

A Novel Combination of Surfactant Addition and Persulfate-assisted Electrokinetic Oxidation for Remediation of Pyrene-Contaminated Soil



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Effect of surfactant addition on persulfate-assisted electrokinetic remediation of pyrene-spiked soil was studied. The influence of effective factors including voltage, surfactant addition, moisture content, and persulfate concentration on the removal of initial pyrene concentration of 200 mg kg⁻¹ were investigated. A complete pyrene removal was observed for voltage of 1 V cm⁻¹, saturated conditions, Tween 80 concentration of 20 mL kg⁻¹, and persulfate concentration of 100 mg kg⁻¹ after 24 h, corresponding to pyrene mineralization of 61 %, based on TPH analysis. The experimental results were best fitted with pseudo-first-order kinetic model with correlation coefficient of 0.968 and rate constant of 0.191 min⁻¹. The main intermediates of pyrene degradation were benzene o-toluic acid, acetic, azulene, naphthalene and decanoic acid. Finally, an unwashed hydrocarbon-contaminated soil was subjected to persulfate-assisted electrokinetic remediation, and a TPH removal of 38 % was observed for the initial TPH content of 912 mg kg⁻¹, under the selected conditions.

Keywords:

soil remediation, electrokinetic oxidation, persulfate, surfactant, pyrene

Introduction

Pyrene is a polycyclic aromatic hydrocarbon (PAH) which may be produced commercially to be utilized as an intermediate in the production of pigments or it can be found in emissions of incomplete combustion of kerosene and diesel. The crystalline structure of pyrene (C₁₆H₁₀) is a four-ring PAHs that is solid at room temperature due to different neutrons^{1,2}. The long-term and continuous emission of PAHs into the environment can pose a serious threat to human health and environment through air pollution or soil contamination pathways, e.g., through industrial discharges and some agricultural tradi-

tions and improper practices of waste disposal^{3,4}. Thus, the quick and effective removal of PAHs from the environment as well as reducing their adverse effects seems to be necessary. Three- and four-ring PAHs are in particular associated with soil particles, and due to their low aqueous solubility and high sorption properties, their removal from subsurface environments using traditional technologies, such as soil washing, conventional chemical oxidation or bioremediation, is inefficient⁵. In fact, their removal from fine soil particles is still a major challenge for geo-environments, because of the high variation in their hydraulic conductivity, a lot of specific contaminants, environmental and dynamic conditions, reversible geochemical processes, and the interactions between soil particles and contaminants^{6,7}.

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Until now, different physicochemical, thermal, and biological methods have been applied for decontamination of polluted soils. However, these methods are often costly and energy-intensive, and are almost ineffective and could, in turn, remain secondary toxic materials, which are potentially harmful to the environment^{8–11}. Thus, electrochemical removal has been considered as a reliable technology for the remediation of contaminated soils^{12,13}. The main advantages of electrokinetic remediation (EK remediation) of soil contaminated with petroleum hydrocarbons is that the procedure can be performed as an *in-situ* or *ex-situ* technology, in soils with heterogeneous texture and low permeability, or in saturated and unsaturated soils. It is also possible to use electrochemical oxidation for simultaneous removal of heavy metals, radionuclides, and organic pollutants. Flexibility of this technology, high energy efficiency, and cost-effectiveness are also merited^{14,15}. EK remediation includes the flow of electrical current in the soil, liquid pole electro-osmotic migration, electrical migration of ions, charged particles and colloids, electrolysis of water in the soil in the vicinity of the electrodes, migration of hydrogen and hydroxide ions into the soil resulting in temporary changes in soil pH, gas production at the electrodes, development of the non-uniform electric field, as well as the production of electro-osmotic flow^{16,17}. In EK decomposition of water reactions, oxygen and hydrogen ions (H^+) are produced due to oxidation at the anode, while hydrogen gas and hydroxide ions (OH^-) are made because of the reduction in cathode^{18,19}. One of the problems in EK remediation of soil contaminated with organic compounds is that PAHs are hydrophobic, thus reducing the efficiency of the process. One of the approaches in order to enhance the solubility of PAHs is the application of intermediate facilitating factors, such as surfactants^{20,21}. Addition of these factors leads to creation of some changes in the fluid properties, such as dielectric constant, pH, fluid viscosity, as well as changes in surface properties of soil particles^{22,23}. Among the surfactants, non-ionic materials have been widely used for transferring non-polar organic substances by electro-osmotic flow. Indeed, surfactants have lower dielectric constant and higher viscosity than water. Consequently, the addition of these facilitators not only reduces the electro-osmotic flow, but also increases the solubility of PAHs²⁴. Another problem concerning EK remediation is the great amount of time required to remove contaminants from the soil. This problem could be solved in the EK remediation process using other oxidations. The application of persulfate as an oxidizing agent can improve the efficiency and significantly reduce the required time for soil

decontamination^{25,26}. The process of oxidation by means of activated persulfate is a promising approach, due to stability, reactivity, solubility, oxidizing properties, and high amount of organic matter degradation²⁷. Persulfate ($S_2O_8^{2-}$), with standard oxidation potential of $E^0 = 2.01 V$, is a novel approach applied in chemical oxidation, and has been considered a promising remediation technique of recalcitrant organics. Moreover, $S_2O_8^{2-}$ activation leads to production of sulfate radical ($SO_4^{\cdot-}$; $E^0 = 2.7 V$), as a strong oxidant for the degradation of organic matter, even at neutral pH values, and acts more selectively for destruction of compounds with carbon-carbon double bonds and benzene rings^{28,29}. Persulfate activation would be carried out via different approaches, such as heat, metal and base transition (elevated $pH > 11$), UV-radiation, electron-beam and ultrasonication³⁰. For soil remediation, UV irradiation is not capable of penetrating the soil matrix, and alkaline activation requires high quantities of alkaline substances. Furthermore, transition of metal-catalyzed activation (e.g., Fe^{2+}) exhibits best results in strict pH value range of 2–4, and metal can act as a radical scavenger³¹. Thermally activated persulfate is known as a green source of sulfate radicals and has been previously applied to remove organic pollutants³². Thermal activation of persulfate also has many benefits, like the enhancement of solubility of slightly soluble PAHs, increase in efficiency of reaction and mineralization, and the consumption of fewer chemical substances³³. Because of the heat generation through EK remediation, persulfate activation can be accomplished at the same time.

Integrated EK remediation with persulfate can be used to overcome limitations of conventional EK remediation and facilitate the distribution of persulfate in soils with low permeability. At the same time, it can directly cause oxidation-reducing reactions in the soil³⁴. This study is intended to remediate pyrene-contaminated soil using persulfate-assisted EK remediation, and to use its results for the unwashed real hydrocarbon-polluted soils.

Materials and methods

Chemicals

All chemicals applied in the present research, including pyrene, sulfuric acid, soda, methanol, n-hexane, acetone, Tween 80, acetonitrile and sodium persulfate were analytical-grade purchased from Merck, Germany, and all solutions were prepared with deionized water and kept at 4 °C, prior to experiments.

Soil sample

All soils were obtained from an oil manufacturing district in southern Iran. The soil samples were collected from the upper layers (0–40 cm) by soil cores, air-dried, and passed through a 2-mm sieve. The process of homogenization of soil grains was then performed by a shaker, followed by washing thrice with acetone, autoclaving, and storing in non-reactive plastic bags at 4 °C. Since the washed soil still contained pyrene, a determined amount of pyrene was dissolved in n-hexane and added to the soil to achieve a final soil concentration of 200 mg kg⁻¹ in all samples. It was mixed vigorously and left under hood for 24 h until the n-hexane evaporated. The pyrene stock solution was added to a shaker for 1 minute before spiking³⁵. Also, an unwashed soil sample of the same origin and without washing was used as naturally contaminated soil. The X-ray diffraction (XRD) patterns of the soil sample were recorded by X-ray diffractometer (Model: GNR-MPD3000) using Cu anode at $\lambda = 0.15060$ nm, voltage = at 40 kV, and current intensity = 30 mA. X-ray Fluorescence (XRF) was applied for finding the chemical substances of soil particles. The pyrene and its degradation metabolites were also determined by GC-MS (Model: Agilent 7890, USA) with HP-5MS capillary column (30 m × 0.25 mm × 0.25 μm film thickness, 5 % Phenyl – 95 % Methyl Siloxane phase). The carrier gas (helium) was fed with a fixed 1 mL min⁻¹ flow rate. The oven temperature was fixed to 40 °C for 1 min, followed by an enhancement to 300 °C at 5 °C min⁻¹ and kept constant for 3 min. Ultimately, the sample was poured in instrument with 10:1 splitting ratio. Mass spectra were obtained by electron impact (EI) at 70 eV with the full scan mode.

Lab-scale experimental setup

The reactor was a cube Plexiglas chamber (Supplementary file S1) consisting of 10 houses, each with a length of 30 cm, width of 10 cm, and height of 20 cm, divided into 10 completely equal sections using nine separating walls in the longitudinal sector. Other facilities in the reactor included 2 pairs of graphite electrodes with a thickness of 4 mm, width of 4 cm, and length of 15 cm for each section, and a DC power supply (Model: Zx 200). The voltage was adjustable between 0–100 V cm⁻¹.

Experimental procedure

All the experiments were carried out in batch mode operation. In fact, for determination of the optimum conditions of the experimental factors, such as voltage (0.3 – 1.5 V cm⁻¹), moisture content (10 – 100 %), effect of Tween 80 as a chemical surfactant (0 – 40 mL kg⁻¹), effect of sodium persulfate

(0 – 100 mg kg⁻¹) and reaction time (0–120 h) on pyrene removal, were investigated consecutively based on one factor at a time experimental design. Additionally, an unwashed soil sample was subjected to persulfate-assisted EK remediation based on the selected conditions.

Analytical methods

The remaining concentrations of pyrene in the soil samples were extracted using an ultrasonic instrument based on EPA method 3550B³⁶. Briefly, the sample was put in a special tube containing n-hexane and acetone with 1:1 v/v ratio. With completion of extraction, the process of centrifugation of sample was carried out for 10 min at 6000 rpm, followed by filtration using polytetrafluoroethylene (PTFE). A specific amount of filtered solution was separated in order to perform the analysis. The pyrene concentration was obtained using gas chromatography (GC) system (Chrompack CP 9001) equipped with a flame ionization detector (FID) using (HP-5) capillary column (30 m, 0.32 mm i.d. and 0.2 μm film thickness). Nitrogen was used as carrier gas at a rate of 2 mL min⁻¹. The temperature program was as follows: column temperature was held at 120 °C for 1 min, and then raised to 240 °C at a rate of 20 °C min⁻¹, then held for 1 min. The temperatures of injector and detector were fixed at 250 and 300 °C, respectively. Removal was analyzed through quantifying initial and final pyrene concentration according to Eq. (1):

$$R(\%) = \left(\frac{C_0 - C_t}{C_0} \right) \cdot 100 \quad (1)$$

where, C_0 and C_t are the initial and residual pyrene concentrations (mg L⁻¹). Pyrene recovery rate was about 85 % immediately after spiking. Considering the value of 15 % as a non-extracted portion of pyrene from the soil, we multiplied all raw data by a factor of 1.15. Soil moisture, EC, and pH were analyzed based on ASTM (D4972-13)³⁷. The soil texture was determined according to the method described by ASTM (D6913M-17)³⁸.

Results and discussion

Soil analysis

Some selected chemical and physical characteristics of the soil are presented in Table 1. Accordingly, the studied soil with 32 % clay was of the clay-loam. SiO₂ and CaO also accounted for most of the mineral parts of the soil. LOI of 22 % made a significant portion of the soil mass. This was because the soil was contaminated with different types of petroleum compounds. Furthermore, the pres-

Table 1 – Characteristics of the soil sample along with XRF results

Characteristic	Value (%)
Clay	32
Silt	37
Sand	31
Moisture	27.8
EC ($\mu\text{S cm}^{-1}$)	76000
pH	6.8
Na	4.4
TiO ₂	0.28
MgO	4.8
Cl	7.5
Fe ₂ O ₃	3.3
Al ₂ O ₃	4.5
K ₂ O	1.5
L.O.I	22.6
SiO ₂	26.5
CaO	24.3
La and Lu	>

ence of 5.7 wt % of chloride ions indicated severe salinity of the studied soil. According to the results of XRD analysis (results are not presented and can be found in supplementary files), the dominant crystalline phases of soil samples included calcite (CaCO₃), quartz (SiO₂), halite (NaCl), dolomite (CaMg (CO₃)₂), gypsum (CaSO₄ · 2H₂O) and clays.

EK remediation

The results indicated that any changes in the applied voltage directly affected the electro-osmotic flow in a way that, with an increase in voltage, the electro-osmotic flow increased. Voltage changes, however, have the maximum effect on the soil geochemical characteristics that critically affect the electro-osmotic flow. Moreover, the voltage of 1 V cm⁻¹ promotes the development and maintenance of the electro-osmotic flow during the reaction^{39,40}. Effect of voltage in the range of 3.0 to 1.5 V cm⁻¹ on the efficiency of the EK remediation process in removing pyrene from soil was examined. All the other variables, including natural soil pH equal to 7 ± 0.3, reaction time of 120 h, initial pyrene concentration of 200 mg kg⁻¹, humidity of 50 %, and zero concentrations of Tween 80 and persulfate were kept constant. Pyrene removal efficiency increased as the voltage increased, but no significant difference was observed between the voltages 1 and 1.5 V cm⁻¹ (*p* value > 0.05). Pyrene removal efficiencies in 0.3, 0.5, 0.7, 1, and 1.5 V cm⁻¹ were 28, 31, 40, 46 and 47.5 %, respectively (Fig. 1a).

At the beginning of the reaction, due to the movement of the electro-osmotic flow from the anode towards the cathode, ionic migration of the contaminants exhibited an increasing trend^{41,42}. In fact, due to the stronger electric field and the resulting higher current density through the electrodes, most of the processes associated with the removal of contaminants, such as electro-osmosis and electrical migration, occur more efficiently and thus more contaminants are eliminated⁴³.

In effect, the high natural EC in loamy soils contributed to the high electro-osmotic flow at the beginning of the reaction. After the maximum streaming, access of water pole and moving ions (H⁺ and OH⁻), due to the electrolysis of water molecules and deposition of ions in the area of the cathode, decreased and resulted in reduced electric current and constant amount of pollutant removal⁴⁴. In this study, due to lower power consumption and non-significant difference (*p* value > 0.05) in removal efficiency of voltages 1 and 1.5 V cm⁻¹, we alternatively selected voltage of 1 V cm⁻¹ for the rest of the experiments. In addition, pseudo-first-order degradation rate constants were 0.0045 and 0.0046 h⁻¹ for voltages of 1 and 1.5 V cm⁻¹, respectively, indicating a non-significant difference between them (Fig. 1b).

Effect of moisture content

In the selected conditions including voltage of 1 V cm⁻¹, and the other variables, such as pyrene concentration of 200 mg kg⁻¹, reaction time of 120 h, natural soil pH equal to 7±0.3, zero concentration of Tween 80 and sodium persulfate, the effect of moisture content in the range of 10 %, 25 %, 50 % and 100 % on the efficiency of the EK remediation for pyrene removal were studied. Pyrene removal efficiency for moisture contents of 10, 25, 50 and 100 % were 15, 29, 45, and 64 %, respectively (Fig. 1c). The higher the moisture content, the greater is the electrical current established, and thus the more H⁺ ions are produced⁴⁵. When an electric field is established in moist soils, electrolysis of water molecules occurs, which reduces the moisture content of the soil. Changes in moisture content took place in the cathode, due to the electro-osmotic flow of water molecules from the anode to the cathode. Although the electro-osmotic streaming reduces with increasing pH and ion concentration in the liquid, the higher the current, the more efficient is the contaminants removal process⁴⁴. Rather than removal efficiency, which was the highest in moisture content of 100 %, the reaction rate constant was much higher for saturation condition (0.0087 h⁻¹) compared to moisture content of 50 % (0.0043 h⁻¹) (Fig. 1d). Therefore, the moisture content of 100 % was selected for the rest of the experiments.

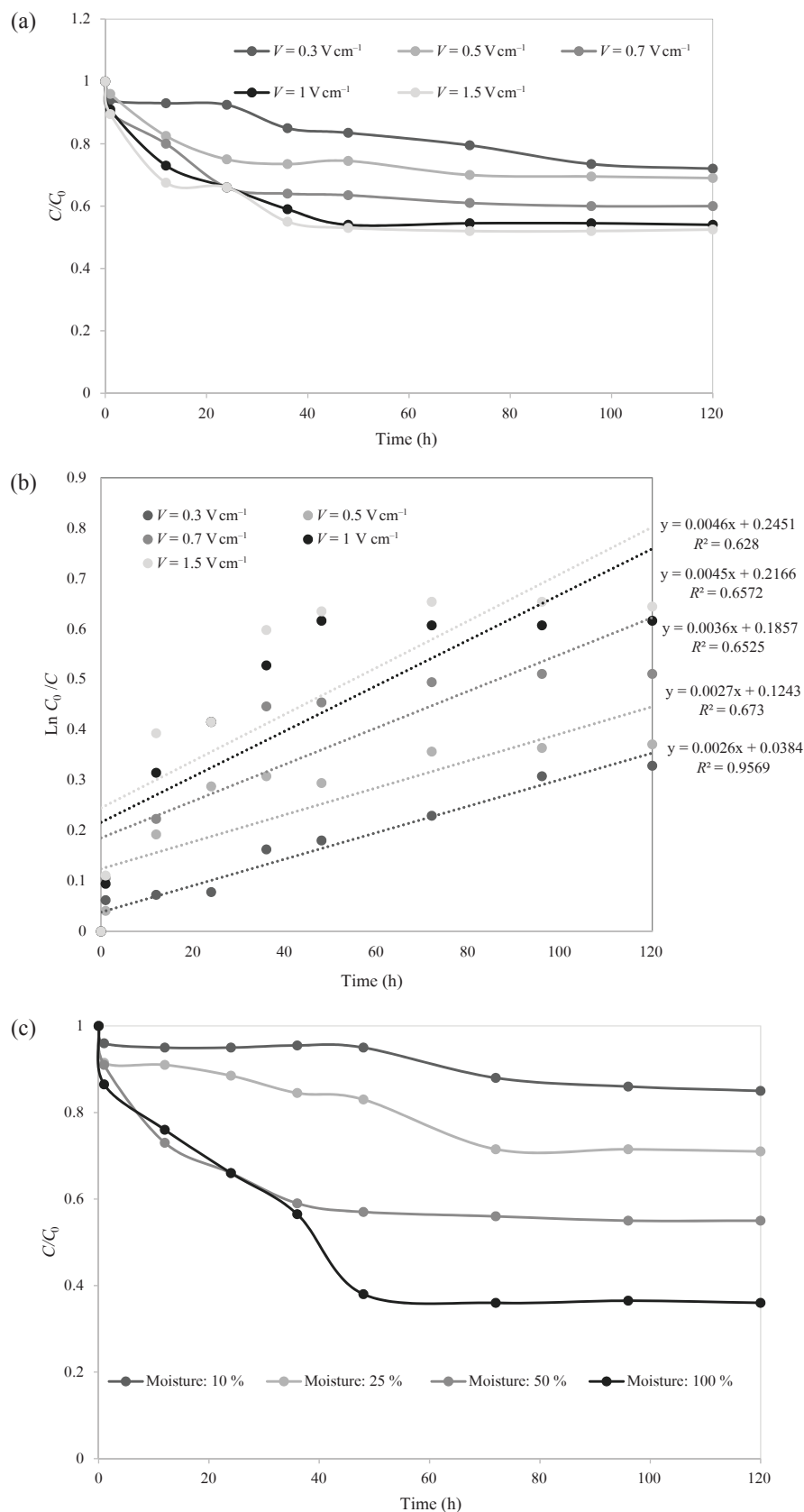


Fig. 1 – Effect of operating parameters on pyrene removal through EK remediation; initial pyrene: 200 mg kg^{-1} , pH: 7 ± 0.5 , reaction time: 120 h, a) effect of voltage variations, and b) pseudo-first-order kinetic modeling, Tween 80: 0 mg kg^{-1} , persulfate: 0 mg kg^{-1} , moisture: 50 %, c) effect of moisture content, and d) pseudo-first-order kinetic modeling, Tween 80: 0 mg kg^{-1} , persulfate: 0 mg kg^{-1} , voltage: 1 V cm^{-1} , e) effect of Tween 80, and f) pseudo-first-order kinetic modeling, persulfate: 0 mg kg^{-1} , voltage: 1 V cm^{-1} , moisture content: 100 % g) effect of persulfate addition, and h) pseudo-first-order kinetic modeling, Tween 80: 20 mL kg^{-1} , voltage: 1 V cm^{-1} , moisture content: 100 %

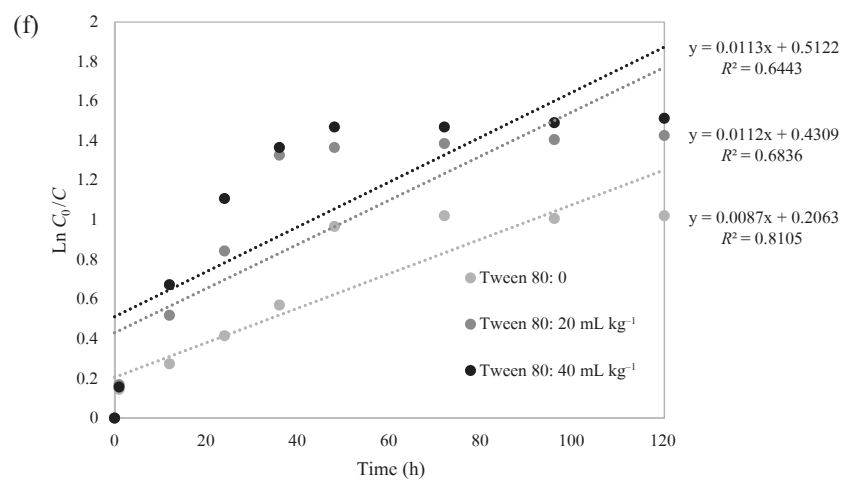
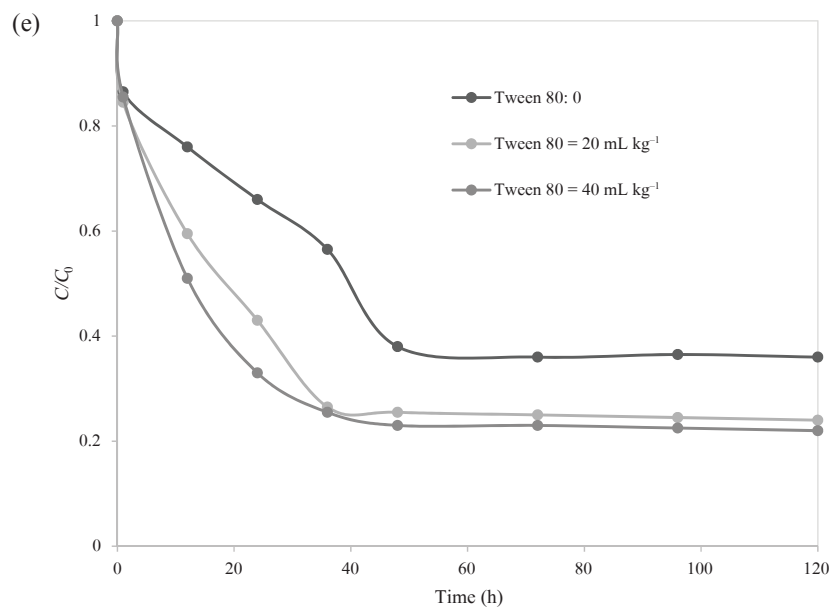
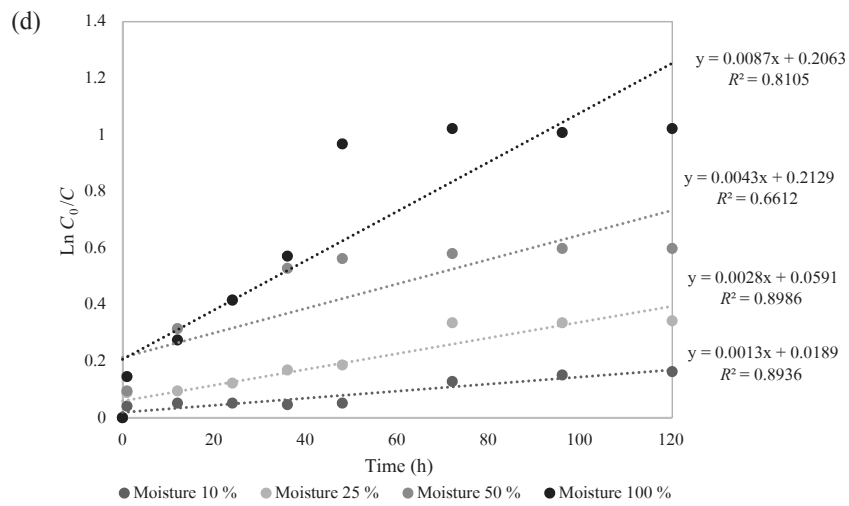


Fig. 1 – Continued.

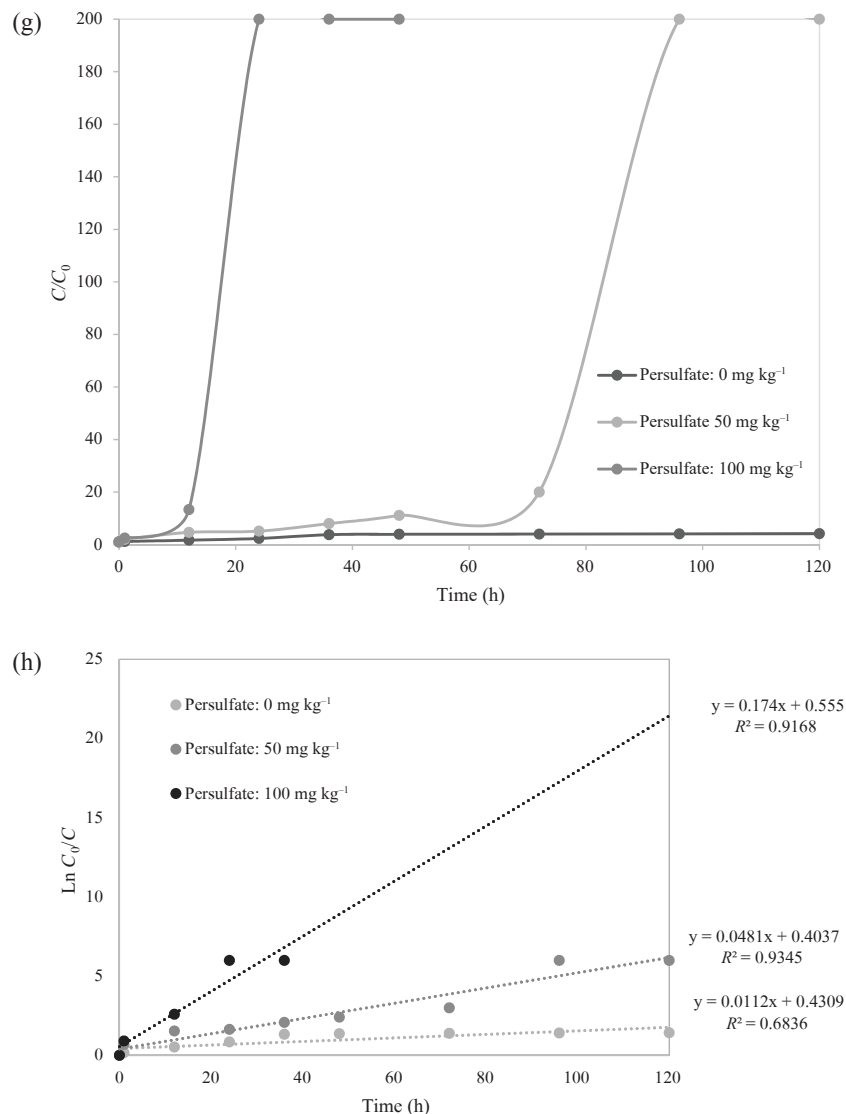


Fig. 1 – Continued.

Effect of Tween 80 addition

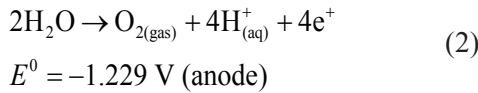
In the selected experimental conditions as mentioned previously, the effect of adding Tween 80 concentrations of 20 and 40 mL kg⁻¹ in pyrene removal using EK remediation was investigated. Pyrene removal efficiency for Tween 80 concentrations of 20 and 40 mL kg⁻¹ were 76 and 78 %, respectively (Fig. 1e), compared to 64 % removal without surfactant addition. Surfactant used in the EK process was affected by chemical oxidation and reduction, and thus decomposed with pyrene and became harmless or low-risk material. In general, surfactant enhanced the water solubility of pyrene. Higher concentration of surfactant than the critical concentration of its micelle increases the mobility of the polycyclic aromatic hydrocarbons within the aqueous phase, and therefore increases the pyrene removal efficiency⁴⁶. Results of several studies have

shown that without addition of surfactant, contaminant decomposition was limited⁴⁷. Adding a small amount of Tween 80 can facilitate the decomposition of endosulfan contamination by using bacteria. In effect, increasing the concentration of Tween 80 will not make a significant difference in removal efficiency⁴⁸. Since an insignificant difference was observed between the removal efficiency as well as the reaction rate constant in Tween 80 concentrations of 20 mL kg⁻¹ and 40 mL kg⁻¹ (Fig. 1f), the value of 20 mL kg⁻¹ was selected due to less usage of chemical.

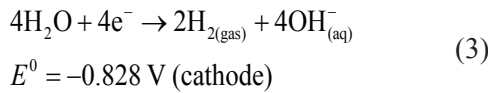
EK remediation is based on various mutual mechanisms, but the principal electron transfer reactions that occur at electrodes during the process is the electrolysis of water upon electric field application. Water decomposition (electrolysis reactions) occurs at the electrodes. The electrolysis reactions

produce oxygen gas and hydrogen ions (H^+) derived from oxidation at the anode, and produce hydrogen gas and hydroxyl (OH^-) ions because of the reduction at the cathode, as illustrated in Eqs. 2 and 3:

At anode (oxidation):



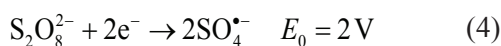
At cathode (reduction):



Effect of persulfate addition

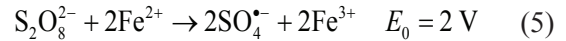
In the selected experimental conditions including voltage of $1V \text{ cm}^{-1}$, saturated moisture, Tween 80 concentration of 20 mL kg^{-1} , pyrene concentration of 200 mg kg^{-1} , reaction time of 120 h, natural soil pH equal to 7 ± 0.3 , and the effect of sodium persulfate in two concentrations of 50 and 100 mg kg^{-1} on EK remediation of pyrene was studied. Pyrene removal efficiencies for sodium persulfate concentration of 50 mg kg^{-1} and 100 mg kg^{-1} were 100 % that were obtained after the reaction time of 96 and 24 h, respectively (Fig. 1g and h). Firstly, persulfate moves to the soil by the electrical or electro-osmotic migration, and then it is activated by temperature and pH^{49,50}. For activation of persulfate, it is necessary to make sure that the temperature is $45 \text{ }^\circ\text{C}$. These conditions can be achieved in an electric field. As a result of high-voltage gradient, soil heats and acid is produced in the anode, which causes soil acidification and, thus, higher removal efficiency is obtained⁵¹.

In an electric field, the incomplete solubility of salt deposits, and the mobility of sodium persulfate ions leads to the production of higher amounts of ion concentration in water. On the other hand, the amount of electrical current is reduced over time, due to the electrical migration of ions towards the electrodes. However, with addition of sodium persulfate, the electrical current significantly increased, as a result of increasing interstitial fluid concentration^{45,52,53}. Persulfates have a high potential without activation, as shown in Eq. (4):

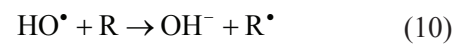
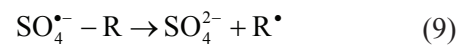
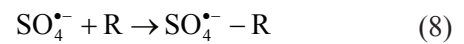
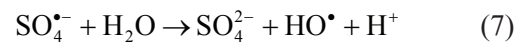


Persulfate provides more oxidation potential when it is activated via an activator like heat or Fe ions. Since the studied soil contained Fe_2O_3 iron oxides, based on XRF analysis, a possible pathway of persulfate activation is iron-based activation. The mechanism of persulfate activation through iron is as follows (Eq. (5)), which yields sulfate radicals

with higher oxidation potential, in comparison to persulfate.



Thermal activation of persulfate in EK oxidation is also a possible mechanism, due to increasing temperature. The mechanism of persulfate oxidation via heat catalysts, which caused sulfate radicals generation to remove pyrene, can be expressed via Eqs. (6–10) as follows⁵⁴:



Based on Eq. 6, persulfate can be catalyzed by heat which caused production of free radicals of $SO_4^{\bullet-}$ ⁵⁵. The production of sulfate radicals in solution could cause the production of the hydroxyl radical (HO^{\bullet} , $E^0 = +2.7 \text{ V}$) through radical inter-conversion reactions⁵⁶. According to Eqs. 9 and 10, both $SO_4^{\bullet-}$ and HO^{\bullet} radicals are responsible for oxidation of recalcitrant organic matter in the heat-activated persulfate oxidation process.

Variations of soil pH

The soil pH of the lab-scale EK setup varied as expected. The soil pH near the anode was 3.82, while the pH near the cathode was about 10.22. The produced protons (H^+) and hydroxyl (OH^-) ions via electrolysis reactions (Eqs. 1 and 2) transported to the electrodes with different charges. In general, the mobility of protons is two times greater than hydroxyl ions, so the protons dominate the system and an acid front moves across the soil until it meets the hydroxyl front in a district close to cathode, where the ions may recombine to generate water. Therefore, the soil sample is separated in two different parts having various pH values, namely, high and low pH zones close to cathode and anode, respectively. The certain amounts of soil pH are highly dependent on the intensity of protons and hydroxyl transport, as well as soil geochemical features⁵⁷.

Kinetic study

Pseudo-first-order and pseudo-second-order models were applied for kinetic studies of pyrene degradation via plotting $-\ln(C_0/C_t)$ and $1/C_t$ versus time, respectively (Fig. 2a and b), in the selected experimental conditions such as pH value of 7 ± 0.3 , persulfate concentration of 100 mg kg^{-1} , pyrene con-

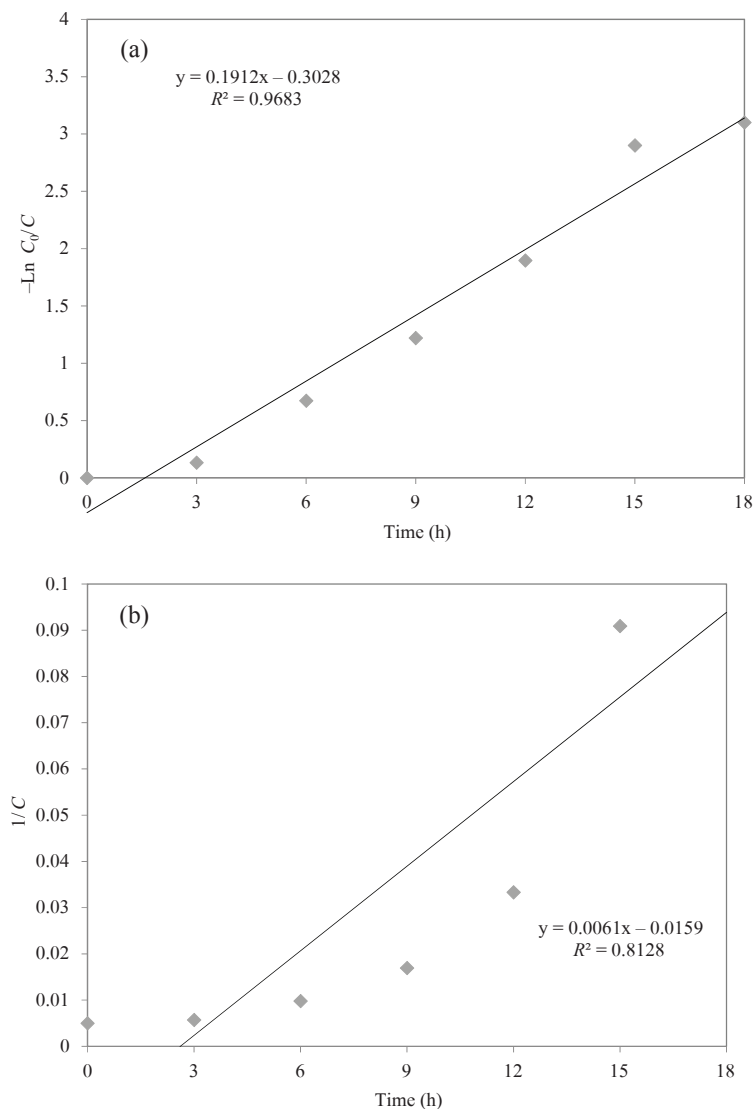


Fig. 2 – Kinetic analysis for persulfate-assisted EK of pyrene: 200 mg kg⁻¹, Tween 80: 20 mL kg⁻¹, pH: 7± 0.3, reaction time: 24 h, voltage: 1 V cm⁻¹, moisture content: 100 %

centration of 200 mg kg⁻¹, Tween 80 concentration of 20 mL kg⁻¹, reaction time of 24 h, voltage of 1 V cm⁻¹, and moisture content of 100 %. The equations of each kinetic model (Eq. (11), pseudo first-order and Eq. (12), pseudo second-order) are as follows^{58,59}:

$$\ln C_0 / C_t = k_1 t \quad (11)$$

$$1 / C_t - 1 / C_0 = k_2 t \quad (12)$$

where, C_0 and C_t are the initial and residual pyrene concentrations (mg kg⁻¹), respectively, t is the reaction time (min), and k_n is the corresponding rate constants ($n = 1$ and 2). The reaction kinetics of pyrene removal through the persulfate-assisted EK remediation of pyrene-contaminated soil was best fitted for pseudo first-order reaction with the regression coefficient of 0.968 and rate constant of 0.191 min⁻¹.

Mineralization and intermediates of pyrene degradation

Intermediates of persulfate-assisted EK remediation of synthetically pyrene-contaminated soil were studied in selected experimental conditions and time intervals 4 and 24 h. A GC-MS analysis was performed exactly 4 h after beginning of the reaction (Fig. 3b). The main intermediate metabolites at this time were obtained as benzene (C₆H₆), o-toluic acid (C₈H₈O₂), acetic acid (C₂H₄O₂), cyclopenta cycloheptene (azulene) (C₁₀H₈), 1,3-cyclopentadiene (C₅H₆), 2-ethyl-pyridine (C₇H₉N), naphthalene (C₁₀H₈), decanoic acid (C₁₀H₂₀O₂), 1-chloropyrene (C₁₆H₉Cl) and pyrene (C₁₆H₁₀). It is obvious that pyrene degradation had been preceded and simpler compounds and aliphatic hydrocarbons had formed. In addition, the presence of 1-chloropyrene can be attributed to the binding of Cl⁻ produced from electrolysis reaction of saline soil and pyrene. It was found from Fig. 3c that the main final products of pyrene degradation through persulfate-assisted EK remediation were benzoic acid (C₇H₆O₂), dimethyl phosphinic azide (C₂H₆N₃OP), methoxyacetic acid (C₃H₆O₃), and hexadecane (C₁₆H₃₄). Similar to the quantitative analysis, pyrene was fully removed after 24 h and converted to aliphatic and simpler components. Results indicated high mineralization rate, based on TPH analysis using Eq. 13:

$$\text{Mineralization (\%)} = P_0 - \text{TPH} / P_0 \cdot 100 \quad (13)$$

where, P_0 is initial pyrene concentration and TPH represents the residual total petroleum hydrocarbons after oxidation. Based on the experimental results, TPH content of remediated soil sample was 92 mg kg⁻¹, corresponding to mineralization rate of 61 % in selected experimental conditions (Fig. 4).

Energy consumption

One of the most important issues in EK processes is the energy consumption, which affects the scale-up and full scale applications of this technology, since the high cost of energy is a limiting factor. Upon selecting the operating conditions in the lab-scale study, the energy consumption (P , kWh kg⁻¹) was calculated using Eq. (14):

$$P = V I t / M \cdot 1000 \quad (14)$$

where, V is the cell voltage (V cm⁻¹), I is the average cell current (A), t is the electrolysis time (h) and M is the remediated soil mass^{60–62}. Energy consumption was calculated in the selected experimental conditions, such as initial pH value of 7 ± 0.3, voltage of 1 V, current intensity of 0.8 A, initial pyrene

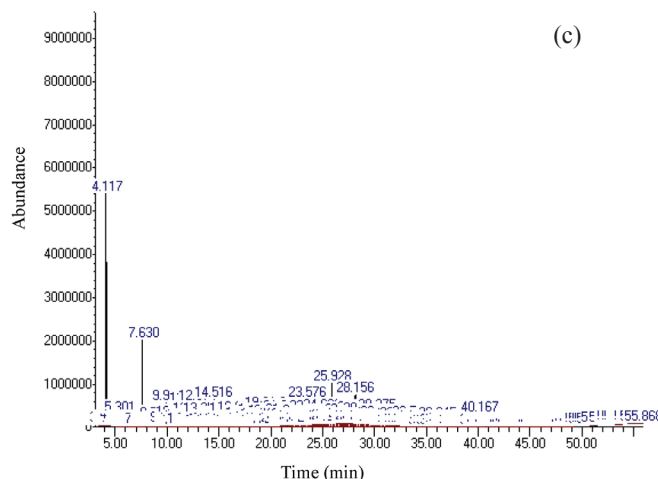
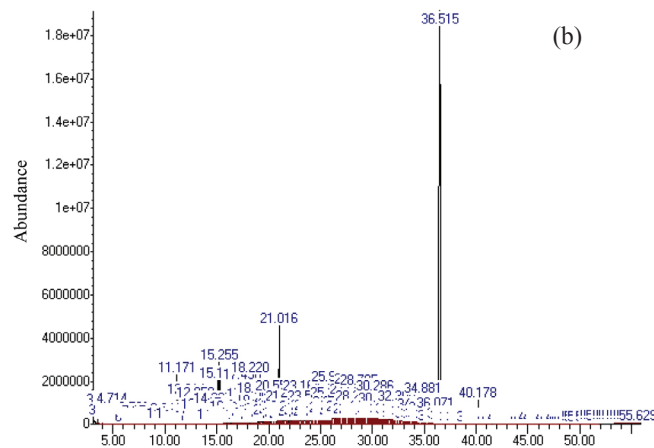
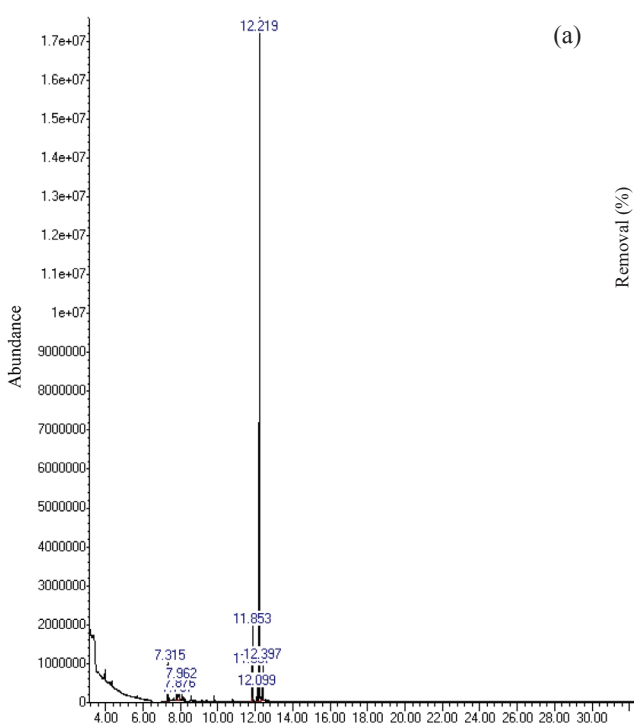


Fig. 3 – GC-MS analysis of a) unwashed soil, b) persulfate-assisted EK remediation within 4 h, and c) persulfate-assisted EK remediation within 24 h under the selected conditions (Tween 80: 20 mL kg⁻¹, pH: 7 ± 0.3, voltage: 1 V cm⁻¹, moisture content: 100 %, persulfate: 100 mg kg⁻¹)

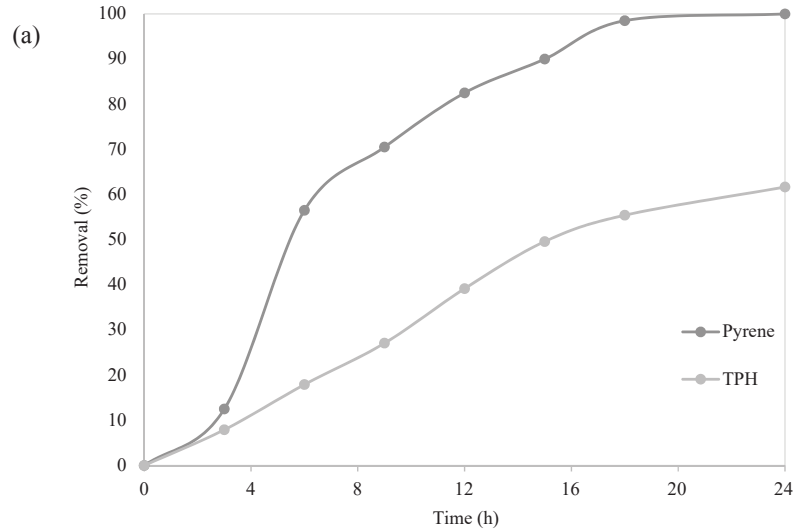


Fig. 4 – Comparison of pyrene and TPH removal using persulfate-assisted EK remediation in the same selected conditions (Tween 80: 20 mL kg⁻¹, pH: 7 ± 0.3, voltage: 1 V cm⁻¹, moisture content: 100 %, persulfate: 100 mg kg⁻¹)

concentration of 200 mg kg⁻¹, persulfate concentration of 100 mg kg⁻¹, Tween 80 content of 20 mL kg⁻¹, reaction time of 24 h, soil mass of 0.5 kg, moisture content of 100 %. According to the obtained results, an energy consumption of 0.11 kWh kg⁻¹ was calculated for remediation of the studied soil to obtain a complete pyrene removal. This finding is in line with literature⁶³.

Synergetic and scavenging effect

The synergetic effect of persulfate-assisted EK system was determined at selected experimental conditions using synergy index (Eq. (15)):

$$SI = \frac{K_{(PTEK)}}{(K_{PEK}) + (K_{TEK}) + (K_{EK}) + (K_P)} \quad (15)$$

where, SI is the synergy index, K is the pseudo-first-order kinetic constant of pyrene removal in all experimented processes (PTEK: Persulfate-assisted EK+ addition of Tween 80, EK: electrokinetic remediation, PEK: electrokinetic remediation + persulfate addition, TEK: electrokinetic remediation+ addition of Tween 80, P: oxidation through persulfate). The removal efficiency of various studied processes are presented in Fig. 5a. It is obvious that persulfate-assisted EK remediation was significantly more efficient compared to individual processes, which can be attributed to synergetic effect of all processes. This can be verified by calculation of synergy index (Fig. 5b), in which the highest value of 1.99 was obtained for persulfate-assisted EK remediation process. This significant synergy index

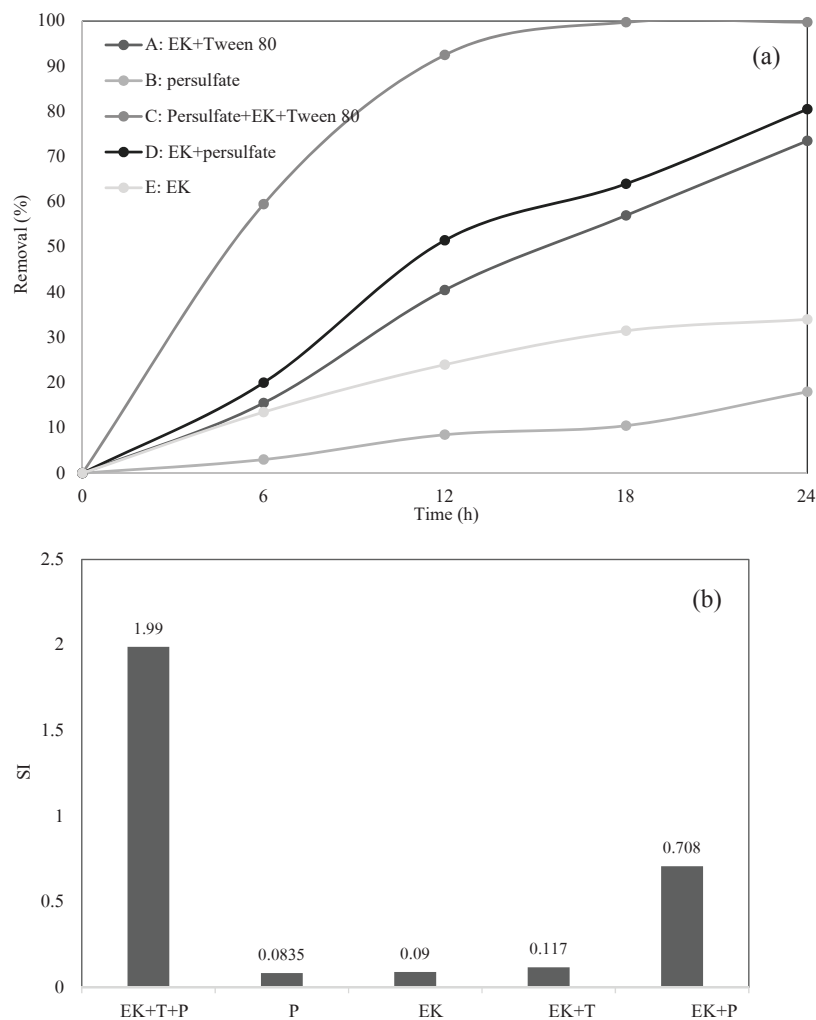


Fig. 5 – a) Pyrene removal efficiency, and b) Synergy indices in various studied processes in selected conditions (Tween 80: 20 mL kg⁻¹, voltage: 1 V cm⁻¹, moisture content: 100 %, persulfate concentration: 100 mg kg⁻¹)

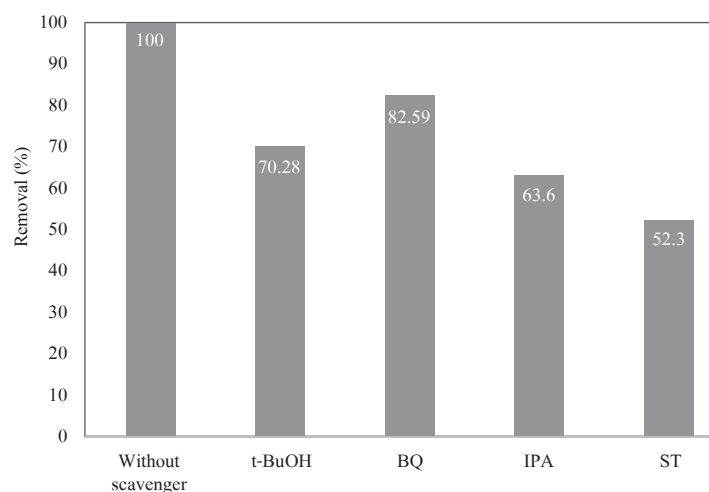


Fig. 6 – Comparison of the effect of different scavengers on the performance of persulfate-assisted EK remediation of pyrene contaminated soil in selected conditions

probably can be associated with the decomposition of pyrene molecules due to solubility enhancement effect of Tween 80, oxidation influence of persulfate, as well as the oxidation function of EK reactions. These findings are in accordance with literature⁶⁴.

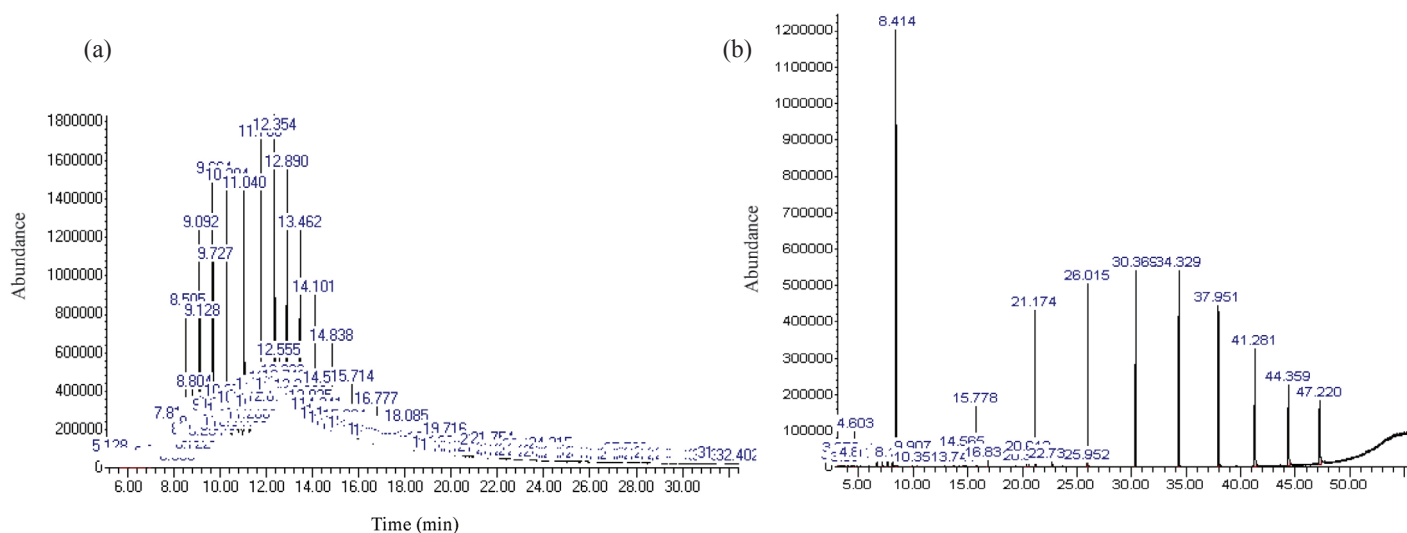
In persulfate-assisted EK system, it is believed that the production of H₂O₂, SO₄⁻, Cl₂ and heat are responsible for pyrene destruction. Scavenging effect of non-target organics on the function of produced oxidants was investigated through addition of tert-butyl alcohol (t-BuOH), benzoquinone (BQ), sodium thiosulfate (ST) and iso-propanol (IPA) as scavenger and effective quenching agent for oxidants (Cl₂, H₂O₂) and SO₄⁻ radicals⁶⁵. It was observed that the degradation efficiency of pyrene reduced from 100 % to 63.6 %, 70.28 %, 52.3 % and 82.59 %, respectively, in the presence of IPA, t-BuOH, ST and BQ agents (Fig. 6). Results of scavenging experiments demonstrated that pyrene degradation was in direct relation with all the oxidation agents.

EK remediation of unwashed soil

Reliability of the persulfate-assisted EK remediation was also evaluated in the remediation of a real unwashed contaminated-soil, based on TPH analysis. In addition, the types of different hydrocarbons were also determined via GC-MS analysis. Initial TPH content of 912 mg kg⁻¹ decreased to 560 mg kg⁻¹ (38 % removal) in the selected conditions like those presented in this work. The unwashed soil sample was mainly contaminated with octadecane, hexadecane, nonadecane, eicosane, heneicosane and similar compounds (Table 2). The production of various aliphatic intermediates, such as comphene, docecane, tetradecane, etc., are clear from GC-MS analysis (Fig. 7 a and b). The high cumulative concentration of different hydrocarbons is also the main reason for lower removal efficiency of the persulfate-assisted EK remediation of the unwashed soil sample. These results are in good agreement with our previous study on soil remediation with the modified Fenton oxidation⁶⁶ as well as with the literature on remediation of hydrocarbon-contaminated soil^{67,68}.

Table 2 – GC-MS analysis of the unwashed real hydrocarbon-contaminated soil before and after the persulfate-assisted EK (voltage: 1 V cm^{-1} , time: 24 h, pH: not adjusted, Tween 80: 20 mL kg^{-1} , persulfate: 100 mg kg^{-1})

Initial contaminant in unwashed soil			Products of persulfate-assisted EK remediation		
RT (min)	Substance	Chemical formula	RT (min)	Substance	Chemical formula
8.377	Tricosyl trifluoroacetate	$\text{C}_{25}\text{H}_{47}\text{F}_3\text{O}_2$	8.414	Camphene	$\text{C}_{10}\text{H}_{16}$
9.092	Heptadecane	$\text{C}_{17}\text{H}_{36}$	15.778	Dodecane	$\text{C}_{12}\text{H}_{26}$
9.127	Pentadecane	$\text{C}_{15}\text{H}_{32}$	21.174	Tetradecane	$\text{C}_{14}\text{H}_{30}$
9.499	Heptadecane	$\text{C}_{17}\text{H}_{36}$	26.015	Hexadecane	$\text{C}_{16}\text{H}_{34}$
9.664	Octadecane	$\text{C}_{18}\text{H}_{38}$	30.369	Octadecane	$\text{C}_{18}\text{H}_{38}$
9.727	Hexadecane	$\text{C}_{16}\text{H}_{34}$	34.329	Eicosane	$\text{C}_{20}\text{H}_{42}$
10.048	Nonadecane	$\text{C}_{19}\text{H}_{40}$	41.281	Tetracosane	$\text{C}_{24}\text{H}_{50}$
10.380	Octatriacontyl pentafluoropropionate	$\text{C}_{41}\text{H}_{77}\text{F}$	44.359	Heneicosane	$\text{C}_{21}\text{H}_{44}$
11.038	Eicosane	$\text{C}_{21}\text{H}_{44}$	47.220	Octacosane	$\text{C}_{28}\text{H}_{58}$
11.759	Heneicosane	$\text{C}_{21}\text{H}_{44}$			
12.354	Docosane	$\text{C}_{22}\text{H}_{46}$			
12.892	Tricosane	$\text{C}_{23}\text{H}_{48}$			
13.464	Tetracosane	$\text{C}_{24}\text{H}_{50}$			
14.540	1,2-Benzenedicarboxylic acid	$\text{C}_8\text{H}_6\text{O}_4$			
15.112	Hexadecane	$\text{C}_{16}\text{H}_{34}$			
15.713	Heptacosane	$\text{C}_{27}\text{H}_{56}$			
16.365	Pentacosane	$\text{C}_{25}\text{H}_{52}$			
18.556	Propiophenone	$\text{C}_9\text{H}_{10}\text{O}$			
19.266	Benz[b]-1,4-oxazepine-4(5H)-thione	$\text{C}_{11}\text{H}_{13}\text{NOS}$			

Fig. 7 – GC-MS analysis of a) unwashed hydrocarbon-contaminated soil, and b) hydrocarbon-contaminated soil after remediation with persulfate-assisted EK remediation under the selected conditions (Tween 80: 20 mL kg^{-1} , initial pH: 7 ± 0.3 , reaction time: 24 h, voltage: 1 V cm^{-1} , moisture content: 100 %, persulfate: 100 mg kg^{-1})

Conclusions

Synthetically pyrene-spiked and naturally hydrocarbon-contaminated soil samples were subjected to persulfate-assisted EK remediation in the lab-scale experimental setup. A total pyrene removal of 76 % was obtained for initial pyrene concentration of 200 mg kg⁻¹, voltage of 1 V cm⁻¹, natural pH, and saturated conditions in a reaction time of 120 h. The addition of persulfate (100 mg kg⁻¹) significantly enhanced the removal efficiency, and a complete removal was obtained in a much shorter reaction time of 24 h. In addition, moisture was also a key factor in the enhancement of pyrene degradation, and desirable results were found to be in higher moisture contents. A removal efficiency of 29 % in a low moisture content of 25 % and a reaction time of 120 h indicated the desired ability of the studied process to be operated in soils with low moisture contents. The initial TPH concentration of 912 mg kg⁻¹ decreased to 560 mg kg⁻¹ in the same conditions, as determined for pyrene removal in the synthetically contaminated soil, for a naturally hydrocarbon-contaminated soil sample. Although the removal (38 %) was lower, the total mass of removed hydrocarbon was considerable. Based on the results of this research, it is obvious that persulfate-assisted EK remediation is a viable, reliable, and efficient alternative for remediation of hydrocarbon-contaminated soil in lab-scale conditions. However, further experiments are needed to optimize the operating parameters for full-scale applications.

CONFLICT OF INTEREST

The authors declare that they have no conflict of interest.

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