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# Boiling Points of the Propylene Glycol + Glycerol System at 1 Atmosphere Pressure: 188.6–292 °c Without and with Added Water or Nicotine

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1	Full title:
2	Boiling Points of the Propylene Glycol + Glycerol System
3	at 1 Atmosphere Pressure: 188.6 to 292 °C
4	Short title:
5	Boiling Points: Propylene Glycol + Glycerol
6	
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## **Abstract**

In electronic cigarettes ("electronic nicotine delivery systems", ENDSs), mixtures of propylene glycol (PG) and/or glycerol (GL; aka "vegetable glycerin", VG) with nicotine are vaporized to create a nicotine-containing aerosol. For a given composition, the temperature required to boil the liquid at 1 atmosphere must be at least somewhat greater than the boiling point (BP). Use of ENDS is increasing rapidly worldwide, yet the BP characteristics of the PG+GL system had not yet been experimentally investigated. BP values at 1 atmosphere pressure were measured over the full binary composition range. Fits based on the Gibbs-Konovalov theorem provide BP as a function of composition (by mole-percent, by weight-percent, and by volume-percent).

# Keywords

- propylene glycol; glycerol; heat exchanger fluid; electronic cigarette; e-cigarette liquid;
- 28 electronic nicotine delivery system (ENDS); e-cigarette.

#### 1. Introduction

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Propylene glycol (PG) and glycerol (GL) are high production volume (HPV) chemicals used in numerous industrial and consumer applications (Pendergrass, 1999; Teschke, 2005). First, they serve as heat exchanging fluids in solar hot water and geothermal energy systems, including as PG+GL mixtures. Second, they are main ingredients in the nicotine-containing liquids (e-liquids) used in electronic cigarettes (aka "e-cigarettes", "electronic nicotine delivery systems", "ENDSs") either individually or as a mixture. The dependence of boiling point (BP) temperature on composition is of interest in heat exchanger, e-cigarette applications, and for separations by distillation (Chen et al., 2015). Boiling is very unwelcome in heat exchange applications, but essential in the e-cigarettes (boiling must occur if the desired subsequent condensation aerosol is to form (Zhang et al., 2013; Glycerine as a heat transfer fluid and antifreeze, 2016). Globally, from 2014 to 2015, solar hot water capacity grew 6.4% from 409 to 435 to gigawatts (Renewables 2016 Global status report, 2016; Mickle, 2015). For the e-cigarette industry, global growth was 58% in 2014 (Market Research on Vapour Devices, 2016). The number of regular adult e-cigarette users in the U.S. in 2014 has been estimated at 11.8 million, with the number of "ever-users" estimated at 40.2 million (Schoenborn and Gindi, 2015).

Remarkably, BP behavior in the binary PG+GL system has received little direct study. For heat exchange applications, such information is needed during design to avoid vapor formation, and in e-cigarette applications, the information reveals the minimum temperatures that the ingredient chemicals (which may include flavor chemicals) will experience. Also, it is now well known that heating of "e-liquids" can lead to degradation products, some of which are toxic (formaldehyde (Jensen et al., 2015), acrolein and other aldehydes, and aromatic hydrocarbons (Hahn et al., 2014)). In a mixture, boiling occurs when the vapor pressure

contributions from all components combine to become at least somewhat greater than the system pressure. It is thus useful to know how BP varies with composition in the PG+GL system.

Antoine equation parameterizations for the temperature-dependent vapor pressures of pure PG ( $p_{PG}^{\circ}$ ) and pure GL ( $p_{GL}^{\circ}$ ) are available (Table 1). By assuming ideal liquid mixtures (i.e., applicability of Raoult's Law), one can use these parameterizations to predict the BP values for the full range of compositions for PG+GL mixtures according to

$$p_{\text{TOT}} = x_{\text{PG}} p_{\text{PG}}^{\text{o}} + x_{\text{GL}} p_{\text{GL}}^{\text{o}}$$
 (1)

For each value of  $x_{PG}$  (with  $x_{GL} = 1 - x_{PG}$ ), Equation 1 can be solved to obtain the normal BP as the value of T that gives  $p_{TOT} = 1$  atm. The predicted BP values thereby obtained in Table 2 are largely within the reported applicability range for the Antoine fit for GL, but are above the applicability range for PG: the applicability range for PG only extends to the BP of PG, which is below the BP for every mixture of PG and GL. The goal of this work was to carry out BP measurements for the full range of PG and GL mixtures.

66 [Place Table I here]

69 [Place Table II here]

#### 2. Materials and Methods

#### 2.1 Materials

United States Pharmacopeia grade PG and GL were obtained from Sigma-Aldrich (St. Louis, MO). Upon each opening and resealing, caps were wrapped with paraffin film to reduce hygroscopic absorption of water from the atmosphere. Reagents were 99.9+% pure, which was verified by nuclear magnetic resonance spectroscopy (NMR). Deuterium oxide (99.9% <sup>2</sup>H, 0.1% <sup>1</sup>H) was obtained from Cambridge Isotope Laboratories (Tewksbury, MA).

# 2.2 Sample preparation

Mixtures of PG and GL were prepared in triplicate at room temperature using 40 mL brown glass vials. The mixtures ranged from 0 to 100% by mass GL in increments of 10% by weight, for a total of 33 individually prepared ~20 mL samples. Mass fractions were used as the basis of the preparations rather than volume fractions because of greater ease, with viscous liquids, in measuring mass vs. volume amounts delivered. Vial caps were wrapped with paraffin film. Each sample was mixed by shaking for five minutes then stored in the dark for no more than 24 hours before testing.

### 2.3 Boiling point determinations

Prior to heating, a "pre-boiling" 10  $\mu$ L aliquot of each sample was mixed with 600  $\mu$ L D<sub>2</sub>O for analysis by NMR. The BP of the remaining ~20 mL of sample was determined using the apparatus represented in Fig 1. A three-necked round bottom flask was fitted with two reflux condensers that allowed nitrogen gas (N<sub>2</sub>) to enter the boiling chamber, then exit via an oil bubbler (not shown); this permitted N<sub>2</sub> gas to flow freely through the system while maintaining an anoxic environment at ambient pressure. An HH12B digital thermometer and a KTSS-HH

temperature probe from Omega (Stamford, CT) were fitted in the third flask opening. The digital temperature probe accuracy was reported by the manufacturer as  $\leq 1.3$  °C, and this was verified by measuring the BP values of three liquids at 1 atm pressure: water (BP: 100.0 °C), acetophenone (BP: 204 °C), and ethyl benzoate (BP: 214 °C). Standard deviation (SD) values for the triplicate PG and GL mixtures were found to be at most 0.5 °C, which is smaller than the probe accuracy (as reported by the manufacturer). Below 200 °C, the probe displayed four significant figures, including one decimal; above 200 °C, only three significant figures were displayed. The flask was held in a rheostat-regulated heating mantle; mixing was provided using a stir plate. The system was thoroughly flushed with N<sub>2</sub> gas prior to heating. Samples were gradually heated over 30 to 90 minutes while stirring continuously until boiling was observed. Boiling temperatures were determined as the stable temperature at which each sample exhibited a steady rolling boil for at least five minutes. Each system was then allowed to return to room temperature under N<sub>2</sub> gas. A "post-boiling" aliquot (10 µL) was taken for analysis by NMR. The pre- and post-boiling NMR samples were collected to ensure that the boiling process did not considerably alter composition.

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#### [Place Figure 1 here]

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# 2.4 1D <sup>1</sup>H NMR analyses

The NMR analyses conducted on each pre- and post-boiling 10  $\mu$ L aliquot (as diluted in 600  $\mu$ L of D<sub>2</sub>O) were carried out using a Bruker (Billerica, MA) Avance III spectrometer (599.90 MHz) with a 5 mm TXI probe. A pulse sequence of zg30 was used to acquire the data,

with the relaxation delay value (d1) set to 5 seconds, in combination with the 30°-observation pulse of the zg30 experiment to allow for full relaxation, and so reliable integrations.

All NMR spectra were processed using the software package MestReNova 9.0 (Santiago de Compostela, Spain; Mnova, 2016). Spectra were auto-phase corrected (but with manual adjustment as needed), followed by auto-baseline correction. Integral values were verified by manually correcting some spectra; the results of which were found to agree with the values from the corresponding auto-corrected spectrum values, to within 0.5%. Satellite peaks caused by the 1.1% natural abundance of <sup>13</sup>C overlapped with some peaks of interest, thereby potentially introducing error to the mole ratio calculation. This error was minimized by integrating peaks of interest and adjusting for the natural abundance of <sup>13</sup>C, allowing for more accurate measurements of mole ratios. This produced mole ratio measurements that were within 1.4 mol% of values based on the mass preparation method. The difference between the NMR-determined and predicted mol% GL (based on initial masses) was calculated; the absolute values of the differences were averaged for all trials to determine the average difference ( $\pm$ SD), which is 0.3  $\pm$ 0.3 mol% GL. Despite gravimetric sample preparation, NMR was used to assess post-boiling composition for analysis because these results were most closely associated in time with observed boiling.

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# 3. Results and Discussion

The overall precision of this BP determination technique was established for each method by calculating the standard deviation of triplicate boiling point (°C) values (Table 3). Standard deviation in terms of %GL for each method results in ≤0.2% for wt% GL (based on initial

mixture masses),  $\leq 0.4\%$  for the mol%, and  $\leq 0.5\%$  for the vol% (calculated using the mol% determined by NMR).

140 [Place Table III here]

BP values of PG and GL mixtures (*t*<sub>b</sub>, °C) shown in Fig 2 as BP vs. mol percent were fit with a Gibbs-Konovalov parameterization (Al-Jiboury, 2007; Malesiński, 1965)

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$$t_{\rm b}$$
 (°C) =  $x_{\rm PG}t_{\rm b,PG} + x_{\rm GL}t_{\rm b,GL} + x_{\rm PG}x_{\rm GL} \left(A + B(x_{\rm PG} - x_{\rm GL}) - C(x_{\rm PG} - x_{\rm GL})^2 + D(x_{\rm PG} - x_{\rm GL})^3\right)$  (2)

where  $t_{b,PG}$  and  $t_{b,GL}$  (°C) are the measured boiling points of pure PG and GL, respectively. Fit values of the coefficients A, B, C, and D for Equation 2 (i.e., using mol fraction composition) were obtained by minimizing the sum of the residuals using the Microsoft Excel *Solver* (Frontline Systems Inc., Incline Village, NV) add-in. Fit values were similarly obtained using volume and weight fraction values. Coefficients A-D are presented in Table 4. Corresponding calculated BP values are given in Table 5. Gibbs-Konovalov calculated values (Table 5) were compared to the Antoine equation values (Table 2) and found to differ by up to 6.7 °C at the upper range (beginning >230 °C), with an average difference ( $\pm$ SD) of 1.8  $\pm$  1.9 °C over the entire range.

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- 154 [Place Table IV here]
- 155 [Place Table V here]

## 4. Conclusions

The data obtained provide the BP values of PG+GL mixtures at 1 atmosphere pressure and smooth fitting allows prediction of BP for any composition (e.g., Table 5). Depending on composition, the minimum temperature required to produce an e-cigarette aerosol from a PG+GL liquid ranges from 188.6 to 292.0 °C; some effects from dissolved nicotine, flavor chemicals, and water will be operative.

## **Acknowledgements**

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Table I. Antoine Equation Parameters for Vapor Pressure po (bar) of the Pure Liquids Propylene Glycol (PG) and Glycerol (GL), with Applicable Temperature Ranges,  $\log_{10}(p^0)$ 

=A-B/(T+C). (1 atm = 1.01325 bar.) http://webbook.nist.gov/chemistry/

	t (°C) range	T(K) range	<u>A</u>	<u>B</u>	<u>C</u>	Reference
PG	45.6 - 188.3	318.7 - 461.4	6.07936	2692.2	-17.94	Richardson, 1886
GL	183.3 - 260.5	456.4 - 533.6	3.9374	1411.5	-200.566	Stull, 1947

Table II. Boiling Point Values
Assuming Raoult's Law (Ideal
Mixtures).
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 $p_{\text{TOT}}(T) = x_{\text{PG}}p_{\text{PG}}^{\circ} + x_{\text{GL}}p_{\text{GL}}^{\circ} = 213$ 1.01325 bar (=1 atm) For Antoine Equation Parameters in Table 1.

		Boili	ng Point
$\underline{x}_{\mathrm{PG}}$	$\underline{x}_{ ext{GL}}$	<u>t (°C)</u>	T(K)
1.00	0.00	188.0	461.2
0.95	0.05	189.6	462.8
0.90	0.10	191.3	464.4
0.85	0.15	193.1	466.2
0.80	0.20	194.9	468.1
0.75	0.25	196.9	470.1
0.70	0.30	199.1	472.2
0.65	0.35	201.4	474.6
0.60	0.40	203.9	477.1
0.55	0.45	206.7	479.8
0.50	0.50	209.6	482.8
0.45	0.55	212.9	486.1
0.40	0.60	216.6	489.8
0.35	0.65	220.7	493.9
0.30	0.70	225.4	498.6
0.25	0.75	230.9	504.0
0.20	0.80	237.3	510.4
0.15	0.85	245.1	518.2
0.10	0.90	254.8	528.0
0.05	0.95	267.8	540.9
0.00	1.00	286.4	559.6

Table III. Measured Boiling Point (BP) Values of Propylene Glycol (PG) and Glycerol (GL) Mixtures With Volume %, Weight %, and Mol % (N=3).

## % Glycerol (Average ± 1 SD)

		`	,
BP average ± SD (°C)	volume %	weight %	mol %
188.6 ± 0.6	$0 \pm 0$	$0.0 \pm 0.0$	$0.0 \pm 0$
191.6 ± 0.2	8.3 ± 0.1	$10.0 \pm 0.0$	$8.3 \pm 0.1$
194.7 ± 0.4	17.3 ± 0.2	$20.1 \pm 0.0$	$17.3 \pm 0.2$
198.6 ± 0.2	26.1 ± 0.2	$30.0 \pm 0.0$	$26.2 \pm 0.2$
$203 \pm 0.0$	$35.8 \pm 0.2$	$40.1 \pm 0.1$	$35.8 \pm 0.2$
$208 \pm 0.6$	45.5 ± 0.1	$49.9 \pm 0.0$	$45.6 \pm 0.1$
$214 \pm 0.0$	$55.8 \pm 0.4$	$60.0 \pm 0.0$	$55.9 \pm 0.4$
$223 \pm 0.6$	$66.4 \pm 0.4$	$69.9 \pm 0.0$	$66.4 \pm 0.4$
$236 \pm 0.0$	77.6 ± 0.5	$80.0 \pm 0.0$	$77.6 \pm 0.4$
$258 \pm 0.6$	$89.2 \pm 0.2$	$90.0 \pm 0.2$	$89.2 \pm 0.2$
$292 \pm 0.0$	99.9 ± 0.1	$100.0 \pm 0.0$	$99.9 \pm 0.1$

# Table IV. Coefficients Determined for Gibbs-Konovalov Parameterization of Propylene Glycol (PG) and Glycerol (GL) Boiling Point Data.

	coefficient						
	Α	B	C	D			
vol %	-119.9	-87.3	55.8	-22.6			
wt %	-130.3	-100.8	66.9	-10.6			
mol %	-119.9	-87.3	55.9	-22.5			

Table V. Calculated Boiling Point (BP) Values (°C) for Propylene Glycol and Glycerol (GL)
Mixtures by Volume, Weight, and Mole Percent GL using Coefficients A-D in Table 4, and
Equation 2.

% GI	0	5	10	15	20	25	30	35	40	45	50	%GL
(C)	189	190	192	194	196	198	200	202	205	207	210	vol %
BP (°C)	189	190	191	193	195	197	199	201	203	205	208	wt %
B	189	190	192	194	196	198	200	202	205	207	210	mol %
% GI	55	60	65	70	75	80	85	90	95	100		%GL
S _	<b>55</b> 213	<b>60</b> 217	<b>65</b> 221				<b>85</b> 249		<b>95</b> 274			%GL <i>vol</i> %

Figure 1. Schematic of Boiling Point (BP) Setup. Thermometer in third port represents a digital thermometer.

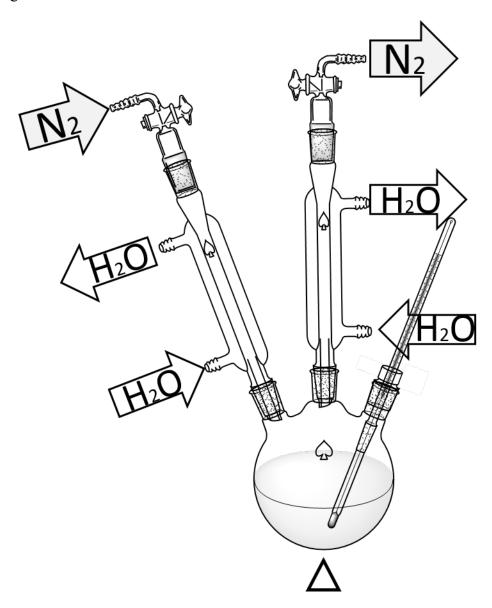
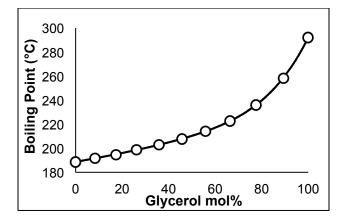


Figure 2. Averages of Triplicate Boiling Point Measurements for Mixtures Composed of Propylene Glycol (PG) and Glycerol (GL). Mole percent GL post-boiling was determined by NMR analysis. Error bars as ±1 SD are too small to be seen.



236 237	Figure 1. Schematic of Boiling Point (BP) Setup. Thermometer in third port represents a digital thermometer.
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239 240 241	Figure 2. Averages of Triplicate Boiling Point Measurements for Mixtures Composed of Propylene Glycol (PG) and Glycerol (GL). Mole percent GL post-boiling was determined by NMR analysis. Error bars as ±1 SD are too small to be seen.

## **Supporting information**

S1 Figure. Comparison Between Pre- and Post-Boiling Compositions in terms of Percent Glycerol (GL) for Propylene Glycol (PG) + GL Mixtures. Average Percent GL, N=3, as Determined by NMR ( $^{\circ}$ PG = 100 $^{\circ}$  -  $^{\circ}$ GL).

mol % glycercol

11101 70 5		
pre-	post-	
boiling	boiling	Idifferencel
0.0	0.0	0.0
8.3	8.3	0.0
16.8	17.3	0.5
25.8	26.2	0.4
35.2	35.8	0.6
44.7	45.6	0.9
55.0	55.9	0.9
65.4	66.4	1.0
76.3	77.6	1.3
87.7	89.2	1.5
99.9	99.9	0.0

PG+GL mixtures were prepared by mass; however, due to differences between pre- and post-boiling composition, the post-boiling molar quantities were used to relate boiling point and (mol% and vol%) compositions. The values for 0, 8.3, and 99.9 mol% GL (0,10, and 100 wt% GL) remained constant with respect to pre- and post-boiling composition, while the 16.8-87.7 mol% GL (20-90 wt% GL) increased by 0.4 – 1.5 mol% with respect to mol% GL. This effect is likely due to the lower vapor pressure of PG.