

# Stochastic simulation of an aggregated model of the Italian economy: methodological and empirical aspects

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1976

Online at https://mpra.ub.uni-muenchen.de/28944/ MPRA Paper No. 28944, posted 23 February 2011 20:50 UTC

Stochastic Simulation of an Aggregated Model of the Italian Economy: Methodological and Empirical Aspects

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# Preface

The IBM Scientific Center of Pisa, the University of Pisa and the University of Siena have been carrying on a research on Stochastic Simulation of Econometric Models.

The first results have been summarized at the 2nd Meeting on «Teoria dei Sistemi ed Economia», Udine, October 1975, in the paper «Simulazione Stocastica ed Analisi di un Modello Aggregato dell'Economia Italiana» (Stochastic Simulation and Analysis of an Aggregated Model of the Italian Economy).

The following Technical Reports present in detail the methodological aspects and the complete results of the research:

C. Bianchi, «Comparison of Alternative Estimates of an Aggregated Model of the Italian Economy», Technical Report CSP031/513-3541.

P. Corsi, «Eigenvalues and Multipliers of Alternative Estimates of an Aggregated Model of the Italian Economy», Technical Report CSP032/513-3542.

E. Cleur, «Spectral Analysis of an Aggregated Model of the Italian Economy», Technical Report CSP033/513-3543.

G. Calzolari, T.A. Ciriani, P. Corsi,

«Generation and Testing of Pseudo-RandomNumbers with Assigned Statistical Properties to be Used in the Stochastic Similation of Econometric Models», Technical Report CSP034/513-3544.

C. Bianchi et alii,

«Stochastic Simulation of an Aggregated Model of the Italian Economy: Methodological and Empirical Aspects», Technical Report CSP035/513-3545.

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# 1. Introduction

The methods used during the identification stage of econometric models generally involve the use of linear structures in the parameters so that economic systems of the usual form may be represented by mathematical models of the following type:

$$\begin{cases} Ay_t + By_{t+1} + Cx_t + Mz_t = \epsilon_t \\ Z_t = Nf(y_t, y_{t+1}, x_t) \end{cases}$$
 (1)

in which A, B, C, M, N are coefficient matrices,  $y_t$ ,  $y_{t+1}$ ,  $x_t$ , endogenous, lagged endogenous and exogenous variable vectors respectively,  $z_t$  a vector of non-linear functions of these different types of variables,  $\varepsilon_t$  a vector of stochastic variables (disturbances) with zero mean and variance-covariance matrix  $\Sigma$ .

In econometrics, the term simulation means the solution of a type (1) mathematical model, in which the values of the current endogenous variables are the unknowns, once the estimated values of the parameters of the model and the actual or expected values of the exogenous variables have been assigned.

Simulation is said to be deterministic when each disturbance therein is equal to its expected value, that is zero.

Simulation is said to be stochastic when a randon disturbance taken from a multivariate distribution assigned a priori is attributed to each structural equation in the model.

There is obviously no guarantee that when a single shock is applied in a replication of stochastic simulation it gets any closer to the real value of the disturbance than when the shock applied is equal to the expected value of the disturbance in question.

At all events, the fundamental characteristic of stochastic simulation is that by executing a given number of replications, it is possible to statt studying the empirical distributions of the solutions yielded by the type (1) class of models.

From the inferential aspect, there is immediate justification for adopting simulation methods for studying this class of models, when their statistical properties cannot be ascertained by direct deduction.

By analyzing the distributions of the solutions obtained by simulation, it is possible to ascertain whether or not the values observed relate to the population illustrated by a given model.

As regards the use of such models, via stochastic simulation tecniques it is possible to define confidence intervals for forecasts and for the results of alternative economic policy measures, thus reintegrating-from the decision aspect also - the probabilistic element which disappears, so to speak, in economic models after being determined during the estimation stage. [7].

In the case of non-linear models, simulation is the only practicable way of obtaining these distributions [6].

For linear models, useful information can be obtained by analytical means also (1), but it should be noted that analytical methods generally call for calculation of the eigenvalues of the characteristic equation of a system, and this may raise difficulties that cannot be resolved immediately in the more complex systems.

The order of the characteristic equation is defined by «mp», where «m» represents the number of equations and "p» the extent of the maximum lag relating to endogenous variables.

Where «m» = 30 (size of an average national economy model) and «p» = 3, the number of characteristic roots is about 90. The degree of accuracy

<sup>(1)</sup> See writings on this subject by E. Cleur [1] and P. Corsi [3] in which the model constituting the subject of the present research is studied via the techniques of spectral analysis and dynamic analysis respectively.

required for calculation of the strategic roots may exceed the precision of the available algorithms (1).

In conclusion, for both non-linear and linear models the use of Montecarlo methods is justified for studying complete solutions of the systems used in economic applications.

Via analysis of a small model of the Italian economy, we aim in the article to demonstrate the use of Montecarlo methods in applications of this kind. We shall limit our considerations to the case of linear models only, laying emphasis on the characteristics of the method used and on its practical limitations, which are more obvious in linear models.

2. Some summary measures of the dicrepancy between deterministic solution and stochastic mean.

In the case of a linear model, (1) is simplified, in the sense that there is no «z» vector of non-linear functions. The structure is error-additive, not only in its structural form, but in the reduced and final forms also. This means that it is possible to separate the contribution of the deterministic part of the system from that of the stochastic part.

In all practical applications based on a limited number of replications, the discrepancy between the deterministic solution and the stochastic mean for a linear model depends entirely on this experimental factor.

As stated, for a linear model (1) may be rewritten as follows:

$$Ay_r + By_{r+1} + Cx_r = \varepsilon_t \tag{2}$$

If it is assumed as at the estimation stage that:

$$\mathbb{E}\left(\epsilon_{t_{i}}\right) = 0 \qquad \qquad \mathbb{E}\left(\epsilon_{t_{i}} \cdot \epsilon_{t_{j}}\right) = \begin{cases} \sum_{i} t_{i} = t_{j} \\ 0 \quad t_{i} \neq t_{j} \end{cases}$$
 (3)

the solution is given by:

$$y_r = -A^{-1} \left\{ By_{r+1} + Cx_r \right\} + v_r$$
 (4)

where: 
$$v_i = A^{-1} \epsilon_i$$
 (5)

with: 
$$E(v_i) = 0$$
  $E(V_{t_i} \cdot V'_{t_j}) = \begin{cases} \Omega = \Lambda^{-1} \Sigma (A'^1)' & t_i = t_j \\ 0 & t_i \neq t_i \end{cases}$  (6)

The experimental discrepancy between the stochastic mean and the deterministic solution for the model considered, with 20(1) replications, is illustrated in tables 3 - 16 of section 3 hereunder. Brief analysis of the columns relating to the two types of solution reveals an average 2% discrepancy.

To illustrate the extent of the error committed by using a fairly limited number of replications (20 in our example), in table 1 we have compared certain indices for the deterministic solution and for the stochastic mean. For this, the stochastic solution was obtained by means of the McCarthy algorithm [9]. The following indices were used:

a) RMSE, root-mean-square error between observed values O<sub>t</sub> and calculated values C<sub>t</sub>

$$RMSE = 0 \quad \text{if} \quad C_t = O_t$$

$$RMSE = 1 \quad \text{if} \quad \begin{cases} C_t = O_t \\ C_t = 2O_t \end{cases}$$

$$RMSE = 1 \quad \text{if} \quad \begin{cases} C_t = 0 \\ C_t = 2O_t \end{cases}$$

$$RMSE -> \infty \quad \text{if} \quad C_t >> O_t$$

<sup>(1)</sup> See the writings on this subject by P. Howrey [5] and K. Mori [10], giving different results for calculation of the characteristic roots of an identical condensed version of the Wharton model. See also the difficulties met by P. Corsi [3] in calculating the spectrum of eigenvalues for the versions of this model, estimated using the single-equation and full-information maximum likelihood methods.

<sup>(1)</sup> The number of replications was established bearing in mind the information given in [12, page 209] regarding the non-parametric tolerance interval and the values used in similar stochastic simulation experiments (see [2], [4], for example).

b) Theil inequality coefficients:

$$T_{t} = \frac{\sum (c_{t} - o_{t})^{2}}{\sum o_{t}^{2}}$$

$$T_{t} = 0 \qquad \text{if } o_{t} = c_{t}$$

$$= 1 \qquad \text{if } c_{t} = 0$$

$$T_{2} = \frac{\sum (c_{t} - o_{t})^{2}}{\sum (o_{t} - o_{t+1})^{2}} \qquad \text{if } o_{t} = c_{t}$$

$$= 1 \qquad \text{if } c_{t} = o_{t+1}$$

where:

 $c_t$  = annual percentage variation of calculated values (deterministic or mean stochastic) between periods t and t-1.

ot = annual percentage variation of observed values between period t and t-1.

The value of each of these two statistics is zero when both the size and sign of the variables are accurately predicted.

 $T_1$  has a value of 1 when no variation is predicted;  $T_2$  has a value of 1 when one variation is predicted, equal to that of the previous year. Values higher than 1 are a clear indication of less accurate forecasting capacity than that of the previous formulae [13].

c) Regression coefficients of the model;  $C_{st} = \alpha + \beta C_{dt} + v_{t}$  where  $C_{st}$  are the realizations of the stochastic simulation at different periods, and  $C_{dt}$  the results of the deterministic simulation. When there is no systematic correlation between the forecasting errors and the values predicted (efficient forecasting):  $\beta = 1$ .

If the forecast is both efficient and correct, it follows that:  $\alpha = 0$ .

Alongside the values of the coefficients are indicated the values generated by test F on the combined zero hypothesis ( $\alpha = 0$ ,  $\beta = 1$ ) and those of the separate "t" tests on the unbias and efficiency hypotheses. For all variables, these hypotheses are not rejected in 95% of cases.

The RMSE values are satisfactory for all variables in any case, as the highest value is .06226 (ILIT); on the other hand, the values of the Theil inequality coefficients tend to be high, even over 1 for KOCC (T1S) and CPN, RNLCF (T2S).

As already stated, the previous results provide indications as to the experimental discrepancy (due to the small number of replications) between the

ummary measurements - McCarthy's Algorithm

|      |        |                             |       |        |   |              |                                   | <br>  | Regression                              | . هر        |       |
|------|--------|-----------------------------|-------|--------|---|--------------|-----------------------------------|-------|---|-------------|-------|
|      | ~      | RMSE                        |       | Ĩ.     | :-  | 2            |                                   |       | ביים ביים ביים ביים ביים ביים ביים ביים | ر<br>ا<br>ا |       |
|      | Det.   | Stoch.                      | Det.  | Stoch. | Det. Stoch, Det. Stoch, Det. Stoch,           | Stoch.       | ö                                 | a     | ە<br>-                                  | ړ           | ā     |
| CPN  | .02215 | .02456                      | .5346 | .5883  | .02215 .02456 .5346 .5883 1.0376 1.1418       | 1.1418       | -7.869 1.0014 3897610939 236.3    | .0014 | 189761.                                 | 0939        | 236.3 |
| ILIT | .05873 | .05873 .06226 .6440 .7355   | .6440 | .7355  | .7172 .8190                                   | .8190        | -18.113 1.0091 593045087 95.89    | .0091 | 59304.                                  | 5087        | 95.8  |
| ×    | .05269 | .05269 .06043 .6980 .8296   | 0869  | .8296  | .5825 .6923                                   | .6923        | -28.421 1.0109 72413,9427 143.69  | .0109 | 72413.                                  | 9427        | 143.0 |
| WIT  | .02241 | .02241 .02538 .4084 .4881   | 4084  | .4881  | 8689  | .8689 1.0383 | 9.872 1                           | .0005 | 9.872 1.0005 4020033157 327.7/          | .3157       | 327.  |
| KOCC | .02697 | KOCC 02697 02809 9223 10291 | 9223  | 10201  | 7065  | .7065 .7883  | 569 1                             | .0071 | -,569 1.0071 262799,0937 15.0           | 0937        | 15.0  |
| PJT  | .03020 | PJT03020 .03115 .6105 .5967 | .6105 | .5967  | 9358  | 9358 9148    | 16.301 0.9981 214579. 3381 183.6  | 9981  | 214579.                                 | 3381        | 183.  |
| KE:  | .01254 | .01330                      | .3362 | 3509   | RMLCF .01254 .01330 .3362 .3509 1.0027 1.0463 | 1.0463       | 18.459 0.9999 1280128. 3134 465.3 | 6666  | 1280128                                 | .3134       | 465   |

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Table

deterministic solution and the stochastic mean. In order to have information regarding the variance-covariance matrix of the results of stochastic simulation, comparison was drawn between the theoretical variance-covariance matrix of reduced form  $A^{-1}\Sigma(A^{-1})'$  and the variance-covariance matrix calculated with 20 replications for each year of the sample period 1952-71, indicated in the table as  $\hat{v}_t\hat{v}_t$ .

It will be seen from Table 2 that in the particular case of 20 replications, the percentage error on variances is 5% on average; in the experimental approximation of the convariances, however, the variability is greater.

Later in this study, we shall give closer attention to the problem of experimental error in relation to the number of replications, comparing the results obtained with the two error-generating algorithms used (Nagar and McCarthy) (see section 3).

Comparison between theoretical and calculated variance-covariance matrix

Table 2

| 137.80 | 99:-   | 19.23  | 49.31                        | - (154              | 68.59 | 117.90 | 129.01 | 1.66   | 23.16 | 44:37       | .051 | 63.13 | 107.53 | -6.38  | -349.63 | 20.40        | 66 6- | 99'9- | 76.7- | -8.81 |
|--------|--------|--------|------------------------------|---------------------|-------|--------|--------|--------|-------|-------------|------|-------|--------|--------|---------|--------------|-------|-------|-------|-------|
| 17.47  | -20.17 | -11.29 | -3.19                        | 35                  | 71.78 |        | 74.69  | -19.77 | -8.20 | -5.39       | 36   | 68.51 |        | -3.58  | -2.00   | -27.39       | 68.92 | 889   | 4.56  |       |
| 16     | .42    | .31    | .29                          | 900                 |       |        | 18     | .42    | .28   | .30         | 900. |       |        | 15.82  | .81     | -10.40       | 2.00  | 1.91  |       |       |
| 60.33  | 19.51  | 30.53  | 52.49                        |                     |       |        | 54.31  | 21.43  | 31.36 | 49.76       |      |       |        | 86.6-  | 9.84    | 2.71         | -5.21 |       |       |       |
| 41.61  | 28.42  | 50.79  |                              |                     |       |        | 43.80  | 26.78  | 47.42 |             |      |       |        | 5.27   | -5.74   | -6.62        |       |       |       |       |
| -11.72 | 39.48  |        |                              |                     |       |        | -9.34  | 37.78  |       |             |      |       |        | -20.38 | -4.92   |              |       |       |       |       |
| 191.13 |        |        |                              |                     |       |        | 182.15 |        |       |             |      |       |        | 7.4    |         |              |       |       |       |       |
|        |        |        | 0 - 4 - 1 8 (4 - 1 V - 10) v | v 01 = ( v) 7 v = 7 |       |        |        |        |       | ŶŶ~=O*=10³× |      |       |        |        | , û,    | "<br> <br> - | 25    |       |       |       |

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# 3. Stochastic simulations over the sample period.

The results of the stochastic simulations carried out for the sample period (1952-1971) in relation to the model [11] - with coefficients estimated via the O.L.S. method, 20 replications, Nagar and McCarthy error generating algorithms - are given in the following tables (Tables 3 - 16).

For the sake of clarity, the results obtained with the two algorithms used are shown in separate tables. In addition to the values observed, the deterministic solution and the stochastic mean, each table also gives the following values:

- a) minimum and maximum value of the stochastic solution in the 20 replications;
- b) standard deviation in the stochastic solution;
- c) comparison between the annual percentage variation in the observed values, in those calculated deterministically and in the stochastic mean value.

The minimum and maximum values which define the stochastic simulalation interval, provide an immediate indication as to whether the sample values belong to the population described by the model. This representation is indicated on the graph, by way of example, to show the solutions obtained with the McCarthy method, which is the one most written about 113.

Via the standard deviations in the stochastic solution it is naturally possible to define a confidence interval in relation to the solution of the model. In the case of linear models, this interval is a constant value for all endogenous variables and, as illustrated in the previous section, it can be defined a priori on the basis of linear transformation of the variance-covariance matrix of the structural errors. It may be seen from the standard deviation columns of tables 3 - 16 that there is marked experimental variability which is due to the small number of replications adopted. In this case, the most advisable solution is that of relating the standard deviation mean calculated for the sample period to each endogenous variable or, better still, estimating the variance on all sample data.

In non-linear models on the other hand, the variability of the standard deviation is intrinsic and it constitutes one of the aspects regarding which stochastic simulation is most useful.

Likewise, the third index, which relates to the annual percentage variations and is also significant in the analysis of turning points in the economy, is not of great importance in the stochastic simulation of linear models (in such cases, in fact, it is merely a measure of the experimental discrepancy between the deterministic solution and the stochastic mean, which we have already analyzed more thoroughly in relation to Table 1). The index becomes essential, however in the dynamic solution of non-linear models.

On the basis of examination of the indices, there is little to add regarding the rotal verification of the model used. The structure involved has already been amply tested (1). The confidence intervals revealed by the stochastic simulation are too wide to be used in any application of economic policy. This is also a consequence of the very aggregative structure of the model and does not therefore make the experiments recorded any less valid as examples.

It is clear from the results that, if it is necessary to limit the number of replications for cost reasons, it is also necessary to exercise a certain care in using the results of stochastic simulation. In view of the importance of this problem, in the next section we show a number of results in terms of both mean and variance, in which the number of replications ranged from 20 to 300.

<sup>(1)</sup> See writings on the subject by E. R. Sowey [12], J.P. Cooper, B.Fisher [2], G.R.Green [4], etc.

<sup>(1)</sup> See writings on the subject by E. Cleur [1] and P. Corsi [3].

REPLICATIONS 20 YPAR 1971 WETH S. PROM YEAR 1952 OUTPUT FOR YARIABLE Y ( 1)

| MEAN STOC<br>K CHANGE | 0.       | 6.93     | .08      | , 76     | 3.65       | ٠ <u>١</u> | . 24     | . 52      | . 32     | .89      | 64.        | . 29     | 6.42     | . 17     | F 77 .   | - 9.2    | . 53     | . <del>.</del> | , 19     | <b>117</b> |
|-----------------------|----------|----------|----------|----------|------------|------------|----------|-----------|----------|----------|------------|----------|----------|----------|----------|----------|----------|----------------|----------|------------|
|                       | 0        | ٥        | 0        | ,        | <u>~</u> ر | Ś          | <b>.</b> | 'n        | œ.       | -T       | <u>د</u> ک | ~        | •        | 3        | <u> </u> | ~        | S        | 30             | ~        | 2          |
| DETERM.<br>K CHANGE   | 0.0      | 4.77     | 2.79     | 7.31     | 3.08       | 6.20       | 2.63     | 4.64      | 0.40     | 5.92     | 5.40       | 3.57     | 5.63     | 3,55     | 3.52     | 4.57     | 5.74     | 7.64           | 2.70     | 08.1       |
| ACTUAL<br>A CHANGE    | 0.0      | 5, 39    | 1.82     | 3.65     | 5.63       | 3.50       | 3.50     | 4.7}      | 5.39     | 6.19     | 5.78       | 7.14     | 1.66     | 3.05     | 7.22     | 7.60     | 4.6B     | 94.46          | 6.55     | 67.0       |
| MAXINDA               | 12192.93 | 13152.20 | 13263.78 | 13898.83 | 14564.16   | 15315.31   | 16517.25 | 17138.88  | 17920.12 | 18957.11 | 20128.07   | 20791.66 | 22012.95 | 22843.21 | 01.01686 | 24384.09 | 25415.47 | 27882.04       | 28379.92 | 30014.31   |
| HOMIKIH               | 10964.11 | 11935.22 | 11693.45 | 12782.93 | 13346.94   | 13673,16   | 14096.82 | 15239 32  | 16697.04 | 17664.91 | 18370.99   | 18900.43 | 20068.56 | 20802.37 | 21713.74 | 22645.86 | 24137.19 | 25801.91       | 27066,80 | 28289.56   |
| STANDARD<br>DEVIAT.   | 294.00   | 341.12   | 417.78   | 298.91   | 346.60     | 411.69     | 607.99   | 515.04    | 332.71   | 373.42   | 390.25     | 468.33   | 479.36   | 455.75   | 4 32,80  | 502.58   | 123.19   | 484,37         | 419.50   | 450.42     |
| MEAN STOC.            | 11612.20 | 17416.72 | 12406.59 | 13368.93 | 13856.51   | 14598.43   | 15217.39 | 16.057.07 | 17393.18 | 18243.02 | 19244.20   | 19685.74 | 20950.50 | 21823.55 | 22580.52 | 21466.39 | 24763.15 | 26789.93       | 27643.78 | 29147.38   |
| DETPRK,<br>Value      | 11634.22 | 17188 90 | 12528.79 | 13445.73 | 13859.36   | 14718.54   | 15105.08 | 15806. 19 | 17212,83 | 18232.17 | 19215. P2  | 19901.48 | 21022.27 | 21767.08 | 22533.97 | 23564.32 | 24916.19 | 26819.14       | 27544.03 | 28866.67   |
| ACTUAL<br>VALUE       | 12017 40 | 12650 60 | 12895.00 | 13365.80 | 14117.70   | 14612.50   | 15124.60 | 15840.20  | 15694.00 | 17727.20 | 18751.90   | 20090,00 | 20422.80 | 21045.30 | 22565.10 | 24279.40 | 25416.70 | 26549.10       | 28288.40 | 28428.07   |
|                       | 19.50    | 200      | 1954     | 6.00     | 1456       | 1957       | 1958     | 1454      | 1960     | 1961     | 1962       | 1963     | 1961     | 1965     | 1966     | 1961     | 1968     | 1969           | 1970     | 1971       |

Table 3 : Results of stochastic simulation for the variable CPN (Mc Carchy's algorithm)

20 HEPLICATIONS FEON YEAR 1952 TO TEAR 1971 WITH 5) OUTPUT FOR VANIABLE Y (

| OTO 2401                       | - 5                 | 0.0 | 3.03    |         | cn.7-                                   | 6.11      | 60.6       | ) 10     | 000      | 10.01         | -5.04                                   | 14.23    | ( " ( )      | 13.42   | 10.49   | 70.0                                    | 3.35    | -14.58   | ,        | -1.22   | 20.4B    | 11.43    | 7.79    |         | 2.63    | 7.09    |         |       |
|--------------------------------|---------------------|-----|---------|---------|---|-----------|------------|----------|----------|---------------|---|----------|--------------|---------|---------|---|---------|----------|----------|---------|----------|----------|---------|---------|---------|---------|---------|-------|
| Š                              | DETERM.<br>A CHANGE |     |         |         |   |           |            |          |          |               |   |          |              |         |         | 0.33                                    | 3.18    |          |          | 1.92    | 18.58    | 10.63    | ***     | *       | 5.95    | 77.7    | ,       |       |
|                                | ACTUAL<br>K CHANGE  | •   |         | 5.18    | 6.02                                    | 7.75      |            | \$ . 5b  | 8.89     | -2.74         | 7. 25                                   |          | 15.81        | 16,36   | 6.61    | 707                                     | 16      | 2 /      | - 14.34  | 6.15    | 13.82    | 30.04    | 00.0    | 97.8    | 12.56   | 0 0     |         |       |
|                                | BAXINGE             | G   | 7724.10 | 2672.88 | 93.966                                  | שוני כסשר | 10.2502    | 2661.29  | 2711.83  | 201117        | 7 | 50.0107  | 1186.85      | 3746.98 | 1979 54 | 7 |         | -10.3874 | 3641.74- | 3443 66 | 25.62.72 | 10000    | 4640.03 | 4920.12 | 6167 15 |         | 3243.73 |       |
| 361                            | HINIMUM             | ,   | 1368.32 | 1517 67 | 0 | 00.000    | 18 50 . 49 | 2038.80  | 2167.51  | 7 7 7 7 7 7 7 | 77.07.7                                 | 2306.45  | 2584.52      | 2025 AT | FO 3000 | 00000                                   | 3343.10 | 3473.17  | 2950.17  | 70 6006 | טר יייני | 16 10 14 | 19.6404 | 4118.59 |         | 2       | 4876.08 |       |
| RUN I CAN                      | STANDARD<br>DEVIAT. |     | 200.45  | 000     | 47.007                                  | 195.13    | . 179.69   | 170.31   |          | 01.171        | 207.16                                  | 159.84   | 480 34       | 200     | 203.01  | 176.35                                  | 231.95  | 195.48   | 00 510   | 70.617  | 165.84   | 196.76   | 161.50  | 100 05  | (6.30)  | 247.61  | 176.53  |       |
| VANIABLE Y ( 2) PBUN 15AN 1772 | MEAN STOC.<br>VALUE |     | 3055 52 | 35.007  | 2117.85                                 | 2074.39   | 2201,16    | 7        | 01.1057  | 2421.12       | 2699.21                                 | 2563.26  | 0000         | 2921.00 | 3320.84 | 3669.11                                 | 3670.59 | 1793,51  | 00000    | 1240.19 | 1200.91  | 3856.50  | 4297.43 |         | 40.0.04 | 4872.97 | 5218.51 |       |
| OUTPUT FOR VANI                | DETERM.<br>VALUE    | 1   |         | 1991.49 | 2083.86                                 | 2133.73   | 2218 50    | 0. 18.77 | 74.186.7 | 2498.RB       | 2690,16                                 | 25.70 79 | 77.7.7       | 2920.55 | 3324.45 | 3638.61                                 | 1649.73 | 7765 01  | 2.015    | 3172.05 | 1233.01  | 1833.78  | 11221   | - 77    | 45.665  | 4872.P1 | 5186.78 |       |
| OUTP                           | ACTUAL              | 9   |         | 1809.10 | 1966-50                                 | 2084.80   | 200        | 00.0177  | 2382.70  | 2594.50       | 2523 40                                 | 2000     | 7 / 00 - 3 0 | 3134.60 | 3647.30 | 1886.40                                 | 4171 00 |          | 03.8666  | 3031.50 | 3217.80  | 1662.40  |         | 06.2404 | 4376.60 | 4926.30 | 00.000  | 22.00 |
|                                |                     |     |         | 1952    | 1953                                    | 10.50     | , ,        | 1455     | 1956     | 1457          | 9699                                    |          | 1959         | 1960    | 1961    | 1962                                    | 100     | 100      | 1964     | 1965    | 1966     | 1967     |         | 1958    | 1969    | 1930    |         |       |

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# 20 REPLICATIONS OUTPUT FOR VARIABLE Y ( 3) PROM YEAR 1952 TO YEAR 1971 WITH

|         | ACTUAL<br>VALUE | DETERM.<br>VALUE | MEAN STOC.<br>VALUE | STANDARD<br>DEVENT. | RINIE    | MAXIMUM   | ACTIFAL<br>& CHANGE | DETERM.<br>% CHANGE | KEAN STU<br>K CHANGE |
|---------|-----------------|------------------|---------------------|---------------------|----------|-----------|---------------------|---------------------|----------------------|
| 1952    | 2104.60         | 194.1.79         | 1986.89             | 172.60              | 1445.00  | 21.14-61  | 0 - 0               | ý. 0                | 0.0                  |
| 145     | 2110.80         | 2667.41          | 2148.09             | 217.61              | 1796.03  | 2484 30   | X                   | 5                   | 9 6                  |
| 1954    | 2087.10         | 2070. 16         | 1988.20             | 198.70              | 1583.87  | 2397.57   | 0.70                |                     | 777 -                |
| 1955    | 2244.76         | 2315.43          | 2278.06             | 182.59              | 1951,92  | 2585, 70  | 54.7                |                     | 20° 31°              |
| 1956    | 2528.00         | 2396.20          | 2431.64             | 235.49              | 2075.41  | 2402,58   | 2,62                |                     | 7. 7.                |
| 1957    | 2861.60         | 2632,15          | 2507.69             | 107.93              | 2142.76  | 2852.32.1 | 3.17                | DH 6                | ~                    |
| 1 × 5 × | 2439.70         | 2716.14          | 2741.75             | 275.68              | 2235,90  | 1129. 16- | 4.73                |                     | . ~                  |
| 1959    | 2567.50         | 2793.14          | 2831.34             | 169.40              | 26 18.70 | 3158.30   | 7 74                |                     | 7 2 7                |
| 0961    | 3520.00         | 1338.02          | 1376.19             | 169.09              | 1961,29  | 3708.11   | 7.34                |                     | 14.00                |
| 1961    | 1785.00         | 3751.18          | 1769.58             | 257.90              | 3374.02  | 4370.68   | 7.35                |                     | 11.55                |
| 1967    | 4135,30         | 4118.63          | 4193.45             | 221.29              | 1896.97  | 4728.62   | 9.25                |                     | 11 24                |
| 1463    | 4744.00         | 4244.16          | 4224.05             | 207.55              | 3811.07  | 45 38.50  | 77.77               |                     | 0 73                 |
| サルケー    | 4255.30         | 45.85.14         | 4612.14             | 231.82              | 4172.27  | 5049.85-  | 0.30                |                     |                      |
| 1967    | 4171.70         | 0678607          | 4589.85             | 244.75              | 4251.03  | 5.155.12  | 97                  |                     | , ~                  |
| 9961    | 4739.30         | 4675.K1          | 4653.85             | 228.00              | 4245.96  | 5372.73   | 1.61                |                     | · · ·                |
| 1967    | 5285.00         | 5168.92          | 5099.30             | 227, 38             | 4572.78  | 50 H7 U1  | . 5.1               |                     |                      |
| 1968    | 54.34.00        | 4718.51          | 5737.11             | 191.40              | 0383 40  | 6170.00   |                     |                     |                      |
| 1969    | 6138.10         | 64.68.19         | 6467.88             | 218 64              | 60.00    | 60.000    | 00.                 |                     | 12.21                |
| 1470    | 7383.2C         | 6713 93          | 172 2 6 7 1         | ) i i               | 21.0000  | 24.044.0  | 70.0                |                     | 12./4                |
| 1471    | 6.00.4          |                  | 0.6270              | 201.18              | 16.46.29 |           |                     |                     | 3.95                 |
|         | 11.7660         | 2                | 1373.76             | 224.15              | h862.12  | 7725.21   |                     |                     | 6.67                 |

Table 5 - Results of stochastic simulation for the variable M (McCarthy's algorithm)

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# 20 REPLICATIONS OUTPUT FOR VARIABLE YE 4) FROM YEAR 1952 TO YEAR 1971 WITH

|      | ACTUAL<br>VALUE | DETERM.<br>VALUE | MEAN STOC. | STANOARD<br>DEVIAT. | E DE LE LE | MAKINUM  | ACTUAL<br>X CHANGE | DETERM.<br>X CRANGE | MEAN STO |
|------|-----------------|------------------|------------|---------------------|------------|----------|--------------------|---------------------|----------|
| 1952 | 4551.20         | 4566.75          | 4577.42    | 264.68              | 3759.46    | 4859.62  | 0.0                |                     | 0.0      |
| 1953 | 08.5864         | 43. P. S         | 4931,31    | 162.92              | 4593.99    | 5245.17  | 8.45               |                     | 7.73     |
| 1954 | 5362.60         | 5196.97          | 5148.12    | 238.56              | 4714.41    | 5642.57  | 8.65               |                     | 07.7     |
| 1955 | 5678.70         | 4704,77          | 5725.70    | 168.27              | 5358.57    | 5978.42  | 5.89               |                     | 11.22    |
| 1956 | 0005.10         | 6C30.P2          | 6025.37    | 175.82              | 5739.69    | 6373.56  | 5.75               |                     | 5.23     |
| 1957 | 6420.20         | 6505,81          | 6463.83    | 219.71              | 6078.59    | 6939.25  | 6.91               |                     | 7.23     |
| 1958 | 6718.10         | 6791.22          | 0853.27    | 233,54              | 6445.67    | 7288,16  | 4.64               |                     | 6.07     |
| 1959 | 7221.60         | 7129. ru         | 7164.59    | 189.49              | 6877.12    | 7726.20  | 7.49               |                     | 4.54     |
| 1960 | 7929.00         | 8061.26          | d122.55    | 262.86              | 7717.78    | 8609.21  | 9.80               | 13.08               | 13.37    |
| 1961 | 8639.80         | 8757.32          | 8760.41    | 285.74              | A219.83    | 9362.91  | H. 75              |                     | 7.85     |
| 1962 | 9451.70         | 9431.65          | 9500,26    | 221.00              | 9211.64    |          | Cn. 6              |                     | 3.45     |
| 1963 | 10554.66        | 9996.24          | 9871.94    | 274.51              | 9233.06    |          | 11.66              |                     | 3.91     |
| 1964 | 11055.80        | 10959.43         | 10935.68   | 210.82              | 10555.85   |          | 4.75               |                     | 10.78    |
| 1965 | 10979.00        | 11230.34         | 11284.30   | 227,43              | 10904.82   |          | -0.69              |                     | 3.19     |
| 1966 | 11459.50        | 11536.21         | 11592.17   | 236.19              | 11243.41   |          | 4.38               |                     | 2.73     |
| 1961 | 12573.40        | 12355.65         | 12339.67   | 175.19              | 12108.08   | 12628.63 | 9.72               |                     | 6.45     |
| 1968 | 13534.70        | 13530.22         | 13521.90   | 211.45              | 13102.68   | 13311.07 | 7.41               |                     | 9.58     |
| 1969 | 14340.20        | 14702. P6        | 14735.68   | 228.14              | 14368.05   | 15237.41 | 6.19               |                     | 8.98     |
| 1970 | 16150.00        | 15734.20         | 15757.59   | 255.08              | 15313.84   | 16297.61 | 12.62              |                     | 6.93     |
| 1971 | 17118.04        |                  | 17631.19   | 156.82              | 17197.00   | 17959.73 | 5-99               | 11.76               | 11.90    |
|      |                 |                  |            |                     |            |          |                    |                     |          |

20 REPLICATIONS OUTPUT POR VAKLABLE Y ( S) PROM YEAR 1952 TO YFAR 1971 WITH

|      | ACTUAL | DETPRM.<br>VALUE | MEAN STOC. | STANDARD<br>DEVEAT. | MININIM | MAXINUH | ACTUAL<br>X CHANGE | DETERM. | MEAN STO |
|------|--------|------------------|------------|---------------------|---------|---------|--------------------|---------|----------|
| 1952 | 98.70  | 90.40            | 96.04      | 3.27                | 81.91   | 96.85   | 0.0                |         | 0.0      |
| 1453 | 88.90  | 90,61            | 91,05      | 2.77                | 85.50   | 96.87   | 0.23               |         | 0.10     |
| 1954 | 90-20  | 96.74            | 89.68      | 2.38                | 84.10   | 93,36   | 30.1               |         | -1.51    |
| 1955 | 06.06  | 96.30            | 90.36      | 2.21                | 85.66   | 96.03   | 0.78               | -0.0-   | 0.76     |
| 1956 | 04.06  | 90.54            | 74.06      | 2, 10               | 86.70   | 01.46   | -0.55              |         | 0.13     |
| 1957 | 90.20  | 9n.u2            | 89.97      | 1.94                | 86.33   | 95.09   | -0.22              |         | -0.56    |
| 1958 | 87.BC  | 46.64            | 96.06      | 2.44                | 86.96   | 94.75   | -2.66              |         | 1.10     |
| 1959 | 89.80  | 86.38            | 88.81      | 1,99                | 85.14   | 92,63   | 2.28               |         | -2.37    |
| 1960 | 09.16  | 10 to            | 91.05      | 2.28                | 86.69   | 94.50   | 5.15               |         | 2.53     |
| 1961 | 94.60  | 40.10            | 92.10      | 2,52                | 88.55   | 91.19   | 0.0                |         | 1.16     |
| 1962 | 94.76  | 91.64            | 92.08      | 2.40                | 87.84   | 97.02   | 0.11               |         | -0.03    |
| 1963 | 95.60  | 89.73            | 89.63      | 2.98                | 86.67   | 99.28   | 0.95               |         | -2.65    |
| 1964 | 89.10  | 89.29            | 89.53      | 2.68                | 85.02   | 94.92   | -6.80              |         | -0.11    |
| 1965 | 85.70  | 85.73            | 86.36      | 2,72                | 82.20   | 69.06   | -3.82              |         | - J. S.t |
| 9961 | 89.10  | 88.47            | 88.24      | 1.06                | 85.73   | 90.80   | 3.97               |         | 2.17     |
| 1967 | 91.16  | 87.78            | 93.11      | 2.38                | 88.45   | 97.41   | 2.24               |         | 5.51     |
| 1968 | 91.90  | 93.74            | 87.76      | 2.37                | 88.24   | 98.50   | 0.88               |         | 1.47     |
| 1969 | 91.76  | 93.49            | 93.71      | 2.70                | 86.33   | 98.36   | -0.22              |         | -0.81    |
| 1970 | 94,36  | 91,15            | 92.72      | 3.09                | 85.70   | 48.69   | 2.84               |         | -1.06    |
| 1971 | 87.60  | 93.17            | 92.99      | 1.86                | 69.02   | 96.82   | -7.10              |         | 0.29     |
|      |        |                  |            |                     |         |         |                    |         |          |

Table 7 - Results of stochastic simulation for the variable KOCC (McCarthy's algorithm)

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| 20 REPLICATIONS     |
|---------------------|
| 1971 WYTH           |
| TO YEAR             |
|                     |
| ROH YEAR 1952       |
| Y (6) F             |
| VERIABLE            |
| OUTPUT FOR VARIABLE |

|       | ACTUAL   | DFTFRM.<br>Value | MEAN STOC. | STANDARD DEVIAT. | RININIR  | MAXIMUR  | ACTUAL<br>A CHANGE | DETERM. | MEAN STO |
|-------|----------|------------------|------------|------------------|----------|----------|--------------------|---------|----------|
| 1952  | 6138 00  | 42 5002          | 01 6005    | טני ניינ         | u585 23  | 5578.95  | 0.0                | 0.0     | 0.0      |
| 200   | 5261.60  | 0.000            | 51.86.26   | 20.50            | משינשנים | \$629.08 | 2.47               | 0.86    | 2.62     |
| 1954  | 5395,50  | 5260-71          | 5210.17    | 238.84           | 4879.52  | 5622.02  | 2,54               | 4.16    | 1.40     |
| 1955  | 5820,20  | 5779.95          | 5708,12    | 227.86           | 5307,91  | 6219.37  | 78.6               |         | 95.6     |
| 1956  | 6098.10  | 5947.77          | 5931.57    | 248.88           | 5513.03  | 6323.53  | 4.77               | 2.40    | 3.91     |
| 1957  | 6473.80  | 6627.44          | 6629.62    | 267,76           | 6186.22  | 7011.68  | 6.16               |         | 11.77    |
| 1958  | 0635.60  | 6437.15          | 6467.08    | 322,94           | 5900,85  | 7111.93  | 2.50               |         | -2.45    |
| 1959  | 7295.90  | 7002.48          | 7163.12    | 308,75           | 6598.05  | 7948.55  | 9.95               |         | 10.76    |
| 1960  | 7918.30  | 8278. P.B        | 8367.11    | 224,26           | 8082.13  | 8878.79  | 8.53               |         | 16.81    |
| 1961  | 8373.00  | 8469.36          | 8457.28    | 212.01           | 7983.12  | 8836.07  | 5.74               |         | 1.08     |
| 1962  | 8608.80  | 8859.74          | 8775.21    | 243,59           | 8201.93  | 9451.79  | 2.82               | 4.61    | 3.76     |
| 1963  | 3644.00  | 8991, 84         | 8941.37    | 297,64           | BC48.07  | 9422.50  | 0.41               | 1,49    | 1.89     |
| 1961  | 8728.80  | 9321.50          | 9274.27    | 275.25           | 8892.19  | 6940.47  | 96.0               | 3.67    | 3.72     |
| 1965  | 9368.70  | 9659.10          | 9632.45    | 257.58           | 8983,46  | 9987.54  | 7.33               | 3.62    | 3.86     |
| 1966  | 10258.10 | 10234.33         | 10209.51   | 206.81           | 9753.66  | 10552.86 | 67.5               | 5.96    | 5.99     |
| 1967  | 10851.50 | 10641.23         | 10652.54   | 276,99           | 10096.04 | 11076.12 | 5.78               | 3.48    | 4. J4    |
| 196 H | 11910.30 | 11299.64         | 11192.21   | 221,90           | 10604.19 | 11518.54 | 9.76               | 6.18    | 70.5     |
| 1969  | 12659.20 | 12659.27         | 12608.73   | 273.93           | 12174.67 | 13184.69 | 6.29               | 12.03   | 12.66    |
| 1970  | 12831.56 | 12807,52         | 12874.30   | 250.50           | 12434.95 | 13281.53 | 1.36               | 1.17    | 2.11     |
| 1971  | 12038.20 | 11958, 19        | 12063.33   | 351.35           | 11431,52 | 12625.70 | -6.18              | -6.63   | -6.30    |
|       |          |                  |            |                  |          |          |                    |         |          |

REPLICATIONS 20 1952 TO YEAR 1971 WITH PROM YEAK ~ CUTPUT FOR VARIABLE Y (

|       | ACTUAL<br>VALUE | DETERM.<br>Valuf | MEAN STOC.  | STANDARD DEVIAT. | RINIROM   | FAXIMUM  | ACTUAL<br>A CHANGE | DETERM. | MEBN STOC. |
|-------|-----------------|------------------|-------------|------------------|-----------|----------|--------------------|---------|------------|
| 1952  | 15042.cc        | 14927.22         | 14940.13    | 276.78           | 14445.41  | 15665.95 | 0.0                | 0.0     | 0.0        |
| 1953  | 16101.00        | 15792.15         | 15973.28    | 248.84           | 15710.57  | 16716.06 | 7.04               | 5.82    | 6.92       |
| 1954  | 16629.00        | 16328,45         | 16229.08    | 375.03           | 15605.83  | 17056.62 | 3.28               | 3.40    | 1.60       |
| 1955  | 17728.60        | 17714.79         | 17662.92    | 200.33           | 17284.90  | 17494.28 | 6.61               | 8.49    | n 8 ⋅ b    |
| 1956  | 18511.00        | 18386.26         | 18 36 4. 64 | 283.37           | 17906.79  | 18773.14 | 4.42               | 3.79    | 3.97       |
| 195.7 | 19485.00        | 19724.27         | 19681.46    | 304.67           | 19072.79  | 20156.63 | 5.26               | 7.28    | 7.17       |
| 1958  | 20442.00        | 20118.Py         | 20408.66    | 444.04           | 19549.63  | 21488.42 | 4.91               | 3.01    | 3.69       |
| 1459  | 21822.00        | 21435.90         | 21632.08    | 382.62           | 21003.68  | 72458.81 | 6.75               | 5.50    | 5.99       |
| 1960  | 23122.00        | 23614.86         | 23764.37    | 274.79           | 23240.95  | 24172.41 | 5.96               | 10.16   | 9.86       |
| 1961  | 20944.00        | 25157, Au        | 25148.88    | 296, 43          | 24624.99  | 25783.42 | 7.88               | 6.53    | 5.83       |
| 1962  | 20436.00        | 25666.74         | 26650.86    | 241,21           | 26325.93  | 27148.82 | 5.98               | 6.00    | 5.97       |
| 196 3 | 27830.00        | 27590.50         | 27415.27    | 373,89           | 26927.65  | 28351.25 | 5.16               | 3.46    | 2.87       |
| 1904  | 24625.00        | 29121,73         | 29050.57    | 356.90           | 28289.58  | 29799.16 | 2.97               | 5.55    | 5.46       |
| 1965  | 29674.00        | 30215.73         | 30242.99    | 351,86           | 29375.85  | 10948.26 | 3.66               | 3.76    | 4.10       |
| 1966  | 31431.00        | 31483.87         | 31515.08    | 345.44           | 30724.21  | 12138.61 | 5.92               | 4.20    | 4.21       |
| 1961  | 33551.00        | 33123.17         | 33117.90    | 340.90           | 32444,38  | 13706.49 | 6.74               | 5.21    | 5.09       |
| 1968  | 35709.00        | 35123,78         | 35008.07    | 268.45           | 34402, 32 | 35513.83 | 6,43               | 6,04    | 5.71       |
| 1969  | 37757.00        | 38119.78         | 3 U 102.06  | 371,01           | 37300.24  | 38791.77 | 5.74               | 8.53    | 8.84       |
| 1970  | 39594.00        | 39162,42         | 39252.64    | 318,38           | 38838, 36 | 39839.14 | 4.87               | 2.74    | 3.62       |
| 1971  | 40241.66        | 40630.94         | 40784.03    | 391,39           | 40016.09  | 41512,32 | 1.63               | 3.75    | 3.90       |
|       |                 |                  |             |                  |           |          |                    |         |            |

Table 9 - Results of stochastic simulation for the variable RNLCF (McCarthy's algorithm)

REPLECATIONS 20 RITH 1971 YEAR 10 PROM YEAR 1952 = **∵** VARIABLE UUTEUT FOR

|      | ACTUAL    | DFTRAM.<br>VAIUE | MEAN STOC.<br>VALUE | STANDARD<br>DEVIAT. | K [ W ] Y   B | PAKINUN  | ACFUAL<br>X CHANGE | DETERM.<br>A CHANGE | MEAN STOC |
|------|-----------|------------------|---------------------|---------------------|---------------|----------|--------------------|---------------------|-----------|
| 1952 | 12017.40  | 11634.22         | 11560.67            | 412.11              | 10844.80      | 12168.23 | 0.3                | 3.3                 | 3.0       |
| 1954 | 12664. b0 | 12188.90         | 12278.19            | 4 10, 74            | 11356.51      | 11134,87 | 5.19               | 4.77                | 0.21      |
| 1954 | 12845.00  | 12528.79         | 12475.51            | 459.70              | 11701,89      | 13698.23 | 1.82               | 7.19                | 1.63      |
| 1955 | 13365.80  | 13445,61         | 13573.32            | 281.58              | 13102.17      | 14422.29 | 3.65               | 1.11                | 9.40      |
| 1956 | 14117.70  | 11854.10         | 11771.65            | 384.19              | 13216.43      | 14744.94 | 5.63               | 3.08                | 1.46      |
| 1957 | 14612.50  | 14718.54         | 14725.19            | 48.54               | 14154.11      | 15447.76 | 3.53               | 6.20                | 25.9      |
| 1958 | 15124.60  | 15165.08         | 14934.01            | 366.31              | 14287,46      | 15914.58 | 04.₹               | 2.63                | 1.42      |
| 1959 | 15840.20  | 15806. 29        | 15723.09            | 386.33              | 14971.60      | 16262.78 | 4.77               | 4.64                | 5.28      |
| 1960 | 16694.66  | 17212.83         | 17334.21            | 351,63              | 16706.45      | 18944.95 | 5.34               | 9.40                | 17.25     |
| 1961 | 17727.20  | 18232.17         | 14330.71            | 417.07              | 17422.32      | 19208.31 | 6.13               | 5.42                | 5.75      |
| 1962 | 18751.90  | 19215.82         | 19194.58            | 512.33              | 18284.21      | 20353.98 | 5.78               | 5.40                | 5.80      |
| 1363 | 20390.00  | 19901.48         | 19966.20            | 446.36              | 19073.69      | 21021.63 | 7.14               | 1.57                | 2,95      |
| 1961 | 23422.80  | 21022.27         | 20915.23            | 387.65              | 19832,36      | 21547.73 | 1.66               | 5-63                | 2.75      |
| 1965 | 21)45.30  | 21767. 90        | 21749.01            | 359,53              | 21071,19      | 22332.48 | 3.05               | 3.55                | 5 T.      |
| 1956 | 22565.10  | 22531,07         | 22722.65            | 382.56              | 21869.39      | 23526.00 | 7.22               | 3.52                | E :       |
| 1967 | 24279.46  | 23564.12         | 23503.94            | 38H.59              | 22601.65      | 24158.26 | 7, 00              | 4.57                | 3 · ·     |
| 1968 | 25416.70  | 24916,19         | 24958.48            | 351.70              | 24416.19      | 25667.28 | 4.6A               | 5.74                | 6.19      |
| 1969 | 26549.10  | 26.819, 14       | 26787.93            | 421.30              | 25837.48      | 27501.40 | 4.46               | 7.64                | 7.33      |
| 1970 | 28288.40  | 27544.01         | 27618.31            | 408.84              | 26893.47      | 28421,42 | 6.55               | 2.70                | 3. 10     |
| 1971 | 28428.07  | 28866.67         | 28861.43            | 449.61              | 28009.07      | 29640.08 | 0.49               | 4.80                | 4.50      |
|      |           |                  |                     |                     |               |          |                    |                     |           |

REPLICATIONS 0.7 MITH YEAR 1911 πO FROM YEAR 1952 ? OUTPUT FOR VARIABLE Y (

|      | AUTUAL<br>VALUE | DETERM,<br>VALUE | MEAN STOC.<br>VALUE | STANDARD<br>DEVIAT. | N CHINE | MAXIMUM  | ACTUAL<br>M CHANGE | DETERM.<br>N CHANGE | MEAN STOC     |
|------|-----------------|------------------|---------------------|---------------------|---------|----------|--------------------|---------------------|---------------|
| 452  | 1303.76         | 1991,43          | 2012,83             | 178.50              | 1725.16 | 2486.29  | 0.0                |                     | 0.0           |
| 453  | 1966.50         | JOR3 PB          | 2006.21             | 211.64              | 1673.91 | 2361.74  | 5.18               |                     | -0.33         |
| 7.5  | 2084.80         | 2133, 73         | 2113.48             | 210.26              | 1738.62 | 2458.15  | 6.02               |                     | 5.35          |
| 958  | 2236.06         | 2214,50          | 2142,58             | 232.61              | 1624.29 | 2469.70  | 7,25               | 3.79                | 1.38          |
| 956  | 2382.70         | 2384.57          | 2330.62             | 141.78              | 1999.73 | 2692.39  | 95.9               | 7.68                | 8.78          |
| 957  | 2594.50         | 2498.88          | 2447.47             | 237.01              | 2007,54 | 3018.88  | 8,89               | 4.79                | 5.01          |
| 95k  | 2523,40         | 260c, 16         | 7574,94             | 189.91              | 2215.90 | 2912.55  | -2.74              |                     | 5.21          |
| 656  | 2706.30         | 2579.79          | 2518,78             | 173.95              | 2176.03 | 2850.87  | 7.25               |                     | -2.18         |
| 960  | 3134.60         | 2920,55          | 2905.17             | 237,50              | 2328,28 | 3343-62  | 15.83              |                     | 15.34         |
| 106  | 3647,30         | 3324,45          | 3348.24             | 248,51              | 2944.75 | 3705.45  | 16.36              | 13.83               | 15.25         |
| 962  | 3888.           | 3638,61          | 1082,37             | 191.54              | 3438.14 | 4354.21  | 6.61               |                     | 9.98          |
| 963  | 4171.00         | 3649.73          | 3654.23             | 204.58              | 3246.78 | 1976.89  |                    |                     | -0.76         |
| 964  | 35.3 B. BC      | 3765.93          | 3832.13             | 190.10              | 3499.65 | 4192.54- |                    |                     | 4.87          |
| 965  | 3031.50         | 2                | 1107.18             | 196, 35             | 2727.59 | 1453.97- | 14.34              | ı                   | -18.92        |
| 966  | 3217.80         | 3233, 61         | 3216.32             | 190.49              | 2822.26 | 3486.93  |                    |                     | 3.51          |
| 767  | 3662.40         | ~                | 1909,30             | 136.82              | 3650.74 | 4240,95  | 13.82              |                     | 21.55         |
| 969  | 4042.50         | 4241.33          | 4277,77             | 224, 74             | 3898,73 | 4726.53  | 10.38              |                     | ð. <b>4</b> 3 |
| 696  | 4176,60         | 45.092 J         | 4562.15             | 211.00              | 4294,92 | 5082.19  | 8.26               | B. L.               | 6.65          |
| 970  | 4 126.36        | 4872.81          | 4819.63             | 184.14              | 4502.40 | 5183.01  | 12.56              |                     | 5.64          |
| 97.1 | 5014.29         | 518F.78          | 5240.40             | 184.67              | 4925,94 | 5683.15  | 1.89               |                     | 8.73          |
|      |                 |                  |                     |                     |         |          |                    |                     |               |

Table 11 - Results of stochastic simulation for the variable ILIT (Nagar's algurithm)

REPLICATIONS 20 HIIM YFAR 1971 ΤO 1952 FROM YEAR 3 **∵** OUTPUT FOR VARIABLE

|      | ACTUAL<br>VALUE | DFTFRK.<br>VAluf | MEAN STOC.<br>VALUE | STANDARD<br>DEVIAT. | MINIMUM | MAXIMUM | ACTUAL<br>% CHANGE | DETERM. | MEAN STOC |
|------|-----------------|------------------|---------------------|---------------------|---------|---------|--------------------|---------|-----------|
| 1952 | 2104.60         | 1961.79          | 1929.14             | 125,59              | 1701.02 | 2205.83 | 0.0                |         | 0.0       |
| 1953 | 2116.80         | 2067,41          | 2006.69             | 195.08              | 1675.51 | 2313.58 | 0.58               | 5.38    | 4.02      |
| 1954 | 2087.16         | 2070.30          | 2075.43             | 223,77              | 1758.54 |         | -1.40              |         | 3.43      |
| 1955 | 2244.7C         | 2315,63          | 2342.50             | 187.77              | 1885.50 |         |                    |         | 12.87     |
| 1950 | 2528.00         | 2396.26          | 2321.58             | 193.53              | 1992.07 |         |                    |         | -0.89     |
| 1957 | 2861.00         | 26 32, 15        | 2598.40             | 231.52              | 2209.94 |         |                    |         | 11.92     |
| 1958 | 2439.70         | 2710.14          | 2539.50             | 262.29              | 1946.81 |         |                    |         | -2.27     |
| 1959 | 2567.50         | 2793. 18         | 27d3.5A             | 172.81              | 2434.29 |         |                    |         | 9.61      |
| 1960 | 1526.00         | 3138.62          | 3354.26             | 173, 11             | 2975.78 |         |                    |         | 20.50     |
| 1961 | 1785.00         | 3753. 14         | 3799.48             | 282.05              | Tr.172F |         |                    |         | 13.27     |
| 1962 | 4135,30         | 4118,68          | 4131.89             | 216.69              | 3665.20 |         |                    |         | 8.75      |
| 1963 | 4744.00         | 4244.16          | 4289.97             | 217,35              | 3933.01 |         | 14.72              |         | 3.83      |
| 1964 | 4255.30         | 4585.19          | 4626.07             | 125,91              | 4345.65 | - 1     | 10.30              |         | 7.83      |
| 1965 | 4171.70         | 4493.20          | 4400.18             | 177, 43             | 4095.56 |         |                    |         | -4.88     |
| 1966 | 4739.30         | 4670,61          | 4722.99             | 212,65              | 4403.37 |         |                    |         | 7.34      |
| 1967 | 5285.00         | 5168.92          | 5202.62             | 244.53              | 4849.52 | 5676.51 |                    | 10.67   | 10.16     |
| 1968 | 54 14,80        | 571R.51          | 5706.42             | 230.72              | 5316,18 | 6218.85 | 2.83               |         | 89.6      |
| 1969 | 6338.10         | 6468.69          | 09.0409             | 271,49              | 5944.00 | 7039.41 |                    |         | 12.47     |
| 1970 | 7083.26         | 6713.00          | 6684,77             | 250.23              | 6213.85 | 7126.24 | 11,71              |         | 3.79      |
| 1371 | 6997.11         | 7214.42          | 7226.08             | 252.2н              | 6811.05 | 7631.41 | -1.17              |         | 8.11      |
|      |                 |                  |                     |                     |         |         |                    |         |           |

| DETERM, MEAN STO<br>% CHANGE % CRANGE | 0.0      | 3.64    | 8.57    | 10.93   |         |          |         |         |         |          |         |          | 9,32     |          |          | 6.62     |          |          |          | 11.80    |
|---------------------------------------|----------|---------|---------|---------|---------|----------|---------|---------|---------|----------|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|                                       | 0.0      | 6.10    | 7.42    | 9.79    | 5.70    | 7.88     | 77.7    | 76° 17  | 13.08   | 8.63     | 7.70    | 5.99     | 9.6      | 2.47     | 2.72     | 7.10     | 9.51     | 8.b7     | 7.31     | 11.76    |
| ACTUAL<br>X CHANGE                    | 0.0      | 8.45    | 8.65    | 5.89    |         |          | ₹       |         | 9.83    |          | 04.6    |          |          | 69-0-    | 4.38     | 9.72     |          |          | •        | 5.99     |
| MAXINUM                               | 4964.85  | 5081.29 | 5661.28 | 6099.43 | 6349.43 | 7178.20  | 7394.21 | 7542.07 | 8416.12 | 9332.39  | 9852.20 | 11279.89 | 11114.27 | 11758.66 | 12300.14 | 12781.15 | 14062,19 | 15191.76 | 16178.26 | 17880.17 |
| RESIDER                               | 4219.51  | 4380.63 | 4785.33 | 5237.22 | 5702.74 | 6013,14  | 6138.05 | 6774.51 | 7574.25 | 8306.80  | 9006.21 | 9598.93  | 10643.18 | 10628.47 | 11333.85 | 11813.12 | 13125,37 | 14275.41 | 15303,28 | 17271.60 |
| STANDARD DEVIAT.                      | 178.94   | 193,75  | 219.66  | 216.15  | 197.00  | 289.64   | 288.39  | 206.20  | 219.73  | 244.47   | 239.74  | 176.16   | 152,84   | 243.11   | 166.69   | 241.55   | 219.87   | 281.41   | 247.45   | 183.21   |
| MEAN STOC.                            | 4598.22  | 4765.62 | 5173.83 | 5739.07 | 5985,10 | 44.6449  | 6685.34 | 7056.55 | 8050.36 | 8810.79  | 9543.86 | 9991.30  | 10922.71 | 11191.67 | 11583.49 | 12350,86 | 13529.74 | 14670.98 | 15744.19 | 17602.30 |
| DETERM.<br>VALUE                      | 4560,064 | 4838,09 | 5196.97 | 5765,77 | 6030,82 | 6505. R1 | 6791.22 | 7129.06 | 8061.26 | 8757, 72 | 9431.65 | 9896.28  | 10959.48 | 11234.38 | 11536.21 | 12355.65 | 13530,22 | 14702.86 | 15734.20 | 17585.6  |
| ACTUAL<br>VALUE                       | 4551,20  | 4935.80 | 5362,66 | 5573.70 | 6205,10 | 6420.20  | 0718.10 | 7221.06 | 7929.00 | 8039.80  | 9451,76 | 10554.00 | 11055.80 | 10974.00 | 11459,50 | 12573.40 | 13504.70 | 14340.20 | 10150.00 | 17118.04 |
|                                       | 1452     | 145.4   | 1954    | 1955    | 1956    | 1957     | 1958    | 1959    | 1960    | 1961     | 1962    | 1963     | 1964     | 1965     | 1966     | 1967     | 1968     | 1969     | 1970     | 1971     |

Table 13 · Results of stochastic simulation for the variable WIT (Nagar's algorithm)

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20 REPLICATIONS POP VARLABLE Y ( 5) FROM YEAR 1952 TO YFAR 1971 WITH いりていり

| 952         88.7C         90.47         1.96         87.30         14.86         0.0         0.0           1953         88.9D         90.76         189.37         2.19         85.63         94.23         0.23         -1.76           1954         90.2C         90.74         89.68         3.26         81.42         95.76         1.46         -0.30         0.58           1955         90.9C         90.74         89.68         3.26         81.27         94.95         0.78         -0.04         0.22           1956         90.4C         90.74         89.68         2.34         85.07         95.81         -0.25         -0.12         -0.47           1956         87.4C         90.26         2.34         85.07         95.81         -0.25         -0.12         -0.14           1958         89.8C         2.34         85.07         95.74         91.76         92.81         -0.13         -0.14           1960         91.74         91.74         91.76         92.81         -0.55         0.24         -0.18         -0.18         -0.18         1.04         -0.18         1.04         -0.18         1.04         -0.18         1.04         -0.18         1.04  |      | ACTUAL<br>VALUR | DETERM.<br>VALUE | KEAN STOC.<br>VALUE | STANDARD<br>DEVIAT. | MINIMIR | MAXIMUM | ACTUAL<br>K CHANGE | OSTERM.<br>K CHANGE | MEAN STOC |
|--|------|-----------------|------------------|---------------------|---------------------|---------|---------|--------------------|---------------------|-----------|
| 88.90         90.61         89.37         2.19         85.63         94.23         0.23           90.20         90.74         89.48         3.02         83.42         95.76         1.46         -0.30           90.90         90.90         90.74         90.91         90.96         97.81         -0.20         90.04           90.90         90.96         91.11         1.71         86.99         93.81         -0.22         -0.04           90.40         90.11         1.71         86.93         93.81         -0.22         -0.12           87.80         90.20         2.57         85.04         92.56         -0.22         -0.12           89.80         91.01         1.81         85.04         92.96         -1.39         1.85           90.56         3.08         81.57         95.34         5.35         1.85         95.34         5.35         1.85           90.60         91.04         90.56         3.08         81.57         95.34         5.35         1.85           90.40         91.64         90.56         3.08         81.52         95.34         5.36         1.85           90.40         91.64         90.56         3.08   | 952  | 38.70           | 00.00            | 40.47               | 1,96                | 87.30   |         |                    |                     | 0.0       |
| 90.20 90.74 89.88 3.02 83.42 95.76 1.46 -0.30 90.90 90.90 90.11 1.71 86.99 93.81 -0.55 0.26 90.90 90.40 90.40 90.11 1.71 86.99 93.81 -0.55 0.26 90.90 90.40 90.40 90.11 1.71 86.99 93.81 -0.55 0.26 90.40 90.20 90.11 1.71 86.99 93.81 -0.55 0.20 90.40 91.64 89.52 2.34 85.45 95.34 5.26 -2.66 0.24 94.60 91.64 90.56 3.08 81.52 95.34 5.38 1.83 91.65 91.64 90.70 91.64 92.22 1.87 85.64 96.45 0.0 11.04 90.75 92.42 83.67 94.30 91.71 89.75 93.71 -6.80 -0.49 85.70 85.77 85.38 2.42 83.67 94.30 91.47 1.90 84.52 93.71 -6.80 -0.49 85.70 85.77 85.38 2.42 83.67 93.71 89.46 -3.82 -3.94 91.90 93.19 13.97 89.75 2.43 84.57 99.54 0.89 1.03 91.70 93.19 93.69 2.70 88.80 97.03 2.84 -0.22 97.70 93.19 93.69 2.40 88.80 97.03 2.84 -0.36 97.03 2.84 -0.36 97.20 93.11 93.69 2.20 88.80 97.03 2.84 -0.36 97.21 0.00 97.01 2.84  | 953  | 88.90           | 90.61            | 89,37               | 2, 19               | 85.63   |         |                    |                     | -1.76     |
| 90.96 90.13 89.68 3.26 83.27 94.95 0.78 -0.04 90.11 1.71 86.99 93.81 -0.55 0.26 90.20 90.40 90.11 1.71 86.99 93.81 -0.55 0.26 90.20 90.20 90.11 1.71 86.99 93.81 -0.55 0.20 90 | 954  | 90.20           | 9C, 74           | 89,88               | 3.02                | 83.42   |         |                    |                     | 0.58      |
| 90,4c 90.54 90.11 1.71 86.99 93.81 -0.55 0.26 90.20 90.20 90.20 90.20 90.20 90.20 90.20 90.20 90.20 90.20 90.20 90.20 90.20 90.20 90.56 3.08 85.74 91.76 2.28 -1.39 91.60 91.74 90.56 3.08 81.52 95.34 5.35 1.85 94.50 91.76 91.64 92.22 1.87 85.64 95.34 5.35 1.04 91.75 91.76 0.0 11 0.03 89.10 89.10 89.67 2.42 83.67 94.39 0.95 -2.08 89.10 89.67 2.43 84.52 93.71 6.80 -0.49 85.70 89.10 81.77 85.38 2.42 84.37 91.47 3.97 3.07 89.10 93.79 93.79 93.79 93.79 93.79 93.79 93.79 93.79 93.79 93.79 93.79 93.79 93.79 93.79 89.80 93.70 93.79 89.80 93.70 89.80 93.70 89.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 88.80 93.70 93.70 88.80 93.70 93.70 88.80 93.70 93.70 88.80 97.03 2.80 97.03 2.80 93.70 93.70 88.80 97.03 2.80 97.0 | 1955 | 90.96           | 61.10            | 89.68               | 3,26                | 83.27   |         |                    |                     | -0.22     |
| 90.20         90.42         89.68         2.57         85.45         92.18         -0.22         -0.12           87.80         90.74         89.52         2.34         85.45         92.56         -2.66         0.24           89.80         89.31         1.81         85.45         92.56         -2.66         0.24           94.60         91.74         90.56         3.08         81.52         95.34         5.35         1.85           94.60         91.61         3.14         85.64         96.45         0.0         1.04           94.76         91.91         3.14         85.64         96.45         0.0         1.04           94.76         91.97         49.79         97.74         0.11         -0.38           89.16         89.75         2.42         83.67         94.39         0.95         -2.08           89.17         89.77         49.39         0.95         -2.08         84.57         94.39         0.95         -2.08           89.16         86.17         2.42         81.52         93.71         60.49         -3.94           89.16         86.37         84.67         2.42         84.37         93.44         -3.94     <   | 9561 | 90,40           | 45° 96           | 90.11               | 1.71                | 86.99   |         |                    |                     | 0.47      |
| 87.80         97.52         2.34         85.45         92.56         -2.66         0.24           89.80         89.34         86.57         1.81         85.74         91.76         2.28         -1.39           94.60         91.74         90.56         3.08         81.52         95.34         5.35         1.85           94.60         91.74         90.56         3.14         85.64         96.45         0.0         1.04           94.70         91.71         92.22         1.87         89.44         96.45         0.03           94.70         89.72         89.67         2.42         83.67         94.39         0.95         -2.08           89.10         89.77         89.67         2.43         84.52         93.71         -6.80         -0.49           85.76         85.34         2.71         79.71         89.46         -3.82         -3.94           85.77         86.41         97.15         2.24         4.95           91.16         97.74         93.46         4.95           91.76         93.74         93.82         94.36         99.54         0.88           94.30         93.11         93.69         2.40  | 1957 | 90,20           | 40.42            | 89.68               | 2.57                | 85.07   |         |                    |                     | -0.47     |
| B9.80         B9.34         B0.57         1.81         B5.74         91.76         2.28         -1.39           94.60         91.74         90.56         3.08         B1.52         95.34         5.35         1.85           94.60         91.91         3.14         85.64         96.45         0.0         1.04           94.70         91.91         1.87         89.64         96.45         0.0         1.04           94.70         91.71         92.22         1.87         89.75         0.11         -0.38           89.10         89.75         2.42         83.67         94.39         0.95         -2.08           89.11         89.77         2.43         84.52         93.71         -6.80         -0.49           85.74         85.34         2.71         79.71         89.46         -3.82         -3.94           85.74         88.47         1.90         84.37         91.47         3.97         4.95           91.16         92.74         93.49         1.93         89.26         99.54         0.88         1.03           91.75         93.49         2.74         88.35         100.34         -0.22         -0.26 <td< td=""><td>1958</td><td>87.60</td><td>47.70</td><td>89.52</td><td>2.34</td><td>85.45</td><td></td><td></td><td></td><td>-0.18</td></td<>  | 1958 | 87.60           | 47.70            | 89.52               | 2.34                | 85.45   |         |                    |                     | -0.18     |
| 94.66 91.74 90.56 3.08 81.52 95.34 5.35 1.85 94.60 91.69 91.91 3.14 85.64 96.45 0.0 1.04 92.22 1.87 89.79 97.74 0.11 -0.38 89.75 2.42 83.67 94.39 0.95 -2.08 89.10 88.41 85.34 2.71 79.71 89.46 -3.82 -3.94 89.10 88.41 88.47 1.90 84.37 91.47 3.97 3.07 89.10 93.74 93.19 1.97 89.26 99.54 0.88 1.03 91.70 93.19 3.01 88.35 100.34 -0.22 -0.26 94.30 97.10 93.69 2.40 88.85 97.03 2.84 -0.36 97.03 2.84 -0.36 87.20 97.17 93.69 2.40 88.87 97.03 2.84 -0.36 87.20 97.17 93.69 2.20 88.87 97.03 2.84 -0.36 97.03 2.84  | 1959 | 38.68           | B9.34            | 88.57               | 1.81                | 45.74   |         |                    |                     | -1.06     |
| 94.60 91.99 91.91 3.14 85.64 96.45 0.0 1.04 94.20 91.64 99.22 1.87 89.79 97.74 0.11 -0.36 95.60 89.73 89.67 2.42 83.67 94.39 0.95 -2.08 89.10 89.77 85.38 2.71 79.71 89.46 -3.82 -3.94 89.10 88.41 88.47 1.90 84.37 91.47 3.97 3.07 89.10 93.74 93.19 1.97 89.26 99.54 0.88 1.03 91.70 93.70 93.70 93.19 3.01 88.35 100.34 -0.22 -0.26 94.30 97.15 2.24 4.95 91.70 93.19 3.01 88.85 300.34 -0.22 -0.26 97.20 93.17 93.69 2.40 88.80 97.03 2.84 -0.36 87.20 97.10 93.69 2.22 88.85 98.77 -7.10 0.02   | 1960 | 94.6Ú           | 91.ru            | 90.56               | 3.08                | 81,52   |         |                    |                     | 2.25      |
| 94,7C 91,64 92,22 1.87 89,79 97,74 0.11 -0.38 89,60 89,73 89,67 2,42 81,67 94,39 0,95 -2.08 89,1C 89,29 89,67 2,43 84,52 93,71 -6.80 -0.49 85,7C 85,77 85,38 2,71 79,71 89,46 -3.82 -3.94 89,10 88,41 88,47 1,90 84,37 91,47 3.97 3.07 91,10 97,10 93,19 1,97 89,81 97,15 2,24 4,95 91,10 93,19 3,01 88,35 100,34 -0.22 -0.26 91,7C 93,49 93,19 3,01 88,35 100,34 -0.22 -0.26 91,7C 91,17 93,69 2,40 88,89 97,53 2,84 -0.36 87,50 91,17 93,69 2,22 88,85 98,77 -7,10 0.02  | 1961 | 94.60           | 66.10            | 91.91               | 3.14                | 85.64   |         |                    |                     | 1.49      |
| 95.60 89.73 89.75 2.42 83.67 94.39 0.95 -2.08 89.10 89.10 89.67 2.43 84.52 93.71 -6.80 -0.49 85.70 85.34 2.71 79.71 89.46 -3.82 -3.94 89.10 88.41 88.47 1.90 84.37 91.47 3.97 3.07 91.10 92.74 93.19 1.97 89.81 97.15 2.24 4.95 91.90 93.19 2.74 89.26 99.54 0.88 1.03 91.70 93.19 3.01 88.35 100.34 -0.22 -0.26 94.30 97.15 93.69 2.40 88.80 97.03 2.84 -0.36 87.20 93.17 93.69 2.22 88.85 98.77 -7.10 0.02   | 1962 | 94.76           | 91.64            | 92.22               | 1.87                | 49.79   |         |                    |                     | 0.33      |
| 89.1C         89.29         89.67         2.43         84.52         93.71         -6.80         -0.49           85.7C         85.38         2.71         79.71         89.46         -3.82         -3.94           89.10         88.47         1.90         84.37         91.47         3.97         3.07           91.10         92.74         89.46         -3.82         -3.94           91.10         93.19         1.97         89.41         97.15         2.24         4.95           91.20         93.74         93.60         2.74         89.26         99.54         0.88         1.03           91.70         93.49         3.01         88.35         100.34         -0.22         -0.26           94.3C         91.15         92.69         2.40         88.80         97.03         2.84         -0.36           87.c0         93.17         93.69         2.22         88.85         98.77         -7.10         0.02   | 1963 | 95.60           | 89.73            | 89.75               | 2.42                | 83.67   |         |                    |                     | -2.67     |
| 85.7¢ 85.77 85.38 2.71 79.71 89.46 -3.82 -3.94 89.10 88.41 88.47 1.90 84.37 91.47 3.97 3.07 31.10 91.10 97.15 2.24 4.95 91.10 93.74 93.69 2.74 89.26 99.54 0.88 1.03 91.7¢ 93.29 93.19 3.01 88.35 100.34 -0.22 -0.26 94.3¢ 97.15 93.69 2.40 88.80 97.03 2.84 -0.36 87.c0 93.17 93.69 2.22 88.85 98.77 -7.10 0.02   | 1964 | 89.10           | 86°58            | 19.68               | 2.43                | 84.52   |         |                    |                     | 60.0-     |
| 89,10     88,47     1,90     84,37     91,47     3,97     3,07       91,10     92,74     93,19     1,97     89,26     92,24     4,95       91,90     93,74     93,50     2,74     89,26     99,54     0,89     1,03       91,70     93,49     93,19     3,01     88,35     100,34     -0,22     -0,26       94,30     91,15     92,69     2,40     88,80     97,03     2,84     -0,36       87,c0     93,17     93,69     2,22     88,85     98,77     -7,10     0,02  | 1965 | 35.76           | 85.77            | 85.38               | 2.71                | 79.71   |         |                    |                     | 66.4-     |
| 91.10 92.7d 93.19 1.97 89.81 97.15 2.24 4.95 41.90 91.90 93.74 89.26 99.54 0.88 1.03 91.70 93.49 93.19 3.01 88.35 100.34 -0.22 -0.26 94.30 97.15 92.69 2.40 88.80 97.03 2.84 -0.36 87.20 93.17 93.69 2.22 88.85 98.77 -7.10 0.02   | 1966 | 89.10           | 88.41            | 88.47               | 1,90                | 84,37   |         |                    |                     | 3.62      |
| 91.90 93.74 93.60 2.74 89.26 99.54 0.88 1.03 91.70 93.44 93.19 3.01 88.35 100.34 -0.22 -0.26 94.30 97.15 92.69 2.40 88.80 97.03 2.84 -0.36 87.40 93.69 2.22 88.85 98.77 -7.10 0.02   | 1961 | 91.10           | Dr. 19           | 93.19               | 1.97                | 89.H1   |         |                    |                     | 5.35      |
| 91.7c 93.4y 93.19 3.01 88.35 100.34 -0.22 -0.26 94.3c 97.53 2.40 88.80 97.53 2.84 -0.36 87.c0 93.17 93.69 2.22 88.85 98.77 -7.10 0.02  | 1968 | 91.90           | 93.74            | 93.60               | 2.74                | 89.26   |         |                    |                     | 0.43      |
| 94.3C 97.15 92.69 2.40 88.80 97.03 2.84 -0.36<br>87.c0 93.17 93.69 2.22 88.85 98.77 -7.10 0.02   | 6961 | 91.70           | 93.49            | 93,19               | 3.01                | 88.35   |         |                    |                     | -J.44     |
| 87.20 91.11 93.69 2.22 88.85 98.77 -7.10 0.02  | 1970 | 94.30           | 97.15            | 92.69               | 2.40                | 88.80   |         |                    |                     | -0.54     |
|  | 1971 | 87.60           | 91.11            | 93.69               | 2.22                | 88.85   |         |                    |                     | 1.09      |

20 REPLICATIONS TO YEAR 1971 BITH PROM YEAR 1952 Y ( b) OUTPUT FOR VARIABLE

|              | ACFÜAL<br>VALUE | DFTERM,<br>VALUE | MEAN STOC. | STANDARD MINIMOM<br>DEVIAT, | ROKIKIK   | MAXINUM  | ACTUAL<br>K CHANGE | DETERM.<br>* CHANGE | MEAN STOC |
|--------------|-----------------|------------------|------------|-----------------------------|-----------|----------|--------------------|---------------------|-----------|
| 1952         | 5135.00         | 5007.56          | E8.6464    | 217.63                      | 4599.64   | 5301.60  | 0.0                | 0.0                 | 0.0       |
| 1953         | 5261.60         | 90505            | 5195.30    | 292.97                      | 4758.88   | 5793.03  | 2.47               | 0.86                | 96.4      |
| 1954         | 5395.50         | 5265.71          | 5205.24    | 347.96                      | 4515.31   | 5791.67  | 2.54               | 4.16                | 0.19      |
| 1955         | 5820,20         | 5779.95          | 5776.13    | 343.49                      | 5180.09   | 6557.82  | 7.87               | 78.6                | 10.97     |
| 1956         | 6 3 9 8 . 10    | 5947,77          | 5326.50    | 193, 19                     | 5541.96   | 6433,15  | 4.77               | 2.90                | 2.60      |
| 1957         | 6473.80         | 4627.44          | 6674.81    | 282.18                      | 6263.84   | 7361,72  | 6.16               |                     | 12.63     |
| 1958         | 99.5199         | 6437.15          | 6429.63    | 259.32                      | 5975.76   | 6923.56  |                    |                     | -1.67     |
| 1959         | 7295,90         | 7002.48          | 84.0469    | 191.28                      | 6531.01   | 7246.72  |                    |                     | 7.95      |
| 1860         | 7918.30         | 8278.88          | H379.55    | 257, 30                     | 7912.87   | 8832,40  | 8.53               | 18.23               | 20.73     |
| 1861         | 8373.00         | 96.0978          | 8492.07    | 292.44                      | 8083.83   | 9058.80  |                    |                     | 1.34      |
| 1962         | 8638.83         | 8850,74          | 4956.78    | 274.56                      | 8431.59   | 9482,46  |                    | 4.61                | 5.47      |
| 1963         | 8644.00         | 8991.P4          | 9020.22    | 314.64                      | 8501.05   | 9834.17  |                    | 1.49                | 0.71      |
| ↑95 <b>।</b> | 8728.80         | 9321,58          | 9276.63    | 296.33                      | 8646.83   | 9106.39  | 96.0               | 3.67                | 2.84      |
| 1965         | 9164.70         | 9659,10          | 9706.99    | 205.44                      | 9416.37   | 10217.41 | 7.33               | 3.62                | 79.1      |
| 1966         | 10258.10        | 10234.13         | 13306.59   | 249.99                      | 9838.65   | 10897.66 | 61.6               | 5.96                | 6.18      |
| 1867         | 13851.56        | 10641.88         | 13628.09   | 2 50.60                     | 10029.15  | 11001.59 | 5.78               | 3,98                | 3.12      |
| 1968         | 11910.33        | 11299,64         | 11390.72   | 226.21                      | 10813,59  | 11774.15 | 9.76               | 6.18                | 7, 18     |
| 1969         | 12659.20        | 12659,77         | 12650.25   | 262,57                      | 12111.76  | 13168.46 | 29                 | 50.51               | 11.06     |
| 1970         | 12831.50        | 12807.52         | 12847.73   | 266.19                      | 12212, 31 | 13186.20 | 3.6                | 117                 | 5.4       |
| 1971         | 12338.20        | 11958,39         | 11977.25   | 256.25                      | 11506 71  | 12510 48 | 01.3               | 6 7 9               | 97.       |
|              |                 |                  | •          | 3                           |           | •        | 2                  |                     | 01.0      |

Table 15 - Results of stochastic simulation for the variable PIT (Nagar's algorithm)

KEPLICATIONS 5.0 MITH 1971 YFAR 40 1952 YEAR PROM 7 , Y VARIABLE FOW OUTPUT

| MEAN STOC           |                  | 7 5 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 | מבים<br>מבים         | ひたって   | 17<br>08<br>56<br>75                         | 37<br>113<br>98                              |
|---------------------|------------------|---|----------------------|--|--|--|
| E W                 | 0.0              | 4 25 m 4                                | 2.49<br>5.44<br>5.44 | 6.45   | 5.17<br>4.08<br>4.56<br>4.75                 | 6.37<br>8.13<br>2.98<br>3.71                 |
| DETERM.<br>M CHANGE | 5.82             | 3.40<br>3.79                            | 3.01                 | 6.53<br>6.00<br>6.00<br>6.00                 | 5.55<br>3.76<br>4.20<br>5.21                 | 6.04<br>8.53<br>2.74<br>3.75                 |
| ACTUAL<br>% CHANGE  | 7.04             | 3.28<br>6.61<br>4.42<br>5.36            | 4.91<br>6.75         | 7.98<br>5.98<br>5.16                         | 2.97<br>3.66<br>5.92<br>6.74                 | 6.43<br>5.74<br>4.87<br>1.63                 |
| RAXINIH             | 15391.78         | 17217.37<br>18606.93<br>18893.91        | 20977.44             | 24330.48<br>26045.09<br>27710.09<br>28488.77 | 29640_46<br>30607.37<br>32272.79<br>33489.32 | 35672,20<br>38925,44<br>39855,84<br>41385,63 |
| HININDH             | 14265.45         | 15534,61<br>17414,53<br>17683,83        | 19810.18<br>20738.26 | 24.48.44<br>26.158.44<br>27.014.77           | 28255.86<br>29763.86<br>31168.96<br>32533.44 | 34669.42<br>37496.11<br>38494.56<br>39902.60 |
| STANDARD<br>DEVIAT. | 328,84<br>347,62 | 381.30<br>252.93<br>292.52              | 262.56<br>334.14     | 292.15<br>321.70<br>389.66<br>335.63         | 295.25<br>276.03<br>263.79<br>280.05         | 264.80<br>326.02<br>359.21<br>340.96         |
| MEAN STOC.          | 14903.66         | 16249,85<br>17744,31<br>18319,30        | 20203.24             | 21104.62<br>25234.07<br>25876.06<br>27613.47 | 29039.99<br>30224.90<br>31603.48<br>33104.63 | 35214.44<br>38078.88<br>39212.67<br>40667.06 |
| DETERM.<br>VAIUF    | 14923.72         | 16.32P.45<br>17714.79<br>18186.26       | 2631H.R9<br>21435.90 | 25157.84<br>25157.84<br>26666.74<br>27590.56 | 29121.70<br>30215.73<br>31483.87             | 35123.78<br>38119.78<br>39162.42<br>40630.94 |
| ACTUAL<br>VALUE     | 15342.60         | 16629.00<br>17728.00<br>18531.00        | 20442.00<br>21822.00 | 23122.60<br>24944.00<br>25436.00<br>27803.60 | 28625.00<br>29674.00<br>31431.00<br>33551.00 | 35709.C0<br>37757.C0<br>39594.00<br>40241.00 |
|                     |                  |   |                      |  | 196 u<br>1965<br>1966<br>1967                |  |

# 4. Analysis of the results of stochastic simulation with variation in the number of replications

We present in this section some of the preliminary results obtained, via the Nagar and McCarthy algorithms, with variation in the number of replications from a minimum of 20 to a maximum of 300. For the sake of simplicity and compactness, the results are presented as an RMSE comparison (table 17) and as a comparison between the Theil inequality coefficients of the deterministic solution and the same indices of the stochastic mean solution (tables 18 · 19).

As regards the RMSE, when the number of replications is low, the results obtained with the Nagar algoritm are nearer to the RMSE of the deterministic solution: The best result is obtained with 200 replications; the McCarthy algorithm prevails slightly when the number of replications reaches 300 (though the differences between the results with the two algorithms are very small).

The same thing applies in the case of the Theil inequality coefficients. It seems we can therefore conclude that, when the number of replications used is not very high (as is generally the case, for reasons of time and cost), the numbers generated on the basis of the Nagar algorithm prevail slightly and this algorithm is also the quickest in this case.

In fact, even though the transformation matrix has to be calculated for the Nagar algorithm, it only has to be calculated once, and for each replication the vector of the independent normal random numbers (which serves as starting point) contains only 5 elements, (the number of structural equations in the model). For the McCarthy algorithm, on the other hand, the vector used contains 20 elements (the same as the number of years in the sample period).

The McCarthy algorithm has the advantage of being much more simple from the computational aspect, and it is the only one that can be used when the number of structural equation in the model exceeds the number of years in the sample period.

As has already been implied, it must be noted that in the operations car-

RMSE values for the deterministic solution and for the stochastic mean with variation in the number of replications

Table 17

|          | 300          | 1.041            | .741  | .587 | 698   | .712 | .934  | 1 010 |       | 1.023 | 749   | .596 | 698.  | 721  | 961   | 1.000 |
|----------|--------------|------------------|-------|------|-------|------|-------|-------|-------|-------|-------|------|-------|------|-------|-------|
|          | 200          | 986              | .748  | 665. | .863  | .736 | .921  | 976   |       | 1.030 | .739  | .587 | .874  | .715 | 913   | 986   |
| rhy      | 100          | 1.053            | .783  | .588 | 889   | .719 | .977  | 1.045 | JE.   | .982  | .723  | .572 | .850  | .705 | .931  | 866.  |
| McCarthy | 50           | 1.183            | 792   | 601  | .925  | .783 | 1.027 | 1.096 | Nagar | 1.054 | .789  | .615 | .963  | 747  | 878   | .984  |
|          | 20           | 1.142            | .819  | .692 | 1 038 | .788 | 516   | 1.046 |       | 1.172 | .764  | .558 | 656   | .761 | 1.069 | 1.126 |
|          | Determinist. | 1.037            | 717   | .582 | 698.  | .706 | .936  | 1.003 |       | 1.037 | .717  | .582 | 698.  | .706 | .936  | 1.003 |
|          |              | C <sub>P</sub> N | II.IJ | M    | WIT   | KOCC | PIT   | RNLCF |       | CPN   | I[],[ | ¥    | .LJ:M | KOCC | PIT   | RNLCF |

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T1 values for the deterministic solution and for the stochastic mean, with variation in the number of replications. Table 18

|          | 300          | .536 | 999. | .705 | .408 | .929  | 609  | .339  |       | .527 | .673 | .714 | .408 | .941 | .627 | .335  |
|----------|--------------|------|------|------|------|-------|------|-------|-------|------|------|------|------|------|------|-------|
|          | 200          | .508 | .672 | .718 | .406 | .961  | .601 | .327  |       | .531 | .664 | .703 | .411 | .933 | .596 | .331  |
| ırthy    | 100          | .543 | .703 | 705  | .418 | .938  | .637 | .350  | şar   | .506 | .649 | 989  | .400 | .920 | .607 | .335  |
| McCarthy | ·\$0         | 609. | .711 | .720 | .435 | 1.022 | .670 | 368   | Nagar | .543 | .709 | .737 | .453 | .976 | .573 | .330  |
|          | 20           | .588 | .735 | .829 | .488 | 1 029 | .597 | .351  |       | .603 | 989. | 699. | .451 | 994  | 269. | .377  |
|          | Determinist. | .535 | .644 | 869. | .408 | .922  | .610 | .336  |       | .535 | .644 | 869: | .408 | .922 | .610 | .336  |
|          |              | CPN  | ILIT | ¥    | WIT  | KOCC  | PIT  | RNLCF |       | CPN  | ILIT | W    | TIM  | KOCC | PIT  | RNLCF |

T2 values for the deterministic solution and for the stochastic mean with variation in the number of replications.

Table 19

|          | 300          | .0218 | .0594 | .0530 | .0222 | .0268 | .0301  | .0124 |       | .0217 | .0594 | .0533 | . 0226 | . 0272 | .0299  | .0123  |
|----------|--------------|-------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|--------|--------|--------|--------|
|          | 200          | .0215 | .0608 | .0531 | .0225 | .0280 | . 0297 | .0122 |       | .0221 | .0587 | .0525 | .0227  | .0268  | .0295  | .0125  |
| thy      | 100          | .0223 | .0599 | .0533 | .0225 | .0273 | .0312  | .0128 | 2 F   |       | .0593 | .0515 | .0220  | .0269  | . 0295 | . 0124 |
| McCarthy | 50           | .0234 | .0607 | .0554 | .0235 | 0283  | .0317  | .0130 | Nagar |       | .0572 | .0551 | .0236  | .0266  | . 0286 | .0121  |
|          | 20           | .0245 | .0623 | .0604 | .0254 | .0281 | .0301  | .0133 |       | .0233 | 6090  | .0508 | .0230  | .0276  | .0313  | .0133  |
|          | Determinist. | .0221 | .0587 | .0526 | .0224 | .0269 | .0302  | .0125 |       | .0221 | .0587 | .0526 | .0224  | .0269  | .0302  | .0125  |
|          |              | CPN   | ILIT  | ¥     | WIT   | KOCC  | Pl'I   | RNLCF |       | CPN   | ILIT  | Σ     | WIT    | KOCC   | PIT    | RNLC!: |

ried out starting from the same seed (1) for the generation of the random numbers, the pseudo-random numbers used are not exactly the same, because of the difference between the two algorithms.

From analysis of tables 17 - 18 - 19 we may conclude that the number of replications that has to be carried out before the experimental error becomes negligible is in fact too high, from the practical application aspect. It should be noted, however, that to ensure the correct statistical use of the model, it is sufficient for the experimental error to be less than the RMSE of the deterministic solution and, clearly, this result is also achieved with the 20 replications selected by way of example.

Similar results are obtained in terms of variances too. In this connection, the following experiment was performed regarding the value of the standard deviation of the stochastic solution, for the y1 (CPN) variable for 1953, generating the errors by means of the McCarthy algorithm (see Table 3, line 1, Standard Deviation column).

Tests were carried out with 20, 50, 100, 200, and 300 replications with random numbers calculated on the basis of 4 different initial values. The asymptotic value for the consumption variance, calculated on the basis of  $A^{-1}\Sigma(A^{-1})'$  is 437 (see Table 2).

In this case also, about 300 replications are necessary to render the experimental error negligible. Analysis of Table 20 (which contains these results) shows the influence of the initial value for generating the uniform random numbers on the dispersion of the standard deviation of the CPN variable.

Whith 20 replications, for example, the dispersion due to the initial values (294 - 395 - 453 - 519) is almost equal to that obtained with the first initial value (294 - 341 - 417 - ... - 450) with 20 replications over the entire sample period (see Table 3, column 4).

### Table 20

Standard deviation values of CPN variable, with variation of the initial value and of the number of replications.

|        |     | Replic | ations |     |     |
|--------|-----|--------|--------|-----|-----|
|        | 20  | 50     | 100    | 200 | 300 |
| Sced 1 | 294 | 367    | 363    | 429 | 440 |
| Seed 2 | 519 | 502    | 475    | 481 | 455 |
| Seed 3 | 395 | 369    | 432    | 439 | 420 |
| Seed 4 | 453 | 454    | 400    | 426 | 408 |

### 5. Conclusions

By the analysis of the results, we can conclude that, when a small number of replications is performed, the experimental discrepancy between deterministic solution and stochastic mean is not very little. Moreover, it is possible to see that the number of replications necessary to make this experimental error negligible is too high, from the practical application aspect.

Nevertheless, the correct statistical use of the model is ensured even with the 20 replications performed by way of example.

As far as a comparison between the two error-generating algorithms is concerned, we can say that there is no clear cut prevalence of any of them, even if the Nagar's algorithm seems to be more convenient for a small number of replications.

To sum up, even if the adopted model is linear, it is possible to get useful information on the characteristics of stochastic simulation and on its practical limitations.

<sup>(1)</sup> This term signifies the starting value used to generate uniform random numbers.

The Gauss-Seidel method was used for solution of the model, for the following main reasons:

- a) it is easy to put on to a computer
- it can be used for the solution of linear and non-linear models, without distinction
- c) it can be used without any difficulty for taking into account particular problems such as: saturation, discontinuity, changes in model parameters, etc.

Given a system of linear or non-linear equations, (leaving aside the disturbance element):

 $y_{it} = f_i(y_{1t}, ..., y_{nt}, y_{1t+1}, y_{nt+p}, x_{1t}, ..., x_{qt+q})$  i = 1, ..., nthe Gauss algorithm used for the numerical solution of this system is (passing from iteration t - 1 to iteration t):

$$f_i(y_{1t_i}^{(r-1)}...y_{it}^{(r-1)}...,y_{nt}^{(r-1)},y_{1t-1},y_{nt-p},x_{1t},...x_{qt-q})$$
  $i=1...,n$ 

Seidel's modification consists in making use - in each iteration - of data already calculated during same iteration and, naturally, during the previous

$$y_{it}^{(r)} = f_i(y_{1t}^{(r)}, ..., y_{i+1t}^{(r)}, y_{it}^{(r+1)}, ..., y_{nt}^{(r+1)}, ..., y_{1t+1}, y_{nt+q}, x_{ti}, x_{qt+q})$$

$$i = 1..., n$$

The iterative process comes to an end when with  $\epsilon$  assigned:

$$\left| \frac{y_{i,\tau}^{(r)} - y_{i,\tau}^{(r+1)}}{y_{i,\tau}^{(r+1)}} \right| < \varepsilon \qquad i = 1, \dots, n$$

In our model, assuming that  $\epsilon=10^{-5}$ , convergence is generally reached with less than 15 iterations.

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Two factors affect convergence in this algorithm; the first is the normalization procedure (that is the choice of the variable rendered explicit for each equation in the model), and the other is the ordering of the equations (but only if the Seidel modification method is used).

As regards economic models in particular, it should be noted that convergence is facilitated if the equations are normalized and ordered so as to reflect the causal flow of economic events, which is implicit in the model. [8]

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