

AUSTRALIA University of Southern Queensland Faculty of Health, Engineering and Sciences

TRIBOLOGICAL BEHAVIOUR OF GRAPHITE/DATE PALM FIBRES REINFORCED EPOXY COMPOSITES

A dissertation submitted by

Abdullah Al-Ajmi 006 10 231 64

For the award of **Doctor of Philosophy**

August 2013

Principal Supervisor: Dr. B.F. Yousif

Abstract

Natural fibres are becoming alternative candidates to synthetic fibres because of their environmental and economic advantages. In this study, the mechanical and the tribological performance of epoxy composites (ECs) based on date palm fibres (DPFs) was evaluated and compared with neat epoxy (NE). The work is divided into three stages: fibre optimisation, graphite optimisation and final composite selection.

Different fibre diameters (0.3–0.7 mm) and concentration of sodium hydroxide (NaOH) (zero to nine per cent) were used in preparing the fibre. For optimisation purposes, the interfacial adhesion between the DPFs and the epoxy matrix was studied using a new fragmentation technique that considers the influence of the NaOH treatment and the fibre diameter. At this stage, the results revealed that NaOH treatment significantly influences both the fibre strength and the fibre interfacial adhesion. Six per cent NaOH exhibited the optimum concentration to gain good mechanical properties for the EC, since it can maintain good interfacial adhesion, while maintaining good fibre strength.

In the second stage, the influence of the graphite weight presentation on ECs was evaluated from a mechanical and tribological perspective. Different weight percentages were used in the sample preparation (zero to seven per cent) for tensile, hardness and adhesive wear experiments. In the first part of this study, ultimate tensile strength and modulus of elasticity values and fracture morphology are determined. In the second part, specific wear rate, friction coefficient, interface temperature and surface morphology of the composites are determined. The results are discussed to gain the optimum mixing ratio of graphite with epoxy. The results revealed that there is a significant influence of the weight fraction of the graphite on both mechanical and tribological performance of the composites. Intermediate weight percentage of three weight per cent graphite in the EC was considered the optimum from both mechanical and tribological performance, since there is a slight reduction in the tensile properties and significant improvement to the hardness, wear and frictional characteristics. The modification on the wear track roughness significantly controlled the wear and frictional behaviour of the composites. Micrographs of the worn surface showed different wear mechanisms, depending on the content of the graphite in the composites. Softening and fragmentation appeared with low content of graphite presence in the composite, since there was no sign of aggregation or detachments of fillers.

From the second stage on the graphite percentage in the composite, it was concluded that three weight per cent of graphite in the ECs represents the optimum content from mechanical and tribological perspectives. In the third stage, the mechanical and tribological performance of the ECs based on three weight per cent graphite, DPF and three weight per cent graphite plus DPF are discussed and compared with NE. Further, the tribological performance of the composites is discussed, considering two different adhesive wear techniques: block on ring (BOR) and block on disk (BOD). This stage revealed that DPF is able to improve the mechanical properties of the ECs with no signs of pull out or debonding of the fibres. The main fracture mechanism was breakage in the fibre, fracture in the resinous regions and micro-cracks with graphite presence in the composites. Further, the addition of the three weight per cent of the graphite into the date fibre/ECs contributed to the improvement of the ECs; the fibres assisted in strengthening the surface, while the graphite generated the lubricant film transfer. Tribological experimental configuration significantly controlled the wear behaviour of the composite; the wear performance worsened under BOD compared to BOR because of the high thermo-mechanical loading in the case of BOD compared to BOR.

List of publications

Shalwan, A** & Yousif, BF 2013, 'In state of art: mechanical and tribological behaviour of polymeric composites based on natural fibres', *Materials & Design*, vol. 48, June, pp 14–24.

Shalwan, A** & Yousif, BF 2014, 'Investigation on interfacial adhesion of date palm/epoxy using fragmentation technique', *Materials & Design. Volume 53*, Pages 928–937.

Shalwan, A** & Yousif, BF 2013 in press, 'Correlation between mechanical and tribological performance of polymer composite materials', *International Journal of Precision Technology*, August.

Shalwan, A** & Yousif, BF 2013, 'Influence of graphite content on mechanical and wear characteristics of epoxy composites', under review August 2013, *Wear*.

Shalwan, A** & Yousif, BF 2013, 'Mechanical, wear and frictional performance of epoxy composites based on date palm fibres and graphite filler', under consideration since July 2013 *Tribology Letter*.

Arhaim, YH, Shalwan, A** & Yousif, BF 2013, 'Correlation between frictional force, interface temperature and specific wear rate of fibre polymer composites', *Advanced Materials Research*, vol. 685, pp. 45–49.

**Note: the candidate used his Arabic surname (Shalwan, A) instead of the English (Al-Ajmi, A.)

Certification of thesis

I certify that the ideas, designs and experimental work, results, analyses and conclusions set out in this thesis are entirely my own effort, except where otherwise indicated and acknowledged.

I further certify that the work is original and has not been previously submitted for assessment in any other course or institution, except where specifically stated.

Abdullah Al-Ajmi 006 10 231 64

Signature of Candidate

Date

Endorsement

Signature of Principle Supervisor

Signature of Associate Supervisor

Date

Date

Acknowledgements

I would like to express my most sincere appreciation to my PhD project supervisors Dr B. F. Yousif and Prof. Dr. Kin Tak Lau for their support, encouragement, aluable input and guidance provided at every stage of this thesis. I would also like to extend my gratitude towards the entire departmental and technical staff for their assistance and support in using the facilities and materials for conducting the experimental work.

In addition, I wish to express my deepest appreciation to my family members for their constant support throughout this study, especially my mother and my son Mohammed. I would like to extend my appreciation to my friends for their encouragement.

My particular appreciation is also extended to the University of Southern Queensland for financial support during this study.

Contents

List of tables	X
List of figures	. xi
Chapter 1: Introduction	1
1.1 Introduction	1
1.2 Objectives	4
1.3 Project significance	5
1.4 Organisation of the thesis	5
Chapter 2: Literature review	8
2.1 Mechanical properties of natural fibres/polymer composites	8
2.1.1 Influence of natural fibres on mechanical behaviour of polymeric	
composites	8
2.1.2 Interfacial adhesion of natural fibres	11
2.1.3 Effect of fibre orientation on mechanical properties	16
2.1.4 Effect of volume fraction	16
2.1.5 Effect of fibre physical properties	18
2.2 Tribological performance of polymeric composites based on natural fibres	19
2.2.1 Influence of natural fibres on tribological behaviour of polymeric	
composites	. 19
2.2.2 Effect of treatments	26
2.2.3 Operating parameters	28
2.2.4 Frictional behaviour	29
2.3 Possible reduction of friction coefficient	31
2.3.1 Liquid lubricants	31
2.3.2 Solid lubricants	35
2.4 Chapter summary	37
Chapter 3: Methodology	39
3.1 Introduction	39
3.2 Materials selection and preparation	41
3.2.1 Date palm fibre preparation and treatment	41
3.3 Preparation of samples	43
3.3.1 Single fibre tensile test	43
3.3.2 Fragmentation test specimens	43
3.3.3 Composite specimens preparation	44
3.4 Experimental procedure	47
3.4.1 Mechanical properties	. 49
3.4.1.1 Single fibre tensile test	49
3.4.1.2 Single fibre fragment test	49
3.4.1.3 Tensile experiments of the composites	50
3.4.2 Tribological experiments	51

3.4.3 Calibration and measurement technique of friction coefficient	. 55
Chapter 4: Interfacial adhesion of date palm/epoxy using fragmentation	
technique	. 56
4.1 Introduction	. 56
4.2 Influence of fibre treatment on surface morphology	. 58
4.2.1 Optical microscope micrographs morphology	. 58
4.2.2 Scanning electron microscope morphology	. 60
4.3 Single fibre tensile test	. 63
4.4 Single fibre fragmentation tensile test	. 68
4.5 Comparison to other published works	. 79
4.6 Chapter summary	. 82
Chapter 5: Influence of graphite content on mechanical and wear	
characteristics of epoxy composites	. 83
5.1 Introduction	. 83
5.2 Tensile properties of graphite/epoxy composites	. 83
5.2.1 Stress strain diagram, ultimate TS and modulus of elasticity	. 83
5.2.2 Fracture behaviour of the epoxy composites	. 86
5.3 Tribological performance of the epoxy composites based on different	
graphite contents	. 93
5.3.1 Running in and steady state of the adhesive wear	. 93
5.3.2 Running in and steady state of the coefficient of friction	. 95
5.3.3 Frictional heat in the interface of graphite/epoxy composites	. 98
5.4 Surface observations	101
5.4.1 Roughness modifications of the wear track	101
5.4.2 Roughness of the composite surface	103
5.4.3 Scanning electron microscopy observation	106
5.4.3.1 Micrographs of NE worn surface	106
5.4.3.2 Micrographs of one weight per cent graphite/epoxy worn surface.	108
5.4.5.5 Micrographs of inree weight per cent graphile/epoxy work	100
Surface	109
5.4.3.5 Micrographs of seven weight per cent graphite/epoxy worn surface.	110
5.4.5.5 Micrographs of seven weight per cent graphile/epoxy work	112
5 5 Comparison with provious works	112
5.5 Comparison with previous works	115
Chapter 6: Mechanical and wear characteristics of DPF and graphite	110
filler/ECS	117
(1 Introduction	117
6.2 Tangila proparties of data palm/graphita/apoyy composites	117
6.2.1 Stress strain diagram ultimate tensile stress and modulus of electicity	11/ v.of
date palm/graphite/epoxy composites	7 UI
6.2.2 Fracture behaviour date nalm/graphite/epoxy composites	124
6.2.3 Shore D hardness of the selected composites	124
5.2.5 Shore D hurdness of the servered composites	140

6.3 Tribological performance of date palm/graphite/epoxy composites under	
BOR technique	127
6.3.1 Wear behaviour of date palm/graphite/epoxy composites	. 127
6.3.2 Frictional behaviour of date palm/graphite/epoxy composites	129
6.3.3 Observation on the worn surfaces after BOR tests	133
6.3.3.1 Roughness modifications of the wear track	133
6.3.3.2 Roughness of the composite surface	134
6.3.3.3 SEM observation	135
6.4 Tribological performance of date palm/graphite/epoxy composites under	
BOD technique	138
6.4.1 Wear and frictional behaviour of date palm/graphite/epoxy composite	s 139
6.4.2 Observation on the worn surfaces of date palm/graphite/ECs after	
BOR testing	143
6.5 Discussion and arguments with previous works	147
6.6 Correlation between mechanical and tribological properties	150
6.7 Chapter summary	154
Chapter 7: Conclusions and recommendations	160
7.1 Conclusion	160
7.1 Conclusion 7.2 Recommendations	160 162
7.1 Conclusion	160 162 1635
 7.1 Conclusion	160 162 1635 7582 for 1793
 7.1 Conclusion	160 162 1635 7582 for 1793 201
 7.1 Conclusion	160 162 1635 7582 for 1793 201 d 201 208
 7.1 Conclusion	160 162 1635 7582 for 1793 201 d 201 208

List of tables

Table 2.1: Comparisons between various existing fibre-reinforced composites	17
Table 2.2: Adhesive wear and coefficient friction result of neat polymers and	
natural fibre composites under dry contact	Table
3.1: Specimen sets of the SFTT	43
Table 3.2: Technical specifications of the newly developed machine (Yousif	
2012)	53
Table 4.1: Summary of the previous works on optimum diameter and chemical	
treatment concentration on mechanical behaviour of fibre/polymer	
composites	
Table 5.1: Summary of the previous works on effect of adding filler tribological	
behaviour of polymer composite	115
Table 6.1: Published works on tensile properties of natural fibre reinforce epoxy	
or polyester composites	
Table 6.3: Summary of previous works on effect of natural fibres and fillers on	
tribological behaviour of polymer composite	148
Table 6.4 correlation coefficient of individual mechanical properties with coeffi	cient
of friction and specific wear rate.	156
Table 6.5 Correlation coefficient of two mechanical properties combined with	
coefficient of friction and specific wear rate	157
Table 6.6 Correlation coefficient of two or more than two mechanical properties	
combined with coefficient of friction and specific wear rate.	158

List of figures

Figure 1.1: Number of synthetic and natural fibre-reinforced polymeric
composite articles. Source: www.ScienceDirect.com. Keywords used:
natural fibres, reinforcement, polymers and synthetic fibres 2
Figure 1.2: Layout of the thesis7
Figure 2.1: Some mechancial properties of natural fibre/polymer composites 10
Figure 2.2: Scheme of reaction of fibre surface with NaOH treatment 12
Figure 2.3: Tensile strength of polymeric composites based on natural fibres
with/without treatment
Figure 2. 4: Specific wear rate and friction coefficient of some polymeric
composites under dry contact conditions
Figure 2.5: Schematic drawing showing the effect of treating the natural fibres
on the wear behaviour of polymeric composites
Figure 2.6: Specific wear rate and friction coefficient of some polymeric
composites under wet contact conditions
Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric
Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites
 Figure 2.7: Influence of solid lubricants on the frictional behaviour of polymeric composites

Figure 3.11: Calibration chart for measuring friction force
Figure 4.1: Optical images of fibre surface ($D = 0.3 \text{ mm}$)—(a) untreated, (b) at
3% NaOH, (c) at 6% NaOH (d) at 9% NaOH 59
Figure 4.2: (a) optical microscope micrographs for three different diameters of
fibre with defects, (b) scheme of cross-section of fibre with lumen and
defects 60
Figure 4.3: Micrographs of the untreated DPF 61
Figure 4.4: Treated DPF with different NaOH concentrations
Figure 4.5: Tensile behaviour of the single DPF (0.3 mm diameter) treated with
different NaOH concentrations
Figure 4.6: Tensile behaviour of the single DPF (0.5 mm diameter) treated with
different NaOH concentration64
Figure 4.7: Tensile behaviour of the single DPF (0.7 mm diameter) treated with
different NaOH concentrations 64
Figure 4.8: Effect of diameter of fibre and NaOH treatment on TS on single fibre 66
Figure 4.9: Effect of diameter of fibre and NaOH treatment on strain at fracture
on single fibre
Figure 4.10: Effect of diameter of fibre and NaOH treatment on modulus of
elasticity on single fibre67
Figure 4.11: Tensile behaviour of the single DPF fragmentation test (0.3 mm
diameter) treated with different NaOH concentrations
Figure 4.12: Tensile behaviour of the single DPF fragmentation test (0.5 mm
diameter) treated with different NaOH concentrations 70
Figure 4.13: Tensile behaviour of the single DPF fragmentation test (0.7 mm
diameter) treated with different NaOH concentrations and NE71
Figure 4.14: Effect of diameter of fibre and NaOH treatment on tensile stress of
date palm/EC72
Figure 4.15: Effect of fibre diameter and NaOH treatment on shear stress on fibre
of date palm/EC73
Figure 4.17: Microscopy of fragmentation samples after testing the treated DPF
(3% NaOH)/epoxy

(6% NaOH)/epoxy76
Figure 4.19: Microscopy of fragmentation sample after testing the treated DPF
(9% NaOH)/epoxy77
Figure 4.20: Schematic drawing showing the treatment effect of different
concentration (0%, 3%, 6% and 9%) on surface and structure fibre 79
Figure 5.1: Stress strain diagrams of graphite/ECs
Figure 5.2: Ultimate TS and modulus of elasticity of graphite/ECs
Figure 5.3: Micrographs of the NE after tensile testing—st = stretching, de =
detachment, fr = fracture
Figure 5.4: Micrographs of the 1% graphite/ECs after tensile testing—cr =
cracks, sl = shear lips, rl = river-like pattern
Figure 5.5: Micrographs of 3% graphite/ECs after tensile testing—rl = river-like
pattern, gp = graphite particle
Figure 5.6: Micrographs of 5% graphite/ECs after tensile testing—rl = river-like
pattern, gp = graphite particle, de = debonding, ag = aggregation90
Figure 5.7: Micrographs of 7% graphite/ECs after tensile testing—de =
debonding, ag = aggregation, cr = cracks, fr = fracture
Figure 5.8: Shore D hardness of graphite/ECs
Figure 5.9: Specific wear rate v. sliding distance of graphite/ECs
Figure 5.10: Schematic drawing representing the running in and steady state
Figure 5.11: Specific wear rate at the steady state of the graphite/ECs after 7.5
km sliding distance
Figure 5.12: Coefficient of friction v. sliding distance of the composites
Figure 5.13: Coefficient of friction at the steady state of the composites after 7
km sliding distance
Figure 5.14: Heat distribution in the interface and both rubbed surfaces of the NE
after 2.52, 5.04 and 7.56 km sliding distances at sliding velocity of 2.8
m/s and applied load of 50 N
Figure 5.15: Interface temperature of graphite/ECs surface at the end of the
adhesive loadings
Figure 5.16: Samples of the roughness profile of the counterface

Figure 5.17: Ra roughness values of the counterface surface after adhesive
loadings for 7.56 km sliding distance 103
Figure 5.18: Samples of the roughness profile of the composite surfaces after 7.56
km sliding distance at sliding velocity of 2.8 m/s and applied load
of 50 N
Figure 5.19: Ra roughness values of graphite/ECs surface after adhesive loadings
for 7.56 km sliding distance106
Figure 5.20: Micrographs of NE after adhesive testing—fg = fragmentation, so =
softening, fr = fracture
Figure 5.21: Micrographs of 1% graphite/ECs after adhesive testing—fg =
fragmentation, so = softening, fr = fracture, gr = graphite, dt =
detachment, cr = crack
Figure 5.22: Micrographs of 3% graphite/ECs after adhesive testing—so =
softening, $fr = fracture$, $pg = patch of graphite$, $df = deformation \dots 110$
Figure 5.23: Micrographs of 5% graphite/ECs after adhesive testing—so =
softening, fr = fracture, fl = film transfer, df = deformation 111
Figure 6.1: Stress strain diagram of different ECs based on graphite and/or DPFs. 118
Figure 6.2: Ultimate TS and modulus of elasticity of different ECs based on
graphite and/or DPF. NE = neat epoxy, GE = 3% graphite/epoxy, FE
= DPFE, GFE = 3 wt% graphite/date palm fibre/epoxy 119
Figure 6.3: Micrographs of DPFE composite after tensile test 125
Bo = bonded, Ep = Epoxy, Br = breakage, Rl = river-like, Tr = Trichome 126
Figure 6.5: Shore D hardness of different ECs based on graphite and/or DPF. NE
= neat epoxy, $GE = 3\%$ graphite/epoxy, $FE = DPFE$, $GFE = 3$ wt%
graphite/date palm fibre/ epoxy 127
Figure 6.6: Specific wear rate v. applied load of different ECs based on graphite
and/or DPF after 5.04 km sliding distance using BOR technique 128
Figure 6.7: Reduction in specific wear rate at the steady state of different ECs
based on graphite and/or DPF at 70 N applied load using BOR
technique

Figure 6.8: Coefficient of friction v. sliding load of different ECs based on	
graphite and/or DPF using BOR technique	0
graphite and/or DPF at 70 N sliding load using BOR technique	51
Figure 6.10: Interface temperature of different ECs based on graphite and/or	
DPF at different applied loads after 5.04 km sliding distance using	
BOR technique	2
Figure 6.11: Roughness values of the counterface surface after adhesive loadings	
of different ECs based on graphite and/or DPF at 50 N applied load	
using BOR technique	4
Figure 6.12: Roughness values of the specimen surface of different ECs based on	
graphite and/or DPF after adhesive loadings at 50 N using BOR	
technique for 5 km sliding distance	5
Figure 6.13: Micrographs of DPF/ECs after testing under 50 N applied load	
using BOR technique 13	36
Bo = bonded, So =Softening, Db =debonding	36
Figure 6.14: Micrographs of date palm/3 wt% graphite/ECs after testing at 50 N	
using BOR technique	:=
cracks, Db =debonding 13	38
Figure 6.15: Specific wear rate v. sliding distance of different ECs based on	
graphite and/or DPF using BOD technique14	0
Figure 6.16: Reduction in specific wear rate at the steady state of different ECs	
based on graphite and/or DPF at 70 N km sliding load using BOD	
technique	0
Figure 6.17: Specific wear rate of the selected composites using BOR and BOD	
techniques after applied load 50 N14	1
Figure 6.18: Coefficient of friction v. sliding load of different ECs based on	
graphite and/or DPF using BOD technique14	2
Figure 6.19: Interface temperature of different ECs based on graphite and/or	
DPF at different applied loads using BOD technique	2

Figure 6.20: Roughness values of the counterface surface after adhesive of
different ECs based on graphite and/or DPF loadings at 50 N using
BOD technique
experiments using BOD under low applied loads. Fr = fragmentation, Ab
= abrasive, Pg = ploughing, Cr = crack, Bo = bonded, Po = pull
out, Fl = film transfer
Figure 6.22: Micrographs of the date palm/3 wt% graphite/ECs after the
experiments using BOD under high applied loads. Pl = pull out fibre,
Pg = ploughing, Fl = film transfer, Db = debonding
Figure 6.23: Correlation between the individual mechanical properties and
specific wear rate of the studied materials
Figure 6.24: Correlation between selective combined mechanical properties and
specific wear rate of the studied materials
Figure A.3: Heat distribution in the interface and both rubbed surfaces of
the 5%Gr-EC after 2.52, 5.04 and 7.56 km sliding distances at sliding
velocity of 2.8 m/s and applied load of 50 N 177
Figure A.4: Heat distribution in the interface and both rubbed surfaces of
the 7%Gr-EC after 2.52, 5.04 and 7.56 km sliding distances at sliding
velocity of 2.8 m/s and applied load of 50 N 178
Figure B.1: Heat distribution in the interface and both rubbed surfaces of the NE
at 20, 30, 40, 50 N sliding loads at sliding velocity of 2.8 m/s and
sliding distance 5.04 km (BOR)
Figure B.2: Heat distribution in the interface and both rubbed surfaces of the GE
at 20, 30, 40, 50 N sliding loads at sliding velocity of 2.8 m/s and
sliding distance 5.04 km (BOR) 182
Figure B.3: Heat distribution in the interface and both rubbed surfaces of the FE
at 20, 30, 40, 50 N sliding loads at sliding velocity of 2.8 m/s and
sliding distance 5.04 km (BOR) 184
Figure B.4: Heat distribution in the interface and both rubbed surfaces of the GFE at
20, 30, 40, 50 N sliding loads at sliding velocity of 2.8 m/s and
sliding distance 5.04 km (BOR) 186

Figure B.5: Heat distribution in the interface and both rubbed surfaces of the NE
at 20, 30, 40, 50 N sliding loads at sliding velocity of 2.8 m/s and
sliding distance 2.52 km (BOD) 188
Figure B.6: Heat distribution in the interface and both rubbed surfaces of the GE
at 20, 30, 40, 50 N sliding loads at sliding velocity of 2.8 m/s and
sliding distance 2.52 km (BOD) 190
Figure B.7: Heat distribution in the interface and both rubbed surfaces of the FE
at 20, 30, 40, 50 N sliding loads at sliding velocity of 2.8 m/s and
sliding distance 2.52 km (BOD) 192
Figure B.8: Heat distribution in the interface and both rubbed surface of the GFE
at 20, 30, 40, 50 N sliding loads at sliding velocity of 2.8 m/s and
sliding distance 2.52 km (BOD) 194
Figure B.9: Roughness values of the counterface surface after adhesive loadings
of different ECs based on graphite and/or DPF at 50 N applied load
using BOR technique
Figure B.10: Roughness values of the specimen surface of different ECs based
on graphite and/or DPF before adhesive loadings at 50 N using BOR
technique
Figure B.11: Roughness values of the specimen surface of different ECs based
on graphite and/or DPF after adhesive loadings at 50 N using BOR
technique 197
Figure B.12: Roughness values of the counterface surface after adhesive of
different ECs based on graphite and/or DPF loadings at 50 N using
BOD technique 198
Figure C. 1 correlation between specific wear rate and modulus of elasticity 199
Figure C. 2 correlation between specific wear rate and elongation at break 199
Figure C. 3 correlation between specific wear rate and hardness 200
Figure C. 4 correlation between specific wear rate and tensile strength 200

Figure C. 6 correlation between specific wear rate and the combination of
modulus of elasticity, tensile strength and elongation at break
modulus of elasticity, tensile strength, hardness and elongation at
break
Figure C. 8 correlation between specific wear rate and the combination of
tensile strength and elongation at break
Figure C. 9 correlation between specific wear rate and the combination tensile
strength and hardness
Figure C. 10 correlation between specific wear rate and the combination of
modulus of elasticity and elongation at break
Figure C. 11 correlation between specific wear rate and the combination of
modulus of elasticity and hardness
Figure C. 12 correlation between specific wear rate and the combination of
hardness and elongation at break
Figure C. 13 correlation between specific wear rate and the combination of
modulus of elasticity, hardness and elongation at break 205
Figure C. 14 correlation between friction coefficient and tensile strength 206
Figure C. 15 correlation between friction coefficient and modulus of elasticity 206
3 Figure C. 16 correlation between friction coefficient and tensile elongation at
break
Figure C. 17 correlation between friction coefficient and hardness
Figure C. 18 correlation between friction coefficient and the combination of
modulus of elasticity and tensile strength
Figure C. 19 correlation between friction coefficient and the combination of
modulus of elasticity, tensile strength and elongation at break 208
Figure C. 20 correlation between friction coefficient and the combination of
modulus of elasticity, tensile strength, hardness and elongation at
break
Figure C. 21 correlation between friction coefficient and the combination of
tensile strength and elongation at break

igure C. 22 correlation between friction coefficient and the combination of	
tensile strength and hardness igure C. 23 correlation between friction coefficient and the combination of	. 210
modulus of elasticity and elongation at break	. 210
igure C. 24 correlation between friction coefficient and the combination of	
modulus of elasticity and hardness	. 211
igure C. 25 correlation between friction coefficient and the combination of	
hardness and elongation at break	. 211
igure C. 26 correlation between friction coefficient and the combination of	
modulus of elasticity, hardness and elongation at break	. 212

List of abbreviations

ABS	Acrylonitrile butadiene styrene
ASTM	American Society for Testing and Materials
BFRP	Betelnut fibres reinforced in polyester
BOD	Block on disk
BOR	Block on ring
CFRP	Coir fibre-reinforced polyester
CPC	Cotton-polyester composite
Df	Fibre diameter
DPF	Date palm fibre
DPFE	Date palm fibre-reinforced epoxy
EC	Epoxy composite
GJ	Gigajoule
GR	Graphite powder
HDPE	High-density polyethylene
ICMF	Incomplete maturation fibres
KFRE	Kenaf fibre-reinforced epoxy
MoS2	Molybdenum disulfide
NaOH	Sodium hydroxide
NE	Neat epoxy
РА	Polyamides
PEEK	Polyarylethe-retherketone
PLA	Polylactic acid
РММА	polymethyl methacrylate
РР	Polypropylene
PPESK	Polyphatalazinone ether sulfone ketone

PPE	Polyphatalazinone ether
PPS	Polyphenylene sulfide
PTFE	Poly-tetrafluoroethylene

Ra	Roughness average
RNFPC	Reinforced natural fibre polymer composite
SCRP	Sugarcane fibre/polyester composite
SEM	Scanning electron microscopy
SiC	Silicon carbide
SFFT	Single fibre fragmentation test
SFTT	Single fibre tensile test
SP	Sisal fibres/polyester composites
T-OPRP	Treated oil palm fibre-reinforced polyester
TS	Tensile strength
T-SP	Treated sisal fibres/polyester composites
UHMWPE	Ultra-High Molecular Weight Polyethylene
US	United States
UT-OPRP	Untreated oil palm fibre-reinforced polyester
UT-SP	Untreated sisal fibres/polyester composites
Vf	Volume fraction
Ws	Specific wear rates
Wt	Weight