202 g b	Excavating and removing materials required to be placed in c	offerdar exc	exc	1,796	3 yd3	2	2,91	2 0.341	0.436	0.223	0	1,27
	203 h b	excavating an additional 75 feet of grouting and drainage tur	nel in kexc	exc	178	3 yd3	83	14,77	4 0.341	0.436	0.223	0	6,44
	209 a b	Order for changes No 5 Excavating ventilation adit and shaf	t exc	exc	65	yd3	146	9,51	9 0.341	0.436	0.223	0	4,15
_	244 a b	Order for Changes No 9 Excavating the power plant drainage	tunnel exc	exc	1	lump sum	81,172	81,17	2 0.341	0.436	0.223	0	35,31
	248 c b	Performing rock excavation in left key way at elevation 7025	0 exc	exc	1	lump sum	3,662	3,66	2 0.341	0.436	0.223	0	1,59
	261 (d) b	Performing excavation for retaining wall between stations 5+		exc	1	lump sum	5,307	5,30	7 0.341	0.436	0.223	0	2,31
	262 (e) b	Performing additional excavation in downstream corners of po		exc	1	iump sum	1,145	1,14	5 0.341	0.436	0.223	0	49
	270 (g) b	Performing structure excavation for drop structure	exc	exc	5,189	yd3	1	3,37	2 0.341	0.436	0.223	0	1,47
	273 (j) b	Furnishing and placing riprap for drop structure	exc	exc	295	5 yd3	3	91	4 0.496	0.199	0.305	0	18
	274 (k) b	Performing river channel diversion for drop structure	exc	exc		lump sum	240	24	0 0.34	0.436	0.223	0	
	275 (o) b	Performing additional excavation in left abutment area of stilling	g basin exc	exc	1	lump sum	541	54	1 0.34	0.436	0.223	3 0	23
	277 (b) b	Removing part of cut-and-cover section of diversion tunnel	exc	exc		lump sum	6,786			0.436	0.223	3 0	2,9
	286 (d) b	Performing additional cuts in penstock intake structure gantry	crane r exc	exc		lump sum	105				0.223		4
	289 (g) b	As an adjustment for underrun in quantity under schedule item		exc		lump sum	3,731				0.223		1,6
	332 (a) b	Order for Changes No. 23 As an adjustment in compensation		exc		lump sum	1,886,888	1,886,88	8 0.341	0.436	0.223	3 0	822,6
	336 (e) b	For the cost increase in performing the penstock shaft excav		exc	1	lump sum	289,678	289,67		0.436	0.223	0	126,3
	362 1 0	Excavation, common for entrance and visitor facilities	exc	exc	2,046.90		\$3.65				0.223	0	3,2
	363 2 C	Excavation, rock, for entrance and visitor facilities	exc	exc	883.5		18.5			0.436	0.223	0	7,1
	364 3 c	Excavation, all classes for switchyard structures	exc	exc		5 yd3	5.6				0.223		
	365 4 c	Excavation from borrow for switchyard embankments	exc	exc		7 yd3	3			0.436	0.223	0	9
	369 8 c	Compacting switchyard embankments	exc	exc		5 yd3	3.5				0.305		7
	370 9 c	Removal of unstable rock from canyon walls	exc	exc) yd3	42			0.436	0.223	0	
	375 14 c	Furnishing and erecting rock deflector fence	exc	exc		3 lin ft	17	4,51	9 0.34	0.436	0.223	0	1,9
	628 251 c	Excavation common for substation structures	exc	exc	1019.4		\$4.00			0.436	0.223	0	1,7
	677 301 c	Excavation, common, for transmission line tov t	exc	exc		yd3	4.5				0.223		
·····	25 27 b	Mobilization and demobilization for drilling and grouting	tabor	labor		lump sum	18,100			1		18,100	
	113 116 b	Testing crane	labor	labor		lump sum	9,500			1		9,500	
	216/h b	mobilizing and demobilizing grouting equipment for grouting ca		labor		l lump sum	150			1 1		150	
·	232 g b	For shortening power plant chamber	labor	labor		lump sum	19,924			1		19,924	
	268 (e) b	Performing corrective work on Government-furnished 3.5- by		labor		l iump sum	405			1		405	
	269 (f) b	Performing additional sandblasting on Government furnished or 3- by		labor		l lump sum	126			1		126	
	271 (h) b	Erecting Government-furnished bin wall for drop structure	labor	labor	3,440		141	13.93				13.932	

APPENDIX A Material Inputs to the Morrow Point Dam 12 of 13

count	line ap	opndx	Pay tiem type	SIC	BEA	Volume	Unit	Unit Cost	Total Cost	% Labor	%Equip	% Profit	Adjusted Total Truck
	295 (d) b		Performing corrective work on ladders for spillway fixedwheel gates	labor	labor	1	lump sum	271	271				271
3	301 (j) b		Cutting bearing plates for hoists of 13.5- by 16.07-foot fixed-whee	labor	labor	1	lump sum	106	106				106
	305 a) b		Order for Changes No. 20 As an adjustment for overrun quantity un	labor	labor	1	lump sum	33,481	33,481				33,481
3	315 (a) b		Order for Changes No. 22 As an adjustment for aesthetic changes is	labor	labor	1 1	lump sum	1.207	1,207		1		1,207
3	325 (k) b		As an adjustment for closure of access to powerplant	labor	labor	1	lump sum	1.285	1.285				1,285
3	326 (I) b		Performing corrective wiring on control cabinets for the 13.5by 16.0	labor	labor	1	lump sum	225	225		1		225
	327 (m) b		Furnishing labor to aid Government personnel in photographing of light		labor	1	lump sum	9				+ · · · · · · · · · · · · · · · · · · ·	9
	335 (d) b		As an adjustment for increases in cost due to design changes in spilly		labor		lump sum	137,508	137,508				137,508
	338 (b) b		Furnishing labor and equipment to aid Government personnel during i		labor	1	lump sum	1,516	1.516	bi aanto noon ni namaa ana ana	+		1,516
	339 (c) b		Performing corrective work on seals for 15- by 16.83-foot fixed-whe		labor		lump sum	619	619	<u>}</u>	+	+	619
	340 (d) b		Performing corrective work on seals for 13.5- by 16.07-foot fixed-w		labor		Tump sum	1.021	1.021				1,021
	341 (e) b		Performing corrective work on guide pin plates for spillway gate hois		labor		lump sum	56	56	ļ	·+		56
	342 (f) b		Performing corrective work on defective eccentric pins for penstock		labor		lump sum	596	596		-+		596
	343 (g) b		Repairing hanger stud for outlet works landern gate hoist	labor	labor		lump sum	2,635	2,635				2.635
	346 (j) b		Repairing coupling between motor and pump for tandem outlet gate		labor				2,635			+	2,035 85
	347 (k) b	· · · · · · · · · · · · · · · · · · ·					lump sum	85					
· · · · ·			Pressure testing -Q-inch stainless steel tilling and vent lines for outle		labor		lump sum	59	59				59
			Repairing hanger stud and upper cylinder head of hoist for penstock f		labor		lump sum	1,325	1,325				1,325
	349 (m) b		Rotating lower cylinder head of both penstock fixed-wheel gate hoist		labor		lump sum	146	146				146
	354 (r) b		Thawing outlet works piezometer line	labor	labor	1	lump sum	492	492				492
	544 183 c		Making electrical connections of equipment installed by others	labor	labor		lump sum	6.000.00	6,000				6,000
	545 184 c		Making additions and revisions of wiring and devices on electrical equ		labor		hour	12.5	3,575				3,575
	546 185 c		Making panel cutouts for mounting equipment on station-service conti		labor		lin ft	3	257		; [·	257
	514 C. c		Furnishing pumping services	labor	labor		days	170	75,480				75,480
	368 292 c		Removing electrical equipment and materials in existing substation	labor	labor		lump sum	1.000.00	1,000				1,000
	589 313 c		Performing work required for removing three s t	labor	labor		lump sum	19.500.00	19,500		1		19,500
. e	392 316 c	94. U.S.	Installing materials for second and third spans t	labor	labor	0	lump sum	4.000.00	40,000				40,000
7	722 (e) c	÷	Clearing Morrow Point-Curecanti, 230-kliovolt t	labor	labor	100%	lump sum	1.593.64	1,594				1,594
7	723 (f) c		Cleaning and greasing cables on 250-ton overhead crane	labor	labor		tump sum	3,003.20	3,003		-		3,003
7	725 (h) c		Repairing 250-ton overhead crane	labor	labor		lump sum	122.51	123				123
	728 (a) c		aOrder for Changes No3: Increasing interrupting ratings of molded ca		labor		lump sum	\$1,926.25	1,926				1.926
	729 (b) c		As an adjustment for revising the water collection system for powers		labor		lump sum	1,000.00	1,000			· · · · · · · · · · · · · · · · · · ·	1.000
	730 (c) c		Furnishing labor to assist in transporting and handling test weights	labor	labor		lump sum	2,118,99	2,119				2,119
	733 (f) c		Modifying stress cones on 15 kilovolt potheads100%	labor	labor		lump sum	563.45	563		-		563
	734 (g) c			labor	labor		lump sum	21.16	21			-	21
	735 (h) c		Furnishing and installing additional flanges, modifying oil piping to gov		labor		lump sum	1.183.64	1,184				1,184
	736 (i) c		Reversing doors on governor actuator cabinets	labor.	labor		lump sum	117.63	118	· · · · · · · · · · · · · · · · · · ·			118
	737 (i) c		Repairing damage to paint on governor actuator tanks	labor	labor		lump sum	635	635				635
	739 (I) c		Repairing cribbing over steel supports in cable tunnel	labor	labor		lumo sum	273.91	274				274
	740 (m) c			labor	labor				68				68
			Modifying caulking ring for a-line tunnel drain	And and the second			lump sum	67.58	140				140
			Government in inspection of shipping damage to high-voltage bushing		labor		lump sum	140.19					130
			Assisting Government in testing 13.8-kilovolt 3/c No.1 underground		labor		lump sum	130.33	130				
	745 (r) c		Repairing coupling and checking alinement on motor- generators for :		labor		lump sum	464.32	464			·	464
	746 (a) c		Order for Changes No4: Repairing damaged concrete around handra		labor		lump sum	\$2,844.40	2,844			· · · · · · · · · · · · · · · · · · ·	2,844
	747 (b) c		As an adjustment for performing groove-weld tests in lieu of fillet-we		labor		lump sum	353.22	353				353
	748 (c) c		Modifying support for check valve on water supply piping	labor	labor		lump sum	210	210				210
	751 (1) c			labor	labor		lump sum	2,808.92	2,809		1	. 	2,809
	754 (а) с		Order for Changes No5: Cleaning turbine grease pumps	labor	labor		lump sum	73.93	74				74
	755(b) c		Installing additional equipment X mounting pads	labor	labor		lump sum	439.78	440			i	440
	758 (e) c		Replacing two one-quarter bends in sewer line for visitor facilities with		labor		lump sum	219.9	220		1		220
	759 (f) c		Removing a buried reinforced concrete pad and foundation from high	labor	labor		lump sum	1.259.19	1,259				1,259
	764 (k) c		Removing broken strands from posttensioned tendon No.5100%	labor	labor	100%	lump sum	420.8	421		1	1	421
7	769 (d) c		Cleaning and unplugging floor drain in powerplant pump room	labor	labor	100%	lump sum	2.450.19	2,450		1	1	2,450
	770 (e) c		Modifying 12-inch turbine vent piping 100%	labor	labor		lump sum	773.95	774	1	1		774
	771 (f) c		Removing and cleaning form material in keyways and blockouts100%		labor		lump sum	255.43	255		· · · ·		255
	774 (i) c		Removing and cleaning up debris under unit 2 penstock100%	labor	labor		lump sum	219.25	219		1		219
	775 (i) c		Repairing a damaged and embedded piezometer coupling in unit 1 pe		labor		iump sum	57.95	58	T	1	1	58
	776 (k) c		Repairing damaged areas of paint on unit 1 penstock100%	labor	labor		lump sum	369.59	370				370
	777 (I) c		Revising stops on 250-ton traveling crane	labor	labor		lump sum	168.9	169			1	169
	786 (b) c		Disassembling, cleaning and reassembling 4-inch gate valve, and instr		labor		lump sum	170.36	170			1	170
	788 (d) c		Modifying support for transformer fire protection waterline	labor	labor		ump sum	55.71	56			·	56
	790 (t) c		Lowering weather doors onto spillways	labor	labor		6 lumo sum	268.08	268			1	268
	791 (g) c		Cleaning and removing debris from a-line drainage tunnel	labor	labor		lump sum	165.38	165				165
	794 (i) c		Cleaning and territoring debris from a line dramage turned Changing location of control valves on generator carbon dioxide syste		labor		lump sum	157.93	158			+	158
	794 (l) c	-	Unwatering spiral case	labor	labor		lump sum	92.54	93			·	93
		····							203				203
	796 (I) c	1.12. <u>1</u>	Resetting clearance on 375 cubic-foot-per minute air compressor and		labor		6 lump sum	202.66			· · · { · · · · · · · · · · · · · · · ·		36
	797 (m) c		Modifying 1.5-inch service air line	labor	labor	1009	lump sum	36.37	36	1	5		301

APPENDIX A Material Inputs to the Morrow Point Dam 13 of 13

799 (a) c 800 (P) c	wounying holes for ground cable in unit 1 switchgear100% labor	labor	100% Jump sum	10 49					
		1940r	10000		101	· · · · · · · · · · · · · · · · · · ·		10	
	Relocate mus on structure at station 1.1 7.1.1.4.	10Hor		110 001 .	116'7			1/8.7	
201/0/ 208	Erredeting and installing of birtht adopted an added of the	International In		47.00.14	001			100	
5	Furnishing and installing six neight adaptors on pedestal insulators it labor	labor	100% Rump sum	170.66	171		The second s	171	
	Helocating temperature relay for 65-cubic-foot-per-minute compress labor	labor	100% hump sum	15.64	16			18	
804 (a) c	ng a section of 8-inch turbine pit drai	labor	1.00% hump sum	\$62.98	63			63	
	Repositioning power transformer	labor	100% lump sum	111.1	111			111	
806 (c) c	Cleaning concrete from handrali blockouts100%	labor	100% lump sum	239.21	239			239	
807 (d) c	Repairing overhead rolling door	labor	100% lump sum	3,521.68	3,522			3.522	
809 (f) c	Assisting Government in moving electrical test equipment	labor	100% lump sum	75.89	76		and the second s	76	
810 (g) c	Leveling and turning flanges on turbine and draft tube vent piping labor	labor	100% htmp sum	183.72	184			184	
822 (a) c	Order for Changes No9: Repairing and cleaning hoist block, brakes, 6 labor	labor	100% lumo sum	\$271.22	271		The second	9711	
823 (b) c	÷	labor	100% lumn sum	272.57	273	and the most second to be a second		1979	
(c)		tahor	100% kmn sum	S 1 618 66	1 619			1 810	
826 (a)	hia tranch		+000/ hims anim		100	·		1700	-
-			1105 0110 2001	330.01	100	· · · · · · · · · · · · · · · · · · ·		100	
	HILL BALLAS	labor	uns duna %001	220.21	250			250	
0 (g) c	Cleaning out drains in dam and powerplant	labor	100% Jump sum	594.38	594			594	
830 (i) c	Inspecting and testing spare cooler for A-phase transformer labor	labor	100% lump sum	557.84	558	-		558	
831 (j) c	Repairing, bushing, and chipping first-stage concrete	labor	100% Jump sum	187.04	187			187	
832 (k) c	Modifying and repairing miscellaneous metal work	labor	100% tump sum	752.03	752		A MARK A REPORT OF	752	
835 (n) c	Assisting Government with inspection of stilling basin labor	labor	100% iumo sum	509.76	510			510	
837 (P) IC	Installing temporary controls in outlet date control cabinet	labor		173.84	174	the same of the same sector with the same sector same	 and the set of second se	174	
		lahor	100% Jumo and	A 225 10	A 225			100 K	
R401(c)		Inhor			1900			0001	
	The second s	1001	ums dunt of 100	2.022	087			9 AN	
841 (T) C		labor		404.4	404		and the second se	404	
(X)	Pressure testing embedded gravity drainage, unwatering and vent pipi labor	labor	100% lump sum	3.993.91	3,994			3,994	
126 129 b		1	1 hump sum	20,000	20,000			20,000	
172 178 b	Dismantling and storing county bridges #3 and 4 storage		1 hump sum	19,400	19,400		-	19,400	
242.g b	area the obsolete fre		1 fump sum	16	16			16	
356 b	12-31-65)	1			5.614		and a second sec	5.614	
357 b	ĺ	13X	and the second second framework and the second		006			006	
358	10.01.001	2 A F4			211 a				
	100-10	101 T						114:0	
		1			3,440			3,240	
191	and the second	4	309 M gal	N	650			650	
7		water	3.62 M gal	en	10,860			10,860	
360 b	Payment for increase in forming galleries, addits, shafts, and chambers within mass concrete of	n mass concrete of	8,332 /1	0	15,415			15,415	
361 b					-5,427		-	-5,427	
	Installing hydraulic board CCB		100% tump sum	1.800.00	1,800	0.297208267	0.217912791	873	
188 c	Installing unit gauge boards H1A and H2A		100% lump sum	1.600.00	1.600	0.297208267	0.217912791	776	1.
580 219 C	Fumishing and installing necessal insulators, technical reference No. 415		15 each	100	1 500	0.297208267	0.917019701	and the second se	
6	Firmithing and installing states of loader average and loader activities		1000/ 1000	00 000					
2 - L			uns duna con i	4.600.00	4,800	0.23/208261	18/218/12.0	7	
u,	Purnishing and installing mechanically held contactor in cable gallery and cable tunnel	le tunnel	1 each	2101	210	0.297208267	0.217912791		
647 271 c	Furnishing and installing all materials for grounding system additions		797 lb	e	2,391	0.297208267	0.217912791	1,159	
661 285 c	Installing 230-kilovolt 3-pole, manualty gang-operated air switch with 3-pole manualty gang-ope	manually gang-ope	0	0	Q	0.297208267	0.217912791	0	
779 (n) c	Reduction in contract price because motors fumished under schedule items 52 and 53 did not	52 and 53 did not	100% fumo sum	-55	-55	0.297208267	0.217912791	-27	
803 (s) c	As an adjustment under the contract for additional costs incurred by reason of interference by	n of interference bu	10.0% home sum	\$2 877 15	L	0 2072/8267	N 917010701	1 305	
	As an antifactor adjustment for increased roots of installing accurate of the		1000t	· 0		Cacaoo 200 0		22.	
				2000.	200	0.237200201	1718/17	00-	
		ind Lining isolated-	uns dumi % nnt	00.856,61	10,538	0.29/20826/	18/218/12/0	1,534	
	Order for Changes No10: For increased costs caused by disruptions and delays due to Gove	lelays due to Gover	100% fump sum	\$141.043.07	141,043		and the second se	141,043	
	For increases in cost due to increases in 1971 wage scales		100% lump sum	29,991.07	29,991			29,991	
847 (c) c	For increases in cost in completion of part 6 due to disruption caused by faulty adhesive spec	aulty adhesive speci	100% Jump sum	\$16.771.90	16.772			16.772	
848 (a) c	Order for Changes No.11: As an adjustment for increased overhead and profit for work under O	fit for work under O	100% lumo sum	1.671.61	1.672			1.672	
	As an adjustment for navment of the remaining portion of the isolated chase hits work for who	a hus work for which	100% himo sum	27 ANG 08	27 000			01.000	
1	As an optimized for increased supervised and and and the unit index Order to	- Choose No 0.01	1000/ human	00 000 0	200.0			600'17	
	2	r Crianges No.9 (UI		2,022.29	2,022			2,022	
6	As an adjustment for a portion of the increased costs of removing mineral depos	deposits	100% fump sum	10,000.00	10,000			10,000	
852 (e) C	For furnishing one additional spare pothead		100% kimp sum	6,849.38	6,849			6,849	a supervise in the
853 C				Subtotal	11,509,561		o	11,509,561	
854 c	Plus				7.002			7.002	
155	ractor operation of crane for Government in accord	2 12			307 7			1907 1	
000	Lourractor operation of crarie for Government in accordance with paragraph 53	n 53	and the second se		1,120			10711	
855	Total For Completion Contract		the second		0 447 070				107 002 6

APPENDIX B	Federal Energy	Regulatory	Commission Database	1 OF5
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	MAX_STOR STAT		HAZARD	AVER	YEAR_COMP	NID_HEIGHT				DAM_HEIGHT	estimated width	MAX_DISCH	DAM_TYPE	NORM_STOR	SURF_AREA	DRAIN_A
2441	453 CT	GREENVILLE	LOW	SHETUCKET RIVER	1888	15	453	65,630	410	15	10.671625	66935	TC	373	80	<u> </u>
2576	3120 CT	BULLS BRIDGE	SIGNIFICANT	HOUSATONIC RIVER	1902	22	3120	49,059	203	22	10.98505	45000	ONPG	1800	120	
2576	3120 CT	SPOONER	SIGNIFICANT	HOUSATONIC RIVER	1902	20	3120	33,994	156	20	10.8955	45000	ERCN	1800	120	
2576	3120 CT	BULLS BRIDGE CANAL SP	SIGNIFICANT	HOUSATONIC RIVER	1902	22	3120	49,059	203	22	10.98505	2000	FG	1800	120	,
2576	3120 CT	BULLS BRIDGE MOUNTAIN	SIGNIFICANT	HOUSATONIC RIVER	1902		3120	49,059		22			PGMS	1800		
2576	218650 CT	ROCKY RIVER CANAL DIKE	HIGH	ROCKY RIVER	1902	20	218650	10,896	······································	20			Æ	172000		
2576	3120 CT	BULLS BRIDGE FOREBAY	SIGNIFICANT	HOUSATONIC RIVER	1903	39	3120	121,397	265	39		i a ser a		1800	wij	
2576	37200 CT	STEVENSON	HIGH	HOUSATONIC RIVER	1919	· · · · · · · · · · · · · · · · · · ·	37200	1.423.069	· · · · · · · · · · · · · · · · · · ·	83		· · · · · · · · · · · · · · · · · · ·		26900	4	
2576	218650 CT	ROCKY RIVER MAIN DAM	HIGH	ROCKY RIVER	1929		218650	1,378,258	de contracto de la maistre de la contracto de la c	100			FE.	172000		
2576	218650 CT	NORTH LANESVILLE DIKE		ROCKY RIVER	1929	7	218650	13,067		7	and the second s		CNPG			
2576	218650 CT	MIDDLE LANESVILLE DIKE	· · · · · · · · · · · · · · · · · · ·	ROCKY RIVER	1929	45	218650					and a second	RE	172000		
2576	218650 CT	SOUTH LANESVILLE DIKE		A R - Mathematica contract of the second sec	1929			90,292	167	45	species and the second se			172000		
2576	a second and the second s	and the second s		ROCKY RIVER		17	218650	71,530			free of the second descent		CNPG	172000		
	218650 CT	DANBURY DIKE NO. 1	HIGH	ROCKY RIVER	1929	42		435,612		42	the second secon		PE	172000	- Provide a second s	
2576	86100 CT	SHEPAUG	HIGH	HOUSATONIC RIVER	1955	140	86100		· · · · · · · · · · · · · · · · · · ·	140	and the second	· · · · · · · · · · · · · · · · · · ·		74000	· • • • • • • • • • • • • • • • • • • •	
2576	218650 CT	DANBURY DIKE NO. 2	HIGH	HOUSATONIC RIVER	1989	7	218650	9,385	· · · · · · · · · · · · · · · · · · ·	7	and a deal of the second dependence of	· · · · · · · · · · · · · · · · · · ·	Æ	172000		·
2597	3100 CT	FALLS VILLAGE	SIGNIFICANT	HOUSATONIC RIVER	1913	16	3100	54,868	320	16	10.7164	38000	CNPG	1135	5 100	4
2662	2000 CT	SCOTLAND	HGH	SHETUCKET RIVER	1909	37	2000	207,454	481	37	11.656675	60000	CBONPG	1300	134	
3472	3480 CT	WYRE - WYND	LOW	OUINEBAUG RIVER	1913	14	3480	71,859	483	14	10.62685	46000	MSCNPG	2900	246	1
5062	340 CT	QUINEBAUG	LOW	QUINEBAUG RIVER	1855	14	340	37,194	250	14	10.62685	3640	MSPG	283	8 85	d i
5062	312 CT	FIVE MILE POND	SIGNIFICANT	FIVE MILE RIVER	1855	17	312	26,526	145	17	10.761175	5283	MSPG	260	65	,
6066	4400 CT	LAKE HOUSATONIC	HIGH	HOUSATONIC RIVER	1870	25	4400	236,287	850	25	11,119375	160000	MSCNPG	4020	320	,
6066	4400 CT	DERBY DIKE	LOW	HOUSATONIC RIVER	1870	10	4400	41,791	· · · · · · · · · · · · · · · · · · ·	10			Æ	4020		
5066	4400 CT	DERBY CANAL WEIR	LOW	HOUSATONIC RIVER	1870	f	4400			10			CNPG	4020		
6066	4400 CT	SHELTON CANAL DIKE	LOW	HOUSATONIC RIVER	1870		4400		designed and the second s	25		· · · · · · · · · · · · · · · · · · ·		4020		1
1143	258 CT	BRUNSWICK	LOW	MOOSUPRIVER	1891	19	258	32,986		19				215	mile a construction construction	
1168	110 CT	DAYVILLE DIKE	LOW				110			19				93		
1168				FIVE MILE RIVER	1925	14		297,552					Æ	· · · · · · · · · · · · · · · · · · ·		
	110 CT	DAYVILLE EMERGENCY SF		FIVE MILE RIVER	1925		110			8	and a second sec		MSCN	93		
1168	110 CT	DAYVILLE WASTEWAY	LOW	FIVE MILE RIVER	1925		110	3,868		14	and the second sec	······································	STMS	93	-j	
1547	СТ	HALE	LOW	QUINEBAUG RIVER	1965	23	65			23			OTCNPG	65		- y
1889	28000 MA	TURNERS FALLS DIKE	LOW	CONNECTICUT CANAL		10		52,239	· · · · · · · · · · · · · · · · · · ·	10	and a set of a set of a difference second set of the	· • • • • • • • • • • • • • • • • • • •	Area and a second second second	16600	· · · · · · · · · · · · · · · · · · ·	
1889	28000 MA	MONTAGUE	SIGNIFICANT	CONNECTICUT RIVER	1915		28000	499,033	630	62	12.77605	280000	ONPG	16600	2000	4
1889	28000 MA	CABOT SPILLWAY	LOW	CONNECTICUT CANAL	1915	35	28000	68,015		35	11.567125			16600	2000	<u>4</u>
1889	28000 MA	CABOT STATION	LOW	CONNECTICUT CANAL	1916	35	28000	95,140	235	35	11.567125	5	PGMS	16600	2000	/
1889	28000 MA	GILL	SIGNIFICANT	CONNECTICUT RIVER	1970	70	28000	453,263	493	70	13.13425	280000	CNPG	16600	2000	1
2004	68900 MA	OVERFLOW NO. 1	LOW	CONNECTICUT RIVER	1850	30	68900	283,808	834	30	11.34325	3364	MSPGPE	26000	2550	1
2004	68900 MA	OVERFLOW NO. 2	LOW	HOLYOKE CANAL	1860		68900	21,791	100	20		the second second second second	MSPG	26000	in the second seco	
2004	68900 MA	OVERFLOW NO. 3	LOW	HOLYOKE CANAL	1860	18	68900	20,812		18				26000		
2004	68900 MA	OVERFLOW NO. 4	LOW	HOLYOKE CANAL	1891	26	68900	43,540	ing a second second second second	26			MSPG	26000		
2004	68900 MA	HOLYOKE DAM	HIGH	CONNECTICUT RIVER	1900		68900	347,103		30				26000		
2004	68900 MA	CANAL GATE HOUSE	SIGNIFICANT	CONNECTICUT RIVER	1900	· · · · · · · · · · · · · · · · · · ·	68900	75,245	the second se	36			MS	26000		
2323	818 MA	DEERFIELD NO. 5 - CAN		DEERFIELD RIVER	1910		818		deferred to the second	39			Æ	248		
2323	B18 MA				4 · · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·				have a summer and service where	and the second s		Æ	248		
		DEERFIELD NO. 5 - CANA		DEERFIELD RIVER	1910		818	and the same state to be a set of the set of		33			Æ			
2323	818 MA	DEERFIELD NO. 5 - CANA		DEERFIELD RIVER	1910	······································				16				248		
2323	551 MA	DEERFIELD NO. 3	LOW	DEERFIELD RIVER	1912		551	109,129	and the second second	21	and a second state of the Party State Street and the second state of			221	where we want ware a	
2323	551 MA	DEERFIELD NO. 3 - FOREE		DEERFIELD RIVER	1912		551	253,686	al an anna an anna an an an an an an an an	23			Æ	221	and a second car an encourage of	A ALL A LABORATION A
2323	1067 MA	DEERFIELD NO. 4	LOW	DEERFIELD RIVER	1912	A	1067	297,412	· · · · · · · · · · · · · · · · · · ·	48		* * * * * * * * * * * * * * * * * * *	CNPGRE	467	· · · · · · · · · · · · · · · · · · ·	
2323	1067 MA	DEERFIELD NO. 4 - FOREE	V LOW	DEERFIELD RIVER	1912		1067	137,283		20	10.8955	······································	Æ	467		
2323	589 MA	DEERFIELD NO. 2	SIGNIFICANT	DEERFIELD RIVER	1913	76	589	455,323	447	76	13.4029	31200	ONPG	350	63	1
2323	5480 MA	SHERMAN	HIGH	DEERFIELD RIVER	1927	110	5480	1,669,688	1017	110	14.92525	87000	RECNIPG	3593	3 218	1
2323	818 MA	DEERFIELD NO. 5	LOW	DEERFIELD RIVER	1992	43				43	11.925325	and the second sec	and the state with the state of the state	248	3 38	
2323	818 MA	DEERFIELD NO. 5 - DUNB		DUNBAR BROOK	1993		818	52,425		29				248		
2334	510 MA	GARDNERS FALLS	LOW	DEERFIELD RIVER	1904	37	510	and a second a second second second	And the second second second	37				50		
2485		the second s			down web			(m	· · · · · · · · · · · · · · · · · · ·	144		······································	EFFE	17240		
<403	21500 MA	NORTHFIELD MOUNTAIN	HIGH	CONNECTICUT RIVER	1972	1 144	21500	26,526,689	1200	144	10.4470	·	- FE	11240	210	Anna war

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APPENDIX B Federal Energy Regulatory Commission Database 20F5

	AX_STOR STATE		HAZARD	RIVER		NID_HEIGHT		the set of		DAM_HEIGHT	estimated width N	AAX_DISCH		NORM_STOR S		RAIN ARE
2485	21500 MA	NORTHFIELD MT UPPER	HIGH	CONNECTICUT RIVER	1973	20	21500	107,430	493	20	10.8955		ONPG	17240	278	
2608	200 MA	WEST SPRINGFIELD	LOW	WESTFIELD RIVER	1840	18	200	106,979	550	18	10.80595	4800	TCCN	200	20	5
2631	2565 MA	WORONOCO	LOW	WESTFIELD RIVER	1938	53	2565	967,265	1475	53	12.373075	210000	CNPGRE	1830	46	3
2669	6800 MA	BEAR SWAMP - NORTH DIK	LOW	DEERFIELD RIVER	1974	155	6800	3,602,487	1372	155	16.940125	9900	EFFE	5100	118	
2669	6800 MA	BEAR SWAMP - DIKE 'A'	LOW	DEERFIELD RIVER	1974	23	6800	89,297	352	23	11.029825		EFFE	5100	118	
2669	6800 MA	BEAR SWAMP - EAST DIKE	HIGH	DEERFIELD RIVER	1974	50	6800	482,819	789	50	12.23875		EFFE	5100	118	
2669	6800 MA	BEAR SWAMP - SOUTH DIK	HIGH	DEERFIELD RIVER	1974	140	6800	6,292,981	2763	140	16.2685		ETTE	5100	118	
2669	7580 MA	FIFE BROOK	High	DEERFIELD RIVER	1974	130	7580	the same the same state of the same state	900	130	15.82075	84200	EPPEPG	5300	152	2
2800	19900 MA	GREAT STONE	LOW	MERRIMACK RIVER	1848	39	19900	431,991	943	39		124600	MSPG	18000	655	44
2801	570 MA	GLENDALE	LOW	HOUSATONIC RIVER	1906	26	570	52,248	180	26		9000	FG	87	40	2
2985	50 MA	WILLOW MILL	SIGNIFICANT		1872	12	50	22,761	180	12			MSPG	50	13	24
3127	145 MA	WARE LOWER	LOW	WARE RIVER	1890	18	145	22,563	116	18		· · · · · · · · · · · · · · · · · · ·	MSPG	90	10	11
8093	210 MA	METHUEN FALLS	HIGH	SPICKETT RIVER	1895	23	210	47,693	188	23			MSPG	210	30	
9100	173 MA	RIVERDALE MILLS	LOW	BLACKSTONE RIVER	1957	10	173	15,881	152	1(ing the second s		ONPG	89	12	14
2142	108000 ME	HARRIS	HIGH	KENNEBEC RIVER	1955	165	108000		2015	165			ONPORE	72250	3666	13
2194	2000 ME	BARMILLS	LOW	SACO RIVER	1956	25	2000	111.194	400	21		16320		600	263	15
2283	2280 ME	DEERRIPS	LOW	ANDROSCOGGIN RIVEF	1903	54	2280	629,660	939	54	· · · · · · · · · · · · · · · · · · ·		CNPG	1200	130	280
2283	56100 ME	GULFISLAND	HIGH	ANDROSCOGGIN RIVEF		99	56100			99			CNPGRE	55100	2862	28
2284	2000 ME	BRUNSWICK	LOW	ANDROSCOGGIN RIVER	1920	42	2000	3,554,953 301,885	2400	42		20000		251	300	34
2302	2800 ME	the second secon	LOW	· · · · · · · · · · · · · · · · · · ·		42	2800		71				MSPG	1600	200	29
		BATES WEIR		LEWISTON CROSS CA		f · - · · · · · · · · · · · · · · · · ·		10,563	· · · · · · · · · · · · · · · · · · ·							
2302	2800 ME	RED SHOP WEIR	LOW	LEWISTON CROSS CA	1859	18	2800	11,670		1			MSPG	1600	200	29
2302	2800 ME	GULLY BROOK LOWER	LOW	LEWISTON CANAL - GU	1859	9	2800	8,426	90		······································		MSONPG	1600	200	29
2302	2800 ME	ANDROSCOGGIN WEIR	LOW	LEWISTON CANAL - GL	1859		2800	2,996	32	9	discussion and the second second		MSONPG	1600	200	29
2302	2800 ME	GREAT STONE	HIGH	ANDROSCOGGIN RIVER		27	2800	289,022	955	27	· · · · · · · · · · · · · · · · · · ·		MSCNPG	1600	200	296
2302	2800 ME	CONTINENTAL WEIR	LOW	LEWISTON CROSS CA		14	2800	4,463	30	1,4		···· ··· ··· ··· ······ ······	MSPG	1600	200	29
2312	2244 ME	GREAT WORKS	LOW	PENOBSCOT RIVER	1914	20	2244	236,650	1086	20			TOERPG	1600	160	66
2322	5100 ME	SHAWMUT	LOW	KENNEBEC RIVER	1912	40	5100	698,027	1480	40	p		ONPG	5000	1310	42
2325	22300 ME	WESTON NORTH CHANNEL		KENNEBEC RIVER	1921	38	22300	235,223	529	38	man our come and the works of the same in the		CNPGOB	18600	930	38
2325	22300 ME	WESTON SOUTH CHANNEL	LOW	KENNEBEC RIVER	1921	51	22300	245,572	392	5 1			CNPGCB	18600	930	38
2329	255000 ME	WYMAN	High	KENNEBEC RIVER	1930	155	255000	8,018,947	3054	158	16.940125	59630	RECNPG	208910	3240	26
2333	183 ME	RUMFORD FALLS MIDDLE	LOW	ANDROSCOGGIN RIVEF	1892	20	183	93,265	428	2(10.8955	132500	TCER	141	21	20
2333	3110 ME	RUMFORD FALLS UPPER D	SIGNIFICANT	ANDROSCOGGIN RIVEF	1918	40	3110	247,139	524	4(11.791	121900	CNPG	2900	419	200
2335	6700 ME	WILLIAMS	LOW	KENNEBEC RIVER	1939	45	6700	367,655	680	45	12.014875	48790	RECNPG	4575	446	27
2364	425 ME	ABENAKI	LOW	KENNEBEC RIVER	1922	25	425	277,984	1000	25	11.119375	126000	CNPG	350	24	31-
2365	14500 ME	ANSON	LOW	KENNEBEC RIVER	1923	38	14500	380,180	855	31	11.70145	90000	ONPG	6000	650	314
2367	2025 ME	GARIBOU	LOW	AROOSTOOK RIVER	1889	24	2025	133,427	502	. 24	11.0746	63000	TCERCN	1821	162	194
2367	29033 ME	MILLINOCKET LAKE	LOW	MILLINOCKET STREAM	1943	11	29033	26,315	228	1	10.492525	2735	TCER	22900	2788	
2368	89215 ME	SQUA PAN	HIGH	SQUA PAN STREAM	1928	35	89215	236,837	585	31	11.567125	5300	CNCBRE	64000	5043	. (
2375	11560 ME	RILEY	LOW	ANDROSCOGGIN RIVER	1897	23	11560	202,949	800	23	11.029825	66000	TCER	3600	578	24
2375	782 ME	LIVERMORE FALLS	LOW	ANDROSCOGGIN RIVER	1908	12	782	106,595	843	12	10.5373	65000	CNPG	300	46	24
2375	2331 ME	JAY	LOW	ANDROSCOGGIN RIVEF	1912	17	2331	145,803	797	15	10.761175	55000	ONPG	1800	206	24
2389	25000 ME	EDWARDS	HIGH	KENNEBEC RIVER	1870	42	25000	520,938		42		87000		16985	1143	55
2403	4800 ME	VEAZIE	LOW	PENOBSOOT RIVER	1913	30	4800	286,530	842	30	and the second		CNPGCB	3500	390	78
2458	14520 ME	STONE DAM	HIGH	WEST BRANCH PENOB		27	14520	381,933	1262	2		and a second second	CNPGRE	8100	1344	18
2458	56290 ME	DOLBY	HIGH	WEST BRANCH PENOB		56	56290	977,078	1395	5(ONPORE	41956	2048	21
2458	2970 ME	EAST MILLINOCKET	LOW	WEST BRANCH PENOB		24	2970	192,166	1	24			CNPGRE	1950	128	21
2458	87670 ME	MILLINOCKET LAKE	HIGH	MILLINOCKET STREAM		20	87670	138,373		2(ONPORE	45370	8640	1
2458	392680 ME	NORTH TWIN	HIGH	WEST BRANCH PENOB		35	392680	425,497	1051	38			RECNPG	346000	17790	18
		The second		A CONTRACTOR OF A CONTRACTOR O						23			ONPGMS		98	4
2519	1663 ME	NORTH GORHAM	HIGH	PRESUMPSCOT RIVER	1901	23	1663	229,078						1300		
2520	69100 ME	MATTACEUNK	HIGH	PENOBSCOT RIVER	1939	a second a second as	69100	632,583	1170	4	a province and the second s		ONFORE	55785	1664	3
2527	33500 ME	SKELTON	HIGH	SACORIVER	1948	1	33500	1,698,152		7			ONPGRE	25250	488	1
2528	266 ME	WEST CHANNEL DAM	LOW	SACO RIVER	1895		266	56,583		10			MSPG	28	14	1
2528	2500 ME	SPRINGS	LOW	SACO RIVER	1925	12	2500	34,014		1	· · · · · · · · · · · · · · · · · · ·		CNPG	711	359	1
2528	2500 ME	BRADBURY	LOW	SACO RIVER	1929	12	2500	25,922	205	1.	10.5373	2060	CNPG	711	359	. 1

APPENDIX B	Federal Energy	Regulatory	Commission Database	3 OF5
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218.8 28.0 E. 99.0 EVEN 199.0	STOR	RİS	STATE	DAM_NAME	HAZARD	RIVER	YEAR_COMP	NID_HEIGHT	NID, STOR	est. volume	DAM_LENGTH	DAM_HEIGHT	estimated width	MAX_DISCH	DAM_TYPE	NORM_STOR	SURF_AREA	DRAIN_AREA
2550 54-00 K 101 10.880/05 112 10.880/05 11200 0PACT 2320 337 2530	266	66 N	VE.	CATARACT	LOW	SACO RIVER	1938	49	266	98,588	165	49	12.193975	5626	ONPG	28	. 14	170
2501 2501M 199M 000 900 PHOT 197 90 2520 11200 432 300 11.3428 14300 PHYE 1200 1330 2531 15300 MM MUTOD C/M PRABADOT MARE 1990 34 13300 64.0 14 1.0 3285 41300 PHYE 13300 64.0 1.0 3285 1.1 3285 3285 1.1 3285 3285 1.1 3285 3285 1.1 3285 3285 3285 1.1 3285 3285 3285 3285	5440	40 N	ME	BONNY EAGLE	SIGNIFICANT	SACO RIVER	1911	67	5440	682,860	784	67	12.999925		ONPORE	2320	347	156
B330 13200 ME WSPR DATONI DW PACKAGOTYPER 1907 320 13200 218.41 4400 453.4 13300 11.34226 7228.6 12300 127.2 918 2834 13300 ME BLAMANT FALLS DW STUDENT FALLS 1000 81 532.0 13300 353.0 143.447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 142.3447 453.0 143.340 143.340 143.340 143.340 143.340 143.3447 453.0 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143.340 143	5440	40 N	ME	NEW RIVER CHANNEL DAN	SIGNIFICANT	SACO RIVER	1911	13	5440	48,148	350	13	10.582075	17000	CNPGOT	2320	347	156
2824 13300 ME MAX PPCMED07111011 1996 14 13300 448 11.62258 1728 9176 9177 9176 </td <td>2530</td> <td>30 N</td> <td>ME</td> <td>HIRAM</td> <td>LOW</td> <td>SACO RIVER</td> <td>1917</td> <td>30</td> <td>2530</td> <td>147,009</td> <td>432</td> <td>30</td> <td>11.34325</td> <td>16475</td> <td>CNPG</td> <td>1000</td> <td>255</td> <td>83</td>	2530	30 N	ME	HIRAM	LOW	SACO RIVER	1917	30	2530	147,009	432	30	11.34325	16475	CNPG	1000	255	83
255/ 13300.ME DUMAN FALLS LOW STUDATION FIRE 1996 9 3300 35.81 475 6 11.2847.57 4910 4917 918 255/ 55.00 MC FORT MARKS LOW MSRAMDROCK FRET 1924 39 14.40 30.81 14.772 29 11.47157 1910 0473 8000 460 87 14.3164 34.8 36 11.4119 34.440 MRSU ADSECT 8000 66 85 2550 1500 ME MSRU ADSECT 1910 88 160 55.311 21.00 29 10.09233 64.64 07007 67 35.8007 29.800 10.09233 64.64 10.09233 64.64 10.09233 64.64 10.09233 64.64 10.09233 64.64 10.09233 64.000768 71.00000 22.00 22.00 22.00 14.01083 60.00 10.09233 60.00 64.51 10.09253 60.00 67.00 28.00 10.021085 10.021085 10.000	13200	00 N	ME	WEST BUXTON	LOW	SACO RIVER	1907	30	13200	218,811	643	30	11.34325	4930	ONPORE	12300	131	157:
2824 13300 ME GUAMPERAL UDW OFFLUMTER NUMBER 1900 6 13320 33.81 475 6 10.288/27 65000 CMR 9000 417 2555 1540 INE LORMING LORM MBRAUCASKE ETT 1924 33 1440 30.680 41 23 11.47757 5100 CMR 6000 43 2555 1750 INE LARMING LOW MBRAUCASKE ETT 193.8 81 1600 55.4 11.07757 1910 600 600 85 2559 1130 INE MBRAUCASKE ETT 193.8 1910 24.85 160 56.41 20.04 67.00 67.0 67.0 67.0 67.0 67.0 67.0 67.0 67.0 67.0 67.0 77.0000 77.0<	13300	00 N	ME	MILFORD	LOW	PENOBSCOT RIVER	1906	34	13300	548,464	1400	34	11.52235	70265	CNPG	9175	918	530
2659 4500 ME COTT HULPAX. LOW. STRANDOOCHWEEL 1908 es 5520 154.841 473 28 112.84773 4500 4500 4500 450 2555 140.94 MISALARKEE ETFE 1924 33 1404 30.840 430 28 11.1.8477573 4400 4500 657 2555 110 ME MARALARKEE ETFE 1920 14 110 17.1.0700 153 14 10.028265 4400 0469 350 153 110.082 10.028625 4400 0476 50 10 4500 1000 350 2500 17500 ME MERALARKEE 1500 1530 1530 104 104 10.0455 12.04077 12.000 12.04075 10.000 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 11.250 <td< td=""><td>13300</td><td>00 N</td><td>ME</td><td>GILMAN FALLS</td><td>LOW</td><td></td><td></td><td></td><td>13300</td><td></td><td></td><td>8</td><td></td><td></td><td>ONFG</td><td></td><td></td><td></td></td<>	13300	00 N	ME	GILMAN FALLS	LOW				13300			8			ONFG			
2555 1440 1640 30 1440 30 14477573 1910 OPC 990 68 2556 7500 HSDNORKESTEF 1938 421 325 11.0119 2400 670 600 251 2557 1500 HE NERSALDRESETEF 1938 23 11.022825 446 GRVEE 10.00 87 2559 11.04E NALADE MESALDRESETEF 1938 11.0119 710.01 11.0119 710.00 2300 0470 11.0000 3800 2517 970.01 HE NALADE 11.0119 710.000 720.042 710.0420 710.0420 710.0	5500	00 N	ME	FORT HALIFAX	LOW	SEBASTICOOK RIVER			5500	and a summer summer.	473	29	······································		CNOBPG	5000		
2550 TSO LE UNX (MOX (AS) UNX INSOLUCENES STREE [104] 56 TSO [150,366] 442 36 11,119 2460 MSO 630 750 150,316 320 231 120,2263 110,				AUTOMATIC	LOW	A service of the serv												
2557 1500 NE Interies SKMMCART VISSALLANGE STIE 1900 23 1500 NE 5511 2200 23 11000 87 2559 111 NE CA MESSALLANGE STIE 1912 1119000 2248 168 13 10.588075 2400 CPC 500 0PC 500 0PC 500 3900 257 577000 FC000 FC000 7700.427 770000 770.442 710.9800 22000 170.9800 2200 10.9850 22000 170.9800 2200 10.9850 22000 170.9800 2200 170.9800 2200 10.9850 22000 170.980 2200 170.9800 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 2200 170.980 22000 170.980	750	50 N	ME	UNION GAS	LOW		·······		750	the same sign a second management		36			MSPG	600		
2856 119.ML OARLAND LOW MESSALDARGE KIE 1991 14 110 115 14 10.62655 2200.049 50 10 2825 118300 MESSALDARELIKE MESSALDARGE KIE MESSALDARGE KIE 1114 11000 22.230 10 22.270 23.2850 113.2857.5 22800, CPGE 112.000 22.270 22.270 23.2850 13.2857.5 22800, CPGE 112.250 112.251 112.250	1500	00 N	ME	and the second	SIGNIFICANT					a second s				· · · · · · · · · · · · · · · · · · ·	the statistic to the second	1000		A COLORADOR
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8272 9270001/KE 9PC0644.5 1954 VEST 1929 720,942 725 725 728 12.98575 12.9001/KE 710,000 22270 8276 11.921 KLUCKWOOD UW REPRESEMENT 1919 20 1830 196,949 20 10.955 122000 1722,0 11225							the second s				4	13	the second					· · · · · · · · · · · · · · · · · · ·
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2200 17300 ME RUM APQ/MD UOW MERPILL BROCK 1884 15 1700 32.015 200 15 10.027162 20200 FT 11250 11250 2500 17000 ME MESTERIED LOW PAXSOCTPME 1989 40 6150 400.844 650 400 11.719 677000 0049 3980 250 2815 275000 ME BAXSOL MEH MODE ENVER 1983 60 1550 ME 10.52275 5450 TCRE 556190 23825 2844 2874 ME CAMADE ALLE DOW WEST BAXCH FENDE 1921 50 2740 475,80 764 50 12.2887 5450 TCRE 55810 724 50 12.2887 30980 DE 7780 743 4750 RFAR 7780 4031 14.3425 6580 TEXP 23218 52818 5728 5430 TCRE 5590 CPA 1280 ME 5490 CPA 1590 C				from the providence of the second sec		and a second second while the second s		· · · · · · · · · · · · · · · · · · ·										
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APPENDIX B Federal Er	ergy Regulatory Commission Database 4 OF5
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	AX_STOR STATE		HAZARD	RIVER	YEAR COMP	NID_HEIGHT	NID_STOR	est. volume	DAM_LENGTH	DAM_HEIGHT	estimated width	MAX_DISCH	DAM_TYPE	NORM_STOR	SURF_AREA	DRAIN_AF
5362	146 ME	TWINE MILL	LOW	MOUSAM RIVER	1980	18	146	35,011	180	18	10.80595	2400	CNPG	104	12	
6398	774 ME	HACKETT MILLS	LOW	LITTLE ANDROSCOGGI	1986		774	18,230	220	8	10.3582	474	TCERCN	480	60	
7189	113000 ME	GREEN LAKE	LOW	REEDS BROOK	1911	8	113000	22,622	273	8	10.3582	2500	MSOT	107000	2989	
8277	2620 ME	OTIS	LOW	ANDROSCOGGIN RIVEF	1898	17	2620	153,670	840	17	10.761175	68000	CNPG	1700	115	2
9340	145 ME	UPPER KEZAR FALLS #2	LOW	OSSIPEE RIVER	1860	8	145	22,374	270	8	10.3582	16600	TOER	130	10	
9340	175 ME	LOWER KEZAR FALLS	LOW	OSSIPEE RIVER	1910	9	175	41,196	440	9	10.402975	17180	TCERON	150		
9340	145 ME	UPPER KEZAR FALLS #1	LOW	OSSIPEE RIVER	1910	11	145	22,622	196	. 11	10.492525	3360	ONPG	130		~;·
1132	720 ME	EUSTIS	LOW	NORTH BRANCH DEAC	1952	17	720	43,906	240	17			ONPORE	570	······································	· · · · · · · · · · · · · · · · · · ·
1433	1400 ME	SANDY RIVER	LOW	SANDY RIVER	1902	18	1400	77,803		18	and a second		ONMSPG	1050	· · · · · · · · · · · · · · · · · · ·	
1482	240 ME	MECHANIC FALLS	LOW	LITTLE ANDROSCOGGI	1866	15	240	27,533	172	15			MSONPG	103		
1855	55560 NH	BELLOWS FALLS	LOW	CONNECTICUT RIVER	1907	48	55560	374,973	for a construction of the second seco	48		· · · · · · · · · · · · · · · · · · ·		30000	-journey and a second second	advances and the second
1892	79800 NH	WILDER	HIGH	CONNECTICUT RIVER	1950	59	79800	2,162,999	4	59	The second		CNPGRE	55000		
1893	5700 NH	GARVINS FALLS	LOW	MERRIMACK RIVER	1901	18	5700	125,457	645	18	a fan e werde en er staar water werde en een een een eerste werde eerste eerste eerste eerste eerste eerste ee	· · · · · · · · · · · · · · · · · · ·	MSCNPG	2700	· · · · · · · · · · · · · · · · · · ·	
1893	8100 NH	AMOSKEAG	LOW	MERRIMACK RIVER	1921	29	8100	352,230	· · · · · · · · · · · · · · · · · · ·	29		,		4320		
1893	4180 NH	HOOKSETT	LOW	MERRIMACK RIVER	1927	11	4180	76,984	the second	23				4320		
1904	54000 NH	VERNON	LOW	CONNECTICUT RIVER	1927		54000	698,476		58	all is the second se			18300		i formania da como da c
2077	57700 NH	COMERFORD	HIGH	ويستعلق فالالاد فارك فستعلق الركاية سيعير كمشعا		58	······································	~	den en e							
2077	14100 NH	MCINDOES	SIGNIFICANT	CONNECTICUT RIVER	1930	170	57700	6,745,476		170	the second	· · · · · · · · · · · · · · · · · · ·	ONPORE	46800	······································	
2077	223722 NH			CONNECTICUT RIVER	1931	25	14100	202,929		25	the second second with the second sec			9800		
		MOORE	HIGH	CONNECTICUT RIVER	1957	144	223722	6,915,887	2920	144			CNPGRE	200000		*****
2287	94 NH	J. BRODIE SMITH	HGH	ANDROSCOGGIN RIVEF	1948	31	94	194,166		31	11.388025			60		
2288	NH	GORHAM	LOW	ANDROSCOGGIN RIVEF	and a second second product dataset	20	258	93,701	430	20	ali		TOERPG	258		
2300	2000 NH	SHELBURNE	LOW	ANDROSCOGGIN RIVEF	1906	16	2000	120,195		16			CNTC	960		
2311	685 NH	GORHAM	LOW	ANDROSCOGGIN RIVER	1904	24	685	205,988		24			TOEFIFIE	370	and the second s	
2326	195 NH	CROSS	HIGH	ANDROSCOGGIN RIVER		30	195	201,796		30				120		
2327	400 NH	CASCADE	HIGH	ANDROSCOGGIN RIVER	1903	58	400	425,953	the second se	58			ONPG	200		
2392	1030 NH	GILMAN	LOW	CONNECTICUT RIVER	1920	30	1030	94,603		30			PGTCER	7 <u>05</u>		
2422	830 NH	SAWMILL	LOW	ANDROSCOGGIN RIVEF	1965	20	830	181,955	835	20	and the second s	33000	CNPG	620	73	1 · · · · · · · · · · · · · · · · · · ·
2423	95 NH	RIVERSIDE	LOW	ANDROSCOGGIN RIVEF	1970	23	95	209,291	825	23	11.029825		PGTCER	60		
2456	16000 NH	AYERS ISLAND	SIGNIFICANT	PEMIGEWASSET RIVER	1924	80	16000	759,505	699	80	13.582	72000	CNCB	10000)
2457	9340 NH	EASTMAN FALLS	SIGNIFICANT	PEMIGEWASSET RIVER	1937	37	9340	178,557	414	37	11.656675	75000	CNPG	4570	530)
2861	2283 NH	PONTOOK	LOW	ANDROSCOGGIN RIVEF	1909	15	2283	63,870	399	15	10.671625	20500	TOER	883	280)
2966	60 NH	CLEMENT	LOW	WINNIPESAUKEE RIVEF	1984	24	60	31,895	120	24	11.0746	7750	CNPG	20	5	
3025	2290 NH	KELLEY'S FALLS	HIGH	PISCATAQUOG RIVER	1916	24	2290	58,474	220	24	11.0746	21300	ONPG	1350	129	
3133	119250 NH	ERROL	LOW	ANDROSCOGGIN RIVEF	1887	25	119250	56,987	205	25	11.119375	19700	OTERCN	80000	7850)
3342	94 NH	ALLIED LEATHER FOREBAY	LOW	CONTOOCOOK RIVER	1982	15	94	16,968	106	15	10.671625		CNOT	54	8	
3342	94 NH	PENACOOK LOWER FALLS	LOW	CONTOOCOOK RIVER	1982	15	94	21,450		15			CNOT	54		
3342	94 NH	ALLIED LEATHER AUXILIAR	LOW	CONTOOCOOK RIVER	1982	15	94	50,584	316	15	10.671625	40000	CNPG	54	8	
3442	2938 NH	MINE FALLS	LOW	NASHUA RIVER	1889	20	2938	70,821	325	20	10.8955	1700	MSCNPG	1970	242	2
3777	527 NH	ROLLINSFORD	LOW	SALMON FALLS RIVER			527	83,895		20			CNMSPG	456		
3820	633 NH	SOMERSWORTH	LOW	SALMON FALLS RIVER	1929	12	633	37,934		12			MSPG	377		
4451	464 NH	LOWER GREAT FALLS	SIGNIFICANT	- particular and a second s	· · · · · · · · · · · · · · · · · · ·	36	464	112,868		36		· · · · · · · · · · · · · · · · · · ·	MSCNPG	272		
4718	330 NH	COCHECO FALLS	LOW	COCHECO FIVER	1930	9	330	14,044		9			ONPG	110		
6440	208000 NH	LAKEPORT	LOW	WINNIPESAUKEE RIVEF	1958	10	208000	23,507		10	1		CNOT	165800		
6597	51 NH	PERCE	LOW	CONTOOCOOK RIVER	1921	12	51	53,108	niya — na sa	12			CBCNPG	33		
6597	50 NH	PAPER MILL	LOW	CONTOOCOOK RIVER	1921		50	26,215		9			ONPG	25		
6597	240 NH	MONADNOCK	LOW	CONTOOCOOK RIVER	1922		240	120,836		22			ONPORE	217	\$ ·	
6597	8600 NH	POWDER MILL	LOW	CONTOOCOOK RIVER	1923	21	8600	84,087		21		- j	ONPGRE	2400		
6689	114 NH	POWDER MILL PENACOOK UPPER FALLS	LOW	CONTOOCOOK RIVER	1924	16	114	45,780	5 · · · · · · · · · · · · · · · · · · ·	16			CNOT	70		
7528	· · · · · · · · · · · · · · · · · · ·	a historia a substanti a s	LOW	a second s		here and a second s				18			ONPG	200		
···· ÷ · · · ÷ · · ·	400 NH	CANAAN		CONNECTICUT RIVER	1943		400	53,489			the second		TCER	200		
7883	320 NH	WESTON	LOW	UPPER AMMONOOSUC		20	320	45,761	210	20			a good allocations are a second	· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·
7887	160 NH	MINNEWAWA	HIGH	MINNEWAWA BROOK	1932	and the second sec	160	214,044	. (63			CNVA	120		1
8405	28 NH	GLEN ROAD MCLANE	SIGNIFICANT	MASCOMA RIVER	1988		28 83	30,006 44,737		16			CNPG CNMSPG	47	and the statement of the state	
8924	83 NH			SOUHEGAN RIVER	1929											

APPENDIX B	Federal Energy	Regulatory	Commission Database	5 OF5
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	AX_STOR STATE		HAZARD	RIVER		NID_HEIGHT			and the work of the second sec		estimated width				8	a constant and second second
0898	300 NH		SIGNIFICANT	SUGAR RIVER	1922	33	300	118,931	314	33		14000	} · · · · · · ·	150		
1128	725 NH	Sector a construction of the sector of the s	LOW	UPPER AMMONOOSUC	1900	10	725	28,731	275	10	10.44775	12500	TOER	200	75	5
1128	240 NH	BROOKLYN	LOW	UPPER AMMONOOSUC	1910	19	240	56,695	275	19	and the second second second second second second	12500		50		
1163	641 NH	SOUTH BERWICK	LOW	SALMON FALLS RIVER	1916	18	641	56,407	290	18	10.80595	14747	CNPG	525	58	8 3
1313	280 NH	APTHORP	SIGNIFICANT	AMMONOOSUC RIVER	1936	24	280	62,461	235	24	11.0746	14800	CNPG	210	20	0 2
2972	360 FI	WOONSOCKET FALLS	LOW	BLACKSTONE RIVER	1960	23	360	67,988	268	23	11.029825	33000	CNPG	300	32	2
3011	530 R	ARCTIC	LOW	SOUTH BRANCH PAWT	1885	30	530	40,836	120	30	11.34325	4000	MSPG	442	45	5
3023	366 Fi	TUPPERWARE	LOW	BLACKSTONE RIVER	1904	13	366	28,889	210	13	10.582075	12750	MSPG	305	4(0 :
3037	180 Fil	ELIZABETH WEBBING MILLS	LOW	BLACKSTONE RIVER	1891	11	180	18,005	156	11	10.492525	8900	MSPG	150	26	6
3063	96 FI	VALLEY FALLS	LOW	BLACKSTONE RIVER	1859	10	96	20,896	200	10	10.44775	19310	MSPG	80	15	5
2205	3725 VT	FAIRFAX FALLS	LOW	LAMOILLE RIVER	1919	45	3725	185,990	344	45	12.014875	66900	CNPG	1080	152	2
2205	2025 VT	MILTON	LOW	LAMOILLE RIVER	1929	25	2025	40,030	144	25	11.119375	83000	ONPG	93		
2205	11520 VT	CLARK FALLS	HIGH	LAMOILLE RIVER	1937	40	11520	400,894	850	40			ONPORE	6000		
2205	6340 VT	PETERSON	HIGH	LAMOILLE RIVER	1949	75	6340	347,645	347	75			T	2840		
2306	6060 VT	ECHO	LOW	CLYDE RIVER	1922	16	6060	20,575	120	16	·····		RG	5000	- and a second second -	0
2306	420 VT	WEST CHARLESTON	LOW	CLYDE RIVER	1928	30	420	66,698	196	30				220		
2306	3400 VT	NEWPORT NO. 1	HIGH	CLYDE RIVER	1936	23	3400	92,595	365	23	provide the second end of the			3000		
2323	190000 VT	SOMERSET	HIGH	EAST BRANCH DEERFI	1913	110	190000	3,449,375	2101	110	the state of a state of a state of a state of the base		RECNIPG	57345		
2323	600 VT	SEARSBURG	LOW	DEERFIELD RIVER	1922	50	600	374,506	612	50			RECNPG	412		
2323	318000 VT	HARRIMAN	HIGH	DEERFIELD RIVER	1924	216	318000	5,311,278	1250	216	· · · · · · · · · · · · · · · · · · ·			117300		
2396	524 VT	PIERCE MILLS	LOW	PASSUMPSIC RIVER	1928	18	524	27,231	140	18	den a la companyem coma		CNPG	50		
2397	2548 VT	GAGE	LOW	PASSUMPSIC RIVER	1928	18	2548	62,437	321	18		of the second second second second		70		
2399	427 VT	ARNOLD FALLS	LOW	PASSUMPSIC RIVER	1928	20	427	91.522	420	20				46		
2400	494 VT	PASSUMPSIC	LOW	in a second s	1928	11	427	29,778	and the second sec	11	· · · · · · · · · · · · · · · · · · ·		A commentation of the second second	70		
2445	490 VT	CENTER RUTLAND		PASSUMPSIC RIVER	1898	14	494	25,887	174	14				30		
2445	592 VT		LOW	OTTER CREEK	1898	39	490 592			39	and the second sec			100		
	· · · · · · · · · · · · · · · · · · ·	CAVENDISH	Madfarment distant and an end	BLACK RIVER		Admit # 1		59,553	the second secon	sector and a sector sector	4		and the second sec	· · · · · · · · · · · · · · · · · · ·		
2490	385 VT	TAFTSVILLE	LOW	OTTAUQUECHEE RIVER	1910	18	385	42,792		18	1 · · · · · · · · · · · · · · · · · · ·			100		
2513	6085 VT	ESSEX NO. 19	SIGNIFICANT	WINOOSKI RIVER	1917	53	6085	252,473	385	53			1	1950	and the second second second second	. j =
2547	24278 VT	HIGHGATE FALLS	SIGNIFICANT	MISSISQUOI RIVER	1918	46	24278	133,139	240	46	den en e	the second second second second second		7000	state of the second second second second	
2558	2122 VT	HUNTINGTON FALLS	LOW	OTTER CREEK	1910		2122	73,259	187	34		showing and a second se		250	A	
2558	3369 VT	PROCTOR	LOW	OTTER CREEK	1910	16	3369	21,947	128	16				460		
2558	1730 VT	BELDENS EAST	LOW	OTTER CREEK	1913		1730	16,948	56	27	2 · 2 ·			150		
2558	1730 VT	BELDENS WEST	LOW	OTTER CREEK	1913		1730	9,124	57	15			· · · · · · · · · · · · · · · · · · ·	150		
2629	1000 VT	CADYS FALLS	LOW	LAMOILLE RIVER	1894	29	1000	121,560	371	29			A.W	1000		
2629	1038 VT	MORRISVILLE DAM	LOW	LAMOILLE RIVER	1924	37	1038	107,824	time to the second second second	37				150		
2629	1038 VT	MORRISVILLE BACK SPILLY	the second second second second	LAMOILLE RIVER	1924	8	1038	12,430		8	A real real real real real real real real		a sector a sector o	150		
2629	17000 VT	GREEN RIVER DAM	HIGH	GREEN RIVER	1947	110	17000	525,369	· · · · · · · · · · · · · · · · · · ·	110		and from any		16900		
2629	17000 VT	GREEN RIVER DIKE	SIGNIFICANT	GREEN RIVER	1947	22	17000	60,418		22	the second secon	and the second se	FE .	16900		
2674	1649 VT	VERGENNES NO. 9	LOW	OTTER CREEK	1912	12	1649	68,029	538	12	10.5373	3459	fG	350	7	0
2731	5100 VT	WEYBRIDGE WEST	LOW	OTTER CREEK	1944	30	5100	51,045	150	30	11.34325	46000	ONFG	600	51	9
2731	5100 VT	WEYBRIDGE EAST	LOW	OTTER CREEK	1951	30	5100	37,433	110	30	11.34325	46000	FG	600	5	9
2737	677 VT	MIDDLEBURY LOWER EAST	LOW	OTTER CREEK	1917	15	677	49,623	310	15	10.671625	13700	CNPG	45		
2737	677 VT	MIDDLEBURY LOWER WEST	LOW	OTTER CREEK	1917	15	677	12,806	80	15	10.671625	1275	FG	45	1	8
2756	400 VT	CHACE MILL	LOW	WINOOSKI RIVER	1876	29	400	78,637	240	29	11.298475	30000	FG	34	5	0
2839	160 VT	GREAT FALLS	HIGH	PASSUMPSIC RIVER	1915	34	160	62,682	160	34	11.52235	1550	FG	135	1:	2
2879	18558 VT	BOLTON FALLS	LOW	WINOOSKI RIVER	1898	75	18558	190,353	190	75	13.358125	68000	TOER	355	7(o
2905	7471 VT	ENOSBERG FALLS	LOW	MISSISQUOI RIVER	1928	21	7471	44,800		21			RG	750		0
5261	14 VT	NEWBURY		WELLS RIVER	1912		14	19,612		20	· · · · · · · · · · · · · · · · · · ·		FG	12	1:	2
5944	209 VT	MORETOWN NO. 8	SIGNIFICANT		1910	1	209	117,559		31		· · · · · · · · · · · · · · · · · · ·	FG	209		
6470	69 VT	WINOOSKI NO. 8	LOW	WINOOSKI RIVER	1985	f	69	74,378		29				34		7
7186	2250 VT	SHELDON SPRINGS	LOW	MISSISQUOLRIVER	1920		2250	125,837	a first the state of the state	38	· · · · · · · · · · · · · · · · · · ·			750		which are reached as a second
7725	793 VT	BARTON VILLAGE	LOW	CLYDE RIVER	1949	and the second second second second	793			9	the second secon			560		
9648	90 VT	FELLOWS	LOW	BLACK RIVER	1949	\$		20,896		10	A		provide the second seco	60		

APPENDIX C National Inventory of Dams Database 1 of 10

	1955 0101 1955 NHOOTIS		HAZARD	EAP STATE NAME	0010 001	COUNTY	NEAR_CITY DIST_CI	i i si esta di si constructione di si construc	PRM_PURPOSE	NID_DAMTYP	TEACTO	VID_HEIGHT	NU SION	DAM LENGTH	MAX DISCH OWNER
	1000.0101 1000 1121	BELLOWS FALLS	LOW	NO NEW HAMPSHIRE	NH-02	CHESHIPE	BELLOWS FALLS, VT.	CONNECTICUT RIVER	HYDROELECTRIC	GRAVITY	1907	48	55560	643	157600 NEW ENGLAND POWER CO.
	1889.0101 1889 MA00845 M	A GILL	SIGNIFICANT	YES MASSACHUSETTS	MA-01	FRANKLIN	TURNERS FALLS	1 CONNECTICUT RIVER	HYDROELECTRIC	GRAVITY	1970		28000	493	280000 WESTERN MASSACHUSETTS EL
	1889.0102 1889 MA0084EN	A MONTAGUE	SIGNIFICANT	YES MASSACHUSETTS	MA-01	FRANKLIN		1 CONNECTICUT RIVER	HYDROELECTRIC	GRAVITY	1915		28000	630	280000 WESTERN MASSACHUSETTS EL
			LOW	NO MASSACHUSETTS	MA-01	FRANKLIN				GRAVITY	1915				15000 WESTERN MASSACHUSETTS EL
															WESTERN MASSACHUSETTS EL
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					NH-02		VERNON, VT.								224700 NEW ENGLAND POWER CO.
					-		<u> </u>	···•	· · · · · · · · · · · · · · · · · · ·						HOLYOKE WATER POWER CO.
0.01 02 MAXDOGALL ORMUTY 1.01 0.01 MAXDOGALL CHANNEL MAXDOGALL CHANNEL CHANNEL <th< td=""><td></td><td></td><td></td><td></td><td> أعلمهم المسيم الم</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>300000 HOLYOKE WATER POWER CO.</td></th<>					أعلمهم المسيم الم										300000 HOLYOKE WATER POWER CO.
08.4.16 Dist (MASSEGMA Destruction of all (MASSEGMA															2615 HOLYOKE WATER POWER CO.
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2000 10000 1000 100000 10000 100000 10000 10000 10000 10000 10000 10000 10000 10000 1														the second of the second second	16320 CENTRAL MAINE POWER CO.
Base Value Search Value Conv.															93000 CENTRAL VERMONT PUBLIC SE
Base Date Desc Desc <thdesc< th=""> Desc Desc <thd< td=""><td></td><td></td><td>LOW</td><td>NO VERMONT</td><td>VT-01</td><td></td><td></td><td>3 LAMOILLE RIVER</td><td></td><td></td><td></td><td></td><td></td><td></td><td>83000 CENTRAL VERMONT PUBLIC SE</td></thd<></thdesc<>			LOW	NO VERMONT	VT-01			3 LAMOILLE RIVER							83000 CENTRAL VERMONT PUBLIC SE
23.3.001 24.3.1.0000/TK ULT VIG MACE								en al francés de la companya de la c							66900 CENTRAL VERMONT PUBLIC SE
28.3.8.000071 CULF_BLAND Herit Color AMAGENCOME EVANDAL EVAND															85000 CENTRAL VERMONT PUBLIC S
Bale Determine Case Method Diverse Month Cold Parameter	2283.0101 2283 ME00006 M	e deerrips	LOW	YES MAINE	ME-02	ANDROSCOGGIN	LEWISTON - AUBURN	2 ANDROSCOGGIN RIVER	HYDROELECTRIC	GRAVITY	1903				2000 CENTRAL MAINE POWER CO.
227 1022 10200 (2001) 1024 (2000) 104 10	2283.0301 2283 ME00007 M	E GULF ISLAND	HGH	YES MAINE	ME-02	ANDROSCOGGIN	LEWISTON - AUBURE	3 ANDROSCOGGIN RIVER	HYDROELECTRIC	GRAVITY	1926		56100	2488	50000 CENTRAL MAINE POWER CO.
3200_M100006 1200_M10006 1200_M1006 1200		E BRUNSWICK	LOW	NO MAINE	ME-01	CUMBERLAND	BRUNSWICK	ANDROSCOGGIN RIVER				42			20000 CENTRAL MAINE POWER CO.
Base Decomposition Base Nets VIS Media	2287.0101 2287 NH00157 N	I J. BRODIE SMITH	HGH	YES NEW HAMPSHIRE	NH-02	coos	BERLIN	ANDROSCOGGIN RIVER	HYDROELECTRIC	GRAVITY	1948	31	94	550	56000 PUBLIC SERVICE COMPANY OF
392.0 100 CHARLEND LIVE APPROXIMAGE LIVE APPROXIMAGE LIVESTIN (APL, GLL) L			LOW		NH-02	COOS	SHELBURNE	3 ANDROSCOGGIN RIVER							23000 JAMES RIVER - NEW HAMPSHIP
302_0100 302_01653004 (L. MORCACUGONYAR) LOW NO More MORCACUGONYARI LOW IN Description Constrain	2302.0101 2302 ME00005 M	E GREAT STONE	HIGH	YES MAINE	ME-02	ANDROSCOGGIN	LEWISTON - AUBURN	ANDROSCOGGIN RIVER	HYDROELECTRIC	GRAVITY	1865	27	2800	955	8050 CENTRAL MAINE POWER CO. 8
32.0 10.0 No. No. <th< td=""><td>2302.0105 2302 ME83003 M</td><td>E GULLY BROOK LOWER</td><td>LOW</td><td>NO MAINE</td><td>ME-02</td><td>ANDROSCOGGIN</td><td>LEWISTON - AUBURN</td><td>LEWISTON CANAL - GULL</td><td>HYDROBLECTRIC</td><td>GRAVITY</td><td>1859</td><td>9</td><td>2800</td><td>90</td><td>1200 CENTRAL MAINE POWER CO. 8</td></th<>	2302.0105 2302 ME83003 M	E GULLY BROOK LOWER	LOW	NO MAINE	ME-02	ANDROSCOGGIN	LEWISTON - AUBURN	LEWISTON CANAL - GULL	HYDROBLECTRIC	GRAVITY	1859	9	2800	90	1200 CENTRAL MAINE POWER CO. 8
392.0103 2302.0105302.014 PERSISTENT NEW F LOW NO MARE MODICOCOGE LEWISTON - MAREE NOW OFFEND NO 148 2.00 1.03 CEMTRATIN, NEW F NO NAME NEW F NEW F <th< td=""><td>2302.0106 2302 ME83004 M</td><td>E ANDROSCOGGIN WEIR</td><td>LOW</td><td>NO MAINE</td><td>ME-02</td><td>ANDROSCOGGIN</td><td>LEWISTON - AUBURN</td><td>LEWISTON CANAL - GULL</td><td>HYDROELECTRIC</td><td>GRAVITY</td><td>1859</td><td>9</td><td>2800</td><td>32</td><td>480 CENTRAL MAINE POWER CO. &</td></th<>	2302.0106 2302 ME83004 M	E ANDROSCOGGIN WEIR	LOW	NO MAINE	ME-02	ANDROSCOGGIN	LEWISTON - AUBURN	LEWISTON CANAL - GULL	HYDROELECTRIC	GRAVITY	1859	9	2800	32	480 CENTRAL MAINE POWER CO. &
392.010 232.014 100.014	2302.0102 2302 ME83001 M	E BATES WEIR	LOW	NO MAINE		ANDROSCOGGIN	LEWISTON - AUBURN	LEWISTON CROSS CANA	HYDROELECTRIC	GRAVITY	1859	14	2800	71	1054 CENTRAL MAINE POWER CO. 8
222.010 232.01 232.01 232.01 232.01 233.01	2302.0103 2302 ME63002 M	E RED SHOP WER	LOW	NO MAINE		ANDROSCOGGIN	LEWISTON - AUBURN	LEWISTON CROSS CANA	HYDROELECTRIC	GRAVITY	1859	18	2800	60	1573 CENTRAL MAINE POWER CO. &
232.0101 232.3 MAOGRAM CEEPFELDINGS LOW NO MASACHASTIS MAYAND PUMCE 232.0106 232.3 MAOGRAM CEEPFELDINGS SEMPECINSS MENSOR MASACHASTIS MENSOR MENSOR MASACHASTIS MASACHASTIS MENSOR MASACHASTIS MENSOR MASACHASTIS MASACHASTIS MENSOR MASACHASTIS	2302.0107 2302 ME83005 M	E CONTINENTAL WEIR	LOW	NO MAINE		ANDROSCOGGIN	LEWISTON - AUBURN	LEWISTON CROSS CANA	HYDROELECTRIC	GRAVITY	1920		2800		1030 CENTRAL MAINE POWER CO. 8
232.0 UND 232.0 UND DESCRIPTION ON MODEL PERMANE Dyname Proces Inforce_Entring Gamma Set Addition Set	2322.0101 2322 ME00084 M	e shawmut	LOW	NO MAINE	ME-01	KENNEBEC	FAIRFIELD	3 KENNEBEC RMER	HYDROELECTRIC	GRAVITY	1912	40	5100	1480	12540 CENTRAL MAINE POWER CO.
232.020 232.020 <t< td=""><td>2323.0101 2323 MAD084C</td><td>A DEERFIELD NO. 5</td><td>LOW</td><td>NO MASSACHUSETTS</td><td>MA-01</td><td>FRANKLIN</td><td>MONFICEBRIDGE</td><td>DEERFIELD RIVER</td><td>HYDROELECTRIC</td><td>GRAVITY</td><td>1992</td><td></td><td>818</td><td>151</td><td>35800 NEW ENGLAND POWER CO.</td></t<>	2323.0101 2323 MAD084C	A DEERFIELD NO. 5	LOW	NO MASSACHUSETTS	MA-01	FRANKLIN	MONFICEBRIDGE	DEERFIELD RIVER	HYDROELECTRIC	GRAVITY	1992		818	151	35800 NEW ENGLAND POWER CO.
223,000 223,000 223,000 MASSACHERTS MA-01 FMARLIN DEERFERD.PRG INCORDELETTIC GRAVITY 1112 211 551 475 5300 PERSINA POXER 233,001 2232 MASSACHERTS MA-01 FMARLIN SERENCE PRODE INCORDELETTIC GRAVITY 112 454 1017 5700 12000 PERSINA POXER 233,001 2232 VIT00014VT SEXESER MASSACHERTS MA-01 FMARLIN MCROEEPIDGE I GRAVITY 1912 458 1017 5700 PERSINA POXER 233,001 2232 VIT00014VT SEXESER MAN MEDIA SEXESER 6 FAST BRANCHEEPHEL MORDELETTIC GRAVITY 1912 51 2200 221 12000 PERSINA POXER 233,010 2232 VIT0014V VIT0011V MARCE SEXESER GRAVITY 1913 110 19000 2101 22000 2201 1202 1500 GRAVITY 1913 150 23000 2421 1500 GRAVITY 1913 150 2300 1500 1500 </td <td></td> <td></td> <td>NELOW</td> <td></td> <td></td> <td>BERKSHIPE</td> <td></td> <td>DUNBAR BROOK</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>6800 NEW ENGLAND POWER CO.</td>			NELOW			BERKSHIPE		DUNBAR BROOK							6800 NEW ENGLAND POWER CO.
232.4 Magode MA 0ESPREJ INVERT 1.007 510 FMARLAN SPERIA PROPERTIALS 3 0ESPREJ PROPE 1.017 7.010 548.0 1.017 7.010 548.0 1.017 7.010 548.0 1.017 7.010 548.0 1.017 7.010 548.0 1.017 7.010 548.0 1.017 7.010 548.0 1.017 7.010 548.0 1.017 7.010 1.017 7.010 1.017 7.010 1.017 7.010 1.017 7.010 1.017 7.010 1.017 7.010 1.017 1.011 1.010 1.0000 2.121 1.01 1.0000 2.121 1.01 1.0000 2.121 1.01 1.0000 2.121 1.01 1.0000 2.121 1.01 1.0000 2.121 1.01 1.0000 2.121 1.01 1.0000 2.121 1.01 1.0000 2.121 1.01 1.0000 2.121 1.01 1.01 1.0000 2.121 1.01 1.010 1.010 1.010 1.010															31200 NEW ENGLAND POWER CO.
223.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501 233.0501															23300 NEW ENGLAND POWER CO.
323.0701 232.321 VT-01 SEMANDICAL VT-01 MENNANDICAL VT-01 MENNANDICAL VERTICAL PORTICIONAL					MA-01	FRANKLIN	SHELBURNE FALLS	3 DEERRELD RIVER	HYDROELECTRIC		1912			510	19100 NEW ENGLAND POWER CO.
323.801 232.81 7100 16 71 Scherster Heft YE Scherster Heft YE Scherster			HGH	YES MASSACHUSETTS	MA-01	FRANKLIN	MONROEBRIDGE	1 DEEPRIELD RIVER	HYDROELECTRIC	GRAVITY	1927	110	5480	1017	87000 NEW ENGLAND POWER CO.
323.5 0101 232.5 MESONS INE WESTON NORTH CHAIN LOW NO. MANE ME-02 SOMERGET			LOW	NO. VERMONT	VT-01	BENNINGTON		7 DEERFIELD RIVER	HYDROELECTRIC	GRAVITY	1922	50	600	612	12200 NEW ENGLAND POWER CO.
235.012 2325 MESION SOUTH CHANNILOW NO. MARE MEC2 SOUTHSER SOUTHSER HOT FLAN MARE POWE 326.0101 2325 MESION SOUTH CHANNILOW MOS HOT YES 5100 CONTAX MARE POWE 326.0101 2325 MESION SOUTH CHANNILOW MOS HOT YES 533 21000 JAMES PIWER NHORE HIDPOELECTRC GMARTY 1903 58 400 583 21000 JAMES PIWER NHORE MARE POWER <			HGH	YES VERMONT	VT-01	WINDHAM	SEARSBURG	6 EAST BRANCH DEERFIELD	HYDROELECTRIC	GRAVITY			190000	2101	27000 NEW ENGLAND POWER CO.
328.011 232.6 HNODBR HGH YES NEWHAMPSHRE NH-02 COOS BEPLIN ANDROSCOGGIN RVER INDBOELECTRC GRAVITY 1903 3.0 195 5.93 21000 JAMES RVER NH-02 COOS GUPLINH ANDROSCOGGIN RVER INDBOELECTRC GRAVITY 1903 5.8 4.00 5.83 4.0000 5.83 4.0000 5.83 4.0000 5.83 4.0000 5.85 2.5000 3.05 5.5 2.5000 3.05 5.5 2.5000 3.05 4.0000 ALMES RVER- NEX NUM 333.02.012 2333 MEGODDS MARCED RVER MANE MEOC CXICRD 1 ANDROSCOGGIN RVER MUDROLECTIC GRAVITY 1918 4.0 3.110 5.2 5.00 5.64 1.21000 RUMPS RVER NUDROLECTIC GRAVITY 1918 4.0 3.110 5.2 5.00 6.80 4.0100 6.80 4.0100 6.80 4.0100 6.80 4.0100 6.80 4.0100 6.80 4.0100		E WESTON NORTH CHAN	N LOW	NO MAINE	ME-02	SOMERSET	SKOWHEGAN	KENNEBEC RIVER	HYDROELECTRIC	BUTTRESS	1921	38	22300	529	143000 CENTRAL MAINE POWER CO.
327.0101 2327 IMOD SSGADE HGH YES NEWHAMPSHEE NH-02 COOR OORFINAL ANDROSCOGRIPHER IMODOLECTRIC GRAVITY 1903 5.8 4000 AMES RIVER ANDROSCOGRIPHER IMODOLECTRIC GRAVITY 1903 5.8 4000 AMES RIVER ANDROSCOGRIPHER IMODOLECTRIC GRAVITY 1913 5.8 4000 AMES RIVER ANDROSCOGRIPHER IMODOLECTRIC GRAVITY 1913 5.8 4000 AMES RIVER ANDROSCOGRIPHER IMODOLECTRIC GRAVITY 1913 4.0 31.1 5.2.4 1.0 5.0 3.0 2.0 0.0 S.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 </td <td></td> <td></td> <td>NILOW</td> <td>NO MAINE</td> <td>ME-02</td> <td>SOMERSET</td> <td>SKOWHEGAN</td> <td>KENNEBEC AMER</td> <td>HYDROELECTRIC</td> <td>BUTTRESS</td> <td>1921</td> <td>51</td> <td>22300</td> <td>392</td> <td>51500 CENTRAL MAINE POWER CO.</td>			NILOW	NO MAINE	ME-02	SOMERSET	SKOWHEGAN	KENNEBEC AMER	HYDROELECTRIC	BUTTRESS	1921	51	22300	392	51500 CENTRAL MAINE POWER CO.
329.0101 2328 MEGODER MEGNORE	2326.0101 2326 NH00088 N	I CROSS	HGH	YES NEW HAMPSHIRE	NH-02	0006	BERLIN	ANDROSCOGGIN RIVER	HMDROBLECTRIC	GRAVITY	1903	30	195	593	21000 JAMES RIVER - NEW HAMPSHI
333.0201 2333 MEODOTS NE PLMFORD FALLS UPPER SCHIPCANT YES MANE ME-02 OGROPO FLMFORD 1 ANDROSCOGON RVER INDROSCOGON RVER 1918 4:0 3110 5:24 121900 FLMFORD FALLS FORE 334.0101 2334 MADOSSIMA CARADRER FALLS LOW VIS MASSACHUSETTS M-01 FRAMELIN BUCKAND 1 DEDRHED RVER HINDROGETTIC GRAVITY 1918 4:0 3110 5:10 337 6:8:20 MESSACHUSETTS M-01 FRAMELIN BUCKAND 1 DEDRHED RVER HINDROGETTIC GRAVITY 1918 4:0 310 5:10 337 6:8:20 MESSACHUSETTS M-01 BUCKAND 1 REMERSER RVER HINDROGETTIC GRAVITY 1928 3:5 1:8:20 8:50 9:000 I////////////////////////////////////	2327.0101 2327 NH00163 N	CASCADE	HGH	YES NEW HAMPSHIRE	NH-02	000S	GORHAM	ANDROSCOGGIN RIVER	HYDROELECTRIC	GRAVITY	1903	58	400	583	40000 JAMES RIVER - NEW HAMPSHI
333.4 0101 233.4 MA00855 MA CAPONERS FALLS LOW YES MASSACHUSETTS MA-01 FRANKLIN BUCKLAND 1 DEBRIELD RVER HYDROEECTIKC GRAVITY 190.4 3.7 5.10 3.37 652.50 MESSACHUSETTS MASSACHUS 336.0101 233.6 MEDORES FALLS LOW ND MARE ME-02 SOMERSET SOLON 1 REININGEC FIVER HYDROEECTIKC GRAVITY 192.4 5.10 3.37 652.50 MESSACHUS 336.0101 233.6 ME0008/ME ABENAVI LOW ND MANE ME-02 SOMERSET MADISON HENDREC PIVER HYDROEECTIKC GRAVITY 192.3 36 14500 65.5 900.01 MADISON PAPER RDUS 35.010 12 7.8 64.3 65.00 MADISON PAPER RDUS 35.010 12 7.8 64.3 65.00 MADISON PAPER RDUS 35.010 23.7 ME00001 ME MURSON PAPER RDUS 35.010 MADISON PAPER RDUS 35.010 MADISON PAPER RDUS 35.010 MADISON PAPER	2329.0101 2329 ME00089 M	E WYMAN	нан	YES MAINE	ME-02	SOMERSET	BINGHAM	1 KENNEBEC RIVER	HYDROELECTRIC	GRAVITY	1930	155	255000	3054	59630 CENTRAL MAINE POWER CO.
334 011 2334 IMAG085S MA GARONERS FALLS LOW YES MASSACHUSETTS MA-01 FRAMELN BUCKLAND 1 DEBRIED RHEIR HYDROELECTIRC GRAVITY 1904 37 510 337 6850 MESTERNIMASSACHUS 335.0101 2335 MEGO088/ME VILLANS LOW ND MARE ME-02 SOLERSET SOLON 1 REINBEEC RIVER HYDROELECTIRC GRAVITY 1924 25 425 1000 12000 RADISON MENDESC RIVER HYDROELECTIRC GRAVITY 1929 36 14500 6550 90002 MADISON PAPER ROLIS 396.0101 2365 MEGO003/ME ANSON LOW ND MANE ME-02 GOMERSET MADISON MEDISON MEDISON PAPER ROLIS 36 14500 6550 5300 MADISON PAPER ROLIS 375.0101 236.0101 236.0101 105.01A PAR STREAM HYDROELECTIRC GRAVITY 1928 35 82215 5500 ANDISON PAPER ROLIS 375.0101 2375.0101 2375.0101 2375.0101 2375.0101 2375.0101 2375.0101 2375.0100 2375.0101	2333.0201 2333 ME00013 M	E RUMFORD FALLS UPPE	FI SIGNIFICANT	YES MAINE	ME-02	OXFORD	RUMFORD	1 ANDROSCOGGIN RIVER	HYDROELECTRIC	GRAVITY	1918	40	3110	524	121900 RUMFORD FALLS POWER CO.
335.011 2335 MERODESINE WILLAWS LOW ND MARE ME-02 SOMERSET SOLON 1 REININGESC PRETE HODOSELETTIC GRAVITY 1939 4.5 67:00 48:00 47:00 CENTRAL MARE ME-02 SOMERSET MADISON KEININGESC PRETE HODOSELETTIC GRAVITY 1922 2.5 4.25 10:00 12:000 MOSION PAPER NOUS 366.0101 2365 ME00031 KE AVEON LOW ND MARE ME-02 APOSTOCK ASHLAND 10 SOLA PAN STREAM HODOSELETTIC GRAVITY 1922 2.5 4.25 10:00 MADISON PAPER NOUS 366.0101 2365 ME00031 KE SULP PAN HE1 YES MANE ME-02 APOSTOCK ASHLAND 10 SOLA PAN STREAM HODOSELETTIC GRAVITY 1928 3.5 89215 50:00 MERENAL STREAM HODOSELETTIC GRAVITY 1928 12 7.3 5:000 MERENAL STREAM HODOSELETTIC GRAVITY 1928 <td>2334.0101 2334 MA00855 M</td> <td>A GARDNERS FALLS</td> <td>LOW</td> <td>YES MASSACHUSETTS</td> <td>MA-01</td> <td>FRANKLIN</td> <td>BUCKLAND</td> <td>1 DEERIFICILO RIVER</td> <td>HYDROELECTRIC</td> <td>GRAVITY</td> <td>1904</td> <td>37</td> <td>510</td> <td></td> <td>65250 WESTERN MASSACHUSETTS E</td>	2334.0101 2334 MA00855 M	A GARDNERS FALLS	LOW	YES MASSACHUSETTS	MA-01	FRANKLIN	BUCKLAND	1 DEERIFICILO RIVER	HYDROELECTRIC	GRAVITY	1904	37	510		65250 WESTERN MASSACHUSETTS E
394.011 238.4 MEXONORI ME ABENANI LOW NO MANE ME-02 SOMEFSET MADISON MENNEECE PINET INDROCELETING GRAVITY 1922 2.5 4.25 10.00 128.00 MADISON MED MENDEDE FAND MENDEDE FAND MENDEDE FAND MENDEDE FAND 10 SOLA PAN 1923 3.8 14500 95.0 90000 MADISON PAPER HOLDS 35 9123 3.8 14500 95.6 90000 MADISON PAPER HOLDS 35 9123 3.8 14500 95.6 90000 MADISON PAPER HOLDS 35 9121 3.8 14500 95.6 90000 MADISON PAPER HOLDS 10 SOLA PAN STREAM HOUCELETING GRAVITY 1923 1.2 7.8 7.8 10.0 N.0 MANE ME.02 ANDOSCOGAN IVERH MODCELETING GRAVITY 1918 1.2 7.8 6.5000 MEENNANCAL PAPER 375.0101 23.65 MANE ME.02 ANDOSCOGAN IVERH MODCELETING GRAVITY 1918 3.2 4.30 CENTRAL VERMANCAL PAPER 396.0101 23.05 Y100150 VT PASSLMPSC RVER	2335.0101 2335 ME00088 M	EWILLIAMS	LOW	NO MAINE	ME-02	SOMERSET	SOLON	1 KENNEBEC RMER	HYDROELECTRIC	GRAVITY	1939	45			48790 CENTRAL MAINE POWER CO.
385.0101 2355 ME00037 ME NO NAME ME-02 GOMERSET MADISON HOPRELEGTING GRAVITY 1923 38 14500 655 90000 MADISON PAPER INDUS 368.0101 2368 ME00234 ME SQUA PAN HE41 YES MANE ME-02 AROOSTOOK ASHLAND 10 SQUA PAN FIB24 35 82215 6565 5300 MANE PAPER INDUS 375.0101 2375 ME000010 ME JAY LOW MANE ME-02 FRANKLIN JAY ANOROSCOGGIN INVER HYDROELECTING GRAVITY 1912 12 7.22 .64.3 65000 NETERNATIONAL PAPER 398.0101 2397 ME00010 ME JAY LOW NO MANE ME-02 FRANKLIN JAY ANOROSCOGGIN INVER HYDROELECTING GRAVITY 1912 17 2331 797 55000 NETERNATIONAL PAPER 398.01012 2397 YT00198 YT GRAVITY 1928 18 524 140 <td>2364.0101 2364 ME00086 M</td> <td></td> <td>·····</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>GRAVITY</td> <td></td> <td></td> <td></td> <td></td> <td>126000 MADISON PAPER INDUSTRIES</td>	2364.0101 2364 ME00086 M		·····							GRAVITY					126000 MADISON PAPER INDUSTRIES
338.0101 238.8 MEOU234 ME SQUA PAN HGH YES MANE ME-02 APROSTOCK ASHLAND 10 SQUA PAN STREAM HOPOELECTRC BUTTRESS 1926 35 69215 595 590 MANE PUBLIC SERVICE 375.0101 2375 ME00003 ME JACRMORE PALLS AVAROSCOGGIN ME HADROSCOGIN ME HOPOELECTRC GRAVITY 1918 12 742 643 65000 MATEPNATIONAL PAREM 375.0101 2336 JYC00250 VT PERDEMILS LOW NO VERMONT VT-01 CALEDONIA PASSUMPSC RWER HOPOELECTRC GRAVITY 1928 18 524 140 6430 CENTRAL VERMONT PU 397.0101 2391 YT00188 VT PASSUMPSC RWER HOPOELECTRC GRAVITY 1928 18 524 321 2770 CENTRAL VERMONT PU 397.0101 2391 YT00188 VT PASSUMPSC RWER HOPOELECTRC GRAVITY 1928 18 254 321 27700 CENTRAL VE								and a second station as a second s							90000 MADISON PAPER INDUSTRIES
375.0101 2375 ME00008 ME NO MANE ME-02 ANDROSCOGGN UVERMORE FALLS ANDROSCOGGN RVER HYDROBLECTIKC GRAVITY 1998 1.2 7.82 84.3 65000 NTEPNATIONAL PAPER 375.0101 237.5 ME00010 ME JAY LOW NO MANE ME-02 FRANELN JAY ANDROSCOGGN RVER HYDROBLECTIKC GRAVITY 1912 1.7 2331 775 56000 INTERNATIONAL PAPER 396.0101 2397 VT005020 VT PERSOLINES CAVE PASSLAMPSC RVER HYDROBLECTIKC GRAVITY 1928 1.8 2548 321 2700 GENTRAL VERMONT PU 397.0101 2397 VT00105 VT BASSLAMPSC 2 PASSLAMPSC RIVER HYDROBLECTIKC GRAVITY 1928 1.8 2548 321 2700 GENTRAL VERMONT PU 400.0101 2400 YT00105 VT PASSLAMPSC 2 PASSLAMPSC RIVER HYDROBLECTIKC GRAVITY 1928 1.8 2548 321400				YES MAINE			ASHLAND	the second reaction where an end of the second		BUTTRESS					5300 MAINE PUBLIC SERVICE CO.
375_03201 2375_ME00010 ME JAY LOW NO MANE ME-02 FRANKLIN JAY ANDROSCOGGIN RVER HYDROELECTIRC GRAVITY 1912 17 2331 797 55000 INTERNATIONAL PAPER 396.0101 2396 Y00050/VT GRAV LOW NO VERKONT VT-01 CALEDONIA PASSUMPSC RVER HYDROELECTIRC GRAVITY 1928 18 524 140 6430 CENTRAL VERKONT RV 400.0101 2400 Y00165 YT PASSUMPSC RVER HYDROELECTIRC GRAVITY 1928 18 524 140 6430 CENTRAL VERKONT RV 400.0101 2400 Y00165 YT PASSUMPSC RVER HYDROELECTIRC GRAVITY 1928 11 494 258 21400 CENTRAL VERKONT RV 430.0101 2400 Y00165 YT PASSUMPSC RVER HYDROELECTIRC GRAVITY 1929 11 494 258 21400 CENTRAL VERKONT RV 422.0101 2428 IM															65000 INTERNATIONAL PAPER CO.
398.011 238.0 YTO 00250 YT PROCENDES LOW NO VERKONT VT-01 CALEDONIA PASSUMPSC RIVER PRODELECTING GRAVITY 1928 18 524 140 6430 CENTRAL VERKONT PUID 397.0101 2395 YT00158 YT GAGE LOW NO VERKONT VT-01 CALEDONIA PASSUMPSC RIVER HMDROELECTING GRAVITY 1928 18 524 140 6430 CENTRAL VERKONT PUID 400.0101 2400 YT00158 VT PASSUMPSC NIVER HMDROELECTING GRAVITY 1928 18 524 140 6430 CENTRAL VERKONT PUID 400.0101 2400 YT00158 VT PASSUMPSC NIVER HMDROELECTING GRAVITY 1928 11 494 28 21400 6400 542 100300 6400 542 100300 6400 542 100300 6400 542 100300 6400 542 100300 6400 542 100300 6400															55000 INTERNATIONAL PAPER CO.
397_0101 2397 VT00 182 VT GAGE LOW NO VERWORT VT-01 CALEDONIA PASSUMPSIC 2 PASSUMPSIC RIVER HPDROELECTRIC GRAVITY 1928 18 2548 321 27700 CENTRAL VERWORT PUI 400.0101 24.00 VT001015 VT PASSUMPSIC LOW NO VERWORT VT-01 CALEDONIA EAST ARMET 4 PASSUMPSIC RIVER HPDROELECTRIC GRAVITY 1928 11 494 258 21400 CENTRAL VERWORT PUI 403.0101 24.00 VT00105 VT PASSUMPSIC RIVER HPDROELECTRIC GRAVITY 1928 11 494 258 21400 CENTRAL VERWORT PUI 432.0101 24.22 NH00058 IN SAMON PENDESCOTTIVER HPDROELECTRIC GRAVITY 1965 20 630 635 33000 JAMES RIVER NEW HAWGENER HERNON ENVERNMENT 14 490 174 1120 VERWORT PUI 1986 14 490 174 </td <td></td> <td>and a second sec</td> <td></td> <td>and the set of the set</td> <td></td> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td>CALCULATION OF A DESCRIPTION OF A DESCRI</td> <td></td> <td>And the second second second second</td> <td>6430 CENTRAL VERMONT PUBLIC SI</td>		and a second sec		and the set of the set			1					CALCULATION OF A DESCRIPTION OF A DESCRI		And the second second second second	6430 CENTRAL VERMONT PUBLIC SI
400.0101 2400_VT00195_VT PASSLMPSIC_RIVER LOW NO VERNONT VT-01 CALEDONIA EAST BARNET 4 PASSLMPSIC_RIVER IMPORELECTRIC GRAVITY 1929 11 494 258 21400 CENTRAL VERNONT PUL 400.0101 2403_ME001371/ME_ VEAZE LOW NO MANE MEQ_PROSECT EDONATION 1 PROCESCOT FRUER IMPORELECTRIC BUTTRESS 1913 30 4800 542 100560 842 100560 843 1905 20 630 853 33000 MANES RVES RIVER IMPORELECTRIC GRAVITY 1983 20 630 853 33000 MANES RIVER RIVER IMPORELECTRIC GRAVITY 1983 30 4800 353 33000 MANES RIVER RIVER RIVER IMPORELECTRIC GRAVITY 1984 44 490 174 1120 VERNONT RUE IMPORELECTRIC GRAVITY 1986 14 490 174 1120 VERNONT RUE REVIEWS FRAVE FRAVE FRAVE FRAVE<							PASSUMPSIC								27700 CENTRAL VERMONT PUBLIC S
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445.0101 244.5 VT00208 VT DEFENSION VT-01 RUTLAND CENTERRUTLAND OFFER RUTLAND SQMPCAUTY 19.90 1.4 49.0 1.74 11.20 VERMONT VERMONT VT-01 RUTLAND OENTERRUTLAND OFFER RUTLAND GRAVITY 19.90 1.4 49.0 1.74 11.20 VERMONT VERMONT VERMONT VERMONT VERMONT VERMONT VERMONT PUMOCULASEST RVER IMDODELECTINC GRAVITY 19.94 9.0 1.4 4.90 7.70 7.000 PUMOCULASEST RVER IMDODELECTINC GRAVITY 19.24 8.00 1.0000 6.90 1.0000 PUMOCULASEST RVER IMDODELECTINC GRAVITY 1.92.4 9.00 1.41 7.5000 PUMOCULASEST RVER IMDODELECTINC GRAVITY 1.93.7 3.70 9.40 4.14 7.5000 PUMOCULASEST RVER IMDODELECTINC GRAVITY 1.93.7 3.70 9.40															
456.0101 2455 NH00160 NH AYERS ISLAND SIGNIFICANT VES NEW HAMPSHIRE NH-02 GRAFTON BRISTOL PEMGEWASSET RIVER HYDROELECTRIC BUTTRESS 1924 80 16000 699 72000 PUBLIC SERVICE COMPY 457.0101 2457 NH00164 NH EASTMAN FALLS SIGNIFICANT VES NEW HAMPSHIRE NH-02 MERRIMACK FRANKLIN PEMIGEWASSET RIVER HYDROELECTRIC GRAVITY 1937 37 9340 414 75000 PUBLIC SERVICE COMPY															
457.0101 2457 NH00164 NH EASTMAN FALLS SIGNIFICANT VES NEW HAMPSHIFE NH-02 MERRIMACK FRANKLIN PENGEWASSET RIVER HYDROELECTRIC GRAVITY 1937 37 9340 414 75000 PUBLIC SERVICE COMPY															
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	2457.0101 2457 NH00164 1 2458.0101 2456 ME00200 M		SIGNIFICANT	YES MAINE	ME-02	PENOBSCOT	EAST MILLINOCKET		HIDHOBLECINC	GRAVITY	1937	24	9340 2970	723	75500 GREAT NORTHERN PAPER, INC

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APPENDIX C National Inventory of Dams Database 2 of 10

	DAM_NAME	HAZARD	EAP STATE_NAME	CONG_DIST	for the parameters are a set		DIST_C	CIT RIVER	PRM_PURPOSE			NID HEIGHT N			WX_DISCH OWNER
······································	DOLBY	HGH	YES MAINE	ME-02	PENOBSCOT	EAST MILLINOCKET		2 WEST BRANCH PENOBSO		GRAVITY	1906	56	56290	1395	75000 GREAT NORTHERN PAP
	STONE DAM	HCH	YES MAINE	ME-02	PENOBSCOT	EAST MILLINOCKET		4 WEST BRANCH PENOBSO	**************************************	GRAVITY	1900	27	14520	1262	109000 GREAT NORTHERN PAP
	MILLINOCKET LAKE	HIGH	YES MAINE	ME-02	PENO89007	MILLINOCKET		6 MILLINOCKET STREAM	HYDROELECTRIC	GRAVITY	1910	20	87670	635	7000 GREAT NORTHERN PAP
	NORTH TWIN	HGH	YES MAINE	ME-02	PENOBSCOT	MILLINOCKET		4 WEST BRANCH PENOBSO		GRAVITY	1934	35	392680	1051	72000 GREAT NORTHERN PAP
	NORTHFIELD MT UPPER		YES MASSACHUSETTS	MA-01	FRANKLIN	FARLEY		1 CONNECTICUT RIVER	HYDROELECTRIC	GRAVITY	1973	20	21500	493	WESTERN MASSACHES
485.0103 2485 MA83022 MA	NORTHFIELD MT UPPE	LOW	YES MASSACHUSETTS	MA-D1	FRANKLIN	FARLEY		1 CONNECTICUT RIVER	HYDROELECTRIC	GRAVITY	1972	9	21500	551	11400 WESTERN MASSACHUS
488.0101 2488 VT00044 VT	BRADFORD	HIGH	YES VERMONT	VT-01	ORANGE	BRADFORD		WAITS RIVER	HYDROELECTRIC	ARCH	1908	50	551	255	20000 CENTRAL VERMONT PU
489.0101 2489 VT00037 VT	CAVENDISH	LOW	NO VERMONT	VT-01	WINDSOR	WHITESVILLE		1 BLACK RIVER	HYDROELECTRIC	GRAVITY	1907	39	592	130	18400 CENTRAL VERMONT PU
	TAFTSVILLE	LOW	NO VERMONT	VT-01	WINDSOF	QUECHEE		4 OTTALQUECHEE RIVER	HYDROELECTRIC	GRAVITY	1910	18	385		15300 CENTRAL VERMONT PU
	VANCEBORO	SIGNIFICANT	YES MAINE	ME-02	WASHINGTON	VANCEBORO		ST. CROIX RIVER	HYDROELECTRIC	GRAVITY	1967	16	214470	469	13400 GEORGIA PACIFIC CORF
	NORTH GORHAM	HGH	YES MAINE	ME-01	CUMBERLAND	GORHAM	r	2 PRESUMPSOOT BIVER	HYDROELECTRIC	GRAVITY	1901	23	1663		1320 CENTRAL MAINE POWE
	MATTACELINK	HGH	YES MAINE	ME-02	PENOESCOT	MATTAWAMKEAG		5 PENOBSCOT RIVER	HYDROELECTRIC	GRAVITY	1939	45	69100	1170	125000 GREAT NORTHERN PAP
	SKELTON	HGH	YES MAINE	ME-02	YORK	BEDEFORD		The provide the second se	HYDROELECTRIC	GRAVITY	1939				WYAW BA NY MARKAN AND A CONTRACT
	CATARACT	LOW	NO MAINE	i a contractor a				SACO RIVER	Contraction and an and a strategy of the		Contraction (Sec.	75	33500		69600 CENTRAL MAINE POWE
	and the second s			ME-01	YORK	BEDDEFORD		SACO RIVER	HYDROBLECTRIC	GRAVITY	1938	49	266	165	5625 CENTRAL MAINE POWE
and the second	SPHINGS_	LOW	NO MAINE	ME-01	YORK	BIDDEFORD		SACO RIVER	HYDROELECTRIC	GRAVITY	1925	12	2500	269	3405 CENTRAL MAINE POWE
the second se	BRADBURY	LOW	NO MAINE	ME-01	YORK	SEDDEFORD		SACO RIVER	HYDROELECTRIC	GRAVITY	1929	12	2500		2060 CENTRAL MAINE POWE
	WEST CHANNEL DAM	LOW	NO MAINE	ME-01	YORK	BEDDEFORD		SACO RIVER	HYDROELECTRIC	GRAVITY	1895	16	266		2250 CENTRAL MAINE POWE
			YES MAINE	ME-01	YOFIK	HOLLIS		1 SACO RIVER	HYDROELECTRIC	GRAVITY	1911	13	5440	350	17000 CENTRAL MAINE POWE
	BONNY EAGLE	SIGNIFICANT	YES MAINE	ME-01	YORK	HOLLIS		1 SACO RIVER	HYDROELECTRIC	GRAVITY	1911	67	5440	784)	CENTRAL MAINE POWE
30.0101 2530 ME00037 ME	HIRAM	LOW	NO MAINE	1	OXFORD	BALOWIN	L	4 SACO RIVER	HYDROELECTRIC	GRAVITY	1917	30	2530	432	16475 CENTRAL MAINE POWE
31.0101 2531 ME00035 ME	WEST BUXTON	LOW	NO MAINE	ME-01	YORK	BUXTON		5 SACO RIVER	HYDROELECTRIC	GRAVITY	1907	30	13200		4930 CENTRAL MAINE POWE
	MILFORD	LOW	NO MAINE	ME-02	PENOBSCOT	OLD TOWN		PENOBSCOT RIVER	HYDROELECTRIC	GRAVITY	1906	34	13300	1400	70265 BANGOR HYDRO-ELECT
	GILMAN FALLS	LOW	NO MAINE	ME-02	PENOBSCOT	OLD TOWN		STILLWATER RIVER	HYDROELECTRIC	GRAVITY	1906	8	13300	475	35132 BANGOR HYDRO ELECT
	FORTHALIFAX	LOW	NO MAINE	ME-01	KENNEBEC	WATERVILLE		SEBASTICOOK RIVER	HYDROELECTRIC	BUTTRESS	1908	29	5500	473	46500 CENTRAL MAINE POWE
	AUTOMATIC	LOW	NO MAINE	ME-01	KENNEBEC	WATERVILLE		MESSALONSKEE STREAM		GRAVITY	1900	33	1440	81	1910 KENNEBEC WATER DIS
	UNION GAS	LOW	- {····												
and a second second				ME-01	KENNEBEC	SIDNEY		5 MESSALONSKEE STREAM		GRAVITY	1924	36	750	343	2460 CENTRAL MAINE POWE
58.0101 2558 VT00042 VT	HUNTINGTON FALLS	LOW	NO VERMONT	VT-01	ADDISON	WEYBRIDGE		1 OTTER CREEK	HYDROELECTRIC	GRAVITY	1910	34	2122	187	2587 VERMONT MARBLE CO
	OAKLAND	LOW	YES MAINE	ME-01	KENNEBEC	WATERVILLE		6 MESSALONSKEE STREAM		GRAVITY	1901	14	110	115	200 CENTRAL MAINE POWE
59.0201 2559 ME00106 ME	MESSALONSKEE LAKE	HCH	YES MAINE	ME-01	KENNEBEC	OAKLAND		MESSALONSKEE STREAM		GRAVITY	1992	13	118300	166	2400 CENTRAL MAINE POWE
72.0101 2572 ME00204 ME	RIPOGENUS	HGH	YES MAINE	ME-02	PISCATAQUIS	MILLINOCKET	L 3	37 WEST BRANCH PENORSC	HYDROELECTRIC	GRAVITY	1916	73	977000	795	92800 GREAT NORTHERN PAR
74.0101 2574 ME00082 ME	LOCKWOOD	LOW	NO MAINE	ME-01	KENNEBEC	WATERVILLE		KENNEBEC RIVER	HYDROELECTRIC	GRAVITY	1919	20	1830	904	123000 MERIMAL LIMITED PARTY
76.0101 2576 CT00232 CT	SHEPAUG	HGH	YES CONNECTICUT	CT-08	NEW HAVEN	BERKSHIPE ESTATES		1 HOUSATONIC RIVER	HYDROELECTRIC	GRAVITY	1955	140	86100	1412	180000 CONNECTICUT LIGHT &
	BULLS BRIDGE	SIGNIFICANT	YES CONNECTICUT	CT-06	LITCHFIELD	GAYLORDSVILLE	1	2 HOUSATONIC RIVER	HYDROELECTRIC	GRAVITY	1902	22	3120	203	45000 CONNECTICUT LIGHT &
	NORTH LANESVILLE DIK		YES CONNECTICUT	CT-06	LITCHFIELD	NEW MILFORD		2 ROCKY RIVER	HYDROELECTRIC	GRAVITY	1929	7	218650	181	CONNECTICUT LIGHT &
- The second s	SOUTH LANESVILLE DIKI		YES CONNECTICUT	CT-06	LITCHFIELD	NEW MILFORD		2 ROCKY RIVER	HYDROELECTRIC	GRAVITY	1929	17	218650	391	CONNECTICUT LIGHT &
	STEVENSON	HGH	YES CONNECTICUT	1-1-1-1-1	FAIRFIELD	OXFORD	t	HOUSATONIC RIVER	HYDROELECTRIC	GRAVITY	1919	83	37200	1250	70000 CONNECTICUTLIGHT&
and the second sec	SPOONER	SIGNIFICANT	YES CONNECTICUT	CT-06	LITCHABLD	GAYLORDSVILLE	ţ.	2 HOUSATONIC RIVER	HYDROELECTRIC	GRAVITY	1902	20	37200	1250	45000 CONNECTICUT LIGHT &
interest condicionations, or							- · ·								
	BULLS BRIDGE MOUNTA		YES CONNECTICUT	CT-06	LITCHFIELD	NEW MILFORD		9 HOUSATONIC RIVER	HYDROELECTRIC	GRAVITY	1902	22	3120	203	150 CONNECTICUT LIGHT &
	FALLS VILLAGE	SIGNIFICANT	YES CONNECTICUT	CT-06	LITCHFIELD	FALLS VILLAGE		1 HOUSATONIC RIVER	HYDROELECTRIC	GRAVITY	1913	16	3100	320	38000 CONNECTICUT LIGHT &
00.0101 2600 ME00142 ME	WESTENFIELD	LOW	NO MAINE	ME-02	PENOBSCOT	HOWLAND		1 PENOBSCOT RIVER	HYDROELECTRIC	GRAVITY	1988	45	17900	664	96000 BANGOR - PACIFIC HYD
11.0101 2611 ME00083 ME	HYDRO-KENNEBEC	LOW	NO MAINE	ME-01	KENNEBEC	WATERVILLE		KENNEBEC RIVER	HYDROELECTRIC	GRAVITY	1989	40	6150	850	667000 SCOTT PAPER CO. & U/
	FLAGSTAFF	HGH	YES MAINE	ME-02	SOMERSET	THE FORKS		17 DEAD RIVER	HYDROELECTRIC	GRAVITY	1948	43	435000	1347	20000 CENTRAL MAINE POWE
13.0101 2613 ME00132 ME	MOXE	LOW	NO MAINE	ME-02	SOMERSET	THE FORKS	1	8 MOXIE STREAM	HYDROELECTRIC	GRAVITY	1925	17	39400	570	1850 CENTRAL MAINE POWE
15.0101 2615 ME00133 ME	BRASSUA	HGH	YES MAINE	ME-02	SOMERSET	ROCKWOOD		4 MOOSE RIVER	HYDROELECTRIC	BUTTRESS	1927	50	275000	1789	27000 CENTRAL MAINE POWE
31.0101 2631 MA00737 MA	WORONOCO	LOW	NO MASSACHUSETTS	MA-01	HAMPOEN	WESTFIELD		8 WESTFIELD RIVER	HYDROELECTRIC	GRAVITY	1938	53	2565	1475	210000 INTERNATIONAL PAPER
	CANADA FALLS	LOW	YES MAINE	ME-02	SOMERSET	PITTSTON FARM	1.1.1	WEST BRANCH PENOBSC		GRAVITY	1921	50	26740	764	10060 GREAT NORTHERN PAP
34.0401 2634 ME00206 ME	SEBOOMOOK	LOW	YES MAINE	ME-02	SOMERSET	SEBOOMOOK	1	WEST BRANCH PENOBSC		GRAVITY	1936	60	159000	621	45000 GREAT NORTHERN PAP
	CAUCOMGOMOC	LOW	YES MAINE	ME-02	PISCATAQUIS	CHESUNCOOK	1	CALICOMGOMOC STREAM		GRAVITY	1981	12	103800	2681	14750 GREAT NORTHERN PAP
and the second sec	RAGGEDLAKE	LOW	YES MAINE		PISCATAQUIS	MILLINOCKET		RAGGED STREAM	HYDROELECTRIC	GRAVITY	1937		40170	1204	6680 GREAT NORTHERN PAP
				ME-02								30			
	SCOTLAND	HGH	YES CONNECTICUT	CT-02	WINDHAM	BALTIC	ļ	4 SHETUCKET RIVER	HYDROELECTRIC	BUTTRESS	1909	37	2000	481	60000 CONNECTICUT LIGHT &
	MEDWAY	LOW	NO MAINE	ME-02	PENOBSCOT	MEDWAY		WEST BRANCH PENOBSC		GRAVITY	1922	35	1980	513	18700 BANGOR HYDRO-ELECT
71.0101 2671 ME00091 ME	MOOSEHEAD - EAST OU		NO MAINE	f	PISCATAQUIS	THEFORKS		2 4 KENNEBEC RIVER	MYDROELECTRIC	GRAVITY	1835	20	1400000	1004	26100 KENNEBEC WATER POV
71.0102 2671 ME00092 ME	MOOSEHEAD - WEST OU	÷	NO MAINE	ME-02	SOMERSET	THEFORKS	ļ., , ,	2 9 KENNEBEC RIVER	HYDROELECTRIC	GRAVITY	1835	18	1400000	830	3900 KENNEBEC WATER POV
10.0101 2710 ME00138 ME	ORONO	LOW	NO MAINE	ME-02	PENOBSCOT	ORONO	<u>.</u>	STILLWATER RIVER	HYDROELECTRIC	BUTTRESS	1917	15	1300	1180	43500 BANGOR HYDRO-ELECT
12.0101 2712 ME00139 ME	STILLWATER	LOW	NO MAINE	ME-02	PENOBSCOT	ORIONO	· · ·	3 STILLWATER RIVER	HYDROBLECTRIC	GRAVITY	1902	25	3830	1712	25000 BANGOR HYDRO-ELECT
21.0101 2721 ME00155 ME	HOWLAND	LOW	NO MAINE	ME-02	PENOBSCOT	HOWLAND		PISCATAQUIS RIVER	HYDROELECTRIC	GRAVITY	1916	17	4370	660	42525 BANGOR HYDRO-ELECT
27.0101 2727 ME00263 ME	ELLSWORTH	HGH	YES MAINE	ME-02	HANCOCK	ELLSWORTH	1	UNION RIVER	HYDROELECTRIC	BUTTRESS	1907	62	3040	377	17000 BANGOR HYDRO-ELECT
27.0201 2727 ME00264 ME	GRAHAM	HGH	YES MAINE	ME-02	HANCOCK	ELLSWORTH		4 UNION RIVER	HYDROELECTRIC	GRAVITY	1924	43	145000	750	19000 BANGOR HYDRO ELECT
31.0101 2731 VT00047 VT	WEYBRIDGE WEST	LOW	NO VERMONT	VT-01	ADDISON	WEYERIDGE	T	OTTERCHEEK	HYDROELECTRIC	GRAVITY	1944	30	5100	150	46000 CENTRAL VERMONT PU
37.0101 2737 VT00194 VT	MIDDLEBURY LOWER EA	LOW	NO VERMONT	VT-01	ADDISON	WEYBRIDGE	1.	5 OTTER CREEK	HYDROELECTRIC	GRAVITY	1917	15	677	310	13700 CENTRAL VERMONT PU
				Y 1-01		TOTAL ADIC	1.5			GRAVITY	101/				15100 CONTRACTORING NI PO
90.0102 2790 MA83042 MA	FISHLADDER	LOW	NO MASSACHUSETTS	÷	MIDDLESEX	Loue	1 -	MERRIMACK RIVER	HYDROELECTRIC			23	4500	85	
	ELF FOREBAY WALL	LOW	NO MASSACHUSETTS		MIDDLESEX	LOWELL		NORTHERN CANAL	HYDROELECTRIC	GRAVITY	1848	20	4500	120	US NATIONAL PARK SE
	ELF FISH PASSAGE	LOW	NO MASSACHUSETTS		MIDDLESEX	LOWELL		NORTHERN CANAL	HYDROELECTRIC	GRAVITY		15	4500	100	US NATIONAL PARK SE
90.0112 2790 MA00836 MA	SWAMP LOCKS	LOW	NO MASSACHUSETTS	MA-05	MIDDLESEX	LOWELL	t	UPPER PAWTUCKET CAN	HYDROELECTRIC	GRAVITY	1823	15	4500	105	3367 BOOTT HYDROPOWER
90.0121 2790 MA83054 MA	EAST CANAL SYPHON S	LOW	NO MASSACHUSETTS	MA-05	MODLESEX	LOWELL	1.	EASTERN CANAL	HYDROELECTRIC	GRAVITY		19	4500	36	500 US NATIONAL PARK SE
	LAWRENCE STREET	LOW	NO MASSACHUSETTS		MIDDLESEX	LOWFIL	+	WESTERN CANAL	HYDROELECTRIC	GRAVITY	1831	12	4500	100	1654 BOOTT HYDROPOWER

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		E DAM_NAME	HAZARD		STATE NAME	CONG_DIST		NEAR_CITY	DIST_C		PRM_PURPOSE	NID DAMTYP				DAM_LENGTH		
2790.0120	2790 MA00835 MA	LOWER PAWTUCKET LO	LOW	NO	MASSACHUSETTS	MA-05	MEDDLESEX	LOWELL	1	LOWER PAWTUCKET CA	HYDROELECTRIC	GRAVITY	1822	20		100	3400	BOOTT HYDROPOWER &
2790.0101	2790 MA00837 MA	PAWTUCKET	LOW	NO	MASSACHUSETTS	MA-05	MIDDLESEX	LOWELL		MERRIMACK RIVER	HYDROELECTRIC	GRAVITY	1848	16	4500	1093	138000	BOOTT HYDROPOWER & (
2790.0103	2790 MA83043 MA	NORTH CANAL GATEHOL	LOW	NO	MASSACHUSETTS	MA-05	MIDDLESEX	LOWELL		MERRIMACK RIVER	HYDROELECTRIC	GRAVITY	1848	16	4500	1093		US NATIONAL PARK SERV
2790.0115	2790 MA8300E MA	MERRIMACK	LOW	NO	MASSACHUSETTS	MA-05	MIDDLESEX	LOWEL		MERRIMACK CANAL	HYDROELECTRIC	GRAVITY	1847	8	4500	18		BOOTT HYDROPOWER &
2790.0118	2790 MA83007 MA	HALL STREET	LOW	NO	MASSACHUSETTS		MIDDLESEX	LOWELL	1	WESTERN CANAL	HYDROELECTRIC	GRAVITY	1831	15	4500	115		BOOTT HYDROPOWER &
2790.0123	2790 MA8301CMA	BOOT	LOW	NO	MASSACHUSETTS		MODLESEX	LOWELL		EASTERN CANAL	HYDROELECTRIC	GRAVITY	1835	7	4500	40		BOOTT HYDROPOWER &
2790.0111	2790 MA00834 MA		SIGNIFICANT	YES		t	MIDDLESEX	LOWELL		MERRIMACK RIVER	HYDROELECTRIC	GRAVITY	1848	13	and the same the same	160	factor and a second second	BOOTT HYDROPOWER &
2790.0117	2790 MA83005 MA	BOLLING	LOW	NO	MASSACHUSETTS		MIDDLESEX	LOWELL		MERRIMACK CANAL	HYDROELECTRIC	GRAVITY	1835	19		18		BOOTT HYDROPOWER &
2790.0104	2790 MA83044 MA	GRW - ISLAND SECTION		NO	MASSACHUSETTS	MA-05	MIDDLESEX	LOWELL		NORTHERN CANAL	HYDROELECTRIC	GRAVITY	1848	31	4500	1200		US NATIONAL PARK SER
2790.0105						MA-05												
	2790 MA8304E MA	GREAT RIVER WALL (GR		NO	MASSACHUSETTS		MIDDLESEX	LOWFLL	den en el compositore el compositore el compositore en el compositore en el compositore en el compositore en el	NORTHERN CANAL	HYDROELECTRIC	GRAVITY	1848	28		900		US NATIONAL PARK SER
2790.0106	2790 MA83046 MA	GRW - WASTE GATE SEC		NO	MASSACHUSETTS	MA-05	MIDDLESEX	LOWELL	+	NORTHERN CANAL	HYDROELECTRIC	GRAVITY	1848	32		65		US NATIONAL PARK SEF
2790.0113	2790 MAB3051 MA	HAMILTON WASTE GATE		NO	MASSACHUSETTS		MIDDLESEX	LOWELL		UPPER PAWTUCKET CAN		GRAVITY	1848	120		10		US NATIONAL PARK SEF
2800.0101	2800 MA00234 MA		LOW	NO	MASSACHUSETTS		ESSEX	LAWRENCE		MERRIMACK RIVER	HYDROELECTRIC	GRAVITY	1848	39	19900	943		LAWRENCE HYDROELEC
2804.0101	2804 ME00287 ME		LOW	NO	MAINE	ME-02	WALDO	SWANVILLE		GOOSERVER	HYDROELECTRIC	GRAVITY	1900	10	11270	250		GOOSE RIVER HYDRO, #
2804.0501	2804 ME00594 ME		LOW	NO	MAINE		WALDO	BELFAST	11	GOOSE RIVER	HYDROELECTRIC	BUTTRESS	1908	21	82	231		GOOSE RIVER HYDRO, I
2804.0201	2804 ME00286 ME	MASONIS	LOW	NO	MAINE	ME-02	WALDO	BELFAST	1 4	GOOSE RIVER	HYDROBLECTRIC	GRAVITY	1835	15	1800	86		GOOSE RIVER HYDRO, I
2804.0301	2804 ME00285 ME	KELLY	LOW	NO	MAINE	ME-02	WALDO	BELFAST	1 2	GOOSE RIVER	HYDROELECTRIC	GRAVITY	1835	15	270	135		GOOSE RIVER HYDRO, I
2808.0101	2808 ME00551 ME	BARKER'S MILL	LOW	NO	MAINE	ME-02	ANDROSCOGGIN	AUBURN		LITTLE ANDROSCOGGIN F	HYDROELECTRIC	BUTTRESS	1874	30		230		CONSOLIDATED HYDRO
2809.0101	2809 ME00094 ME		HGH		MAINE	ME-01	KENNEBEC	GARDINER	1	COBBOSSEECONTEE STR		GRAVITY	1900	24		227		CONSOLIDATED HYDRO
897.0101	2897 ME00065 ME		LOW	NO		ME-01	CUMBERLAND	WESTBROOK		PRESUMPSCOT RIVER	HYDROELECTRIC	GRAVITY	1911	12		102		S. D. WARREN COMPAN
897.0102	2897 ME83037 ME	SACCARAPPA EAST	LOW	NO		ME-01	CUMBERLAND	WESTBROOK	-	PRESUMPSCOT RIVER	HYDROELECTRIC	GRAVITY	1911	9	100	220		S. D. WARREN COMPA
									+					the second contracts				
931.0101	2931 ME00067 ME	GAMBO	LOW	NO	MAINE	ME-01	CUMBERLAND	WINDHAM		PRESUMPSCOT RIVER	HYDROELECTRIC	GRAVITY	1911	24		350		S. D. WARREN COMPA
932.0101	2932 ME00325 ME	MALLISON FALLS	LOW	NO	MAINE	ME-01	CUMBERILAND	WESTBROOK		PRESUMPSCOT RIVER	HYDROELECTRIC	GRAVITY	1900	14		288		S. D. WARREN COMPA
942.0101	2942 ME00068 ME	DUNDEE	HIGH	YES		ME-01	CUMBERLAND	SOUTH WINDHAM	4	PRESUMPSCOT RIVER	HYDROELECTRIC	GRAVITY	1913	44		1375		S. D. WARREN COMPA
2966.0101	2966 NH83001 NH	CLEMENT	LOW	NO	NEW HAMPSHIRE	NH-02	BELKNAP	FRANKLIN		WINNPESAUKEE AIVER	HYDROELECTRIC	GRAVITY	1984	24	60	120	7750	KATSEKAS, J. & DIMOS
2972.0101	2972 RI03902 R	WOONSOCKET FALLS	LOW	YES	RHODE ISLAND	RI-01	PROVIDENCE	WOONSOCKET		BLACKSTONE RIVER	HYDROELECTRIC	GRAVITY	1960	23	360	268	33000	WOONSOCKET, CITY O
985.0101	2985 MA00262 MA	WILLOW MILL	SIGNIFICANT	YES	MASSACHUSETTS	MA-01	BERKSHIRE	STOCKBRIDGE		HOUSATONIC RIVER	HYDROELECTRIC.	GRAVITY	1872	12	50	180	10000	MEAD PAPER CORP.
998.0101	2998 MA83011 MA	LAWRENCE STREET	LOW	NO		MA-05	MODLESEX		1	CONCORD RMER	HYDROELECTRIC	GRAVITY		15		320		CENTENNIAL ISLAND H
011.0101	3011 RI03802 R	ARCTIC	LOW		RHODE ISLAND	RI-02	KENT	ARCTIC		SOUTH BRANCH PAWTUN		GRAVITY	1885	30		120		NATCO PRODUCTS CO
023.0101	3023 Ri83001 R	TUPPERWARE	LOW		FIHODE ISLAND	111 02	PROVIDENCE	NORTH SMITHFIELD	1	BLACKSTONE RIVER	HYDROELECTRIC	GRAVITY	1904	13		210		BLACKSTONE HYDRO I
						linne												
3025.0101	3025 NH00299 NH	KELLEY'S FALLS	HGH		NEW HAMPSHIRE	NH-01	HILLSBOROUGH	MANCHESTER		PISCATAQUOG RIVER	MOROELECTRIC	GRAVITY	1918	24	2290	220		NH DEPT. OF ENVIR. SE
037.0101	3037 RI83002 RI	ELIZABETH WEBBING MIL		ND	RHODEISLAND	RI-01	PROVIDENCE	CENTRAL FALLS	+	BLACKSTONE RIVER	HYDROELECTRIC	GRAVITY	1891	11		156		ROOSEVELT HYDRO EL
3051.0101	3051 VT83006 VT	EAST BARNET	LOW	ND	VERMONT	VT-01	CALEDONIA		+	PASSUMPSIC RIVER	HYDROELECTRIC	GRAVITY	1984	12		290		CENTRAL VERMONT PL
3063.0101	3063 RI00401 FI	VALLEY FALLS	LOW	NO	RHODE ISLAND	RI-01	PROVIDENCE	CENTRAL FALLS	L.	BLACKSTONE RIVER	HYDROELECTRIC	GRAVITY	1859	1.0	96	200	19310	BLACKSTONE FALLS A
127.0101	3127 MA83012 MA	WARELOWER	LOW	NO	MASSACHUSETTS	MA-02	HAMPSHERE	WARE		WARE RIVER	HYDROELECTRIC	GRAVITY	1890	18	145	118	5770	PIONEER HYDROPOWE
3127.0201	3127 MA00594 MA	WAREUPPER	LOW	NO	MASSACHUSETTS	MA-02	HAMPSHIRE	WARE	1	WARE RIVER	HYDROELECTRIC	GRAVITY	1890	34	985	250	5900	PIONEER HYDROPOWE
128.0101	3128 NH00015 NH	LOCHMERE	LOW	NO	NEW HAMPSHIRE	NH-02	BELKNAP	EAST TILTON		WINIMPESAUKEE RIVER	HYDROELECTRIC	GRAVITY	1910	11	33280	223	2400	NH DEPT. OF ENMR. SE
3133.0101	3133 NH00161 NH	ERIPICIL	LOW	NO		NH-02	00005	EFIFICI.		ANDROSCOGGIN RIVER	HYDROELECTRIC	GRAVITY	1887	25		205		UNION WATER POWER
180.0101	3180 NH00093 NH	GREGG'S FALLS	HCH	YES		NH-01	HILLSBOROUGH	PINARDVILLE		PISCATAQUOG RIVER	HYDROELECTRIC	GRAVITY	1917	60		1360		NH DEPT. OF ENVIR. SE
185.0101	3185 NH00378 NH	WEBSTER	LOW	NO	NEW HAMPSHIRE		MERRMACK	PEMBROKE	¹		HYDROELECTRIC	GRAVITY						
		· · · · · · · · · · · · · · · · · · ·				NH-02		PEWERKANE		SUNCOOK RIVER			1917	18		250		PEMBROKEHYDROCO
185.0201	3185 NH00377 NH		LOW	NO	NEWHAMPSHIRE	NH-02	MERRIMACK			SUNCOOK RIVER	HYDROELECTRIC	GRAVITY	1891	26	·····	108		PEMBROKE HYDRO CO
3240.0201	3240 NH00348 NH	YOPK	LOW	NO	NEW HAMPSHIRE	NH-02	MERRIMACK	CONCORD	لحنهد سميله	CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1967	10	500	300	14150	NH DEPT. OF ENVIR. SE
8240.0101	3240 NH00614 NH	BRIAR PIPE	LOW	NO	NEW HAMPSHIRE	NH-02	MERRIMACK		1	CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1936	17	50	130	2100	BRIAR HYDRO ASSOCI
265.0101	3265 NH00037 NH	STEELS POND	LOW	NO	NEWHAMPSHIPE	NH-02	HILLSBOROUGH	HILLSBORD	1	NORTH BRANCH CONTOC	HYDROELECTRIC	GRAVITY	1909	14	540	104	4300	NH DEPT. OF ENVIR. SE
320.0101	3320 NH83003 NH	SUGAR RIVER I	SIGNIFICANT	YES	NEW HAMPSHIRE	NH-02	SULLIVAN	NEWPORT	1	SUGAR PIVER	HYDROELECTRIC	BUTTRESS	1928	18	70	175		RUGER, WILLIAM B.
342.0101	3342 NH83004 NH	ALLIED LEATHER FOREB	LOW	NO	NEW HAMPSHIPE	NH-02	METERMACK	1	1	CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1982	15		106	1	NEW HAMPSHIRE HYDE
342.0102	3342 NH83005 NH	PENACOOK LOWER FALL		NO	NEW HAMPSHIRE	NH-02	MERRIMACK	1		CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1982	15		134		NEW HAMPSHIRE HYDE
342.0103	3342 NH83006 NH	ALLIED LEATHER AUXIL		NO	NEWHAMPSHIRE	NH-02	MERRIMACK	1	1	CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1982	15		316	1	NEW HAMPSHIRE HYDA
442.0101	3442 NH00116 NH	MINE FALLS	LOW	NO	NEW HAMPSHIRE	NH-02	HILLSBOROUGH	NASHUA	1 .	NASHUA RIVER	HYDROELECTRIC	GRAVITY	1889	20				
444.0101	3444 ME00391 ME	ROCKY GORGE UPPER	LOW	NO		ME-01	YORK	SOUTH BERWICK	÷;		HYDROELECTRIC	GRAVITY				325		NASHUA, CITY OF
464.0101										GREAT WORKS RIVER			1900	10		140	· · · · · · · · · · · · · · · · · · ·	ROCKY GORGE CORP.
	3464 NH00144 NH	LOWERLISBON	LOW	NO	a second s	NH-02	GRAFTON	BATH		AMMONOOSUC RIVER	HYDROELECTRIC	GRAVITY	1986	24	224	197		WHITE MOUNTAIN HYDI
472.0101	3472 CT83006 CT	WYRE - WYND	LOW	NO		ļ	NEWLONDON	JEWETT CITY		OUINEBAUG RIVER	HYDROELECTRIC	GRAVITY	1913	14		483		SOUTHWIPE COMPANY
562.0101	3562 ME83013 ME	BARKER MILL UPPER	LOW	NO	MAINE	ME-02	ANDROSCOGGIN	AUBURN	4:	LITTLE ANDROSCOGGIN	HYDROELECTRIC	GRAVITY	1987	24	665	230	19900	CONSOLIDATED HYDR
777.0101	3777 NH00396 NH	ROLLINSFORD	LOW	ND	NEW HAMPSHIRE	1	STRAFFORD	ROLLINSFORD	1	SALMON FALLS RIVER	HYDROELECTRIC	GRAVITY	1910	20	527	385	7000	
820.0101	3820 NH00127 NH	SOMERSWORTH	LOW	NO	NEW HAMPSHIRE	NH-01	STRAFFORD	SOMERSWORTH		SALMON FALLS RIVER	HYDROELECTRIC	GRAVITY	1929	12	633	300	8000	GENERAL ELECTRIC CO
984.0101	3984 NH83049 NH	SOUTH MILTON	LOW	NO	NEW HAMPSHIRE	1	STRAFFORD	SOMMERSWORTH	11	SALMON FALLS RIVER	HYDROELECTRIC	GRAVITY	1893	15		160		SALMON FALLS RIVER
985.0101	3985 NH00390 NH	NORTH ROCHESTER	SIGNIFICANT	YES		1	STRAFFORD	ROCHESTER	1	SALMON FALLS RIVER	HYDROELECTRIC	GRAVITY	1903	27		1865		TILLOTSON HEALTHCA
202.0101	4202 ME83014 ME	LOWELL TANNERY	LOW	NO		ME-02	PENDESCOT	EASTLOWELL	· †	PASSADUMKEAG RIVER	HYDROELECTRIC	GRAVITY	1987		820	230		CONSOLIDATED HYDR
														27				
254.0101	4254 NH00304 NH	EXETER RIVER	LOW	NO	NEW HAMPSHIRE	NH-01	ROCKINGHAM	EXELER	· 	EXETER AVER	HYDROELECTRIC	GRAVITY	1927	15		110		PHILLIPS, PAUL T. II
293.0101	4293 ME00111 ME	WAVERLY AVENUE	HGH	YES		ME-02	SOMERSET	PITTSFIELD		SEBASTICOOK RIVER	HYDROELECTRIC	GRAVITY	1893	11	7300	272		PITTSFIELD, TOWN OF
318.0101	4318 NH00427 NH	NOONEMILLS	LOW	NO	NEW HAMPSHIRE	NH-02	HILLSBOROUGH	PETERBOROUGH		CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1938	14	315	200	6700	RIVER STREET ASSOCI
1320.0101	4320 MA00091 MA	SOUTH BARRE MILL PON	LOW	NO	MASSACHUSETTS	MA-01	WORCESTER	SOUTH BARRE		WARE RIVER	HYDROELECTRIC	GRAVITY	1981	20	260	315	17230	SOUTH BARRE HYDRO
	4413 ME00028 ME	MAHANEY	LOW	NO	MAINE	ME-02	FRANKLIN	RANGELEY		KENNEBAGO RIVER	HYDROELECTRIC	GRAVITY	1932	15		232		KENNEBAGO HYDRO CO
413.0101			and a second			and a special section of the section												
413.0101		KENNEBAGOFALIS	LOW	in	MAINE	1ME-02	FRANKIN	FANGELEV		KENNERMOORVER	HYDROFICMEN	GRAVEY	1015)			160	1 1004	
413.0101 413.0201 451.0101	4413 ME00317 ME 4451 NH00126 NH	KENNEBAGO FALLS	SIGNIFICANT	NO	NEW HAMPSHIRE	ME-02	FRANKLIN STRAFFORD	ROLLINSPORD		KENNEBAGO RIVER	HYDROELECTRIC HYDROELECTRIC	GRAVITY	1915	15 36		160 270		KENNEBAGO HYDRO C SOMERSWORTH, CITY

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		E DAM_NAME	HAZARD		STATE_NAME	CONG_DIST			DIST_C		PRM_PURPOSE	NID DAMTYP					MAX_DISCH	
4609,0101	4609 NH00061 NH	AMMONOOSUC RIVER	LOW	NO	NEW HAMPSHIRE	NH-02	GRAFTON	BATH		AMMONOOSUC RIVER	HYDROELECTRIC	GRAVITY	1900	17	352	365	40000	NEW HAMPSHIRE WOOD PRODU
4718.0101	4718 NH00547 NH	COCHECO FALLS	LOW	NO	NEWHAMPSHIRE	NH-01	STRAFFORD	DOVER		COCHECORIVER	HYDROELECTRIC	GRAVITY	1930	9	330	150	2900	DOVER, CITY OF
5018.0101	5018 MA00752 MA	BEN SMITH	LOW	NO	MASSACHUSETTS	MA-05	MODLESEX	MAYNARD	-	ASSABET RIVER	HYDROELECTRIC	GRAVITY	1907	10	130	168	3054	DIGITAL EQUIPMENT CORP.
5062.0101	5062 CT00513 CT	QUINEBAUG	LOW	NO	CONNECTICUT	CT-02	WINDHAM	BROOKLYN		QUINEBAUG RIVER	HYDROELECTRIC	GRAVITY	1865	14	340	250	3640	QUINEBAUG PARTNERSHIP
5062.0201	5062 CT00550 CT	FIVE MILE POND	SIGNIFICANT	YES	CONNECTICUT	CT-02	WINDHAM	KILLINGLY		FIVE MILE RIVER	HYDROELECTRIC	GRAVITY	1855	17	312	145	5283	OLINERAUG PARTNERSHIP
5073.0101	5073 ME83016 ME	BENTON FALLS	LOW	NO	MAINE	ME-01	KENNEBEC	BENTON FALLS	1	SEBASTICOOK RIVER	HYDROELECTRIC	GRAVITY	1987	27	1536	500	23000	WHITMAN, E. & BENTON FALLS
5274.0101	5274 NH00059 NH	SQUAM LAKE	SIGNIFICANT	YES	NEW HAMPSHIRE	NH-02	GRAFTON	ASHLAND	1	SQUAM RIVER	HYDROELECTRIC	GRAVITY	1856	16	53000	100	1,470	NH DEPT. OF ENVIR. SERV W
5307.0101	5307 NH00069 NH	WOODSVILLE	LOW	NO	NEW HAMPSHIRE	NH-02	GRAFTON	HAVERHILL		AMMONOOSUC RIVER	HYDROELECTRIC	GRAVITY	1827	23	280	450	18500	
5362.0201	5362 ME83017 ME	KESSLEN	LOW	NO	MAINE	ME-01	YORK	KENNEBLINK		MOUSAM RIVER	HYDROELECTRIC	GRAVITY	1954	18	351	140		KENNEBUNK LIGHT & POWER D
5362,0301	5362 ME83018 ME	TWINE MILL	LOW	NO	MAINE	ME-01	YORK	KENNEBUNK	3	MOUSAM RIVER	HYDROELECTRIC	GRAVITY	1980	18	146	180		KENNEBUNKLIGHT & POWER D
5362.0401	5362 ME83019 ME	DANE PERKINS	LOW	NO	MAINE	ME-01	YORK	KENNEBUNK		MOUSAM RIVER	HYDROELECTRIC	GRAVITY	1979	12	240	65		KENNEBUNK LIGHT & POWER C
5379.0101	5379 NH00020 NH	HADLEY FALLS	LOW	NO		NH-01	HILLSBOROUGH	GOFFSTOWN		PISCATAQUOG RIVER	HYDROBLECTRIC	GRAVITY	1922	20	270	230		NH DEPT. OF ENVIR. SERV W.
5399.0101	5399 ME00095 ME	NEW MILLS	HGH		MAINE	ME-01	KENNEBEC	GARDINER	1	COBBOSSEECONTEE STF	NUROELECTRIC	GRAVITY	1885	21	20360	167	106	
5613.0101	5613 ME00156 ME	BROWINS MILL	LOW	NO	MAINE	ME-02	PISCATAQUIS	DOVER - FOXCROFT	L	PISCATAOUIS RIVER	HYDROELECTRIC	BUTTRESS	1856	22	78	265		DOVER - FOXOROFT, TOWN OF
5735.0101	5735 NH00204 NH	HOPKINTON	LOW	NO	and the second s	NH-02	MERRMACK	HOPKINTON		CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1890	10	820	325		HOPKINTON, TOWN OF
5824.0101	5824 MA00106 MA	NORTH VILLAGE POND	LOW	NO	A CONTRACT OF A	MA-02	WORCESTER	WEBSTER		FRENCHRIVER	HYDROELECTRIC	GRAVITY	1914	13	324	168		WEBSTER HYDRO ELECTRIC O
5912.0101	5912 ME00157 ME	UPPERDAM	LOW		MAINE	ME-02	PISCATAQUIS	DOVER - FOXCROFT		PISCATAQUIS RIVER	HYDROBLECTRIC	GRAVITY						
6066.0103	6066 CT83010 CT	DERBY CANAL WEIR	LOW		CONNECTICUT			DUVERSTOACHOFT					1908	12	300	182		DOVER - FOXCROFT, TOWN O
6066.0101	6066 CT00026 CT	LAKE HOUSATONIC				CT-05	NEW HAVEN	-		HOUSATONIC RIVER	HYDROELECTRIC	GRAVITY	1870	10	4400	60		MCCALLUM ENTERPRISES I, L
			HGH		CONNECTICUT	CT-05	FAIRFIELD	DEFIEY		HOUSATONIC RIVER	HYDHOBLECTRIC	GRAVITY	1870	25	4400	850		MCCALLUM ENTERPRISES I, L
6132.0101	6132 ME00580 ME	WEST WINTERPORT	LOW		MAINE	ME-02	WALDO	FRANKFORT		MARSH STREAM	HYDROELECTRIC	GRAVITY	1948	12	125	105		JONES, JOHN C.
6240.0101	6240 NH00549 NH	WATSON	LOW		NEW HAMPSHIRE	NH-01	STRAFFORD	DOVER		COCHECO RIVER	HYDROELECTRIC	GRAVITY	1900	12	560	290		WATSON ASSOCIATES
6338.0101	6338 NH00120 NH	PITTSFIELD MILL	HCH		NEWHAMPSHIRE	NH-01	MERRIMACK	PITTSFIELD		SUNCOOK RIVER	HYDROELECTRIC	GRAVITY	1921	22	572	422		NH DEPT. OF ENVIR. SERV W
6440.0101	6440 NH00216 NH	LAKEPORT	LOW	NO	NEWHAMPSHIRE	NH-01	BELKNAP	LACONIA		WINNIPESAUKEE PIVER	HYDROELECTRIC	GRAVITY	1958	10	208000	225		NH DEPT. OF ENVIR. SERV W
6522.0101	6522 MA00715 MA	CHCOPEE	LOW	NO	MASSACHUSETTS	MA-02	HAMPDEN	CHICOPEE		CHICOPEE AIVER	HYDHOELECTRIC	GRAVITY	1898	10	450	314	24800	CHICOPEE, CITY OF
6597.0301	6597 NH00250 NH	PERCE	LOW	NO	NEW HAMPSHIPE	NH-02	HILLSBOROUGH	BENNINGTON		CONTOOCOOK RIVER	HYDROELECTRIC	BUTTRESS	1921	12	51	420	13400	MONADNOCK PAPER MILLS, IN
6597.0401	6597 NH00251 NH	PAPERMIL	LOW	NO	NEW HAMPSHIRE	NH-02	HILLSBOROUGH	BENNINGTON		CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1922	9	50	280	13400	MONADNOCK PAPER MILLS, IN
6597.0101	6597 NH00248 NH	POWDER MILL	LOW	ND	NEW HAMPSHIRE	NH-02	HILLSBORDUGH	BENNINGTON		CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1924	21	8600	366	18200	MONADNOCK PAPER MILLS, IN
6597.0201	6597 NH00249 NH	MONADNOCK	LOW	NO	NEW HAMPSHIRE	NH-02	HILLSBOROUGH	BENNINGTON		CONTOOCOOK RIVER	HYDROELECTRIC	GRAVITY	1923	22	240	500	13400	MONADNOCK PAPER MILLS, IN
6618.0101	6618 ME00149 ME	FHANKFORT	LOW	NO	MAINE	ME-02	WALDO	FRANKFORT	1	MARSH STREAM	HYDROELECTRIC	GRAVITY	1840	14	240	250	2200	FRANKFORT, TOWN OF
6689.0101	6689 NH83023 NH	PENACOOK UPPER FALL	LOW	NO	NEW HAMPSHURE	NH-02	MERRIMACK	BOGCAWEN		CONTOCCOCK RIVER	HYDROELECTRIC	GRAVITY	1987	16	114	267		BRIAR HYDRO ASSOCIATES
6752.0101	6752 NH00465 NH	AVERY	LOW	NO	NEW HAMPSHIRE	NH-01	BELKNAP	LACONIA		WINNIPESAUKEE RMER	HYDROELECTRIC	GRAVITY	1947	13	5500	114		NH DEPT. OF ENMR. SERV W
6756.0101	6756 NH00139 NH	OPM	SIGNIFICANT		NEWHAMPSHIRE	NH-02	SULLIVAN	CLAREMONT	5	SUGAR RIVER	HYDROELECTRIC	GRAVITY	1921	29	36	145		SWEETWATER HYDROELECTR
7148.0101	7148 MA00126 MA	ASSABET	HIGH	YES		MA-05	MIDDLESEX	ACTON		ASSABET RIVER	HYDROELECTRIC	GRAVITY	1921	13	122	478		A & D HYDRO, INC.
7189.0101	7189 ME00266 ME	GREENLAKE	LOW		MAINE	ME-02	HANCOCK	ELLSWORTH		REEDSBROOK	HYDROELECTRIC	GRAVITY	1911	. 8	113000	273		GREEN LAKE WATER POWER C
7254.0101	7254 MA00114 MA		LOW	NO		MA-02	WORCESTER	THOMPSON, CT.		QUINEBAUG RIVER	HYDROELECTRIC	GRAVITY	1919	17	240	259		A & D HYDRO, INC.
7473.0101	7473 ME00320 ME	GILMAN STREAM	LOW	NO	MAINE	ME-02	SOMERSET	NEW PORTLAND	····· •	GILMAN STREAM	HYDROELECTRIC	GRAVITY	1911	8	2785	228		GILMAN STREAM HYDRO
7528.0101	7528 NH00129 NH	CANAAN	LOW			NH-02	COOS	STEWARTSTOWN	• • • • • • • • • •	CONNECTIOUT RIVER	HYDROELECTRIC	GRAVITY	1943	18	400			
7590.0101	7590 NH00121 NH	JACKSON MILLS	SIGNIFICANT	YES								GRAVITY				275		PUBLIC SERVICE COMPANY OF
7887.0101	7887 NH00104 NH	MINNEWAWA	HIGH			NH-02	HILSBOROUGH	NASHUA	····	NASHUA RIVER	HYDROELECTRIC		1920	32	470	330		NASHUA HYDRO ASSOC.
					NEWHAMPSHIRE	NH-02	CHESHFE	MARLBOROUGH		MINNEWAWA BROOK	HYDROELECTRIC	ARCH	1932	63	160	265		MARLEOROUGH HYDRO ASSOC
7890.0101	7890 NH00803 NH	WENDELL	LOW	NO	the second se	NH-02	SULLIVAN	NEWPORT		SUGAR RIVER	HYDROELECTRIC	GRAVITY	1924	9	67	56		NEW HAMPSHIRE FISH & GAME
7920.0101	7920 NH00355 NH	WATERLOOM FALLS	LOW	NO	NEW HAMPSHIRE	NH-02	HALLSBOIROUGH	GREENVILLE	_ 3	SOUHEGAN RIVER	HYDROELECTRIC	GRAVITY	1980	18	925	205		GREENWOOD, ALDEN T.
7921,0101	7921 NH00041 NH	OTIS FALLS	LOW	NO	NEW HAMPSHIRE	NH-02	HILLSBOROUGH	GREENVILLE		SOUHEGAN RIVER	HYDROELECTRIC	GRAVITY	1982	27	97	150		GREENWOOD, ALDEN T.
8012.0101	8012 MA00634 MA	HUNTS POND	LOW	ND		MA-01	WORCESTER	WINCHENDON	· ·	MILLERS RIVER	HYDROELECTRIC	GRAVITY	1936	15	133	184		BEHRENS ENERGY SYSTEMS, #
8093.0101	8093 MA00178 MA	METHUEN FALLS	HGH	YES		MA-05	ESSEX	METHLEN		SPICKETT RIVER	HYDROELECTRIC	GRAVITY	1895	23	210	188	1800	METHUEN FALLS HYDRO ELECT
8277.0101	8277 ME00009 ME	OTIS	LOW	NO	MAINE	ME-02	FRANKLIN	LIVERMORE FALLS		ANDROSCOGGIN RIVER	HYDROELECTRIC	GRAVITY	1898	17	2620	840	68000	OTIS HYDROELECTRIC CO.
8405.0101	8405 NH00159 NH	GLEN ROAD	SIGNIFICANT	YES	NEW HAMPSHIRE	NH-02	GRAFTON	LEBANON	·	MASCOMA RIVER	HYDROELECTRIC	GRAVITY	1988	16	28	175	8600	MASCOMA HYDRO CORP.
8417.0101	8417 ME00187 ME	BRIDGESTREET	LOW	NO	MAINE	ME-01	CUMBERLAND	YARMOUTH		ROYAL RIVER	HYDROELECTRIC	GRAVITY	1873	8	106	224	4000	YARMOUTH, TOWN OF
8450.0101	8450 ME83024 ME	STONY BROOK	LOW	NO	MAINE	ME-02	OXFORD			STONY BROOK	HYDROELECTRIC	GRAVITY	1976	12	108	100	500	SMALL HYDRO EAST
8640.0101	8640 ME00277 ME	SEABRIGHT	HIGH	YES	MAINE	ME-01	KNOX	CAMOEN	1	MEGUNTICOOK RIVER	HYDROELECTRIC	GRAVITY	1900	22	1290	372		SEABRIGHT HYDRO, INC.
B736.0101	8736 ME00110 ME	PIONEER	LOW	NO	MAINE	ME-02	SOMERSET	PITTSFIELD		WEST BRANCH SEBASTIC	HYDROELECTRIC	GRAVITY	1890	12	388	170		PITTSFIELD, TOWN OF
8794.0101	8794 CT00399 CT	RIMMON POND	LOW	NO	· blances - serve - serve - server - se	CT-05	NEW HAVEN	SEYMOUR		NAUGATUCK RIVER	HYDROELECTRIC	GRAVITY	1850	17	118	280		SOUTHERN NEW HAMPSHIRE H
8895.0101	8895 MA00854 MA	TANNERY POND	LOW	NO			WORCESTER	WINCHENDON		MILLERS RIVER	HYDROELECTRIC	GRAVITY	1936	10	81	248		BEHRENS ENERGY SYSTEMS, I
8924.0101	8924 NH00312 NH	MCLANE	LOW	NO		NH-02	HILLSBOROUGH	MILFORD	•••••	SOUHEGAN RIVER	HYDROELECTRIC	GRAVITY	1929	18	83	230		MILFORD, TOWN OF
9100.0101	9100 MA00942 MA	RIVERDALE MILLS	LOW	NO			WORDESTER	NORTHBRIDGE		BLACKSTONE RIVER	HYDROELECTRIC	GRAVITY	1957	10	173			KNOTT, JAMES M.
9282.0101	9282 NH00258 NH	HILLSBOROUGH MILL	LOW	NO	the start warm to an an an in the	NH-02	HELLSBOROUGH	WILTON		SOUHEGAN RIVER	HYDROELECTRIC	GRAVITY	1957	27	98	152		MACDONALD, WINSLOW H.
9340.0201	9340 ME00045 ME	UPPER KEZAR FALLS #1		NO				KEZAR FALLS	·····	OSSPEERVER	HYDROBLECTRIC	GRAVITY	1925	11	145	200		
9411.0101	9411 ME00295 ME			NO	1 mm	117.00	YORK			\$						196		CENTRAL MAINE POWER CO.
		BISCOE FALLS	LOW		MAINE	ME-02	OXFORD	SOUTH PARIS		LITTLE ANDROSCOGGIN		GRAVITY	1986	15	210	115		JOHN CROUCH JR. & SONS
0163.0101	10163 MA00932 MA	CRESTICON UPPER	LOW	NO			WORCESTER	ATHOL		MILLERS RIVER	HYDROELECTRIC	GRAVITY	1931	12	457	280		L. P. ATHOL CORP.
0675.0101	10675 MA00721 MA	DWIGHT	LOW		MASSACHUSETTS		HAMPDEN	CHICOPEE	1	CHICOPEE RIVER	HYDROELECTRIC	GRAVITY	1860	2.4	423	327		WESTERN MASSACHUSETTS E
10677.0101	10677 MA00724 MA	PUTTS BRIDGE	LOW		MASSACHUSETTS		HAMPDEN	LUDLOW		CHICOPEE RIVER	HYDROELECTRIC	GRAVITY	1918	22	1090	223		WESTERN MASSACHUSETTS E
0678.0101	10678 MA00722 MA	INDIAN ORCHARD	HGH		MASSACHUSETTS	MA-02	HAMPOEN	SPRINGFIELD	1	CHICOPLE RIVER	HYDROELECTRIC	GRAVITY	1846	28	1800	401	71000	WESTERN MASSACHUSETTS E
0898.0101	10898 NH00140 NH	COY PAPER MILL	SIGNIFICANT	YES	NEW HAMPSHIRE	NH-02	SULLIVAN	CLAREMONT		SUGAR RIVER	HYDROELECTRIC	GRAVITY	1922	33	300	314	14000	SWEETWATER HYDROELECTR
0981.0101	10981 ME83029 ME	BASIN MILLS	LOW	NO	MAINE	ME-02	PENOBSCOT	ORONO		PENOESCOT RIVER	HYDROELECTRIC	GRAVITY		18	6600	1650		BANGOR HYDRO-ELECTRIC CO.
11058.0101	11058 MA83026 MA	FITCHBURG PAPER MILL	SIGNIFICANT	NO	MASSACHUSETTS	MA-01	WORCESTER	FTICHBURG		NORTH NASHUA RIVER	HYDROELECTRIC	GRAVITY	1907	10	3	200		PWA ROLAND DECOR, INC.
11132.0101	11132 ME00129 ME	EUSTIS	LOW	NO		ME-02	FRANKLIN	EUSTIS		NORTH BRANCH DEAD R		GRAVITY	1952	17	720	240		CONSOLIDATED HYDRO MAINE
	11142 ME00183 ME	ESTES LAKE	HGH	YES	MAINE	ME-01	YORK	KENNEBLINK	9	MOUSAM RIVER	HYDROELECTRIC	GRAVITY	1906	40	5550	726	9500	CONSOLIDATED HYDRO MAINE

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ERC#	FERC# NID #	STATE	DAM_NAME	HAZARD	EAP	STATE NAME	CONG_DIST	COUNTY	NEAR_CITY DIST_	CIT AVER	PRM_PURPOSE	NID_DAMTYP	YEAR CND	HEIGHTIN	ID_STOR I	DAM LENGTH M	MX DISCH OWNER
11143.0101	11143 CT0057	9 CT	BRUNSWICK	LOW	NO	CONNECTICUT	CT-02	WINDHAM	MOOSUP	1 MOOSUP RIVER	HYDROELECTRIC	GRAVITY	1891	19	258	160	3960 GLEN FALLS REALTY PAR
11163.0101	11163 NH0036	5 NH	SOUTH BERWICK	LOW	NO	NEW HAMPSHIRE		STRAFFORD	DOVER	SALMON FALLS RIVER	HYDROELECTRIC	GRAVITY	1916	18	641	290	14747 CONSOLIDATED HYDRO
11168.0103	11168 CT8302	4 CT	DAYVILLE EMERGENCY	LOW	NO	CONNECTIOUT	CT-02	WINDHAM	DAYVILLE	FIVE MILE RIVER	HYDROELECTRIC	GRAVITY	1925	8	110	37	WILLIAM PRYM, INC.
11313.0101	11313 NH006	1 NH	APTHORP	SIGNIFICANT	YES	NEW HAMPSHIRE	NH-02	GRAFTON	LITTLETON	AMMONOOSUC RIVER	HYDROELECTRIC	GRAVITY	1936	24	280	235	14800 WHITE MOUNTAIN HYDRO
11365.0101	11365 ME000	8 ME	SWANS FALLS	LOW	NO	MAINE	ME-02	OXFORD	FRYEBURG	2 SACO RIVER	HYDROELECTRIC	GRAVITY	1923	10	535	63D	50800 SWANS FALLS CORP.
11433.0101	11433 ME001	9 ME	SANDY RIVER	LOW	NO	MAINE	ME-02	SOMERSET	NORRIDGEWOCK, STARKS	SANDY RIVER	HYDROELECTRIC	GRAVITY	1902	18	1400	400	12000 MADISON, TOWN OF, DE
11472.0101	11472 ME0010	9 ME	BURNHAM	SIGNIFICANT	YES	MAINE		WALDO	BURNHAM	2 SEBASTICOOK RIVER	HYDROELECTRIC	BUTTRESS	1929	32	1904	615	12200 CONSOLIDATED HYDRO
11475.0101	11475 VT002	4 VT	CARVER FALLS	LOW	NO	VERMONT		RUTLAND	WHITEHALL, NY	POULTNEY RIVER	HYDROELECTRIC	GRAVITY	1894	34	105	455	6900 CENTRAL VERMONT PUE
11478.0201	11478 VT002	2 VT	SUCKER BROOK DIVERS	SIGNIFICANT	YES	VERMONT	VT-01	ADDISON	LAKE DUNMORE	3 SUCKER BROOK	HYDROELECTRIC	GRAVITY	1917	36	20	725	4180 CENTRAL VERMONT PUE
11478.0301	11478 VT001	6 VT	SUGAR HILL	HIGH	YES	VERMONT	VT-01	ADDISON	LAKE DUNMORE	5 SUCKER BROOK	HYDROELECTRIC	GRAVITY	1931	61	1861	855	3032 CENTRAL VERMONT PUE
11478.0101	11478 VT0018	6 VT	SILVER LAKE	HIGH	YES	VERMONT	VT-01	ADDISON	LAKE DUNMORE	3 SUCKER BROOK	HYDROELECTRIC	BUTTRESS	1917	30	4445	284	550 CENTRAL VERMONT PUE
11482.0101	11482 ME003	9 ME	MECHANIC FALLS	LOW	NO	MAINE	ME-02	ANDROSCOGGIN	MECHANIC FALLS	LITTLE ANDROSCOGGIN I	HYDROELECTRIC	GRAVITY	1866	15	240	172	1000 CONSOLIDATED HYDRO
11547,0101	11547 CT0167	7 CT	HALE	LOW	NO	CONNECTICUT	CT-02	WINDHAM	PUTNAM	QUINEBAUG RIVER	HYDROELECTRIC	GRAVITY	1965	23	65	100	SUMMIT HYDROPOWER

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Puesto (Trutz) Requerenses Puesto (Trutz) Ruder (O e Ruyersonalen uizo Erenso Puesto (Trutz) Ruyersonalen (O DO Erenso Puesto (Trutz) Ruger (O DO Erenso	DOFFERC NO	£	e So	37	1300	2000	134	300 2000 134 429.C 228 34828 YSS 33 51 7 10111 200 3484 YSS	228	34828 YES		2	C DOEFERC	0 35064 DOEFERC		7		đ	9015
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PUBLIC UTILITY PRB	DOEHERC NO	r	HEONEG	25	600	2000	263	1595 U	26	34562 YBS	DOEFEIIC	DOCHER	C DOEHBAC	35004 DOERERC	C 35004	4 -70.55	43.61333	23	23031
PUBLIC UTILITY PSB	DOETERC NO	Ŧ	HEONE	75	2840	6340	136	700 C	9	34772 YES	DOEFERC	DOEFER	C DOEFEDC	35004 DOEFERC	C 35004	4 -73.16333	44.63833	50	50007
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FUBLIC UTURY DEP	DOEFERC NO	£	CEONFG	23	226	280	18	420 U		300	4514 YES	DOEHERC	DOEREHC	DOEFEHC	35004 DOERER	0	15004 -72.03333		0	3300
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PUB CENTY	17	Se se se se se se se se se se se se se se	CARGE	4	¥ C ¥	146	10	135 0		1 7 3		NGEED.	New State	D.C.C.C.C.	SEAD A POET			à., .		2002
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		C 3	2 4	- C	07	2	<u> </u>	0 151	-	4 C	04844 YES	Die rent	Die Ference	Nerence Sectors	35004 DOCHEN.		35004 -71.92667	÷÷-		1055
	-		220	א ה ע	42	5	2.5	D 707	ŧ	2 0	148// 10	of the second	METHON I	Mereto -	33004 LAET	-		4		022
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	-r.,		5 6	8	200	400	207	381 U	-	140	34827 YES	COLLEGE COLLEGE	DOE HENC	DCFHHC	35004 DOEHHK		4	-		0066
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PHIVALE MALDERT OF ENVIRONMENTAL DOCHERC			1	12	60	108	12	2 0	22	34471 YES	DOEHERC	DOEFEHC	DOEFERC	35004 DOEFERC	35004	-70.76667	44.51667	23
	DOCETERC VES	HARC	Webc	12	250	388	30	320 U	160	34512 YES	DOEHERC	DOEFERC	DOEHERC	35004 DOERERC	35004	-69.38167	44.78667	23
PRIVATE	- the second second second second second second second second second second second second second second second s		MSPG	10	89	173	12	142 C	142	34666 NO	DOEPERC	DOEFERC	DOEFEHC	35004 DOEFERC	35004	-71.64	42.13833	25
PRIVATE			WSPG	Ŧ	130	145	10	416 U	176	34564 NO	DOFFERIC	DOEFERC	DOEHEHC	35004 DOEFERC	35004	-70.89187	43 80687	23
				22	715 1	060	65	686 U	200	34969 NO	DOEFEINC	DOEFERC	DOEFFIC	35004 DOEFERC	35004	-72.48333	42.15667	25
PRIVATE MA DEPT OF ENVIRONMENTAL DOCHERC		HARC	1	33	150	300	30	270 U	143	34877 YES	DOEFERC	DOEFERC	DOCHERC	35004 DOEHERC	35004	-72.37667	43.39	33
HIVAIE		ļ		18	5000 5	600	325	7800 U	1640	34087 NO	DOEFFIERC	DOEFERC	DOEFFIC	35004 DOEFERC	35004	-68.7	44.83333	23
	1		1	18	525	641	58	_235 U	220	34288 YES	SOE FEE	DOETERC	DEFERC		35004	-70.81167	43.22667	33
		1		24	210	280	20	205 U	180	34514 NO	DOEFERC	DOEFERC	DCFFERC	35004 DOGHERC	35004	-71.74667	44.30833	33
			1	34	75	105	10	184 C	455	34493 ND	DOERERC	DOEFERC	DOEHENC	35004 DOEFERC	35004	-73.30667	43.62667	50
;	DOEFEHC		MSST	8 14	2590		625	57 C	52	34421 NO	DOEFFIC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-69.52833	44.06167	23
	CENTIC		9.4SW	38	8600 22	-	930	3894 C	507	34514 YES	DOCIENC	DOEFERC	DOEFFIC	35004 DOEFERC	35004		44.765	23
	T.		CNISH	51	8600 22		930	3894 C	245		DOEFERC	DOEFERC	DOEHENC	35004 DOEFERC	35004	-69.72167	44.765	23
			SCO-NO	30	3500 4	4800	390	7800 U	160	34487 NO	DOEHENC	DOEFERC	DOEATING	35004 DOEFERC	35004	-68.70167	44.83167	23
		Ŧ	9 .5 5	15	812	300	140	2300 U	617	34843 NO	DOEHENC	DOCHERIC	DOEFERC	35004 DOEFERC	35004	-68.665	44.86333	23
PRIVATE			WSPG	21	72	82	5	N 81		34423 NO	DOFFIEIC	DOFFERIC	DOEFFERC	35004 DOERERC	35004	-69.99667	44.41667	23
PRIVATE		Ŧ	CNOBPG	23	1300	663	86	444 U	272	34862 YES	DOEFERC	DOEHERC	DOEHENC	35004 DOEFERC	35004	-70.45	43.80167	23
PHIVALE		Ŧ	MSONFG	13	2320 5	440	347	1563 U	339	34856 YES	DOEFERC	DOEFERIC	DOEFERC	35004 DOEFERC	35004	-70.61167	43.68667	23
VE	1.5	I.	88 S	25	25		3	53 U	150	34862 NO	DOFFERO	DOCIENC	DOETERC	35004 DOEHERC	35004	-71.185	44.12833	33
PHIVATE	DOCHENC	E	CAPB CAPB	59 5	5000 7.9	800 3	3100	3375 C	521	34968 YES	DOGREPIC	DOEFFIC	DOEFERC	35004 DOEFERC	35004	-72.30333	43.66667	33
PRIVATE	DOEHERO	н	BB	170 4	6800 57	700	093	1635 U	801	34968 YES	DOEHERC	DOEFERC	DOEFERC	35004 DOERERC	35004	-72.00167	44.325	33
PRIVATE	DOERENC NO	Ŧ	MEONPG	144 20	0000 223	722 3	3490	1600 C	373	34968 NO	DOEFERC	DOEFERC	DOEFFINC	35004 DOCPERC	35004	-71.88167	44.33667	33
PRIVATE	DOEFERC NO	£	OPGE	165 7	2250 108	08000 3	3666	1355 C	272	34858 YES	DOEHERC	DOEFERC	DOEFFERC		35004	-69.86667	45.46167	23
	DOERERC NO	r	ONG	40	6000 11		740	690,0	387	34772 YES	DOERERC	DOEHENC	DOCHERC		35004	-73.11333	44 64187	50
LOCAL GOVT RHODE ISLAND DEM	DOEFERC NO	¥	ore	86	5100 56	100 2	862	2863 C	370	34968 YES	DOEHERC	DOEFERC	DOEFFERC		35004	10 02-	44 15333	0.0
PRIVATE MA DEPT OF ENVIRONMENTAL DOE HERC	ITAL DOEFERC NO	I	MSPG	48	467	1067	75	404 U	241	34837 NO	DOCETERIC	DOFIERC	DOF FEEDC		35004	70 746	40.62	0
PRIVATE	DOEHERC NO		MSOT	24	1950 2	970	128	21110	366		DOFFERC	DOF FEED	DEFERC		35004	-68 57667	45 60867	2.0
PRIVATE RHODE ISLAND DEM	DOERERC NO		MSPG	56	1966 56	290	048		521		COFFECT	Certification of the second	DEFENC.		35004	29908 99	10000-01 AV	000
шi	DOEFERC NO	Ŧ	EPG8M	27	8100 14	520 1	344	1690 C	10.86	34963 ND	DOFFER	DEFER	DCHHC.		F0026	58 73	45.63839	200
STATE NEW HAMPSHIRE WPD	DOEFFERC NO	£	SARG	20 4	5370 87	670 8	8640	122 C	115	34961 NO	DOFFERC	DOFFERC	DOFFERC		35004	66 73333	45 74167	60
PRIVATE	DOEFERC NO	Ξ	MSPG	16 18	7100 21447	0	8250	417 C	45	34933 YES	DOEHERC	DOFFERC	DOFFERC		35004	-67 42833	45 56833	0.0
PUBLIC UTLITY	DOFFERC NO	I	880	45	5785 69	100	1664	3308 C	657	34860 NO	DOEFERC	DOEFERC	DOEHERC		35004	-58.41	45.57	23
PRIVATE RHODE ISLAND DEM	DOE FERC NO	r	NS-C	75 2	5250 33	500	488	1622 C	495	34856 YES	DOEFERC	DOEFERC	DOEFERC		35004	-70 56	43 575	6
PRIVATE	DOEFERC NO	I	MSPG	67	2320	440	347	1563 N	164	34856 YES	DEFERC	DEFER	CHHOU I	SEADA INFERENC	2500A	70 61167	12 50627	
PRIVATE MA DEPT OF ENVIRONMENTAL	DOETERC		MSPG	30	2300 13	200	131	1679/11	100	34669 100	NOC DELID						10000.04	
	UCE HER	-	MISCHOT	72 74	220 0000	00	01000	1007							10000	2000.07-	10000.04	3
	1												WE'LE'L	Sourt Horen	40045	P	40.48333	23
1				-	50 0000	1004	1077		204		2442			35004 DOE HENC	35004	-69.87333	45.35	53
	T		HT-S	20	2 002	000	40	346.U	652		DOEHERC	DOFFERIC	DOEFERC	35004 DOEFERC	35004	-72.82667	42.15667	25
1			ore ore	601 11	7800 159	000	6838	526 C	4291	34549 NO	DOFIERC	DOEFERIC	DEFENC	35004 DOEFERC	35004	-69.73333	45.91167	23
		r	D-SM	20 108	0000 1400	0	4200	1268 C	484	34627 YES	DOEABAC	DOEFFIC	DOFTENC	35004 DOEPERC	35004	-69.715	45.58667	23
SIAIE NEW HANFSHIRE WRD			SPR0	18 108	0000 140000	0	74200	1268 C	50	34627 ND	DOEFERC	DOCFERIC	DOEFFINC	35004 DOEFERC	35004	-69.745	45.65167	23
	- T	•	WSFG	43 14	4670 145	45000 12	200	452 C	70	34844 NO	DOEFERC	DEFER	DOEFERC	35004 DOERERC	35004	-58.44167	44.59167	23
STATE NEW HAMPSHIRE WRD	DOEFERC NO	Ŧ	OPE	44	2900 3	337	190	443 U	150	34864 YES	DOEPERC	DOEHENC	DOEFERC	35004 DOEFERC	35004	-70.45333	43.78	23
PRIVATE	DOCFEERC NO	I	8000	60	3600 4	695	138	200 U	472	34925 YES	DOEFERC	DOFTERC	DOFFER	35004 DOFFERC	35004	.71 56833	43 01833	86
PRIVATE	DOEFFERC NO	Ξ	CNOT	20	115	260	23	104 U	310	34871 YES	DOFFERC	DOFFERC	DOFFERC	35004 DOFER	35004	72 045	19 38667	10
PRIVATE	DOEFERC	L.	CNOT	27	1 255	F36	8.8	Sen C	.04	SARDE NO						000		
PRIVATE	÷	: 1	Service Se			000	-		-	0407040					40045	0.60-	44.56667	23
LOCAL GOVT NEW HAMPSHIPE WIPD		-	MSCHER	00	212	070		11 001	0 14 4 4	34044 TED			Merenco Merenco		35004	528.17-	42.993331	23
	2		Cardo	000	1020	000	1			211 110 10 10 10					10045		43	33
	-					204) i			2404Z 1E3	ne an		T	30004 INCLUSION	35004	_	44.21667	23
1	1	-			10/0			200 5	8/1	34609 NU				36004 DOEFEHC	35004		45.21833	23
DDhivite		-	- MORM	61	904	CP O	150	445 U	455	34564 NO	DOEFERC	DOETHIC	DOCINE	35004 DOEFERC	35004	-70.98333	44.03667	23
t	· · ·	-	5,50	9	860	000	210	1494 C	205	34920 YES	DOEFERC	DOEFERC	DEFE	35004 DOEHERC	35004	-71.115	44.405	33
		:	CUMBER		2550 7	300	850		183	34947 YES	DOEFEHC	DOEHENC	DEFERC	35004 DOEFERC	35004	69.38667	44.795	23
	÷1.,		PHW PH	63	120	160	2	23 U	40	34948 YES	DOEHERC	DOEFEIIC	DEFERC		35004	-72.18	42.91667	33
	· · · ·		WSCNOT	20	1800 3	120	120	784 U	131		DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004		41.675	61
PHUVALE INEW HAVE SPHERE WHO		-	CMARG COMARG	36	6000 88	2 006	550				DOEHENC	DOETERC	DOEFERC	35004 DOEHERC	35004		42.21333	25
			PHO 0	10	4500	500	664	0	15	34927 NO	DOEFERC	DOEFERC	D06FBHC	35004 DOEFERC	35004	-71.32556	42.64694	25
E.	MERTER NO	-	2	N	4500	500	664		65	34927 NO	DOEHENC	DOEHENC	DOFFERC	35004 DOEFERC	35004	-71.31369	42.65139	52
Š	1	1	C	8	93	110	31			34283	DOFTEHC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.89167	41,85	6
PHIVALE NEW HAMPSHIPE WIED DOC FLAC		1	OWER	22	10	76	4	362 U	160	34893 YES	DOEFERC	DOEFFIC	DOEHENC	35004 DOERERC	35004	-69.23	45.18	23
			1000	50	4500	500	664		78	34927 NO	DOEFERC	000000	DOEFERC		35004	-71.30833	42.64333	25
PRIVATE		1	- Change		0800 33	280	264	428 C	160	34816 YES	DOEFERC	DOEFERC	DOEFERC		35004	-71.535	43.47333	33
COAL COULT NEW DAMOCHIDE WOOL	Menter N		P-MD	0	P.0	22	2	250 C	140	34570 YES	DOEFFINC	DOEFERS	DOETHIC	35004 DOEFERC	35004			33
		r i	WALNE	18	27001													
			TOPE	P			250	2427 U	550	34457 YES	DOEFEHC	DOE HENC	DOEFERC	35004 DOEFERC	35004	-71.5	43.16867	33

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OWN TYPE	STATE AGCY	FED AGO	V NON	EED PLEADER	DAM TYPE	drive HORL	NODU STOC	AAY PTOP		DOARI ADEA	SPILL_TYPE SPILL_W	onuli						[
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC	NO	H	CNPG	CLANNE (TECHNIC	1600	2800	200			15	34969 NO	DOEFERC	DOE FERC	DOE FERC	SUPP_DATE_SOURC_AGC 35004 DOEFERC					
LOCAL GOV'T	NEW HAMPSHIRE WAD	DOEFERC	NO	н	CNPG	9	1600	2800	200	2901		28	34969 NO	DOEFERC	DOEFERC	DOE FERC	· · · · · · · · · · · · · · · · · · ·	35004	-70.16667		23	
PRIVATE	MA DEPT OF ENVIRONMENTA		NO	н	MSPG	24		120	3	220		100	34857 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOE FERC	35004	-70.16667		23	
PRIVATE	0 9 7	DOEFERC	NO	н	MSPG	14		56	7	503		263	34863 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEHERC	35004	-69.78333			
PRIVATE	D€P	DOEFERC	NO	н	IMSPG	20		2938	242	405		145	34900 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC 35004 DOEFERC	35004	-70.42		23	
PRIVATE	· · · · · · · · · · · · · · · · · · ·	DOE FERC	*****	н	CNPGRE	14		3480	246	650		473	34458 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004 35004	-71.50667	42.74833		3301
STATE	NEW HAMPSHIRE WRD	DOEFERC	NO	HFP	CNMSPG	36		464	32	220		178	34935 YES	DOEFERC	DOEFERC	DOEFERC						
LOCAL GOVT	NEW HAMPSHIRE WRD	DOEFERC	NO	HS	OVPG	19		324	47	84		178	34871 YES	DOEPERC	DOEFERC	DOEFERC	35004 DOEFERC 35004 DOEFERC	35004	-70.86	43.26		
LOCAL GOVT		DOEFERC	NO	HB	CNPG	25		4400	320			675	34857 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-73.10333			
LOCAL GOVT		DOEFERC	NO	HR	CNPG	14		240	20			200	34422 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEPERC	35004	+68.87333	41.325		000
LOCAL GOVT		DOEFERC	NO	HR	ONPG	10		81	9			138	34872 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004 35004	-72.05333	44.61	23	
STATE	NEW HAMPSHIRE WRD	DOEFERC	NO	HPP	ONFG	15		210	21	76		65	34808 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC			4	the set of a set of a set of a set of a set of a set of a set of a set of a set of a set of a set of a set of a	
LOCAL GOVT		DOEFERIC	NO	HS	MSPG	10		3	1	58		160	34688 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOE FERC	35004	-70.51	44.22333	23	
LOCAL GOV'T		DOEFERC	NO	ΗP	MSONCE	15	and the second se	240	27			126	34598 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.85		25	
LOCAL GOVT	NEW HAMPSHIRE WRD	DOEFERC	NO	н	CNMSPG	14	· · · · · · · · · · · · · · · · · · ·	240	65	1250		350	34457 NO	DOEPERC	DOEFERC	DOEFERC	35004 DOEPERC	35004	-70.39167		23	
PRIVATE	MA DEPT OF ENVIRONMENTA		NO	in in	MSCNPG	15	+	75	20			310	34969 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004 35004	-72.05	41.59867	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
LOCAL GOV'T		DOEFERC	NO	HC	CNPG	12		406	58	140		103	34654 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC					
PRIVATE		DOEFERC	NO	ю	ONFG	8	107000	113000	2989	58		80	34422 NO	DOEFERC	DOEFERC	DOEFERC		35004	-70.93333			
PRIVATE	DEP	DOEFERC	NO	HC	MSCNPG	11		4180	405	2805		590	34422 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOE FERC 35004 DOE FERC	35004	-68.44333			
PRIVATE		DOEFERC	NO	н	CNPG	30		68900	2550	8309		010	34968 YES	DOEFERC	DOEFERC	DOERERC	· · · · · · · · · · · · · · · · · · ·	35004				
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC	NO	H	CNFG	20		68900	2550	8309		98	34968 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC 35004 DOEFERC	35004	-72.60167			
STATE	NEW HAMPSHIRE WRD	DOEFERC	NO	HRS	CNMSPG	18		68900	2550	8309		100	34968 NO	DOEFERC	DOEFERC	DOEPERC	35004 DOEFERC	35004	-72.6	42.2		
STATE	NEW HAMPSHIRE WRD	DOEFERC	NO	HFC	CNOT	26		68900	2550	8309		147	34968 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-72.6			
LOCAL GOVT		DOEFERC	NO	HOPA	MGPG	14		2800	200	2901		57	34969 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOE FERC	35004	-72.6			farmer and a second
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC	NO	HS	CECNPG	18		2800	200	2901		40	34969 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC		-70.5			
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC	NO	HS	ONPG	14		2800	200			15	34969 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004 35004	-70.16667		23	
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC		HS	CNPGRE	16		266	14	1703		275	34562 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-70.45187			
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC		HS	ONPOPE	36		750	25	207		32	34626 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC		-69.65333	der eine eine eine eine eine		
LOCAL GOVT		DOEFERC	NO	H	MSONPG	16		4500	664	3979		083	34926 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.33333		A statement of the statement	a subcash fadam cardy
PRIVATE	· · · · · · · · · · · · · · · · · · ·	DOEPERC	NO	H.	CNOT	16		4500	664		<u> </u>	003	34926 NO	DOEFERC	DOEFERC	DOEFERC	and the second s	· · · · · · · · · · · · · · · · · · ·				
STATE	NEW HAMPSHIRE WRD	DOEFERC	NO	HRP	CNMSPG	8	4500	4500	664		c	16	34927 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC 35004 DOEFERC	35004	-71.33194	42.64917 42.65558	25	
PRIVATE	NEW HAMPSHIRE WRO	DOEFERC	NO	HS	ONFG	15		4500	664		U	78	34927 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC		-71.31389			
PRIVATE	MA DEPT OF ENVIRONMENTA		NO	н	MSREOT	7	4500	4500	664		c	17	34927 NO	DOEFERC	DOEFERC	DOEFERC		35004				
PRIVATE		DOEFERC	NO	HPSFF	MSOT	39		19900	655	4450		920	34793 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC 35004 DOEFERC	35004 35004	-71.31	42.65558	25 25	
PRIVATE	MA DEPT OF ENVIRONMENTA		NO	н	CNPG	15		1800	70	19		920	34423 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-69.00667			
PRIVATE		DOEFERC	NO	н	OTON	15		270	16				34423 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOE FERC	35004	-69.00333	44.44	23	
PUBLIC UTILITY	NEW HAMPSHIRE WOD	DOEFERC	NO	H .	CNPG	12		50	13	244		102	34956 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-09.00333			
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC	NO	н	CNMSPG	30		530	45	73		110	34282 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.52167	4.1 Contract Constants		4400
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC	NO	H	CNVA	13		366	40	261		200	34969 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-/1.5210/	41.70667	44	4400
STATE	NEW HAMPSHIRE WRD	DOEFERC	NO	HAL	CNPG	11		180	26	473		140	34596 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.4	41.86667		4400
PRIVATE	NEW HAMPSHIRE WAD	DOEFERC	NO	н	ONFG	10	7	96	15			165	34596 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.39		44	4400
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC	ND	н	CNMSPG	18		145	10	And a second second second second		115	34753 NO	DOE FERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-72.23333		44	
PRIVATE	MA DEPT OF ENVIRONMENTA		NO	H H	ONFG	34		985	40			115	34753 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC			·····		
PRIVATE	MA DEPT OF ENVIRONMENTA		INC	H	MSPG	26		34	10	and the second second		77	34487 YES	DOEPERC	DOEFERC	DOEFERC	35004 DOEFERC	35004 35004	-72.235			
PRIVATE		DOEFERC	NO	H	CNPG	17		50	3	760		80	34899 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOE FERC	35004	-71.60333	43.13		
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC		н	CNPG	.24		665	41			86	34897 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-70.23333			
LOCAL GOVT		DOEFERC		HOTER	MSPG	12	a second a second second	633	55	218		287	34570 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-70.86333		23	
PRIVATE		DOEFERC	NO	HP IN	CNPG	10		130	19	105		166	34570 TES 34794 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-70.86333			
PRIVATE	· · · · · · · · · · · · · · · · · · ·	DOEFERC		HFR	CNEGRE	14		340	85	384		130	34751 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004			25	
LOCAL GOVT		DOEFERC	NO	н	ONEG	17		312	85	77	alaadaa ahaa ahada ahaa ahaa ahaa ahaa a	135	34751 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.885		, and the second second second second second second second second second second second second second second se	901
PRIVATE	069	DOEFERC	NO	н	MSPG	21		20360	1456	217		55	34856 NO	DOEFERC	DOEFERC	DOEFERC				provident data and		901
PRIVATE	MA DEPT OF ENVIRONMENTA		NO	H	MSONPG	10		450	1430	714		256	34751 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC 35004 DOEFERC	35004	-69.79 -72.58167	44.22	23	
LOCAL GOVT	NEW HAMPSHIRE WAD	DOEFERC	NO	n of the same	CNMSPG	23		210	30	74		100	34751 YES	DOEFERC	DOEFERC	DOEFERC	1	and the second s				<u> </u>
PRIVATE	MA DEPT OF ENVIRONMENTA		NO	HSC	CNPG	23	70	106	30	140		140	34572 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.19		25	
PRIVATE	NEW HAMPSHIRE WHO	DOEFERC	NO	н	CNMSPG	17		118	9 5	297		278	34572 ND 34928 ND	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC 35004 DOEFERC	35004	-73.07833		23 9	
PRIVATE	Contract of the Contract of the Party of	DOEFERC	NO	н	ONPG	24	· · · · · · · · · · · · · · · · · · ·	423	32			306	34928 NO 34970 YES	DOEFERC	DOEFERC	DOEFERC	*					
PRIVATE		DOE FERC	NO	H.	MSONFG	24		1800	74			400	34970 YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-72.6	42.15	25	
PRIVATE	MA DEPT OF ENVIRONMENTA		ino	- <u>-</u> -	CNMSPG	28		258	43			150	34970 YES 34667 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC		-72.50333		25	
	MA DEPT OF ENVIRONMENTA		NO.	HR H				258									35004 DOEFERC	35004	-71.86	1	9	
			NU		MSPG	24			40			325	34269 ND	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-70.63667		23	
	MA DEPT OF ENVIRONMENTA		NO	HR	CNPG	13		4500	664			158	34927 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.33		25	
	MA DEPT OF ENVIRONMENTA		NO	HR	MSPG	19		4500	664		U	16	34927 NO	DOEPERC	DOEFERC	DOE FERC	35004 DOE FERC	35004	-71.31	42.65558	25	
PRIVATE	NEW HAMPSHIRE WAD	DOEFERC	NO	н	CNPG	13		122	30			476	34794 NO	DOEFERC	DOE FERC	DOE FERC	35004 DOEFERC	35004	-71.43167	42.44	26	
PUBLIC UTILITY		DOE FERC	NO.	HR	CNPG	31		4500	664		N		34926 NO	DOEFERIC	DOE FERC	DOE FERC	35004 DOEFERC	35004	-71.33194	r	25	
PRIVATE		DOE FERC	NO	H	MSONPG	28		4500	664				34926 NO	DOEFERC	DOE FERC	DOE FERC	35004 DOE FERC	35004	-71.1625		25	
PRIVATE	· · · · · · · · · · · · · · · · · · ·	DOE FERC		н	CNPGPE	32		4500	664		c	60	34926 NO	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.32889		25	
PRIVATE	1	DOEFERC	ino	H ·	CNMSPG	120	4500	4500	664		1	1	34927 NO	DOEFERC	DOFFERC	DOFFERC	35004 DOEFERC	35004	-71 32583	42 64333	25	2501

APPENDIX C National Inventory of Dams Database 10 of 10

OWN_TYPE	STATE_AGCY	FED_AGCY	NONFE	D PURPOS	E DAM_TY	PEIDAM	HEIGHT	KORM_STOP	MAX_STOF	SURF_AREA	DRAIN_AREA	PILL_TYPE	SPILL_WDTH	INSP_DATE	PHASEL IN	S FD_INSPECT	FD_REGUL	SUPP_FED	SUPP_DATE SOURC_AGC	SOURC DATE	LONGITUD_X	LATITUDE Y	IPS STATE F	FIPS_ONT
PRIVATE	DEP	DOE FERC	NO	H	MSPG		8	1600	2785	790	100 0	3	72	34513	ND	DOEFERC	DOE FENC	DOEFERC	35004 DOEFERC	35004	-70.025	44.92333	23	23025
PRIVATE	NEW HAMPSHIRE WRD	DOE FERC	NO	Ìн	ONPG		23	65		13	289 (3	1	34906		DOEFERC	DOE FERC	DOEFERC	35004 DOEFERC	35004	-71.91167	41.92687	9,	901!
PRIVATE		DOE FERC		н	MISCIN		25	80000	119250	7850	1045	3	72	34556	YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-71.125	44.78833	33	33007
PRIVATE	NEW HAMPSHIRE WRD	DOEFERC	NO	H	CNPG		35	16600	28000	2000		4	1	34935		DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	.72.57833	42.58833	25	25011
PRIVATE		DOE FERC	NO	HR	ONPETC		22	1800	3120	120		2	9	34955		DOE FERC	DOEFERC	DOE FERC	35004 DOE FERC	35004	-73.51167	41.67667	9	9005
LOCAL GOVT		COE FERC	NO	н	CNMSPG		36	1	20	1	10	3	60	34927	YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-73.04167	43.90167	50	50001
PRIVATE		DOE FERC	NO	н	CNCORE		61	1240	1861	67	3 1	1	150	34927	YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-73.005	43.915	50	50001
PUBLIC UTILITY	PSB	DOEFERC	NO	н	CNFG		30	3120	4445	110	11	3	8	34927	YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-73.05333	43.89833	50	50001
PUBLIC UTILITY	PSB	DOE FERC,U	NO	н	RECN		110	3593	5480	218	236	J	179	34836	YES	DOFFERC	DOEFERC	DOE REAC	35004 DOE FERC	35004	-72.93	42.73	25	25011
PUBLIC UTILITY	DEC	DOEFERC	NO	H	FEON	1	50	412	600	30	90 1	J	137	34835	YES	DOEFERC	DOEFERC	DOEFERC	35004 DOEFERC	35004	-72.93333	42.86667	50	50003
PUBLIC UTILITY	PSB	DOE FERC,	NO	н	RECINCE		110	57345	190000	1514	30 1	J	1921	34835	YES	DOEFERC	DOE FERC	DOEFERC	35004 DOEFERC	35004	-72.95	42.96667	50	50025
PRIVATE		DOE FEFIC	NO	н	MSONPG		155	208910	255000	3240	2619	3	430	34948	YES	DOEFERC	DOE FERC	DOE FERC	35004 DOE FERC	35004	-69.90667	45.07	23	23028
PRIVATE		DOEFERC	NO	HC	OTONPO		45	4575	6700	446	2720	2	508	34858	YES	DOEFERC	DOEFERC	DOE FERC	35004 DOEFERC	35004	-69.87	44.96	23	23025

APPENDIX D Characteristics of NE and HQ Dams Used in this Study 1 of	APPENDIX D	Characteristics of NE and HQ	Dams Used in this St	udy 1 of6
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FERC#	MAX_STOR STATE	DAM_NAME	HAZARD	RIVER	YEAR_COMP	NID_HEIGHT	NID_STOR	est. volume	DAM_LENGTH	DAM_HEIGHT	estimated width	MAX_DISCH	DAM_TYPE	NORM_STOR	SURF_AREA	DRAIN_AREA
2441	453 CT	GREENVILLE	LOW	SHETUCKET RIV	1888	15	453	65,630	410	15	10.671625	66935	TC	373	80	1264
2576	3120 CT	BULLS BRIDGE	SIGNIFICANT	HOUSATONIC R	1902	22	3120	49,059		22		45000	ONPG	1800	120	784
2576	3120 CT	SPOONER	SIGNIFICANT	HOUSATONIC R	1902	20	3120	33,994	156	20	10.8955	45000	ERCN	1800	120	784
2576	3120 CT	BULLS BRIDGE CANAL SPILL	SIGNIFICANT	HOUSATONIC R	1902	22	3120		203	22	10,98505	2000	FG	1800	120	1
2576	3120 CT	BULLS BRIDGE MOUNTAINS!	SIGNIFICANT	HOUSATONIC P	1902	22	3120	49,059	203	22	10.98505	150	PGMS	1800	120	1
2576	218650 CT	ROCKY RIVER CANAL DIKE	HIGH	ROCKY RIVER	1902	20	218650	10,896	50	20	10.8955	1	Æ	172000	5600	
2576	3120 CT	BULLS BRIDGE FOREBAY DIK	SIGNIFICANT	HOUSATONIC F	1903	39	3120	121,397	265	39	11.746225	1250	Æ	1800	120	784
2576	37200 CT	STEVENSON	HIGH	HOUSATONIC R	1919	83	37200	1,423,069	1250	83	13.716325	70000	CNPG	26900	1063	1542
2576	218650 CT	ROCKY RIVER MAIN DAM	HIGH	ROCKY RIVER	1929	100	218650	1,378,258	952	100	14.4775		Æ	172000	5600	40
2576	218650 CT	NORTH LANESVILLE DIKE	HIGH	ROCKY RIVER	1929	7	218650	13,067	181	7	10.313425		CNPG	172000	5600	40
2576	218650 CT	MIDDLE LANESVILLE DIKE	HIGH	ROCKY RIVER	1929	45	218650	90,292	167	45	12.014875		Æ	172000	5600	40
2576	218650 CT	SOUTH LANESVILLE DIKE	HIGH	ROCKY RIVER	1929	17	218650	71,530	391	17	10.761175		CNPG	172000	5600	40
2576	218650 CT	DANBURY DIKE NO. 1	HIGH	ROCKY RIVER	1929	42	218650	435,612	873	42	11.88055		Æ	172000	5600	40
2576	86100 CT	SHEPAUG	High	HOUSATONIC R	1955	140	86100	3,215,957	1412	140	16.2685	180000	ONPG	74000	1870	1391
2576		DANBURY DIKE NO. 2	High	HOUSATONIC R	1989	7	218650		t	7			Æ	172000	5600	
2597	3100 CT	FALLS VILLAGE	SIGNIFICANT	HOUSATONIC P	1913	16	3100	54,868	320	16		38000	CNPG	1135	100	· · · · · · · · · · · · · · · · · · ·
2662		SCOTLAND	HIGH	SHETUCKET RIV	1909	37	2000	· · · · · · · · · · · · · · · · · · ·	481	37	and the second second second second second second second second second second second second second second second	and the second second second second second	CBCNPG	1300	÷ · ·	and an example the second state of
3472	3480 CT	WYRE - WYND	LOW	QUINEBAUG RIV	1913	14	3480	71,859	483	14		46000	MSCNPG	2900	246	
5062	340 CT	QUINEBAUG	LOW	QUINEBAUG RIV	1855	14	340	37,194	250	14	10.62685	3640	MSPG	283	85	384
5062	312 CT	FIVE MILE POND	SIGNIFICANT	FIVE MILE RIVER	1855	17	312	26,526	145	· · · · · · · · · · · · · · · · · · ·		5283	MSPG	260	65	1000 01. / / / / / / /
6066	4400 CT	LAKE HOUSATONIC	HIGH	HOUSATONIC R	1870	25	4400	236,287	850	25	11.119375	160000	MSCNPG	4020	and the second second	
6066	4400 CT	DERBY DIKE	LOW	HOUSATONIC F	1870	10	4400	41,791	400	10	10.44775		Æ	4020	320	1574
6066	4400 CT	DERBY CANAL WEIR	LOW	HOUSATONIC R	1870	10	4400	6,269	60	10	10.44775	500	CNPG	4020	320	1574
6066	4400 CT	SHELTON CANAL DIKE	LOW	HOUSATONIC R	1870	25	4400	489,253		25	11.119375	448	Æ	4020	320	25
11143	258 CT	BRUNSWICK	LOW	MOOSUP RIVER	1891	19	258	32,986	160	19	10.850725	3960	MSPG	215	43	77
11168		DAYVILLE DIKE	LOW	FIVE MILE RIVE	1925	14	110	· · · · · · · · · · · · · · · · · · ·		14			Æ	93	31	1
11168		DAYVILLE EMERGENCY SPILI	LOW	FIVE MILE RIVER	1925	8	110					1	MSCN	93	· · · · · · · · · · · · · · · · · · ·	
11166	110 CT	DAYVILLE WASTEWAY	LOW	FIVE MILE RIVE	1925	14	110	3,868	t	14	10.62685		STMS	93	31	
11547		HALE	LOW	QUINEBAUG RIV	1965	23	65			23	1	•	OTCNPG	65		
1889	28000 MA	TURNERS FALLS DIKE	LOW	CONNECTICUT	1905	10	28000		*			15000		16600	2000	
1889		MONTAGUE		CONNECTICUT	1915	62	28000		······································	62		280000		16600	2000	
1889	28000 MA	CABOT SPILLWAY	LOW	CONNECTICUT	1915	35	28000		6	35		15000	CNPG	16600	2000	7163
1889	· [· · · · · · · · · · · · · · · · · ·	CABOT STATION	LOW	CONNECTICUT	1916	35	28000		· · · · · · · · · · · · · · · · · · ·	35	• • • • • • • • • • • • • • • • • • • •		PGMS	16600	2000	
1889		GILL	SIGNIFICANT	CONNECTICUT	1970	70	28000			70	The second	280000	<u></u>	16600	2000	
2004		OVERFLOW NO. 1	LOW	CONNECTICUT	1850	30	68900		· · · · · · · · · · · · · · · · · · ·	30	had a second of a second of the second of the second of the second of the	and the second second	MSPGRE	26000	2550	(
2004	68900 MA	OVERFLOW NO. 2	LOW	HOLYOKE CAN	1860	20	68900		100				MSPG	26000	2550	8309
2004		OVERFLOW NO. 3	LOW	HOLYOKE CAN	1860	18	68900	······		18			MSPG	26000	2550	·
2004		OVERFLOW NO. 4	LOW	HOLYOKE CAN	1891	26	68900		*·····	26		and the second second second second second second second second second second second second second second second	MSPG	26000	2550	
2004		HOLYOKE DAM	HIGH	CONNECTICUT	1900	30	68900		· · · · · · · · · · · · · · · · · · ·	30				26000	2550	+- ···
2004		CANAL GATE HOUSE	SIGNIFICANT	CONNECTICUT	1900	36	68900		· · · · · · · · · · · · · · · · · · ·	36			MS	26000	2550	
2323		DEERFIELD NO. 5 - CANAL		DEERFIELD RIVE	1910	39	818			39			FE .	248	÷	
2323	a second s	DEERFIELD NO. 5 - CANAL	· · · · · · · · · · · · · · · · · · ·	DEERFIELD RIVE	1910	33	818		1430	33	and a second s		FE.	248	38	· · · · · · · · · · · · · · · · · · ·
2323	ada na manana ang ang ang ang ang ang ang ang an	DEERFIELD NO. 5 - CANAL		DEERFIELD RIVE	1910	16	818			16		And the second s	Æ	248	A CONTRACTOR CONT	5
2323		DEERFIELD NO. 3	LOW	DEERFIELD RIVE	1912	21	551		· · · · · · · · · · · · · · · · · · ·	21		· · · · · · · · · · · · · · · · · · ·	ip — a caracterization and a second	221	42	
2323	and a second second second second second second second second second second second second second second second	DEERFIELD NO. 3 - FOREBAN		DEERFIELD RIVE	1912		551			23		And a second sec	Æ	221	42	1
2323		DEERFIELD NO. 4	LOW	DEERFIELD RIVE	1912	48	1067	share and the second		48	-}	7	CNPGRE	467	75	
2323		DEERFIELD NO. 4 - FOREBAY	·	DEERFIELD RIVE	1912		1067	-g i	The second second second	20		· · · · · · · · · · · · · · · · · · ·	IFE.	467	75	
2323	the second second second second second second second second second second second second second second second se	DEERFIELD NO. 2	=	DEERFIELD RIVE	1913	76	589	· · · · · · · · · · · · · · · · · · ·		76	and a second to construct the second			350		
2323		SHERMAN	HIGH	DEERFIELD RIVE	1910	110	5480	1	· · · · · · · · · · · · · · · · · · ·	·		j	RECNPG	3593	·····	
2323		DEERFIELD NO. 5	LOW	DEERFIELD RM	1992	Second Contractor Providence	and the contraction field and it is being	······································	·····			aleren et aleren andere andere andere andere andere andere andere andere andere andere andere andere andere an		248	· · · · · · · · · · · · · · · · · · ·	

APPENDIX D	Characteristics of NE and HQ Dams Used in this Study	2 of6
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		DAM_NAME	HAZARD	River	YEAR_COMP	NID_HEIGHT			E .	and a set of the set o	estimated width	· · · · · · · · · · · · · · · · · · ·	1	NORM_STOR	SURF_AREA	DRAIN_AREA
2323	818 MA	DEERFIELD NO. 5 - DUNBAR	LOW	DUNBAR BROOK	1993	29	818	52,425		29	11.298475	6800	CNPG	248	38	1
2334	510 MA	GARDNERS FALLS	LOW	DEERFIELD RIVE	1904	37	510	145,347	337	37	11.656675	65250	CNPG	50	21	50
2485	21500 MA	NORTHFIELD MOUNTAIN	HIGH	CONNECTICUT	1972	144	21500	26,526,689	11200	144	16.4476		EFFE	17240	278	
2485	21500 MA	NORTHFIELD MT UPPER RI	LOW	CONNECTICUT	1972	9	21500	51,588	551	9	10.402975	11400	CNPG	17240	278	
2485	21500 MA	NORTHFIELD MT UPPER RI	HIGH	CONNECTICUT	1973	20	21500	107,430	493	20	10.8955		ÓNPG	17240	278	
2608	200 MA	WEST SPRINGFIELD	LOW	WESTFIELD RIV	1840	18	200	106,979	550	18	10.80595	4800	TOCN	200	20	51
2631	2565 MA	WORDNOCO	LOW	WESTFIELD RIV	1938	53	2565	967,265	1475	53	12.373075	210000	ONPGRE	1830	46	34
2669	6800 MA	BEAR SWAMP - NORTH DIKE	LOW	DEERFIELD RIVI	1974	155	6800	3,602,487	1372	155	16.940125	9900	EFFE	5100	118	· · · · · · · · · · · · · · · · · · ·
2669	6800 MA	BEAR SWAMP - DIKE 'A'	LOW	DEERFIELD RIVE	1974	23	6800	89,297	352	23	11.029825		she	5100	118	
2669	6800 MA	BEAR SWAMP - EAST DIKE	HIGH	DEERFIELD RM	1974	50	6800	482,819	789	50	12.23875		EFFRE	5100	118	
2669	6800 MA	BEAR SWAMP - SOUTH DIKE	HIGH	DEERFIELD RIVE	1974	140	6800	6,292,981	2763	140	16.2685	L	EFFE	5100	118	
2669	7580 MA	FIFE BROOK	HIGH	DEERFIELD RIVE	1974	130	7580	1,851,028	900	130	15.82075	84200	EFFEFG	5300	152	25
2800	19900 MA	GREAT STONE	LOW	MERRIMACK RIV	1848	39	19900	431,991	943	39	11.746225	124600	MSPG	18000	655	446
2801	570 MA	GLENDALE	LOW	HOUSATONIC F	1906	26	570	52,248	180	26	11.16415	9000	FG	87	40	27
2985	50 MA	WILLOW MILL	SIGNIFICANT	HOUSATONIC F	1872	12	50	1	special and a second se	12	10.5373	10000	MSPG	50	13	24
3127	145 MA	WARE LOWER	LOW	WARE RIVER	1890	18	145			18			MSPG	90	10	16
8093	210 MA	METHUEN FALLS	HIGH	SPICKETT RIVE	1895	23	210			23	11.029825	1800	MSPG	210	30	7
9100	173 MA	RIVERDALE MILLS	LOW	BLACKSTONE F	1957	10	173		and the construction	10	10.44775	5400	CNPG	89	12	14
2142	108000 ME	HARRIS	HIGH	KENNEBEC RIVE	1955	165	108000	5,781,034	2015	165	17.387875	22000	ONPORE	72250	3666	135
2194	2000 ME	BAR MILLS	LOW	SACO RIVER	1956	25	2000	111,194	400	25	11.119375	16320	CNPG	600	263	159
2283	2280 ME	DEER RIPS	LOW	ANDROSCOGGI			2280	629,660	939	54	12.41785	2000	CNPG	1200	130	286
2283	56100 ME	GULF ISLAND	HIGH	ANDROSCOGG	Ş	99	56100		the second of the second secon	·	14.432725	50000	ONPORE	55100	2862	286
2284	2000 ME	BRUNSWICK	LOW	ANDROSCOGGI	\$	42	2000			1	a far an an an an an an an an an an an an an			251		343
2302	2800 ME	BATES WEIR	LOW	LEWISTON CR		14	2800	10,563	· · · · · · · · · · · · · · · · · · ·		1	1	MSPG	1600		
2302	2800 ME	RED SHOP WEIR	LOW	LEWISTON CR		18	2800				· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	MSPG	1600	· · · · · · · · · · · · · · · · · · ·	
2302	2800 ME	GULLY BROOK LOWER	LOW	LEWISTON CAN		.9	2800	dan sana sa sa sa sa sa sa sa sa sa sa sa sa sa		\$	· · · · · · · · · · · · · · · · · · ·		MSCNPG	1600		f
2302	2800 ME	ANDROSCOGGIN WEIR	LOW	LEWISTON CAN		9	2800	farmer er serie		· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		MSONPG	1600	· · · · · · · · · · · · · · · · · · ·	
2302	2800 ME	GREAT STONE	HIGH	ANDROSCOGGI	i a construction de la construct	27	2800	· · · · · · · · · · · · · · · · · · ·	a an is is in the second second second second second second second second second second second second second se	· · · · · · · · · · · · · · · · · · ·	11.208925	+	MSCNPG	1600		
2302	2800 ME	CONTINENTAL WEIR	LOW	LEWISTON CR		14	2800			· · · · · · · · · · · · · · · · · · ·		1	MSPG	1600	·}	
2312	2244 ME	GREAT WORKS	LOW	PENOBSCOT RI	4		2244	1	÷		· · · · · · · · · · · · · · · · · · ·		TCERPG	1600		+
2322	5100 ME		LOW	KENNEBEC RM		40	5100		den a companya and a den ana ana		(franciska star star star en en en en en en en en en en en en en	dia manana manjarana	ONPG	5000		
2322	22300 ME	SHAWMUT WESTON NORTH CHANNEL	LOW	KENNEBEC RM		38	22300						CNPGCB	18600		
2325	22300 ME	WESTON NORTH CHANNEL	LOW	KENNEBEC RIVI		38 51	22300	 Communication and the second se	1		and the second second second second second second second second second second second second second second second	· · · · · · · · · · · · · · · · · · ·	CNPGC8	18600		····
2325	22300 ME	· · · · · · · · · · · · · · · · · · ·	HGH			1	255000	1		· · · · · · · · · · · · · · · · · · ·	A = 1 - A = A = A = A = A = A = A = A = A = A		RECNPG	208910	· · · · · · · · · · · · · · · · · · ·	
2329	183 ME	WYMAN RUMFORD FALLS MIDDLE D/		KENNEBEC RM ANDROSCOGG			255000		and the second second second second	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·			141		
2333	3110 ME	RUMFORD FALLS WIDDLE DA					3110				CD construction of the second seco	A CONTRACTOR OF A CONTRACTOR O		2900	· · · · · · · · · · · · · · · · · · ·	
2333	6700 ME	WILLIAMS	LOW	ANDROSCOGG			6700	367,655					REONEG	4575		
					f	states a subsection of sector				Commence of the second se	· · · · · · · · · · · · · · · · · · ·					
2364	425 ME	ABENAKI	LOW	KENNEBEC RM		25	425	former and the second second		· · · · · · · · · · · · · · · · · · ·	T			350		
2365	14500 ME	ANSON	LOW	KENNEBEC RM		38	14500	· · · · · · · · · · · · · · · · · · ·		A 11 YO M AND A 12 YO M A 12 YO		L		6000	and a second second second second second second second second second second second second second second second	+
2367	2025 ME	CARIBOU	LOW	AROOSTOOK R	· · · · · · · · · · · · · · · · · · ·	24	2025		1	L	1 · · · · · · · · · · · · · · · · · · ·		TOERCN	1821		······································
2367	29033 ME	MILLINOCKET LAKE	LOW	MILLINOCKET S	f · · · · · · · · · · · · · · · · · · ·	11	29033	a construction and a second second second second second second second second second second second second second	1		the second second second second	· · · · · · · · · · · · · · · · · · ·	TOER	22900		+ ····· ··· ···
2368	89215 ME	SQUA PAN	HIGH	SQUA PAN STR			89215			· · · · · · · · · · · · · · · · · · ·		1	CNCBRE	64000	· • · · · · · · · · · · · · · · · · · ·	1
2375	11560 ME	RLEY	LOW	ANDROSCOGG		23	11560	· · · · · · · · · · · · · · · · · · ·					· · · · · · · · · · · · · · · · · · ·	3600		
2375	782 ME	LIVERMORE FALLS	LOW	ANDROSCOGG		12	782				de construction de comme d'au	· · · · · · · · · · · · · · · · · · ·	CNPG	300	and the second s	
2375	2331 ME	JAY	LOW	ANDROSCOGG	gan a say arrenarier.		2331	145,803	······		star and a second second second second second second second second second second second second second second s	· · · · · · · · · · · · · · · · · · ·	CNPG	1800		
2389	25000 ME	EDWARDS	HIGH	KENNEBEC RIV			25000		-famous a construction of the			· · · · · · · · · · · · · · · · · · ·		16985		t
2403	4800 ME	VEAZIE	LOW	PENOBSCOT RI		· · · · · · · · · · · · · · · · · · ·	4800				Contraction and the second sec	4	CNPGCB	3500		
2458	14520 ME	STONE DAM	HIGH	WEST BRANCH	1		14520				· · · · · · · · · · · · · · · · · · ·		CNPGRE	8100		
2458	56290 ME	DOLBY	High	WEST BRANCH	1906	56	56290	977,078	and a second sec				CNPGRE	41956	-}e	
2458	2970 ME	EAST MILLINOCKET	LOW	WEST BRANCH	1907	24	2970	192,166	723	24	11.0746	75500	CNPGRE	1950	128	211

APPENDIX D Characteristics of NE and HQ Dams Used in this Study 3	of6
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	MAX_STOR STATE	DAM_NAME	HAZARD	RIVER	YEAR_COMP	NID_HEIGHT	NID_STOR	est. volume	DAM_LENGTH	DAM_HEIGHT	estimated width	MAX_DISCH DAM_TYPE	NORM_STOR		
2458	87670 ME	MILLINOCKET LAKE	HIGH	MILLINOCKET S	1910	20	87670	138,373	635	20	10.8955	7000 CNPGRE	45370		·····
2458	392680 ME	NORTH TWIN	HIGH	WEST BRANCH	1934	35	392680	425,497	1051	35	11.567125	72000 RECNPG	346000	17790	187
2519	1663 ME	NORTH GORHAM	HIGH	PRESUMPSCOT	1901	23	1663	229,07B	903	23	11.029825	1320 ONPGMS	1300	98	44
2520	69100 ME	MATTACEUNK	HIGH	PENOBSCOT RIV	1939	45	69100	632,583	1170	45	12.014875	125000 ONPGRE	55785	1664	330
2527	33500 ME	SKELTON	HIGH	SACO RIVER	1948	75	33500	1,698,152	1695	75	13.358125	69600 CNPGRE	25250	488	162
2528	266 ME	WEST CHANNEL DAM	LOW	SACO RIVER	1895	16	266	56,583	330	16	10.7164	2250 MSPG	28	14	170
2528	2500 ME	SPRINGS	LOW	SACO RIVER	1925	12	2500	34,014	269	12	10.5373	3405 CNPG	711	359	170
2528	2500 ME	BRADBURY	LOW	SACO RIVER	1929	12	2500	25,922	205	12	10.5373	2060 CNPG	711	359	170
2528	266 ME	CATARACT	LOW	SACO RIVER	1938	49	266	98,588	165	49	12.193975	5625 CNPG	28	14	170
2529	5440 ME	BONNY EAGLE	SIGNIFICANT	SACO RIVER	1911	67	5440	682,860	784	67	12.999925	ONPGRE	2320	347	156
2529	5440 ME	NEW RIVER CHANNEL DAM	SIGNIFICANT	SACO RIVER	1911	13	5440	48,148	350	13	10.582075	17000 CNPGOT	2320	347	156
2530	2530 ME	HIRAM	LOW	SACO RIVER	1917	30	2530	147,009	432	30	11.34325	16475 CNPG	1000	255	83
2531	13200 ME	WEST BUXTON	LOW	SACO RIVER	1907	30	13200	218,811	643	30	11.34325	4930 ONPGRE	12300	131	157
2534	13300 ME	MILFORD	LOW	PENOBSCOT RM	1906	34	13300	548,464	1400	34	11.52235	70265 ONPG	9175	918	530
2534	13300 ME	GILMAN FALLS	LOW	STILLWATER RI	1906	8	13300	39,361	475	. 8	10.3582	35132 CNPG	9175	918	530
2552	5500 ME	FORT HALIFAX	LOW	SEBASTICOOKI	1908	29	5500	1	the second second second		11.298475		5000		94
2555	1440 ME	AUTOMATIC	LOW	MESSALONSKE		33		÷		33	11.477575	/ /	900		
2556	750 ME	UNION GAS	LOW	MESSALONSKE		36					11.6119	1	600		
2557	1500 ME	RICERIPS	SIGNIFICANT			23			· · · · · · · · · · · · · · · · · · ·		11.029825		1000		······································
2559	110 ME	OAKLAND	LOW	MESSALONSKE		14		17,109	· · · · · · · · · · · · · · · · · · ·			·····	50		t
2559	118300 ME	MESSALONSKEE LAKE	HIGH	MESSALONSKE		13		a second second second second second	· · · · · · · · · · · · · · · · · · ·			The second s	110000		
2572	977000 ME	RIPOGENUS	HIGH	WEST BRANCH	1916		5		· · · · · · · · · · · · · · · · · · ·		13.268575	· · · · · · · · · · · · · · · · · · ·	710000		· · · · · · · · · · · · · · · · · · ·
2574	1830 ME	LOCKWOOD	LOW	KENNEBEC RIVE		20	1830				10.8955		600		
2600	17900 ME	RUN AROUND	LOW	MERRILL BROOM		15	17900	francis and a second second				· · · · · · · · · · · · · · · · · · ·	11250		
2600	17900 ME	WESTENFIELD	LOW	PENOBSCOT R		45	17900				12.014875	· · · · · · · · · · · · · · · · · · ·	11250		
2611	6150 ME	HYDRO - KENNEBEC	LOW	KENNEBEC RIVE		40	6150			1	11.791	· · · · · · · · · · · · · · · · · · ·	3900		
2615	275000 ME	BRASSUA	HIGH	MOOSE RIVER	1927	50					12.23875		207000		
2618	639580 ME	WEST GRAND LAKE	SIGNIFICANT	and an experimental and a second second second	· · · · · · · · · · · · · · · · · · ·			A strange of the s			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	556190	· · · · · · · · · · · · · · · · · · ·	
2634	26740 ME	CANADA FALLS	LOW	WEST BRANCH	1921	50		÷				· · · · · · · · · · · · · · · · · · ·	21700		
2634	159000 ME	SEBOOMOOK	LOW	WEST BRANCH	8 · · · · · · · · · · · · · · · · · · ·			· · · · · · · · · · · · · · · · · · ·		60	· · · · · · · · · · · · · · · · · · ·		117800		
2634	40170 ME	RAGGEDLAKE	LOW	RAGGED STREA		30	f				·····		30490		1
2634	103800 ME	CAUCOMGOMOC	LOW	CAUCOMGOMC		12		·····	J.,	. 12	10.5373		42516		
2660	113330 ME	FOREST CITY	LOW	EAST BRANCH	1949				· · · · · · · · · · · · · · · · · · ·			······································	105300		the second secon
2666	1980 ME	MEDWAY	LOW	WESTBRANCH				· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·				1500		· · · · · · · · · · · · · · · · · · ·
2671	1400000 ME	MOOSEHEAD - EAST OUTLE	And the second second second second		• · · · · = · · · · · · · · · ·		1400000				and the second sec		1080000		
2671	1400000 ME	MOOSEHEAD - WEST OUTLE	*			18					2		1080000		
2710	1300 ME	ORONO	LOW	STILLWATER R		15				••••••••••••••••		· · · · · · · · · · · · · · · · · · ·	812		
2710	3830 ME	STILLWATER	LOW	STILLWATER R	1	25	1						3040		
2721	4370 ME	HOWLAND	LOW	PISCATAQUIS F	j			· · · · · · · · · · · · · · · · · · ·	rije og state i state og state og state og state og state og state og state og state og state og state og state				3400	-1	
		strate in the second se	· · · · · · · · · · · · · · · · · · ·		1978		1				{		2500		· · · · · · · · · · · · · · · · · · ·
2727	3040 ME	ELLSWORTH	HIGH	UNION RIVER	1907	62				· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	14467(
2727	145000 ME	GRAHAM	HIGH	UNION RIVER	f	43	+	alan an tao an tao amin' an tao amin' an tao amin' an tao amin' an tao amin' an tao amin' an tao amin' an tao a			· · · · · · · · · · · · · · · · · · ·		1620		
2804	1800 ME	MASONS	LOW	GOOSE RIVER	1835	15	·						200		
2804	270 ME	KELLY	LOW	GOOSE RIVER	1835	family and a second second		· · · · · · · · · · · · · · · · · · ·			1		7500		
2804	11270 ME	SWAN LAKE	LOW	GOOSE RIVER	1900		· · · · · · · · · · · · · · · · · · ·		+		10.44775				
2804	82 ME	CMP	LOW	GOOSE RIVER	1908	Contra de la contr					¢	- dealer and a second s	72		
2808	210 ME	BARKER'S MILL	LOW	LITTLE ANDROS	j					in the second second second second second second second second second second second second second second second			150		· · · · · · · · · · · · · · · · · · ·
2809	120 ME	AMERICAN TISSUE	HIGH	COBBOSSEECC		24	and the second s		and the second second second second second second second second second second second second second second second				101		
2897	100 ME	SACCARAPPA WEST	LOW	PRESUMPSCOT		12				and the second s	Set the rest of the se	· · · · · · · · · · · · · · · · · · ·	1.		
2897	100 ME	SACCARAPPA EAST	LOW	PRESUMPSCOT		9			a second a second second second second second second second second second second second second second second se		A second se		1		
2931	1261 ME	GAMBO	LOW	PRESUMPSCOT	1911	24	1261	93,027	350	24	11.0746	14600 CNPG	1000	0 7	1

APPENDIX D Characteristics of NE and HQ Dams Used in this Study 4 of6

	AX_STOR STATE	DAM_NAME				NID_HEIGHT	NID_STOR			1	estimated width		DAM_TYPE	NORM_STOR	SURF_AREA	
2932	56 ME		LOW	PRESUMPSCOT	1900	14	56	42,847	288	· · · · · · · · · · · · · · · · · · ·	10.62685	5682	MSONPG	31	7	
2942	3337 ME	DUNDEE	High	PRESUMPSCOT	1913	44	3337	724,191	1375	44	11.9701	22800	ONPGRE	2900	190	44
2984	383990 ME	EELWEIR	HIGH	PRESUMPSCOT	1879	23	383990	111,622	440	23	11.029825	29800	MSPGRE	330000	29184	4 43
3428	2960 ME	WORLINBO	LOW	ANDROSCOGGI	1988	17	2960	159,158	870	17	10.761175	136735	TOEFFPG	1700	180	337
3562	665 ME	BARKER MILL UPPER	LOW	LITTLE ANDROS	1987	24	665	61,132	230	24	11.0746	19900	MSPG	255	5 41	1 35
4026	321195 ME	AZISCOHOS	HIGH	MAGALLOWAY	1911	74	321195	867,951	881	74	13.31335	7746	OBPGRE	221355	5 8320	21
4026	321195 ME	ABBOTT BROOK DIKE	High	ABBOTT BROOK	1911	27	321195	272,377	900	27	11.208925		Æ	221355	5 8320	21
4202	820 ME	LOWELL TANNERY	LOW	PASSADUMKEA	1987	27	820	69,607	230	27	11.208925	9623	CNPG	680	69	9 30
4784	5191 ME	PEJEPSOOT	LOW	ANDROSCOGGI	1896	48	5191	326,570	560	48	12.1492	95000	TCERCN	3278	3 225	5 342
5073	1536 ME	BENTON FALLS	LOW	SEBASTICOOKI	1987	27	1536	151,320	500	27	11.208925	23000	ONPORE	955	5 83	3 86
5362	351 ME	KESSLEN	LOW	MOUSAM RIVER	1954	18	351	27,231	140	18	10.80595	6200	CNPG	224	4 20	12
5362	240 ME	DANE PERKINS	LOW	MOUSAM RIVER	1979	12	240	8,219	65	12	10.5373	1150	CNPG	150	25	5 12
5362	146 ME	TWINE MILL	LOW	MOUSAM RIVEF	1980	18	146	35,011	180	18	10.80598	2400	CNPG	104	4 12	2 12
6398	774 ME	HACKETT MILLS	LOW	LITTLE ANDROS	1986	8	774	18,230	220	8	10.3582	474	TCERCN	480	60	0 31
7189	113000 ME	GREEN LAKE	LOW	REEDS BROOK	1911	. 8	113000	22,622	273	8	10.3582	2500	MSOT	107000	2989	9 5
8277	2620 ME	OTIS	LOW	ANDROSCOGGI	1898	17	2620	153,670	840	17	10.761175	68000	ONPG	1700	0 115	
9340	145 ME	UPPER KEZAR FALLS #2	LOW	OSSIPEE RIVER	1860	8	145	22,374	270	8	10.3582	16600	TCER	130	0 10	0 41
9340	175 ME	LOWER KEZAR FALLS	LOW	OSSIPEE RIVER	1910	9	175	41,196	440	9	10.402978	17180	TCERCN	150	0 5	
9340	145 ME	UPPER KEZAR FALLS #1	LOW	OSSIPEE RIVER	1910	11		22,622	196	11	10.492525	3360	ONPG	130	0 10	0 41
11132	720 ME	EUSTIS	LOW	NORTH BRANC	1952	17	720	43,906	240	17	10.761175	11345	CNPGRE	570	0 74	4 23
11433	1400 ME	SANDY RIVER	LOW	SANDY RIVER	1902	18	1400	77,803	400	18	10.80595	12000	CNMSPG	1050	0 150	0 57
11482	240 ME	MECHANIC FALLS	LOW	LITTLE ANDROS	1866	15	240	27,533	172	1.5	10.671625	1000	MSCNPG	105	3 27	7 25
1855	55560 NH	BELLOWS FALLS	LOW	CONNECTICUT	1907	48	55560	374,973	643	48	12.1492	157600	CNPG	30000	2804	4 541
1892	79800 NH	WILDER	HIGH	CONNECTICUT	1950	59	79800	The second s		59	12.641725	213300	CNPGRE	55000	0 3100	0 337
1893	5700 NH	GARVINS FALLS	LOW	MERRIMACK RIV	1901	18		al and the second second second		18	10.80598	113000	MSCNPG	2700	0 250	0 242
1893	8100 NH	AMOSKEAG	LOW	MERRIMACK RIV	1921	29	8100	 a contra colore contra 	f	29	11.298478	87000	CNPG	4320	0 478	8 285
1893	4180 NH	HOOKSETT	LOW	MERRIMACK RIV	1927	11	4180		· · · · · · · · · · · · · · · · · · ·	11	10.492525	78500	MSPG	1650	0 405	5 280
1904	54000 NH	VERNON	LOW	CONNECTICUT	1909	58		1		· · · · · · · · · · · · · · · · · · ·				18300		
2077	57700 NH	COMERFORD	HIGH	CONNECTICUT	1930	170		÷	· · · · · · · · · · · · · · · · · · ·	-{			CNPGRE	46800		3 163
2077	14100 NH	MCINDOES	SIGNIFICANT	CONNECTICUT	1931	25	fearer an earlier strate					1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		9800		
2077	223722 NH	MOORE	HIGH	CONNECTICUT	1957	144	and the second second second second second second second second second second second second second second second	-}	second contract and the third the second				ONPORE	200000		
2287	94 NH	J. BRODIE SMITH	HIGH	ANDROSCOGGI	1948	31			and a second second second second		11.388025		CNPG	6(B 137
2288	NH	GORHAM	LOW	ANDROSCOGGI	1958	20	a second to the second s	The second secon				and the second s	TCERPG	258		
2300	2000 NH	SHELBURNE	LOW	ANDROSCOGGI	1906	16	the second second second second second second second second second second second second second second second s		·				CNTC	960		······································
2311	685 NH	GORHAM	LOW	ANDROSCOGGI	1904	24		*				a grant and an an analysis of the	TCERRE	370		
2326	195 NH	CROSS	HIGH	ANDROSCOGGI	1903	30		· · · · · · · · · · · · · · · · · · ·			, , , , , , , , , , , , , , , , , , ,	naj na za na manana na sia isan	CNPG	12(
2327	400 NH	CASCADE	HIGH	ANDROSCOGGI	1903	58		sila na serie na serie de la serie de la serie de la serie de la serie de la serie de la serie de la serie de l			· · · · · · · · · · · · · · · · · · ·	19 ···· 10 ···· 10 ····	ONPG	20(
2392	1030 NH	GILMAN	LOW	CONNECTICUT	1920	30		· · · · · · · · · · · · · · · · · · ·	Access to the second statement		· · · · · · · · · · · · · · · · · · ·		PGTOER	70		
2422	830 NH	SAWMILL	LOW	ANDROSCOGGI	a serie de la constante de la	20						· - · - · · · · · · · · · · · · · ·	CNPG	621		
2423	95 NH	RIVERSIDE	LOW	ANDROSCOGGI	1970	here an an an an an an an an an an an an an		· · · · · · · · · · · · · · · · · · ·					PGTCER	6		7 133
2456	16000 NH	AYERS ISLAND	SIGNIFICANT	PEMIGEWASSE	1970	80							CNCB	1000		
2450	9340 NH	EASTMAN FALLS	SIGNIFICANT	PEMIGEWASSE	1924	37						and the second sec	ONPG	457		
2861	2283 NH	PONTOOK	LOW	ANDROSCOGGI	1937		· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·				TCER	88		
		CLEMENT				4		and the second second			· · · · · · · · · · · · · · · · · · ·		ONPG	21		
2966	60 NH	a parameter and a second second second second second second second second second second second second second s	LOW	WINNIPESAUKE		24	1	()				· · · · · · · · · · · · · · · · · · ·	CNPG	135		
3025	2290 NH	KELLEY'S FALLS	HIGH	PISCATAQUOG	1916			ala se se se ana se a a a a a a a a a a a a a a a a a a			and the second s		OTERON	8000		
3133	119250 NH	EPROL	LOW	ANDROSCOGGI		25										
3342	94 NH	· · · · · · · · · · · · · · · · · · ·	LOW	CONTOOCOOK	1982			1					CNOT	5.		
3342	94 NH	PENACOOK LOWER FALLS D		CONTOOCOOK	1982						- Sec		CNOT	5-		
3342	94 NH	ALLIED LEATHER AUXILIARY		CONTOOCOOK	1982	· · · · · · · · · · · · · · · · · · ·					Alter and assessment and	section that a subscreen	CNPG	5	the second secon	
3442	2938 NH	MINE FALLS	LOW	NASHUA RIVER	1889	20	2938	70,821	325	5 20	10.895	1700	MSONPG	197	0 242	2 4

APPENDIX D	Characteristics of NE and HQ Dams Used in this Study	5 of6

	the stand and a second se	DAM_NAME	HAZARD	RMER	a sea any the course has a co	NID_HEIGHT			DAM_LENGTH	DAM_HEIGHT	estimated width	MAX_DISCH	DAM_TYPE	NORM_STOR	SURF_AREA	DRAIN_AREA
3777	527 NH	ROLLINSFORD	LOW	SALMON FALLS	1910	20	527	83,895	385	20	10.8955	7000	CNMSPG	456	57	231
3820	633 NH	SOMERSWORTH	LOW	SALMON FALLS	1929	12	633	37,934	300	12	10.5373	8000	MSPG	377	55	21
4451	464 NH	LOWER GREAT FALLS	SIGNIFICANT	SALMON FALLS	1984	36	464	112,868	270	36	11.6119	7850	MSONPG	272	32	22
4718	330 NH	COCHECO FALLS	LOW	COCHECO RIVE	1930	9	330	14,044	150	9	10.402975	2900	ONPG	110	55	18
6440	208000 NH	LAKEPORT	LOW	WINNIPESAUKE	1958	. 10	208000	23,507	225	10	10.44775	4080	CNOT	165800	46720	36
6597	51 NH	PIERCE	LOW	CONTOOCOOK	1921	12	51	53,108	420	12	10.5373	13400	CBONPG	33	7	19
6597	50 NH	PAPER MILL	LOW	CONTOOCOOK	1922	9	50	26,215	280	9	10.402975	13400	CNPG	25	5	19
6597	240 NH	MONADNOCK	LOW	CONTOOCOOK	1923	22	240	120,836	500	22	10.98505	13400	ONPGRE	217	4	19
6597	8600 NH	POWDER MILL	LOW	CONTOOCOOK	1924	21	8600	84,087	366	21	10.940275	18200	CNPGRE	2400	435	18
6689	114 NH	PENACOOK UPPER FALLS	LOW	CONTOOCOOK	1987	16	114	45,780	267	16	10.7164	35000	CNOT	70	11	76
7528	400 NH	CANAAN	LOW	CONNECTICUT	1943	18	400	53,489	275	18	10.80595	37000	CNPG	200	20	38
7883	320 NH	WESTON	LOW	UPPER AMMON	1987	20	320	45,761	210	20	10.8955	14250	TOER	275	30	26
7887	160 NH	MINNEWAWA	HIGH	MINNEWAWA B	1932	63	160	214,044	265	63	12.820825	1700	CNVA	120	10	2
8405	28 NH	GLEN ROAD	SIGNIFICANT	MASCOMA RIVE	1988	16	28	30,006	175	16	10.7164	8600	CNPG	10	2	19
8924	83 NH	MCLANE	LOW	SOUHEGAN RIV	1929	18	83		· · · · · · · · · · · · · · · · · · ·	And a second sec	10.80595	9400	CNMSPG	47	6	
9282	98 NH	HILLSBOROUGH MILL	LOW	SOUHEGAN RIV	1925	the second second to second second second	98	provide a contract of the second	A PARTY AND A PART	A second se		And a set of the set o	CNMSPG	70	- jan	r
0898	300 NH	COY PAPER MILL	the case of the second s	SUGAR RIVER	1922	 An analysis and the second second second second second second second second second second second s 	AV1741.414.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4	a contra co	314					150		
1128	725 NH	RED	LOW	UPPER AMMON	1900	a second second second second second second	and the second se	Second and the second sec	275	the second second second second second second	and the same of the second secon		And the part of the second second	200	And a second sec	
1128	240 NH	BROOKLYN	LOW	UPPER AMMON	1910				· · · · · · · · · · · · · · · · · · ·		1			50	· · · · · · · · · · · · · · · · · · ·	······································
1163	641 NH	SOUTHBERWICK	LOW	SALMON FALLS	1916		641		290	(· · · · · · · · · · · · · · · · · · ·		And the second se	1	525		
1313	280 NH	APTHORP	for a second second second second	AMMONOOSUC	1936		280		235	and the second second second second second second second	afar and a second second			210	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
2972	360 FI	WOONSOCKET FALLS	LOW	BLACKSTONE F	1960	CONTRACTOR CONTRACTOR CONTRACTOR				And a second sec		33000	· · · · · · · · · · · · · · · · · · ·	300	· · · · · · · · · · · · · · · · · · ·	
3011	530 FI	ARCTIC	LOW	SOUTH BRANC	1885							· · · · · · · · · · · · · · · · · · ·	MSPG	442		
3023	366 FI	TUPPERWARE	LOW	BLACKSTONE F	1904	The second second second second second second second second second second second second second second second s	366							305		· · · · · · · · · · · · · · · · · · ·
3037	180 FI		LOW			11			and the second second second second		· · · · · · · · · · · · · · · · · · ·		MSPG	150		
3063	96 Fil		Ý	BLACKSTONE F				· · · · · · · · · · · · · · · · · · ·	a contract of the second		of a construction of the second s		· · · · · · · · · · · · · · · · · · ·			
2205	3725 VT	VALLEY FALLS	LOW	BLACKSTONE F	1859							19310 66900		80		· · · · · · · · · · · · · · · · · · ·
		FAIRFAX FALLS	LOW	LAMOILLE RIVE			3725					and the second second second second second				
2205	2025 VT	MILTON	LOW	LAMOILLE RIVE	1929	the viral production		······································			*]	83000		93		
2205	11520 VT	CLARK FALLS	HIGH	LAMOILLE RIVE	1937		11520	· · · · · · · · · · · · · · · · · · ·	850			· · · · · · · · · · · · · · · · · · ·	ONPGRE	6000		
2205	6340 VT	PETERSON	HIGH	LAMOILLE RIVE	1949	· · · · · · · · · · · · · · · · · · ·				j · · · · · · · · · · · · · ·	······································			2840		
2306	6060 VT	ECHO	LOW	CLYDE RIVER	1922			A CONTRACTOR	a second to the second se		······································	693		5000		and the second second second second second second second second second second second second second second second
2306	420 VT	WEST CHARLESTON	LOW	CLYDE RIVER	1928	÷							4	220	······································	and the second sec
2306	3400 VT	NEWPORT NO. 1	HIGH	CLYDE RIVER	1936					the state of the second s		a second and the second second		3000	· · · · · · · · · · · · · · · · · · ·	
2323	190000 VT	SOMERSET	HIGH	EAST BRANCH	1913	t		· · · · · · · · · · · · · · · · · · ·	1	110	· /· · · · · · · · · · · · · · · · · ·	1	RECNPG	57345		
2323	600 VT	SEARSBURG	LOW	DEERFIELD RIVE	1922	ali in antini antini antini antini antini a						+ · · · · · · · · · · · · · · · · · · ·	RECNPG	412		
2323	318000 VT	HARRIMAN	HIGH	DEERFIELD RIVI	the second second second				P		in the second seco	35200		117300		
2396	524 VT	PIERCE MILLS	LOW	PASSUMPSIC R	1928				140	the second			CNPG	50		
2397	2548 VT	GAGE	LOW	PASSUMPSIC RI	1928	j		4	321		internet and a second second second second second			70	· · · · · · · · · · · · · · · · · · ·	**···
2399	427 VT	ARNOLD FALLS	LOW	PASSUMPSIC RI			427		420	T		· · · · · · · · · · · · · · · · · · ·		46	· · · · · · · · · · · · · · · · · · ·	
2400	494 VT	PASSUMPSIC	LOW	PASSUMPSIC RI	1929			A contraction of the second se	258					70	· · · · · · · · · · · · · · · · · · ·	
2445	490 VT	CENTER RUTLAND	LOW	OTTER CREEK	1898	14	490	25,887	174					30		
2489	592 VT	CAVENDISH	LOW	BLACK RIVER	1907	39	592	59,553		1			CNPG	100		
2490	385 VT	TAFTSVILLE	LOW	OTTAUQUECHE	1910	18	. 385	42,792	220	18	10.80595	15300	CNPG	100	21	
2513	6085 VT	ESSEX NO. 19	SIGNIFICANT	WINOOSKI RIVE	1917	53	6085	252,473	385	53	12.373075	150000	FG	1950	352	
2547	24278 VT	HIGHGATE FALLS	SIGNIFICANT	MISSISQUOI RIV	1918	46	24278	133,139	240	46	12.05965	8200	FG	7000	65	
2558	2122 VT	HUNTINGTON FALLS	LOW	OTTER CREEK	1910	34	2122	73,259	187	34	11.52235	2587	ON	250	23	74
2558	3369 VT	PROCTOR	LOW	OTTER CREEK	1910	16	3369	21,947	128	16	10.7164	2328	ST	460	92	3-
2558	1730 VT	BELDENS EAST	LOW	OTTER CREEK	1913		1730	16,948	· · · · · · · · · · · · · · · · · · ·	3	11.208925	3	2	150	22	6
2558	1730 VT	BELDENS WEST	LOW	OTTER CREEK	1913	1	A REPORT OF A REPORT OF A REPORT OF	adama a construction and a second				A set a set of a set		150		
2629	1000 VT	CADYS FALLS	LOW	LAMOILLE RIVE										1000		

APPENDIX D	Characteristics of	of NE and HQ Dams	Used in this Study 6 of6

FERC#	MAX_STOR STATE	DAM_NAME	HAZARD	RIVER	YEAR_COMP	NID_HEIGHT	NID_STOR	est. volume	DAM_LENGTH	DAM_HEIGHT	estimated width	MAX_DISCH DAM	TYPE NORM_STOR	SURF_AREA	DRAIN_AREA
2629	1038 VT	MORRISVILLE DAM	LOW	LAMOILLE RIVE	1924	37	1038	107,824	250	37	11.656675	140000 FG	150	15	222
2629	1038 VT	MORRISVILLE BACK SPILLWA	LOW	LAMOILLE RIVE	1924	8	1038	12,430	150	8	10.3582	35000 FG	150	15	1
2629	17000 VT	GREEN RIVER DAM	HIGH	GREEN RIVER	1947	110	17000	525,369	320	110	14.92525	2535 VA	16900	625	14
2629	17000 VT	GREEN RIVER DIKE	SIGNIFICANT	GREEN RIVER	1947	22	17000	60,418	250	22	10.98505	Æ	16900	625	L
2674	1649 VT	VERGENNES NO. 9	LOW	OTTER CREEK	1912	12	1649	68,029	538	12	10.5373	3459 PG	350	70	866
2731	5100 VT	WEYBRIDGE WEST	LOW	OTTER CREEK	1944	30	5100	51,045	150	30	11.34325	46000 ONPG	600	59	750
2731	5100 VT	WEYBRIDGE EAST	LOW	OTTER CREEK	1951	30	5100	37,433	110	30	11.34325	46000 FG	600	59	750
2737	677 VT	MIDDLEBURY LOWER EAST	LOW	OTTER CREEK	1917	15	677	49,623	310	15	10.671625	13700 ONPG	48	16	632
2737	677 VT	MIDDLEBURY LOWER WEST	LOW	OTTER CREEK	1917	15	677	12,806	80	15	10.671625	1275 FG	48	16	632
2756	400 VT	CHACE MILL	LOW	WINOOSKI RIVE	1876	29	400	78,637	240	29	11.298475	30000 FG	34	50	1060
2839	160 VT	GREAT FALLS	HIGH	PASSUMPSIC R	1915	34	160	62,682	160	34	11.52235	1550 FG	135	12	220
2879	18558 VT	BOLTON FALLS	LOW	WINOOSKI RIVE	1898	75	18558	190,353	190	75	13.358125	68000 TCER	355	70	835
2905	7471 VT	ENOSBERG FALLS	LOW	MISSISQUOI RIV	1928	21	7471	44,800	195	2	10.940275	26443 FG	75(120	587
5261	14 VT	NEWBURY	SIGNIFICANT	WELLS RIVER	1912	20	14	19,612	90	20	10.8955	3200 PG	11	12	90
5944	209 VT	MORETOWN NO. 8	SIGNIFICANT	MAD RIVER	1910	31	209	117,559	333	3	11.388025	122000 FG	201	36	143
6470	69 VT	WINOOSKI NO. 8	LOW	WINOOSKI RIVE	1985	29	69	74,378	227	21	11.298475	14500 PG	34	7	199
7186	2250 VT	SHELDON SPRINGS	LOW	MISSISQUOI RIV	1920	38	2250	125,837	283	31	11.70145	3822 OB	750	175	5 794
7725	793 VT	BARTON VILLAGE	LOW	CLYDE RIVER	1949	9	793	7,209	77		10.402975	762 OT	56	187	108
9648	90 VT	FELLOWS	LOW	BLACK RIVER	1990	1.0	90	20,896	200	11	10.44775	1780 FG	61	21	190

APPENDIX E Summary of Emissions for Dam Assessed in this Study 1 of4

:	· · · · · · · · · · · · · · · · · · ·				Summar	y or 15001551	UNS IUL DAI	п дээсээси	in this stut	ay 1014			1. S. S. S. S. S. S. S. S. S. S. S. S. S.
Dam #	VOCs to air (S	NOx to air (ST	CO to air (ST)	SO2 to air (ST	PM10 to air (S	Fossil CO2 (m	TRI Rel Air (lb:	TRI Rel Water	TRI Rel UnGno	TRI Rel Land (TRI TI POTW	TRI Tf OffSite	Cost D&T (\$
7591.0101	5.5596E-06	1.8382E-05	2.9694E-05	3.6225E-05	5.319E-06	0.00573654	0.00372311	0.00038292	0.00146089	0.00200248	0.00083912	0.01587577	1.2085E-0
4253.0101	4.6285E-05	0.00015303	0.0002472	0.00030158	4.4281E-05	0.04775743	0.0309954	0.00318784	0.01216206	0.01667086	0.00698578	0.13216781	0.0001006
7961.0101	2.0645E-05	6.8259E-05	0.00011027	0.00013452	1.9752E-05	0.02130231	0.01382557	0.00142194	0.00542491	0.00743608	0.00311602	0.05895376	4.4878E-0
11168.0101	3.4538E-05	0.00011419	0.00018446	0.00022504	3.3043E-05	0.03563704	0.02312906	0.0023788	0.00907544	0.01243995	0.00521285	0.09862486	7.5077E-0
7888.0101	5.1306E-06	1.6963E-05	2.7402E-05	3.3429E-05	4.9085E-06	0.00529381	0.00343578	0.00035337	0.00134814	0.00184793	0.00077436	0.01465053	1.1153E-0
7464.0101	0.00147729	0.00488429	0.00789008	0.00962555	0.00141336	1.52429843	0.98929612	0.10174789	0.3881827	0.53209254	0.22296869	4.21846821	0.0032112
10163.0201	1.3637E-05	4.5086E-05	7.2832E-05	8.8851E-05	1.3046E-05	0.01407045	0.00913196	0.00093921	0.00358322	0.00491162	0.00205817	0.03893971	2.9642E-0
5362.0401	2.7961E-05	9.2445E-05	0.00014934	0.00018218	2.6751E-05	0.02885038	0.0187244	0.00192578	0.00734713	0.01007091	0.00422013	0.07984291	6.078E-0
8791.0101	0.00022908	0.00075738	0.00122347	0.00149258	0.00021916	0.23636458	0.15340471	0.01577749	0.06019336	0.08250866	0.03457453	0.65413468	0.0004979
10934.0101	3.9568E-05	0.00013082	0.00021133	0.00025781	3.7855E-05	0.0408267	0.02649724	0.00272521	0.01039706	0.01425153	0.00597198	0.11298715	8.601E-0
6474.0101	5.2946E-05	0.00017505	0.00028278	0.00034498	5.0654E-05	0.05463046	0.03545612	0.00364662	0.01391237	0.01907006	0.00799114	0.15118882	0.0001150
8450.0101	0.00011229	0.00037126	0.00059974	0.00073166	0.00010743	0.11586499	0.07519839	0.00773406	0.02950655	0.04044542	0.0169483	0.32065425	0.0002440
2897.0101	2.946E-06	9.7402E-06	1.5734E-05	1.9195E-05	2.8185E-06	0.00303973	0.00197284	0.0002029	0.00077411	0.00106109	0.00044464	0.00841241	6.4038E-0
6132.0101	2.9727E-05	9.8285E-05	0.00015877	0.00019369	2.8441E-05	0.03067303	0.01990733	0.00204744	0.00781129	0.01070715	0.00448674	0.08488707	6.4619E-0
4718.0101	8.8036E-06	2.9107E-05	4.7019E-05	5.7362E-05	8.4226E-06	0.00908375	0.00589551	0.00060635	0.0023133	0.0031709	0.00132874	0.02513912	1.9137E-0
3265.0101	9.4221E-06	3.1152E-05	5.0323E-05	6.1391E-05	9.0143E-06	0.00972189	0.00630968	0.00064894	0.00247581	0.00339366	0.00142208	0.02690516	2.0481E-0
9100.0101	3.679E-05	0.00012164	0.00019649	0.00023971	3.5198E-05	0.03796046	0.02463699	0.00253388	0.00966713	0.013251	0.00555271	0.10505487	7.9972E-0
6752.0101	2.8533E-05	9.4337E-05	0.00015239	0.00018591	2.7298E-05	0.02944082	0.0191076	0.00196519	0.00749749	0.01027702	0.00430649	0.08147693	6.2023E-0
7410.0201	2.7567E-05	9.1142E-05	0.00014723	0.00017961	2.6373E-05	0.0284437	0.01846045	0.00189863	0.00724356	0.00992895	0.00416064	0.07871742	5.9923E-0
3342.0101	2.3483E-06	7.7641E-06	1.2542E-05	1.5301E-05	2.2467E-06	0.00242304	0.00157259	0.00016174	0.00061706	0.00084582	0.00035443	0.00670571	5.1046E-0
2556.0301	3.8793E-06	1.2826E-05	2.0719E-05	2.5276E-05	3.7114E-06	0.00400272	0.00259784	0.00026718	0.00101935	0.00139725	0.0005855	0.01107746	8.4326E-0
5274.0101	0.00011943	0.00039485	0.00063784	0.00077814	0.00011426	0.12322543	0.07997544	0.00822538	0.03138098	0.04301476	0.01802496	0.34102414	0.000259
4254.0101	0.00013403	0.00044314	0.00071585	0.0008733	0.00012823	0.13829591	0.08975645	0.00923134	0.03521888	0.04827547	0.02022941	0.38273143	0.0002913
8486.0101	0.00016123	0.00053306	0.0008611	0.00105051	0.00015425	0.16635826	0.1079694	0.01110452	0.04236532	0.0580713	0.02433427	0.46039346	0.0003504
8242.0101	9.7932E-05	0.00032379	0.00052305	0.0006381	the second s		decourses and the second second second second second second second second second second second second second s	· · · · · · · · · · · · · · · · · · ·	a comment of the state of the s		0.01478102	,	
9411.0101	0.00017915	0.00059233	0.00095684	0.0011673	0.0001714	0.18485382	0.11997333	0.01233911	0.04707546	0.06452761	0.02703973		
7473.0101	0.00010067	0.00033284	0.00053767	0.00065593	the management of the second se		4 ··· ··· ····				0.01519413	0.2874662	
8736.0101	4.165E-05	0.00013771	0.00022245	0.00027138	3.9848E-05	0.04297538	0.02789177	0.00286863	0.01094425	0.01500158	0.00628628	0.11893358	9.0537E-0
7410.9999	2.6797E-05	8.8596E-05	0.00014312	0.0001746	2.5637E-05	0.02764921	0.01794482	0.0018456	0.00704124	0.00965161	0.00404442	0.07651869	
9340.0201	2.1916E-05	7.2459E-05	0.00011705	0.0001428	and a findered same as a contract time is a series of	·					0.00330775	0.06258118	4.7639E-0
5563.0201	0.00019692	0.00065107	0.00105174	0.00128307	0.0001884	0.20318699	0.13187188	0.01356286	0.05174425	0.07092724	0.02972144	0.5623163	0.0004280
3309.0101	5.8456E-05	0.00019327	0.00031221	0.00038088	5.5926E-05	0.06031612				The second	0.00882282		
5912.0101	5.39E-05	0.00017821	0.00028788	0.0003512	5.1567E-05	of the state times are the three presences			\$1 million and 11 million and 10 million and		0.00813518		
4318.0101	4.5452E-05	0.00015028	0.00024276	0.00029615	and a compared to a second second						0.00686016		
3128.0101	1.1195E-05	5 3.7014E-05	5.9792E-05	7.2944E-05	1.0711E-05	0.01155139	0.00749705		· ····	· · · · · · · · · · · · · · · · · · ·	0.00168969		
5824.0101	6.8051E-05	0.00022499	0.00036346	0.0004434	····	0.07021662					0.01027102	a serve a server server server server server server server server server server server server server server ser	
2445.0101	+	0.00018315									0.00836083		
6597.0401		5 8.3103E-05									0.00379366		
2396.0101		5 0.00011919									0.00544082		
5362.0201		5 0.00023986		0.0004727				and the second data and the se			0.01094965		0.00015
11482.0101		5 4.4338E-05	· · · · · · · · · · · · · · · · · · ·		1.283E-05				0.00352383		0.00202405		
8012.0101		5 0.00024418	and the second sec	0.0004812							0.01114673		
8615.0101			0.00010108	and that a factor of the second second					0.00497298		0.00285644		
2400.0101			8.7634E-05								0.00247647		
8405.0101	1.0659E-05	5 3.524E-05	5.6927E-05	6.9449E-05	1.0197E-05	0.01099787	0.00713781	0.00073411	0.00280075	0.00383907	0.00160873	0.0304364	2.3169E-0

APPENDIX E Summary of Emissions for Dam Assessed in this Study 2 of4

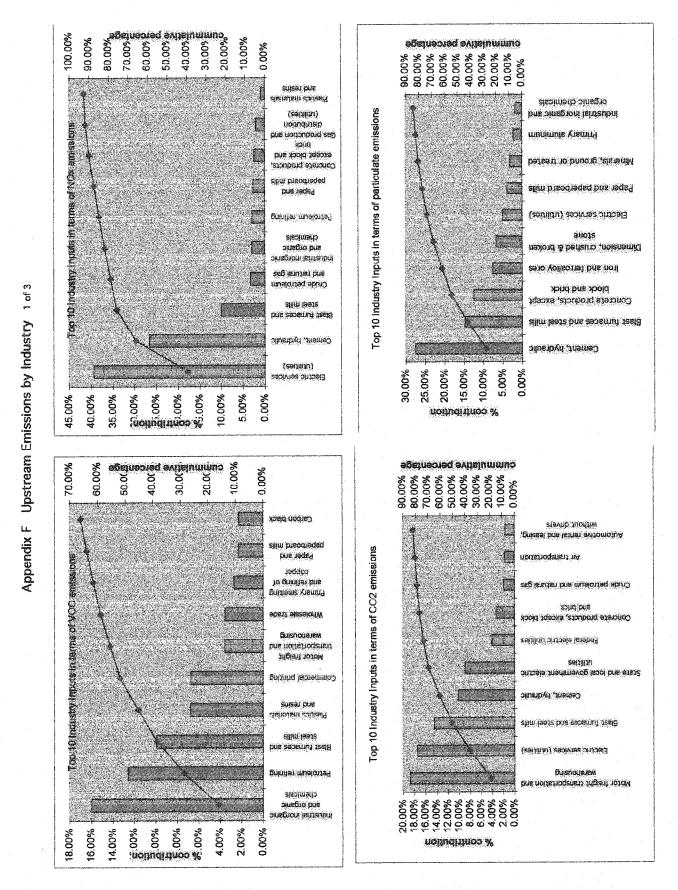
David II						·			The this Stut				0 1 0 1 T
		NOx to air (ST		Without and a second and a second sec	consider of the construction of the construction of the second	a succession and a succession of the second s				· · · · · · · · · · · · · · · · · · ·			a second s
2555.0101		7.1078E-05		concernance and the ballocation of	and a second second second second second second second second second second second second second second second		· · · · · · · · · · · · · · · · · · ·	contractor and the second state of the second			And the second s		
		8.8488E-05			and the second second second second second second second second second second second second second second second		· · · · · · · · · · · · · · · · · · ·		0.00703268	· · · · · · · · · · · · · · · · · · ·			
2966.0101		2.2475E-05				0.00701412	The second		0.00178624	·····		0.01941146	
and the second s		0.00035809	- A - Contract Contract of the second s			0.11175427			the second second second second second second second second second second second second second second second se	0.03901048	and a comparison the second second	0.30927792	A
5735.0101		0.00018405	A COMPANY AND A			make of a state of a second se			0.01462789				
	0.00011161	0.00036902	0.00059611	0.00072722	· · · · · · · · · · · · · · · · · · ·	tal annual rails - for an end	The second second second second second second second second second second second second second second second se		the second second second and the second second second second second second second second second second second s		ALL AND AND AND AND AND AND AND AND AND AND		······································
11547.0101	3.1165E-05	0.00010304	0.00016645	0.00020306	2.9816E-05	0.03215672	0.02087027	0.00214648	0.00818913	0.01122507	0.00470377	0.08899315	6.7745E-0
10163.0101	and the second second second second second second second second second second second second second second second	0.00024949	·	the state of the second s			وسيستحد بالمتحاصين والمراجع والمراجع والمراجع والمراجع		· · · · · · · · · · · · · · · · · · ·	the standard standard with the standard s	0.01138926		· · · · · · · · · · · · · · · · · · ·
3051.0101	1.0561E-05	3.4919E-05	5.6408E-05	6.8815E-05	1.0104E-05	0.01089757	0.00707271	0.00072742	0.00277521	0.00380406	0.00159406	0.03015883	2.2958E-
6240.0101	9.7694E-05	0.000323	0.00052177	0.00063654	9.3466E-05	0.10080254	0.0654226	0.00672863	0.0256707	0.03518752	0.01474502	0.2789692	0.000212
7920.0101	0.0002623	0.00086722	0.0014009	0.00170904	0.00025095	0.27064324	0.17565216	0.01806561	0.06892287	0.09447445	0.03958868	0.74900026	0.000570
2490.0101	5.3934E-05	0.00017832	0.00028806	0.00035142	5.16E-05	0.05565029	0.036118	0.00371469	0.01417208	0.01942605	0.00814032	0.15401116	0.000117
2932.0101	1.6514E-05	5.4599E-05	8.8199E-05	0.0001076	1.5799E-05	0.01703934	0.01105883	0.00113739	0.00433929	0.00594799	0.00249245	0.04715607	3.5897E-
5362.0301	5.7779E-05	0.00019103	0.00030859	0.00037647	5.5278E-05	0.05961743	0.03869274	0.0039795	0.01518236	0.02081088	0.00872061	0.16499014	0.00012
11566.0101	5.0758E-05	0.00016782	0.00027109	0.00033072	4.8561E-05	0.05237318	0.0339911	0.00349594	0.01333752	0.0182821	0.00766095	0.14494182	0.000110
7921.0101	0.00026876	0.00088859	0.00143543	0.00175116	0.00025713	0.27731245	0.17998059	0.01851078	0.07062127	0.09680249	0.04056423	0.76745716	0.000584
6689.0101	1.301E-05	4.3013E-05	6.9484E-05	8.4767E-05	1.2447E-05	0.01342369	0.0087122	0.00089604	0.00341852	0.00468586	0.00196357	0.03714981	2.828E-
2941.0101	1.4456E-05	4.7794E-05	7.7206E-05	9.4188E-05	1.383E-05	0.01491551	0.00968043	0.00099562	0.00379843	0.00520661	0.00218179	0.04127842	3.1423E-
7254.0101	9.1805E-05	0.00030353	0.00049032	0.00059817	8.7831E-05	0.09472586	0.06147873	0.00632301	0.02412319	0.03306631	0.01385615	0.26215211	0.000199
6756.0101	3.6164E-05	0.00011957	0.00019315	0.00023563	3.4599E-05	0.03731476	0.02421793	0.00249078	0.0095027	0.0130256	0.00545826	0.10326793	7.8612E
3253.9999	6.8502E-05	0.00022648	0.00036586	0.00044634	6.5537E-05	0.07068161	0.04587359	0.00471804	0.018	0.02467309	0.01033904	0.19561006	0.000148
5379.0101	9.7109E-05	0.00032107	0.00051865	0.00063273	9.2907E-05	0.10019942	0.06503116	0.00668838	0.0255171	0.03497698	0.0146568	0.27730006	0.000211
2731.0101	7.7709E-06	2.5693E-05	4.1504E-05	5.0633E-05	7.4346E-06	0.00801816	0.00520393	0.00053522	0.00204193	0.00279893	0.00117287	0.02219012	1.6892E-
7528.0101	1.5617E-05	5.1633E-05	8.3408E-05	0.00010175	1.4941E-05	0.01611381	0.01045814	0.00107561	0.00410359	0.00562491	0.00235707	0.04459467	3.3947E-
10677.0101	7.4601E-06	2.4665E-05	3.9844E-05	4.8607E-05	7.1372E-06	0.00769744	0.00499577	0.00051381	0.00196025	0.00268697	0.00112595	0.02130253	1.6216E-
6597.0301		0.0001614	0.00026073	0.00031808	4.6705E-05	0.05037087	0.03269157	0.00336229	0.01282761	0.01758315	0.00736806	0.13940048	0.000106
2556.0201	2.2028E-05	7.283E-05	0.00011765	0.00014353	2.1075E-05	0.02272889	0.01475144	0.00151717	0.00578821	0.00793406	0.0033247	0.06290179	4.7883E-
11163.0101	2.6716E-05	8.8329E-05	0.00014269	0.00017407	2.556E-05	0.027566	0.01789081	0.00184005	0.00702005	0.00962257	0.00403225	0.07628842	5.8074E
8505.0101	0.00069267	0.00229015	0.00369951	0.00451324	0.0006627	0.71471434	0.463862	0.04770764	0.18201143	0.249488	0.10454575	1.97795896	0.00150
3133.0101	9.9555E-06	3.2915E-05	5.3171E-05	6.4867E-05	9.5246E-06	0.01027229	0.00666689	0.00068568	0.00261597	0.00358579	0.00150259	0.02842838	2.1641E-
3025.0101	4.5526E-05	0.00015052	0.00024315	0.00029663					0.01196265				
3464.0101		0.0001848	0.00029853	0.0003642	5.3476E-05	0.05767393	0.03743138	0.00384977	0.01468743	0.02013246	0.00843633	0.15961156	0.00012
6116.0101	3.1392E-05	0.00010379	0.00016766	0.00020454	3.0033E-05	0.03239072	0.02102214	0.0021621	0.00824873	0.01130675	0.00473799	0.08964074	6.8238E-
2489.0101	2.0777E-05	6.8694E-05	0.00011097	0.00013538	1.9878E-05	0.02143824	0.01391379	0.00143102	0.00545953	0.00748352	0.00313591	0.05932993	4.5164E
2809.0101		7.8733E-05	· · · · · · · · · · · · · · · · · · ·	Parameter was a second	and the second s	0.02457108	0.01594706	0.00164014	0.00625735	0.00857712	0.00359417	0.06800002	5.1764E
9282.0101		0.00018504			· · · · · · · · · · · · · · · · · · ·	the second second second second second second second second second second second second second second second se	· · · · · · · · · · · · · · · · · · ·		0.01470638		1	and the second sec	
		0.00098125					the second		0.07798523				0.000645
2397.0101		0.00015906	· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	f	· · · · · · · · · · · · · · · · · · ·		0.01264175		0.00726131	· · · · · · · · · · · · · · · · · · ·	
11313.0101		0.00020006		• •					0.01590023				
5613.0101	· · · _ · · · · · · · · · · · · · · · ·	0.00018018		Windows Conservation and a second second	and the minimum many control of			······································	0.01431955	-, -,			
4609.0101		0.00026283			. The second second second second second second second second second second second second second second second		· · · · · · · · · · · · · · · · · · ·		0.02088825				
11365.0101		0.00011595	······						0.00921557			0.1001477	
11574.0101		0.00015204		0.00022001					0.01208321				÷
4202.0101		0.00010983				0.03427597			0.00872883			and a star star	
		4.6467E-05					· · · · · · · · · · · · · · · · · · ·			a company of a large state of a state of a state of the s	· · · · · · · · · · · · · · · · · · ·		
3442.0101	1.40346-05	4.0407E-03	1.30026-03	3.10/4E-00	1.0440E-00	0.01400107	0.00341104	0.00030/30	0.00003231	0.00000200	0.00612121	0.04010220	0.0002-

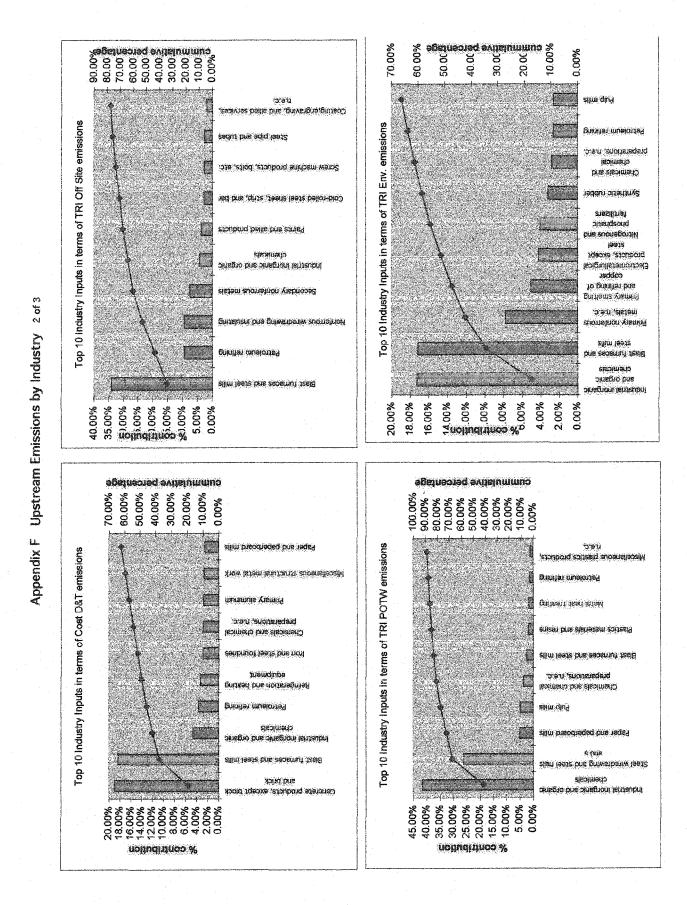
APPENDIX E Summary of Emissions for Dam Assessed in this Study 3 of4

Dom #	VOCa to all 10	NOv to air (97							TDI Dal UnGac		TOUTO	TOL TH OHONA	Cont DIT /
Dam # 2558.0201		NOx to air (ST	والوالا المتعاوية فتعاص ومحاد والمستعادين					and present strength and the strength of the s		····	and the second		
			ومراجعهم ومصر فستشت المعاد			0.00537758		والمواد ومتأثف والعادي ومستعد ومستعد					
11433.0101		0.00017731				0.05533398		i			·		
2323.0101	3.1021E-06	and an and a second s	1.6568E-05	and a second sec		0.00320079	to see the second of the secon		······································	· · · · · · · · · · · · · · · · · · ·	1 - · · · · · · · · · · · · · · · · · ·	0.00885812	·
2808.0101	1.8956E-05		0.00010124	- Characteristic de Carteris d	· · · · · · · · · · · · · · · · · · ·	0.01955946				· · · · · · · · · · · · · · · · · · ·			
8640.0101	construction and and and and and a	0.00198341				0.61898552			······		· · · · · · · · · · · · · · · · · · ·		
3777.0101	2.7092E-05			0.00017652		0.02795418					0.00408903	0.0773627	
2931.0101	1.5299E-05		8.1708E-05	and a second second of the second second second second second second second second second second second second		0.01578539					· · · · · · · · · · · · · · · · · · ·		J
11478.0101	3.197E-05		0.00017075	0.0002083		0.03298693		- where the second second second second second	0.00840056	· •• •• •• •• •• •• •• •• •• •• ••	The second second second second second second second second second second second second second second second se	0.09129072	
2528.0101	4.5679E-06	1.5103E-05	2.4397E-05	2.9763E-05	4.3702E-06	0.00471325	0.00305898	0.00031461	0.00120029	0.00164527	0.00068944	0.01304383	9.9295E-0
11132.0101	0.00013208	0.00043669	0.00070543	0.00086059	0.00012636	0.13628272	0.08844985	0.00909696	0.03470619	0.04757272	0.01993493	0.37715996	0.0002871
6338.0101	0.00015526	0.00051333	0.00082923	0.00101162	0.00014854	0.16019982	0.10397246	0.01069344	0.040797	0.05592155	0.02343343	0.44335008	0.000337
2608.0101	3.3729E-05	0.00011152	0.00018014	0.00021977	3.2269E-05	0.03480201	0.02258711	0.00232306	0.00886279	0.01214847	0.00509071	0.09631393	7.3318E-0
2375.0101	9.8909E-06	3.2702E-05	5.2826E-05	6.4446E-05	9.4628E-06	0.01020562	0.00662362	0.00068123	0.00259899	0.00356251	0.00149284	0.02824386	2.15E-0
2323.0301	7.8844E-06	2.6068E-05	4.211E-05	5.1372E-05	7.5432E-06	0.00813527	0.00527993	0.00054303	0.00207175	0.00283981	0.00119	0.02251421	1.7139E-0
2194.0101	1.1285E-05	3.7312E-05	6.0273E-05	7.3531E-05	1.0797E-05	0.01164432	0.00755736	0.00077727	0.00296538	0.00406472	0.00170329	0.03222543	2.4531E-0
4451.0101	4.3149E-05	0.00014266	0.00023046	0.00028115	4.1282E-05	0.0445223	0.02889574	0.00297189	0.01133819	0.01554156	0.00651256	0.12321465	9.3796E-0
2721.0101	3.2258E-05	0.00010665	0.00017229	0.00021018	3.0862E-05	0.0332846	0.02160229	0.00222177	0.00847636	0.01161878	0.00486875	0.09211454	7.0121E-0
7590.0101	6.4329E-05	0.00021269	0.00034357	0.00041915	6.1545E-05	0.06637575	0.04307901	0.00443062	0.01690346	0.02317003	0.0097092	0.18369367	0.0001398
6597.0201	0.00019811	0.00065499	0.00105807	0.0012908	0.00018953	0.20441099	0.13266628	0.01364456	0.05205595	0.07135451	0.02990048	0.56570371	0.0004306
1893.0301	5.008E-06	1.6558E-05	2.6748E-05	3.2631E-05	4.7913E-06	0.0051674	0.00335373	0.00034493	0.00131595	0.0018038	0.00075587	0.01430068	1.0886E-0
2300.0101	1.3647E-05	4.5119E-05	7.2885E-05	8.8917E-05	1.3056E-05	0.01408087	0.00913873	0.00093991	0.00358588	0.00491526	0.0020597	0.03896856	2.9664E-0
2326.0101	1.4428E-05	4.7703E-05	7.7059E-05	9.4008E-05	1.3804E-05	0.01488708	0.00966197	0.00099372	0.00379119	0.00519669	0.00217763	0.04119972	3.1363E-
2334.0101	1.8662E-05	6.17E-05	9.967E-05	0.00012159	1.7854E-05	0.01925534	0.01249705	0.00128531	0.00490363	0.00672153	0.0028166	0.05328879	4.0565E-0
2530.0101	5.8163E-06	1.923E-05	3.1064E-05	3.7897E-05	5.5645E-06	0.00600134	0.00389498	0.00040059	0.00152832	0.00209491	0.00087785	0.01660861	1.2643E-
5073.0101	2.5782E-05	8.5243E-05	0.0001377	0.00016799	2.4667E-05	0.02660284	0.01726571	0.00177576	0.00677476	0.00928635	0.00389136	0.07362288	5.6045E-0
2552.0101	4.2229E-05	0.00013962	0.00022554	0.00027515	4.0401E-05	0.04357266	0.02827941	0.0029085	0.01109635	0.01521007	0.00637365	0.12058653	9.1795E-0
2488.0101	5.7341E-05	0.00018958	0.00030626	0.00037362	5.486E-05	0.05916599	0.03839975	0.00394937	0.0150674	0.02065329	0.00865458	0.1637408	0.000124
2375.0301	the second second second second second second second second second second second second second second second s	0.00010928			3.1623E-05	0.03410512	0.02213482	0.00227654	0.00868532	0.0119052	0.00498877	0.09438531	7.185E-
2422.0101	2.1256E-05	7.0278E-05	0.00011353	0.0001385	and a second sec	0.02193259	second style states and strained						
11475.0101	5.2409E-05	0.00017328	0.00027991	0.00034148	5.014E-05	0.0540762	0.03509639	0.00360962	0.01377122	0.01887658	0.00791006	0.1496549	0.000113
2666.0101	1.3891E-05	4.5926E-05	7.4189E-05	9.0507E-05	1.329E-05	0.01433272	0.00930219	0.00095672	0.00365002	0.00500318	0.00209654	0.03966555	3.0195E-
2710.0101	2.7055E-05			0.00017628		0.02791604					\$1111111111111111111111111111111111111		
2288.0101	2.9988E-05		0.00016016			0.03094187							
2574.0101	7.9217E-06		4.2309E-05			0.00817377					0.00119563		1.722E-0
2077.0101	8.9176E-06	• • • • • • • • • • • • • • • • • • •	4.7628E-05			0.00920141	···· · · · · · · · · · · · · · · · · ·	Contraction of the second			0.00134595	10	
2458.0101	1.2237E-05			7.9733E-05		0.01262649					0.00184696	and community of the second second	
2457.0101	1.701E-05		9.0849E-05			0.01755134	The second		1919 P. B. B. B. B. B. B. B. B. B. B. B. B. B.		a minimum and the first statement of the		
	0.00013034		0.00069614		Second Se	0.13448914		· ····	Contraction of the second second of the second		A REAL PROPERTY AND A REAL		
8277.0101	9.2684E-06					0.00956336	· · · · · · · · · · · · · · · · · · ·	17 M T = 7 17 1	·····	and the state of t			
2531.0101		process and a second seco	7.5478E-05		k	0.01458172				second and the second s			· · · · · · · · · · · · · · · · · · ·
2368.0101		0.00163574			j	· · · · · · · · · · · · · · · · · · ·	0.33131362		0.13000174		0.07467184		
2325.0102						0.00658437			an and an an a state of the sta	· · · · · · · · · · · · · · · · · · ·	0.00096314	I	
2323.0102		farm survey of the state of the	The second s			0.00318173					0.00046541	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
2403.0101		······································			and the second sec	0.01086415							
	5.1603E-06		2.7561E-05			0.00532449	and characterized in the second secon					j · · · · · _ · · · · · · · · · · · · ·	
2002.0101	J.1003E-06	1.7001E-05	2./00(E-05	3.30232-05	4.93/2-00	0.00002449	0.00345509	0.00035541	0.001000000	0.00100004	0.00077865	0.014/0042	1.121/2

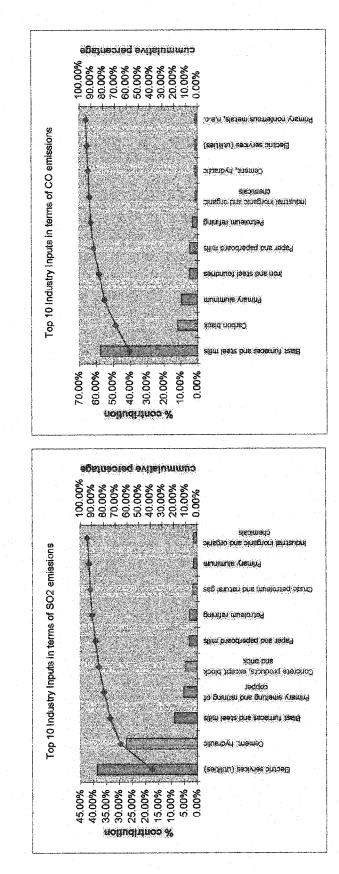
APPENDIX E Summary of Emissions for Dam Assessed in this Study 4 of4

i r		· · · · · · · · · · · · · · · · · · ·					· · · · · · · · · · · · · · · · · · ·							
1	Dam #		NOx to air (ST	CO to air (ST)	SO2 to air (ST	PM10 to air (S	Fossil CO2 (m	TRI Rel Air (lbs	TRI Rel Water	TRI Rel UnGno	TRI Rel Land (TRI TI POTW	TRI Tf OffSite	Cost D&T (\$P
	2323.0401	2.383E-05	7.8788E-05	0.00012727	0.00015527	2.2799E-05	0.0245884	0.0159583	0.00164129	0.00626176	0.00858317	0.0035967	0.06804796	5.1801E-05
	2727.0101	2.0616E-05	6.8161E-05	0.00011011	0.00013433	1.9724E-05	0.02127177	0.01380575	0.0014199	0.00541714	0.00742542	0.00311156	0.05886925	4.4814E-05
	2287.0101	6.1712E-06	2.0403E-05	3.296E-05	4.0209E-05	5.9041E-06	0.00636755	0.00413265	0.00042504	0.00162158	0.00222274	0.00093142	0.01762207	1.3415E-05
	2513.0101	1.8279E-05	6.0436E-05	9.7629E-05	0.0001191	1.7488E-05	0.01886106	0.01224116	0.00125899	0.00480322	0.0065839	0.00275893	0.05219764	3.9735E-05
	2519.0101	6.0755E-05	0.00020087	0.00032449	0.00039586	5.8125E-05	0.06268811	0.04068567	0.00418447	0.01596435	0.02188277	0.00916978	0.17348821	0.00013207
	1893.0101	8.6788E-06	2.8694E-05	4.6353E-05	5.6548E-05	8.3032E-06	0.00895495	0.00581192	0.00059775	0.0022805	0.00312594	0.0013099	0.02478266	1.8866E-05
	2335.0101	8.3361E-06	2.7561E-05	4.4522E-05	5.4315E-05	7.9753E-06	0.00860133	0.00558241	0.00057414	0.00219044	0.0030025	0.00125817	0.02380403	1.8121E-05
	2323.0701	3.2185E-05	0.00010641	0.0001719	0.00020971	3.0792E-05	0.0332093	0.02155341	0.00221674	0.00845719	0.01159249	0.00485773	0.09190613	6.9963E-05
1	1855.0101	3.6195E-06	1.1967E-05	1.9331E-05	2.3584E-05	3.4629E-06	0.00373468	0.00242387	0.00024929	0.00095109	0.00130368	0.0005463	0.01033567	7.8679E-06
	2458.0301	4.004E-06	1.3238E-05	2.1385E-05	2.6089E-05	3.8308E-06	0.00413145	0.00268138	0.00027578	0.00105213	0.00144218	0.00060433	0.01143371	8.7038E-06
	2365.0101	1.4819E-05	4.8994E-05	7.9145E-05	9.6553E-05	1.4177E-05	0.01529016	0.00992358	0.00102063	0.00389384	0.00533739	0.00223659	0.04231523	3.2212E-05
	2611.0101	1.004E-05	3.3195E-05	5.3624E-05	6.5418E-05	9.6056E-06	0.01035962	0.00672357	0.00069151	0.00263821	0.00361627	0.00151537	0.02867005	2.1825E-05
	2327.0101	1.7009E-05	5.6235E-05	9.0842E-05	0.00011082	1.6273E-05	0.01754987	0.01139017	0.00117146	0.0044693	0.0061262	0.00256713	0.04856893	3.6973E-05
	2458.040	1.9173E-05	6.339E-05	0.0001024	0.00012492	1.8343E-05	0.01978281	0.01283939	0.00132052	0.00503795	0.00690566	0.00289376	0.05474856	4.1677E-05
	2323.020	·····			0.00024894	en en entreger des relacións en el seu 🗕	0.03942204	and a second sec		and an a second of the part of the second second second second second second second second second second second				
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	2600.010	· j · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	the second resident and the second second second second	9.1226E-05		0.01444644		······································			<u></u>		and the second sec
	2534.010	2.3612E-05	7.8068E-05	0.00012611	0.00015385	the second s	0.02436365	commencement also in the local state of the state of the state of the		and the second of the second sec				
	2283.030	1.0237E-05	3.3845E-05	5.4673E-05	6.6699E-05		0.0105624		and a second second second second second second second second second second second second second second second		waar naameerik kan seen tiin too too aanaa	·		
	2520.010		· · · · · · · · · · · · · · · · · · ·		8.3551E-05		0.01323117				terms as an enternance of the state of	have been accessible and the second second	1	
	2529.010	3.1044E-05		and a summer in and one	0.00020228	- the second sec	······································	· · · · · · · · · · · · · · · · · · ·		and the second second second second second second second second second second second second second second second	and the second s	a concern a concern contraction		the second second
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	1904.010				5.3738E-05	No. 1995, page 1996 and a second second	deservation and the second second second		 Name and service and price instance any resource 				0.02355113	· · · · · · · · · · · · · · · · · · ·
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	2942.010		· · · · · · · · · · · · · · · · · · ·	the second of the second	0.00063682				· · · · · · · · · · · · · · · · · · ·			and the second s	······	
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	2631.010	0.00024232												
	2572.010				5.5116E-05									
		0.00025361												
		0.00013564												
		2.6541E-05												
.		0.00012399												
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	· · · · · · · · · · · · · · · · · · ·	7.2022E-05					0.07431407							
1	2077.020				0.00031281									
1	2077.030		0.00018831				0.0587674							
L	2329.010	4.8E-05	0.0001587	0.00025636	0.00031275	4.5922E-05	0.04952701	0.03214389	0.00330596	0.01261271	0.01728858	0.00724463	0.13706511	0.00010434





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Appendix F Upstream Emissions by Industry 3 of 3

Appendix G - Assessment of Environmental Im	pacts Based on Literature R	leview. Page 1 c	of 2

Air Emissions					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
CO_2 , SO_2 , NO_x , CH_4 , particulate	Released from production of construction materials	Human health, terrestrial ecosystems	Partially quantified	None	Recognized
CO ₂ , CH ₄ ,	Released from biomass decomposition in impoundment	Global warming	Partially quantified	None	None

Hydrology					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
Flow Alteration	D tailrace velocity	Bio-diversity, aquatic	None	Assessed	Quantified
	dewatering construction	Bio-diversity, aquatic	None	Assessed	Quantified
	> in-stream flow	Bio-diversity, aquatic	None	Assessed	Quantified
	Entrainment	Bio-diversity, aquatic	None	Assessed	Quantified
	Dam as barrier to fish migration	Bio-diversity, aquatic	None	Assessed	Quantified
Flooding	Flooding from dam failure	Human injury & property damage	None	Assessed	Recognized
Fluctuation	Flow D inundates and dries habitat	Aquatic organisms, bio- diversity	None	Assessed	Recognized

Water Quality					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
Emissions from infrastructure construction	Direct and indirect releases from materials and processes	Eutrophication, biodiverstiy, aquatic	Recognized	None	Recognized
Dissolved Oxygen	Reduced aeration	Aquatic org.	None	Assessed	Assessed
D Temperature	Temp differential between impoundment and river	Aquatic Org.	None	Assessed	Assessed
Increased sedimentation	Erosion from construction, or dam failure	Aquatic Org., human health and property, recreation	None	Assessed	Quantified
Heavy metals	Contaminated sediments, or anoxic release	Aquatic orgs, human health	None	Assessed	Recognized
New impoundment	Stratified temp, nutrients, and oxygen	Aquatic ogr. and recreation.	None	Assessed	Recognized
salinization			None	None	None

Land Use					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
Solid Waste	Direct and indirect land fill from construction materials and processes		Partially Quantified	None	None
D in Land use	New transmission path, and roads	Bio-diversity	None	Assessed	Assessed
D in Land use	Increased/ decreased recreational usage	Bio-diversity, aquatic effects	None	Assessed	Assessed
Creation of impoundment	Decreased terrestrial habitat, increased aquatic habitat	D in bio-diversity	None	Assessed	Recognized
Socio oconomio				r	1997 - 19

Socio-economic					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality
			<u> </u>		Cost

Land use change	New infrastructure	Aesthetics, culture, recreation	None	Assessed	Assessed
Jobs	New construction, operation & maintenance	Economic benefit	None	Assessed	Quantified
Decimation of fisheries,			None	None	Recognized
Flooded hunting territories,			None	None	Recognized

Other	· · · ·				
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
seismic effects			None	None	None
D local climate	Weather changes from large impoundment		None	None	None
D speed of earth's rotation	Change in rotation of earth caused by large impoundment		None	None	None
D magnetic field	Change in magnetic flux lines caused by flooding magnetic fields and change in earth rotation.		None	None	None

(Tables adapted from DOE, 94)

Appendix H NID Classification Page 1 of 2

1) The NID ID is the Corps Identification No assigned to each dam in the 1981 National Inventory of Dams update, under the National Dam Inspection Program (P.L. 92-367). For those dams that were not included in the 1981 update, an identification number was generated.

2) STATE (ALPHANUMERIC, 2) The two letter abbreviation for the state in which the dam is located. A calculated field based on field item #1 NID ID.

3) DAM_NAME (ALPHANUMERIC, 65) Official name of the dam. For dams that do not have an official name, the popular name is used.

4) OTHER_NAME (ALPHANUMERIC, 65) Reservoir name or names in common use other than the official name of the dam. Names are separated with semi-colons.

5) HAZARD (ALPHANUMERIC, 11) Term indicating the potential hazard to the downstream area resulting from failure or mis-operation of the dam or facilities. Terms used are as follows: Low, Significant, High.

6) EAP (ALPHANUMERIC, 3) Term indicating whether this dam has an Emergency Action Plan (EAP), which is defined as a plan of action to be taken to reduce the potential for property damage and loss of life in an area affected by a dam failure or large flood. Terms used are as follows: Yes; No; N/R. (N/R = Not required by submitting agency. For name of submitting agency, see field item #53 Source Agency)

7) STATE_NAME (ALPHANUMERIC, 20) The state name in which the dam is located. A calculated field based on the NID ID.

8) CONG_DIST (ALPHANUMERIC, 5) The 104th Congressional District in which the dam is located (example, KS-02). A calculated field based on items #56 LONGITUDE_X and #57 LATITUDE_Y, using as a source the MapInfo Corporation 104th Congressional District Boundaries dataset.

9) COUNTY (ALPHANUMERIC, 30) Name of county in which the dam is located.

10) NEAR_CITY (ALPHANUMERIC, 30) Name of the nearest downstream city, town, or village that is most likely to be affected by floods resulting from the failure of the dam.

11) DIST_CITY (NUMERIC) Distance from the dam to the nearest downstream affected City-Town-Village, to the nearest mile. (See field item #10 NEAR CITY)

12) RIVER (ALPHANUMERIC, 30) Official name of the river or stream on which the dam is built. If the stream is unnamed, it is identified as a tributary ("TR") to the named river. If the dam is located offstream, the name of the river or stream is entered plus "-OS" or "OFFSTREAM".

13) PRM_PURPOSE (ALPHANUMERIC, 15) Term indicating the primary purpose for which the reservoir is used. A calculated field based on the leading code provided in field item #26 PURPOSE. Terms used are as follows: Irrigation; Hydroelectric; Flood Control; Navigation; Water Supply; Recreation; Fire/Farm Pond; Fish & Wildlife; Debris Control; Tailings; Other.

14) NID_DAMTYP (ALPHANUMERIC, 8) Term indicating dam type as one of the following: Arch, Buttress, Gravity. A calculated field, based on the codes provided in field item #27 DAM TYPE, using the following precedence: (VA or MV) = Arch; B = Buttress; not (VA, MV or B) = Gravity.

15) YEAR_COMPL (NUMERIC) Year when the original main dam structure was completed.

16) NID_HEIGHT (NUMERIC) A calculated field based on the maximum value of field items #28 DAM HEIGHT, #29 HYDRAULIC HEIGHT, and #30 STRUCTURAL HEIGHT, providing a single height value to facilitate database queries.

Appendix H NID Classification Page 1of 2

1) The NID ID is the Corps Identification No assigned to each dam in the 1981 National Inventory of Dams update, under the National Dam Inspection Program (P.L. 92-367). For those dams that were not included in the 1981 update, an identification number was generated.

2) STATE (ALPHANUMERIC, 2) The two letter abbreviation for the state in which the dam is located. A calculated field based on field item #1 NID ID.

3) DAM_NAME (ALPHANUMERIC, 65) Official name of the dam. For dams that do not have an official name, the popular name is used.

4) OTHER_NAME (ALPHANUMERIC, 65) Reservoir name or names in common use other than the official name of the dam. Names are separated with semi-colons.

5) HAZARD (ALPHANUMERIC, 11) Term indicating the potential hazard to the downstream area resulting from failure or mis-operation of the dam or facilities. Terms used are as follows: Low, Significant, High.

6) EAP (ALPHANUMERIC, 3) Term indicating whether this dam has an Emergency Action Plan (EAP), which is defined as a plan of action to be taken to reduce the potential for property damage and loss of life in an area affected by a dam failure or large flood. Terms used are as follows: Yes; No; N/R. (N/R = Not required by submitting agency. For name of submitting agency, see field item #53 Source Agency)

7) STATE_NAME (ALPHANUMERIC, 20) The state name in which the dam is located. A calculated field based on the NID ID.

8) CONG_DIST (ALPHANUMERIC, 5) The 104th Congressional District in which the dam is located (example, KS-02). A calculated field based on items #56 LONGITUDE_X and #57 LATITUDE_Y, using as a source the MapInfo Corporation 104th Congressional District Boundaries dataset.

9) COUNTY (ALPHANUMERIC, 30) Name of county in which the dam is located.

10) NEAR_CITY (ALPHANUMERIC, 30) Name of the nearest downstream city, town, or village that is most likely to be affected by floods resulting from the failure of the dam.

11) DIST_CITY (NUMERIC) Distance from the dam to the nearest downstream affected City-Town-Village, to the nearest mile. (See field item #10 NEAR CITY)

12) RIVER (ALPHANUMERIC, 30) Official name of the river or stream on which the dam is built. If the stream is unnamed, it is identified as a tributary ("TR") to the named river. If the dam is located offstream, the name of the river or stream is entered plus "-OS" or "OFFSTREAM".

13) PRM_PURPOSE (ALPHANUMERIC, 15) Term indicating the primary purpose for which the reservoir is used. A calculated field based on the leading code provided in field item #26 PURPOSE. Terms used are as follows: Irrigation; Hydroelectric; Flood Control; Navigation; Water Supply; Recreation; Fire/Farm Pond; Fish & Wildlife; Debris Control; Tailings; Other.

14) NID_DAMTYP (ALPHANUMERIC, 8) Term indicating dam type as one of the following: Arch, Buttress, Gravity. A calculated field, based on the codes provided in field item #27 DAM TYPE, using the following precedence: (VA or MV) = Arch; B = Buttress; not (VA, MV or B) = Gravity.

15) YEAR COMPL (NUMERIC) Year when the original main dam structure was completed.

Appendix H NID Classification Page 2 of 2

16) NID_HEIGHT (NUMERIC) A calculated field based on the maximum value of field items #28 DAM HEIGHT, #29 HYDRAULIC HEIGHT, and #30 STRUCTURAL HEIGHT, providing a single height value to facilitate database queries.

17) NID_STOR (NUMERIC) A calculated field based on the maximum value of field items #31 NORMAL STORAGE, and #32 MAXIMUM STORAGE providing a single storage value to facilitate database queries.

18) DAM_LENGTH (NUMERIC) Dam length in feet. It is defined as the length along the top of the dam. Included in dam length are spillway, powerplant, navigation lock, fish pass, etc., if these form part of the length of the dam; if detached from the dam, these structures are not included.

19) MAX_DISCH (NUMERIC) Number of cubic feet per second (cu ft/sec) which the spillway is capable of discharging when the reservoir is at its maximum designed water surface elevation.

20) OWNER (ALPHANUMERIC, 50) Name of the owner of the dam.

21) OWN_TYPE (ALPHANUMERIC, 14) Term indicating owner type. Terms used are as follows: Federal, State, Local Gov't, Public Utility, Private.

~22) STATE_AGCY (ALPHANUMERIC, 30) Name of the primary state agency with regulatory or approval authority over the dam.

23) FED_AGCY (ALPHANUMERIC,20) Code identifying federal agency involvement in the dam. Codes are concatenated if several agencies were involved. See field items #43-50 and the related Federal Agency

Ap	oendix G -	Assessment	of Environ	mental Imp	acts Based	on Litera	ture Review.	Page 1 of 2	1

Air Emissions					· · · · ·
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
CO_2 , SO_2 , NO_x , CH_4 , particulate	Released from production of construction materials	Human health, terrestrial ecosystems	Partially quantified	None	Recognized
CO ₂ , CH ₄ ,	Released from biomass decomposition in	Global warming	Partially quantified	None	None
	impoundment		1.		

Hydrology			1		
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
Flow Alteration	Δ tailrace velocity	Bio-diversity, aquatic	None	Assessed	Quantified
	dewatering construction	Bio-diversity, aquatic	None	Assessed	Quantified
· · · · · · · · · · · · · · · · · · ·	> in-stream flow	Bio-diversity, aquatic	None	Assessed	Quantified
	Entrainment	Bio-diversity, aquatic	None	Assessed	Quantified
	Dam as barrier to fish migration	Bio-diversity, aquatic	None	Assessed	Quantified
Flooding	Flooding from dam failure	Human injury & property damage	None	Assessed	Recognized
Fluctuation	Flow Δ inundates and dries habitat	Aquatic organisms, bio- diversity	None	Assessed	Recognized

Water Quality					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
Emissions from infrastructure construction	Direct and indirect releases from materials and processes	Eutrophication, biodiverstiy, aquatic	Recognized	None	Recognized
Dissolved Oxygen	Reduced aeration	Aquatic org.	None	Assessed	Assessed
∆ Temperature	Temp differential between impoundment and river	Aquatic Org.	None	Assessed	Assessed
Increased sedimentation	Erosion from construction, or dam failure	Aquatic Org., human health and property, recreation	None	Assessed	Quantified
Heavy metals	Contaminated sediments, or anoxic release	Aquatic orgs, human health	None	Assessed	Recognized
New impoundment	Stratified temp, nutrients, and oxygen	Aquatic ogr. and recreation.	None	Assessed	Recognized
salinization			None	None	None

Land Use					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
Solid Waste	Direct and indirect land fill from construction materials and processes		Partially Quantified	None	None
Δ in Land use	New transmission path, and roads	Bio-diversity	None	Assessed	Assessed
Δ in Land use	Increased/ decreased recreational usage	Bio-diversity, aquatic effects	None	Assessed	Assessed
Creation of impoundment	Decreased terrestrial habitat, increased aquatic habitat	Δ in bio-diversity	None	Assessed	Recognized

Socio-economic					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality
					Cost

Land use change	New infrastructure	Aesthetics, culture, recreation	None	Assessed	Assessed
Jobs	New construction, operation & maintenance	Economic benefit	None	Assessed	Quantified
Decimation of fisheries,			None	None	Recognized
Flooded hunting territories,			None	None	Recognized

Other					
Impact Area	Path	Affect	Hydro LCA	FERC	Externality Cost
seismic effects			None	None	None
Δ local climate	Weather changes from large impoundment		None	None	None
Δ speed of earth's rotation	Change in rotation of earth caused by large impoundment		None	None	None
Δ magnetic field	Change in magnetic flux lines caused by flooding magnetic fields and change in earth rotation.		None	None	None

(Tables adapted from DOE, 94)

APPENDIX I Per Unit Externality Values Used in This Study 1 of 2

	A	В	С	D	E .	F	G	н	· · · ·	L	к	L	· · M	N	0	P	Q	R	S
2 0	onventional A	Air Pollutants (1992 \$ /metric	ton)		Greenhouse G	as (1992 \$ / me	tric ton)			1	1		1	1		1		T
3		Low	Midpoint	High	Approximation of the second second second second second second second second second second second second second	CO2	\$24		1				1	1	1	1	1	l	T
4 VC	oc	\$87	\$1,485			CH4	\$128		· · · · · · · · · · · · · · · · · · ·							1	1		
5 PM		\$699	\$2,970			Nitrous Oxide (i					ł	1		1		1			
6 NK		\$175	\$2,009			Tanous Oxido (· · · · · · · · · · · · · · · · · · ·		+	-		1
7. 50		\$1,747	\$5,067	\$5,242		•••••			+ · · · · · · · · · · · · · · · · · · ·		·•••••••••••••••••••••••••••••••••••••							1	
8 CC		\$0	\$2				· · · · · · · · · · · · · · · · · · ·		4			••••••••••							
9 Le		\$174,720	\$742,560							i a como	4 / a	+				+			
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	isposal & Inc	ceneration (1992	\$/ metric ton)							1					1	· · · · · · · · · · · · · · · · · · ·		
17		Lendilli					<u> </u>					<u> </u>					: 3	L	
18 Ur	hban	Rural	Onsite										1	1			1		
19	4	4	3	1															1
20		Incine	rator				1				1	1		1			1	1	
	irban			Onsite-rural							1			1	1	1	1		1
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26	10.58	ACETALDEHYDE		4		C.I. SOLVENT Y		*******************************	0.01	DIETHYL PHT			0.00						+
27		ACETAMIDE				C.I.FOOD RED 1	5			DIETHYL SUL				METHYL ISOC				QUINONE	
28		ACETONE	<u> </u>		8,653.39		1		0.01	DIMETHYL PH				METHYL MET		1		QUINTOZENE	
29		ACETONITRILE				CADMIUM COMP				DIMETHYL SU		1	0.00		T-BUTYL ETHER			SACCHARIN (
30		ACROLEIN		· · · · · · · · · · · · · · · · · · ·		CALCIUM CYAN	MIDE				ENE (MIXED IS	MERS)		METHYLENE		1		SEC-BUTYL A	LCOHOL
31	6,249.67	ACRYLAMIDE				CAPTAN			5.77	EPICHLOROHN	(DRIN			METHYLENER	315(PHENYLISOC	YANATE)		SELENIUM	
32	4.18	ACRYLIC ACID		· ·	1	CARBARYL				ETHYL ACRYL	ATE			MOLYBDENU		1	1	SELENIUM CC	MPOUNDS
33	326.91	ACRYLONITRILE			0.01	CARBON DISULF	NDE .		1	ETHYL CHLOP	OFORMATE			MONIOCHLOF	OPENTAFLUOR	DEHTANE		SILVER	1
04		ALLYL ALCOHOL			72.11	CARBON TETRA	CHLORIDE		0.00	ETHYLBENZER	Æ	1	1	N,N-DIMETHY	LANILINE			SILVER COMP	OUNDS
35	4.81	ALLYL CHLORIDE				CARBONYL SULL	FIDE		1	ETHMLENE	1	1		N-BUTYL ALC	COHOL		0.00	STYPENE	
36		ALPHA-NAPHTH				CATECHOL	1	·····	0.24	ETHYLENE GL	YCOL	1		N-DIOCTYL P		1		STYPENE OXI	DE
37		ALUMINUM (FUM				CHLORDANE				ETHYLENE OX					PHENYLAMINE	1	1	SULFURIC AC	
38		ALUMINUM OXIDE		A		CHLORINE	+	*****		ETHYLENE TH				NA				TERT-BUTYL	
39	0 50	AMMONIA		1	01.01	CHLORINE DIOX	ne			ETHYLENEM			· · · • • · · · · · · · · · · · · · · ·	NAPHTHALE			35.58	TETRACHLOP	
40	0.50	AMMONIUM NITE			24.04	CHLOROACETIC				FLUOMETURC				NICKEL	· ·	1	00.00	TETRACHLOF	
40		AMMONIUM SUL		4						FORMALDEHY				NICKEL COM				THALLIUM CC	
			FATE (SOLUTION	y	0.24	CHLOROBENZEN			62.50		<u>ua</u>		- 0.12			· [THOUREA	AND COUNDO
42		ANILINE				CHLOROETHAN	=		- · · ·	FREON 113				NITRIC ACID					
43		ANTHRACENE				CHLOROFORM				GLYCOL ETHE				NITRILOTRIA		+ •	4	THORIUMDIO	
44		ANTIMONY	مترجبا ويترجب		8.65	CHLOROMETHA			6,249.67	HEPTACHLOF		<u>.</u>	0.46	NTROBENZE		+	-		TRACHLORIDE
45		ANTIMONY COMP	OUNDS				LMETHYLETHER		1		D-1,3-BUTADIEN	<u>е</u>	· •••••••	NTROGLYCE				TOLUENE	1
46	20,671.98		<u>k</u>			CHLOROPHENO				HEXACHLORC		<u> </u>		O-ANISIDINE		+		TOLUENE-2,4	
47		ARSENIC COMPO			I	CHLOROPRENE					CYCLOPENTAL	RENE		O-CRESOL	1	l	68.68	TOLUENE-2,6	
		ASBESTOS (FRIA	BLE)	J	Į	CHLOROTHALO	NIL			HEXACHLOR	ETHANE			O-DINITROBE		·		TOLUENEDIIS	
49		BARIUM	I	I	57,689.25					HYDRAZINE	I			O-TOLUIDINE	·			TRICHLORFO	
50	9.61	BARIUM COMPOL		1		CHROMIUM COM	POUNDS		23,556.44	HYDRAZINE S				O-XYLENE	·			TRICHLOROE	
51		BENZAL CHLORIE	Œ			COBALT				HYDROCHLOU	RIC ACID	1		P-ANISIDINE			0.00	TRICHLOROFI	
52	39.90	BENZENE	1	T		COBALT COMPC	UNDS	·	1.60	HYDROGEN C	YANIDE	1		P-CRESIDINE			1	TRIFLURALIN	
53		BENZOK TRICHL	ORIDE	1		COPPER			1	HYDROGENFI		1	ſ	P-CRESOL				URETHANE	1
54		BENZOYL CHLOR		1		COPPERCOMPC	NNOS		1	HYDROQUINO		1		P-DINITROBE	NZENE		1	VANADIUM (F	UME OR DUS
55		BENZOYL PEROX		1	•	CREOSOTE			1	SOBUTYRALL		-			PHENYLAMINE	•	0.05	VINYL ACETA	
56		BENZYLCHLORIC		+		CRESOL (MIXED	ISOMERS)	l	+	ISOPROPYL A			- 1	P-PHENYLEN		1		VINYL BROM	
57	11 597 00	BERYLLIUM	<u>~</u>	· • · · · · · · · · · · · · · · · · · ·	0.00	CUMENE		ł		ISOPROPYL A			····	P-XYLENE	AND A VIN PL			VINYL CHLOF	
58					U.01				-1	LEAD	LOUTULE		··· · · · · · · · · · ·	PARATHION		-1	403.84	VINYLIDENE	
	11,537.85	BERYLLIUM COM	FOUNERS			CUMENEHYDRO	- CHUNIDE	l									ada a ganadan		
59		BIPHENML	L	1		CUPFERFICIN	1			LEAD COMPC	UNDS		107.0	PENTACHLO		-{		XYLENE (MIX	
60		BIS(2-CHLORO-1		ETHER	1,045,222.22	CYANIDE COMP			13,936.30		·		a barana ang sa sa sa sa sa sa sa sa sa sa sa sa sa	PERACETIC /	ν <u>ω</u> D	- 	· • · · · · · · · · · · · · · · · · · ·	ZINC (FUME (
61	1,586.45	5 BIS(2-CHLOROET	HYL) ETHER		<u>.</u>	CYCLOHEXANE		l	_	MCRESOL			0.00	PHENOL				ZINC COMPO	
62	48.07	BIS(2-ETHYLHEX	YL) ADIPATE	1	1	DECABROMODI	HENYLOXIDE			MOINTROBE	NZENE			PHOSGENE				1,1,1-TRICHU	
63	298,061.93	BIS(CHLOROMET	HYL) ETHER	L	1	DI(2-ETHYLHEX	YL) PHTHALATE	L	1	M-XYLENE	1		0.4	PHOSPHORIC			1	1,1,2,2-TETR	
64			HUDROMETHA	NE	1		YL) PHTHALATE (DEHP)	1	MALEIC ANHY	'DRIDE			PHOSPHORI	S (YELLOW OR	WHITE)	1	1,1,2-TRICHL	ORDETHANE
		BROMOFORM		1	1		NE (MIXED ISOMEP		1	MANEB	1		1	PHTHALIC AM	HYDRIDE	1	1	1,1-DIMETHY	LHYDRAZINE
65			An		· · · · · · · · · · · · · · · · · · ·			·			1	· · · · · · · · · · · · · · · · · · ·	1			1	- I		
	0.96	5 BROMOMETHANE		1		DIBENZOFURAN		1	96.15	MANGANESE	1		1	PICRIC ACID	1	1	1	1,2,4-1 HICHL	DROBENZENE

APPENDIX I Per Unit Externality Values Used in This Study 2 of 2

	A B C	D	E F G	Н	1	. J	к	L	м	N	0	P	Q	R	S
68	BUTYL ACRYLATE	1	DIBUTYL PHTHALATE		16.02	MERCURY	-			POLYCHLORIN	ATED BIPHENYLS	3		1,2-BUTYLENE	OXIDE
69	0.17 BUTYL BENZYL PHTHALATE		0.34 DICHLOROBENZENE (MIXED ISOMER	S)		MERCURY CON	POUNDS			PROPANE SUL	TONE			1,2-DIBROMO-3	3-CHLOROPROF
70	BUTYRALDEHYDE		1,057.64 DICHLOROBROMOMETHANE			METHANOL	1			PROPIONALDE	HYDE			1,2-DIBROMOE	THANE
71	C.I. BASIC GREEN 4		DICHLORODIFLUOROMETHANE			METHOXYCHLC	XR		1	PROPOXUR				1,2-DICHLOROE	BENZENE
72	C.I. BASIC RED 1		0.01 DICHLOROMETHANE		6.87	METHYL ACRY	LATE			PROPYLENE				1,2-DICHLOROI	ETHANE
73	C.I. DISPERSE YELLOW 3	-	DICHLORDTETRAFLUOROETHANE		0.00	METHYLETHYL	LKETONE	1	17.79	PROPYLENE O)	KIDE			1,2-DICHLOROE	ETHYLENE
74			9.61 DICHLORVOS			METHYLHYDR	AZINE		1	PROPYLENEM	NE			1,2-DICHLOROF	PROPANE
75			DICOFOL			METHYL KODIDI	E			PYRIDINE				1,3-BUTADIEN	ε .
76			DIETHANOLAMINE				1							1,3-DICHLOROE	BENZENE
77				·····										1,3-DICHLOROF	PROPYLENE
78									1					1.4-DICHLORO	BENZENE
79														1,4-DIOXANE	
80	······································	1												2,3-DICHLOROF	PROPENE
81				·····			1							2,4,5-TRICHLO	
82		1									1			2,4-0	
83		1					1							2,4-DIAMINOTO	OLUENE
84		1					1				1			2,4-DICHLORO	IPHENOL .
85											1			2,4-DIMETHYL	PHENOL
86														2,4-DINITROPH	HENOL
87		1					1				1			2,4-DINITROTO	JLUENE
88		1				1					1			2,6-XYLIDINE	
89														2-ETHOXYETH	
90								1						2-METHOXYET	THANOL
91		1												2-NITROPHEN	
92													1	2-NITROPROP/	
93								1					<u> </u>	2-PHENYLPHE	
94														3,3'-DICHLORC	
95		1				1								3,3'-DIMETHOX	
96					f /////									4,4'-DIAMINOD	
97		1				1	1						l	4,4'-ISOPROPY	
98						1	1								NEBIS(2-CHLOP
99						ļ								4.4'-METHYLEI	
100					ļ									4,6-DINITRO-O	
101					ļ									4-AMINOAZOBI	
102					Í				· · ·				[4-AMINOBIPHE	
103		. (,	ļ	+							 	4-NITROPHEN	
104		1.			1	1	1				1		L	5-NITRO-O-AN	ISIDINE

APPENDIX J Hydro Externality Estimates per Megawatt Hour 1013

	SCA AD	\$4.727	\$1.786	\$10.147	\$0.410	51.125	\$17.538	\$3.066	\$4.027	\$12.452	\$0.306	\$6.613	\$2.023	\$1.614	\$3.795	\$34.519	\$2.076	\$0.218	\$0.370 *17 006	\$12.464	\$9.057	\$21.247	\$5.367	\$2.147	\$1.792	\$14.684 \$4.684	56.401	\$4.665	\$9.912	\$5.149	\$2.016	\$3.951	\$1.420	\$6.688	\$1.481	\$1.593	\$0.805	\$30.991	\$0.538	\$8.702	\$11.283	\$2.740	\$6.276	\$1.058	\$12.884	\$4.990	\$1.311	\$4.850	\$21.239	\$1.065	\$9.096	\$2.695	\$8.938	\$0.945	\$1.372	\$0.905 \$2 005	\$3.000
1	- I		2		_	· 1	÷	1			<u> </u>	_	_				-4									Ĺ.	-i	+		hard	- i.		4								.i.,		land	-			فسأد			. k			\$7,157				\$0.805 \$3 805
Total Imaged T																																																					\$9.096		\$7.157	58.938 50.045	51.345
																																																	\$1.061 e0.108	\$0.642	\$1.664	\$0.125 50.012	\$2.410	\$0.061	\$2,168	\$1.866	40.5/4
Inclusion no	Upstream no	\$3.371	\$1.504	\$2.516	\$0.374	060 V4	\$2.036	\$16.684	\$2.882	\$3.856	\$8.179	\$0.215	\$2.165	\$0.641	\$0.686	\$2.680	\$2.078	\$2.008	50.171	59.762	\$11.743	\$7.133	\$13.048	\$7.332	\$3.034	302.14	080.16 075 715	\$4.258	\$3.926	\$3.310	\$0.815	\$4.956	81 831	\$2.626	\$5.284	\$0.977	\$5.379	\$1,195	\$0.776	\$1,566	\$1.949	\$7.888	\$4.055	\$8.129	\$2.270	\$0.769	\$7.115	\$19.104	\$3.928	\$4.208	\$19.575	\$0.948	\$6.686	\$2.634	\$4.989	\$7.073	2000.00
Total Inter	SO 448	\$4.727	\$1.786	\$10.147	\$0.410	\$110.444	\$4.708	\$17.538	\$3.066	\$4.027	\$12.452	\$0.306	\$6.613	\$2.023	\$1.614	\$3.795	\$34.519	\$2.076	\$0.218	\$2 010 953	\$17.096	\$12.464	\$9.057	\$21.247	\$175.980	105.05	51 705	\$14.684	\$4.459	\$6.491	\$4.685	\$75.191	20.01	\$2.016	\$3.951	\$7.425	\$1.489 ¢¢ ¢po	\$1.481	\$1.593	\$0.805 20.705	\$3.508	\$0.538	\$8.702	\$11.283	29.051	\$6.276	\$1.058	\$12.884	\$38.914	\$1.311	\$4.850	\$221.503	CL0.1\$	\$1.065	\$9.096	\$2.695	101 10
Totalee Imr	1018135 111D	\$130.16	\$57.73	\$103.74	\$14.31	44,113.64 #20.0E	\$80.48	\$638.32	\$110,29	\$147.51	\$316.76	\$8.29	\$87.17	\$25.88	\$27.15	\$103.49	\$111.84	\$76.78	55.58	\$2 334 59	\$380.31	\$449.39	\$274.45	\$506.74	\$448.79	\$118.24	561 18	\$548.33	\$162.87	\$152.56	\$127.84	\$106.53	0124.00	\$70.13	\$101.64	\$204.03	\$37.83	\$52.77	\$46.06	\$29.69	\$61.77	\$18.95	\$302.21	\$162.14	\$311.51	\$210.77	\$29.68	\$277.63	\$749.73	\$46.06	\$161.43	\$359.05	\$36.33	\$40.24	\$257.88	\$100.70	8146.14
Total Doora	CO 0433	\$1,3563	\$0.2827	\$7.6310							- 19 P											1			a a shere	21-		11.12	2		and and							-									1.00				\$0.6418	\$217.8057	\$0.1254	\$0.0126	\$2.4099	S0.0612	42.1004
Deretione 8	2000 0	0.000	0.000	0.0037	0.000	00000	0.0026	0.0001	0.0000	0.000	0.0034	0.000	0.0014	0.000.0	0.000	0.001	0.042	0.000	0000 0	0.940	0.0098	0.000	0.002:	0.007	0.0548	0.003	0.000	0.000	0.000	0.002	0.0011	0.0582		0.000	0.000	0.0031	0.000	0.000	0.000	0.000	0.004	0.000	0.000	0.004	0.001	0.0050	0.000	0.004(0.028	0.000	0.000	1.067	000.0	0.000	0.002	0.000	E00.0
Dreratione (SO 044	\$1.361	\$0.284	\$7.662	\$0.036	\$0.130	\$2.680	\$0.858	\$0.185	\$0.172	\$4.288	\$0.092	\$4.467	\$1.387	\$0.931	\$1.119	\$32.518	\$0.069	\$0.04/	\$2.010.347	\$7.351	\$0.724	\$1.930	\$8.224	\$169.379	42.339 50 105	SO 195	\$0.343	\$0,202	\$2.573	\$1.358	\$74.630	51 1 10	\$0.186	\$1.332	\$2.144	50.515 61 210	\$0.103	\$0.399	\$0.029	51.944	\$0.043	\$0.817	\$7.257	\$0.924	\$0.772	\$0.290	\$5.789	\$19.852 c1 net	\$0.109	\$0.643	\$216.747	\$0.126	\$0.013	\$2.417	\$0.061	94.110
Fotal linetra	S150	\$129	\$57	296	\$15 514	828	82\$	\$637	\$110	\$147	\$312	\$ 8	69 89	\$24	\$26	\$102	625	1/5	1114	3332	\$373	\$449	\$273	\$499	\$280	0110	361 361	\$548	\$163	\$150	\$126	153	0 4	\$70	\$100	\$202	537	\$53	\$46	000	560	\$10	\$301	\$155	1159	\$210	\$28	\$272	\$730	\$46	\$161	\$141	953	\$40	\$255	\$101	2.4
Unstream To	\$15.07	\$125.43	\$55.95	\$93.60	\$13.90 \$4 003 40	\$36.95	\$75.77	\$620.78	\$107.23	\$143.48	\$304.31	\$7.98	\$80.56	\$23.86	\$25.53	\$99.70	\$77.32	\$74.70	86.36 610 61	\$323.64	\$363.22	\$436.92	\$265.39	\$485.50	\$272.81	0112.01	\$59.39	\$533.65	\$158.41	\$146.07	\$123.17	\$30.34	\$150.12	\$68.11	\$97.69	\$196.60	\$36.34	\$51.29	\$44.46	\$28.88	\$58.26	\$18.42	\$293.51	\$150.86	\$302.46	\$204.49	\$28.62	\$264.75	\$710.81	\$44.75	\$156.58	\$137.55	\$35.26	\$39.17	\$248.79	\$98.00	4100.04
5	5	\$3.37	\$1.50	\$2.52	\$0.37 \$107.60	00.1019	\$2.04	\$16.68					1	\$0.64	\$0.69	\$2.68	\$2.08	52.01	\$0.1V	\$8.70	\$9.76	\$11.74	\$7.13	\$13.05	\$7.33 e.a. 0.9	\$1.02	\$1.60	\$14.34	\$4.26	\$3.93	\$3.31	\$0.82	02.46	\$1.83	\$2.63	\$5.28	50.98	\$1.38	\$1.20	\$0.78	\$1.57 61.05	\$0.50	\$7.89	\$4.05	\$8.13	\$5.50	\$0.77	\$7.12	\$19.10	\$1.20	\$4.21	\$10,50	\$0.95	\$1.05	\$6.69	\$2.63	DD TA
00 Con	50.14	\$1.13	\$0.60	\$0.84	\$35 0F	\$0.33	\$0.68	\$5.58	\$0.96	\$1.29	\$2.73	\$0.07	\$0.72	\$0.21	\$0.23	\$0.90	\$0.69	20.02	80.08	\$2.91	\$3.26	\$3.92	\$2.38	\$4.36	\$2.45	10.14	S0.53	\$4.79	\$1.42	\$1.31	\$1.11	\$0.27	\$1.00 \$1.35	\$0.61	\$0.88	\$1.77	50.33 6+ 80	\$0.4B	\$0.40	\$0.26	\$0.52 *0.52	\$0.17	\$2.64	\$1.35	52./2 \$0.76	\$1.84	\$0.26	\$2.38	56.38	\$0.40	\$1.41	51.24	\$0.32	\$0.35	\$2.23	\$0.88	10.10
Cost D&T	\$0.00	\$0.00	\$0.00	\$0.00	50.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	20.00	00.04	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	00.09	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	00.05	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	50.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	20.00
PM10	\$0.02										Company of the			in and				1								l	1.1			-	i										1					ĺ			ł	Ì.			\$0.04				ł
s02	\$0.20	\$1.68	\$0.75	\$1.26	553 76	\$0.50	\$1.02	\$8.34	\$1.44	\$1.93	\$4.09	\$0.11	\$1.08	\$0.32	\$0.34	\$1.34	51.04	00.1%	80.08	\$4.35	\$4.88	\$5.87	\$3.56	\$6.52	\$3.66	80.08	\$0.80	\$7.17	\$2.13	\$1.96	\$1.65	\$0.41 \$7 4 B	20.05	\$0.91	\$1.31	\$2.64	30.49	\$0.69	\$0.60	\$0.39	\$0.78	\$0.25	\$3.94	\$2.03	54.06 61.13	\$2.75	\$0.38	\$3.56	\$9.55 ¢1 06	\$0.60	\$2.10	\$1.85	\$0.47	\$0.53	\$3.34	\$1.32	24.74 27.74
s 00	\$0.00	\$0.00	\$0.00	\$0.00	00.05	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	50.00	00.04	00.04	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00 50.00	20.00	00.05	\$0.00	\$0.00	\$0.00	\$0.00	20.00	00.00	80.00	\$0.00	\$0.00	\$0.00	20.00	\$0.00	\$0.00	\$0.00	50.00	\$0.00	\$0.00	\$0.00	00.02	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00 \$0.00	\$0.00	\$0.00	\$0.00 50.00	50.00	20.00
NOX	\$0.04	\$0.34	\$0.15	\$0.25	\$10.82	\$0.10	\$0.20	\$1.68	\$0.29	\$0.39	\$0.82	\$0.02	\$0.22	\$0.06	\$0.07	\$0.27	\$0.21	90.20	20.04	\$0.87	\$0.98	\$1.18	\$0.72	\$1.31	\$0,/4	00.04	\$0.16	\$1.44	\$0.43	\$0.39	\$0.33	\$0.08 60 50	S0.41	\$0.18	\$0.26	\$0.53	\$0.10 50 64	\$0.14	\$0.12	\$0.08	\$0.16	\$0.05	\$0.79	\$0.41	80.82	\$0.55	\$0.08	\$0.72	51.92	\$0.12	\$0.42	\$0.37	\$0.10	\$0.11	\$0.67	\$0.26 \$0.26	20.06
VOCs	\$0.01	\$0.08	\$0.03	20.05	\$2.42	\$0.02	\$0.05	\$0.38	\$0.06	\$0.09	\$0.18	\$0.00	\$0.05	\$0.01	\$0.02	\$0.06	40.04 40.04	00.06	10.05	\$0.20	\$0.22	\$0.26	\$0.18	\$0.29	\$0.16	\$0.04	\$0.04	\$0.32	\$0.10	\$0.09	50.07	50.11	\$0.09	\$0.04	\$0.06	\$0.12	\$0.12	\$0.03	\$0.03	\$0.02 \$0.02	\$0.04	\$0.01	\$0,18	\$0.09	80.05	\$0.12	\$0.02	\$0.16	\$0.43	\$0.03	\$0.09	\$0.08 \$0.44	\$0.02	\$0.02	\$0.15 e0.0e	50.05	
FERC Dam # V	7,591	4,253	7,961	7 909	7.464	10,163	5,362	8,791	10,934	6,474	8,450	2,897	6,132	4,718	3,265	9,100	20/10	3 345	2.556	5,274	4,254	8,486	8,242	9,411	8 736	7,411	9,340	5,563	3,309	5,912	9 139	5, 824	2.445	6,597	2,396	5,362	R 012	8,615	2,400	8,405	CCC, 7	2,966	5,638	5,735	11 547	10,163	3,051	6,240	0767/	2,932	5,362	7 921	6,689	2,941	7,254	100/0	0.644

APPENDIX J Hydro Externality Estimates per Megawatt Hour 2013

FER		n # VOC	s N	Ox CO	80	2	PM10	Cost D&T	CO2 Con.	Total Up,no	Upstream T	Total Upstre	Operations (Operations \$	Total Operat	Total\$5 imp	Total Impact	Upstream nc C	Operations r	Total Impact	Total Impact	Total Impac
	2,7		\$0.01	\$0.06	\$0.00	\$0.28		\$0.00	\$0.19	\$0.57	\$21.06	\$22	\$0.380	0.0006	\$0.3791	\$22.00	\$0.945	\$0.543	\$0.362	\$0.905	\$2.984	\$3.049
1	7,5		\$0.03 \$0.01	\$0.11 \$0.05	\$0.00	\$0.57		\$0.00	\$0.38	\$1.14	\$42.32			0.0004	\$0.2345	\$43.69	\$1.372	\$3.556	\$0.249	\$3.805	\$3.049	\$7.407
	6,5		\$0.08	\$0.36	\$0.00	\$0.27 \$1.78		\$0.00	\$0.18 \$1.19	\$0.54 \$3.56	\$20.22 \$132.29			0.0006	\$0.3615 \$0.2493	\$21.12 \$136.10	\$0.905 \$3.805	\$1.604	\$1.380 \$1.103	\$2.984 \$3.049	\$51.428	\$6.527 \$2.329
	2,5	56	\$0.04	\$0.16	\$0.00	\$0.80	\$0.07	\$0.00	\$0.54	\$1.60	\$59.69			0.0025	\$1,3799	\$62.68	\$2.984	\$50.450	\$0.978	\$51.428	\$55.814 \$7.407	\$2.329
	11,1		\$0.04	\$0.20	\$0.00	\$0.97		\$0.00	\$0.65	\$1.95	\$72.40	\$74	\$1.105	0.0015	\$1,1031	\$75.45	\$3.049	\$0.725	\$55.088	\$55.814	\$6.527	\$1.782
	8,5		\$1.13 \$0.02	\$5.07	\$0.01	\$25.21		\$0.00	\$16.86	\$50.45	\$1,877.12			0.0016	\$0.9784	\$1,928.54	\$51.428	\$3.316	\$4.091	\$7.407	\$2.329	\$4.335
1	3,0		\$0.02	\$0.07	\$0.00 \$0.00	\$0.36 \$1.66		\$0.00 \$0.00	\$0.24 \$1.11	\$0.73 \$3.32	\$26.98			0.0898	\$55.0885 \$4.0909	\$82.79 \$130.78	\$55.814	\$4.071	\$2.456	\$6.527	\$1.653	\$26.084
1	3,4		\$0.09	\$0.41	\$0.00	\$2.03		\$0.00	\$1.36	\$4.07	\$151.47			0.0009	\$2.4558	\$130.78	\$7.407 \$6.527	\$2.286 \$1.513	\$0.043 \$0.140	\$2.329 \$1.653	\$1.782 \$4.336	\$3.968
.		16	\$0.05	\$0.23	\$0.00	\$1.14	\$0.10	\$0.00	\$0.76	\$2.29	\$85.07			0.0001	\$0.0428	\$87.40	\$2.329	\$1,734	\$0.048	\$1.782	\$26.084	\$4.106
1		89	\$0.03	\$0.15	\$0.00	\$0.76		\$0.00	\$0.51	\$1.51	\$56.31			0.0002	\$0.1401	\$57.96	\$1.653	\$4.076	\$0.260	\$4.336	\$3.968	\$6.975
-		809 182	\$0.04 \$0.09	\$0.17 \$0.41	\$0.00	\$0.87		\$0.00 \$0.00	\$0.58 \$1.36	\$1.73 \$4.08	\$64.53 \$151.67			0.0003	\$0.0480	\$66.32	\$1.782		\$4.468	\$26.084	\$5.186	\$5.758
1		20	\$0.49	\$2.17	\$0.00	\$10.80		\$0.00	\$7.22	\$21.62	\$804.26			0.0004	\$0.2600 \$4.4679	\$156.01 \$830.36	\$4.336 \$26.084	\$3.504 \$4.407	\$0.463 \$0.778	\$3.968 \$5.186	\$4.106 \$6.975	\$5.138 \$3.742
	2,3		\$0.08	\$0.35	\$0.00	\$1.75		\$0.00	\$1.17	\$3.50	\$130.38			0.0003	\$0.4635	\$134.34	\$3.968	\$3.969	\$0.137	\$4.106	\$5.758	\$2.951
1	11,3		\$0.10	\$0.44	\$0.00	\$2.20		\$0.00	\$1.47	\$4.41	\$163.98			0.0013	\$0.7784	\$169.17	\$5.186	\$5.790	\$1.186	\$6.975	\$5.138	\$0.642
	5,6		\$0.09 \$0.13	\$0.40	\$0.00	\$1.98		\$0.00	\$1.33	\$3.97	\$147.68			0.0001	\$0.1366	\$151.79	\$4.106	\$2.554	\$3.203	\$5.758	\$3.742	\$8.182
	11,3		\$0.06	\$0.58 \$0.26	\$0.00 \$0.00	\$2.89 \$1.28		\$0.00 \$0.00	\$1.93 \$0.85	\$5.79 \$2.55	\$215.42 \$95.04			0.0022	\$1.1855 \$3.2032	\$222.40 \$100.80	\$6.975 \$5.758	\$3.349 \$2.419	\$1.789 \$1.323	\$5.138	\$2.951 \$0.642	\$0.287
· .	11,5		\$0.08	\$0.34	\$0.00	\$1.67		\$0.00	\$1.12	\$3.35	\$124.62			0.0013	\$1.7889	\$129.75	\$5.138	\$1.024	\$1.928	\$3.742 \$2.951	\$8.182	\$1.497 \$2.712
		202	\$0.05	\$0.24	\$0.00	\$1.21	\$0.10	\$0.00	\$0.81	\$2.42	\$90.02	\$92	\$1.325	0.0021	\$1.3226	\$93.76	\$3.742		\$0.262	\$0.642	\$0.287	\$2.111
- I		42	\$0.02	\$0.10	\$0.00	\$0.51		\$0.00	\$0.34	\$1.02	\$38.09			0.0025	\$1.9279	\$41.04	\$2.951	\$3.906	\$4.276	\$8.182	\$1.497	\$3.799
1.0	2,:	58	\$0.01 \$0.09	\$0.04 \$0.39	\$0.00	\$0.19		\$0.00 \$0.00	\$0.13 \$1.31	\$0.38 \$3.91	\$14.12 \$145.33			0.0002	\$0.2625 \$4.2764	\$14.77	\$0.642		\$0.061	\$0.287	\$73.119	\$0.359
-	2,3		\$0.01	\$0.02	\$0.00	\$0.11		\$0.00	\$0.08	\$0.23	\$8.41	\$9		0.0048	\$0.0611	\$153.51 \$8.69	\$8.182 \$0.287	\$1.381 \$43.693	\$0.117 \$29.427	\$1.497 \$73.119	\$2.712 \$2.111	\$13.550 \$12.537
	2,8	808	\$0.03	\$0.14	\$0.00	\$0.69		\$0.00	\$0.46		\$51.37			0.0002	\$0.1168	\$52.87	\$1.497	\$1.973	\$0.739	\$2.712	\$3.799	\$2.710
1		640	\$0.98	\$4.39	\$0.01	\$21.83		\$0.00	\$14.60	\$43.69	\$1,625.69			0.0461	\$29.4265	\$1,698.81	\$73.119	\$1.114	\$0.996	\$2.111	\$0.359	\$0.890
	3,7		\$0.04 \$0.03	\$0.20	\$0.00	\$0.99		\$0.00	\$0.66		\$73.42			0.0009	\$0.7389	\$76.13	\$2.712	\$2.328	\$1.470	\$3.799	\$13.550	\$0.696
	11,4		\$0.05	\$0.23	\$0.00	\$0.56 \$1.16		\$0.00 \$0.00	\$0.37 \$0.78	\$1.11 \$2,33	\$41.46 \$86.64			0.0011	\$0.9964 \$1.4702	\$43.57 \$90.44	\$2.111 \$3.799	\$0.333 \$9.620	\$0.026 \$3.930	\$0.359 \$13.550	\$12.537 \$2.710	\$1.891 \$3.634
		528	\$0.01	\$0.03	\$0.00	\$0.17		\$0.00	\$0.11	\$0.33	\$12.38			0.0000	\$0.0260	\$12.74	\$0.359	\$11.308	\$1.229	\$12.537	\$0.890	\$5.286
	11,1		\$0.22	\$0.97	\$0.00	\$4.81	\$0.41	\$0.00	\$3.21	\$9.62	\$357.93			0.0049	\$3.9299	\$371.48	\$13.550	\$2.457	\$0.253	\$2.710	\$0.696	\$5,540
·		138	\$0.25	\$1.14	\$0.00	\$5.65		\$0.00	\$3.78	\$11.31	\$420.75			0.0049	\$1.2289	\$433.28	\$12.537	\$0.720	\$0.170	\$0.890	\$1.891	\$14.696
-		08 375	\$0.06 \$0.02	\$0.25 \$0.07	\$0.00 \$0.00	\$1.23 \$0.36		\$0.00 \$0.00	\$0.82 \$0.24	\$2.46 \$0.72	\$91.40 \$26.80			0.0004	\$0.2533 \$0.1700	\$94.11 \$27.69	\$2.710 \$0.890	\$0.574	\$0.122 \$1.070	\$0.696	\$3.634	\$1.389
		23	\$0.01	\$0.06	\$0.00	\$0.29		\$0.00	\$0.19	\$0.57	\$21.37			0.0002	\$0.1217	\$22.06	\$0.696	\$0.822 \$3.143	\$0.491	\$1.891 \$3.634	\$5.286 \$5.540	\$1.891 \$1.149
	2,1	94	\$0.02	\$0.08	\$0.00	\$0.41	\$0.04	\$0.00	\$0.27	\$0.82	\$30.58			0.0004	\$1.0695	\$32.47	\$1.891	\$2.349	\$2.937	\$5.286	\$14.696	\$1.467
		151	\$0.07	\$0.32	\$0.00	\$1.57		\$0.00	\$1.05		\$116.93			0.0007	\$0.4912	\$120.57	\$3.634	\$4.685	\$0.854	\$5.540	\$1.389	\$0.828
1	2,7	590	\$0.05	\$0.24 \$0.47	\$0.00	\$1.17 \$2.34	\$0.10 \$0.20	\$0.00 \$0.00	\$0.79 \$1.57	\$2,35 \$4,69	\$87.42 \$174.33			0.0059	\$2.9369	\$92.70 \$179.87	\$5.286	\$14.429	\$0.267	\$14.696	\$1.891	\$2.446 \$7.643
-	6,5		\$0.32	\$1.45	\$0.00	\$7.21		\$0.00	\$4.82	\$14.43	\$536.86			0.0005	\$0.8544 \$0.2671	\$551.56	\$5.540 \$14.696	\$0.365 \$0.994	\$1.024 \$0.897	\$1.389 \$1.891	\$1.149 \$1.467	\$4.309
		393	\$0.01	\$0.04	\$0.00	\$0.18		\$0.00	\$0.12	\$0.36	\$13.57			0.0007	\$1.0243	\$14.96	\$1.389	\$1.051	\$0.098	\$1.149	\$0.828	\$4.081
		800	\$0.02	\$0.10	\$0.00	\$0.50		\$0.00	\$0.33	\$0.99	\$36.98			0.0007	\$0.8973	\$38.87	\$1.891	\$1.359	\$0.108	\$1.467	\$2.446	\$1.898
		326 334	\$0.02 \$0.03	\$0.11 \$0.14	\$0.00 \$0.00	\$0.53 \$0.68		\$0.00	\$0.35 \$0.45	\$1.05 \$1.36	\$39.10 \$50.57			0.0001	\$0.0981 \$0.1080	\$40.25 \$62.04	\$1.149	\$0.424	\$0.404	\$0.828	\$7.643	\$3,935
1		530	\$0.03	\$0.04	\$0.00	\$0.08		\$0.00 \$0.00	\$0.14	\$1.35	\$15.76			0.0000	\$0.4045	\$16.59	\$1.467 \$0.828	\$1.878 \$3.078	\$0.568 \$4.567	\$2.446 \$7.643	\$4.309 \$4.081	\$1.378 \$2.775
	5,0	073	\$0.04	\$0.19	\$0.00	\$0.94		\$0.00	\$0.63	\$1.88	\$69.87	\$72	\$0.569	0.0010	\$0.5683	\$72.32	\$2.446		\$0.133	\$4.309	\$1.898	\$2.383
	2,5		\$0.07	\$0.31	\$0.00	\$1.54		\$0.00	\$1.03	\$3.08	\$114.44	\$118		0.0088	\$4.5669	\$122.08	\$7.643	\$2.407	\$1.673	\$4.081	\$3.935	\$0.709
		88 375	\$0.09 \$0.05	\$0.42	\$0.00	\$2.09		\$0.00	\$1.40 \$0.80	\$4.18	\$155.39			0.0001	\$0.1327	\$159.70	\$4.309	\$1.548	\$0.350	\$1.898	\$1.378	\$1.610
		122	\$0.03	\$0.24 \$0.16	\$0.00	\$1.20		\$0.00 \$0.00	\$0.52	\$2.41 \$1.55	\$89.57 \$57.60			0.0023	\$1,6735 \$0.3499	\$93.65 \$59.50	\$4.081 \$1.898	\$3.817 \$1.012	\$0.118 \$0.366	\$3.935	\$2.775 \$2.383	\$1.198 \$2.944
	11.4		\$0.09	\$0.38	\$0.00	\$1.91	\$0.16		\$1.28	\$3.82	\$142.02			0.0001	\$0.1180	\$145.96	\$3.935		\$0.804	\$2.775	\$0.709	\$9.738
		366	\$0.02	\$0.10	\$0.00	\$0.51	\$0.04		\$0.34	\$1.01	\$37.64	\$39	\$0.366	0.0007	\$0,3659	\$39.02	\$1.378		\$0.198	\$2.383	\$1.610	\$0.874
1.2		710	\$0.04	\$0.20	\$0.00	\$0.98		\$0.00	\$0.66	\$1.97	\$73.32			0.0007	\$0.8044	\$76.09	\$2.775	\$0.577	\$0.132	\$0.709	\$1.198	\$1.378
		288	\$0.05 \$0.01	\$0.22 \$0.06	\$0.00	\$1.09 \$0.29		\$0.00 \$0.00	\$0.73 \$0.19	\$2.18	\$81.27 \$21.47			0.0003	\$0.1984 \$0.1315	\$83.65 \$22.18	\$2.383 \$0.709		\$0.961 \$0.307	\$1.610	\$2.944	\$1.440 \$0.434
1		077	\$0.01	\$0.07	\$0.00	\$0.32		\$0.00	\$0.19	\$0.65	\$21.47			0.0002	\$0.9609	\$25.78	\$1.610	\$0.891 \$1.239	\$1.705	\$1.198 \$2.944	\$9.738 \$0.874	\$1.342
	2,4	58	\$0.02	\$0.09	\$0.00	\$0.45		\$0.00	\$0.30	\$0.89	\$33.16			0.0007	\$0.3067	\$34.36	\$1.198		\$0.245	\$9.738	\$1.378	\$0.519
	2,4		\$0.03	\$0.12	\$0.00	\$0.62		\$0.00	\$0.41	\$1.24	\$46.10	\$47	\$1.709	0.0024	\$1.7050	\$49.04	\$2.944	\$0.675	\$0.199	\$0.874	\$1.440	\$1,977
	7,8		\$0.21	\$0.95	\$0.00	\$4.74		\$0.00	\$3.17	\$9.49	\$353.22			0.0005	\$0.2448	\$362.96	\$9.738	\$1.029	\$0.349	\$1.378	\$0.434	\$1.847
ŀ		277 531	\$0.02	\$0.07	\$0.00	\$0.34 \$0.51	\$0.03 \$0.04	\$0.00 \$0.00	\$0.23 \$0.34	\$0.68 \$1.03	\$25.12 \$38.30			0.0005	\$0.1990 \$0.3490	\$25.99 \$39.68	\$0.874 \$1.378	\$0.465 \$0.225	\$0.975	\$1.440 \$0.434	\$1.342 \$0.519	\$0.456 \$2.160
		368	\$0.81	\$3.62	\$0.01	\$18.00		\$0.00	\$12.04	\$36.03				0.8522	\$419.9251	\$1,796.69	\$455.959	\$0.225	\$0.575	\$1.342	\$1.977	\$5.178
		325	\$0.01	\$0.05	\$0.00	\$0.23		\$0.00	\$0.15	\$0.46	\$17.29			0.0031	\$0.9748	\$18.73	\$1.440	\$0.376	\$0.143	\$0.519	\$1.847	\$1.105
1		333	\$0.01	\$0.02	\$0.00	\$0.11	\$0.01	\$0.00	\$0.08	\$0.22	\$8.30	\$ \$9	\$0.210	0.0002	\$0.2098	\$8.79	\$0.434	\$1.736	\$0.241	\$1.977	\$0.456	\$1.013
		103	\$0.02	\$0.08	\$0.00	\$0.38		\$0.00	\$0.26	\$0.77	\$28.53			0.0008	\$0.5755	\$29.88	\$1.342	\$1.502	\$0.346	\$1.847	\$2.160	\$2.448
	2,3	323	\$0.01 \$0.04	\$0.04 \$0.17	\$0.00	\$0.19		\$0.00 \$0.00	\$0.13 \$0.58	\$0.38	\$13.98 \$64,58			0.0002	\$0.1433 \$0.2411	\$14.50	\$0.519 \$1.977	\$0.449	\$0.007 \$0.829	\$0.456	\$5.178 \$1.105	\$1.351 \$0.857
	ن ک	22.2	QU.V4	au, 171	30.001	30.8/	\$0.07	30.00	QU.58	31./4	\$04,58	\$55	30.242	0.0002	50.24111	\$66,56	31.977	\$1,331	\$0.829	\$2.160	\$1.105	\$U.85/

APPENDIX J Hydro Externality Estimates per Megawatt Hour $\,{\tt 3003}$

1			50.13 \$0.00 \$0.67 \$0.06 \$0.50
50.00 \$0.15	\$0.02 \$0.15	\$0.22 \$0.02 \$0.00 \$0.15	\$0.00 \$0.6/ \$0.06 \$0.00
\$0.00 \$0.44	\$0.06 \$0.00 \$0.44	\$0.44	
\$0.00 \$1.48	\$0.19 \$0.00 \$1.48	\$2.21 \$0.19 \$0.00 \$1.48	
S0.00 \$0.20	SO 03 SO 001 SO 201	\$0.30 \$0.03 \$0.00 \$0.20 \$0.20	\$0.00 \$0.30 \$0.00 \$0.00 \$0.00 \$0.00
\$0.00 \$0.78	\$0.10 \$0.00 \$0.78	\$1.17 \$0.10 \$0.00 \$0.78	\$0.00 \$1.17 \$0.10 \$0.00 \$0.78
\$0.00 \$0.09	\$0.01 \$0.00 \$0.09	\$0.13 \$0.01 \$0.09 \$0.09	\$0.00 \$0.13 \$0.01 \$0.09
\$0.00	\$0.00 \$0.00	\$0.15 \$0.01 \$0.00	\$0.00 \$0.15 \$0.01 \$0.00
\$0.00	\$0.05 \$0.00	\$0.54 \$0.05 \$0.00	\$0.00 \$0.54 \$0.05 \$0.00
\$0.00	\$0.03 \$0.00	\$0.37 \$0.03 \$0.00	\$0.00 \$0.37 \$0.03 \$0.00
\$0.00	\$0.05 \$0.00	\$0.62 \$0.05 \$0.00	\$0.00 \$0.62 \$0.05 \$0.00
\$0.00	\$0.06 \$0.00	\$0.70 \$0.06 \$0.00	\$0.00 \$0.70 \$0.06 \$0.00
\$0.00	\$0.12 \$0.00	\$1.39 \$0.12 \$0.00	\$0.00 \$1.39 \$0.12 \$0.00
\$0.00	\$0.24 \$0.00	\$2.81 \$0.24 \$0.00	\$0.00 \$2.81 \$0.24 \$0.00
\$0.00	\$0.04 \$0.00	\$0.51 \$0.04 \$0.00	\$0.00 \$0.51 \$0.04 \$0.00
\$0.00	\$0.07 \$0.00	\$0.86 \$0.07 \$0.00	\$0.00 \$0.86 \$0.07 \$0.00
\$0.00	\$0.03 \$0.00	\$0.37 \$0.03 \$0.00	\$0.00 \$0.37 \$0.03 \$0.00
\$0.00	\$0.04 \$0.00	\$0.47 \$0.04 \$0.00	\$0.00 \$0.47 \$0.04 \$0.00
\$0.00	\$0.10 \$0.00	\$1.13 \$0.10 \$0.00	\$0.00 \$1.13 \$0.10 \$0.00
\$0.00	\$0.00	\$0.08 \$0.08 \$0.00	\$0.00 \$0.88 \$0.08 \$0.00
\$0.00	\$0.03 \$0.00	S0.30 \$0.03 \$0.00	\$0.00 \$0.30 \$0.03 \$0.00
\$0.00	\$0.11 \$0.00	S1 33 S0.11 \$0.00	\$0.00 \$1.33 \$0.11 \$0.00
8	\$0.31 \$0.00	\$3.55 \$0.31 \$0.00	\$0.00 \$3.55 \$0.31 \$0.00
\$0.00	\$0.22	\$2.59 \$0.22 \$0.00	S0.00 \$2.59 \$0.22 \$0.00
\$0.00	\$0.76 \$0.00	58.82 50.76 50.00	\$0.00 \$8.82 \$0.76 \$0.00
90.00	90.00 90.00	80.00 80.00 80.00	
\$0.00	\$0.00 \$0 00	SA 94 SO 42 \$0 00	S0 00 S4 94 S0 42 S0 40
00	\$0.08 \$0.00	\$0.97 \$0.08 \$0.00	\$0.97 \$0.08 \$0.00
\$0.00	\$0.39 \$0.00	\$4.51 \$0.39 \$0.00	\$0.00 \$4.51 \$0.39 \$0.00
\$0.00	\$0.11 \$0.00	\$1.23 \$0.11 \$0.00	\$0.00 \$1.23 \$0.11 \$0.00
\$0.00	\$0.10 \$0.00	\$1.13 \$0.10 \$0.00	\$0.00 \$1.13 \$0.10 \$0.00
	\$0.23	\$2.62 \$0.23	\$0.00 \$2.62 \$0.23
	\$0.15	\$1.75 \$0.15	\$0.00 \$1.75 \$0.15
	\$0.18	\$2.07 \$0.18	\$0.00 \$2.07 \$0.18
		\$1.75 \$0.15	\$0.00 \$1.75 \$0.15
Average	Average	Average	Average
Median	Median	Median	Median
Smallest	Smallest	Smallest	Smallest
Largest			Largest

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