Some Environmental Geologic Factors as Aids to Planning in Hendricks County, Indiana

By JOHN R. HILL and GEORGE S. AUSTIN

ENVIRONMENTAL STUDY 6

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Eight maps of Hendricks County showing:
Bedrock geology
Bedrock topography
Drift thickness
Water well locations and corresponding depths to static water levels
Land-use suitability for sanitary landfilling
Land-use suitability for septic systems
Sand and gravel resources
Locations of auger boring sites

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Some Environmental Geologic Factors as Aids to Planning in Hendricks County, Indiana

By JOHN R. HILL and GEORGE S. AUSTIN

Introduction

With the expanding awareness of environmental needs during the past decade, the value of geologic information to urban and regional planning has become increasingly apparent. Earth materials in the form of rock and unconsolidated sediments provide a basis for our very existence. They yield building stone, coal, oil, gas, ground water, a wide variety of minerals, and sand and gravel, and we grow our crops in soils—all from a small portion of the earth's upper crust.

Continued use of these mostly nonrenewable natural resources and increasingly complex economic and distributional problems have ushered in the era of shortages. Clearly, every effort must be made to plan future use and urban growth in such a way as to maximize efficiency and minimize waste. This calls for a cooperative approach to planning. Practical knowledge of hydrology, geology, soils, engineering, biology, botany, and economics can help planners to make judgments that will result in the greatest benefit to urban and rural communities alike.

The maps presented here are to supply as much simple and direct geologic information for a particular area as is possible. These special geologic maps and their explanations were prepared after consultation with official representatives of Hendricks County, who outlined their then-current needs. The information contained in this report is not comprehensive, but it answers many practical questions posed at the onset of the study.

Bedrock Geology

This map illustrates the disposition of the bedrock units as they would appear today if there were no glacial deposits present to cover them up. The county is underlain by rocks of the Borden Group (siltstone, sandstone, and shale) except along the eastern third of the county where preglacial erosion stripped away the Borden rocks to expose the underlying New Providence and New Albany Shales.

The bedrock formations formed hundreds of millions

of years ago when shallow seas covered much of Indiana, including what is now Hendricks County. During a long period of geologic time called the Paleozoic Era, sediments were deposited on the bottom of these inland seas and later hardened into solid rock. After deposition, a long period of erosion occurred during which upper portions of the bedrock were removed, thus exposing underlying strata. Other information on the erosional history of the bedrock surface is provided under the heading "Bedrock Topography."



Bedrock geology

Bedrock Topography

The contour lines on this map detail the bedrock-surface topography in the same way that the surface topography is depicted on a modern topographic quadrangle map. As discussed on page 2, erosion of the bedrock surface began as soon as it was exposed to the elements. Running water cut extensive and complex valleys into the bedrock, which resulted in an elaborate system of hills and valleys that somewhat resemble the landforms in present-day Brown County.

Interestingly, some of the modern streams, such as

Mill and Lick Creeks, follow nearly the same courses that their preglacial ancestors did. Bedrock topography has had a definite effect on the postglacial landscape, the first evidence of which is the similarity in drainage patterns. In some parts of the county, however, such as Washington Township, the overlying glacial drift has not only filled the old valleys but mounded high above them, thus masking the original topography completely. Glacial modification of the bedrock surface is further discussed under the heading "Drift Thickness" on page 6.



Bedrock topography. Contour interval 50 ft. Datum is mean sea level.

Drift Thickness

Prepared from water well driller's logs, this map shows the thickness of the unconsolidated deposits. Generally, the areas of greatest drift¹ thickness correspond to underlying bedrock valleys (see p. 4) but also reflect the presence of rolling ground and end moraines (constructional topographic features formed by glacial deposition). Where the glacial deposits are thinnest (for example, near Clayton and Coatesville), the underlying bedrock is generally relatively high. (Refer to bedrock topography map.)

The variable thickness of drift in Hendricks County results from both glacial erosion and deposition. Indiana was affected by at least three of the four major ice advances of the Pleistocene Epoch (last 1.5 million years of geologic time, known also as the Ice Age). Evidence for all but the last glaciation (the Wisconsinan) has either been eroded away or covered by successive deposits associated with later advances and retreats of the continental ice sheets. The most common material deposited by ice in this county is till, which is an unsorted conglomeration of sediments ranging in size from boulders several tons in weight to fine silt and clay. Such tills in part were smeared over the landscape by mile-high thicknesses of ice much as butter is spread on bread.

Periodically throughout the Wisconsinan, climatic conditions warmed and caused the ice to retreat to northern latitudes, only to readvance as temperatures fell again. During each ice-recessional phase, large volumes of water were released that cut deep valleys into the underlying till and deposited sand and gravel in these valleys just as modern rivers fill their floodways with alluvium. These deeply incised valley fills are called valley-train deposits, and, where near the surface, provide excellent sources of commercial sand and gravel.

As ice readvanced over an area, the glacial floodways and their outwash deposits were covered by a fresh layer of till. Buried valley-train deposits now carry large volumes of ground water and serve as the principal aquifers in the county. As the ice left this area for the last time some 18,000 years ago, the major drainageways now occupied by the White River, Mill Creek, and Walnut Creek were established. Once the ice had melted and the glacial uplands were drained, the meltwater sluiceways remained as broad valleys filled with sorted sand and gravel; along their margins deposits of silt and clay formed in backwater areas. Prevailing westerly winds picked up and transported silt from the sluiceway flood plains and redeposited it throughout the area and on top of the till as a finegrained veneer called loess.

Thus, the whole of the glacial and immediately postglacial deposits found in Hendricks County consists of till, interlayered sand and gravel, recent alluvial deposits, and loess. The vertical and lateral heterogeneity of these deposits is so great that the descriptions provided here should be considered as generalities. The actual vertical sequence at any one place may differ from the condition stated above in general terms.

 $^{^{1}}$ Drift refers to all deposits of glacial origin, including those of glaciofluvial origin.



Drift thickness. Contour interval 50 ft. 25-ft supplementary contour shown with dashed line.

Water Well Information

Two kinds of aquifer systems are present in Hendricks County: the bedrock aquifer, which consists of porous and permeable sandstone, and glacial drift aquifers, which consist of sand and gravel units generally bounded above and below by nearly impermeable till. The bedrock aquifer (refer to drift thickness map for information on depth to bedrock) is mostly restricted to sandstone within the Borden Group, although some ground water is extracted from the thin overlying shale. For the most part, this shale has low permeability, high iron and sulfur content, and poor yields. Bedrock wells (open circles on map) having relatively high static water levels suggest high hydrostatic heads caused by the confining effect of an impermeable cover material on top of the aquifer. The bedrock wells generally are not good producers because the water-bearing units are thin and have low permeability.

Almost all wells producing 100 gallons per minute² or better are completed in the unconsolidated drift aquifers, the best producers being restricted to buried river valleys that are now filled with great thicknesses of highly permeable sand and gravel of valley-train origin. Walnut and White Lick Creeks course over much of the buried preglacial valley trends, so that many of the best producing wells happen to be on or near the flood plains of these creeks. Most of the drift aquifer recharge takes place along the larger streams, so the highest yields are expected along their courses. Perched water tables within the glacial till are common. Yield from perched ground-water reservoirs is low because most of the water-bearing deposits are small pods or lenses of sand and gravel within an impermeable till matrix. Depths to reliable water-bearing units within glacial deposits are less predictable than are depths to water in bedrock because of the compositional irregularity of these deposits. Glacial aquifers may thicken or thin abruptly and even pinch out altogether. In fact, lateral regularity throughout a given sand and gravel horizon is exceptional. Therefore, depths to principal glacial aquifers cannot be predicted on a county-wide basis. Wells close to a proposed drilling site, however, are excellent guides to probable drilling depths and to water yields.

²All ground-water information was provided by the Division of Water, Department of Natural Resources.



Water well locations and corresponding depths to static water levels

Sanitary Landfill Information

The most important geologic requirements for a sanitary landfill site (summarized from Indiana Geological Survey Special Report 5) are: (1) the base of a proposed landfill should be in relatively fine-grained materials and more than 20 to 30 feet above the shallowest aquifer; sites should not be located in abandoned sand and gravel pits for this reason; (2) the base of a proposed landfill should be above the highest seasonal level of the water table; (3) a proposed site should not be subject to flooding; sites should not be located on river flood plains for this reason; and (4) adequate cover material must be available near a proposed site.

In Hendricks County, much of the land is fairly well to well suited to sanitary landfilling because most of the near-surface materials consist of fine-grained, relatively impermeable till and loess. In most areas the water table is sufficiently low to permit excavation for a fill, and adequate cover material is present. Two problems may be encountered: (1) a hardpan exists in many parts of the county at an average depth of 12 feet below grade, and (2) owing to the fine texture of most of the soil materials, excavation and working of these materials can be difficult, especially in dry weather. The hardpan is generally no more than 1 or 2 feet thick but requires special equipment to break through it. Furthermore, the hardpan, which is an aquitard (nearly impermeable layer), is commonly associated with a perched water table. The hardpan is a discontinuous unit and should not, therefore, be relied on to prevent leachate contamination of the underlying aquifers.

On-site borings are essential for all proposed landfill sites, because the exact local conditions may differ from the map generalizations.



Land-use suitability for sanitary landfilling

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Septic System Information

Most of Hendricks County is poorly suited to the use of the septic system because of low-permeability soils and a seasonally high water table. The dominant earth material in the county is glacial till of loamy to silty loam texture that is covered by loessial³ silt of variable thickness. Both till and loess have relatively low permeability, and septic effluent does not percolate readily through these materials. Septic fields usually require tiling, especially in flat or depressional areas, to provide proper drainage because of their low watertransmitting properties. Fields throughout the county require extensive tile and finger systems, and even then heavy rains can drastically reduce efficiency of a given field.

Soils that do offer fair to good septic suitability include Ockley, Fox, Martinsville, Russel, and the loamy phase of the Miami Series. All these soils, except the Miami soils, develop atop outwash sand and gravel or atop outwash loess mantles. These soils do not offer optimum conditions, however, because they are sparsely distributed and are associated with high water tables or other potential water-table contamination problems. Generally, the Miami soils offer the best suitability to septic systems.

As the county grows, the need for municipal sewer systems to replace overtaxed septic fields will become apparent.

³Loess is a windblown deposit composed of silt-size particles.



Land-use suitability for septic systems

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Sand and Gravel Information

Glacial valley-train deposits along the streams account for most of the sand and gravel deposits in Hendricks County. Carried hundreds of miles from their points of origin by ice and water, these materials were deposited in front of the waning Pleistocene glaciers by torrents of meltwater that washed and sorted the sand and gravel and left variable thicknesses of these sediments along the old meltwater courses. Since Pleistocene time, valley-train materials have been reworked and redeposited by the modern streams flowing over them.

Hill and moundlike structures composed of stratified sand and gravel called kames are scattered throughout the county and account for a minor amount of the potential aggregate materials. Kames are ice-contact features that formed directly adjacent to the melting glacier (as it retreated from the area). Deposits of coarse to very coarse gravel are found within or at the base of many kames.

The information on this map was compiled from water well records on file in the Ground Water Section, Division of Water, Department of Natural Resources, and from field investigations of operating and abandoned gravel pits throughout the county. The siting of kame and kame-terrace deposits was taken from geologic maps on file at the Indiana Geological Survey.

Guilford, Brown, and Liberty Townships probably contain greater quantities of sand and gravel than do the other townships. All of Guilford Township has good potential, but only the northwest portion of Brown Township and the northeast quarter of Liberty Township appear to offer good potential in those townships. Areas in which sand and (or) gravel is exposed at the surface should be considered as potential gravel extraction sites in zoning considerations. Terraces are developed along some of the creeks in the county, but in general they are not large enough to supply sizable quantities of sand and gravel. In the center of sec. 15, T. 15 N., R. 1 W., a terrace deposit as large as 3 acres is present, but it is an exceptional example. White Lick Creek and its branches are the most highly exploited areas of sand and gravel in the county, although nearly every stream bears some evidence of former removal of sand and gravel.



Sand and gravel resources

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Auger Boring Information

The numbered localities on this map are sites at which subsurface information was gathered. Table 1 provides a summary of the data gathered at each site where samples were collected. The entries labeled "Texture," "Total carbonate," and "Atterberg limits" were derived from laboratory analyses of the samples. Texture refers to the percentages (expressed as weight percent of the total sample) of the different particle sizes constituting the total sample (granule, 4 to 2 mm; sand, 2 to .063 mm; silt, .063 to .004 mm; and clay, .004 to .00006 mm). Total carbonate is the percentage by weight of calcium carbonate and calcium-magnesium carbonate of the sample that passed through a 200-mesh sieve. If the total carbonate content is more than 3 to 5 percent, the sample is considered to be unweathered. That is, the interval from which the sample was taken has not been exposed to subaerial oxidation and leaching as have modern soils. Atterberg limits (liquid and

plastic limits) are the values (expressed as percent by weight of moisture in the sample) at which the soil behaves as a liquid or a plastic. The plasticity index is derived by subtracting the plastic limit from the liquid limit and is used in rating soil strengths and behavior under different moisture and load conditions. Wherever available, compressive strengths (given in tons per sq ft) are presented along with the stratigraphic description in table 1.

Locations for the boring sites were predetermined by officials of the Hendricks County Planning Commission to answer specific questions about stratigraphic, hydrologic, and engineering conditions within and near various towns and subdivisions. The information was not gathered to make general engineering or geologic interpretations but rather to illustrate some of the properties of the subsurface materials at particular points of interest to the county planners.



Locations of auger boring sites

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ation	Depth			Textu	re ¹		Total	A	terberg ID	nits
No	(i)	outaugraphuc description	Granule	Sand	Silt	Clay	carbonate ²	Liquid limit	Plastic limit	Plasticity index
1	ф 3	Brown silt-loam till (sand in patches), 3 tons per sq ft strength at R-nercent field moisture	0.2 ³	39.7	44.9	15.3	24.32	18	13	S
	3-12 12-204 20-100	Yellow-brown oxidized clay-rich till Gray shale Sandy blue soft shale	2.4	10.6	21.1	46.1	13.12	21.5	8.2	13.3
3	0- 3 3- 10 10- 15	Oxidized B-horizon of loamy till As above, but unoxidized and unleached Silt-loam till, drier than above with increase in compressive streact					-			
	15-20 20-1474 147-480 ⁴ 480-4924	Progressively harder blue clay and silt Alternating sandstone and shale Shale Limestone	0.3	8.6	65.9	25.5	2.63	52	12	10
ε	0 3 8 13 32-38 32-38	Fill Brown mottled till As above, but saturated As above, alternately dry-wet Water sand	0.5	6.3	56.6	37.0	24.44	24	18	ø
4	45+4	Surt un (~ 4 vous per eq 11) Blue stone (probably shale) F Fill								
t	2- 5 5- 10 10- 12 16- 17 22- 454	Fun Brown till, .575 ton per sq ft Reddish silt loam Sandy saturated layer, oxidized Stiff gray till Very stiff gray till (>3 tons per sq ft compressive strength) Blue stone (shale)								
N .	0- 2 2- 5 5- 8 8- 12 12- 25 12- 25 88- 904 88- 904 90- 954 90- 954 9260-275	Fill Sandy till Water sand Very soft wet mud Blue-gray stiff till As above Sand Shale Siltstone Blue shale	6.0	56.2	29.3	14.5	2.24	16	12	4

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	ę	0-3 3-5 8-18 18-704 701304	Brown to buff till Brown till (1.5 tons per sq ft) Water sand Gray till As above Blue shale	0.2	14.05	54.2	31.7	1.78	28	23	ŝ
8 No hole No h	L	0-3 3-8 8-10 10-13 13-20 20-504	Fill Buff silt-loarn till Water sand Silty till Very stiff till Siltstone	1.6 1.7 1.8	37.3 51.9 17.0	33.3 34.5 63.9	29.4 13.6 19.1	2.28 26.64 1.58	28.6 24.2 21.8	17.3 13.1 0	11.3 11.1 21.8
11 0-2 5 Fill Kare smail, muddy 0.0 2.24 7 41.7 35.9 14.32 29 18 11 2.8 Vare smail, muddy 1.7 42.5 35.1 2.24 34.9 18 11 7 2.9.35 Solid till 20.35 Solid till 34.30 18 11.7 7 2.9.35 Solid till 84.120 ⁴ Bibs sandfatone 1.7 42.5 35.1 22.4 34.30 18 11 7 13 2.2 Prival Bibs sandfatone 0.2 47.7 34.5 17.8 27.61 16 NP5 17 13 2.2 P 34 13.8 27.61 16 NP 17 2.8 Above 0.2 47.7 34.5 17.8 22.61 16 NP 17 3.2 2.3 Biby sandfatone 0.1 42.4 36.4 21.2 19.09 23 14 2 3.4 0.1<	8 e 01	0- 3 3- 6 6- 804 80-1154	No hole No hole Brown silty sand Very hard silty till Gray dense till Blue shale	1.3 0.7	40.8 58.8	43.2 27.2	16.0 14.0	6.45 1.11	21.4 17.4	0 13.6	21.4 3.8
12 No hole 13 0 2 Full 13 0 2 Full 15 16 NP5 16 13 2 3 Dirty sand and gravel 0.3 47.9 33.3 18.8 27.61 16 NP5 16 2 3 As above 0.2 47.7 34.5 17.8 292.11 17 NP 17 8 34 Cray till, very hard at 15 ft and deeper 0.2 47.7 34.5 17.8 292.11 17 NP 17 8 34 0 10 Tar study loam 0.1 42.4 36.4 21.2 1909 23 14 9 10<-10	Ξ	0 2 2 8 8 20 8 20 35 47 84-1204	Fill Gray till Water sand, muddy Solid till Alternating hard and soft layers within the till Gray till Blue sandstone	0.0 1.7	22.4 42.5	41.7 35.1	35.9 22.4	14.32 34.30	29 18	11	11 7
14 0-10 Tan sandy foam 0.1 42.4 36.4 21.2 19.09 23 14 9 10-18 Water sand 10-18 Water sand 3.5.9 41.0 23.2 31.11 18 12 6 15 0-3 Red oxidized clay till 3.6.9 41.0 23.2 31.11 18 12 6 15 0-3 Red oxidized clay till 0.0 46.0 31.1 22.9 16.67 21 14 7 3-5 Silt-toam till 5-8 Dry buff till 22.9 16.67 21 14 7 5-8 Dry buff till 5 8 12 6 14.8 33.37 15 14 7 15-18 Story layer in till 15 14.8 33.37 15 NP 15 16-21.04 Biu-grap shale 0.4 52.6 32.6 14.8 33.37 15 NP 15 22- 304 Biu-grap shale <td>12 13</td> <td>9- 2- 2 8- 3- 3 34- 724</td> <td>No hole Fill Dirty sand and gravel As above Gray till, very hard at 15 ft and deeper Blue shale</td> <td>0.3</td> <td>47.9 47.7</td> <td>33.3 34.5</td> <td>18.8 17.8</td> <td>27.61 29.21</td> <td>16 17</td> <td>NP5 NP</td> <td>16 17</td>	12 13	9- 2- 2 8- 3- 3 34- 724	No hole Fill Dirty sand and gravel As above Gray till, very hard at 15 ft and deeper Blue shale	0.3	47.9 47.7	33.3 34.5	18.8 17.8	27.61 29.21	16 17	NP5 NP	16 17
15 0-3 Red oxidized clay till 21 14 7 3-5 Silt-loam till 2.9 16.67 21 14 7 5-8 Dry buff till 8-15 As above 2 15 16 2 14 7 15-18 Story layer in till 15 18 Story layer in till 22-304 33.37 15 NP 15 22-304 Brown sandstone 0.4 52.6 32.6 14.8 33.37 15 NP 15 30-110 ⁴ Blue-gray shale 0.4 52.6 32.6 14.8 33.37 15 NP 15	14	0-10 10-18 18-50	Tan sandy loam Water sand Very stiff clay-loam till	0.1 3.8	42.4 35.9	36.4 41.0	21.2	19.09 31.11	23 18	14 12	6 9
	15	0-3 -5 -5 -8 -15 -18 -18 -18 -18 -18 -18 -22 -304 -1104	Red oxidized clay till Silt-loam till Dry buff till As above Stony layer in till Silt-loam till Brown sandstone Blue-gray shale	0.0	46.0 52.6	31.1 32.6	22.9	16.67 33.37	21 15	14 NP	7 15

AUGER BORING INFORMATION

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Table 1. Geologic and engineering data for 42 sites on the map of He

1	1			Ē	, -			At	terberg lin	nits
No.	E (E)	Stratigraphic description	Granule	Sand	Silt	Clay	carbonate ²	Liquid	Plastic	Plasticity
								limit	rimit	index
16	9 6	FII								
	ų v	Soft wet sandy loam	0.2	42.5	38.5	19.0	32.52	17.5	đ	17.5
	5-12	Ås above					-			
	12-13	Gravel, saturated								
_	13-14	Muddy sand								
	14-15	Loamy till	0.2	39.7	44.9	15.3	24.33	18	13	ŝ
	15-16	Gravel lens								
	16-20	Very hard till								
	20-304	As above								
	30- 454	Sand and gravel								•
	45-1104	Gray till								
	110-1124	Sand								
	112-1454	TUI								
	145-1474	Sand								
	147-1774	Gray till								
	177+4	Sandstone								
17	۰ ۳	Weathered till				-				
	بع 8	Light-brown wet silt loam	0.2	42.5	38.5	19.0	32.52	17.5	đ	17.5
	*	Hard till								
	8-584	Gray till								
	58-874	Blue shale								
18	9 9	Brown weathered till								
	3- 6	Very hard till	1.8	56.0	42.4	1.6	10.98	19.5	AN	19.5
	6-584	Gray till								
	58-874	Blue shale								
19		No hole								
20	9 6	Sand	7.6	6.99	21.7	11.3	25.51	16.3	đ	16.3
	3- S	Sand grading into silty clay-loam till								
	بہ 8	Silt-loam till								
	8-12	Dirty sand (stone layer at 12 ft)								
	12-15	Kesistant till								
	15- 237									
	22- 20-									
	PCC1 211	Gray Cray								
	27CT-/11	Danc								
21	0 0	Til	0.2	8.2	45.7	46.1	.94	27.3	24.4	2.9
	به ش	Yellow clay zone (illuviated)								
	6- 12	As above, but sand lens at 10 ft	0.4	15.1	55.4	29.5	9.30	24.2	12	12.2
	57 -71 57 -71								-	
		Auternaung sort and nard tut Too hard to drift								
-			_	-	-	-	-	_	-	

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77	0-3 3-10 10-804 80-1004	Brown oxidized till Gray hard till As above Limestone	3.0	34.0	37.3	28.7	19.41	19.0	14.7	4.3
23	0-3 3-8 8-35 35-1094	Upper soil in till Brown silt-loam till As above, very stiff; some sand lenses As above, shale at 109 ft	2.3	34.0	46.1	20.0	21.77	17.5	13.5	4
24		No hole								
25	0-3 -5 -5 -10 -30 -10 -30 -52 -80 -52 -80 -135 -80 -135	Tan-buff sandy loam As above Very hard till As above Red sand Oxidized till Blue shale	5.5	49.8	29.8	20.4	27.5	15.2	12.6	2.6
26	0-75 75-1104	Gray till Biue shale								
12	0-3 3-5 5-18 18-444 44-474 47-474 47-704 70-1034	Till As above, 1-ft gravel layer at 5 ft Very hard blue till As above Dry sand Till Shale	2.6	32.2	47.2	20.5	37.49	15.5	13.7	1.8
28	0-3- 5-10 10-15	Oxidized brown clay-silt till As above but saturated Water sand Head hive till	3.0	42.6	34.2	23.2	33.06	15.9	13.4	2.5
	15-764 15-764 76-814 81-1174 117-1284 117-1284 128-1604 128-1604	Blue till Sand Blue sand Gray clay till Sand and gravel	Э.Э. Э.Э	45.5	31.3	23.4	34.88	17	П	Q
29		No hole								
30	0-3 3-5 5-11 11-12 12-25 28-524 52-544	Brown till Sandy loam Wet sandy loam Hard stony till Till with saturated sand lenses As above, very hard Gray hard till Sand and gravel	0.3	17.6	49.5	32.9	1.55	24	18	Ŷ

AUGER BORING INFORMATION

Deun	rbeng limits	Plastic Plasticity limit index	13.7 7.9	14 5.5	5.2 5.2 10.3 7.2
on the map of Hendricks County showing locations of auger holes (p. 17)–Continued	Atte	Liquid limit	21.6	19.5	20.7
ger holes (p	Total	carbonate ²	16.05	25.58	16.15
ons of au		Clay	15.3	23.8	17.9 20.1
ing locati	ture ¹	Silt	37.0	47.4	37.0
ity showi	Textu	Sand	47.7	28.8	45.1 31.8
cks Coun		Granule	12.6	1.7	3.0
liogic and engineering data for 42 sites on the map of Hend	Ctentinensultin Association	Dualityau usanyi uon	Sand clay Alternating hard till and soft sandy lenses Water sand Very hard till Till Fine sand Till	r me saud Clay till Fine sand Till Brown silt-loam till As above, soft As above, very hard Till Sand Till Sand Clay Sand	No hole Sandy loam Brown sandy loam till Gray sandy silt-loam till As above Till with boulders and sand blebs Gravelly till Till with sand blebs and many shale fragments Brown silt loam Tan pebbly till Very stiff gray till, hardpan at 20 ft Till as above Sand Till Sand
able 1. Geo	Depth	(IJ)	0- 8 8- 15 15- 17 17- 20 20-1064 106-1104 110-1104	144-1504 150-1614 151-1664 166-170 0- 5 9- 10 9- 10 9- 10 10- 604 60- 624 60- 624 60- 624 61- 624 61- 624 61- 624 62-1664 166-20377 169-204	0-3 8-10 8-10 10-13 1-20 0-3 3-20 20-304 30-324 30-3324 30-3224 30-324 30-3
	Location	No.	31	32	36 33 34

2.9		7	1.6 3.5	4.8	2.4	3.8
13		13.8	14.2 11	12.7	13	12.6
15.9		15.8	15.8 14.5	17.5	15.4	16.4
17.61		27.26	25.11 20.30	22.0	22.90	28.16
18.7	1	12.6	28.3 24.5	22.1	16.0	22.9
35.6		44.4	26.3 36.4	38.0	31.4	30.3
45.7		43.0	45.4 39.0	39.9	52.6	46.8
2.8		4.2	4.7 4.1	1.6	8.1	2.6
Brown sandy till As above Water sand Clay loam Clay-loam till Till with scattered sand lenses	No hole	Brown silt-loam till, hardpan at 15 ft Till	Brown and blue sitt-loam till, hardpan at 18 ft As above. till	Sand Clay and gravel Fine sand	Hard till, rock at 13 ft Till Gravel Till	Very stiff silt-loam till too hard to drill Till, oxidized Blue-mud till Hardpan Water gravel
0- 3 3- 5 5- 8 8- 10 10- 524 52-2044		0-15 15-2064	0- 18 18- 654	65- 684 68-1604 160-1734	0- 13 13- 624 62- 644 64-1804	0-8 8-124 12-184 18-284 28-334
37	38	39	40		41	42

¹Textural elements are expressed as a percentage of the total sample weight.

²Total carbonate is expressed as a percentage of the weight of all the sample that passes through the .074-mm sieve.

3Values for texture, carbonate content, etc., correspond to the depth increment adjacent to the line containing this information.

⁴This is a driller's log, not an Indiana Geological Survey boring log. 5NP – nonplastic.

Suggested Sources for Further Information

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 - 1971 Interim soil survey of Hendricks County, Indiana: U.S. Dept. Agriculture, Soil Conserv. Service.
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 - 1968 Water resources of Hendricks County with emphasis on ground water availability: Indiana Div. Water [map].