

SOLUTION METHODS FOR RE-ENTRANT CORNERS IN
ELLIPTIC PARTIAL DIFFERENTIAL EQUATIONS

By

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CHAPTER I

OVERVIEW

Re-entrant corners in systems governed by elliptic partial differential equations strongly affect finite difference methods for determining solutions. A re-entrant corner is a boundary feature formed by intersecting line segments having an internal angle larger than π radians. The accuracy and, in some instances, the convergence characteristics of numerical solution methods are degraded. In this thesis, several finite difference techniques are examined. A technique for restoring their accuracy is the subject of analysis and experiment, here.

In Chapter II, necessary aspects of the theory of partial differential equations are presented: classification and boundary conditions. The focus there is on elliptic partial differential equations. Laplace's equation, which is elliptic, is introduced; it serves in the development and testing of the finite difference methods used here.

Chapter III deals with the discrete problem: the formation of discrete analogues of the solution domain and elliptic differential operator. The discrete problem consists of a network of points and a system of difference equations. The effects of curved boundaries and boundary conditions on the process are discussed. In addition, the basic iterative methods for solving the system of difference equations, the Jacobi and Gauss-Seidel methods, are introduced.

Techniques for accelerating the basic iterative methods are discussed in Chapter IV. Analysis of the accuracy and convergence characteristics of the basic and accelerated methods is given. The accelerated methods studied include the successive overrelaxation method (SOR), the symmetric successive overrelaxation method (SSOR), and the multigrid method. Vector extrapolation is also examined as an acceleration technique.

In Chapter V, re-entrant corners in problems governed by Laplace's equation are studied. Analysis shows that finite difference formulations are invalid in the vicinity of re-entrant corners. Errors propagated from the region of the re-entrant corner by the finite difference method affect the entire solution. Motz's method for singular points in partial differential equations is developed for use in combination with finite difference methods when re-entrant corners are present.

The results of several numerical experiments are given in Chapter VI. The various iterative techniques are used to solve a test problem in order that comparisons of their accuracy and convergence characteristics can be made. Efficient methods are chosen and used to solve a problem having a single re-entrant corner: the L-shaped region problem. Numerical solutions are formed with and without the use of Motz's method. Analysis of the solutions shows to what extent the re-entrant corner affects solutions by finite difference methods and how effective Motz's method is in restoring accuracy. Conclusions from the findings of the experiments and suggestions for further investigations are also presented.

CHAPTER II

ELLIPTIC PARTIAL DIFFERENTIAL EQUATIONS

Partial Differential Equations in Physical Systems

Second order partial differential equations (PDEs) describe the behavior of many important physical systems. Among the systems are fluids, mechanical stress in solid structures, gravitational and electrostatic potentials, and wave phenomena. A solution for the PDE of a particular system depends on the configuration of the system. Thus, for a particular system a wide variety of solutions is possible. Much effort is expended in determining solutions of PDEs, both analytical and numerical solutions. With a solution, the underlying mechanisms of a system can be examined; its future behavior or the effects of a change of configuration can be predicted. In the forecasting of weather, a fluid flow problem, solutions are projected into the future. The design of airfoils requires an understanding of the effects of small changes in shape on the behavior of the airfoils. Much computational effort goes into the solution of these two problems.

Classification of Second Order Partial Differential Equations

A technique for the classification of PDEs is useful. An appropriate solution method can be selected and general features of the

behavior of the system can be determined. Consider the general second order equation in two dimensions.

$$au_{xx} + bu_{xy} + cu_{yy} = f \quad (2.1)$$

with solution $u(x,y)$ (4, 11, 19). The subscripts x and y in (2.1) indicate partial derivatives with respect to x or y . Thus, u_{xx} indicates the second partial derivative with respect to x . The coefficients a , b , c , and f in (2.1) are all functions of x , y , u , u_x , and u_y . An equation cast in the form of (2.1) can be classified on the basis of the behavior of the coefficients a , b , and c . As the coefficients may vary spatially, an equation may change type over the domain on which it is defined.

In a region where $b^2 - 4ac > 0$, equation (2.1) is hyperbolic (19). Wave phenomena and supersonic flow problems are governed by hyperbolic equations. The wave equation,

$$u_{xx} - u_{tt} = 0 \quad (2.2)$$

is hyperbolic. In the case of an ideal string vibrating without frictional losses, the terms u_{xx} and u_{tt} are proportional to the tension and acceleration in string elements, respectively.

Where $b^2 - 4ac = 0$, equation (2.1) is parabolic (19). Heat conduction and diffusion in isotropic media are described by parabolic equations. The diffusion equation,

$$u_{xx} - u_t = 0 \quad (2.3)$$

is parabolic. In (2.3), u_t is a velocity term. It may represent a frictional, retarding force. Characteristic of parabolic systems is the propagation of a solution in time or space.

In a region where $b^2 - 4ac < 0$, an equation of the form (2.1) is elliptic (19). Systems in equilibrium are described by elliptic equations: electrostatic and gravitational potentials, thermal equilibrium, and mechanical stress. Laplace's equation for potentials is elliptic,

$$u_{xx} + u_{yy} = 0 . \quad (2.4)$$

The Laplacian differential operator occurs frequently,

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} . \quad (2.5)$$

For the remaining discussion, equations will be considered to be of one type only on the domain of the problem.

Boundary Conditions

A problem to be solved is specified by the differential equation, the domain of the solution, and the conditions imposed on the solution on the boundary of the solution domain. The boundary conditions may specify the value of the solution there, the normal derivative of the solution, $\frac{\partial u}{\partial n}$, or combinations of the solution value and normal derivative. On a segment of the boundary where the solution only is specified, Dirichlet conditions exist; Neumann conditions occur where the normal derivative alone is specified. If both the value and normal derivative are specified on a segment, then Cauchy conditions are in effect there (19).

Elliptic problems require a closed, stationary boundary with static boundary conditions. In contrast, hyperbolic and parabolic problems may have open boundaries or moving boundaries, and boundary conditions that change with time. Figure 1 depicts an elliptic problem; Figure 2 depicts a parabolic problem.

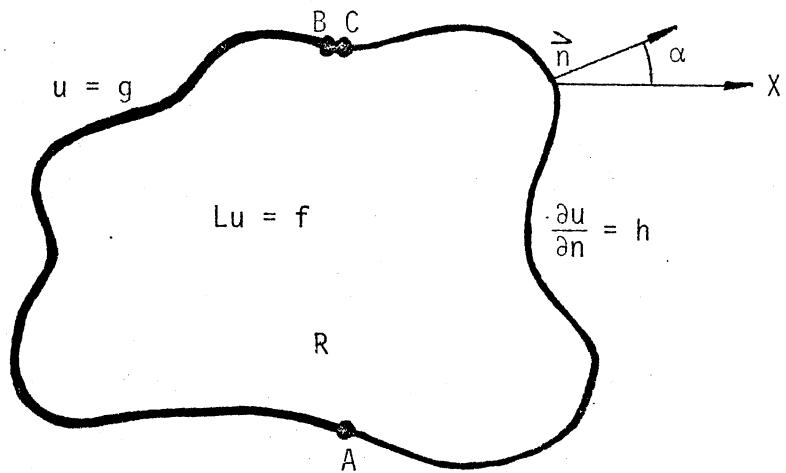


Figure 1. An Elliptic Problem With Mixed Neumann and Dirichlet Boundary Conditions

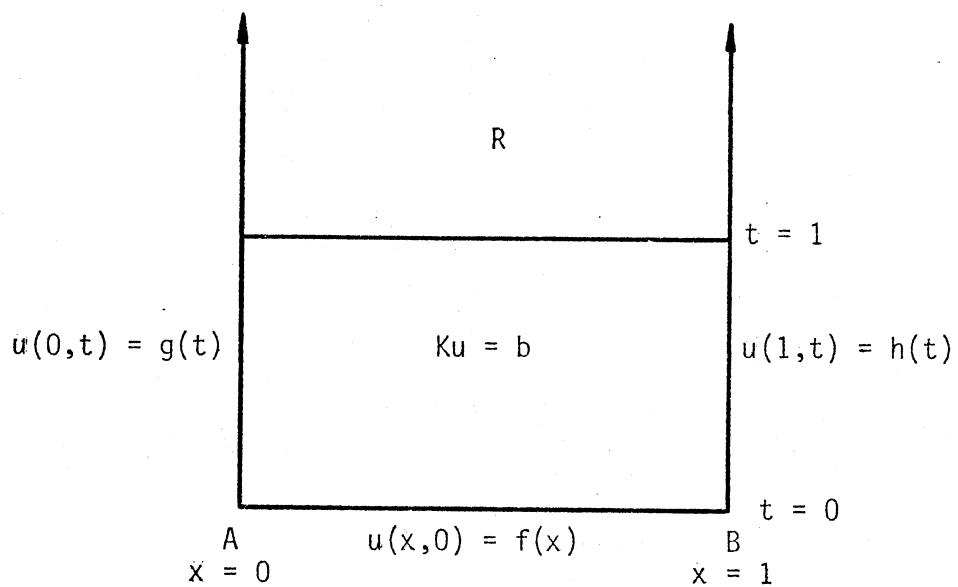


Figure 2. A Parabolic Problem--Solution Propagating in Time

The elliptic problem has Dirichlet conditions on the boundary segment AB and Neumann conditions on the segment AC. On AB, the solution is given by the function $g(x,y)$. On AC, the normal derivative is given by $h(x,y)$,

$$\frac{\partial u}{\partial n} = \frac{\partial u}{\partial x} \cos \alpha + \frac{\partial u}{\partial y} \sin \alpha = h(x,y) . \quad (2.6)$$

The angle α is formed by the x-axis of the problem and the normal vector n on AC. It is convenient to summarize the conditions of the boundary of R , as

$$\Delta u(x,y) = \phi(x,y) . \quad (2.7)$$

The system of Figure 1 attains some equilibrium configuration on the domain R according to the elliptic equation $\Delta u = f$.

The initial value of the solution of the parabolic problem of Figure 2 ($t = 0$) is given by $f(x)$. The solution propagates in time according to the equation $\Delta u = b$ and the boundary conditions given by $g(t)$ on the line $x = 0$ and $h(t)$ on $x = 1$.

The solution of an elliptic problem is uniquely determined by Dirichlet or Neumann conditions, alone, or by a combination of Dirichlet and Neumann conditions as in Figure 1. Cauchy conditions are overly restrictive for elliptic problems and may rule out solutions altogether (19).

Laplace's Equation

Electrostatic and gravitational potentials and temperature distributions in bodies in thermal equilibrium are governed by Laplace's equation,

$$\nabla^2 u = 0 . \quad (2.8)$$

Sources of the potentials or temperature distributions are kept outside the solution domain. The related Poisson equation,

$$\nabla^2 u = f . \quad (2.9)$$

takes into consideration sources within the solution domain.

Solutions for Laplace's and Poisson's equations contain information about vector fields that is often the object of a solution attempt. If $u(x,y)$ is an electrostatic potential, the electric field is given by

$$\mathbf{E} = - \hat{\nabla} u \quad (2.10)$$

where

$$\hat{\nabla} = \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} .$$

The vectors \hat{i} and \hat{j} are unit vectors in the x - and y - directions, respectively (15).

Solutions for Laplace's equation have two important properties to consider here. The maximum and minimum values of the solution occur on the boundary of the solution domain. Also, the solution is harmonic. That is, complex transformations of the solution and solution domain produce functions that are, in turn, solutions of Laplace's equation (19). Transformations can be used to simplify problems having complicated geometries.

CHAPTER III

FINITE DIFFERENCE METHODS FOR SOLVING ELLIPTIC PARTIAL DIFFERENTIAL EQUATIONS

Introduction

Finite difference methods are important tools for the solution of PDEs. Problems that will not yield to analytical techniques can be solved with finite difference methods. The tools of analysis are supplanted by the ability of a computer to perform elementary operations rapidly. The finite difference approach seeks an economical solution for a system of difference equations that approximates the behavior of a PDE on some solution domain. Solution of the system is easily adapted to the use of high speed digital computers.

Finite difference methods can be classified according to the type of problem to be solved. There are methods specific to elliptic, parabolic, and hyperbolic problems.

Among the first to discuss the use of finite difference methods and to identify techniques specific to the different types of problems was Richardson (4) in 1910. He identified methods for elliptic and parabolic problems and presented a solution for a problem of stress in an earthen dam based on those methods. In a 1925 paper, Richardson (25) characterized propagation and equilibrium problems as "marching" and "jury" problems, respectively. The solution is "marched" out from the

boundary in a propagation problem; the boundary parts of an equilibrium problem sit in "judgment" of solution values within the solution domain.

Another important paper in the development of finite difference methods was released in 1928 by Courrant, Friedrichs, and Lewy (9). Their work covered techniques for elliptic and hyperbolic problems. The 1938 paper by Shortley and Weller (27) dealt with solution methods for Laplace's equation. In it, extrapolation methods were proposed to speed the solution of the system of difference equations.

The Discrete Solution Domain

The finite difference solution consists of discrete points that are representative of the continuous solution. These are usually arranged on the solution domain in some regular grid; uniform triangles, rectangles, or hexagons are the cells of the network. For convenience, a grid is usually formed of rectangular or square cells. Consider the domain R of Figure 3 with a grid of rectangular cells superimposed. A grid point P in R with coordinates (x,y) can be located in a number of ways; if numbered, the row and column of the grid point can serve. Thus, a value in the discrete solution at point (x,y) can be represented as

$$u(x,y) = u(ih,jk) = u_{ij} \quad (3.1)$$

where h and k are the dimensions of the grid cells. Grids with square cells are used most commonly ($h = k$). Here, they are called uniform grids.

A set of points u_{ij} making up the discrete solution will be called the solution vector and will be designated \vec{u} . As will be seen in coming discussions, a method for storing the solution vector in

computer memory is needed that will allow ready access to a point u_{ij} and its immediate neighbors. The two-dimensional array of FORTRAN, whether simulated or used as it exists, is a storage scheme which will allow such access. For a solution domain that has an irregular shape, such as the one of Figure 3, a system of pointers will be necessary to establish the proper shape in the two-dimensional array.

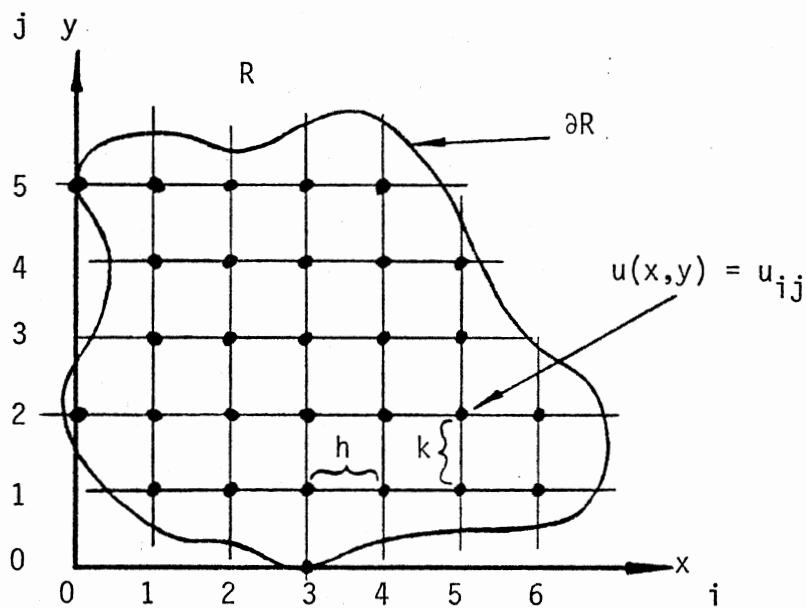


Figure 3. A Rectangular Grid Superimposed on the Solution Domain R

The mesh of Figure 3 has few grid points that coincide with the boundary of R , ∂R . Then, R is being misrepresented and information supplied by the boundary is lost. The boundary should be represented as closely as is possible to insure that the final solution has the most accuracy attainable (4) (11).

Figure 4 shows a boundary segment, AB, that is represented more closely by the solution grid. Auxiliary points are added to the solution grid where grid lines intersect the boundary. The penalty for adding the auxiliary points is a more complicated storage scheme in the computer implementation; the distance from each auxiliary point to the adjacent grid point must be stored.

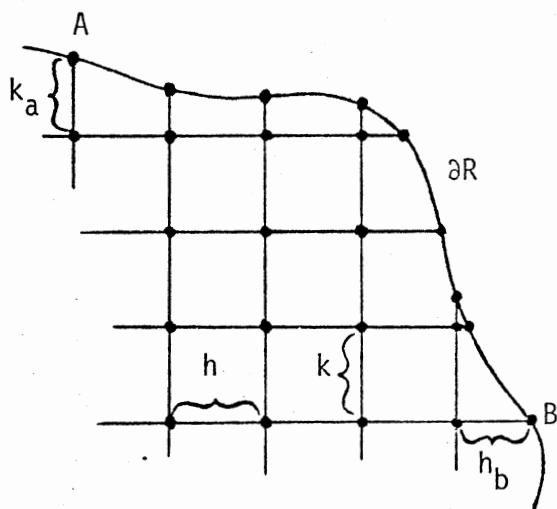


Figure 4. An Improved Boundary Treatment--Grid Points Added at Intersections With ∂R

The Difference Equation

Now that the solution domain, R , has been made discrete, the partial differential equation whose solution is sought there must be made discrete. Assume that the PDE with differential operator L ,

$$L u(x,y) = f(x,y) \quad (3.2)$$

is to be solved on R with the conditions

$$L u(x,y) = \phi(x,y) \quad (3.3)$$

on the boundary, ∂R . Some discrete analogue of the differential operator, L , is needed which, when applied to the points of the discrete solution, closely approximates the behavior of L applied to the continuous solution.

For the remainder of this discussion L will be the Laplacian operator

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}. \quad (3.4)$$

The discrete operator will approximate the behavior of the Laplacian.

Consider the grid of Figure 5. It is a portion of the grid of Figure 3, having spacing h and k . Taylor series expansions of the solution $u(x,y)$ at the grid points adjacent to the point (x,y) can be used to develop approximations for the derivatives of the Laplacian operator, (3.4) (11).

The expansion for $u(x+h,y)$ is

$$u(x+h,y) = u + h \frac{\partial u}{\partial x} + \frac{h^2}{2!} \frac{\partial^2 u}{\partial x^2} + \frac{h^3}{3!} \frac{\partial^3 u}{\partial x^3} + O(h^4) \quad (3.5)$$

with all terms of the expansion evaluated at (x,y) . The expansion for $u(x-h,y)$ is similar

$$u(x-h,y) = u - h \frac{\partial u}{\partial x} + \frac{h^2}{2!} \frac{\partial^2 u}{\partial x^2} - \frac{h^3}{3!} \frac{\partial^3 u}{\partial x^3} + O(h^4). \quad (3.6)$$

Adding the two together gives a difference equation for the second derivative in x that is centered about the point (x,y) .

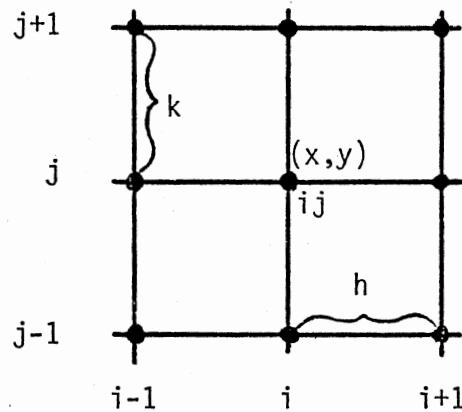


Figure 5. Cells From a
Rectangular Grid

$$\frac{\partial^2 u}{\partial x^2} \Big|_{x,y} = \frac{1}{h^2} (u(x-h,y) - 2u(x,y) + u(x+h,y)) + O(h^2). \quad (3.7)$$

Terms with odd powers of h cancel.

Written in the notation of grid points, the expression becomes

$$\frac{\partial^2 u}{\partial x^2} \Big|_{i,j} = \frac{1}{h^2} (u_{i-1,j} - 2u_{i,j} + u_{i+1,j}) + O(h^2). \quad (3.8)$$

The second derivative in y follows the same development

$$\frac{\partial^2 u}{\partial y^2} \Big|_{i,j} = \frac{1}{k^2} (u_{i,j-1} - 2u_{i,j} + u_{i,j+1}) + O(k^2). \quad (3.9)$$

Dropping the terms $O(h^2)$ and $O(k^2)$, equations (3.8) and (3.9) become the finite difference approximations for the second derivatives of Laplace's equation. The deleted terms are the truncation error of the two approximations.

The most common choice for the cells of a grid is a square ($h=k$). Then, equations (3.8) and (3.9) combine conveniently to form the finite difference representation of the Laplacian

$$\nabla^2 u|_{ij} = \frac{1}{h^2} (u_{i-1j} + u_{i+1j} + u_{ij-1} + u_{ij+1} - 4u_{ij}) + O(h^2) . \quad (3.10)$$

This is the important five-point Laplacian difference operator. Near a curved boundary, as in Figure 4, equations (3.8) through (3.10) will not suffice. The centered difference equations must be replaced with less accurate formulas that take into consideration the unequal spacing of the auxiliary points (4) (11). No problem will be considered here with curved boundaries.

Higher order approximation formulas (larger powers of h in the truncation term) can be obtained by including more grid points in the difference equations (11). A rotation of (3.10) to make use of the points of $\pi/4$, $3\pi/4$, ..., $7\pi/4$ in Figure (3.3) gives

$$\begin{aligned} \nabla_x^2 u|_{ij} &= \frac{1}{2h^2} (u_{i+1 j+1} + u_{i-1 j+1} + u_{i+1 j-1} + u_{i-1 j-1} \\ &\quad - 4u_{ij}) + O(h^2) . \end{aligned} \quad (3.11)$$

No apparent improvement in the order of the truncation is made.

A judicious combination of (3.10) and (3.11), however, can produce a difference equation with truncation $O(h^6)$ for Laplace's equation,

$$\nabla^2 u(x,y) = f(x,y) \quad (3.12)$$

when the solution is harmonic, and $O(h^2)$ in other circumstances.

Weighting (3.10) and (3.11) properly causes truncation terms through

$O(h^5)$ to vanish (11). The result is the nine-point difference operator given by

$$\nabla(9) = \frac{1}{3} \nabla_x^2 + \frac{2}{3} \nabla^2 \quad (3.13)$$

or

$$\begin{aligned} \nabla(9) = & \frac{1}{6h^2} (u_{i+1,j+1} + u_{i-1,j+1} + u_{i+1,j-1} + u_{i-1,j-1} + \\ & 4(u_{i-1,j} + u_{i+1,j} + u_{ij-1} + u_{ij+1}) - 20u_{ij}) . \end{aligned} \quad (3.14)$$

Schematic representations of (3.10) and (3.14), computational molecules, are given in Figure 6.

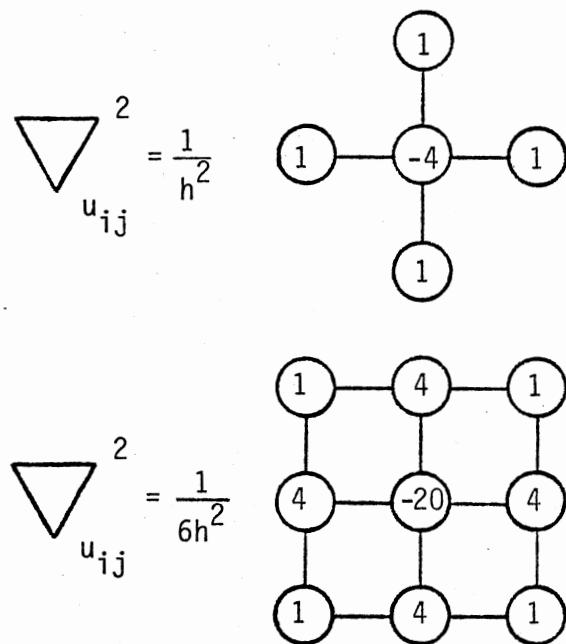


Figure 6. Computational Molecules
for the Five- and Nine-
Point Laplacians

The finite difference representations of other differential operators can be built up using the methods demonstrated here. Sources for other finite difference operators are (1) and (11).

Dirichlet and Neumann conditions must be considered in the formation of difference equations on or near the boundary of the solution domain. Figure 7 shows a boundary segment, AC, with Dirichlet conditions on BC and Neumann conditions on AB. Dirichlet conditions are easily dealt with; a grid point falling on BC is assigned a permanent value based on the function that specifies the Dirichlet conditions. The value may enter into other difference equations, but no different equation applies at its location.

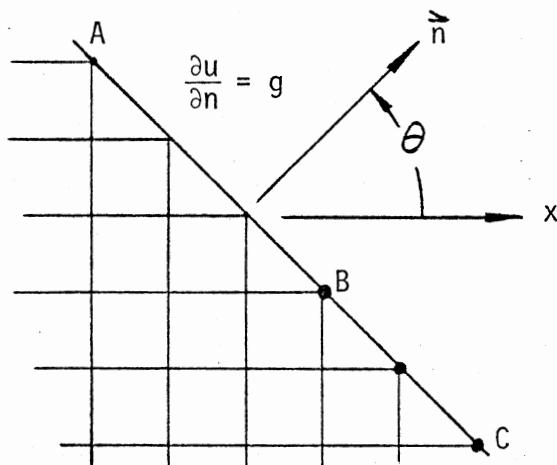


Figure 7. Neumann and Dirichlet Conditions

Treating Neumann conditions can be quite involved (4) (11). A difference equation is required where Neumann conditions hold, but points may be missing that are required for the centered differences of equations (3.10) and (3.14). In Figure 7 the normal derivative is given by

$$\frac{\partial u}{\partial n} = \frac{\partial u}{\partial x} \cos \theta + \frac{\partial u}{\partial y} \sin \theta = g \quad (3.15)$$

where θ is the angle between the normal vector and the x-axis. For a particular point the terms in θ and g can be computed and saved. Taylor series expansions involving adjacent points can be used to give the derivatives in x and y . Enough information can be derived from equation (3.15) to make up for missing points.

The problems considered here have two elements that simplify the treatment of Neumann points: g is everywhere zero and θ is either 0, $\pi/2$, π , or $3\pi/2$. Then, for Neumann points the requirements become

$$\frac{\partial u}{\partial x} = 0, \quad \theta = 0, \pi \quad (3.16)$$

or

$$\frac{\partial u}{\partial y} = 0, \quad \theta = \pi/2, 3\pi/2$$

The Taylor series of equations (3.5) and (3.6) can be combined to form a centered difference approximation for the x-derivative of (3.16),

$$\frac{\partial u}{\partial x} |_{ij} = \frac{1}{2h} (u_{i+1j} - u_{i-1j}) + O(h^2) . \quad (3.17)$$

When (3.17) is used at a Neumann point on the boundary one of the values on the right will correspond to a point that is not in the solution

domain. That does not prevent the determination of a value that will satisfy (3.17). Since the derivative is zero (3.17) becomes

$$u_{i+1j} = u_{i-1j} + O(h^3). \quad (3.18)$$

For the y -derivative, a similar procedure gives

$$u_{ij+1} = u_{ij-1} + O(h^3). \quad (3.19)$$

The boundary, then, serves to mirror the solution; the missing value is the same as the value on the opposite side of the boundary. With this information, difference equations can be constructed at Neumann points.

Suppose that $\theta = 0$ for some Neumann point at location (i,j) . The point $(i+1,j)$ will not be in the solution domain. Equation (3.10) will take the form

$$\nabla^2 u|_{ij} = \frac{1}{h^2} (2u_{i-1j} + u_{ij+1} + u_{ij-1} - 4u_{ij}) + O(h). \quad (3.20)$$

The modification of the truncation term is discussed in (11).

Figure 8 gives the computational molecules of the difference equations that would be used for a problem with the Neumann conditions of equation (3.16) on all of the boundary.

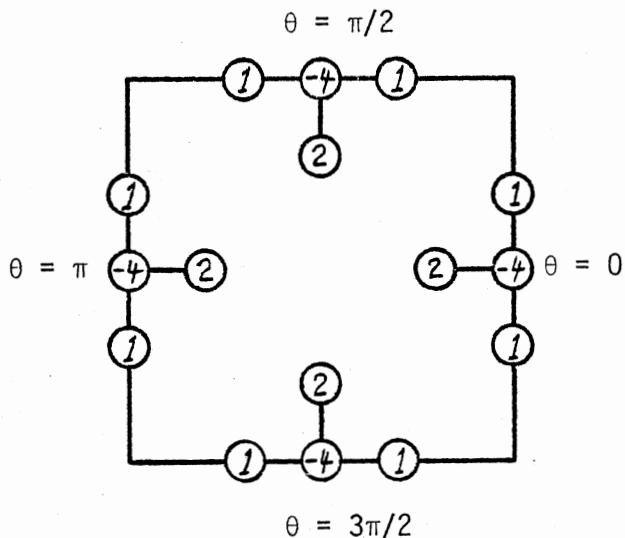


Figure 8. Computational Molecules for Neumann Conditions

The System of Difference Equations

The difference equations of the previous section provide a framework in which a discrete solution can be determined. To determine an approximate solution for Laplace's equation on domain R,

$$\nabla^2 u(x,y) = 0, \quad (3.21)$$

we can require that the five-point (or nine-point) Laplacian difference equation, (3.10), satisfy

$$\nabla^2 u_{ij} = 0$$

for each point of a uniform grid on R. The truncation term is dropped and the discrete solution satisfies

$$\frac{1}{h^2} (u_{i-1,j} + u_{i+1,j} + u_{i,j+1} + u_{i,j-1} - 4u_{i,j}) = 0 \quad (3.22)$$

for each grid point that is not a boundary point expressing Dirichlet conditions.

Consider the square domain of Figure (3.7), S , where Laplace's equation is to be solved. There are Dirichlet conditions on the boundary, and a uniform grid with spacing $h = 1/3$ is placed on S .

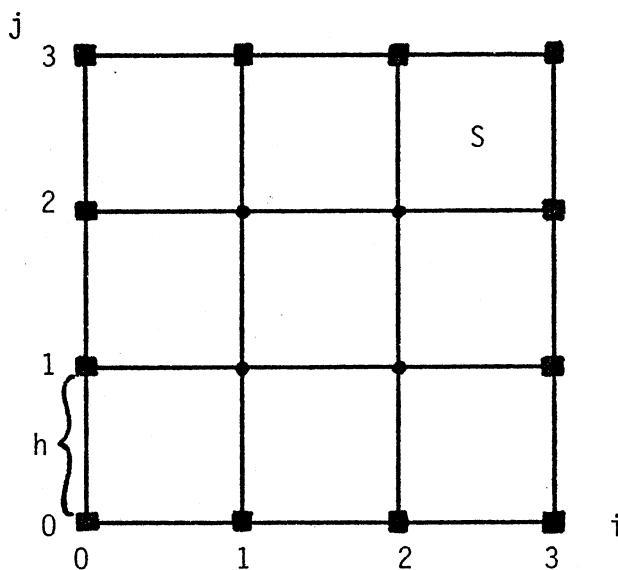


Figure 9. A Uniform Grid on Domain S

The solution is unknown for the four central points only; these will form the solution vector, \vec{u} . Writing equation (3.22) for each of the four points gives a system of four equations in four unknowns of the form

$$A\vec{u} = \vec{b}. \quad (3.23)$$

The system, with the components of \vec{u} ordered by rows, is

$$\begin{bmatrix} -4 & 1 & 1 & 0 \\ 1 & -4 & 0 & 1 \\ 1 & 0 & -4 & 1 \\ 0 & 1 & 1 & -4 \end{bmatrix} \begin{bmatrix} u_{11} \\ u_{21} \\ u_{12} \\ u_{22} \end{bmatrix} = \begin{bmatrix} -u_{01} - u_{10} \\ -u_{20} - u_{31} \\ -u_{02} - u_{13} \\ -u_{23} - u_{32} \end{bmatrix} \quad (3.24)$$

The right-hand side of (3.24), \vec{b} , reflects the Dirichlet conditions of the problem. The coefficient matrix, A, reflects in its rows the relationship between a component of the solution vector and its immediate neighbors in the solution grid. Note that A is symmetric as a result of the ordering of the components of the solution vector. Other orderings also exist which will cause A to be symmetric.

Writing the system of difference equations for other problems is little different. Neumann conditions add components to the solution vector that require modified difference equations. The size of the coefficient matrix is very sensitive to the number or components in the solution vector.

If h is reduced to $1/32$, the grid of Figure 9 would have 961 interior points. There would be 923,521 entries in A. Of these, 4,681 would be non-zero; 841 equations would have non-zero elements, 116 would have four non-zero elements, and four would have three non-zero elements.

Coefficient matrices tend to be highly sparse, that is, zeros predominate as coefficients. In computer implementations, the coefficient matrix is not stored at all, or the non-zero coefficients only are stored.

Solution Methods for the System of Difference Equations

The determination of the approximate solution of the PDE now depends on the solution of a linear system. A number of methods can be used and many computer implementations exist. There are two categories of methods: direct and iterative.

A direct method involves the algebraic manipulation of a linear system to determine its solution. Gaussian elimination is commonly used. Solving sparse systems directly requires complicated routines for storage management in computer implementations. Symmetry in the linear system or banding, the clustering of elements along diagonals, can be exploited to simplify the solution process. Systems resulting from the finite difference process with regular grids are often symmetric and are generally banded (11). The program package ITPACK2B contains routines written in FORTRAN for the direct solution of systems resulting from the discretization of elliptic problems (18).

An iterative method produces a vector sequence that converges to the solution of a problem as the number of iterations approaches infinity. An iterate is generally produced by multiplying the previous iterate by a matrix that is some function of the coefficient matrix of the linear system. An iterate deemed a sufficiently accurate solution estimate is selected after some number of iterations. Iterative methods for solving the sparse systems generated here require only enough storage for the solution vector and boundary values. The matrix multiplications require numbers of additions and multiplications proportional to N rather than N^2 for a solution vector with N components. Sophisticated acceleration schemes can be applied to the iterative processes to

enhance their performance. Iterative methods will be considered exclusively, here.

Basic Iterative Solution Methods:

The Jacobi and Gauss-Seidel Methods

In solving the linear system of order N ,

$$A\vec{u} = \vec{b} \quad (3.23)$$

an iterative method produces the sequence

$$\vec{u}^0, \vec{u}^1, \dots, \vec{u}^n, \dots . \quad (3.25)$$

The vector \vec{u}^0 is some initial solution estimate. The limit of the sequence is \vec{u} . An iterate \vec{u}^n is produced by a function of n , A , \vec{b} , and some number of the previous iterates; a method of order k involves the previous k iterates (4) (32):

$$\vec{u}^n = F(A, \vec{b}, n, \vec{u}^{n-1}, \dots, \vec{u}^{n-k}). \quad (3.26)$$

The most common methods have no dependence on n (they are stationary), they are of order $k=1$, and they are linear in \vec{u}^{n-1} . For these methods, equation (3.26) becomes

$$\vec{u}^n = F(A, \vec{b}, \vec{u}^{(n-1)}). \quad (3.27)$$

A general linear, stationary iterative method can be written as

$$\vec{u}^n = G \vec{u}^{n-1} + \vec{r}^n \quad (3.28)$$

where G is a matrix that depends on A and \vec{b} . The vector \vec{r}^n also depends

on A and \vec{b} . Using the relation $\vec{u} = A^{-1} \vec{b}$, equation (3.28) can be rewritten to give the error at each iteration,

$$\vec{e}^n = \vec{u} - \vec{u}^n = G \vec{e}^{n-1} \quad (3.29)$$

or

$$\vec{e}^n = G^n \vec{e}^0. \quad (3.30)$$

For the iterative scheme of (3.28) to converge to the solution, \vec{u} , we must have

$$\vec{e}^n \rightarrow 0 \text{ as } n \rightarrow \infty. \quad (3.31)$$

This implies

$$G^n \rightarrow 0 \text{ as } n \rightarrow \infty. \quad (3.32)$$

The condition (3.32) is crucial, and it must be predictable from the structure of G . It will be examined more closely in the following sections.

To describe the basic iterative methods it is convenient to partition A . The three matrices L , D , and U formed from the elements of A below the diagonal, on the diagonal, and above the diagonal, respectively, with zeros elsewhere give the partitioned representation $L + D + U$. It is also convenient to adopt a single subscript in referring to the components of the solution vector, numbering them from 1 to N .

For the Jacobi (J) method, each component of \vec{u}^{n-1} is allowed a displacement in order to satisfy one of the equations of the linear system. The displaced components make up \vec{u}^n ; they are given by

$$u_j^n = a_{jj}^{-1} \left(\sum_{k \neq j} a_{jk} u_k^{n-1} + b_j \right) \quad (3.33)$$

where a_{ij} is an element of A. The desired effect of the displacements is an iterate that better approximates the solution, \vec{u} . Equation (3.33) can be rewritten in matrix form as (32):

$$\vec{u}^n = D^{-1}(D - A)\vec{u}^{n-1} + D^{-1}\vec{b} \quad (3.34)$$

The requirement that D^{-1} exist is satisfied since the diagonal elements of A are all non-zero (from equation (3.22)). Although the J method is not used as a solution method, its behavior is the basis for the selection of parameters for more sophisticated methods.

The Gauss-Seidel (GS) method uses a strategy similar to that of the J method. As soon as a component of \vec{u}^n is determined, though, it is used to help determine the remaining components of \vec{u}^n . Component j is given by

$$u_j^n = a_{jj}^{-1} \left(\sum_{k=1}^{j-1} a_{jk} u_k^n + \sum_{k=j+1}^N a_{jk} u_k^{n-1} + b_j \right) \quad (3.35)$$

In matrix form this becomes

$$\vec{u}^n = K\vec{u}^{n-1} + KD^{-1}\vec{b} \quad (3.36)$$

where

$$K = (I - L)^{-1}$$

The matrix I is the identity matrix. The matrix $(I - L)$ is non-singular since all the diagonal entries are non-zero and the matrix is lower triangular (32).

There is one important difference between the J and GS methods to note here. The order of the difference equations in the system $\vec{A}\vec{u} = \vec{b}$ is immaterial for the J method; the sequence of values for a particular grid location will be the same whether $\vec{A}\vec{u} = \vec{b}$ or a shuffled version of the system is used. This same statement can not be made for the GS method; the sequence of values at a particular location will change as the order of the difference equations changes.

The successive overrelaxation (SOR) method involves a slight modification of the GS method. Each displacement of a component of \vec{u}^{n-1} is weighted before it is used to produce \vec{u}^n . The weighting factor or overrelaxation parameter, ω , is in the range

$$1 \leq \omega < 2 . \quad (3.37)$$

Defining u_j^n to be the result of (3.35), the basic operation of the GS method, the components of \vec{u}^n are given by

$$u_j^n = u_j^{n-1} + \omega(u_j^n - u_j^{n-1}) . \quad (3.38)$$

For $\omega = 1$, the SOR method reduces to the GS method. The matrix representation of SOR is

$$\vec{u}^n = M(I - \omega(U - I))\vec{u}^{n-1} + MD^{-1}\vec{b} \quad (3.39)$$

where

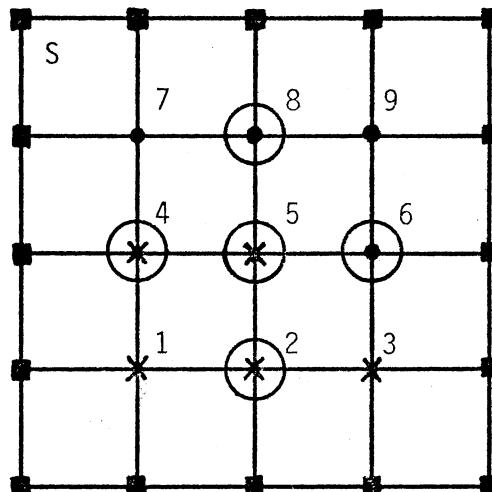
$$M = (I - \omega L)^{-1} .$$

SOR shares the sensitivity of the GS method to the order of the components of the solution vector (32). For an optimal choice of ω , SOR is far superior to the J and GS methods for solving the system of

(3.23). The choice of the overrelaxation parameter is discussed in Chapter IV.

Implementation of the Basic Iterative Methods

Figure 10 shows a uniform grid on domain S ; there are Dirichlet conditions on the boundary. The solution methods of the previous section can be easily implemented for such a problem. As noted earlier, the two-dimensional array of FORTRAN can be used to store the values of solution components and boundary values and maintain the organization imposed by the grid.



- - old component
- x - new component
- boundary value

Figure 10. A Gauss-Seidel or SOR Iteration

Let the array contain the components of \vec{u}^{n-1} . For component j , designate the values at the four nearest grid points u_A , u_B , u_C , and u_D ; as many as two of the values can be boundary values.

The equations that govern the J and GS method, (3.33) and (3.35), can be written explicitly from the difference equation (3.21). For the J method a component of \vec{u}^n is given by

$$u_j^n = \frac{1}{4} (u_A + u_B + u_C + u_D). \quad (3.40)$$

There is no place to put the new component in the single array so a duplicate array is needed. An iteration of the J method involves performing (3.40) for all values of j . The uses of the two arrays interchange for the next iteration.

For the GS method, components of \vec{u}^n replace components of \vec{u}^{n-1} as they become available; old values of u_A, \dots, u_D are replaced with new ones. It is natural, then, to use a single array and put the new values of components in place of the old values. During the course of a GS iteration parts of the old and new iterate will be contained in storage. The GS method requires the choice of some order for the components. The results of an iteration are not independent. Figure 10 shows a GS iteration where the order is by rows. Modifying a GS iteration according to (3.38) gives an SOR iteration.

A variant of SOR is the symmetric successive overrelaxation method (SSOR). An iteration consists of an SOR sweep of the solution components in order followed by an SOR sweep of the components in reverse order. The primary advantage of SSOR is that its iteration matrix is symmetric (32).

Convergence of the Basic Iterative Methods

As noted earlier, the behavior of G^n for increasing n determines the convergence of the error sequence, \tilde{e}^n . Some idea of the convergence characteristics of the J, GS, and SOR methods is needed before proceeding.

The three iteration matrices, G_j , G_g , and G_s for the J, GS, and SOR methods, respectively, each have performances determined by their eigenvalue spectra (32). The eigenvalue spectrum of a square matrix B of order N consists of the set of all Λ_i such that

$$B\tilde{V}_i = \Lambda_i \tilde{V}_i \quad (3.41)$$

is satisfied; the \tilde{V}_i are eigenvectors of B . There are N eigenvalues of B ; some may be complex and a single value may be repeated.

The spectral radius of B , $S(B)$, is defined by

$$S(B) = \max_i |\Lambda_i|. \quad (3.42)$$

The eigenvalue corresponding to $S(B)$ is the dominant eigenvalue of B . For large N , it is difficult to determine the eigenvalue spectrum of B ; $S(B)$ can be determined indirectly, though.

A necessary and sufficient condition for $G^n \rightarrow 0$ (also $\tilde{e}^n \rightarrow 0$) as $n \rightarrow \infty$ is $S(G) < 1$ (32). Thus, the spectral radii of G_j , G_g , and G_s must be less than one for the J, GS, and SOR methods to converge for a particular problem.

A norm is a useful measure of the convergence of a vector sequence. For some norm a , $\| \cdot \|_a$, a vector sequence \tilde{u}^n is convergent if and only if

$$\| \tilde{u} - \tilde{u}^n \|_a \rightarrow 0 \text{ as } n \rightarrow \infty. \quad (3.43)$$

A norm that is easily computed is

$$\|\vec{u}\| = \left(\sum_{i=1}^N |u_i| \right) / N. \quad (3.44)$$

Then, $\|\vec{e}^n\|_a \rightarrow 0$ as n increases (32). The improvement in the solution estimate made by a single iteration can be gauged by the ratio

$$\|\vec{e}^n\| / \|\vec{e}^{n-1}\|. \quad (3.45)$$

This ratio approaches the spectral radius of the iteration matrix, $S(G)$ as n increases. It often serves as an estimate of $S(G)$ (4) (32).

Young (32) uses a measure he calls the asymptotic rate of convergence,

$$R(G) = -\log S(G), \quad (3.46)$$

which can be estimated using (3.45).

Only in artificial situations is \vec{e}^n available during the computation of \vec{u} , hence, the ratio (3.45) must be determined indirectly.

The displacement vector, \vec{d}^n , given by

$$\vec{d}^n = \vec{u}^n - \vec{u}^{n-1} \quad (3.47)$$

should approach zero as \vec{u}^n approaches \vec{u} . An operation common to the J, GS, and SOR methods is that of equation (3.40). A residual vector, \vec{r}^n , whose components are given by

$$r_j^n = u_A + u_B + u_C + u_D - 4u_j^{n-1} \quad (3.48)$$

is another displacement measure. It, also, should approach zero as \vec{u}^n converges. It can be shown (4) that the displacement and residual vectors have behavior similar to that of the error vector. The sequence of residual vectors is given by

$$\hat{r}^n = (AGA^{-1})^n \hat{r}^{n-1} . \quad (3.49)$$

Either of the two ratios, $\|\hat{d}^n\| / \|\hat{d}^{n-1}\|$ or $\|\hat{r}^n\| / \|\hat{r}^{n-1}\|$, can be used in place of (3.45) to determine $S(G)$.

The requirement for the convergence of a general iterative method has been described, $S(G) < 1$. No general criteria have been offered to determine which systems of difference equations will produce iteration matrices that fulfill this requirement. The coefficient matrix, A , that results when the five-point Laplacian difference equation is written for a uniform grid has properties that guarantee that $S(G)$ will be less than one for the J, GS, and SOR methods. First, A has weak diagonal dominance, that is,

$$|a_{ii}| \geq \sum_{j \neq i} |a_{ij}| , \quad i = 1, 2, \dots, N, \quad (3.50)$$

and

$$|a_{ii}| > \sum |a_{ij}|$$

for at least one i . This is assured by the form of the Laplacian equation (3.22). The diagonal entry of each row is -4, and the sum of the remaining elements is never more than 4. Second, A is irreducible. This follows from the grid structure; the components of the solution vector are all interrelated. No subsystem of $\hat{A}\hat{u} = \hat{b}$ can be solved independently. With these two properties for A it follows that $S(G)$ is less than one for the three methods (4) (11) (32).

Young (32) has described an important property found among many of the coefficient matrices that results when the discrete problem is formed. It has been mentioned that the GS and SOR methods produce sequences of iterates that are different for the different orderings of the difference

equations that make up the linear system. Young's observations limit the consideration that must be given to the order of the difference equations.

The Property (A) that Young describes assures that for each "consistent" ordering of the coefficient matrix the eigen values of the iteration matrix, G_g or G_{SOR} , will be the same. This means that every consistently ordered system for a particular problem will have the same convergence characteristics when the GS method is used. The same will be true when SOR is used.

The matrix A has Property (A) if and only if there exists a permutation matrix P such that $P^{-1}AP$ has the form

$$P^{-1}AP = \begin{bmatrix} D_1 & H \\ K & D_2 \end{bmatrix} \quad (3.51)$$

where D_1 and D_2 are square diagonal matrices and H and K are rectangular matrices. Consistent orderings can be formed for any matrix having Property (A) (32). If A is symmetric and has Property (A) then the eigenvalues of G_j are real and occur in pairs (positive and negative values) (4). Also, the eigenvalues of the SSOR iteration matrix are real.

With the assurance that the spectra of G_g and G_s are invariant, relations can be formed between the eigenvalues of G_j , G_g , and G_s . For an eigenvalue μ of G_j there is a corresponding eigenvalue Λ of G_s . The two are related by

$$(\Lambda + \omega - 1)^2 = \omega\mu^2 \Lambda \quad (3.52)$$

where ω is the overrelaxation parameter (4) (11) (32). For $\omega = 1$, the GS method, the eigenvalues are related by

$$\Lambda = \mu^2. \quad (3.53)$$

Equations (3.52) and (3.53) can serve to relate spectral radii. The implication of (3.53) is that the GS method converges at twice the rate of the J method (from (3.46)).

Assuming that $S(G)$ is known for the J or GS method for a particular problem, then the optimum value of ω , ω_b , can be determined. It is chosen to minimize $S(G_s)$. In terms of $S(G_j)$, ω_b is given by (4) (11)

$$\omega_b = 2(1 + \sqrt{1 - S(G_j)^2})^{-1}. \quad (3.54)$$

If the value of $S(G_j)$ is given for a problem, the relative effectiveness of the J, GS, and SOR methods can be demonstrated. If $S(G_j)$ is .980, $S(G_g)$ will be .960, and $S(G_s)$ is .668. Comparing the assymptotic convergence rates of convergence, the GS method is 2.02 times as fast as the J method, and SOR is 20.0 times as fast.

Discussion of the determination of ω_b for SOR will be given in the next chapter.

CHAPTER IV

ACCELERATED ITERATIVE SOLUTION METHODS

Techniques for accelerating the convergence of the basic iterative solutions have been developed over the last 30 years. These techniques include methods to reduce the value of $S(G)$, and the use of extrapolation in order to skip unnecessary iterations. The methods discussed here include SOR, symmetric SOR, vector Aitken acceleration, and the multigrid method.

Behavior of the Eigenvalues of the SOR Iteration Matrix

Because SOR with the optimum value of ω is the basic iteration for a number of accelerated methods, much study has gone into the determination of that value. Although there are relations between the eigenvalues of the SOR, GS, and J iteration matrices and ω_b , those eigenvalues are, in practice, difficult to obtain. Any error in determining the dominant eigenvalue for the J or GS matrices, and consequently in ω_b , can seriously degrade the performance of SOR.

Solving the equation relating eigenvalues,

$$(\Lambda + \omega - 1)^2 = \omega^2 \mu^2 \Lambda , \quad (3.52)$$

for Λ , the dominant eigenvalue of G_s , in terms of ω , the dominant eigenvalue of G_j , gives

$$\Lambda = \frac{1}{4} (\omega\mu + (\omega^2\mu^2 - 4(\omega - 1)^{\frac{1}{2}})^2) \quad (4.1)$$

for $1 \leq \omega \leq \omega_b$ (4). For $\omega_b \leq \omega < 2$, Λ is given by

$$\Lambda = \omega - 1. \quad (4.2)$$

The eigenvalues of G_s lie along the positive real axis for $\omega = 1$ (the GS method). As ω increases, eigenvalues migrate onto a circle with radius $\omega - 1$ centered about the origin in the complex domain. When $\omega = \omega_b$, all eigenvalues lie on the circle. Equation (4.1) is no longer appropriate since the circle continues to expand. For $\omega > \omega_b$ all the eigenvalues are complex and lie on the circle (11) (14).

A graph of $S(G_2)$ versus ω using (4.1) and (4.2) illustrates the sensitivity of SOR to the choice of ω . Figure 11 shows the relation for $S(G_j) = \mu = .981$. The line AB, a reflection of BC, is useful for evaluating the effects of errors in an estimate of ω_b ; ω_a and ω_c will correspond to the points A and C. Clearly, an estimate that falls in the interval $[\omega_a, \omega_b]$ will cause a larger value of $S(G_s)$ than an estimate falling in $[\omega_b, \omega_c]$. Gross errors should result in underestimates due to the steeper slope of BC as opposed to the curve on $[1, \omega_a]$. Graphs of $S(G_s)$ in (8) indicate that the interval $[\omega_a, \omega_c]$ becomes shorter as $S(G_j)$ approaches 1 making the choice of ω_b more critical.

Numerical Determination of the Optimum

Overrelaxation Parameter

Determining the dominant eigenvalue of either G_j or G_g accurately is of the first importance in determining ω_b . There are two environments in which ω_b must be determined: a problem is solved repeatedly

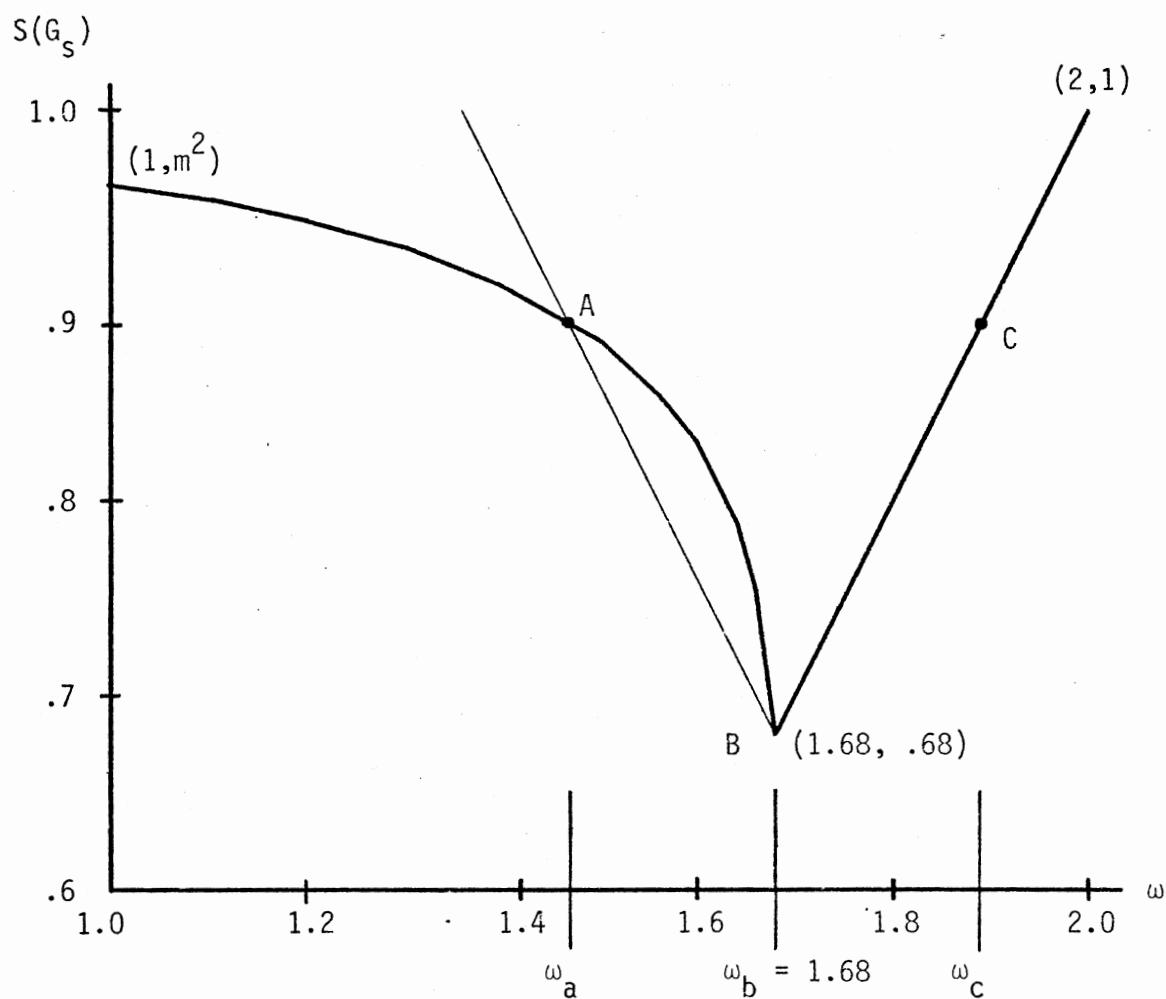


Figure 11. The Dependence of the Spectral Radius for SOR on ω
 $(S(G_j) = .981)$

with no change in the iteration matrix; a range of unrelated problems is encountered.

In the first case an exhaustive effort to determine ω_b might be justified. In the second, a solution produced with a poor choice of ω_b might be less costly than a modest effort to determine ω_b .

All methods employ one of the vector sequences produced by the iteration scheme. Here, the residual vector defined in Chapter III is used. The most important characteristic of the sequence is

$$P_n = \|\tilde{r}^n\| / \|\tilde{r}^{n-1}\| \rightarrow S(G), \text{ as } n \rightarrow \infty \quad (4.3)$$

for iteration matrix G.

Most of the techniques discussed here are variations on the power method (17). Assume that matrix B (order N) has eigenvalues Λ_i and eigenvectors \tilde{x}_i ; the eigenvalues are ordered so that Λ_1 is dominant and Λ_N is smallest.

Multiplying an arbitrary vector \tilde{v}^0 by B k times gives

$$\tilde{v}^k = B^k \tilde{v}^0 = \Lambda_1^k c_1 \tilde{x}_1 + \Lambda_2^k c_2 \tilde{x}_2 + \dots + \Lambda_N^k c_N \tilde{x}_N \quad (4.4)$$

where the c_i are constants.

If $|\Lambda_1|$ is greater than $|\Lambda_2|$ and k is sufficiently large, then (4.4) can be reduced to

$$v^k = B^k v^0 \approx \Lambda_1^k c_1 \tilde{x}_1. \quad (4.5)$$

Some vector norm can be used to extract Λ_1 ,

$$\|\tilde{v}^k\| / \|\tilde{v}^{k-1}\| = \Lambda_1. \quad (4.6)$$

Therefore, the use of (4.3) to determine S(G) is equivalent to the power method with the iteration matrix replacing B.

A hindrance in the use of (4.3) is the fact the two eigenvalues with the largest magnitude for G_j and G_g (Λ_1 and Λ_2 in (4.4)) have magnitudes that differ only slightly (8). Then, many iterations are required before (4.4) applies. The sequence P_n in (4.2) is slowly convergent, but a process like Aitken extrapolation can be used to skip many iterations and resolve the dominant eigenvalue (8). Using the ratios of (4.2), an Aitken extrapolation is given by (2)

$$P = P_n - \frac{(P_n - P_{n-1})^2}{(P_n - 2P_{n-1} + P_{n-2})} . \quad (4.6)$$

The extrapolated value, P , can be used as an estimate of $S(G)$.

Acceleration through the use of Chebyshev polynomials is also possible for the power method (13).

A simple method for determining ω_b requires 15 to 20 SOR iterations with ω_b set to one (a GS iteration); equation (4.6) is used with ratios from the last three iterations to determine $S(G_g)$. Then, with results from the previous chapter, ω_b is given by

$$\omega_b = 2/(1 + \sqrt{1 - S(G_g)}) . \quad (4.7)$$

Carré (8) presents an iterative method for determining ω_b that operates while SOR iterations are conducted. A value ω_0 is used as an initial estimate of ω_b . Ten to 15 iterations are allowed, and (4.6) is used to determine Λ , the dominant eigenvalue of G_s corresponding to ω_0 . Then, a combination of (3.52) and (3.53) is used,

$$\omega_i = 2/(1 + \sqrt{1 - (\Lambda + \omega_{i-1} - 1)^2 / (\Lambda \omega_{i-1}^2)}) . \quad (4.8)$$

The new estimate of ω_b , ω_i , is used for several iterations, and (4.6) and (4.8) are used again. As the method proceeds ω_i will approach ω_b

and may exceed it. Carré includes a mechanism that assures that ω_b will not be exceeded.

The method involving equations (4.6) and (4.7) was used here to determine ω_b . This was done once for each of the iteration matrices used. One hundred iterations were usually sufficient to determine ω_b to four digits.

Acceleration of Convergent Vector Sequences

A number of methods exist for speeding the convergence of the vector sequences produced by iterative methods such as SOR. These use combinations of several iterates to produce an improved solution, skipping many iterations in the process. Some of the most recent methods include Chebyshev semi-iterative techniques (12) (14) (32) and conjugate gradient techniques (14) (17) (22). These are typically used with SOR or SSOR iterations (33).

The method used here is vector Aitken acceleration adapted to vector sequences. In a 1937 paper, Aitken presents his δ^2 -process for accelerating the determination eigenvalues and eigenvectors (2). The extrapolation of equation (4.6) is applied to the eigenvalue sequence and to corresponding components of the eigenvector sequence. An assumption is made that each component of the eigenvector sequence is convergent. This may not be true for the initial iterations and following extrapolations. Then, applying (4.6) may produce absurd values for some components of the new iterate. A modified vector Aitken method is due to Jennings (16) (17). An extrapolation factor, s , is produced that is a composite of the tendencies of the individual components. For a vector sequence \vec{P}^n , the improved iterate is given by

$$\hat{P} = \hat{P}^n + s(\hat{P}^n - \hat{P}^{n-1}) \quad (4.9)$$

where

$$s = \frac{(\hat{P}^{n-2} + \hat{P}^{n-1})^T (\hat{P}^{n-1} - \hat{P}^n)}{(\hat{P}^{n-2} + \hat{P}^{n-1})^T (\hat{P}^{n-2} - 2\hat{P}^{n-1} + \hat{P}^n)} \quad (4.10)$$

Two additional constraints can limit the effects that fluctuations in a few component produce: upper and lower limits can be placed on s to prevent absurd extrapolations, and extrapolation can be postponed until the last two iterates are closely aligned. The angle θ between the last two iterates can be determined from

$$(\hat{P}^n)^T \hat{P}^{n-1} = q_n q_{n-1} \cos \theta \quad (4.11)$$

where q_n and q_{n-1} are the lengths of \hat{P}^n and \hat{P}^{n-1} , respectively.

If $\cos \theta$ is close to one, then an extrapolation can be allowed. The routine VAITK written by Dr. J. P. Chandler of the Computing and Information Sciences Department of Oklahoma State University uses Jenning's method and employs the constraints mentioned above. It is included in Appendix A as part of the program CORNER.

The modified Aitken acceleration can be used for sequences generated by matrices with real eigenvalues. Then, the J, GS, and SSOR methods are candidates for Aitken acceleration.

The Multigrid Method

The multigrid method is a recent development in finite difference methods due to Brandt (5) (6) (7). The performance of multigrid methods exceeds that of the most recent accelerated iterative methods. The method used here is the Cycle-C algorithm that appears in (6). It is intended for elliptic problems.

A practice that speeds the convergence of iterative methods is the use of a collection of n grids with spacing h , $2h$, $4h$, ..., $2^{n-1}h$. A solution is obtained on each grid to prescribed accuracy, and interpolation is used to fill in values missing in the next grid. The solution is eventually governed by the rate of convergence on the fine grid, but most of the initial work required to build up a solution is bypassed. An iteration on a coarse grid requires roughly one fourth the effort required on the next finest grid.

This process is inverted in the Cycle-C algorithm: iterations begin on the solution grid and then proceed to coarser grids. The multigrid philosophy encompasses the range of errors that occurs in a problem: there are error components that have short wavelengths (on the order of h) and there are components that span the solution domain. The short wavelength components represent local roughness of the solution; the longer components result from the slow propagation of boundary values into the solution domain.

On the finest grid, error components with wavelength $2h$ or less can be damped effectively by GS iterations. The magnitudes of the components can be reduced by an order of magnitude with just a few iterations. Due to the limited range of the five-point Laplacian difference equation, longer components are essentially unaffected. If coarser grids are used, though, GS iterations can damp the longer components.

Rather than computing the solution on coarse grids, corrections are calculated. If the system to be solved is

$$\hat{A}\hat{u} = \hat{b}, \quad (4.10)$$

the GS method will produce the sequence \hat{u}^n . Defining the residual vector \hat{r}^n ,

$$\hat{r}^n = \hat{u}^n - \hat{u}^{n-1} \quad (4.11)$$

the vector \hat{u}^n satisfies

$$A\hat{u}^n = \hat{b} - \hat{r}^n. \quad (4.12)$$

Combining equations (4.10) gives

$$A(\hat{u} - \hat{u}^n) = \hat{r}^n \quad (4.13)$$

Defining the correction \hat{v}^n ,

$$\hat{v}^n = \hat{u} - \hat{u}^n \quad (4.14)$$

(4.13) becomes

$$A\hat{v}^n = \hat{r}^n. \quad (4.15)$$

Assume that there is a system of grids numbered 1 though k with spacing h , $2h$, ..., $2^{k-1}h$. If the short wavelength components are smoothed on grid 1, the residual will be free of that error and the system (4.15) can be solved economically on grid 2. The same steps can be taken in solving (4.15) on grid 2: short wavelength components are damped and an equation similar to (4.15) is formed and solved on grid 3. The process can be extended through grid k . Whenever a solution on a coarse grid meets some convergence criterion it is interpolated and added to the next finest grid as a correction.

It becomes necessary to define solution vectors and residual vectors for each grid. For grid k the residual and solution vectors are \hat{r}_k^n and \hat{v}_k^n .

Figure 12 shows the behavior of the residual vector for several GS iterations on grid k . The initial steep slope reflects the reduction of short wavelength error components. The initial rapid progress towards a solution abates as long wavelength error components begin to dominate. A parameter η can be used to govern the jump to a coarser grid. If two successive residuals obey

$$\|\tilde{r}_k^n\| / \|\tilde{r}_k^{n-1}\| < \eta \quad (4.16)$$

then the system of (4.15) should be formed and solved on grid $k+1$. If the residual norm on grid k becomes less than some fraction δ of the last residual norm on grid $k-1$, the correction of grid k can be interpolated and added to the solution of grid $k-1$. Typical values for η and δ are .7 and .2, respectively.

Figure 13 shows the interactions of a three level grid system. The right-hand side of the system (4.15) must be stored; it accounts for the duplicate grids at each level. The difference equation (3.22) becomes

$$\frac{1}{h^2} (u_{i-1j} + u_{i+1j} + u_{ij+1} + u_{ij-1} - 4u_{ij}) = r_{ij} \quad (4.17)$$

The extra grid on level 1 can be employed for solutions of Poisson's equation, (2.9). The term r_{ij} in (4.17) is replaced by $h^2 f_{ij}$.

A Cycle-C multigrid routine, VBOUND, is included in Appendix B. It can be used to solve Laplace's equation or Poisson's equation on a region with irregular boundaries; a uniform square mesh approximates the region.

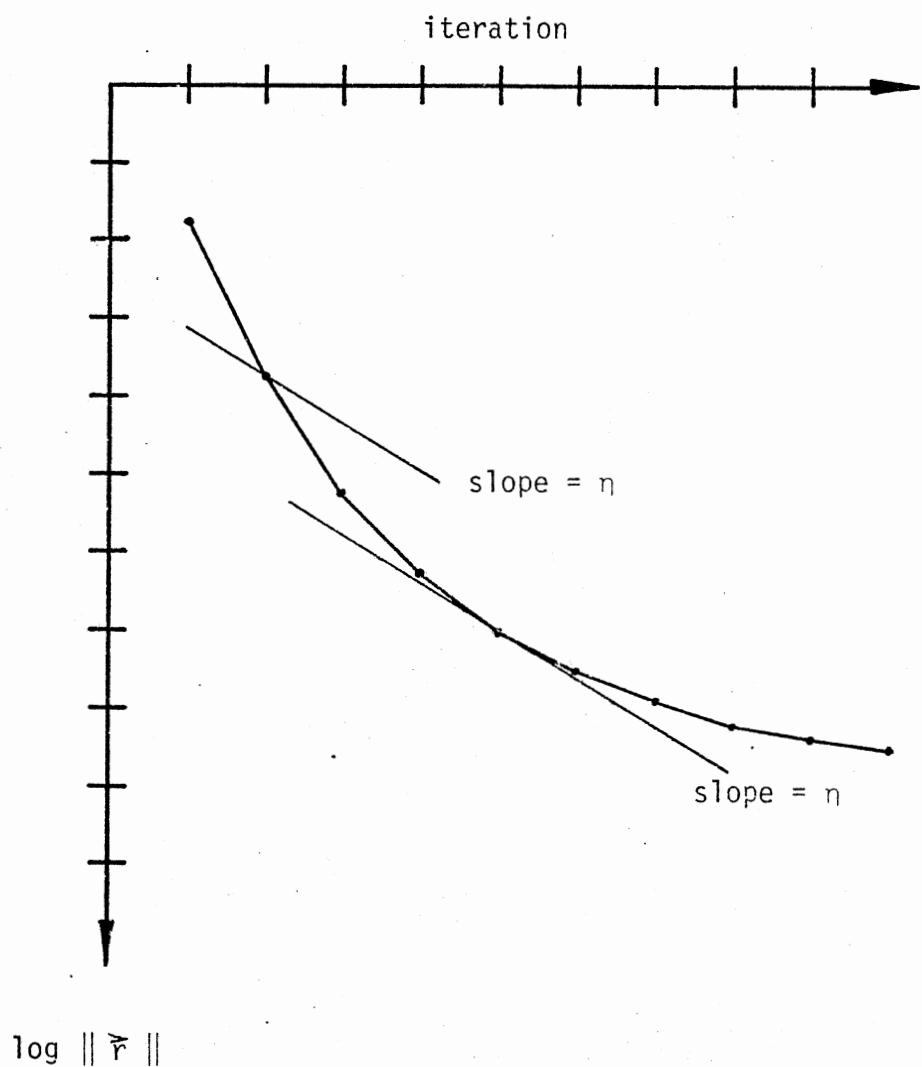
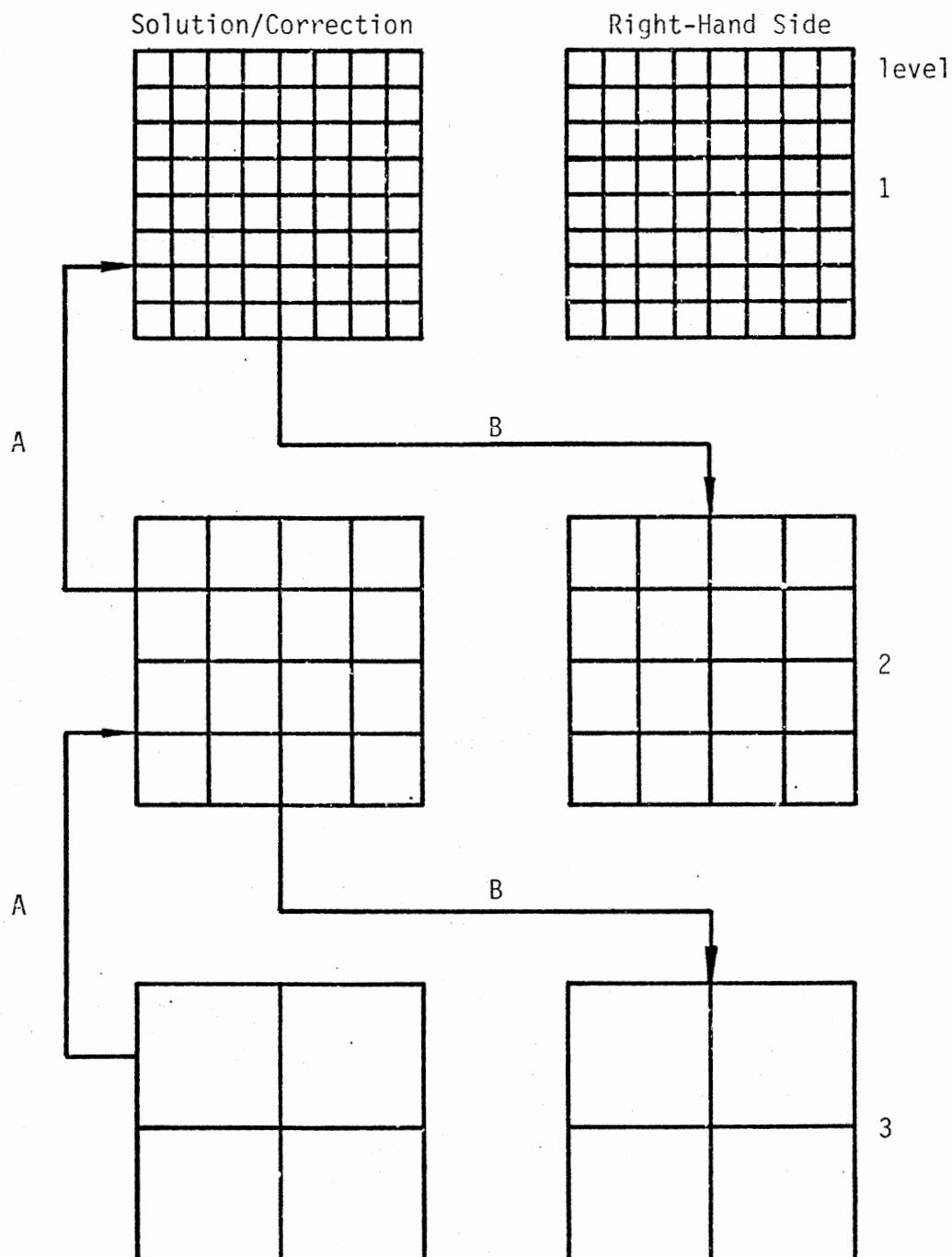


Figure 12. Behavior of the Residual Vector for Gauss-Seidel Iterations



A - Interpolation and Addition of Corrections
B - Calculation of residuals

Figure 13. The Interactions of a Three Grid System in a Multigrid Solution

CHAPTER V

RE-ENTRANT CORNERS IN ELLIPTIC PARTIAL DIFFERENTIAL EQUATIONS

Determining the Form of the Solution

For the general elliptic equation, (2.1), posed on some domain S ,

$$au_{xx} + bu_{xy} + cu_{yy} = f \quad (2.1)$$

the solution has a singularity wherever the coefficients a , b , c , and f are singular or discontinuous, and where boundary features cause derivatives of the solution to be undefined (4). A common singularity arises in elliptic problems when the boundary makes a discontinuous change of direction that forms an internal angle of greater than π radians. This feature is called a re-entrant corner. In Figure 14, the boundary of domain S changes direction at O , the origin of a rectangular coordinate system. The internal angle formed by the segments AO and OB , α , is greater than π .

Re-entrant corners cause finite difference methods to produce results that contain error greater than that which can be attributed to discretization. It is useful in studying re-entrant corners to determine the functional dependences of a solution in its vicinity given some idealized problem. Laplace's equation affords a representative study of re-entrant corners in elliptic problems and their effect on finite difference methods.

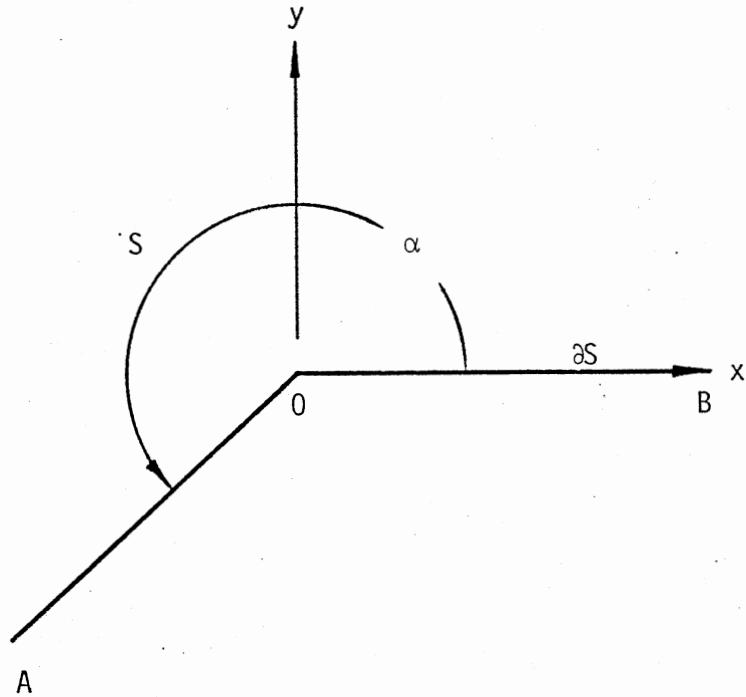


Figure 14. A Re-entrant Corner

Writing Laplace's equation in polar coordinates simplifies the analysis of the solution near the re-entrant corner of Figure 14 (15). It becomes

$$\left(\frac{1}{r} \frac{\partial}{\partial r} + \frac{\partial^2}{\partial r^2} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} \right) u(r_1 \theta) = 0. \quad (5.1)$$

Assuming that u is made up of separate functions in r and θ ,

$$u(r, \theta) = R(r) T(\theta), \quad (5.2)$$

equation (5.1) reduces to two related second order ordinary differential equations (15):

$$\frac{r}{R(r)} \left[\frac{dR(r)}{dr} + r \frac{d^2R(r)}{dr^2} \right] = c^2 \quad (5.3)$$

and

$$\frac{1}{T(\theta)} \frac{d^2 T(\theta)}{d\theta^2} = -c^2 \quad (5.4)$$

General solutions are

$$R(r) = ar^c + br^{-c} \quad (5.5)$$

and

$$T(\theta) = A \cos(c\theta) + B \sin(c\theta). \quad (5.6)$$

Since $u(r, \theta)$ must be defined at the corner ($r = 0$), we can choose to have $c > 0$ and $b = 0$. Then (5.5) becomes

$$R(r) = ar^c. \quad (5.7)$$

Particular solutions can be determined from the conditions on $u(r, \theta)$ on the boundary of S , ∂S . If u is zero on ∂S (Dirichlet conditions), then requiring that $T(\theta)$ vanish there satisfies that condition. Setting A to zero and letting c have the values

$$c = 0, \pi/\alpha, 2\pi/\alpha, 3\pi/\alpha, \dots \quad (5.8)$$

causes T to vanish on ∂S . The solution becomes

$$u(r, \theta) = \sum_{n=1}^{\infty} b_n r^{n\pi/\alpha} \sin(n\pi\theta/\alpha). \quad (5.9)$$

A constant can be added to (5.9) if u is to have some constant value on ∂S .

For Neumann conditions, the normal derivative on ∂S is $\partial u / \partial \theta$. If the normal derivative is to vanish on ∂S , then setting B to zero and

allowing c to have the values in (5.8) will satisfy that requirement.

The solution becomes

$$u(r, \theta) = \sum_{n=1}^{\infty} a_n r^{n\pi/\alpha} \cos(n\pi\theta/\alpha). \quad (5.10)$$

For each of the solutions, the exponent of the first term in r is π/α . Taking the first derivative with respect to r as in (5.1) the exponent becomes $\pi/\alpha - 1$. If α is greater than π then both derivatives in r in (5.10) are undefined at the corner 0 ($r = 0$).

Implicit in the development of the finite difference methods of Chapter III is the requirement that derivatives of the solution through a specified order exist and that they be continuous over all of the solution domain. For the development of the five-point approximation of the Laplacian operator, equation (3.10), the solution must be three times continuously differentiable (11). Since the solutions given by (5.9) and (5.10) are not differentiable at the re-entrant corner, the five-point approximation is invalid there. Its use at the corner introduces error in excess of the expected $O(h^2)$ discretization error (4) (29).

The L-Shaped Region Problem

The effects of a re-entrant corner on the solution of Laplace's equation by finite difference methods can be studied conveniently for the region S of Figure 15. The coordinates of the vertices, A through F, are $(-1,1)$, $(1,1)$, $(0,1)$, $(0,0)$, $(0,-1)$, and $(-1,-1)$, respectively. All of the internal angles are either $\pi/2$ or $3\pi/2$. The problem requires a solution of Laplace's equation on S subject to mixed boundary conditions. The solution has the value -1 on EF and $+1$ on BC. On AB, AF, CD, and DE, the normal derivative must be zero.

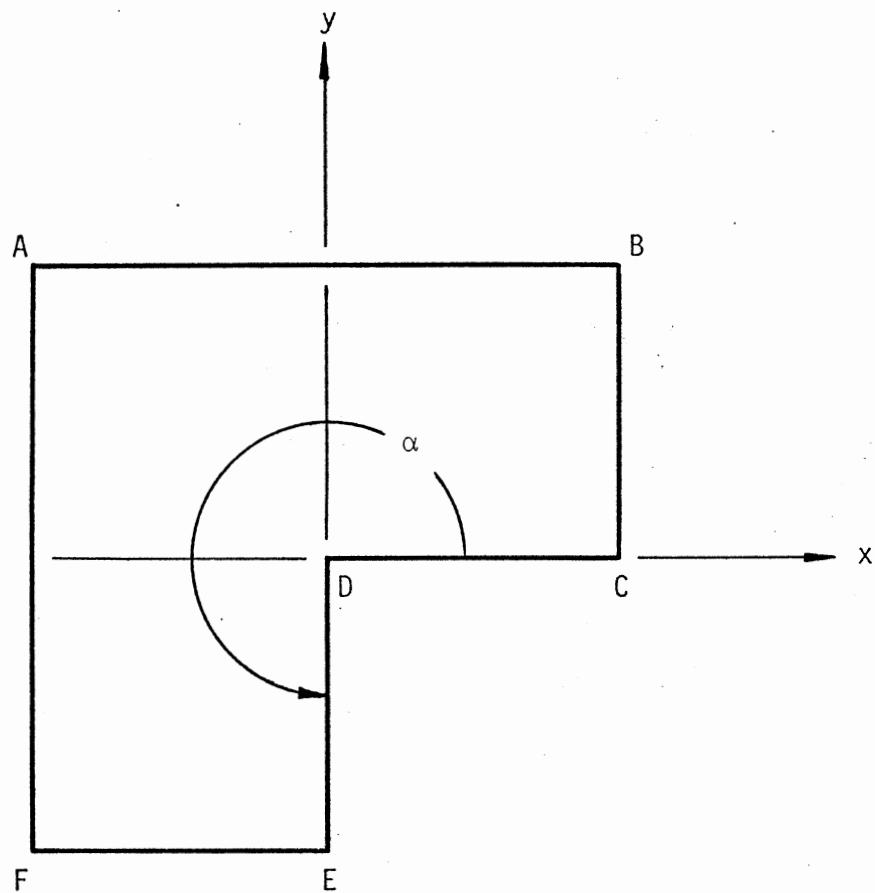


Figure 15. The L-Shaped Region

This is commonly called the L-shaped region problem; a related problem is the L-shaped membrane problem (11) (23). A physical system that corresponds to the problem described above is that of a conducting plate of the same shape with bar contacts attached at BC and EF. The bar contacts are maintained at +1 volt and -1 volt. The solution of the problem describes the electrostatic potential (voltage) on the surface of the plate. The electric field at the surface of the plate can be determined from the potential. Written in polar coordinates, the electric field has a dependence on the first derivative of the

solution with respect to r . Thus, at the re-entrant corner, the electric field becomes undefined (from (5.9) and (5.10)).

At the re-entrant corner, point D, α is $3\pi/2$. The expansion of equation (5.10) applies in the vicinity of the corner due to the Neumann conditions on CD and DE. It can be rewritten as

$$u(r, \theta) = \sum_{n=0}^{\infty} a_n r^{2n/3} \cos(2n\theta/3) \quad (5.11)$$

The solution in this form can be used to determine the truncation error in the five-point approximation of the Laplacian near the singularity.

Figure 16 shows a uniform grid with spacing h in the vicinity of the re-entrant corner. The expected truncation error in the approximation at point P is $O(h^2)$,

$$\nabla^2 u_p = \frac{1}{h^2} (u_D + u_G + u_H + u_J - 4u_p) + O(h^2), \quad (5.12)$$

(from (3.10)). Substituting the series expansion of the solution (5.11), for each value appearing on the right of (5.12) demonstrates that the truncation error is not $O(h^2)$ (29)

$$\nabla^2 u_p = h^{-2} (u_D + u_G + u_H + u_J - 4u_p) + O(h^{-4/3}) + O(h^{-2/3}) + \dots \quad (5.13)$$

The same truncation error occurs at point N in Figure 16. The symmetry in the placement of the values making up the five-point approximation at point D substantially reduces the truncation error,

$$\begin{aligned} \nabla^2 u_D = h^{-2} (u_M + u_N + u_P + u_Q - 4u_D) + O(h^{-2/3}) + \\ O(h^{2/3}) + \dots \end{aligned} \quad (5.14)$$

Thus, the Laplacian is poorly represented by finite difference approximations near the re-entrant corner. From (5.13) and (5.14) an unusual finding is that the truncation error increases as the solution grid is refined (h grows small).

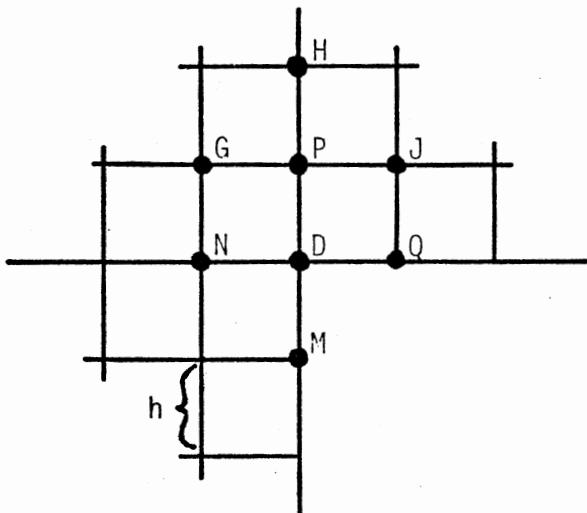


Figure 16. A Uniform Grid Near a Re-entrant Corner

The error in the solution near the singularity is not as serious as that in the approximation of the Laplacian. For Laplace's equation, (5.13) can be rewritten for u_p in terms of the surrounding points,

$$u_p = \frac{1}{4} (u_D + u_G + u_H + u_J) + O(h^{2/3}) + O(h^{4/3}) + \dots \quad (5.15)$$

The truncation error in u_D has the leading term $O(h^{4/3})$. The truncation error in the solution is large compared to that at points some distance from the re-entrant corner. Solution iterations spread this error over

the entire solution domain; the re-entrant corner pollutes the whole solution.

There are methods for restoring the accuracy of the solution. These use some sort of special treatment in the region about the re-entrant corner, or they seek to restate the problem in a way that eliminates the re-entrant corner altogether. Near the corner, the analytical form of the solution can be used (when it is known), or a finer grid can be employed.

Motz's Method for Re-Entrant Corners

When the analytical form of the solution is known near a re-entrant corner or any other type of singularity, it can be incorporated into a finite difference solution method. Such modified methods are due to Motz (20) and Woods (31); the methods are applied by Reid and Walsh (23) and Whiteman (30). The method considered here is the one due to Motz.

The form of the solution of Laplace's equation near a re-entrant corner is given by one of (5.9) and (5.10). Thus, the solution of Laplace's equation can serve to test and develop Motz's method. Returning to the L-shaped region problem, the solution near the re-entrant corner is given by equation (5.10). The coefficients, a_n , are not given, though they can be determined from the continuous solution. Making the assumption that values of the discrete solution some distance away from the corner are exact, approximation for the first few coefficients can be determined. Equation (5.10) must be truncated after k terms and k remote values of the discrete solution must be selected in order to determine a set of coefficients. Equation (5.10) becomes

$$u_j = \sum_{n=0}^{k-1} a_n c_{jn} \quad (5.16)$$

for each remote value, u_j . The coefficients c_{jn} depend on the coordinates of u_j , (r_j, θ_j) ,

$$c_{jn} = r_h^{2n/3} \cos (2n\theta_j/3). \quad (5.17)$$

Defining the vector \vec{u}_r made up of remote values and the vector \vec{b} made up of the coefficients, b_n , the system

$$\vec{C}\vec{b} = \vec{u}_r \quad (5.18)$$

results from writing (5.16) for each u_j . The system of (5.18) can be solved directly or iteratively for the vector of coefficients, \vec{b} .

Figure 17 shows the grid points near the re-entrant corner of Figure 15. The truncated series used to give the solution value at each grid point within a distance d of the corner (23),

$$u_m = \sum_{h=0}^{k-1} b_n d_{mn} \quad (5.19)$$

The coefficients d_{mn} depend on the coordinates of u_m ,

$$d_{mn} = r_m^{2n/3} \cos (2n\theta_m/3). \quad (5.20)$$

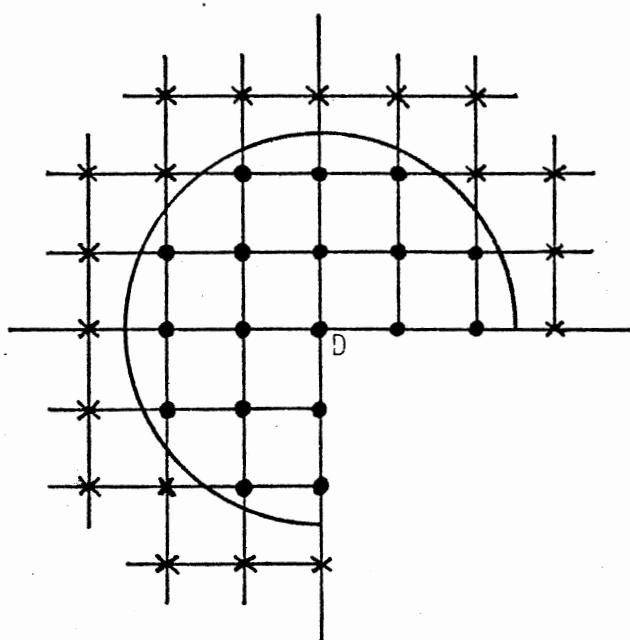
Defining the vector u_s of series replacement values, the system

$$D\vec{b} = \vec{u}_r \quad (5.21)$$

results when (5.19) is written for each u_m ; D is not necessarily a square matrix. Values at grid points farther than d from the re-entrant corner, outside the arc in Figure 17, are candidates for components of \vec{u}_r .

Motz's method has been presented as if an accurate solution exists. In practice, the steps outlined here must be used at each iteration.

The vector of series values approaches the correct solution with each iteration causing the vector of finite difference values, \vec{u}_r , to approach the correct solution, in turn. Information flows in two directions across the boundary between the series process and the finite difference process. The vector \vec{u}_s is built up from information propagated from distant boundaries by the finite difference process. Values of \vec{u}_r that are linked to values of \vec{u}_s by the five-point approximation, (5.12), are prevented from seeking the erroneous values of the uncorrected solution. They influence the remaining points of \vec{u}_r through the iteration process.



- components of \vec{u}_s
- choices for components of \vec{u}_r

Figure 17. Remote Points and Series Replacement Points

It is important to note that the matrices C and D of (5.18) and (5.21) do not change from iteration to iteration. The matrix C can be put in a form that requires only $O(k^2)$ operations to determine \vec{b} from a new \vec{u}_r as opposed to $O(k^3)$ operations if C changes. The routines DECOMP and SOLVE from (10) provide this economy. An iteration of the hybrid method involves a sweep with SOR or some other method followed by the determination of \vec{b} and \vec{u}_s .

Conformal Mapping for Re-entrant Corners

As mentioned in Chapter II, complex transformations, conformal mappings, can be used to simplify the geometry of problems with complicated features. Also, a solution of Laplace's equation for the transformed problem is a solution of the original problem when it is transformed to the original setting. Thus, conformal mappings can be used to eliminate re-entrant corners and dispense with the need for a special treatment near a corner (23) (28) (29) (30).

For the L-shaped region of Figure 15, a useful mapping is

$$w = z^{2/3} \quad (5.22)$$

Domains w and z are given by $z = (x + iy)$ and $w = (t + iv)$. The corner formed by segments CD and DE is eliminated. Figure 18 shows the transformed region; the vertices are labeled so that they correspond to the vertices of the L-shaped region. Only the segments CD and DE are lines in the transformed problem; all other segments become curves.

The potential problem described earlier for the L-shaped region can be solved on the domain of Figure 18. The boundary conditions of the original problem apply to the transformed problem segment by

segment: Dirichlet conditions on BC and EF, Neumann conditions elsewhere. Finite difference methods can be used to produce a solution.

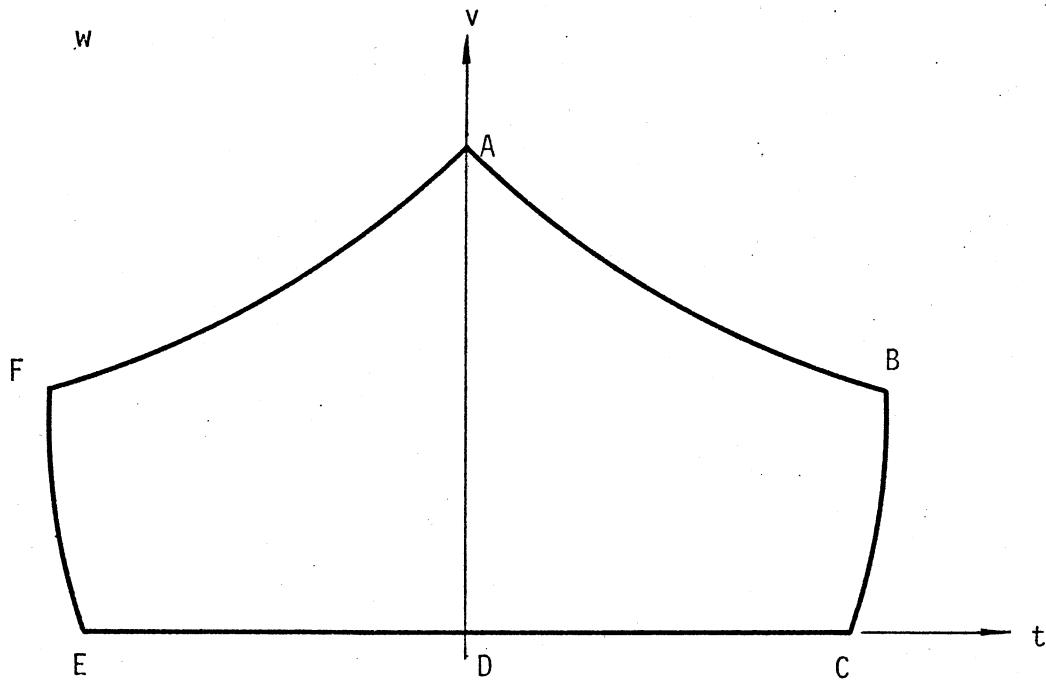


Figure 18. Tranformed L-Shaped Region

Several complications are introduced by the conformal mapping of (5.22). The curved boundaries of transformed solution domain require the use of irregular grids near the boundary in the finite difference process. The accuracy of the solution can be reduced (4) (11) (23). The Neumann conditions are particularly troublesome. Complicated interpolation schemes are required to implement them (4) (11). If the solution is to be used in the z domain the inverse mapping

$$z = w^{3/2} \quad (5.23)$$

can be used or points in the z domain can be transformed using (5.22).

In either case, an interpolation scheme with accuracy equivalent to that of the solution must be used.

For a general re-entrant corner with internal angle $\alpha = \pi/m$ the form of (5.22) becomes

$$w = z^m = r^m e^{im\theta} \quad (5.24)$$

for z in polar coordinates.

Grid Refinement

The largest truncation term for the L-shaped region problem is $O(h^{2/3})$; it occurs at points adjacent to the re-entrant corner. The truncation error there can be made to approach the $O(h^4)$ error that exists at points far removed from the re-entrant corner. If a fine grid is used near the re-entrant corner, its spacing, h_d , must approach h^6 to give the desired truncation error.

The use of such a grid must be restricted to the immediate neighborhood of the re-entrant corner in order to keep storage to a minimum. It must be used in concert with coarser solution grid. By using a collection of grids with spacing $h/2, h/4, \dots, h_d$, the solution grid can be connected to the fine grid. Figure 19 shows such a grid system.

The multigrid method can be adapted to use refined grids near a re-entrant corner. The grids can be fixed in place (5) or they can be generated as needed (6) (7). The adaptive multigrid process requires sophisticated routines for sensing error and managing the collection of grids. Near a feature such as a re-entrant corner as many as 20 grids might be used (7).

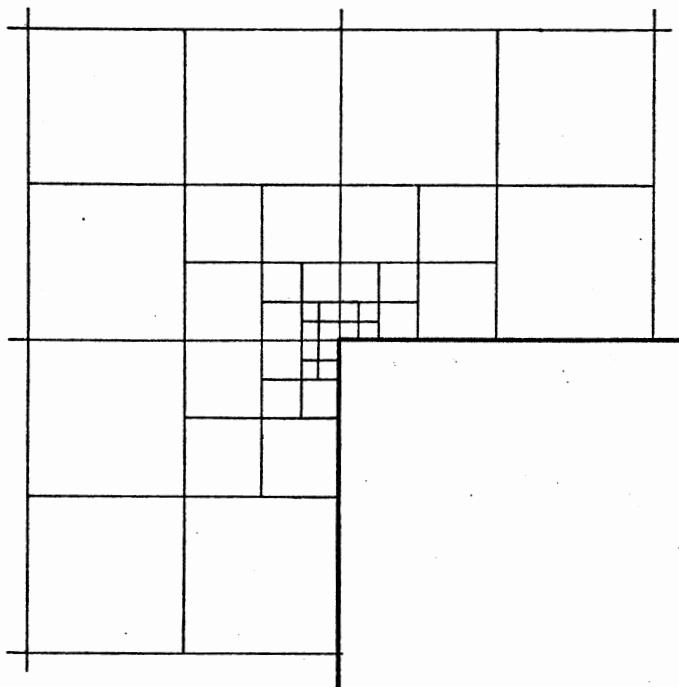


Figure 19. Refined Grids Near a Re-Entrant Corner

Here, grid refinement is used in conjunction with extrapolation to produce an accurate solution for the L-shaped region problem. As h goes to zero, solutions produced with finite difference methods approach the actual solution. By using a sequence of spacings, a convergent sequence of solutions can be produced. Aitken extrapolation can be used to give an estimate of the limit. Here, the sequence

$$h, h/2, h/4, \dots \quad (5.25)$$

is used.

CHAPTER VI

RESULTS OF NUMERICAL EXPERIMENTS AND CONCLUSIONS

Performance Comparisons for Several Iterative Methods

Young's test problem (32) is an excellent means for comparing the iterative methods developed here. The dominant eigenvalues of the iteration matrices of the J and GS methods are known, hence, the optimum value of ω can be determined for the SOR and SSOR methods.

The test problem requires the solution of Laplace's equation on a square with sides of length π . There are Dirichlet conditions on the boundary of the square. The solution is set to zero on the boundary; the initial solution estimate is everywhere one. After each iteration of a particular method, the solution estimate serves as the error for the iteration since the solution must be everywhere zero.

The dominant eigenvalue of G_j is given by

$$\mu = \cos(h) \quad (6.1)$$

where h is the spacing of a uniform grid on the square (4) (11). Then, the dominant eigenvalue for G_g is

$$\Lambda = \cos^2(h) \quad (6.2)$$

from (3.53). Equation (4.7) for the optimum ω becomes

$$\omega_b = 2/(1 + \sin(h)) \quad (6.3)$$

Figure 20 shows the behavior of the residual vectors produced by the J, GS, SOR, and SSOR methods over 50 iterations for the test problem. The grid spacing is $h = \pi/32$. The norm of equation (3.44) is used as a measure of the residual vectors. The logarithm of the norm is plotted versus the iteration number in order to make its behavior visible over several orders of magnitude. Iterations of the SSOR method are counted as two iterations of the SOR method.

In Figure 20, the GS and J methods rapidly become asymptotic and exhibit the slow convergence predicted earlier. The lines representing the GS and J methods eventually cross. The SOR and SSOR methods make large initial reductions of their solution vectors towards zero. Once they become asymptotic they demonstrate superior performance in reducing the residuals to zero. The value of ω_b used for SOR and SSOR iterations is 1.821465 (from equation (6.3)).

Figure 21 shows the behavior of the error (solution) vectors over 50 iterations for the problem described above. Again, SOR and SSOR demonstrate superior convergence characteristics. From Figures 20 and 21, it is evident that SOR is a better solution method than SSOR. The symmetric iteration matrix of the SSOR method requires a performance sacrifice (32).

Table I gives comparisons between the known values of the dominant eigenvalues of the J and GS iteration matrices and experimentally determined values for the test problem. The experimental values are determined from the residual norm by using equations (4.3) and (4.6), Aitken extrapolation. The experimental values are given after 20 iterations and 100 iterations; the values of ω_b they would give are included in the table. It is apparent that the GS method affords better estimates of ω_b than the J method.

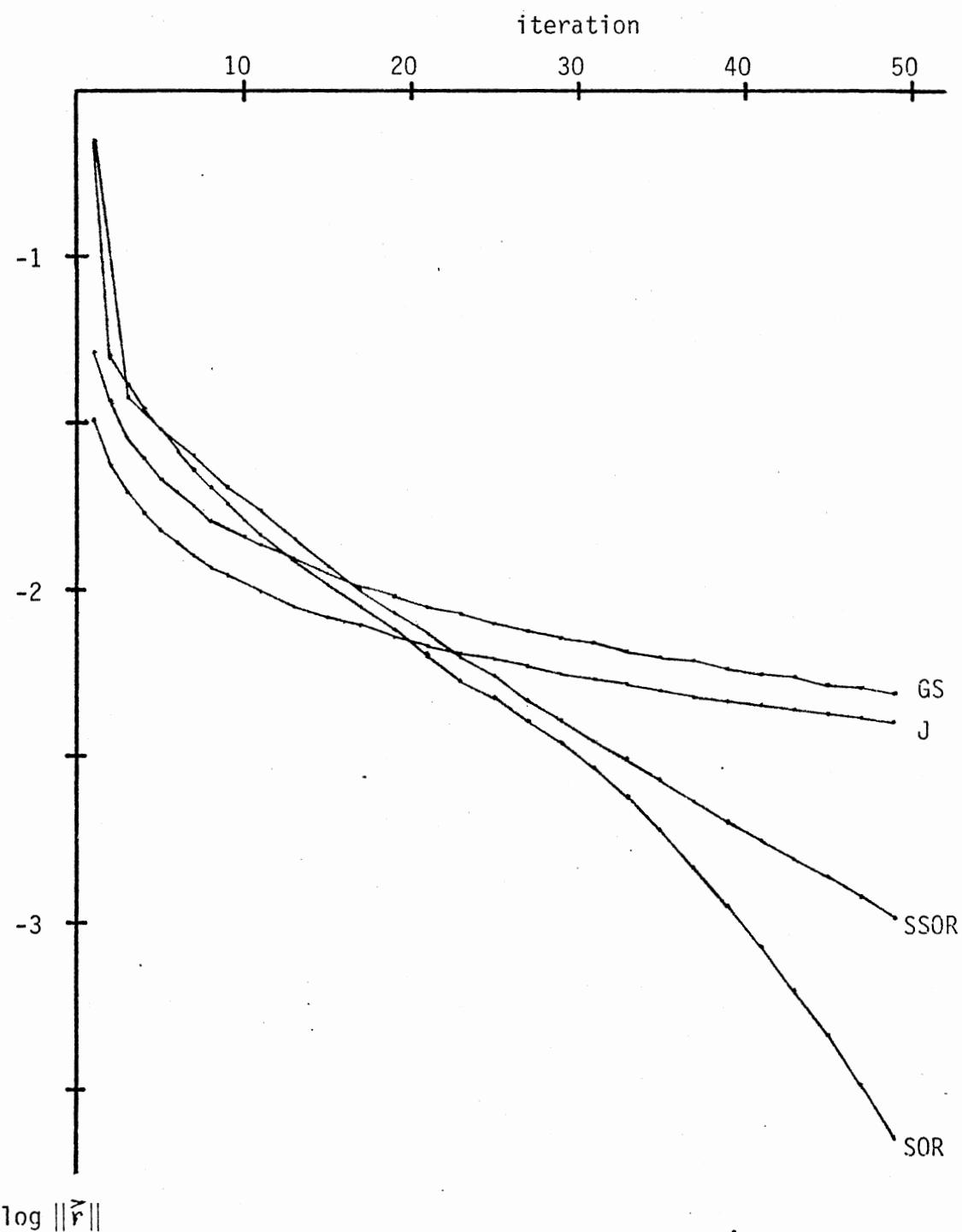


Figure 20. Behavior of the Residual Norms of the J, GS, SOR, and SSOR Methods for Young's Test Problem ($h = \pi/32$)

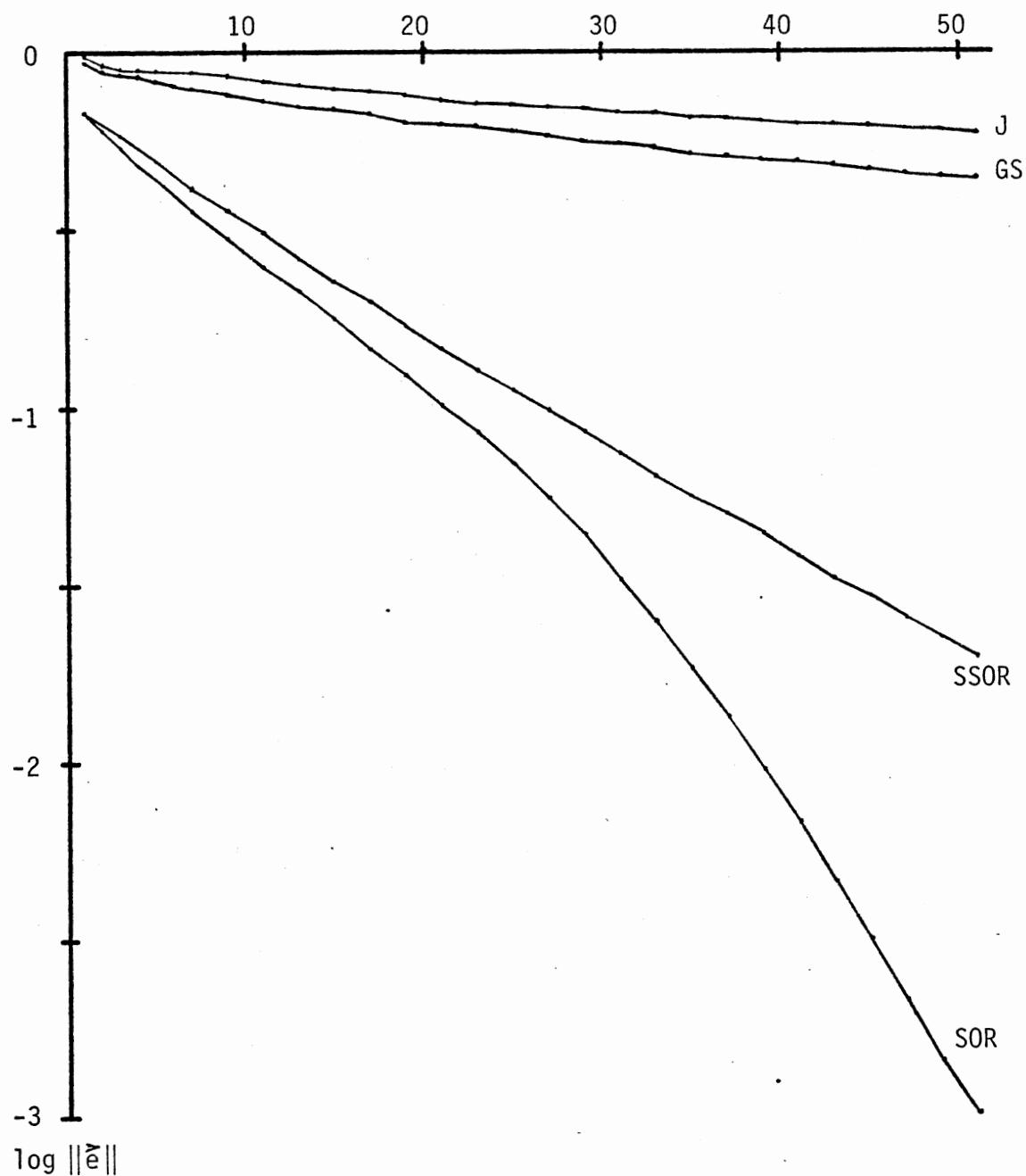


Figure 21. Behavior of the Error Norms of the J, GS, SOR, and SSOR Methods for the Test Problem ($h = \pi/32$)

TABLE I
KNOWN AND EXPERIMENTAL VALUES OF THE
DOMINANT EIGENVALUES FOR THE J AND
GS METHODS FOR THE TEST PROBLEM

	J	GS
Known $S(G)$ (ω_b)	.9951847 (1.821465)	.9903926 (1.821465)
$S(G)$ from 20 iterations (ω_b)	.9820577 (1.682679)	.9808125 (1.756668)
$S(G)$ from 100 iterations (ω_b)	.9924346 (1.781302)	.9894568 (1.813763)

Figure 22 shows the general characteristics of the iterates produced by the J, GS, and SSOR methods in a solution of the test problem. The sharp edges of the initial solution estimate are smoothed and the iterates take on a "pillow" shape. The solution tapers from a central maximum to zero on the boundary. For SOR, the maximum is skewed away from the center. The J and GS methods are particularly good at smoothing iterates. If their iterates are normalized to one following each iteration, they approach the function

$$f(x,y) = \sin(x) \sin(y), \quad (6.3)$$

an eigenfunction of the Laplacian differential operator.

The value of the central maximum of an iterate after a specified number of iterations is an additional indication of its effectiveness. The values range from .907 for the J method to $.545 \times 10^{-6}$ for SOR after 100 iterations. The exact value is zero.

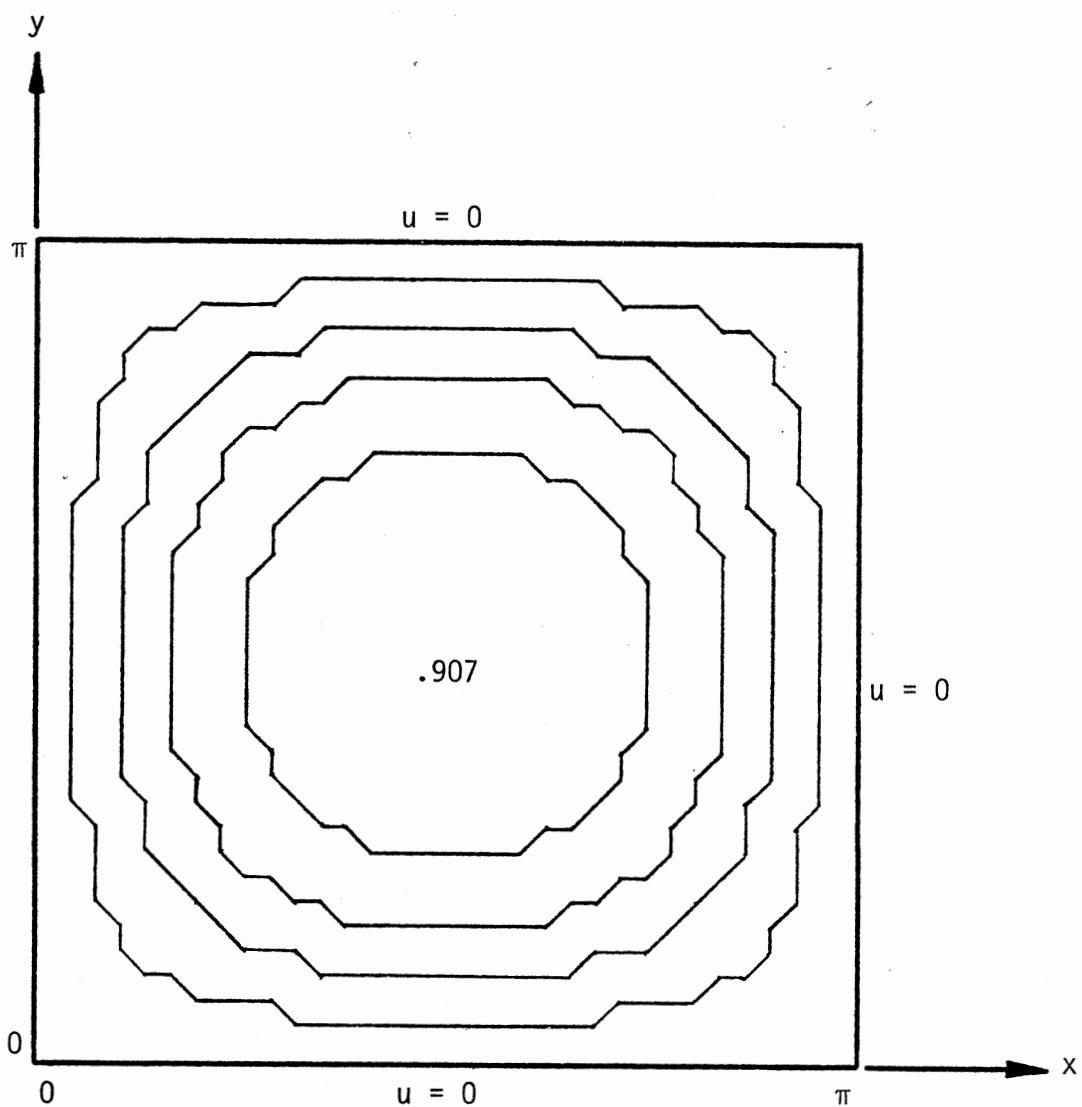


Figure 22. The Solution Vector of the J Method After 100 Iterations ($h = \pi/32$)

Figure 23 shows the residual norms of SOR, SSOR with vector Aitken acceleration (SSOR/VA), and the Cycle-C multigrid method. Dashed lines indicate extrapolations for SSOR/VA and coarse grid excursions for the multigrid method. The effort expended in coarse grid operations is measured according to iterations on the solution grid (identical to the SOR and SSOR grids). Figure 24 shows the error norms for the three methods.

Clearly, the Cycle-C multigrid method is superior to the SOR and SSOR/VA methods for the test problem. It meets its stopping criterion after the equivalent of 29 iterations. The SOR and SSOR/VA method show essentially the same performance over 100 iterations.

Table II gives a summary of the results for the test problem. Asymptotic rates of convergence, $R(G)$, determined experimentally, are given for each method; actual rates are given when the dominant eigenvalue is known. Equation (3.46) is used to determine the rates. The value of the central maximum of the solution vector produced by each method is given, also. Each result is based on 100 iterations of the corresponding solution method (29 for the multigrid method). The exponential notation of FORTRAN is used in the table.

The experiments with the test problem indicate that the Cycle-C multigrid method should be the first choice for a solution method. The SSOR/VA method should be the second choice.

Analysis of the L-Shaped Region Problem

When no re-entrant corner or other type of singularity is present, the error in individual components of a solution of Laplace's equation using the five-point approximation, (3.10), is $O(h^2)$ (11). If the

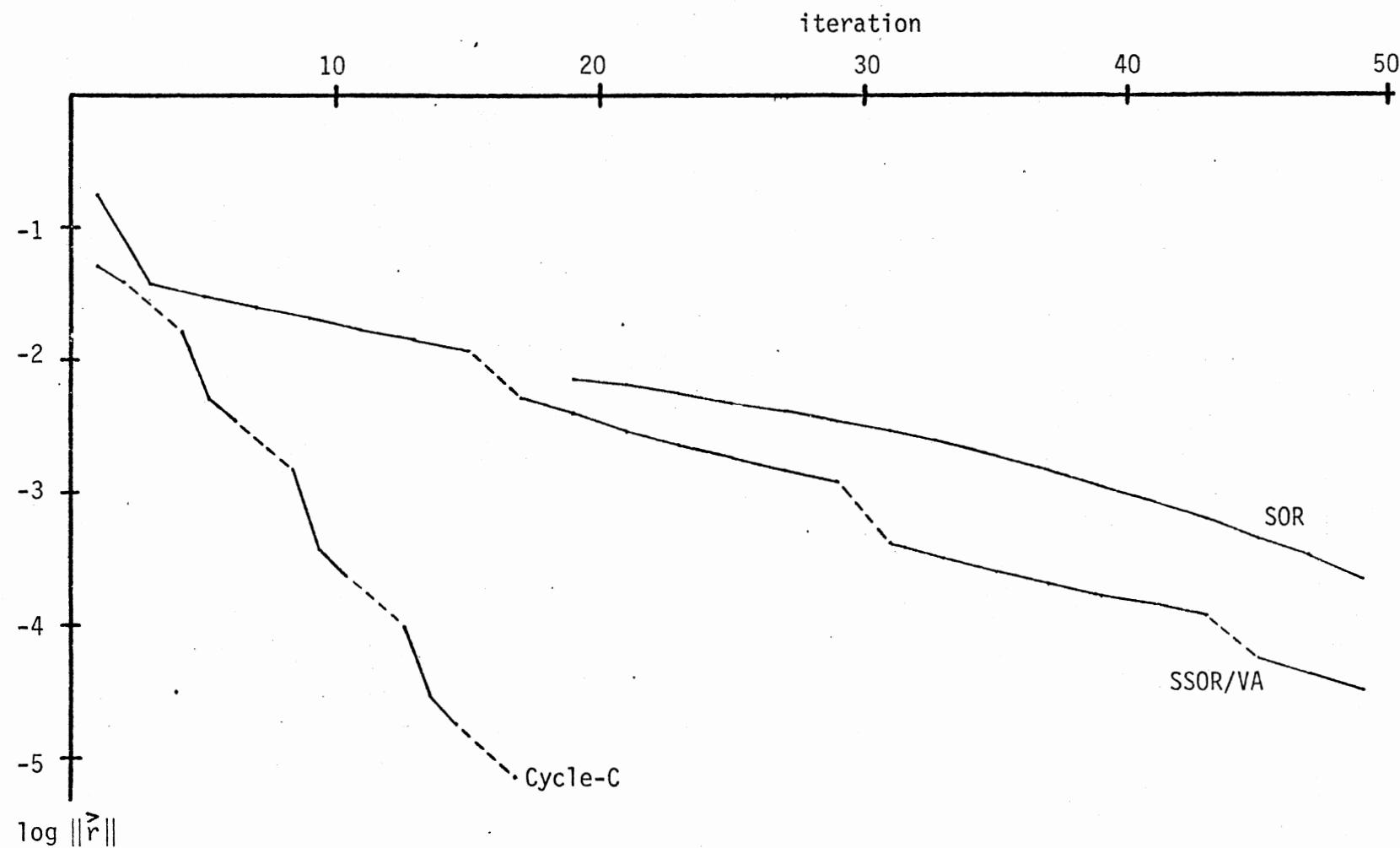


Figure 23. Behavior of the Residual Norms of the SOR, SSOR/VA, and Cycle-C Methods for the Test Problem ($h = \pi/32$)

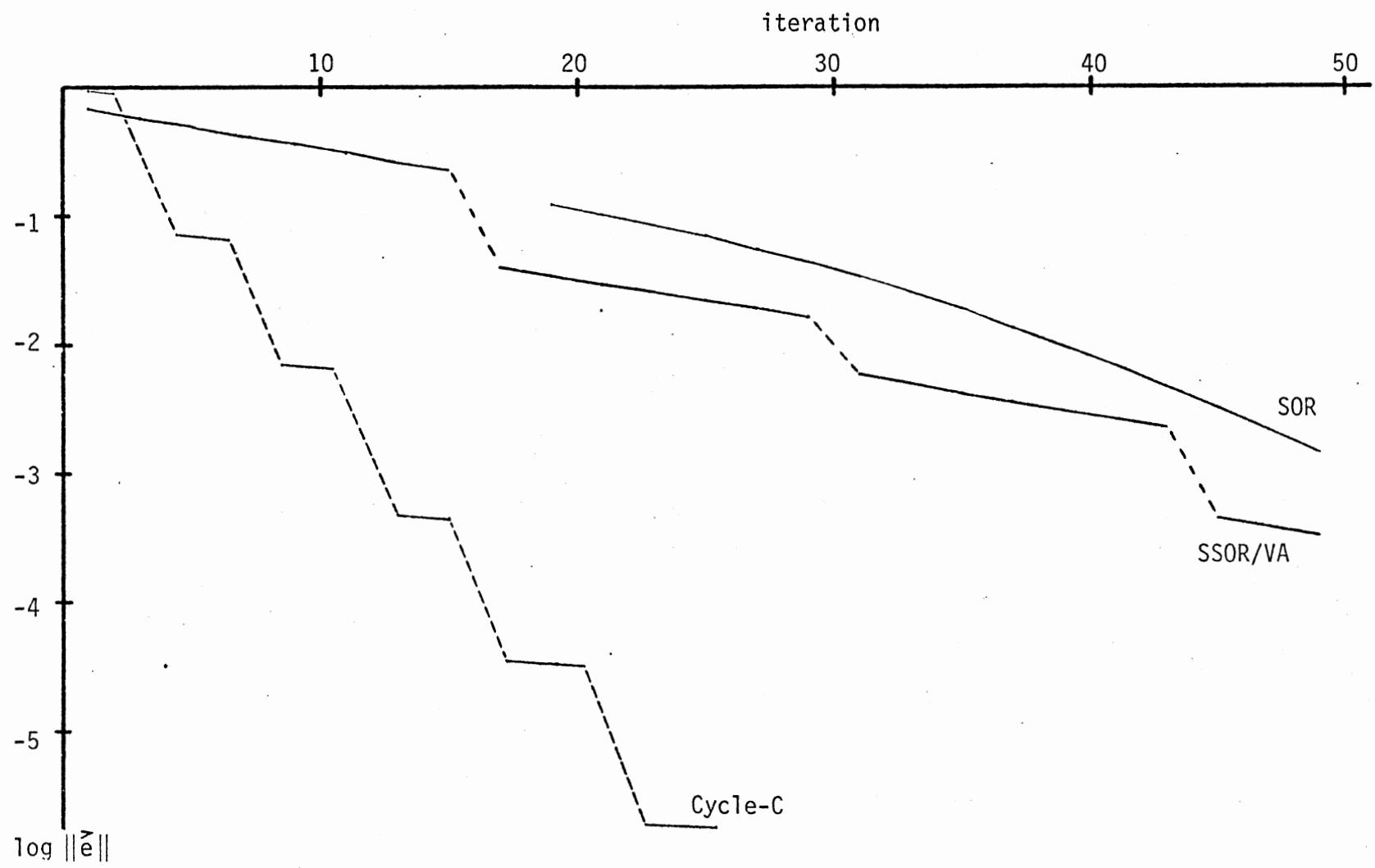


Figure 24. Behavior of the Error Norms of the SOR, SSOR/VA, and Cycle-C Methods for the Test Problem
($h = \pi/32$)

actual solution at a grid point with coordinates (x,y) is $u_\infty(x,y)$, the value given by a finite difference solution can be written

$$u_k(x,y) = u_\infty(x,y) + ah_k^2 + bh_k^4 + \dots \quad (6.4)$$

where h_k is the spacing of a uniform grid (11). By producing solutions for several values of h_k , the coefficients in (6.4) can be determined.

TABLE II
SUMMARY OF RESULTS FOR THE TEST PROBLEM

Method	R(G) (known)	R(G) (experimental)	$\max e_i $
J	.2096309E-2	.3298102E-2	.9069986E0
GS	.4192613E-2	.4603162E-2	.6105773E0
SOR	.8541094E-1	.1306649E0	.5452358E-6
SSOR	--	.5590545E-1	.2024361E-2
SSOR/VA	--	.1520199E0	.3419504E-7
Cycle-C	--	.2589699E0	.2329918E-6

The effect of a re-entrant corner on the accuracy of finite difference solutions can be gauged by seeking a relation of the form (6.4). If it has the same powers in h , then the re-entrant corner has little influence.

Here, the L-shaped region problem of Chapter V is used to model the effects of a re-entrant corner. Figure 25 shows a solution that results

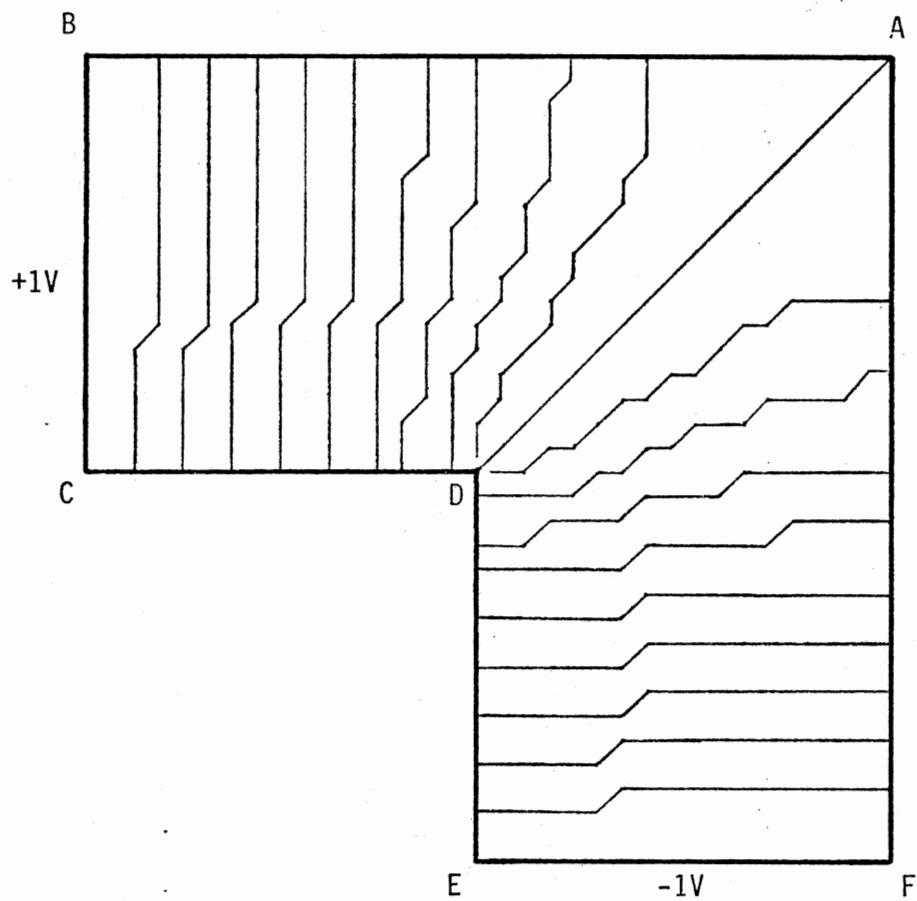


Figure 25. A Solution of the L-Shaped Region Problem
Using SSOR/VA (20 Graduations)

from roughly 150 iterations of the SSOR/VA method; the segment AB has length 1.0 and h is 1/32. The solution is indicated by contours that range from -1.0 on EF to +1.0 on BC in 20 graduations. The solution is zero on the line of symmetry AD. From the Neumann conditions on BAF and CDE, each contour is tangent to the boundary at points of intersection.

The model used for the error in components of the solution is

$$u_k(x,y) = u_\infty(x,y) + ah_k^\alpha + bh_k^\beta. \quad (6.5)$$

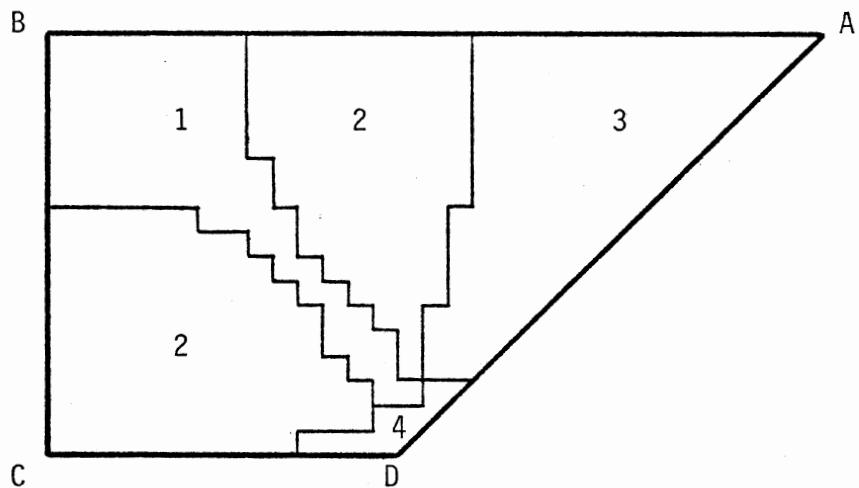
The terms in α and β are the dominant error terms. By producing solutions for the spacings h_0 , h_1 , h_2 , and h_3 where $h_k = 2^{-k}h_0$, approximate values for α and β can be determined. Assuming that the term in α is dominant, the term in β can be dropped from (6.5). Then, writing the resulting equation for h_1 , h_2 , and h_3 gives

$$\alpha \approx \log [(u_3 - u_2)/(u_2 - u_1)]/\log (k) \quad (6.6)$$

at point (x,y) ($k = h_3/h_2$).

Solutions for $h_0 = 1/16$ through $h_3 = 1/128$ were produced in order to determine α and β . The residual norm for each solution was reduced to 10^{-14} by using double precision in a FORTRAN program.

Using (6.6) at points (x,y) where u_1 , u_2 , and u_3 exist gives the distribution of Figure 26. The segment AD is a line of symmetry for the distribution. Values of α range from 1.166 to 1.476. The greatest variance of values occurs about the re-entrant corner. The large number of values in the range 1.290 to 1.383 and the previous analysis of the L-shaped region problem (Chapter V) suggests that α is 4/3.



- 1--1.243 to 1.290 (77 points)
- 2--1.290 to 1.282 (189 points)
- 3--1.383 to 1.461 (115 points)
- 4--1.166 to 1.476 (10 points)

Figure 26. Distribution of Values of α

Using $\alpha = 4/3$ and both of the terms of (6.5) in h , an expression for β can be derived,

$$\beta = \log \left[\frac{k^{-\alpha}(u_3 - u_2) - (u_2 - u_1)}{k^{-\alpha}(u_2 - u_1) - (u_1 - u_0)} \right] / \log (k) \quad (6.7)$$

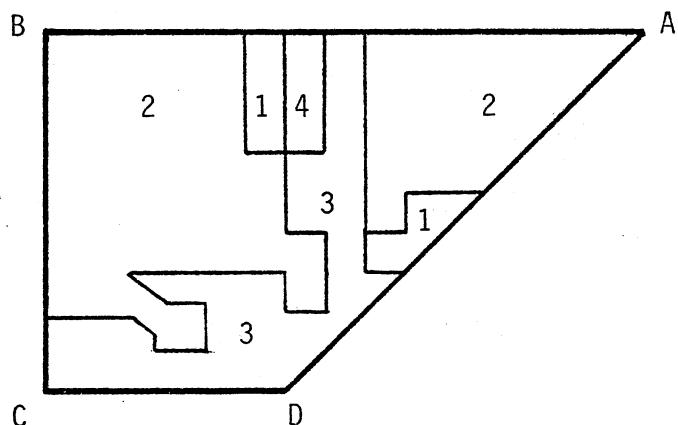
Applying (6.7) where u_0 through u_3 exist gives the distribution of Figure 27. The values range from 1.214 to 3.684. The largest number of values lie in the range 1.708 to 2.202 suggesting that β is 2 or 6/3.

Thus, it seems likely that the error components of the solution are given by

$$u_k(x,y) = u_\infty(x,y) + ah_k^{4/3} + bh_k^2 + ch_k^{8/3} + \dots \quad (6.8)$$

or $O(h^{4/3})$. This is serious degradation of the accuracy normally

afforded by finite difference methods. One of the techniques developed in Chapter V should be used to reduce the influence of the re-entrant corner.



- 1--1.214 to 1.708 (7 points)
- 2--1.708 to 2.202 (61 points)
- 3--2.202 to 2.860 (19 points)
- 4--2.820 to 3.684 (5 points)

Figure 27. Distribution of Values of β

The Multigrid Method for Re-Entrant Corners

It was hoped that the multigrid method could be used to develop solutions for the L-shaped region problem due to its speed and economy. It was found, though, that a single re-entrant corner could completely disrupt the Cycle-C process. As a result, the multigrid method had to be abandoned.

Figure 28 shows the behavior of the residual norm produced by iterations on the finest grid ($h = 1/32$); dashed lines indicate coarse grid excursions. After rapid initial progress toward a solution, the

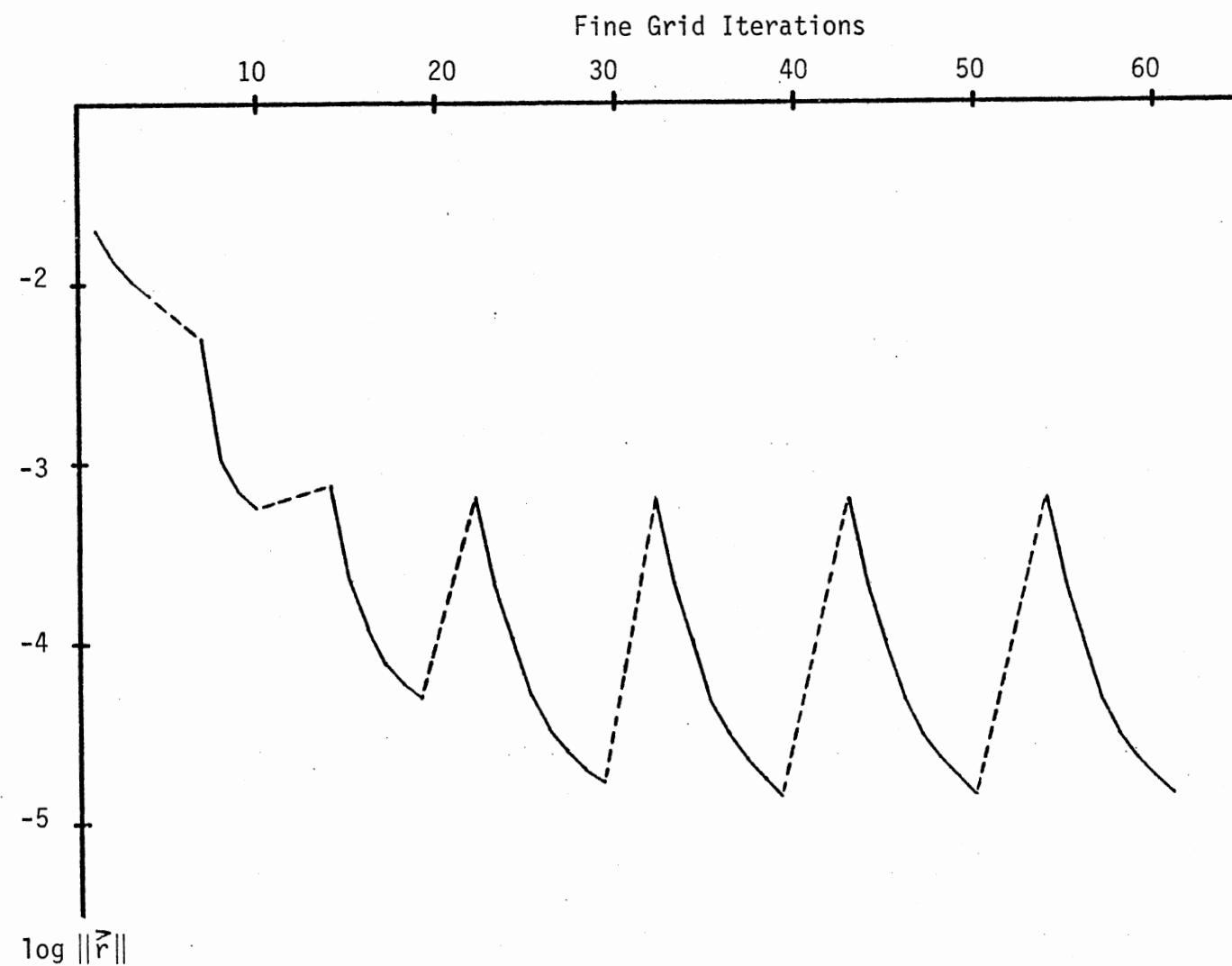


Figure 28. Behavior of the Multigrid Cycle-C Method for the L-Shaped Region Problem
($h = 1/32$)

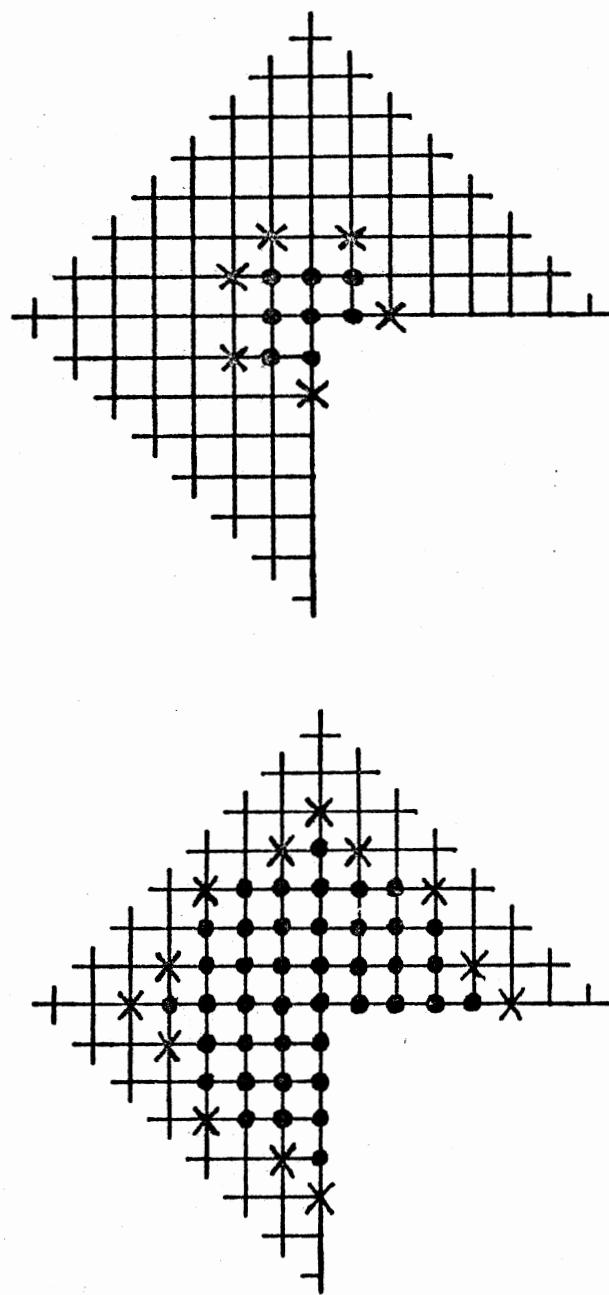
solution process enters a cyclic phase during which little progress is made. The operations on coarse grids to calculate corrections degrades to the point that large amounts of error are introduced into the solution on the fine grid. That error is quickly eliminated, but another coarse grid excursion reintroduces it.

The Behavior of Motz's Method for the L-Shaped Region Problem

Motz's method was used in conjunction with the SSOR/VA method in an attempt to restore the $O(h^2)$ discretization error when a re-entrant corner was present. The method was tested for accuracy and stability by using the L-shaped region problem with varying grid sizes. The use of extrapolation provided an additional test of stability.

Two sets of patterns of remote points and series replacement points were used. The simpler set of patterns involved 6 remote points and 8 series points. The more complex set had 13 remote points and 41 series points. The two sets are referred to as the 8-point and 41-point patterns, respectively. Figure 29 gives their organization. At the beginning of the forward and backward sweeps on an SSOR iteration, Motz's method was used to assign values to the series points. During an iteration, the series points were skipped.

The results of experiments with single precision arithmetic demonstrate limitations of Motz's method. The combined method converges (SSOR/VA and Motz), but progress slows when Motz's method becomes the dominant source of error. This occurs when the displacements in the series values and the quantities that make up the series values vary over the range of the single precision mantissa (seven digits). The



• - series point

x - remote point

Figure 29. The 8- and 41-Point
(Series) Patterns for
Use with Motz's Method

vector \vec{d}_s^n made up of displacements in the series point vector, \vec{u}_s , is useful for observing the behavior of Motz's method,

$$\vec{d}_s^n = \vec{u}_s^n - \vec{u}_s^{n-1}. \quad (6.9)$$

Figure 30 shows the norm of \vec{d}_s^n for the 8-point pattern and the residual norm following the final vector Aitken extrapolation.

The displacement vector exhibits similar behavior when double precision arithmetic (16 digit mantissa) is used. Figure 31 shows the displacement norm for the 41-point pattern and the residual norm following the final extrapolation. Figure 32 indicates that the norm of \vec{d}_s^n exhibits the characteristics observed earlier in the error and residual norms produced by the SSOR/VA method. A minimum of 10 iterations occurs between extrapolations.

An Accurate Solution for the L-Shaped Region Problem

An accurate solution is needed to gauge the effectiveness of Motz's method. It must be free of the error induced by the re-entrant corner. By using vector extrapolation, the uncorrected solutions used earlier to determine the exponents of (6.5) can yield an accurate solution. As mentioned in Chapter V, grid refinement produces solutions that converge to the actual solution. An extrapolation scheme based on equation (6.5) can be used to determine the components of the actual solution.

Solutions from grids with spacing $h_1 = 1/2$ through $h_7 = 1/128$ ($h_k = h_{k-1}/2$) were used to test the effects of extrapolation. Aitken extrapolation, equation (4.6), was used with corresponding components

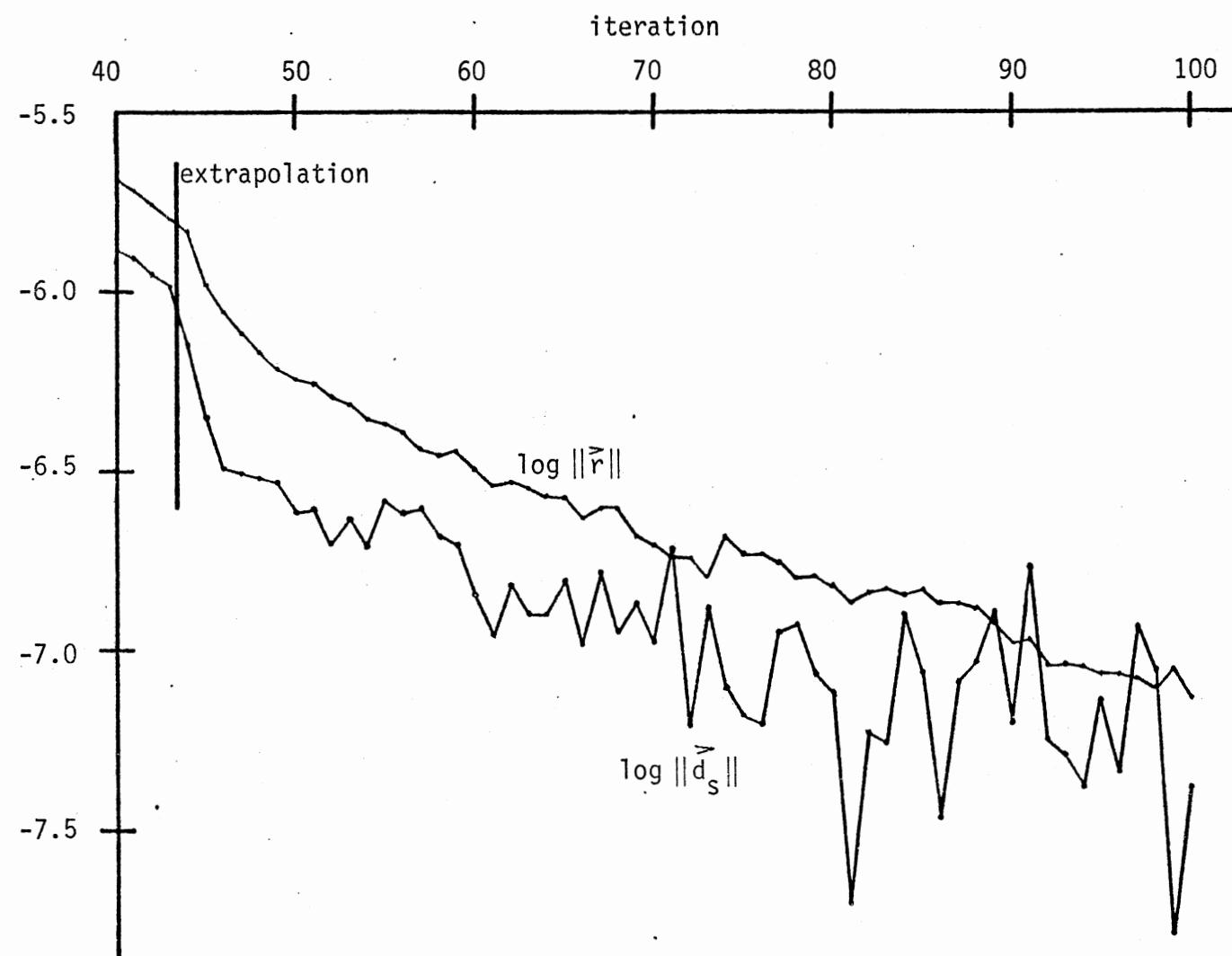


Figure 30. The Behavior of SSOR/VA and Motz's Method (8-Point Pattern) in Single Precision (Seven Digit Mantissa)

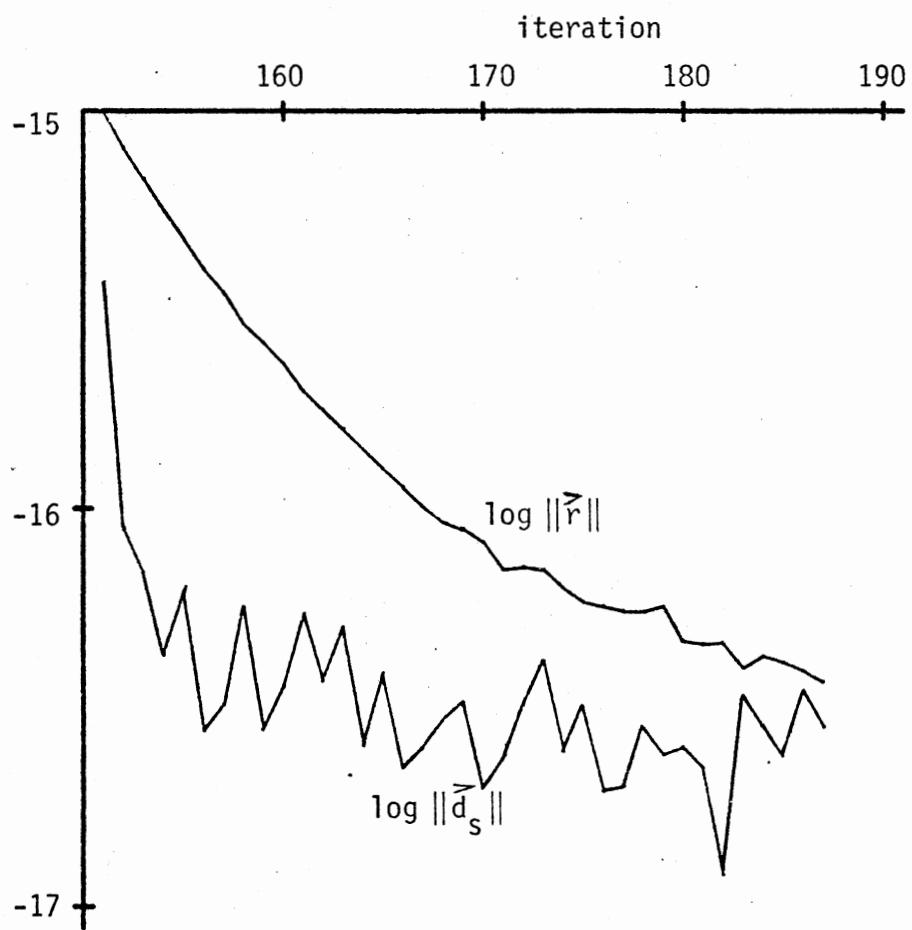


Figure 31. The Behavior of SSOR/VA and Motz's Method
(41-Point Pattern) in Double Precision
(Sixteen Digit Mantissa)

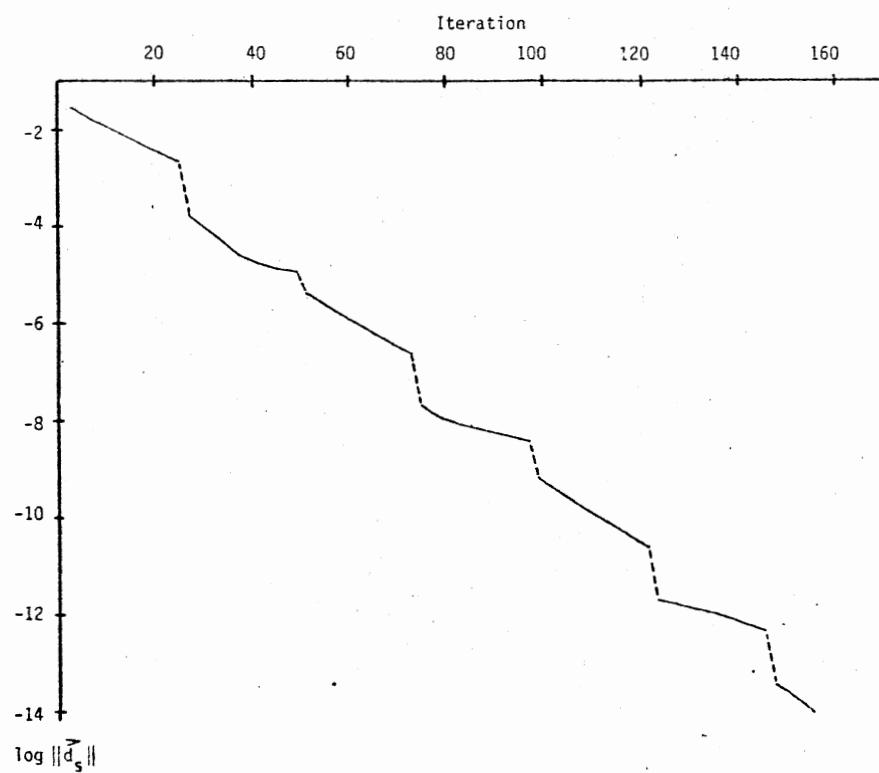


Figure 32. The Behavior of the Displacement Vector for SSOR/VA and Motz's Method (41-Point Pattern)

of the solutions for grids with spacing h_{k-2} , h_{k-1} , and h_k . The resulting vector of extrapolated components had spacing h_{k-2} . It was observed that an extrapolated solution for grid spacing h_{k-2} through h_k gave accuracy exceeding that of a solution for grid spacing h_{k+2} . Thus, the extrapolated solution for h_5 through h_7 had accuracy exceeding that of a solution produced with a grid of spacing 1/512. This extrapolated solution was chosen for comparison with the results from Motz's method.

Approximate values of ω_b were determined in producing the uncorrected solutions for the L-shaped region problem. They were used again for the solutions produced with Motz's method. The values of ω_b are given in Table III.

TABLE III
VALUES OF ω_b FOR THE L-SHAPED
REGION PROBLEM

h	ω_b
1/16	1.659
1/32	1.811
1/64	1.893
1/128	1.930

Evaluation of Motz's Method

The 8-point and 41-point patterns of Figure 29 were used in testing Motz's method. L-Shaped region solutions were produced for the grid spacings $h_1 = 1/16$, $h_2 = 1/32$, and $h_3 = 1/64$. The convergence

criterion for each solution required that the residual error be reduced to 10×10^{-14} .

Figure 33 shows the residual norms for solutions produced by the combination of SSOR/VA and Motz's method with the 8-point pattern. The decrease in the rate of convergence with decreasing h is apparent. The solutions for h_1 , h_2 , and h_3 required 168, 296, and 684 iterations to meet the convergence criterion. Figure 34 shows the residual behavior for solutions produced with the 41 point pattern. The solutions for h_1 , h_2 , and h_3 required 156, 316, and 688 iterations, respectively. Thus, there is little difference in the effort required to produce a solution with one method or the other. These two trials and previous trials with varying h suggest that the number of iterations required to produce a solution is $O(h^{-1})$.

In order to compare the results of Motz's method and the exact solution, an error vector is needed,

$$\vec{e} = \vec{u}_e - \vec{u}_m, \quad (6.10)$$

where \vec{u}_e is the exact solution and \vec{u}_m results from Motz's method. The norm given by equation (3.44) can be used to measure the error vectors that result from comparison. It is scaled according to the number of components.

Tables IV, V, and VI give comparisons between the exact solution and the uncorrected solutions, the 8-point Motz solutions, and the 41-point Motz solutions.

Figure 35 gives the relationship between grid spacing and the error norm for the 8-point Motz solutions, the 41 point Motz solutions, and the uncorrected solutions. The important feature is that the 8-point and 41-point Motz solutions for $h = 1/16$ have accuracy equivalent

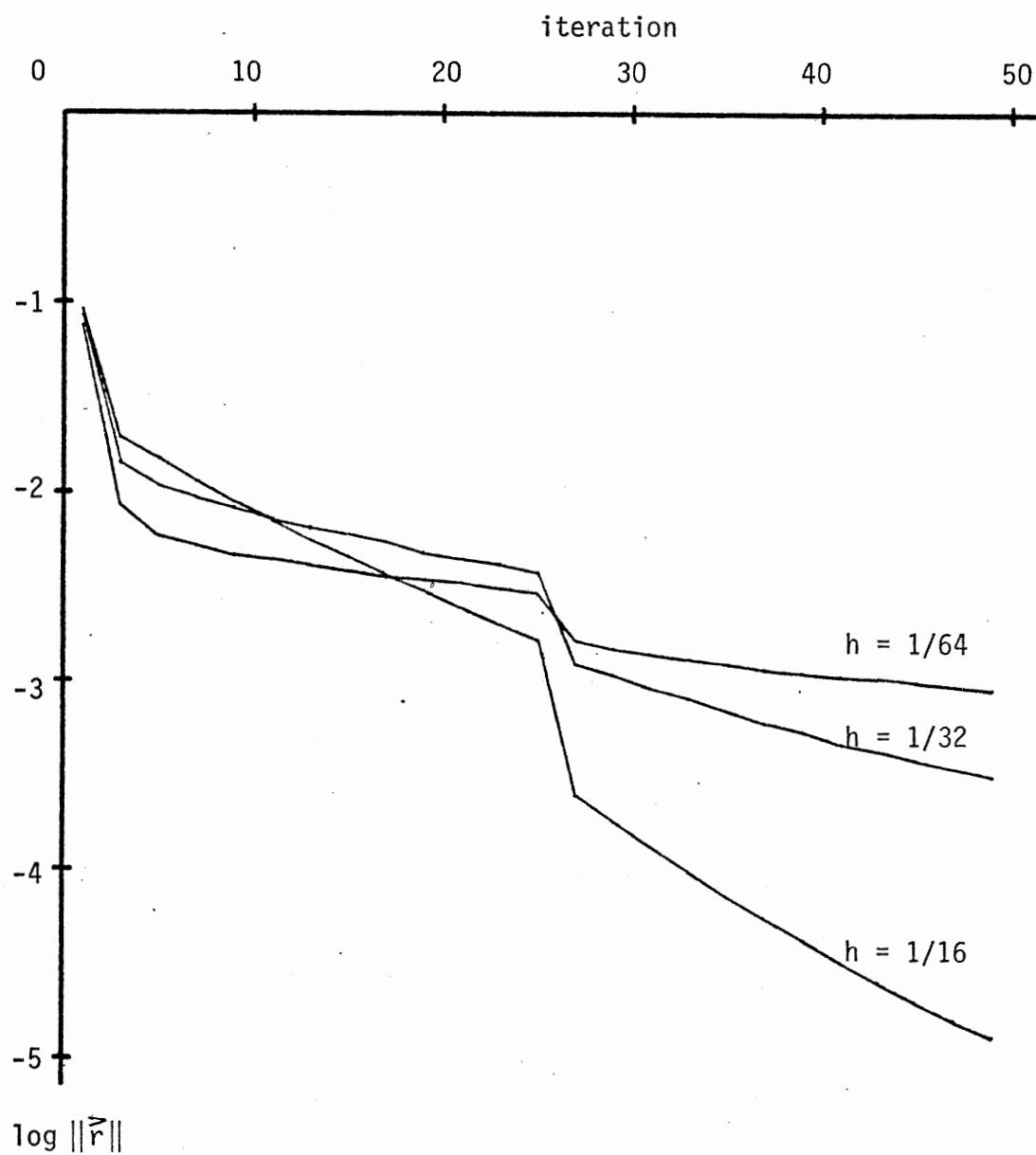


Figure 33. Behavior of Residual Norms for Solutions with 8-Point Motz and SSOR/VA

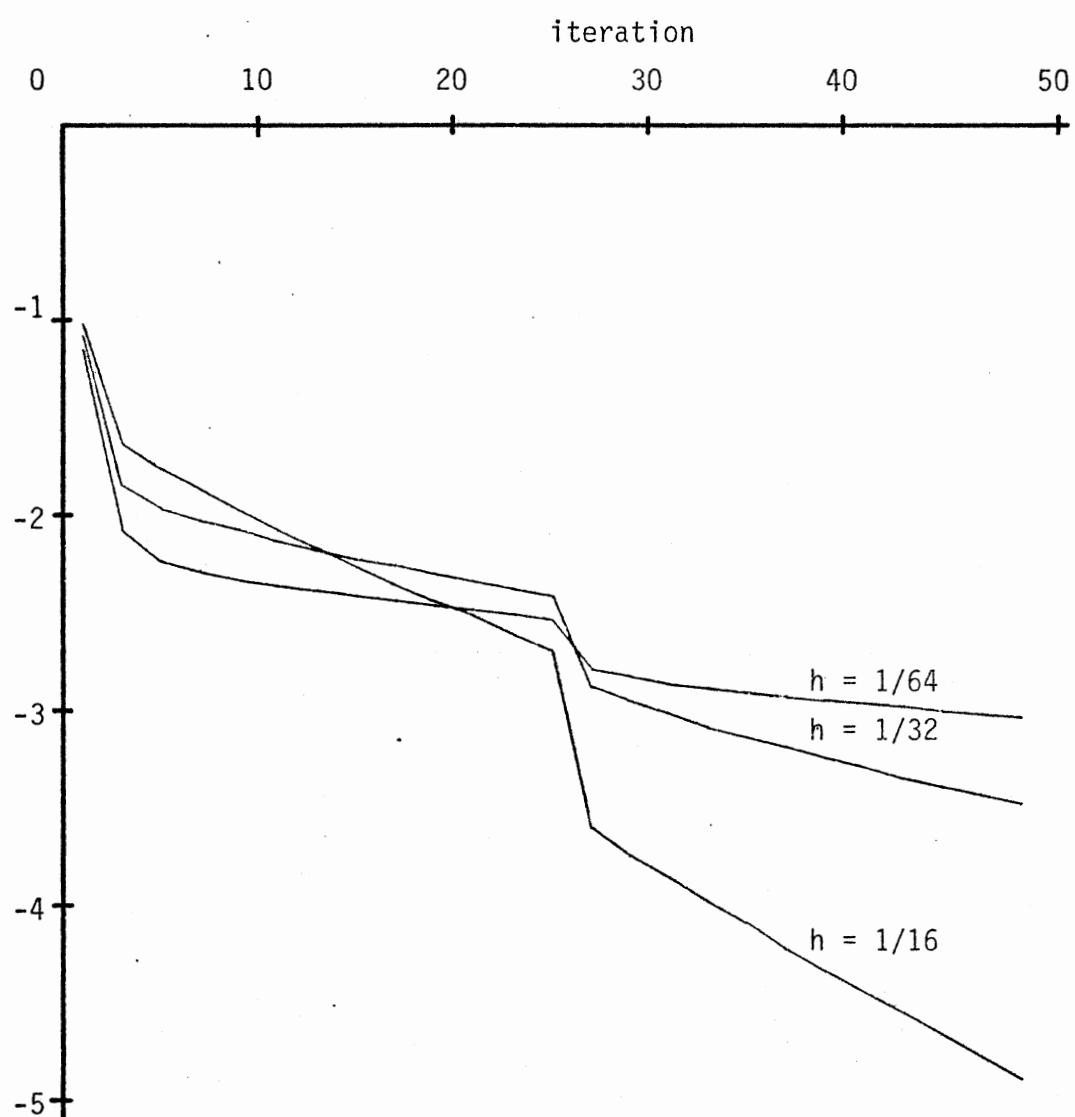


Figure 34. Behavior of Residual Norms for Solutions with 41-Point Motz and SSOR/VA

TABLE IV
COMPARISONS BETWEEN THE EXACT SOLUTION AND THE
UNCORRECTED SSOR/VA SOLUTIONS

h	$\ \tilde{e}\ $	$\max e_i $
1/8	.6510000E-2	.3082128E-1
1/16	.2646606E-2	.2058514E-1
1/32	.1049086E-2	.1373039E-1
1/64	.4161518E-3	.5684991E-2
1/128	.1653452E-3	.2343839E-2

TABLE V
COMPARISONS BETWEEN THE EXACT SOLUTION AND THE 8-POINT MOTZ
SSOR/VA SOLUTIONS

h	$\ \tilde{e}\ $	$\max e_i $
1/16	.1993717E-3	.1220212E-2
1/32	.6905748E-4	.7440496E-2
1/64	.2859288E-4	.9446983E-3

TABLE VI
COMPARISONS BETWEEN THE EXACT SOLUTION AND THE 41-POINT
MOTZ SSOR/VA SOLUTIONS

h	$\ \tilde{e}\ $	$\max e_i $
1/16	.9698017E-4	.2139818E-3
1/32	.3952888E-4	.4088687E-3
1/64	.1151425E-4	.4162266E-3

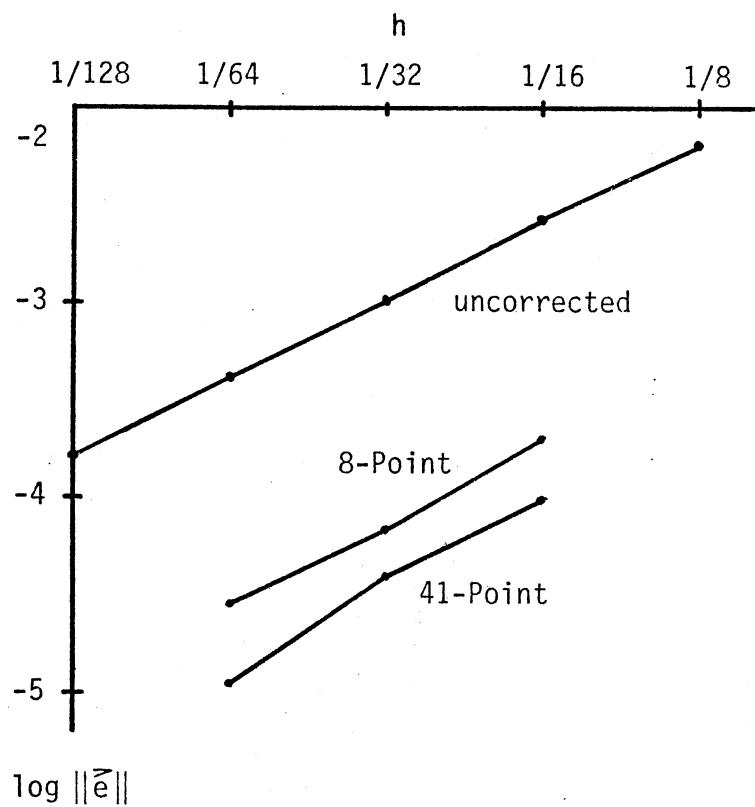


Figure 35. The Variation in the Error Norm with h for the 8-Point, 41-Point, and Uncorrected Solutions

to uncorrected solutions for $h = 1/128$ and $h = 1/256$, respectively. The solutions for $h = 1/16$ require approximately 160 iterations to converge while the solutions for $h = 1/128$ and $h = 1/256$ require 1,280 and 2,560 iterations, respectively.

Figures 36 and 37 demonstrate the effects that grid refinement and Motz's method have on the solution near the re-entrant corner. Both show the solution along the segment CD, with point D on the right of the diagram; distance is measured from D.

In Figure 36, the uncorrected solutions approach the extrapolated solution. The two lower lines are projected from points outside the range of the diagram. Note that the slopes of the lines at D increase as h decreases, but they remain finite. As noted earlier, first derivatives of the solution become undefined at D. Also, the solutions for $h = 1/16$ and $1/64$ are noticeably different than the extrapolated solution.

Figure 37 shows Motz 41-point solutions for $h = 1/16$ and $h = 1/64$. The two solutions coincide with the exact solution at corresponding grid points. Thus, Motz's method immediately eliminates much of the error due to the re-entrant corner.

The line segments connecting the solution values in Figure 36 indicate the need for a smooth interpolant near the re-entrant corner. An extremely useful feature of Motz's method is the built-in interpolating function. The solution near the re-entrant corner is of primary importance in a solution, and Motz's method provides an analytical approximation of it.

An attempt was made to determine if solutions from Motz's method had error that could be modeled by equation (6.5), and, if so, what

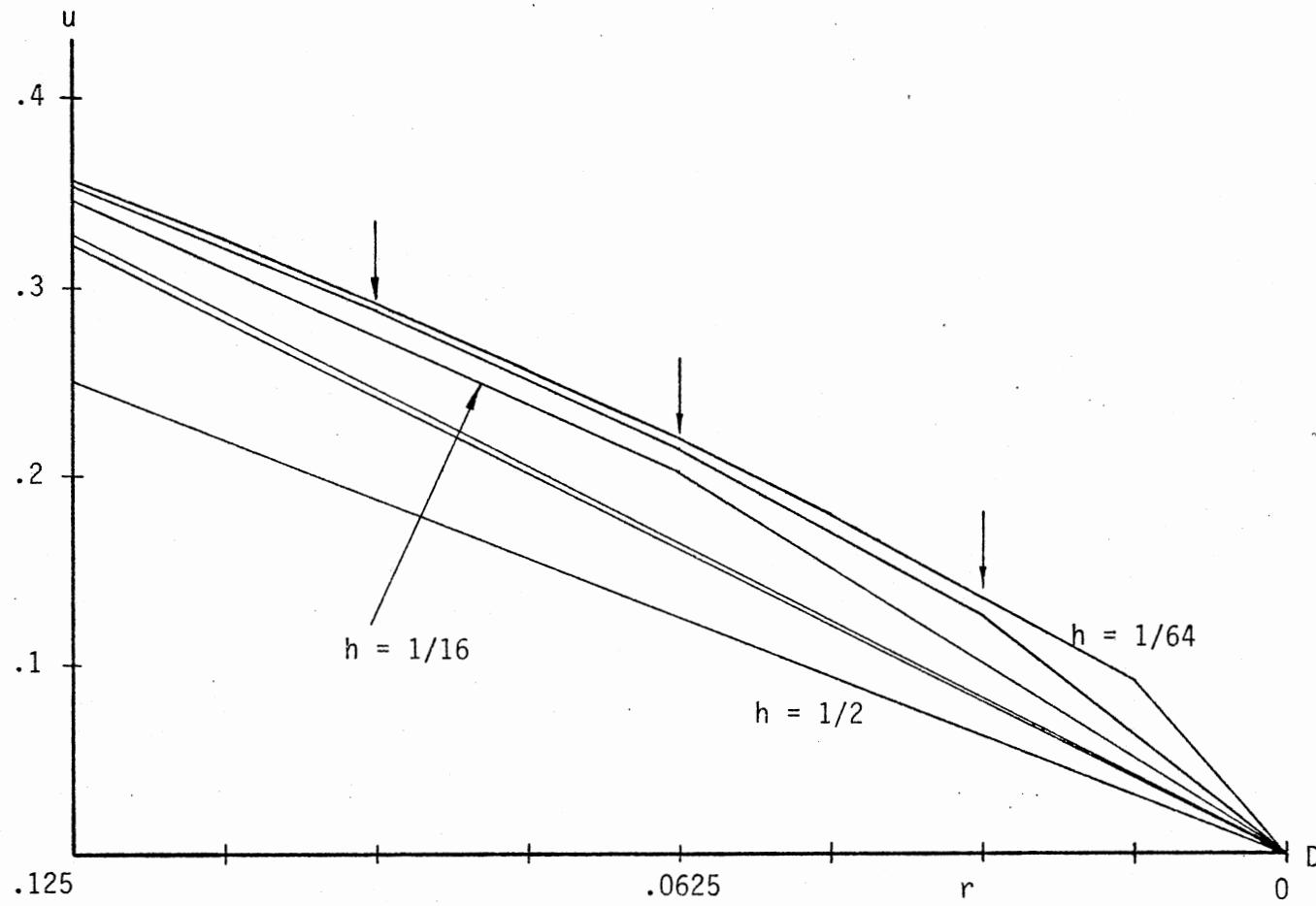


Figure 36. Uncorrected Solutions Along the Edge CD (Figure 28) for $h = 1/2$ through $h = 1/64$ (Vertical Arrows Give the Exact Solution)

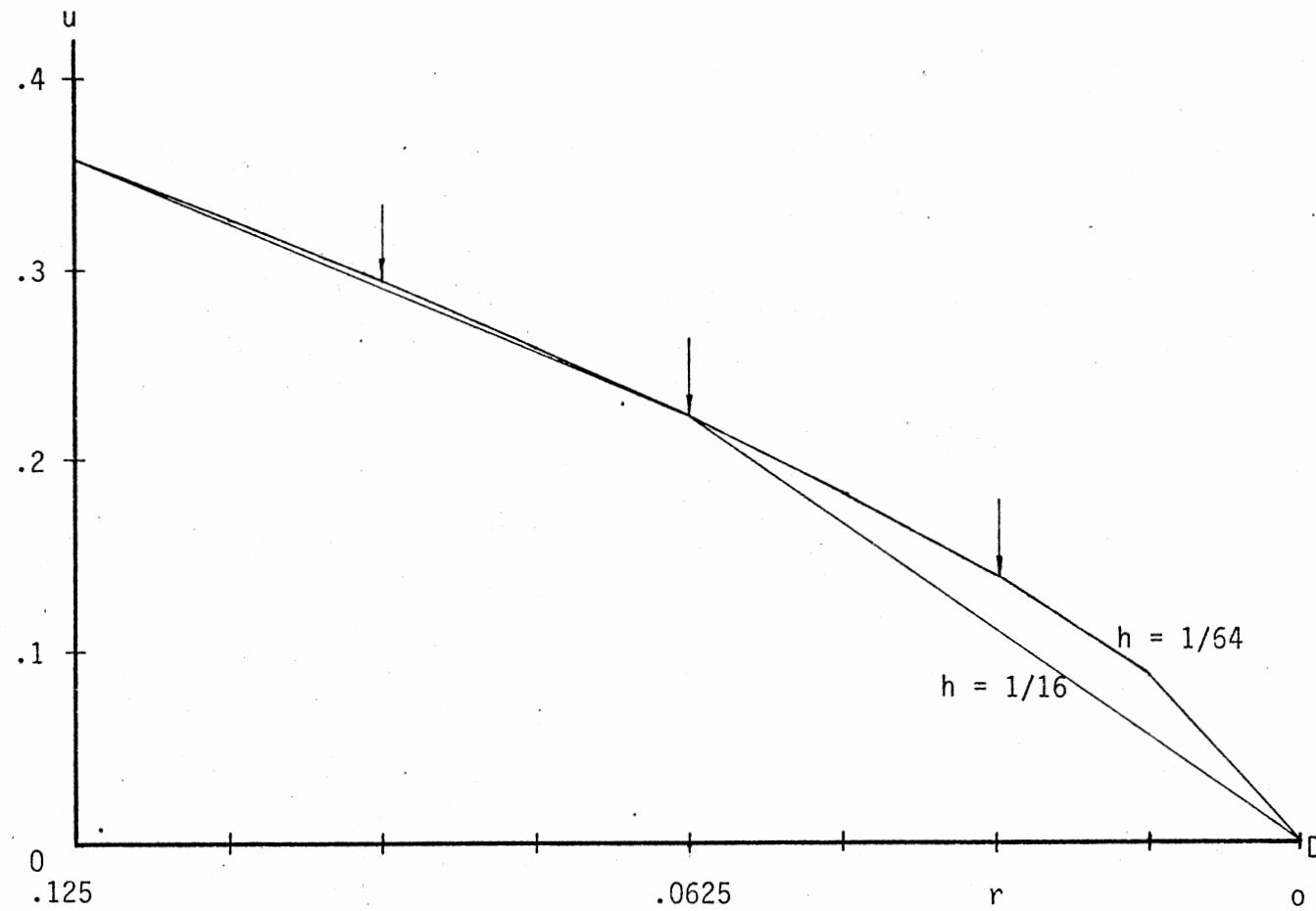


Figure 37. Motz 41-Point Solutions Along the Edge CD (Figure 28) for $h = 1/16$ and $h = 1/64$ (Vertical Arrows Indicate the Exact Solution)

the dominant power of h was. The process employed with the uncorrected solution was used with the 8-point and 41-point Motz solutions. Values for α were so widely scattered that no attempt was made to determine β . A method suggested by Reid and Walsh (23) was also used: Motz's method was used within a constant radius of the re-entrant corner for each grid spacing. This method was also unsuccessful.

The inability to determine the error behavior of Motz's method empirically is in keeping with its criticisms (30). No theory of its stability or error behavior exists. An examination of the Motz solutions shows that the $h = 1/16$ solutions agree with the exact solution to four digits; the $h = 1/64$ solutions agree to five digits. An optimum grid size seems to be $h = 1/32$. The density of solution values is adequate for interpolation, and only 110 iterations are required to reduce the residual norm to 1.0×10^{-5} . Single precision can be used throughout the solution process.

Conclusions and Suggestions for Further Study

As demonstrated, re-entrant corners seriously degrade the accuracy afforded by finite difference methods. Two of the methods used here, grid refinement and Motz's method, have been shown to reduce the effects of re-entrant corners. Each has limitations: grid refinement over the entire solution domain is not practical, and Motz's method is not well understood.

A more practical grid refinement scheme appears in Figure 19. It should be considered for study since it does not require large amounts of storage, and because it can be incorporated into multigrid formulations (5) (6) (7). Dr. D. D. Fisher of the Computing and Information

Sciences Department at Oklahoma State University has the program GRIDPACK, an adaptive multigrid routine capable of grid refinement near re-entrant corners and other types of singularities. GRIDPACK should be examined in future studies of numerical solution of PDES and re-entrant corners. It is an outgrowth of the work of Brandt and his associates (6) (7).

Motz's method appears to be well-suited to problems requiring a grid with moderate refinement. It is stable in the formulations used to date, including some that involve extrapolation. Motz's method should be examined as a means of correcting the multigrid Cycle-C process. The solution process on each grid is affected by a re-entrant corner. The routines for performing Motz's method in the program CORNER (Appendix A) could be adapted and used in the Cycle-C routines VBOUND (Appendix B).

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APPENDIXES

APPENDIX A

THE PROGRAM CORNER

The program CORNER is included here. It will solve Laplace's equation on any domain that can be represented by a uniform grid. The boundary conditions can be Dirichlet, Neumann, or mixed. At present, the Neumann conditions are restricted to vanishing normal derivatives and boundaries that are parallel to lines of the grid. The solution method can be SOR or SSOR with Aitken acceleration. The GS method is available for the determination of the relaxation parameter for SOR and SSOR; Aitken extrapolation is used to speed its determination. Also, Motz's method is included for use with re-entrant corners with internal angles of $3/2$.

The solution grid is represented in Figure 3. The rows and columns must be numbered from one, though, in the description for CORNER. The program requires a row by row description of the grid; the location and type (Neumann or Dirichlet) must be given for each boundary point on a row of the grid.

Figure 8 shows four computational molecules for use with Neumann conditions. For CORNER, an integer code must be used to identify which molecule must be used on a particular boundary segment. Clockwise from the top the codes for the molecules of Figure 8 are 4, 2, 3, and 1. The corners require special molecules; clockwise from the upper right they are 8, 6, 5, 7. Dirichlet points have the code 0. The data required for the L-shaped region follow the program listing.

Motz's method can be used at several re-entrant corners in a solution domain. The patterns of remote and series points must be given. In the data following the listing, patterns used with the L-shaped region problem are given. They are defined for a corner in the orientation of Figure 17. The location and orientation of each

re-entrant corner must be given. The four corners of a cross-shaped region give the four possible orientations. Clockwise from the upper right they are coded 2, 4, 3, 1 for CORNER.

```

C C C C
      CORNERIX,DH01Z,FORT
      DRIVER
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON /TRACE/ IN,LP,NINT,NDRUG
      COMMON /CONTRL/ OMEGA,RESMT,KSWEEP,MAXIT,KOMEGA
      INTEGER LEFT,RIGHT
      COMMON /BOUND/ XMIN,XMAX,YMIN,YMAX,H,
      MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPI
      COMMON /ATKLEN/COSTH,SMAX,SMIN,KOUNT,KPER,METHOD,
      NPREP,NPER
      IN=12
      LP=6
      NDRUG=0
      NINT=20
      COSTH=.995D0
      SMAX=.50,D0
      SMIN=0,D0
      KPER=0
      NPER=1
      METHOD=3
      CALL ITRAI
      STOP
      END
      FUNCTION F(X,Y,H10L)
      IMPLICIT REAL*8 (A-H,O-Z)
      IF(X,L1,H10L)=1,000
      IF(Y,L1,H10L)=-1,000
      RETURN
      END
      SUBROUTINE ITRAI
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON /TRACE/ IN,LP,NINT,NDRUG
      COMMON /CONTRL/ OMEGA,RESMT,KSWEEP,MAXIT,KOMEGA
      COMMON /STORE/ V(65,65),V(65,65)
      INTEGER LEFT,RIGHT
      COMMON /BOUND/ XMIN,XMAX,YMIN,YMAX,H,
      MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPI
      INTEGER SP1,SRW,SC01,EPI,IROW,ECOL
      COMMON /SNG/ SMAT(50,15),FMAT(15,15),EXPVAL(10,15),SCALF(15),
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C
C      CALL DECOMP(EMAXR,NL,EMAT,COND,EPVT,SCALE,B)          000387900
C
C      WRITE(LP,30)COND,(SCALE(J),J=1,NF)                  000388000
C      CONDP1=COND+1.                                       000388100
C
C      IF( CONDP1.NE.COND) GO TO 900
C          WRITE(LP,60)
C              STOP
C
C      RETURN
C
C      FORMAT(10X,12I5)
C      FORMAT(11X,'CONDITION',E20.16//11X,'SCALE',E120.16/
C             '(16X,E120.16)')
C      $      FORMAT(11X,'*** MATRIX IS SINGULAR TO WORKING PRECISION ***') 000389600
C      FORMAT(//6X,'-- SNGLOC --'//11X,'NSING',I5)           000395000
C      FORMAT(11X,'SING NO., ROW,COL,SING TYPE',I4)          000397000
C      FORMAT(10X,'ROW, COL')                                000398000
C      FORMAT(10X,'SING NO.')                               000399000
C      FORMAT(18X,'ROW,ECOL')                                000400000
C      FORMAT(//4IX,'SMAT')
C      FORMAT(//4IX,'TMAT')
C
C      END
C      SUBROUTINE SHAPE
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      INTEGER SPAIR,SPATC,EPAIR,EPATC
C      COMMON /PATR/ NS,SPAIR(50),SPATC(50),NF,EPPAIR(15),EPATC(15)
C      COMMON /TRACE/ IN,LP,NINT,NDBUG
C
C      READ(IN,20)NS
C      READ(IN,20)(SPAIR(J),J=1,NS)
C      READ(IN,20)(SPATC(J),J=1,NS)
C      WRITE(LP,50)NS,(SPATC(J),SPAIR(J),J=1,NS)
C
C      READ(IN,20)NF
C      READ(IN,20)(EPPAIR(J),J=1,NF)
C      READ(IN,20)(EPATC(J),J=1,NF)
C
C      WRITE(LP,60)NF,(EPPAIR(J),EPATC(J),J=1,NF)
C      RETURN
C
C      FORMAT(10X,12I5)
C      FORMAT(//6X,'-- SHAPE --'//11X,'REPLACEMENT PATTERN ',I5,
C             ' POINTS')/(16X,215))
C      $      FORMAT(//11X,'EXTREME POINT PATTERN ',I5,' POINTS')/
C             '(16X,215))                                     000412000
C
C      END
C
C      SUBROUTINE ROTATE(IX,IY,NEWX,NEWY,NPT,LOCX,LOCY,STYP) 000413000
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON /TRACE/ IN,LP,NINT,NDBUG
C      DIMENSION IX(NPT),IY(NPT),NEWX(NPT),NEWY(NPT)          000414000
C
C      INTEGER STYP,ROTAIE
C      DIMENSION ROTAIE(4,2,2)
C      DATA ROTAIE/-1.0,0.0,1.0,-1.0,0.0,-1.0,0.0,1.0/        00044600
C
C      MX=ROTAIE(STYP,1,1)
C      MY=ROTAIE(STYP,1,2)
C      NX=ROTAIE(STYP,2,1)
C      NY=ROTAIE(STYP,2,2)                                     00044500
C
C      DO 400 J=1,NPT
C          NEWX(J)=((IX(J)*MX+IY(J)*NY)+LOCX
C                     -((IX(J)*NX+IY(J)*NY)+LOCY)
C
C          $      WRITE(LP,20)NEWY(J),NEWX(J)
C              FORMAT(16X,215)
C
C      CONTINUE
C
C      RETURN
C
C      END
C
C      SUBROUTINE POLAR(IX,IY,THETA,RADIUS,NPT,II)          00045500
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON /TRACE/ IN,LP,NINT,NDBUG
C      DIMENSION IX(NPT),IY(NPT),THETA(NPT),RADIUS(NPT)       00045600
C
C      IWOP1=8.00*DATAN(1.000)                                00045700
C
C      DO 200 J=1,NPT
C          NX=IX(J)
C          NY=IY(J)
C
C          THETA(J)=0.000
C          RADIUS(J)=0.000
C
C          IF(NX.EQ.0 .AND. NY.EQ.0)GO TO 200
C              THETA(J)=DATAN2(DFLOAT(NY),DFLOAT(NX))
C              RADIUS(J)=DSQR1(DFLOAT((NX**2)+(NY**2)))
C              IF(THETA(J).LT.0.000)THETA(J)=IWOP1+THETA(J)
C
C      200 CONTINUE
C
C      IF(NDBUG.GT.50)WRITE(LP,50)(J,IX(J),IY(J),RADIUS(J),THETA(J),
C                           J=1,NPT)
C
C      RETURN
C
C      50      FORMAT(//6X,'-- POLAR --'//21X,'J,IX,IY,RADIUS,THETA'/
C                           '(11X,315,2E24.16))                                00049900
C
C      END
C
C      SUBROUTINE MATCAL(XMAT,MAXR,MAXC,NR,NC,XRAD,XTHETA)  00050000
C
C

```

```

C IMPLICIT REAL*8 (A-H,O-Z)
COMMON /TRACE/IN,LP,NINT,NDEBUG
DIMENSION XMAT(MAXR,MAXC),XRAD(NR),XTHETA(NR)
INTEGER LEFT,RIGHT
COMMON /BOUND/ XMIN,XMAX,YMIN,YMAX,H,
      MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPT
C $ G=2,DO/3,00
DO 600 J=1,NR
C
      THETA=XTHETA(J)
      RAD=XRAD(J)
C
      KMIN=1
      IF(RAD.GT.,500)GO TO 480
C
      KMIN=2
      XMA1(J,1)=1.000
C 480   RAD=RAD**C
C
      DO 500 K=KMIN,NC
C
      N=K-1
      XMA1(J,K)=(RAD**N)*DCOS(C*DFOAT(N)*THETA)
C 500   CONTINUE
      WRITE(LP,20)J,(XMA1(J,K),K=1,NC)
C 600   CONTINUE
C
      RETURN
C
      FORMAT(/4X,'ROW',14,4E24.16/(11X,4E24.16))
C
      END

C SUBROUTINE INIT
C
C IMPLICIT REAL*8 (A-H,O-Z)
COMMON /STORT/U(65,65),V(65,65)
INTEGER LEFT,RIGHT
COMMON /BOUND/ XMIN,XMAX,YMIN,YMAX,H,
      MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPT
C $ H101=H*.500
C
DO 200 J=1,NROW
C
      Y=YMIN+DFOAT(J-1)*H
      KMIN=LEFT(J)
      KMAX=RIGHT(J)
C
      DO 180 K=KMIN,KMAX
C
      X=XMIN+DFOAT(K-1)*H
      U(J,K)=F(X,Y,H101)
C 180   CONTINUE
C
      CONTINUE
C
      END

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```

      RETURN
      END

      SUBROUTINE DECOMP (NDIM, N, A, COND, IPVT, SCAL1, WORK)
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      DIMENSION A(NDIM,NDIM),WORK(N),IPVT(N),SCALE(N)
C
C      DECOMPOSES A REAL MATRIX BY GAUSSIAN ELIMINATION,
C      AND ESTIMATES THE CONDITION OF THE MATRIX.
C
C      -COMPUTER METHODS FOR MATHEMATICAL COMPUTATIONS-, BY G. E. FORSYTHE,
C      M. A. MALCOLM, AND C. B. MOLER (PRENTICE-HALL, 1977)
C
C      USE SUBROUTINE SOLVE TO COMPUTE SOLUTIONS TO LINEAR SYSTEMS.
C
C      INPUT..
C
C      NDIM = DECLARED ROW DIMENSION OF THE ARRAY CONTAINING A
C      N   = ORDER OF THE MATRIX
C      A   = MATRIX TO BE TRIANGULARIZED
C
C      OUTPUT..
C
C      A CONTAINS AN UPPER TRIANGULAR MATRIX U AND A PERMUTED
C      VERSION OF A LOWER TRIANGULAR MATRIX L-L SO THAT
C      (PERMUTATION MATRIX) * A = L * U
C
C      COND = AN ESTIMATE OF THE CONDITION OF A.
C      FOR THE LINEAR SYSTEM A*X = B, CHANGES IN A AND B
C      MAY CAUSE CHANGES COND TIMES AS LARGE IN X.
C      IF COND+1.0 .EQ. COND, A IS SINGULAR TO WORKING
C      PRECISION. COND IS SET TO 1.0E+32 IF EXACT
C      SINGULARITY IS DETECTED.
C
C      IPVT   = THE PIVOT VECTOR
C      IPVT(K) = THE INDEX OF THE K-TH PIVOT ROW
C      IPVT(N) = (-1)**(NUMBER OF INTERCHANGES)
C
C      WORK SPACE. THE VECTOR WORK MUST BE DECLARED AND INCLUDED
C      IN THE CALL. ITS INPUT CONTENTS ARE IGNORED,
C      ITS OUTPUT CONTENTS ARE USUALLY UNIMPORTANT.
C
C      THE DETERMINANT OF A CAN BE OBTAINED ON OUTPUT BY
C      DET(A) = IPVT(N) * A(1,1) * A(2,2) * ... * A(N,N) .
C
C
C      XABS(Z)=DABS(Z)
C      XT1OAT(IZ)=D1OAT(IZ)

      PERFORM COLUMN SCALING

      CALL CSCALE(NDIM,N,A,SCALE)

      IPVT(N)=1
      IF(N .EQ. 1) GO TO 150
      NM1=N-1
      COMPUTE THE 1-NORM OF A .

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      DO 20 J=1,N          00063900
      I=0,000               00064000
      DO 10 I=1,N           00064100
      I=I+XABS(A(I,J))     00064200
      IF(I,L,ANORM) ANORM=I 00064300
20    CONTINUE              00064400
C      DO GAUSSIAN ELIMINATION WITH PARTIAL
C      PIVOTING.            00064500
C      DO 70 K=1,NM1         00064600
C      KPI=K+1
C      FIND THE PIVOT.      00064700
C      H-K                 00064800
C      DO 30 L=KPI,N         00064900
C      I=(XABS(A(L,K))) .GT. XABS(A(M,K)) M=I 00065000
C      CONTINUE              00065100
C      IPVI(K)=M             00065200
C      IF(M,NL,K) IPVI(N)=IPVI(N)             00065300
C      I=A(H,K)               00065400
C      A(H,K)=A(K,K)           00065500
C      A(K,K)=I                00065600
C      SKIP THE ELIMINATION STEP IF PIVOT IS ZERO. 00065700
C      IF(I,EQ.0.000) GO TO 70 00065800
C      COMPUTE THE MULTIPLIERS. 00065900
C      DO 40 I=KPI,N           00066000
C      A(I,K)=A(I,K)/I        00066100
C      INTERCHANGE AND ELIMINATE BY COLUMNS. 00066200
C      DO 60 J=KPI,N           00066300
C      I=A(M,J)               00066400
C      A(M,J)=A(K,J)           00066500
C      A(K,J)=I                00066600
C      IF(I,EQ.0.000) GO TO 60 00066700
C      DO 50 I=KPI,N           00066800
C      A(I,J)=A(I,J)+A(I,K)*I 00066900
C      CONTINUE              00067000
70    CONTINUE              00067100
C      COND = (1-NORM OF A)*(AN ESTIMATE OF THE 1-NORM OF A-INV)
C      THE ESTIMATE IS OBTAINED BY ONE STEP OF INVERSE ITERATION FOR THE
C      SMALL SINGULAR VECTOR. THIS INVOLVES SOLVING TWO SYSTEMS
C      OF EQUATIONS, (A-TRANSPOSE)*Y = E AND A*Z = Y WHERE E
C      IS A VECTOR OF +1 OR -1 COMPONENTS CHOSEN TO CAUSE GROWTH IN Y.
C      ESTIMATE = (1-NORM OF Z)/(1-NORM OF Y) 00067200
C      SOLVE (A-TRANSPOSE)*Y = E . 00067300
C      DO 100 K=1,N           00067400
C      I=0,000                 00067500
C      IF(K,EQ.1) GO TO 90     00067600
C      KPI=K+1                 00067700
C      DO 80 I=1,KM1           00067800
C      I=I+A(I,K)*WORK(I)      00067900
80    EK=1.0                  00068000
90    EK=-1.0                 00068100
      IF(I,I,0.000) EK=-1.0  00068200
      IF(A(K,K),EQ.0.000) GO TO 160 00068300
100   WORK(K)=-(EK+1)/A(K,K) 00068400
      DO 120 K=1,NM1           00068500
C      K=N-KB                 00068600
C      I=0,000                 00068700
C      KPI=K+1                 00068800
C      DO 110 I=KPI,N           00068900
C      I=I+A(I,K)*WORK(I)      00069000
      WORK(K)=1                 00069100
      H=IPVI(K)                 00069200
      IF(M,IQ,K) GO TO 120     00069300
      I=WORK(H)                 00069400
      WORK(H)=0                 00069500
      WORK(K)=1                 00069600
      H=IPVI(K)                 00069700
      IF(M,IQ,K) GO TO 120     00069800
      I=WORK(H)                 00069900
      WORK(H)=0                 00070000
      WORK(K)=1                 00070100
      H=IPVI(K)                 00070200
      IF(M,IQ,K) GO TO 120     00070300
      I=WORK(H)                 00070400
      WORK(H)=0                 00070500
      WORK(K)=T                 00070600
      CONTINUE                  00070700
      YNORM=0.000               00070800
      DO 130 I=1,N           00070900
      YNORM=YNORM+XABS(WORK(I)) 00071000
      CALL SOLVE (NDIM,N,A,WORK,IPVI,SCALE,0) 00071100
      ZNORM=0.000               00071200
      DO 140 I=1,N           00071300
      ZNORM=ZNORM+XABS(WORK(I)) 00071400
      ESTIMATE THE CONDITION. 00071500
      COND=ANORM*ZNORM/YNORM 00071600
      IF(COND.LT.1.0) COND=1.0 00071700
      RETURN                   00071800
      1-BY-1 CASE.. 00071900
      150 COND=1.000             00072000
      IF(A(1,1).NE.0.000) RETURN 00072100
      EXACT SINGULARITY.. 00072200
      160 COND=1.0032             00072300
      RETURN                   00072400
      END                      00072500
      SUBROUTINE CSCALE(NDIM,N,A,SCALF) 00072600
      IMPLICIT REAL*8 (A-H,O-Z) 00072700
      DIMENSION A(NDIM:NDIM),SCALF(N) 00072800
      COMPUTE COLUMN NORMS 00072900
      DO 400 JCOL=1,N           00073000
      ASUM=0.00 00073100
      DO 200 JROW=1,N           00073200
      ASUM=ASUM+ABS(A(JROW,JCOL)) 00073300
      200 CONTINUE                00073400
      300 SFACI=DFLOAT(N)/ASUM 00073500
      SCALF(JCOL)=SFACI 00073600
      DO 300 JROW=1,N           00073700
      A(JROW,JCOL)=A(JROW,JCOL)*SFACI 00073800
      300 CONTINUE                00073900
      400 RETURN                  00074000
      END                      00074100
      SUBROUTINE SOLVE (NDIM,N,A,B,IPVI,SCALE,MODE) 00074200
      IMPLICIT REAL*8 (A-H,O-Z) 00074300

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C      DIMENSION A(NDIM,NDIM),B(N),IPVI(N),SCALE(N)          00076900
C      SOLVES A LINEAR SYSTEM, A*X = B.                      00077000
C      DO NOT SOLVE THE SYSTEM IF DECOMP HAS DETECTED SINGULARITY. 00077200
C      -COMPUTER METHODS FOR MATHEMATICAL COMPUTATIONS-, BY G. E. FORSYTHE, 00077300
C          B. A. MALCOLM, AND C. B. MOLER (PRENTICE-HALL, 1977) 00077500
C      INPUT..                                                 00077600
C      NDIM = DECLARED ROW DIMENSION OF ARRAY CONTAINING A 00077700
C      N = ORDER OF MATRIX                                     00077800
C      A = TRIANGULARIZED MATRIX OBTAINED FROM SUBROUTINE DECOMP 00077900
C      B = RIGHT HAND SIDE VECTOR                            00078000
C      IPVI = PIVOT VECTOR OBTAINED FROM DECOMP              00078100
C      OUTPUT..                                                00078200
C      B = SOLUTION VECTOR, X                                00078300
C      DO THE FORWARD ELIMINATION.                           00078400
C      IF(N .EQ. 1) GO TO 50
C      DO 20 K=1,NM1                                         00078500
C          KPK=K+1
C          M=IPVI(K)
C          L=NM1
C          D(M)=B(K)
C          B(K)=1
C          DO 10 I=K+1,N
C              B(I)=B(I)+A(I,K)*T
C 10      CONTINUE
C      NOW DO THE BACK SUBSTITUTION.
C      DO 40 KB=1,NM1
C          KMI=N-KB
C          K=KMI+1
C          B(K)=B(K)/A(K,K)
C          L=B(K)
C          DO 30 I=L,NM1
C              B(I)=B(I)+A(I,K)*T
C 30      CONTINUE
C      40      CONTINUE
C      50      B(I)=B(I)/A(I,I)
C      IF(NODE.LT.1)GO TO 999
C      CORRECT FOR COLUMN SCALING
C      DO 100 J=1,N
C          B(J)=B(J)*SCALE(J)
C 100      CONTINUE
C      999      RETURN
C      END
C
C      SURROUNIQUE EXSAVE
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON /TRACE/IN,LP,NINT,NDEBUG
C
C      INTEGER SPAIR,SPATC,EPPAIR,EPATC
C      COMMON /PATTIN/ NS,SPAIR(50),SPATC(50),NE,EPPAIR(15),EPATC(15)
C      INTEGER SPT,STORE,SCOL,EP1,EROW,ECOL
C      COMMON /STORL/ V(65,65),V(65,65)
C      INTEGER SNG,SMAT(50,15),EMAT(15,15),EXPVAL(10,15),SCALE(15),
C              B(15),SROW(100),SCOL(100),EROW(100),ECOL(100),SPT(10),
C              EP1(10),IPVI(15),NSING
C      INTEGER LEFT,RIGHT
C      COMMON /BOUND/ XMIN,XMAX,YMIN,YMAX,H,
C                     MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPI
C      INTEGER ROW,COL
C      IF(NSING.LE.1)RETURN
C      DO 200 J=1,NSING
C          EPOS=EP1(J)
C          DO 100 K=1,NE
C              ROW=EROW(EPOS)
C              COL=ECOL(EPOS)
C              EXPVAL(J,K)=0(ROW,COL)
C              EPOS=EPOS+1
C 100      CONTINUE
C 200      CONTINUE
C      IF(NDEBUG.LE.100)GO TO 300
C      DO 280 J=1,NSING
C          WRITE(LP,50)J,(EXPVAL(J,K),K=1,NE)
C 280      CONTINUE
C      300      RETURN
C      FORMAT('//6X,'-- EXSAVE --'/9X,'SING',40X,'EXI. PIS.'/
C             6X,15,4E24.16/(11X,4(24.16)))
C 50      FORMAT('EXSAVE')
C      END
C
C      SUBROUTINE SNGCAL
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON /TRACE/IN,LP,NINT,NDEBUG
C      INTEGER SPAIR,SPATC,EPPAIR,EPATC
C      COMMON /PATTIN/ NS,SPAIR(50),SPATC(50),NE,EPPAIR(15),EPATC(15)
C      INTEGER ROW,COL,SPOS
C      COMMON /STORE/ V(65,65),V(65,65)
C      INTEGER SPT,STORE,SCOL,EP1,EROW,ECOL
C      COMMON /SNG/ SMAT(50,15),EMAT(15,15),EXPVAL(10,15),SCALE(15),
C                  B(15),SROW(100),SCOL(100),EROW(100),ECOL(100),SPT(10),
C                  EP1(10),IPVI(15),NSING
C      INTEGER LEFT,RIGHT
C      COMMON /BOUND/ XMIN,XMAX,YMIN,YMAX,H,
C                     MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPI
C      DIMENSION USAVE(50)
C      INTEGER EMAXR
C      DATA EMAXR/15/

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C      IF(NSING.LT.1)RETURN          00089900
C      IF(NDEBUG.GT.20)WRITE(LP,00)    00090000
C      DO 400 J=1,NSING             00090200
C          IF(NDEBUG.GT.20)WRITE(LP,50)J 00090400
C          DO 200 K=1,NE              00090500
C              B(K)=EXPVAL(J,K)        00090600
C          CONTINUE                   00091000
C          CALL SOLVI(EMAXR,NF,EMAT,B,IPVT,SCALE,1) 00091100
C          REPLACE EACH POINT ABOUT THE SINGULARITY WITH ITS 00091200
C          SERIES REPRESENTATION 00091500
C          SPOS SPT(J)                00091600
C          RESSUM=0.000               00091700
C          DO 300 K=1,NS              00091800
C              USUM=0.000             00091900
C              ROW SROW(SPOS)          00092000
C              COL SCOL(SPOS)          00092300
C              SPOS=SPOS+1             00092400
C              DO 280 L=1,NI              00092500
C                  USUM=USUM+D(L)*SMAT(K,L) 00092600
C              CONTINUE                   00092700
C              RESSUM=RESSUM+DABS(U(ROW,COL)-USUM) 00092800
C              U(ROW,COL)=USUM           00092900
C              USAVI(K)=USUM            00093100
C          CONTINUE                   00093200
C          RESAVE=RESSUM/DFLOAT(NS)    00093300
C          RESLOG=-1.0D70              00093400
C          IF(RESAVE.GT.0.0D0)RESLOG=DILOG10(RESAVE) 00093500
C          WRITE(LP,70)J,RESAVE,RESLOG 00093600
C          IF(NDEBUG.GT.20)WRITE(LP,60)(USAVID(K),K=1,NS) 00093700
C          CONTINUE                   00093800
C          RESAVE=RESSUM/DFLOAT(NS)    00093900
C          RESLOG=-1.0D70              00094000
C          IF(RESAVE.GT.0.0D0)RESLOG=DILOG10(RESAVE) 00094100
C          WRITE(LP,70)J,RESAVE,RESLOG 00094200
C          IF(NDEBUG.GT.20)WRITE(LP,60)(USAVID(K),K=1,NS) 00094300
C          CONTINUE                   00094400
C          RETURN                     00094500
C          IF(NDEBUG.GT.20)WRITE(LP,60)(USAVID(K),K=1,NS) 00094600
C          RETURN                     00094700
C          IF(NDEBUG.GT.20)WRITE(LP,60)(USAVID(K),K=1,NS) 00094800
C          RETURN                     00094900
C          IF(NDEBUG.GT.20)WRITE(LP,60)(USAVID(K),K=1,NS) 00095000
C          FORMAT(//1X,'SING NO.',15)   00095100
C          FORMAT(//6X,'-- SNGCAL --//)  00095200
C          FORMAT(2X,'SNG. PTS.',4E24.16/(11X,4E24.16)) 00095300
C          FORMAT(11X,'SNG. PTS.-NO,AVE,LOG',15,2E24.16) 00095400
C          END                         00095500
C          END                         00095600
C          END                         00095700
C          END                         00095800
C          END                         00095900
C          SUBROUTINE SWEEP(KSWEEP,OMEGA,RESAVE,RESLOG) 00096000
C          IMPLICIT REAL*8 (A-H,O-Z)    00096100
C                                         00096200
C                                         00096300

COMMON /TRACE/IN,LP,NINI,NDEBUG          00096400
INTEGER BPIOC,BPOINI                 00096500
COMMON /STORE/ U(65,65),V(65,65)       00096600
INTEGER SPT,SROW,SCOL,LP1,EROW,ECOL    00096700
COMMON /SNG/ SH(150,15),EMAT(15,15),EXPVAL(10,15),SCALE(15), 00096800
$      D(15),SROW(100),SCOL(100),EROW(100),ECOL(100),SPT(10), 00096900
$      EPT(10),IPV(15),NSING              00097000
INTEGER LEFT,RIGHT                   00097100
COMMON /ROUND/ XMIN,XMAX,YMIN,YMAX,H, 00097200
$      MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPI 00097300
00097400
DIMENSION MDIR(8,4)                   00097500
DATA MDIR/1,1,-1,1,-1,-1,-1,1,1,-1,-1, 00097600
$      1,-1,-1,-1,1,-1,1,-1,1,1,-1,1,-1/ 00097700
INTEGER EFLAG,DFLAG                 00097800
DATA EFLAG,DFLAG/-2,0/               00097900
IF(NDEBUG.GT.100)WRITE(LP,50)          00098000
NSWEEP=1                             00098100
IF(KSWEEP.NE.1)NSWEEP=2               00098200
00098300
*****CALL EXSAVE***** 00098400
DO 600 N=1,NSWEEP 00098500
SAVE THE VALUES OF THE EXTREME POINTS 00098600
CALL EXSAVE 00098700
CALL SNGCAL 00098800
INC=1 00098900
J=1 00099000
IF(N.EQ.2)GO TO 180 00099100
INC=-1 00099200
J=NROW 00099300
WRITE(LP,80)RESAVE,RESLOG 00099400
00100000
00100100
00100200
00100300
00100400
00100500
00100600
00100700
00100800
00100900
00101000
00101100
00101200
00101300
00101400
00101500
00101600
00101700
00101800
00101900
00102000
00102100
00102200
00102300
00102400
00102500
00102600
00102700
180  RESUM=0.000 00100000
RESMAX=0.000 00100100
DO 400 JCOUNT=1,NROW 00100200
KMAX=RIGHT(J) 00100300
KMIN=LEFT(J) 00100400
K=KMIN 00100500
IF(N.EQ.2)K=KMAX 00100600
DO 300 KCOUNT=KMIN,KMAX 00100700
USAVID=U(J,K) 00100800
HOLYP=MAP(J,K) 00100900
IF(HOLYP.LE.EFLAG)GO TO 200 00101000
BOUNDARY POINT OR SPECIAL POINT 00101100
IF(HOLYP.LE.EFLAG)GO TO 280 00101200
JC=J+MDIR(HOLYP,1) 00101300
JB=J+MDIR(HOLYP,2) 00101400

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C   KU=KINDIR(MOLTYP,3)          00102800
C   KR=KINDIR(MOLTYP,4)          00102900
C
C   UNEW=.25D0*(U(JI,K)+U(JB,K)+U(J,KI)+U(J,KR)) 00103000
C   GO TO 240                   00103100
C
C   NORMAL MOLECULE             00103200
C
C   200   UNEW=.25D0*(U(J+1,K)+U(J-1,K)+U(J,K+1)+U(J,K-1)) 00103300
C
C   240   RES=UNEW-USAVE          00103400
C   RESUM=RESUM+DABS(RES)       00103500
C
C   280   K=K+INC                00103600
C
C   300   CONTINUE                00103700
C
C   J=J+INC                    00103800
C
C   400   CONTINUE                00103900
C
C   RESAVE=RESUM/DELOAD(NP1)    00104000
C   RESLOG=LOG10(RESAVE)       00104100
C
C   600   CONTINUE                00104200
C
C   *****CALL *SNGCAL*****      00104300
C
C   RESUM=RESUM/DELOAD(NP1)    00104400
C   RESLOG=LOG10(RESAVE)       00104500
C
C   600   CONTINUE                00104600
C
C   *****CALL *SNGCAL*****      00104700
C
C   RETURN                      00104800
C
C   50   FORMAT(/6X,'-- SWEEP --') 00104900
C   80   FORMAT(/6X,'RES.= AVE, LOG, MAX,R,C',5X,3F24.16,2I5,5X,
C   S   '(FORWARD SWEEP)')        00105000
C
C   END                         00105100
C
C   SUBROUTINE VATIK (METHOD,NPLP,NPER,
C   KOUNT,KPER, COSTH, SHAX, SHIN, COSIN, SRAW, S) 00105200
C
C   IMPLICIT REAL*8 (A-H,O-Z)
C   COMMON /STORE/ U(65,65),V(65,65) 00105300
C   INTEGER L111,L1111
C   COMMON ZBOUND/ XMIN,XMAX,YMIN,YMAX,II,
C   MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPT 00105400
C   DIMENSION X(4500),TA(4500),IB(4500) 00105500
C   EQUIVALENCE (X(1),U(1,1)) 00105600
C   COMMON /TRAC1/IN,LP,NINI,NBUG 00105700
C   INTEGER CPIMIN,CPIMAX 00105800
C   COMMON /SIAP/ KTOP(65),KBOT(65),CPIMIN(65),CPIMAX(65) 00105900
C
C   VATIK 3.1      A.N.S.I. STANDARD BASIC FORTRAN      JULY 1981 00106000
C   SUBROUTINE VATIK PERFORMS DYNAMIC VECTOR AITKEN EXTRAPOLATION, 00106100
C
C   IN AN ATTEMPT TO ACCELERATE THE CONVERGENCE OF A GIVEN SLOWLY 00109300
C   CONVERGENT VECTOR ITERATION SCHEME. 00109400
C   J. P. CHANDLER, COMPUTER SCIENCE DEPT., OKLAHOMA STATE UNIVERSITY 00109500
C   00109600
C   A. JENNINGS, J. INST.MATH.APPLIC. 8 (1971) 99-110 00109700
C   E. F. DOYLE AND A. JENNINGS, INT.J.NUM.METH.ENG. 7 (1971) 232-235 00109800
C   H. K. CHENG AND M. M. JATZ, PAGES 101-122 IN 00109900
C   -PADE APPROXIMANTS METHOD AND ITS APPLICATIONS TO MECHANICS-, 00110000
C   EDITED BY H. CADANNE (SPRINGER-VIRAG 1976) 00110100
C   E. GELKELER, MATHEMATICS OF COMPUTATION 26 (1972) 421-436 00110200
C   C. BREZINSKI AND A. G. RIEU, MATH. OF COMP. 28 (1974) 731-741 00110300
C   C. BREZINSKI, COMPUTING 14 (1975) 205-211 00110400
C   P. WYNN, MATH. OF COMP. 16 (1962) 301-322 00110500
C   00110600
C   INPUT QUANTITIES.... X(*),NX,METHOD,NPLP,NPER, 00110700
C   (KOUNT,KPER). COSTH,SHAX,SHIN 00110800
C   OUTPUT QUANTITIES.... COSIN,SRAW,S,X(*) 00110900
C   COUNTERS..... KOUNT,KPER 00111000
C   SCRATCH ARRAYS..... TA(*),IB(*) 00111100
C   00111200
C   X(*) -- INPUT VECTOR ITERATE. ALSO RETURNS THE EXTRAPOLATED 00111300
C   OUTPUT VECTOR. 00111400
C   NX -- NUMBER OF COMPONENTS IN THE VECTORS X(*), TA(*), 00111500
C   AND IB(*) 00111600
C   TA(*) -- SCRATCH VECTOR OF NX COMPONENTS 00111700
C   IB(*) -- SCRATCH VECTOR OF NX COMPONENTS 00111800
C   METHOD -- =1 TO USE THE -FDA- METHOD OF JENNINGS, 00111900
C   =2 TO USE THE -SDM- METHOD (THIS IS THE FIRST STAGE 00112000
C   OF THE VECTOR EPSILON ALGORITHM OF WYNN), 00112100
C   =3 TO USE AN -SDM- (SECOND DIFFERENCE NORM) METHOD, 00112200
C   =4 TO USE A -DDDN- (DIFFERENCE OF FIRST DIFFERENCE 00112300
C   NORMS) METHOD 00112400
C   (SUGGESTION ... TRY METHOD 3, AND PERHAPS 2 AND 4) 00112500
C   NPLP -- NUMBER OF ITERATES DISCARDED BEFORE EACH 00112600
C   EXTRAPOLATION BEGINS 00112700
C   (SUGGESTION ... SET NPLP=0, OR PERHAPS 1 OR 2) 00112800
C   NPER -- =1 IF THE X(*) ITERATES ARE THOUGHT TO BE CONVERGING 00112900
C   ALONG A LINE, EITHER MONOTONICALLY OR 00113000
C   ALTERNATING IN DIRECTION, 00113100
C   =2 IF THE X(*) ITERATES ARE THOUGHT TO BE ZIGZAGGING 00113200
C   WITH A PERIOD OF TWO ITERATIONS, ETC. 00113300
C   (USE THE SMALLEST VALUE OF NPER SUCH THAT COSTH 00113400
C   APPROACHES +1 OR -1. NPER=2 GIVES THE 00113500
C   -SQUARED- EXTRAPOLATION METHODS OF JENNINGS.) 00113600
C   KOUNT -- ITERATION COUNTER 00113700
C   KPER -- COUNTER FOR ZIGZAGGING 00113800
C   COSTH -- EXTRAPOLATION IS DONE ONLY IF THE MAGNITUDE OF 00113900
C   COSTH (SEE BELOW) IS GE. COSTH 00114000
C   (SUGGESTION ... SEE COSTH,.95 OR LARGER) 00114100
C   SHAX -- UPPER LIMIT ON THE EXTRAPOLATION FACTOR (SEE BELOW) 00114200
C   SHIN -- LOWER LIMIT ON THE EXTRAPOLATION FACTOR 00114300
C   COSTH -- RETURNS THE COSINE OF THE ANGLE BETWEEN THE TWO 00114400
C   FIRST DIFFERENCE VECTORS 00114500
C   SRAW -- RETURNS THE RAW VALUE OF THE EXTRAPOLATION FACTOR S, 00114600
C   BEFORE COSTH, SHAX, AND SHIN ARE APPLIED 00114700
C   S -- RETURNS THE VALUE OF S ACTUALLY USED 00114800
C   00114900
C   THE USER CALLS VATIK REPEATEDLY. THE X(*) VECTORS ARE SUCCESSIVE 00115000
C   VECTORS FROM SOME ITERATION SCHEME HAVING ROUGHLY LINEAR CONVERGENCE. 00115100
C   THE COUNTERS KOUNT AND KPER MUST BE SET TO ZERO BEFORE THE FIRST 00115200
C   CALL TO VATIK FOR A GIVEN PROBLEM, AND NOT CHANGED UNTIL THE NEXT 00115300
C   CALL. PROBLEM IS TO BE STARTED, EXCEPT AS NOTED BELOW. 00115400
C   ON CERTAIN CALLS TO VATIK, THE VECTOR X(*) WILL BE EXTRAPOLATED 00115500
C   INSIDE OF VATIK TO AN ESTIMATE OF THE LIMIT VECTOR TOWARD WHICH 00115600
C   THE ITERATES X(*) HAVE BEEN CONVERGING. THIS IS DONE BY ADDING 00115700

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C TO XI(*) A SCALAR MULTIPLE S OF THE RESULTANT CHANGE IN X(*)  

C DURING THE PREVIOUS NPER ITERATIONS.  

C IF AN ITERATION DIVERGES, IT IS PROBABLY BEST TO FORCE CONVERGENCE  

C BY APPLYING UNDER-RELAXATION TO IT, AND THEN APPLY VALIK TO THIS  

C CONVERGENT ITERATION.  

C  

C MONOTONIC BEHAVIOR OF THE ITERATION IS ASSOCIATED WITH VALUES OF  

C COSIN THAT ARE LT. ZERO, AND OSCILLATORY BEHAVIOR WITH VALUES THAT  

C ARE LT. ZERO. IN ADDITION, WHEN THE VALUE OF COSIN IS NEAR 1.0  

C OR NEAR -1.0, THE VALUE OF S INDICATES THE BEHAVIOR OF SETS OF  

C NPER CONSECUTIVE ITERATIONS, AS FOLLOWS....  

C       S .LT. -1.0           MONOTONIC DIVERGENCE           00116900  

C       -1.0 .LT. S .LT. -0.5   OSCILLATORY DIVERGENCE    00117000  

C       S .EQ. -0.5           OSCILLATION                  00117100  

C       -0.5 .LT. S .LT. 0.0   OSCILLATORY CONVERGENCE    00117200  

C       0.0 .LT. S            MONOTONIC CONVERGENCE        00117300  

C WHEN COSIN IS NEAR 1.0 OR -1.0, THE FIRST DIFFERENCE VECTOR FOR  

C SETS OF NPER CONSECUTIVE ITERATIONS IS APPROXIMATELY MULTIPLIED  

C BY S/(S+1) ON EACH SUCCESSIVE SET.  

C  

C THE PURPOSE OF SMAX AND SMIN IS TO PREVENT A WILD VALUE OF S FROM  

C CAUSING AN ABSURD EXTRAPOLATION. FOR A SEQUENCE THAT IS KNOWN  

C TO BE NONCONVERGENT, THE USER SHOULD PROBABLY SET SMIN=-0.5.  

C SMAX MIGHT BE SET TO 10., OR 20., OR 50., OR ...  

C  

C TO IMPLEMENT DOUBLE PRECISION ACCUMULATION OF INNER PRODUCTS,  

C ACTIVATE THE FIRST DOUBLE PRECISION STATEMENT BELOW.  

C TO IMPLEMENT COMPLETE DOUBLE PRECISION ARITHMETIC, ACTIVATE ALSO  

C THE SECOND DOUBLE PRECISION STATEMENT AND THE DOUBLE PRECISION  

C FORM OF THE STATEMENT FUNCTIONS BELOW.  

C  

C       DOUBLE PRECISION DOT,DXLSQ,DXSQ,DXDDX,DXDSQ,DXOLD,DX,DX  

C       DOUBLE PRECISION X,IA,IB,COSTH,SMAX,SMIN,COSIN,SHAW,S,  

C       X = ARG,QABS,DABS,QSQR1,DSQRT,RZTRO,  

C       X = TEMP,SXI,SQ,SXSQ,XDXD,SIXSQ,SXOLD,SX,BINOM  

C  

C       QABS(ARG)-ABS(ARG)                           00118900  

C       QSQR1(ARG)-SQRT(ARG)                        00119000  

C       QABS(ARG)-DAHS(ARG)                        00119100  

C       QSQR1(ARG)-DSQRT(ARG)                      00119200  

C  

C       RZTRO=0.00                                    00120000  

C       COSIN=RZTRO                                  00120100  

C       SHAW=RZERO                                    00120200  

C       S=RZERO  

C       11(KOUNT-NPREP)10,40,20                   00120400  

10 KOUNT=KOUNT+1  

GO TO 350  

20 11(KPER-(NPER-1))30,40,40                   00120700  

30 KPER=KPER+1  

GO TO 350  

40 KPER=0  

KOUNT=KOUNT+1  

11(KOUNT-(NPREP+2))290,330,50                00121300  

C  

C                                                        ACCUMULATE ALL INNER PRODUCTS.    00121400  

50 DOT=RZERO                                        00121500  

DXLSQ=RZTRO                                        00121600  

DXSQ=RZTRO                                        00121700  

DXDDX=RZTRO                                        00121800  

DXDSQ=RZTRO                                        00121900  

DO 60 I=1,NCOL  

C  

C       JMAX=CPIMAX(1)                             00122100

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C JMIN=CPIMIN(1)
C DO 60 J=JMIN,JMAX
C
DXOLD=IB(J)-IA(J)
DX=X(J)-IB(J)
DDX=DX-DXOLD
D01=D01+DXOL D*DDX
DXI SQ=DXI SQ+DXOL D*DDXOLD
DXSQ=DXSQ+DX*DDX
DXDDX=DXDDX+DX*DDX
DDXSQ=DDXSQ+DX*DDX
C
C 60 CONTINUE
SXI SQ=DXI SQ
SXSQ=DXSQ
SXDDX=DXDDX
DDXSQ=DDXSQ
C COMPUTE COSIN.
C
SXOL D=QSORT( SXI SQ)
SX=QSORT( SXSQ)
DENOM=SXOL D*SX
IF(DENOM)310,310,70
70 TEMP=D01
COSIN=TEMP/DENOM
C SELECT THE METHOD AND COMPUTE SRAW.
C
IF(METHOD=2)90,110,80
80 IF(METHOD=4)130,170,170
C
90 IF(SXDDX)100,310,100
100 SRAW=-SXSQ/SXDDX
GO TO 210
C
110 IF(SDXSQ)120,310,120
120 SRAW=-SDDX/SDXSQ
GO TO 210
C
130 IF(SDXSQ)140,310,140
140 SRAW=SX/QSORT( SDXSQ)
150 IF(COSIN)160,150,150
150 IF(SXOLD-SX)160,210,210
160 SRAW=-SRAW
GO TO 210
C
C METHOD=1 ...
S = -(DX,DX)/(DDX,DX)
C
170 IF(COSIN)180,190,190
180 SXOLD=SXOLD
190 DENOM=SX-SXOLD
IF(DENOM)200,310,200
200 SRAW=-SX/DENOM
C
C 210 IF(QABS(COSIN)-COSTH)310,220,220
C
C ILSI FOR SUFFICIENT COLLINEARITY.
C
C 220 S=SRAW
IF(S-SMAX)240,240,230
230 S=SMAX
240 IF(S-SMIN)250,260,260
250 S=SMIN
260 IF(S)270,310,270
C
C EXTRAPOLATE.
C
C 270 DO 280 L=1,NCOL
C

```

```

      JMAX=CPIMAX(L)
      JMIN=CPIMIN(L)
C      DO 280 J=JMIN,JMAX
C          X(J)=X(J)+S*(X(J)-TB(J))
C 280      CONTINUE
C          KOUNT=1
C          SAVE X(*).
C 290      DO 300 I=1,NCOL
C              JMAX=CPIMAX(L)
C              JMIN=CPIMIN(L)
C              DO 300 J=JMIN,JMAX
C                  TA(J)=X(J)
C 300      CONTINUE
C          GO TO 350      SHIFT THE STORED ITERATES BACK ONE PLACE.
C 310      DO 320 I=1,NCOL
C              JMAX=CPIMAX(L)
C              JMIN=CPIMIN(L)
C              DO 320 J=JMIN,JMAX
C                  TA(J)=TB(J)
C 320      CONTINUE
C          SAVE X(*).
C 330      DO 340 I=1,NCOL
C              JMAX=CPIMAX(L)
C              JMIN=CPIMIN(L)
C              DO 340 J=JMIN,JMAX
C                  TB(J)=X(J)
C 340      CONTINUE
C          RETURN
C          END
C          SUBROUTINE PLOTB
C          IMPLICIT REAL*8 (A-H,O-Z)
C          COMMON /TRACE/ IN,LP,NINT,NDEBUG
C          INTEGER IINT,RIGHT
C          COMMON /BOUND/ XMIN,XMAX,YMIN,YMAX,H,
C                         MAP(65,65),LEFT(101),RIGHT(101),NROW,NCOL,NPT
$          00128800
$          00128900
$          00129000
$          00129100
$          00129200
$          00129300
$          00129400
$          00129500
$          00129600
$          00129700
$          00129800
$          00129900
$          00130000
$          00130100
$          00130200
$          00130300
$          00130400
$          00130500
$          00130600
$          00130700
$          00130800
$          00130900
$          00131000
$          00131100
$          00131200
$          00131300
$          00131400
$          00131500
$          00131600
$          00131700
$          00131800
$          00131900
$          00132000
$          00132100
$          00132200
$          00132300
$          00132400
$          00132500
$          00132600
$          00132700
$          00132800
$          00132900
$          00133000
$          00133100
$          00133200
$          00133300
$          00133400
$          00133500
$          00133600
$          00133700
$          00133800
$          00133900
$          00134000
$          00134100
$          00134200
$          00134300
$          00134400
$          00134500
$          00134600
$          00134700
$          00134800
$          00134900
$          00135000
$          00135100
$          00135200
$          00135300
$          00135400
$          00135500
$          00135600
$          00135700
$          00135800
$          00135900
$          00136000
$          00136100
$          00136200
$          00136300
$          00136400
$          00136500
$          00136600
$          00136700
$          00136800
$          00136900
$          00136A00
$          00136B00
$          00136C00
$          00136D00
$          00136E00
$          00136F00
$          00136G00
$          00136H00
$          00136I00
$          00136J00
$          00136K00
$          00136L00
$          00136M00
$          00136N00
$          00136O00
$          00136P00
$          00136Q00
$          00136R00
$          00136S00
$          00136T00
$          00136U00
$          00136V00
$          00136W00
$          00136X00
$          00136Y00
$          00136Z00
$          00137000
$          00137100
$          00137200
$          00137300
$          00137400
$          00137500
$          00137600
$          00137700
$          00137800
$          00137900
$          00138000
$          00138100
$          00138200
$          00138300
$          00138400
$          00138500
$          00138600
$          00138700
$          00138800
$          00138900
$          00139000
$          00139100
$          00139200
$          00139300
$          00139400
$          00139500
$          00139600
$          00139700
$          00139800
$          00139900
$          00140000
$          00140100
$          00140200
$          00140300
$          00140400
$          00140500
$          00140600
$          00140700
$          00140800
$          00140900
$          00141000
$          00141100
$          00141200
$          00141300
$          00141400
$          00141500
$          00141600
$          00141700

```

```

      IF(UVAL .GT. UMAX)UMAX=UVAL
      IF(UVAL .LT. UMIN)UMIN=UVAL
100      CONTINUE
C
C
      WRITE(LP,10)UMAX,UMIN,NINT
      UDF1=UMAX-UMIN
      USCALE=DFLOAT(NINT)/UDF1
      J=NROW
C
      DO 400 I=1,NROW
C
        KMIN=LEFT(I,J)
        KMAX=RIGHT(I,J)
C
        DO 300 K=KMIN,KMAX
C
          NCHAR=IDINT((U(J,K)-UMIN)*USCALE)+1
          IF(NCHAR.GT.NINT)NCHAR=NINT
          LINE(K)=ICHAR(NCHAR)
300      CONTINUE
C
        IF(NCOL.GT.25)WRITE(LP,20)(IBUNK,M-1,KMIN),
           (11NL(K),K-KMIN,KMAX)
        IF(NCOL.LE.25)WRITE(LP,21)(IBUNK,M-1,KMIN),
           (11NL(K),K-KMIN,KMAX)
        J=J-1
C
400      CONTINUE
C
        UINC=UDF1/DFLOAT(NINT)
        U2=UMIN
        WRITE(LP,25)
C
        DO 600 J=1,NINT
C
          U1=U2
          FORMAT(1X,25A2)
          U2=UMIN+UINC*DFLOAT(J)
C
          WRITE(LP,30)ICHAR(J),U1,U2
600      CONTINUE
C
        RETURN
C
        FORMAT(//6X,'-- PLOT --'/1IX,'UMAX,UMIN,NINT',2E15.7,110/)
        FORMAT(1X,120A1)
        FORMAT(//21X,'CHARACTER RANGES'//)
        FORMAT(11X,A1,2E15.7,' 10 ',E15.7)
        END
C
C
C
      SUBROUTINE RESULT(MINR,MAXR)
C
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON /STORE/ U(65,65),V(65,65)
      COMMON /TRACE/ IN,LP,NINT,NDBUG
      INTEGER LEFT,RIGHT

```

```

      00141800
      00141900
      00142000
      00142100
      00142200
      00142300
      00142400
      00142500
      00142600
      00142700
      00142800
      00142900
      00143000
      00143100
      00143200
      00143300
      00143400
      00143500
      00143600
      00143700
      00143800
      00143900
      00144000
      00144100
      00144200
      00144210
      00144220
      00144230
      00144300
      00144400
      00144500
      00144600
      00144700
      00144800
      00144900
      00145000
      00145100
      00145200
      00145300
      00145400
      00145410
      00145500
      00145600
      00145700
      00145800
      00145900
      00146000
      00146100
      00146200
      00146300
      00146400
      00146500
      00146600
      00146700
      00146800
      00146900
      00147000
      00147100
      00147200
      00147300
      00147400
      00147500
      00147600
      00147700
      00147800
S      COMMON /BOUND/ XMIN,XMAX,YMIN,YMAX,H,
      DATA LHEX/1/
      WRITE(LP,10)NROW,NCOL,XMIN,XMAX,YMIN,YMAX,H
      WRITE(LHFX,12)NROW,NCOL
C
      DO 200 J=MINR,MAXR
C
        Y=YMIN+H*DFLOAT(J-1)
        KMIN=LEFT(J)
        KMAX=RIGHT(J)
C
        XLEFT=XMIN+H*DFLOAT(KMIN-1)
        XRIGHT=XMIN+H*DFLOAT(KMAX-1)
C
        WRITE(LP,20)J,Y,KMIN,XLEFT,KMAX,XRIGHT,
           (U(J,K),K-KMIN,KMAX)
        WRITE(LHFX,30)(U(J,K),K-KMIN,KMAX)
200      CONTINUE
C
      RETURN
C
      FORMAT(//1IX,'ROW',14.4X,'Y=',E15.7,10X,'COLS',14.4,'( X=',
         E15.7,1) 10,14,( X,E15.7,1)"/
      20      FORMAT(11X,4E24.16)
      10      FORMAT(11H,5X,-- RLSULT --'/1IX,'ROWS,COLS',215/
           11X,'KMIN,XMAX,YMIN,YMAX,H',5E15.7//)
      12      FORMAT(2Z8)
      30      FORMAT(5Z16)
C
      END

```

	MAX1 *****																MAX2 *****																		
KSWI EP	2																	00000100	N SING	1	00006200														
KOMEGA	0																	00000200	NR	-1	00006300														
OMEGA	1.65900																	00000300	COL/XCOOR	-1	00006400														
NPRUP	10																	00000400	ROW/YCOOR	-1	00006500														
NIROW, NCOL	17 17																	00000500	NE	6	00006600														
XMIN, XMAX	0.0	1.0															00000600	COL /XCOOR	0	00006700															
YMIN, YMAX	0.0	1.0															00000700	ROW/YCOOR	-2	00006800															
ROW1	9 17 9																00000800	R, C, TYPE	9 9 3	00006900															
LOC	9 10 11 12 13 14 15 16 17																00000900			00007000															
TYPE	0 0 0 0 0 0 0 0 0																00001000																		
ROW2-8	9 17 2																00001100																		
LOC	9 17																00001200																		
TYPE	1 2																00001300																		
ROW2-8	9 17 2																00001400																		
LOC	9 17																00001500																		
TYPE	1 2																00001600																		
ROW2-8	9 17 2																00001700																		
LOC	9 17																00001800																		
TYPE	1 2																00001900																		
ROW2-8	9 17 2																00002000																		
LOC	9 17																00002100																		
TYPE	1 2																00002200																		
ROW2-8	9 17 2																00002300																		
LOC	9 17																00002400																		
TYPE	1 2																00002500																		
LOC	9 17																00002600																		
TYPE	1 2																00002700																		
ROW2-8	9 17 2																00002800																		
LOC	9 17																00002900																		
TYPE	1 2																00003000																		
ROW2-8	9 17 2																00003100																		
LOC	9 17																00003200																		
TYPE	1 2																00003300																		
ROW 9	1 17 9 4 5 6 7 8 17																00003400																		
LOC	1 2 3 3 3 3 3 3 3																00003500																		
TYPE	0 3 3 3 3 3 3 3 3																00003600																		
ROW10-16	1 17 2																00003700																		
LOC	1 17																00003800																		
TYPE	0 2																00003900																		
ROW10-16	1 17 2																00004000																		
LOC	1 17																00004100																		
TYPE	0 2																00004200																		
ROW10-16	1 17 2																00004300																		
LOC	1 17																00004400																		
TYPE	0 2																00004500																		
ROW10-16	1 17 2																00004600																		
LOC	1 17																00004700																		
TYPE	0 2																00004800																		
LOC	1 17																00004900																		
TYPE	0 2																00005000																		
ROW10-16	1 17 2																00005100																		
LOC	1 17																00005200																		
TYPE	0 2																00005300																		
ROW10-16	1 17 2																00005400																		
LOC	1 17																00005500																		
TYPE	0 2																00005600																		
ROW 17	1 17 17 6 5 6 7 8 9 10 11 12																00005700																		
LOC	1 2 3 4 5 6 7 8 9 10 11 12																00005800																		
TYPE	0 4 4 4 4 4 4 4 4 4 4 4																00005900																		
	4 4 4 4 4 4 4 4 4 4 4 4																00006000																		
																	00006100																		

APPENDIX B

THE PROGRAM VBOUND

The program VBOUND is included here. It can be used to solve Poisson's equation on a solution domain with an irregular shape. A uniform grid is used to represent the irregular shape. The boundary conditions can be of Neumann (vanishing normal derivative) or Dirichlet type. The shape of the solution domain is specified in a manner similar to that used in the program CORNER; rows and columns of the grid are numbered from zero. Boundary conditions are specified in the same manner as for CORNER. In selecting fine and coarse grids, each must fully represent the shape of the solution domain.


```

C          100 MANY LEVELS OR IMPROPER CONFIGURATION OF GRIDS      00025600
C          100      NLVEL=K                                         00025700
C          NLVEL=(IP,20)NLVEL                                         00025800
C          20      WRITE((IP,20)NLVEL)                                00025900
C          FORMAT(IX,'// INCONSISTENT REQUEST FOR LEVELS -',15,     00026000
C          '$ USED #/#')                                         00026100
C          GO TO 240                                         00026200
C
C          160      NROW(J)=NROW(J-1)/2+1                           00026300
C          NCOL(J)=NCOL(J-1)/2+1                           00026400
C          IVAL(J)=XDTF/FL0A1(NCOL(J)-1)                     00026500
C          200      CONTINUE                                         00026600
C
C          240      CONTINUE                                         00026700
C
C          PRODUCE POINTERS TO THE LEFT AND RIGHT ELEMENTS OF    00026800
C          EACH ROW FOR EACH GRID.                               00026900
C
C          280      CONTINUE                                         00027000
C
C          320      CONTINUE                                         00027100
C
C          360      PRODUCE POINTERS TO THE LEFT AND RIGHT ELEMENTS OF    00027200
C          EACH ROW FOR EACH GRID.                               00027300
C
C          400      CONTINUE                                         00027400
C
C          440      CONTINUE                                         00027500
C
C          480      CONTINUE                                         00027600
C
C          520      CONTINUE                                         00027700
C
C          560      CONTINUE                                         00027800
C
C          600      CONTINUE                                         00027900
C
C          640      CONTINUE                                         00028000
C
C          680      CONTINUE                                         00028100
C
C          720      UP1=1                                         00028200
C
C          760      KMIN=1                                         00028300
C
C          800      KMAX=NROW(1)                                 00028400
C
C          840      SIVL(1)=SPT                                         00028500
C
C          880      DO 400 KROW=KMIN,KMAX
C                  LLOC(KROW)=UP1
C                  UP1=UP1+(RIGHT(KROW)-LEFT(KROW))
C                  RLOC(KROW)=UP1
C                  UP1=UP1+1
C
C          920      CONTINUE                                         00028600
C
C          960      SPT=UP1+1                                         00028700
C
C          1000      POINTERS FOR THE COARSER GRIDS                00028800
C
C          1040      DO 1000 LEVEL=2,NLEVEL
C                  SIVL(LEVEL)=SPT
C                  KMIN=SIVL(LEVEL-1)
C                  KMAX=SIVL(LEVEL)-1
C
C          1080      DO 600 K=KMIN,KMAX,2
C                  LEFT(SPT)=LEFT(K)/2
C                  RIGHT(SPT)=RIGHT(K)/2
C                  LLOC(SPT)=UP1
C                  UP1=UP1+RIGHT(SPT)-LEFT(SPT)
C                  RLOC(SPT)=UP1
C                  UP1=UP1+1
C                  SPT=SPT+1
C
C          1120      CONTINUE                                         00028900
C
C          1160      CONTINUE                                         00029000
C
C          1200      DETERMINE THE NUMBER OF POINTS IN EACH GRID      00029100
C
C          1240      DO 1100 LEVEL=1,NLEVEL
C
C          1280      LMIN=SIVL(LEVEL)                                00029200
C
C          1320      LMAX=SIVL(LEVEL+1)-1                            00029300
C
C          1360      NPOINT(LEVEL)=(RLOC(LMAX)-LLOC(LMIN))+1        00029400
C
C          1400      CONTINUE                                         00029500
C
C          1440      FOR THE LEFT-HAND ELEMENT OF EACH ROW OF A GRID PRODUCE    00029600
C          POINTERS TO THE NORTH AND SOUTH ELEMENTS OF THE    00029700
C          LAPLACIAN (CENTERED ABOUT THAT ELEMENT)           00029800
C
C          1480      SPT=SPT-1                                         00029900
C
C          1520      DO 1400 LEVEL=1,NLEVEL
C
C          1560      GENERATE POINTERS FOR GRID LEVEL                 00030000
C
C          1600      LMIN=SIVL(LEVEL)+1                                00030100
C
C          1640      LMAX=SIVL(LEVEL+1)-2                            00030200
C
C          1680      GIVE NULL VALUES TO POINTERS THAT WOULD POINT TO    00030300
C          ROWS OUTSIDE THE CURRENT GRID                      00030400
C
C          1720      SLOC(LMIN-1)=-1                                00030500
C
C          1760      NLOC(LMAX+1)=-1                                00030600
C
C          1800      GENERATE THE REMAINING POINTERS FOR GRID LEVEL      00030700
C
C          1840      NLOC(LMIN-1)=LLOC(LMIN)+(LEFT(LMIN-1)-LEFT(LMIN))  00030800
C
C          1880      SLOC(LMAX+1)=LLOC(LMAX)+(LEFT(LMAX+1)-LEFT(LMAX))  00030900
C
C          1920      DO 1200 LPT=LMIN,LMAX
C
C          1960      SLOC(LPT)=LLOC(LPT-1)+(LEFT(LPT-1)-LEFT(LPT-1))  00031000
C
C          2000      NLOC(LPT)=LLOC(LPT+1)+(LEFT(LPT)-LEFT(LPT+1))   00031100
C
C          2040      1200      CONTINUE                                         00031200
C
C          2080      SET UP THE LISTS OF BOUNDARY POINT LOCATION AND TYPE    00031300
C          FOR EACH GRID                                         00031400
C
C          2120      BLVL(1)=1                                         00031500
C
C          2160      BROW(1)=1                                         00031600
C
C          2200      DETERMINE WHERE THE ROWS ARE IN THE LIST OF    00031700
C          BOUNDARY LOCATIONS FOR THE FINEST GRID            00031800
C
C          2240      JMAX=NROW(1)+1                                00031900
C
C          2280      BPT=1                                         00032000
C
C          2320      BLOC(NBNDP1+1)=-1                            00032100
C
C          2360      BPREV=BLOC(1)+1                            00032200
C
C          2400      DO 1800 JROW=1,JMAX
C
C          2440      CONTINUE                                         00032300
C
C          2480      IF(BPREV.GE.BLOC(BPT))GO TO 1600
C
C          2520      1500      CONTINUE                                         00032400
C
C          2560      1500      CONTINUE                                         00032500
C
C          2600      1500      CONTINUE                                         00032600
C
C          2640      1500      CONTINUE                                         00032700
C
C          2680      1500      CONTINUE                                         00032800
C
C          2720      1500      CONTINUE                                         00032900
C
C          2760      1500      CONTINUE                                         00033000
C
C          2800      1500      CONTINUE                                         00033100
C
C          2840      1500      CONTINUE                                         00033200
C
C          2880      1500      CONTINUE                                         00033300
C
C          2920      1500      CONTINUE                                         00033400
C
C          2960      1500      CONTINUE                                         00033500
C
C          3000      1500      CONTINUE                                         00033600
C
C          3040      1500      CONTINUE                                         00033700
C
C          3080      1500      CONTINUE                                         00033800
C
C          3120      1500      CONTINUE                                         00033900
C
C          3160      1500      CONTINUE                                         00034000
C
C          3200      1500      CONTINUE                                         00034100
C
C          3240      1500      CONTINUE                                         00034200
C
C          3280      1500      CONTINUE                                         00034300
C
C          3320      1500      CONTINUE                                         00034400
C
C          3360      1500      CONTINUE                                         00034500
C
C          3400      1500      CONTINUE                                         00034600
C
C          3440      1500      CONTINUE                                         00034700
C
C          3480      1500      CONTINUE                                         00034800
C
C          3520      1500      CONTINUE                                         00034900
C
C          3560      1500      CONTINUE                                         00035000
C
C          3600      1500      CONTINUE                                         00035100
C
C          3640      1500      CONTINUE                                         00035200
C
C          3680      1500      CONTINUE                                         00035300
C
C          3720      1500      CONTINUE                                         00035400
C
C          3760      1500      CONTINUE                                         00035500
C
C          3800      1500      CONTINUE                                         00035600
C
C          3840      1500      CONTINUE                                         00035700
C
C          3880      1500      CONTINUE                                         00035800
C
C          3920      1500      CONTINUE                                         00035900
C
C          3960      1500      CONTINUE                                         00036000
C
C          4000      1500      CONTINUE                                         00036100
C
C          4040      1500      CONTINUE                                         00036200
C
C          4080      1500      CONTINUE                                         00036300
C
C          4120      1500      CONTINUE                                         00036400
C
C          4160      1500      CONTINUE                                         00036500
C
C          4200      1500      CONTINUE                                         00036600
C
C          4240      1500      CONTINUE                                         00036700
C
C          4280      1500      CONTINUE                                         00036800
C
C          4320      1500      CONTINUE                                         00036900
C
C          4360      1500      CONTINUE                                         00037000
C
C          4400      1500      CONTINUE                                         00037100
C
C          4440      1500      CONTINUE                                         00037200
C
C          4480      1500      CONTINUE                                         00037300
C
C          4520      1500      CONTINUE                                         00037400
C
C          4560      1500      CONTINUE                                         00037500
C
C          4600      1500      CONTINUE                                         00037600
C
C          4640      1500      CONTINUE                                         00037700
C
C          4680      1500      CONTINUE                                         00037800
C
C          4720      1500      CONTINUE                                         00037900
C
C          4760      1500      CONTINUE                                         00038000
C
C          4800      1500      CONTINUE                                         00038100
C
C          4840      1500      CONTINUE                                         00038200
C
C          4880      1500      CONTINUE                                         00038300
C
C          4920      1500      CONTINUE                                         00038400
C
C          4960      1500      CONTINUE                                         00038500

```



```

C          CONTINUE
C          CONTINUE
C          RETURN
C
5      FORMAT(1H0, '-- LEVEL1, 15, 'POINTERS --'(1X,'(H-',E15.7,')'))
6      FORMAT(//1X,'NROW',6X,'NCOL',6X,'NPOINT',10X,'H//'
7          ,(6X,31I0,120,1))
8      FORMAT(//12X,'[FFF1',5X,'RIGHT'/(11X,15,5X,15))
9      FORMAT(//12X,'[FFF1',5X,'RIGHT',6X,'[LOC',6X,'RLOC',6X,'SLOC',
10     '       ,6X,'[NLOC'/(11X,61,5X,15)))
11     FORMAT(//12X,'[FFF1',5X,'Y--',E15.7,')--')
12     FORMAT(1H0, '-- ROW',15,5X,'Y--',E15.7,')--')
13     FORMAT(11X,'BLOC',1,2015/(1/X,2015))
14     FORMAT(11X,'BNDLOC',2015/(17X,2015))
15     FORMAT(11X,'BNDIYP',2015/(17X,2015))
C
C          END
C
C          SUBROUTINE VERIFY(NLEVEL)
C
C          VERIFY -- PRINT DIAGRAMS OF THE GRIDS
C
C          INTEGER CHAR(20), DASH,BLANK,I LINE(115), BPOS,BPI,BTYP,RPI
C          INTEGER SLVI(20), LPI, BLEFT, RRIGHT, RLOC, NLOC, SLOC, BNDLOC, BROW, BLOC,
C          BNDIYP
C          COMMON /TRACE/IN,LP,NDRUG,NPRINT,NINT
C          COMMON /POINT/SLVI(20), BI VI(20), LEFT(400), RIGHT(400),
C          ILOC(400), RLOC(400), NLOC(400), SLOC(400), BNDLOC(1000),
C          RNDIYP(1000), BROW(400), BLOC(1000)
C          COMMON /SIZE/NROW(20), NCOL(20), NPOINT(20), IIVAL(20), XMIN,XMAX,
C          YMIN,YMAX
C          DATA CHAR/'1','2','3','4','5','6','7','8','9','A','B','C',
C          'D','E','S','/,
C          BLANK'/ ',DASH'/-'/
C
C          WRITE(LP,10)
C
C          DO 1000 JLEVEL=1,NLEVEL
C
C              WRITE(LP,20)JLEVEL
C
C              KPI=SLVI(JLEVEL+1)-1
C              RPI=BI VI(JLEVEL+1)-1
C              KMAX=BROW(JLEVEL)
C
C              DO 800 KROW=1,KMAX
C
C                  BPI=BROW(RPI)
C                  BPOS=BNDLOC(BPI)
C
C                  NBRK=LEFT(KPI)+1
C                  NCHAR=RIGHT(KPI)-LEFT(KPI)+1
C                  IPI=ILOC(KPI)
C
C                  PRODUCE A LINE OF PRINT
C
C                  DO 600 IPOS=1,NCHAR
C
C

```

```

LINE(LPOS)-DASH
IF(BPOS.NE.LPT) GO TO 500
C
      B1YP=BNDIYP(BP1)
      LINL(LPOS)=CHAR(B1YP+1)
      BP1=BP1+1
      BPOS=BNDILOC(BP1)
      500          LPT=LPT+1
C
      CONTINUE
C
      LROW=KMAX-KROW
      WRITE(LP,30) LROW, (BLANK,N-1,NBINK),
      (LINE(N),N=1,NCHAR)
C
      RP1=RP1-1
      KP1=KP1-1
C
      600          CONTINUE
C
      RETURN
C
      1000        CONTINUE
C
      FORMAT(1H1,6X,'GRID DIAGRAMS'//11X,'MOLECULES --'//,
      /21X,'X     X     X     X     X     X     X',
      /21X,'X     X     X3X   X0X   5X   X6    7X   X8   X9X',
      /21X,'X     X     X     X     X     X     X     X     X',
      //21X,'A,B,C,D -- HOECKER MOLECULE'//)
      20           FORMAT(//11X,'LEVEL',15//1X,'ROW')
      30           FORMAT(1X,15,115A1)
C
      END
C
C
      SUBROUTINE PREP(LEVEL,G,R)
C
      PREP -- ASSIGN INITIAL VALUES TO THE SOLUTION VECTOR
      (FINE GRID) AND FORM THE CORRESPONDING RIGHT-HAND
      SIDE
C
      INTEGER SLVI,BLVL,RIGHT,RLOC,NLOC,SLOC,BNDLOC,BROW,BLOC,
      BNDTYP
      COMMON /POINT/SLV(20),BLVI(20),LEFT(400),RIGHT(400),
      LLOC(400),RLOC(400),NLOC(400),SLOC(400),BNDLOC(1000),
      BNDTYP(1000),BROW(400),BLOC(1000)
      COMMON /SIZE/NROW(20),NCOL(20),NPINT(20),BVAL(20),XMIN,XMAX,
      #      YMIN,YMAX
      COMMON /STORE/U(5000),I(5000)
C
      JROW=0
      MCOL=NCOL(1 LEVEL)
C
      JMIN=SLVI(1 LEVEL)
      JMAX=SLVI(1 LEVEL+1)-1
      II=RVAL(LEVEL)
      IIOLM=.5*II
C
      PRODUCE VALUES BY ROWS

```

```

C      DO 400 JPF=JMIN,JMAX
C
C          Y=YMIN+H*FLOAT(JROW)
C          JROW=JROW+1
C
C          KMIN=LLOC(JPF)
C          KMAX=RLOC(JPF)
C          JCOL=FF1(JPF)
C
C          DO 300 KPT=KMIN,KMAX
C
C              X=XMIN+H*FLOAT(JCOL)
C              JCOL=JCOL+1
C
C              U(KPT)=G(X,Y,H101)
C              F(KPT)=R(X,Y,H101)
C
C 300          CONTINUE
C
C 400          CONTINUE
C
C          RETURN
C
C          END
C
C          SUBROUTINE TEST(G,R)
C
C          EXTERNAL G,R
C
C          INTEGER NOPRNT,PRNT,SHORT,LONG,NOPLOT,PLOT,NOSVEC,SVEC,
C                  NORHS,RHS
C          COMMON /CONTROL/ NLEVEL,LOI,WMAX
C
C          DATA NOPRNT,SHORT,NOPLOT,NOSVEC,NORHS/5*0/,
C                  PRNT,LONG,PLOT,SVEC,RHS/5*1/
C
C          LEVEL=1
C          CALL PREP(LEVEL,G,R)
C          CALL RSLUST(LEVEL,NOPRNT,LONG,PLOT,SVEC,RHS)
C          CALL RELAX(LEVEL,X,Y,Z)
C          CALL RSLUST(LEVEL,PRNT,LONG,PLOT,SVEC,RHS)
C          CALL RESCAL(LEVEL)
C          CALL RSLUST(LEVEL+1,PRNT,LONG,PLOT,SVEC,RHS)
C
C          RETURN
C          END
C
C          SUBROUTINE MULTIG
C
C          MULTIG -- THIS ROUTINE PERFORMS THE MULTIGRID PROCESS
C          DESIGNATED CYCLE-C ON A GRID OF ARBITRARY SHAPE
C          WITH UNIFORM SPACING. THE ALGORITHM IS OUTLINED
C          IN THE ARTICLE BY AGUSTIN BRANDE, MATHEMATICS OF

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COMPUTATION, APRIL, 1977, PAGES 333-390.
 DIRICHLET PROBLEMS MAY BE SOLVED WITH NO
 RESTRICTIONS. NEUMANN AND MIXED NEUMANN-DIRICHLET
 PROBLEMS MAY BE SOLVED WITH THE RESTRICTION OF ZERO
 NORMAL DERIVATIVES. THIS SET OF ROUTINES MAY BE
 MODIFIED TO ACCEPT NEUMANN OR MIXED PROBLEMS IN
 WHICH EITHER THE X OR Y COMPONENT IS ZERO AT EVERY
 BOUNDARY POINT.

PARAMETERS --
 NLEVEL -- THE NUMBER GRIDS TO BE EMPLOYED IN THE
 MULTIGRID PROCESS
 TOL -- TOLERANCE ON THE ERROR ON GRID M
 WMAX -- MAXIMUM WORK ALLOWED FOR SOLUTION PROCESS

VARIABLES AND ARRAYS
 U -- STORAGE FOR GRIDS 1 THROUGH M AND ACCOMPANYING
 RIGHT-HAND SIDES
 KLEVEL -- THE CURRENT LEVEL
 WORK -- THE TOTAL EFFORT EXPENDED IN THE SOLUTION
 PROCESS
 DELTA -- THE UPPER LIMIT ON THE RATIO OF ERROR ON
 GRID K TO THAT ON GRID K+1 IF INJECTION IS TO
 OCCUR
 EPS(K) -- LIST OF THE ERROR LIMITS THAT MUST BE MET
 TO GET BACK TO GRID M BY INJECTION FROM GRID K
 ETA -- THE CONVERGENCE FACTOR (CURRENT ERROR DIVIDED
 BY PREVIOUS ERROR) MUST BE LESS THAN ETA FOR
 RELAXATION SWEEPS TO CONTINUE

COMMON STORAGE --
 /TRACE/
 IN -- INPUT DEVICE
 LP -- OUTPUT DEVICE
 NDEBUG -- SWITCH THAT CONTROLS THE DEBUG TRACE
 0 -- OFF
 ANYTHING ELSE -- ON
 NPRINT -- THE NUMBER OF ROWS OF THE SOLUTION VECTOR
 AND RIGHT-HAND SIDE TO BE PRINTED WHEN THE
 TRACE IS ON
 NINT -- THE NUMBER OF INTERVALS TO BE USED IN PLOTS

/SIZE/
 NROW(*) -- THE NUMBER OF ROWS IN EACH GRID
 NCOL(*) -- THE NUMBER OF COLUMNS IN EACH GRID
 IVAL(*) -- THE SPACING OF EACH GRID (UNIFORM)
 XMIN, XMAX, YMIN, YMXX -- SAME AS XMINT, TIC

/STORE/
 U -- STORAGE FOR GRIDS 1 THROUGH M AND ACCOMPANYING
 RIGHT-HAND SIDES
 F(*) -- STORAGE FOR THE RIGHT-HAND SIDE

USE OF MULTIG --
 MULTIG REQUIRES THREE ADDITIONAL ROUTINES FOR
 OPERATION. ONE FUNCTION MUST GIVE THE BOUNDARY
 CONDITIONS OF THE SOLUTION DOMAIN AND AN ESTIMATE
 OF THE SOLUTION. ANOTHER MUST GIVE THE POISSON
 EQUATION RIGHT-HAND SIDE. A MAIN ROUTINE IS NEEDED
 TO CALL MULTIG AND GIVE VALUES TO THE PARAMETERS
 IT REQUIRES THE NAMES OF THE TWO FUNCTIONS MUST BE

```

C IF(WORK,LE,WMAX) GO TO 220          00083900
C C LIMIT EXCEEDED - PRINT SOLUTION VECTOR AND QUIT 00084000
C C
C WRITE(1,P,20)                         00084300
C KLEVEL=1                             00084400
C CALL RESULT(KLEVEL,PRNT,SHORT,PLOT,SVEC,NORHS)
C RETURN                                00084600
C C DETERMINE IF CONVERGENCE IS FAST ENOUGH 00084700
C C
C 220 IF(ERR,LE,EPSS(KLEVEL)) GO TO 240 00084900
C C CONTINUE THE RELAXATION SWEEPS IF THE PRESENT 00085000
C GRID IS THE COARSEST GRID OR IF THE RATE OF 00085300
C CONVERGENCE IS WITHIN THE DESIRED RANGE 00085400
C OR IF THE ERROR IS CONVERGING AS REQUIRED 00085500
C
C IF(KLEVEL,LE,MAXLVL,OR,ERR/FRRPRV,LT,EIA) 00085600
C $ GO TO 200                            00085700
C C DETERMINE IF THE PROCESS ON THE COARSER GRID 00085800
C IS REDUCING THE ERROR ON THE PRESENT GRID 00086200
C
C IF(ERR,LE,ERRLM(KLEVEL))GO TO 230      00086300
C C ELIMINATE THE COARSER GRIDS FROM USE 00086400
C
C NXLEV=L-1+KLEVEL+1                   00086500
C WRITE(1,P,50)NXLEV,MAXLVL             00086720
C MAXLVL=KLEVEL                         00086800
C GO TO 200                            00086900
C C
C C THE CONVERGENCE IS SLOW - TAKE THE RESIDUALS 00087000
C THAT WOULD RESULT FROM ANOTHER RELAXATION SWEEP 00087200
C 230 ERRLM(KLEVEL)=ERR                 00087300
C ERRLM(KLEVEL+1)=1,L30                00087400
C CALL RESCAL(KLEVEL)                  00087600
C KLEVEL=KLEVEL+1                      00088100
C IF(NORUG,NE,0)CALL RESULT(KLEVEL,PRNT,SHORT,PLOT, 00088200
C NOSVEC,NORHS)                        00088300
C EPS(KLEVEL), DELTA,ERR               00088400
C CALL ZERO(KLEVEL)                   00088500
C ERR=1,0,30                           00088600
C GO TO 200                            00088700
C C
C C THE ERROR FOR THIS GRID IS WITHIN SPECIFIED 00089200
C TOLERANCES. IF THE CURRENT GRID IS NOT THE 00089300
C FINE GRID, INJECT THE SOLUTION OF THE CURRENT 00089400
C RESIDUAL EQUATION INTO THE NEXT FINER GRID. 00089500
C
C 240 IF(KLEVEL,NE,1) GO TO 250          00089600
C C
C C THE RESIDUAL ON THE FINE GRID IS 00089700
C WITHIN THE SPECIFIED TOLERANCE SO QUIT 00089800
C C

```

```

C JCHAX=RLOC(JROW) 00096700
C BPT=BROW(JROW) 00096800
C BPOS=BNDLOC(BPT) 00096900
C DO 4000 JC=JCMIN,JCMAX 00097000
C      BOLD=U(JC) 00097100
C      CHECK FOR BOUNDARY POINT 00097200
C      IF(BPOS.EQ.JC) GO TO 60 00097300
C      OTHERWISE USE A 4-PT MOLECULE 00097400
C      U(JC)=.25*(U(JC-1)+U(JC+1)+U(JN)+U(JS)-F(JC)) 00097500
C      GO TO 4800 00097600
C
C 60 BTYP=BNDTYP(BPT) 00097800
C      BPT=BPT+1 00097900
C      BPOS=BNDLOC(BPT) 00098000
C      CHECK FOR DIRICHLET POINT 00098100
C      IF(BTYP.EQ.0) GO TO 4800 00098200
C      SELECT THE INDICATED COMPUTATIONAL MOLECULE 00098300
C      X   X   X   X   X   X   X   X 00098400
C      1X  X2  X3X  X4X  5X  X6  7X  X8  X9X 00098500
C      X   X   X   X   X   X   X   X 00098600
C      00098700
C      10, 11, 12, 13 HOECKER MOLECULE 00098800
C      GO TO(100, 200, 300, 400, 500, 600, 700, 800, 900, 00098900
C          1000, 1100, 1200, 1300), BTYP 00099000
C
C 100 U(JC)=.25*(U(JN)+U(JS)+U(JC+1)+U(JC+1)-F(JC)) 00099100
C      GO TO 4800 00099200
C
C 200 U(JC)=.25*(U(JN)+U(JS)+U(JC-1)+U(JC-1)-F(JC)) 00099300
C      GO TO 4800 00099400
C
C 300 U(JC)=.25*(U(JN)+U(JN)+U(JC+1)+U(JC-1)-F(JC)) 00099500
C      GO TO 4800 00099600
C
C 400 U(JC)=.25*(U(JS)+U(JS)+U(JC+1)+U(JC-1)-F(JC)) 00099700
C      GO TO 4800 00099800
C
C 500 U(JC)=.25*(U(JN)+U(JN)+U(JC+1)+U(JC+1)-F(JC)) 00099900
C      GO TO 4800 00100000
C
C 600 U(JC)=.25*(U(JN)+U(JN)+U(JC-1)+U(JC-1)-F(JC)) 00100100
C      GO TO 4800 00100200
C
C      00100300
C
C      00100400
C      00100500
C      00100600
C      00100700
C
C      00100800
C      00100900
C      00101000
C      00101100
C      00101200
C      00101300
C      00101400
C      00101500
C      00101600
C      00101700
C      00101800
C      00101900
C      00102000
C      00102100
C      00102200
C      00102300
C      00102400
C      00102500
C      00102600
C      00102700
C      00102800
C      00102900
C      00103000
C      00103100
C
C      250
C      $      CALL RESULT(KLEVEL, PRNT, LONG, PLOT, SVFC, NORHS) 00090200
C      RETURN 00090300
C
C      INJECT THE RESIDUAL - INTERPOLATE IT AND 00090400
C      ADD TO THE NEXT FINER GRID 00090500
C
C      250
C      $      CALL INTADD(KLEVEL)
C      KLEVEL=KLEVEL-1 00091100
C      IF(NDBUG.GE.100)CALL RESULT(KLEVEL, PRNT, SHORT, PLOT, 00091200
C                      SVFC, NORHS) 00091300
C      ERR=1.0E30 00091400
C      GO TO 200 00091500
C
C      250
C      $      5      FORMAT(IIII)
C      FORMAT(III,5X,'-- MULTIG --',// 00092000
C          1IX,'MAXLVL, TOL, MAX',15,2E20,7) 00092100
C      15      FORMAT(6X,15,4E15.7) 00092200
C      20      FORMAT(1II0,10X,'-- WORK LIMIT EXCEEDED --') 00092300
C      40      FORMAT(/8X,'LEVEL, DMAX, ERR, ERLOG, WORK') 00092500
C      50      FORMAT(/1IX,'DROPPING GRIDS ',15,' TO ',15) 00092650
C
C      250
C      $      C      END 00092700
C
C      250
C      $      C      SUBROUTINE RELAX(LEVEL, RESSUM, DMAX, ERR, UAV) 00093600
C
C      250
C      $      C      RELAX -- PERFORM A RELAXATION SWEEP ON GRID LEVEL 00093700
C
C      250
C      $      C      INTEGER BPT, BPOS, BTYP 00093800
C      250
C      $      C      INTEGER SLVL,BVVL,RIGH,RLOC,NLOC,SLOC,BNDLOC,BROW,BLOC, 00094000
C          BNDTYP 00094100
C      250
C      $      C      COMMON /IRACI/IN,LP,NDRUG,NPRINT,NINT 00094200
C      250
C      $      C      COMMON /POINT/SLVL(20),BVVL(20),LEFT(100),RIGHT(100), 00094300
C          LLOC(400),RLOC(400),NLOC(400),SLOC(400),BNDLOC(1000), 00094400
C          BNDTYP(1000),BROW(1000),BLLOC(1000) 00094500
C      250
C      $      C      COMMON /SIZF/NROW(20),NCOL(20),NPOINT(20),IVAI(20),XMIN,XMAX, 00094600
C          YMIN,YMAX 00094700
C      250
C      $      C      COMMON /STORI/U(5000),I(5000) 00094800
C
C      250
C      $      C      00094900
C      250
C      $      C      00095000
C      250
C      $      C      00095100
C      250
C      $      C      00095200
C      250
C      $      C      00095300
C      250
C      $      C      00095400
C      250
C      $      C      00095500
C      250
C      $      C      00095600
C
C      250
C      $      C      00095700
C      250
C      $      C      00095800
C      250
C      $      C      00095900
C      250
C      $      C      00096000
C      250
C      $      C      00096100
C      250
C      $      C      00096200
C      250
C      $      C      00096300
C      250
C      $      C      00096400
C      250
C      $      C      00096500
C      250
C      $      C      00096600
C
C      250
C      $      C      IROW=BVVL(LEVEL)
C      JNIN=SLVL(LEVEL)
C      JMAX=SLVL(LEVEL+1)-1
C
C      250
C      $      C      DO 6000 JROW=JMIN,JMAX
C
C      250
C      $      C      JN=NLOC(JROW)
C      JCMIN=LLOC(JROW)
C      JS=SLOC(JROW)

```

```

700      U(JC)=.25*(U(JS)+U(JS)+U(JC+1)+U(JC+1)-F(JC)) 00103200
         GO TO 4800
C
C
800      U(JC)=.25*(U(JS)+U(JS)+U(JC+1)+U(JC+1)-F(JC)) 00103500
         GO TO 4800
C
C
900      U(JC)=.25*(U(JN)+U(JS)+U(JC+1)+U(JC+1)-F(JC)) 00103600
         GO TO 4800
C
C
1000     U(JC)=(U(JC-1)+U(JN)+2.*(U(JC+1)+U(JS))-        00104400
         F(JC))/6.                                         00104500
         GO TO 4800
C
C
1100     U(JC)=(U(JC+1)+U(JN)+2.*(U(JC+1)+U(JS))-        00104900
         F(JC))/6.                                         00105000
         GO TO 4800
C
C
1200     U(JC)=(U(JC-1)+U(JS)+2.*(U(JC+1)+U(JN))-        00105400
         F(JC))/6.                                         00105500
         GO TO 4800
C
C
1300     U(JC)=(U(JC+1)+U(JS)+2.*(U(JC+1)+U(JN))-        00105900
         F(JC))/6.                                         00106000
         GO TO 4800
C
C
4800      JN=JN+1
         JS=JS+1
C
         DIFF=ABS(U(JC)-UOLD)
         RESSUM=RESUM+DIFF
         USUM=USUM+ABS(U(JC))
         IF(DIFFMAX.LT.DIFF) DIFFMAX=DIFF
C
4900      CONTINUE
C
         LROW=LROW+1
C
C
5000      CONTINUE
C
         DETERMINING THE AVERAGE RESIDUAL
C
         ERR=RESUM/FLOAT(NPOINT(LEVEL))
         UAV=USUM/FLOAT(NPOINT(LEVEL))
C
         RETURN
C
10      FORMAT(//6X,'--- RELAX --- (LEVEL',15,' )')
C
C
END

```

```

SUBROUTINE RESCAL(LEVEL) 00109800
C
C
         * RELAX -- PERFORM A RELAXATION SWEEP ON GRID LEVEL
         * IN ORDER TO CALCULATE THE COARSE RESIDUAL.
         * 00110000
         * 00110100
         * 00110200
         * 00110300
         * 00110400
         * 00110500
         * 00110600
         * 00110700
         * 00110800
         * 00110900
         * 00111000
         * 00111100
         * 00111200
         * 00111300
         * 00111400
         * 00111500
         * 00111600
         * 00111700
         * 00111800
         * 00111900
         * 00112000
         * 00112100
         * 00112200
         * 00112300
         * 00112400
         * 00112500
         * 00112600
         * 00112700
         * 00112800
         * 00112900
         * 00113000
         * 00113100
         * 00113200
         * 00113300
         * 00113400
         * 00113500
         * 00113600
         * 00113700
         * 00113800
         * 00113900
         * 00114000
         * 00114100
         * 00114200
         * 00114300
         * 00114400
         * 00114500
         * 00114600
         * 00114700
         * 00114800
         * 00114900
         * 00115000
         * 00115100
         * 00115200
         * 00115300
         * 00115400
         * 00115500
         * 00115600
         * 00115700
         * 00115800
         * 00115900
         * 00116000
         * 00116100
         * 00116200
C
         IF(NDEBUG.NE.0) WRITE(1,P,10) LEVEL
C
C
         LROW=BLVL(LEVEL+1)
         JROW=SLVL(LEVEL)
         KMAX=SLVL(LEVEL+2)-1
         KMIN=SLVL(LEVEL+1)
C
         DO 6000 KROW=KMIN,KMAX
C
         JN=NLOC(JROW)
         JS=SLOC(JROW)
         JC=LLOC(JROW)
C
         BPT=BROW(LROW)
         BPOS=BNDLOC(BPT)
C
         KCMIN=LLOC(KROW)
         KCHAX=RLOC(KROW)
C
         DO 4000 KC=KCMIN,KCHAX
C
         CHECK FOR A BOUNDARY POINT
C
         IF(BPOS.EQ.KC) GO TO 60
C
         OTHERWISE USE A 4-PT MOLECULE
         UVAL=(U(JC-1)+U(JC+1)+U(JN)+U(JS)-F(JC))
         GO TO 4800
C
         60      BPT=BNDLOC(BPT)
                 BPT=BPT+1
                 BPOS=BNDLOC(BPT)
C
         CHECK FOR DIRICHLET POINT
C
         IF(BIYP.NE.0) GO TO 90
C
         UVAL=U(JC)

```



```

C   600      CONTINUE
C
C   TAKE CARE OF ANY POINT ON THE RIGHT OF A FINE
C   GRID SEGMENT THAT HAS NOT BEEN CHANGED
C
C   IF(KL.NE.BPOS1)GO TO 620
C
C   IF(CHECKB(BPOS1,BP1TOP),EQ.0)GO TO 800
C
C   U(KL)-.5*(U(JB)+U(JT))
C
C   620      CONTINUE
C
C   TAKE CARE OF THE BOTTOM POINT ON THE RIGHT SIDE OF
C   THE LAST SEGMENT
C
C   IF(KB.NE.BPOS2)GO TO 820
C
C   IF(CHECKB(BPOS2,BP1BOT),EQ.0)GO TO 840
C
C   820      U(KB)-U(KB)+U(JB)
C
C   MOVE ROW POINTERS
C
C   840      JSPIR=JSPIR+1
C             KSPIR=KSPIR+2
C
C   1000     CONTINUE
C
C   *RETURN
C
C   10        FORMAT(//6X,'--- INITADD --- (LEVEL',I5,' )')
C
C   END
C
C   FUNCTION CHECKB(BPOS,BP1)
C
C   DETERMINE THE TYPE OF THE BOUNDARY POINT AT BPOS
C
C   INTEGER CHECKB,BPOS,BP1
C   INTEGER SLVL,BLVL,RIGHT,RLOC,NLOC,SLOC,BNDLOC,BROW,BLOC,
C             BNDTYP
C   COMMON /POINT1/SLVL(20),BLVL(20),LEFT(400),RIGHT(400),
C             LLOC(400),RLOC(400),NLOC(400),SLOC(400),BNDLOC(1000),
C             BNDTYP(1000),BROW(400),BLOC(1000)
C
C   CHECKB=BNDTYP(BP1)
C             BP1=BP1+1
C             BPOS=BNDLOC(BP1)
C
C   100      NSEG=1
C             KSEG(1)=1
C             JBOT(1)=LLOC(JSPIR)
C             JBO1R(1)=RLOC(JSPIR)
C             KBOT(1)=LLOC(KSPIR)
C             JIOP(1)=NLOC(JSPIR)
C             KIOP(1)=NLOC(KSPIR)
C             GO TO 600
C
C   100      NSEG=NSEG+1
C             OR  *-----*
C             *-----* OR  *-----*
C             *-----* OR  *-----*
C
C   100      NSEG=1
C             KSEG(1)=1
C             JBOT(1)=LLOC(JSPIR)
C             JBO1R(1)=RLOC(JSPIR)
C             KBOT(1)=LLOC(KSPIR)
C             JIOP(1)=NLOC(JSPIR)
C             KIOP(1)=NLOC(KSPIR)
C             GO TO 600
C
C   100      NSEG=NSEG+1
C             OR  *-----*

```

```

C-----#-----#
C-----#-----#
C      200      NSEG=2
C      KSLG(1)=1
C      JBOIL(1)=LLOC(JSPIR)
C      JBOIR(1)=RLOC(JSPIR)-(JBR-JTR)
C      KB01I(1)=LLOC(KSPIR)
C      JTOP1(1)=NLOC(KSPIR)
C      KTOP1(1)=NLOC(KSPIR)
C
C      KSLG(2)=0
C      JBOIL(2)=JBOIR(1)
C      JBOIR(2)=JBR
C      KB01I(2)=RLOC(KSPIR)-(JBR-JTR)*?
C      KTOP1(2)=1
C      JTOP1(2)=1
C      GO TO 600
C
C      -----# OR -----#
C
C      300      NSEG=2
C      KSLG(1)=0
C      JBOIL(1)=LLOC(JSPIR)
C      JBOIR(1)=SLOC(JSPIR+1)
C      KB01I(1)=LLOC(KSPIR)
C      JTOP1(1)=1
C      KTOP1(1)=1
C
C      KSLG(2)=1
C      JBOIL(2)=JBOIR(1)
C      JBOIR(2)=RLOC(JSPIR)
C      JTOP1(2)=LLOC(JSPIR+1)
C      KB01I(2)=SLOC(KSPIR+1)
C      KTOP1(2)=LLOC(KSPIR+1)
C      GO TO 600
C
C      -----#
C
C      400      NSEG=3
C      KSLG(1)=0
C      JBOIL(1)=LLOC(JSPIR)
C      JBOIR(1)=SLOC(JSPIR+1)
C      KB01I(1)=LLOC(KSPIR)
C      JTOP1(1)=1
C      KTOP1(1)=1
C      KSLG(2)=1
C      JBOIL(2)=JBOIR(1)
C      JBOIR(2)=RLOC(JSPIR)-(JBR-JTR)
C      JTOP1(2)=LLOC(JSPIR+1)
C      KB01I(2)=SLOC(KSPIR+1)
C      KTOP1(2)=LLOC(KSPIR+1)
C
C      KSLG(3)=0
C      JBOIL(3)=JBOIR(2)
C      JBOIR(3)=RLOC(JSPIR)
C      KB01I(3)=RLOC(KSPIR)-(JBR-JTR)*?
C      JTOP1(3)=1
C      KTOP1(3)=1
C      GO TO 600
C
C      500      NSEG=1
C      KSLG(1)=0
C      JBOIL(1)=LLOC(JSPIR)
C      JBOIR(1)=RLOC(JSPIR)
C      KB01I(1)=LLOC(KSPIR)
C      JTOP1(1)=1
C      KTOP1(1)=1,
C      GO TO 600
C
C      600      RETURN
C
C      SUBROUTINE RESULT LEVEL,JPRNT,flen,jplot,jsol,jrhs
C      RESULT -- PRINT ALL OR PART OF THE SOLUTION VECTOR
C      LEVEL -- GRID TO BE USED
C      JPRNT --
C          0 - DO NOT PRINT EITHER THE SOLUTION VECTOR OR THE RIGHT-HAND SIDE
C          1 - ENABLE PRINTING OF THE SOLUTION VECTOR OR THE RIGHT-HAND SIDE
C      flen --
C          0 - PRINT THE NUMBER OF ROWS GIVEN BY NPRINT
C          1 - PRINT ALL ROWS OF THE GRID
C      jplot --
C          0 - DO NOT PLOT EITHER THE SOLUTION VECTOR OR THE RIGHT-HAND SIDE
C          1 - ENABLE PRINTING OF THE SOLUTION VECTOR OR THE RIGHT-HAND SIDE
C      jsol --
C          0 - DO NOT PRINT OR PLOT THE SOLUTION VECTOR
C          1 - PRINT OR PLOT THE SOLUTION VECTOR IF ENABLED
C      jrhs --
C          0 - DO NOT PRINT OR PLOT THE RIGHT-HAND SIDE
C          1 - PRINT THE RIGHT-HAND SIDE AND GIVE A PLOT
C              IF PLOTS ARE ENABLED
C
C      INTEGER SLYL,BIVL,RIGHL,RLOC,NLOC,SLOC,BNDLOC,BROW,BLOC,
C      BNDTYPE
C      COMMON /TRACL/IN,LIP,NDEBUG,NPRINT,NINI
C      COMMON /POINT/SLYL(20),BIVL(20),EL1(400),RIGHT(400),
C          LLOC(400),RLOC(400),NLOC(400),SLOC(400),BNDLOC(1000),
C          BNDTYPE(1000),BROW(400),BLOC(1000)
C      COMMON /SIZE/NROW(20),NCOL(20),NPONT(20),IVAL(20),XMIN,XMAX,
C          YMIN,YMAX
C      COMMON /STOR/ I(5000),L(5000)
C      DATA JSIZL/5000/
C
C      WRITE(IP,10)LEVEL
C
C      00155400
C      00155500
C      00155600
C      00155700
C      00155800
C      00155900
C      00156000
C      00156100
C      00156200
C      00156300
C      00156400
C      00156500
C      00156600
C      00156700
C      00156800
C      00156900
C      00157000
C      00157100
C      00157200
C      00157300
C      00157400
C      00157500
C      00157600
C      00157700
C      00157800
C      00157900
C      00158000
C      00158100
C      00158200
C      00158300
C      00158400
C      00158500
C      00158600
C      00158700
C      00158800
C      00158900
C      00159000
C      00159100
C      00159200
C      00159300
C      00159400
C      00159500
C      00159600
C      00159700
C      00159800
C      00159900
C      00160000
C      00160100
C      00160200
C      00160300
C      00160400
C      00160500
C      00160600
C      00160700
C      00160800
C      00160900
C      00161000
C      00161100
C      00161200
C      00161300
C      00161400
C      00161500
C      00161600
C      00161700
C      00161800
C
C      00161900
C      00162000
C      00162100
C      00162200
C      00162300
C      00162400
C      00162500
C      00162600
C      00162700
C      00162800
C      00162900
C      00163000
C      00163100
C      00163200
C      00163300
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C      00166300
C      00166400
C      00166500
C      00166600
C      00166700
C      00166800
C      00166900
C      00167000
C      00167100
C      00167200
C      00167300
C      00167400
C      00167500
C      00167600
C      00167700
C      00167800
C      00167900
C      00168000
C      00168100
C      00168200
C      00168300

```

```

C IF(JPRNT.EQ.0)GO TO 200
C
C      KMAX=NROW(LEVEL1)
C      IF(JLEN.EQ.0)KMAX=AMINO(KMAX,NPRINT)
C
C      KMIN=SLVL(LEVEL)
C      KMAX=KMAX-KMIN+1
C      JROW=0
C      I=HVAL(LEVEL)
C
C      DO 200 KPI=KMIN,KMAX
C
C          Y=YMIN+I*1.0/DA(I,JROW)
C
C          WRITE(LP,20)JROW,LEFT(KPI),RIGHT(KPI),Y
C
C          JMIN=LLOC(KPI)
C          JMAX=RLOC(KPI)
C
C          IF(JSOL.NE.0)WRITE(LP,30)(U(J),J=JMIN,JMAX)
C          IF(JRHS.NE.0)WRITE(LP,40)(F(J),J=JMIN,JMAX)
C          JROW=JROW+1
C
C 200      CONTINUE
C
C 240      CONTINUE
C
C
C      IF(JPLOT.EQ.0)GO TO 300
C
C      IF(JSOL.EQ.0)GO TO 280
C
C          WRITE(LP,50)
C          CALL PLOT(LEVEL1,U,JSIZE)
C
C 280      IF(JRHS.EQ.0) GO TO 300
C
C          WRITE(LP,60)
C          CALL PLOT(LEVEL1,F,JSIZE)
C
C
C 300      RETURN
C
C
C 40      FORMAT(//7GX,'--- RESULT --- (LEVEL1,15.7)')
C
C 50      FORMAT(/11X,'ROW',15.5X,'LEFT COL',15.5X,'RIGHT COL',15.
C 60      *      5X,'Y=15.7')
C 60      *      FORMAT(/16X,'SOLUTION VICTOR'/(11X,6E15.7))
C 60      *      FORMAT(/16X,'RIGHT-HAND SIDE'/(11X,6E15.7))
C 60      *      FORHAI(111,5X,'SOLUTION VICTOR')
C 60      *      FORHAI(111,5X,'RIGHT-HAND SIDE')
C
C      END
C
C
C      SUBROUTINE PLOT(LEVEL,Z,JSIZE)

```

```

C PLOT -- GIVE A CONTOUR PLOT OF THE SOLUTION VECTOR OF
C GRID LEVEL
C
$ INTEGER SLEVEL,BLVL,RIGHT,RLOC,NLOC,SLOC,BNDLOC,BROW,BLOC,
  BNDTYPE
COMMON /TRACE/IN,LP,NDBG,NPRINT,NINI
COMMON /POINT/SLEVEL(20),BLVL(20),LEFT(400),RIGHT(400),
  LLOC(400),RLOC(400),NLOC(400),SLOC(400),BNDLOC(1000),
  BNDTYPE(1000),BROW(400),BLOC(1000)
COMMON /SIZE/ROW(20),NCOL(20),NPOINT(20),BVAL(20),XMIN,XMAX,
  YMIN,YMAX
DIMENSION 7/JSIZE/
INTEGER LINE(120),CHAR(20)*BLANK
DATA CHAR/'A','B','C','D','E','F','G','H','I','J','K','L','M','O',
  'P','R','S','T','U','W','X','Z'/
DATA BLANK/' ',MAXINT/20/,Z11BH/1.0E-20/,Z11H/1.0E+20/
C
$ JMIN=SELV(1,LEVEL)
$ JMAX=SELV(LEVEL+1)-1
C
$ KMIN=LLOC(JMIN)
$ KMAX=RLOC(JMAX)
C
$ ZMAX=Z(KMIN)
$ ZMIN=ZMAX
C
DO 200 K=KMIN,KMAX
C
  ZVAL=Z(K)
  IF(ZMIN.GT.ZVAL)ZMIN=ZVAL
  IF(ZMAX.LT.ZVAL)ZMAX=ZVAL
C
200 CONTINUE
C
C
ZDIF=ZMAX-ZMIN
KINI=AMINO(NINI,MAXINT)
ZFACT=0.0
IF(ZDIF.LE.ZLIM)ZFACT=FLOAT(KINI)/ZDIF
C
LEN=MAXU(NROW(LEVEL),NCOL(LEVEL))
JP1=JMAX
LMAX=NROW(LEVEL)
C
WRITE(LP,10)LEVEL
C
DO 400 L=1,LMAX
C
  NBLANK=(LEFT(JP1)+1)
  NCHAR=RIGHT(JP1)-LEFT(JP1)+1
  KMIN=LLOC(JP1)
  KMAX=RLOC(JP1)
  NPI=1
C
  DO 300 KPI=KMIN,KMAX
C
    NUM=AINT((Z(KPI)-ZMIN)*ZFACT)+1
    IF(NUM.GT.KINI)NUM=KINI
    LINE(NPI)=CHAR(NUM)
    NPI=NPI+1
300 CONTINUE
C
  IF(LIN(11,33))WRITE(LP,20)(BLANK,N=1,NBLANK),
    (LINE(N),N=1,NCHAR)
400

```

```

C      HLLIN(X, GL, 33)HRL((LP, 30)(BLANK, N, 1, NBLANK),
C      { (INI(N), N-1, NBLANK)
C
C      JPI:=JPF-1
C
C      600      CONTINUE
C      PRINT THE RANGES OF THE CONTOURS
C
C      WRITE((LP, 60)ZMIN, ZMAX
C      ZIN, ZOUT, FOAT(KINI)
C
C      DO 600 NUM, 1, KINI
C      Z1=FLOAT(NUM)*ZLEN/ZMIN
C      WRITE(11, 50)CHAR(NUM), Z0, Z1
C      Z0=ZMIN
C
C      600      CONTINUE
C
C      RETURN
C
C      10      ORHAL((//6X, '--- PI01 -- (LVI1, 15, '1')
C      20      ORHAL((1X, 60A2)
C      30      ORHAL((1X, 120A1)
C      40      ORHAL((16X, 'CONTOUR RANGES'//?IX, 'ZMIN, ZMAX', 2E20, 7)
C      50      ORHAL((16X, A1, 5X, ((20, I, '--', (20, I, 7)
C
C      END

```

2

VITA

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Master of Science

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