AN N-BODY INTEGRATOR FOR GRAVITATING PLANETARY RINGS, AND THE OUTER EDGE OF SATURN'S B RING

JOSEPH M. HAHN[1] AND JOSEPH N. SPITALE[2]
[1] Space Science Institute, c/o Center for Space Research, University of Texas at Austin, 3925 West Braker Lane, Suite 200, Austin, TX 78759-5378, USA; jhahn@spacescience.org
[2] Planetary Science Institute, 1700 East Fort Lowell, Suite 106, Tucson, AZ 85719-2395, USA; jnspitale@psi.edu
Received 2012 December 28; accepted 2013 June 4; published 2013 July 15

ABSTRACT

A new symplectic N-body integrator is introduced, one designed to calculate the global 360° evolution of a self-gravitating planetary ring that is in orbit about an oblate planet. This freely available code is called epi_int, and it is distinct from other such codes in its use of streamlines to calculate the effects of ring self-gravity. The great advantage of this approach is that the perturbing forces arise from smooth wires of ring matter rather than discreet particles, so there is very little gravitational scattering and so only a modest number of particles are needed to simulate, say, the scalloped edge of a resonantly confined ring or the propagation of spiral density waves. The code is applied to the outer edge of Saturn's B ring, and a comparison of *Cassini* measurements of the ring's forced response to simulations of Mimas's resonant perturbations reveals that the B ring's surface density at its outer edge is $\sigma_0 = 195 \pm 60$ g cm^{-2}, which, if the same everywhere across the ring, would mean that the B ring's mass is about 90% of Mimas's mass. *Cassini* observations show that the B ring-edge has several free normal modes, which are long-lived disturbances of the ring-edge that are not driven by any known satellite resonances. Although the mechanism that excites or sustains these normal modes is unknown, we can plant such a disturbance at a simulated ring's edge and find that these modes persist without any damping for more than $\sim 10^5$ orbits or ~ 100 yr despite the simulated ring's viscosity $\nu_s = 100$ cm^2 s^{-1}. These simulations also indicate that impulsive disturbances at a ring can excite long-lived normal modes, which suggests that an impact in the recent past by perhaps a cloud of cometary debris might have excited these disturbances, which are quite common to many of Saturn's sharp-edged rings.

Key word: planets and satellites: rings

1. INTRODUCTION

A planetary ring is often coupled dynamically to a satellite via orbital resonances. The ring's response to resonant perturbations varies with the forcing, and if the ring is for instance composed of low optical depth dust, then the ring's response will vary with the satellite's mass and its proximity. But in an optically thick planetary ring, such as Saturn's main A and B rings or its many dense narrow ringlets, the ring is also interacting with itself via self-gravity, so its response is also sensitive to the ring's mass surface density σ_0 (Shu 1984; Melita & Papaloizou 2005; Hahn et al. 2009). Therefore, by measuring a dense ring's response to satellite perturbations, and comparing that measurement to a model for the ring–satellite system, one can then infer the ring's physical properties, such as its surface density σ_0, and perhaps other quantities too (Melita & Papaloizou 2005; Tiscareno et al. 2007; Hahn et al. 2009). Recently, Hahn et al. (2009) developed a semi-analytic model of the outer edge of Saturn's B ring, which is confined by an $m = 2$ inner Lindblad resonance (ILR) with the satellite Mimas. The resonance index m also describes the ring's anticipated equilibrium shape, with the ring-edge's deviations from circular motion expected to have an azimuthal wavenumber of $m = 2$, so the B ring's expected shape is a planet-centered ellipse, which has $m = 2$ alternating inward and outward excursions. The model of Hahn et al. (2009) also calculates the ring's equilibrium $m = 2$ response excited by Mimas, but that comparison between theory and observation was done during the early days of the *Cassini* mission when that spacecraft's measurement of the ring-edge's semimajor axis $a_{\rm edge}$ was still rather uncertain. It turns out that the ring's inferred surface density is very sensitive to how far the B ring's outer edge extends beyond the resonance, which was quite uncertain

then due to the uncertainty in $a_{\rm edge}$, so the uncertainty in the ring's inferred σ_0 was also relatively large. Now, however, $a_{\rm edge}$ is known with much greater precision, so a re-examination of this system is warranted.

Cassini's monitoring of the B ring also reveals that the ring's outer edge exhibits several normal modes, which are unforced disturbances that are not associated with any known satellite resonances. Figure 1 illustrates this phenomenon with a mosaic of images that *Cassini* acquired of the B ring's edge on 2008 January 28. Spitale & Porco (2010) have also fit a kinematic model to four years' worth of *Cassini* images of the B ring; that model is composed of four normal modes having azimuthal wavenumbers $m = 1, 2, 2, 3$ that steadily rotate over time at distinct rates. In the best-fitting kinematic model there are two $m = 2$ modes, one that is forced by and corotating with Mimas, as well as a free $m = 2$ mode that rotates slightly faster. The amplitudes and orientations of all the modes as they appear in the 2008 January 28 data are also shown in Figure 2. Note that although the B ring's outer edge, as seen in Figure 1, might actually resemble a simple $m = 2$ shape on 2008 January 28, at other times the ring-edge's shape is much more complicated than a simple $m = 2$ configuration, yet at other times the ring-edge is relatively smooth and nearly circular; see, for example, Figure 1 of Spitale & Porco (2010). This behavior is due to the superposition of the normal modes that are rotating relative to each other, which causes the B ring's edge to evolve over time. Since this system is not in simple equilibrium, a time-dependent model of the ring that does not assume equilibrium is appropriate here.

Therefore, the following develops a new N-body method that is designed specifically to track the time evolution of a self-gravitating planetary ring, and that model is then applied to the
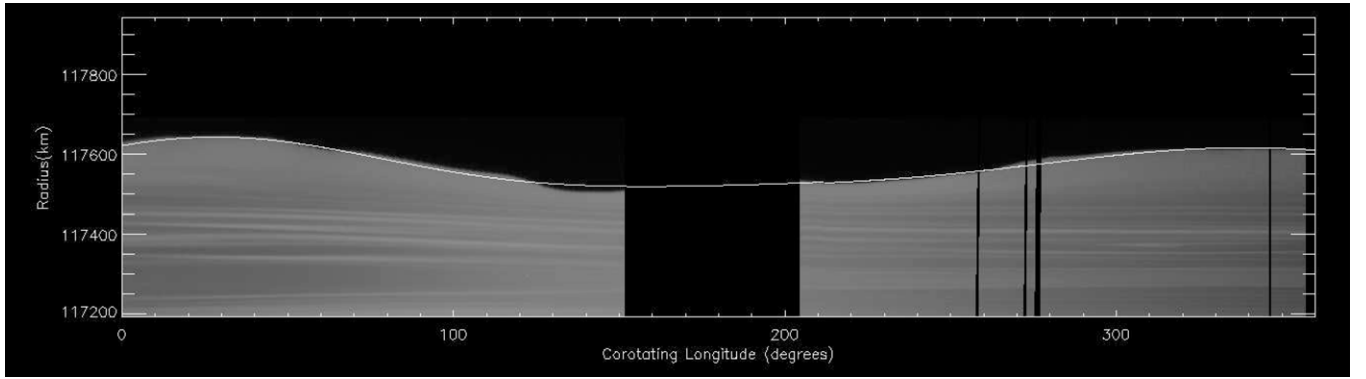
Figure 1. Mosaic of *Cassini* images of the B ring's outer edge acquired during 9 hr on 2008 January 28. Gray scale indicates the ring's optical surface brightness at various radii and corotating longitudes, meaning that local Keplerian motion about an oblate planet is assumed as all the individual image elements are mapped to positions held at some common instant of time. (Note that a true instantaneous snapshot of the ring would still have a different shape than this mosaic because the various normal modes rotate at differing speeds, and those differential rotations are not accounted for in this projection.) The curve at the ring's edge is the four-component kinematical model of Spitale & Porco (2010), which is a best fit to 18 such mosaics like this one but acquired over four years of monitoring, and the black zones are regions not used in that kinematic fit.
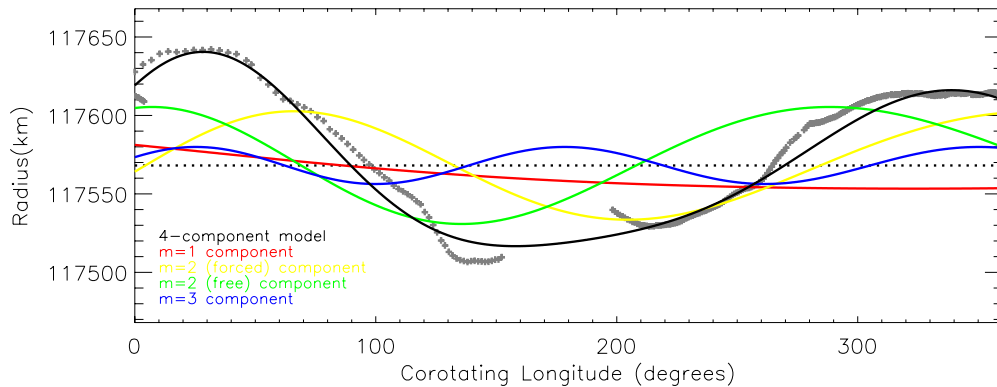

Figure 2. Crosses are the B ring-edge's observed radius vs. corotating longitude on 2008 January 28 extracted from the mosaic seen in Figure 1. Colored curves show the amplitudes and orientations of the $m = 1$, $m = 2$ (forced), $m = 2$ (free), and $m = 3$ normal modes that Spitale & Porco (2010) fit to four years of *Cassini* imaging. Black curve is the superposition of those modes at this instant, and the dotted line is the B ring-edge's semimajor axis. Note that these curves do not agree at $0°$ and $360°$ corotating longitudes due to the rotation of the normal modes that occurs during the 9 hr observing window.

latest *Cassini* results. Section 2 describes in detail the *N*-body model that can simulate all $360°$ of a narrow annulus in a self-gravitating planetary ring using a very modest number of particles. Section 3 then shows results from several simulations of the outer edge of Saturn's B ring and demonstrates how a ring's observed epicyclic amplitudes and pattern speeds can be compared to *N*-body simulations to determine the ring's physical properties. Results are then summarized in Section 5.

2. NUMERICAL METHOD

The following briefly summarizes the theory of the symplectic integrator that Duncan et al. (1998) use in their SYMBA code and Chambers (1999) use in the MERCURY integrator to calculate the motion of objects in nearly Keplerian orbits about a point-mass star. That numerical method is adapted here so that one can study the evolution of a self-gravitating planetary ring that is in orbit about an oblate planet.

2.1. Symplectic Integrators

The Hamiltonian for a system of N bodies in orbit about a central planet is

$$H = \sum_{i=0}^{N} \frac{p_i^2}{2m_i} + \sum_{i=0}^{N} \sum_{j>i}^{N} V_{ij}, \qquad (1)$$

where body i has mass m_i and momentum $\mathbf{p}_i = m_i \mathbf{v}_i$ where $\mathbf{v}_i = \dot{\mathbf{r}}_i$ is its velocity and V_{ij} is the potential such that $\mathbf{f}_{ij} = -\nabla_{\mathbf{r}_i} V_{ij}$ is the force on i due to body j where $\nabla_{\mathbf{r}_i}$ is the gradient with respect to coordinate $\mathbf{r}_i$, and the index $i = 0$ is reserved for the central planet whose mass is m_0. Next choose a coordinate system such that all velocities are measured with respect to the system's barycenter, so $\mathbf{p}_0 = -\sum_{j=1}^{N} \mathbf{p}_j$, and the Hamiltonian becomes

$$H = \sum_{i=1}^{N} \left(\frac{p_i^2}{2m_i} + V_{i0} \right) + \sum_{i=1}^{N} \sum_{j>i}^{N} V_{ij} + \frac{1}{2m_0} \left(\sum_{i=1}^{N} \mathbf{p}_i \right)^2$$

$$\equiv H_A + H_B + H_C \qquad (2)$$

since $V_{ij} = V_{ji}$. This Hamiltonian has three parts,

$$H_A = \sum_{i=1}^{N} \left(\frac{p_i^2}{2m_i} + V_{i0} \right) \qquad (3a)$$

$$H_B = \sum_{i=1}^{N} \sum_{j>i}^{N} V_{ij} \qquad (3b)$$

$$H_C = \frac{1}{2m_0} \left(\sum_{i=1}^{N} \mathbf{p}_i \right)^2, \qquad (3c)$$

and the following will employ spatial coordinates such that all $\mathbf{r}_i$ are measured relative to the central planet. This combination of planetocentric coordinates and barycentric velocities is referred to as "democratic-heliocentric" coordinates in Duncan et al. (1998) and "mixed-center" coordinates in Chambers (1999). In the above, H_A is the sum of two-body Hamiltonians, H_B represents the particles' mutual interactions, and H_C accounts for the additional forces that arise in this particular coordinate system that are due to the central planet's motion about the barycenter.

Hamilton's equations for the evolution of the coordinates $\mathbf{r}_i$ and momenta $\mathbf{p}_i$ for particle $i \geqslant 1$ are $\dot{\mathbf{r}}_i = \nabla_{\mathbf{p}_i} H$ and $\dot{\mathbf{p}}_i = -\nabla_{\mathbf{r}_i} H$. So a particle that is subject only to Hamiltonian H_B during short time interval δt would experience the velocity kick

$$\delta \mathbf{v}_i = \frac{\dot{\mathbf{p}}_i \delta t}{m_i} = -\nabla_{\mathbf{r}_i} H_B \frac{\delta t}{m_i} = \frac{\delta t}{m_i} \sum_{j=1}^{N} \mathbf{f}_{ij}, \qquad (4)$$

which of course is i's response to the forces exerted by all the other small particles in the system. And since H_C is a function of momenta only, a particle subject to H_C during time δt will see its spatial coordinate kicked by

$$\delta \mathbf{r}_i = \frac{\delta t}{m_0} \sum_{j=1}^{N} \mathbf{p}_j \qquad (5)$$

due to the planet's motion about the barycenter.

Now let $\xi_i(t)$ represent any of particle i's coordinates x_i or momenta p_i; that quantity evolves at the rate (Goldstein 1980)

$$\frac{d\xi_i}{dt} = [\xi_i, H] = [\xi_i, H_A + H_B + H_C] = (A + B + C)\xi_i, \quad (6)$$

where the brackets are Poisson brackets and the operator A is defined such that $A\xi_i = [\xi_i, H_A]$, with operators B and C defined similarly. The solution to Equation (6) for ξ_i evaluated at the later time $t + \Delta t$ is formally

$$\xi_i(t + \Delta t) = e^{(A+B+C)\Delta t} \xi_i(t) \qquad (7)$$

(Goldstein 1980), but this exact expression is in general not analytic and not in a useful form. However, Duncan et al. (1998) and Chambers (1999) show that the above is approximately

$$\xi_i(t + \Delta t) \simeq e^{B\Delta t/2} e^{C\Delta t/2} e^{A\Delta t} e^{C\Delta t/2} e^{B\Delta t/2} \xi_i(t), \qquad (8)$$

which indicates that five actions that are to occur as the system of orbiting bodies are advanced one timestep Δt by the integrator. (1) First, the operator $e^{B\Delta t/2}$ acts on $\xi_i(t)$, which increments (i.e., kicks) particle i's velocity $\mathbf{v}_i$ by Equation (4) due to the system's interparticle forces with $\delta t = \Delta t/2$. (2) Then, the $e^{C\Delta t/2}$ operator acts on the result of substep (1) and kicks the particle's spatial coordinates $\mathbf{r}_i$ according to Equation (5) due to the central planet's motion about the barycenter. (3) Then, the $e^{A\Delta t}$ operation advances the particle along its unperturbed epicyclic orbit about the central planet during a full timestep Δt, with this substep being referred to below as the orbital "drift" step. (4) This step is another coordinate kick $\delta \mathbf{r}_i$ and step (5) is the final velocity kick.

In a traditional symplectic N-body integrator, the planet's oblateness is treated as a perturbation whose effect would be accounted for during steps (1) and (5), which provide an extra kick to a particle's velocity every timestep. Those kicks cause a

particle in a circular orbit to have a tangential speed that is faster than the Keplerian speed by the fractional amount that is of the order of $\sim J_2(R/r)^2 \sim 3 \times 10^{-3}$ where $J_2 \simeq 0.016$ is Saturn's second zonal harmonic and $r/R \sim 2$ is a B ring particle's orbit radius r in units of Saturn's radius R. The particle's circular speed is super-Keplerian, and if its coordinates and velocities were to be converted to Keplerian orbit elements, its Keplerian eccentricity would also be of the order of $e \sim 3 \times 10^{-3}$. This putative eccentricity should be compared to the observed eccentricity of Saturn's B ring, which is the focus of this study and is of the order of $e \sim 10^{-4}$, about 30 times smaller than the particle's Keplerian eccentricity. The main point is that one does not want to use Keplerian orbit elements when describing a particle's nearly circular motions about an oblate planet because the Keplerian eccentricity is dominated by planetary oblateness whose effects obscure the ring's much smaller forced motions.

To sidestep this problem, the following algorithm uses the *epicyclic* orbit elements of Borderies-Rappaport & Longaretti (1994), which provide a more accurate representation of an unperturbed particle's orbit about an oblate planet. Note that this use of epicyclic orbit elements effectively takes the effects of oblateness out of the integrator's velocity kick steps (1) and (5) and places oblateness effects in the integrator's drift step (3), which is preferable because the forces in the B ring that are due to oblateness are about $\sim 10^4$ times larger than any satellite perturbation. The following details how these epicyclic orbit elements are calculated and are used to evolve the particle along its unperturbed orbit during the drift substep.

2.2. Epicyclic Drift

This two-dimensional (2D) model will track a particle's motions in the ring plane, so the particle's position and velocity relative to the central planet can be described by four epicyclic orbit elements: semimajor axis a, eccentricity e, longitude of periapse $\tilde{\omega}$, and mean anomaly M. For a particle in a low-eccentricity orbit about an oblate planet, the relationship between the particle's epicyclic orbit elements and its cylindrical coordinates r, θ and velocities v_r, v_θ are

$$r = a\left[1 - e\cos M + \left(\frac{\eta_0}{\kappa_0}\right)^2 (2 - \cos^2 M)e^2\right] \qquad (9a)$$

$$\theta = \tilde{\omega} + M + \frac{\Omega_0}{\kappa_0}\left\{2e\sin M + \left[\frac{3}{2} + \left(\frac{\eta_0}{\kappa_0}\right)^2\right]e^2\sin M\cos M\right\} \qquad (9b)$$

$$v_r = a\kappa_0\left[e\sin M + 2\left(\frac{\eta_0}{\kappa_0}\right)^2 e^2\sin M\cos M\right] \qquad (9c)$$

$$v_\theta = a\Omega_0\left\{1 + e\cos M - 2\left(\frac{\eta_0}{\kappa_0}\right)^2 e^2 + \left[1 + \left(\frac{\eta_0}{\kappa_0}\right)^2\right]e^2\cos^2 M\right\}, \qquad (9d)$$

which are adapted from Equations (47)–(55) of Borderies-Rappaport & Longaretti (1994). These equations are accurate to the order of $\mathcal{O}(e^2)$ and require $e \ll 1$. Here, $\Omega_0(a)$ is the angular velocity of a particle in a circular orbit while $\kappa_0(a)$ is its epicyclic frequency and the frequency $\eta_0(a)$ is defined

below, all of which are functions of the particle's semimajor axis a. Also keep in mind that when the following refers to the particle's orbit elements, it is the *epicyclic* orbit elements that are intended,[3] which are distinct from the *osculating* orbit elements that describe pure Keplerian motion around a spherical planet. But these distinctions disappear in the limit that the planet becomes spherical and the orbit frequencies Ω_0, κ_0, and η_0 all converge on the mean motion $\sqrt{Gm_0/a^3}$, where G is the gravitational constant and m_0 is the central planet's mass; in that case, Equations (9) recover a Keplerian orbit to the order of $\mathcal{O}(e^2)$.

The three orbit frequencies Ω_0, κ_0, and η_0 appearing in Equations (9) are obtained from spatial derivatives of the oblate planet's gravitational potential Φ, which is

$$\Phi(r) = -\frac{Gm_0}{r} + \frac{Gm_0}{r} \sum_{k=1}^{\infty} J_{2k} P_{2k}(0) \left(\frac{R_p}{r}\right)^{2k}, \quad (10)$$

where R_p is the planet's effective radius, J_{2k} is one of the oblate planet's zonal harmonics, and $P_{2k}(0)$ is a Legendre polynomial with zero argument. For reasons that will be evident shortly, these calculations will only preserve the J_2 term in the above sum, so

$$\Phi(r) = -\frac{Gm_0}{r} \left[1 + \frac{1}{2} J_2 \left(\frac{R_p}{r}\right)^2\right] \quad (11)$$

and the orbital frequencies are

$$\Omega_0^2(a) = \frac{1}{r}\frac{\partial\Phi}{\partial r}\bigg|_{r=a} = \frac{Gm_0}{a^3}\left[1 + \frac{3}{2} J_2\left(\frac{R_p}{a}\right)^2\right] \quad (12a)$$

$$\kappa_0^2(a) = \frac{3}{r}\frac{\partial\Phi}{\partial r}\bigg|_{r=a} + \frac{\partial^2\Phi}{\partial r^2}\bigg|_{r=a} = \frac{Gm_0}{a^3}\left[1 - \frac{3}{2} J_2\left(\frac{R_p}{a}\right)^2\right] \quad (12b)$$

$$\eta_0^2(a) = \frac{2}{r}\frac{\partial\Phi}{\partial r}\bigg|_{r=a} - \frac{r}{6}\frac{\partial^3\Phi}{\partial r^3}\bigg|_{r=a} = \frac{Gm_0}{a^3}\left[1 - 2J_2\left(\frac{R_p}{a}\right)^2\right] \quad (12c)$$

$$\beta_0^2(a) = -\frac{r^4}{24}\frac{\partial^4\Phi}{\partial r^4}\bigg|_{r=a} = \frac{Gm_0}{a^3}\left[1 + \frac{15}{2} J_2\left(\frac{R_p}{a}\right)^2\right], \quad (12d)$$

where the additional frequency $\beta_0(a)$ is needed below.

During the particle's unperturbed epicyclic drift phase, its angular orbit elements M and $\tilde{\omega}$ advance during timestep Δt by the amount

$$\Delta M = \kappa \Delta t \quad (13a)$$

$$\Delta\tilde{\omega} = (\Omega - \kappa)\Delta t, \quad (13b)$$

where the frequencies Ω and κ in Equations (13) differ slightly from Equations (12) due to additional corrections that are of the order of $\mathcal{O}(e^2)$:

$$\Omega(a, e) = \Omega_0 \left\{1 + 3\left[\frac{1}{2} - \left(\frac{\eta_0}{\kappa_0}\right)^2\right]e^2\right\} \quad (14a)$$

---

[3] Actually what we identify here as the semimajor axis a is called r_0 in Borderies-Rappaport & Longaretti (1994), which differs slightly from what they identify as the epicyclic semimajor axis a_e where $a_e = r_0(1 + e^2)$.

$$\kappa(a, e) = \kappa_0 \left(1 + \left\{\frac{15}{4}\left[\left(\frac{\Omega_0}{\kappa_0}\right)^2 - \left(\frac{\eta_0}{\kappa_0}\right)^4\right] - \frac{3}{2}\left(\frac{\beta_0}{\kappa_0}\right)^2\right\}e^2\right) \quad (14b)$$

(Borderies-Rappaport & Longaretti 1994).

Borderies-Rappaport & Longaretti (1994) also show that the above equations have three integrals of the motion: the particle's specific energy E, its specific angular momentum h, and its epicyclic energy I_3. Those integrals are

$$E = \frac{1}{2}\left(v_r^2 + v_\theta^2\right) + \Phi(r) = \frac{1}{2}(a\Omega_0)^2 + \Phi(a) + \frac{1}{2}(a\kappa_0)^2 e^2 + \mathcal{O}(e^4) \quad (15a)$$

$$h = rv_\theta = a^2\Omega_0 + \mathcal{O}(e^4), \quad (15b)$$

and

$$I_3 = \frac{1}{2}\left[v_r^2 + \kappa_0^2(r-a)^2\right] - \eta_0^2(r-a)^3/a$$
$$= \frac{1}{2}(a\kappa_0 e)^2 + \mathcal{O}(e^4). \quad (15c)$$

Advancing the particle along its epicyclic orbit requires converting its cylindrical coordinates and velocities into epicyclic orbit elements. To obtain the particle's semimajor axis, solve the angular momentum integral $h(a) = a^2\Omega_0$, which is quadratic in a, so

$$a = g\left(1 + \sqrt{1 - \frac{3J_2}{2g^2}}\right)R_p, \quad (16)$$

where $g = (rv_\theta)^2/2Gm_0R_p$. Note though that if the J_4 and higher oblateness terms had been preserved in the planet's potential, then the angular momentum polynomial would be of the degree of 4 and higher in a, for which there is no known analytic solution. That equation could still be solved numerically, but that step would have to be performed for all particles at every timestep, which would slow the N-body algorithm so much as to make it useless. Therefore, only the J_2 term is preserved here, which nonetheless accounts for the effects of planetary oblateness in a way that is sufficiently realistic.

To calculate the particle's remaining orbit elements, use Equation (15c) to obtain the I_3 integral, which then provides its eccentricity via

$$e = \frac{\sqrt{2I_3}}{a\kappa_0}. \quad (17)$$

Then set $x = e\cos M$ and $y = e\cos M$ and solve Equations (9a) and (9d) for x and y:

$$x = \left(\frac{\eta_0}{\kappa_0}\right)^2\left[2(1 + e^2) - \frac{v_\theta}{a\Omega_0} - \frac{r}{a}\right] + 1 - \frac{r}{a} \quad (18a)$$

and

$$y = \frac{v_r/a\kappa_0}{1 + 2(\eta_0/\kappa_0)^2 x}, \quad (18b)$$

which then provides the mean anomaly via $\tan M = y/x$.

To summarize, the epicyclic drift step uses Equations (15)–(18) to convert each particle's cylindrical coordinates into epicyclic orbit elements. The particles' orbit frequencies $\Omega(a, e)$ and $\kappa(a, e)$ are obtained via Equations (12) and (14), and Equations (13) are then used to advance each particle's orbit elements M and $\tilde{\omega}$ during timestep Δt, with Equations (9) used to convert the particles' orbit elements back into cylindrical coordinates.

2.3. Velocity Kicks due to the Ring's Internal Forces

The *N*-body code developed here is designed to follow the dynamical evolution of all $360°$ of a narrow annulus within a planetary ring, and it is intended to deliver accurate results quickly using a desktop PC. The most time-consuming part of this algorithm is the calculation of the accelerations that the gravitating ring exerts on all of its particles, so the principal goal here is to design an algorithm that will calculate these accelerations with sufficient accuracy while using the fewest possible number of simulated particles.

2.3.1. Streamlines

The dominant internal force in a dense planetary ring is its self-gravity, and the representation of the ring's full $360°$ extent via a modest number of *streamlines* provides a practical way to calculate rapidly the acceleration that the entire ring exerts on any one particle. A streamline is the closed path through the ring that is traced by those particles that share a common initial semimajor axis a. The simulated portion of the planetary ring will be comprised of N_r discreet streamlines that are spaced evenly in semimajor axis a, with each streamline comprised of N_θ particles on each streamline, so a model ring consists of $N_r N_\theta$ particles. Simulations typically employ $N_r \sim 100$ streamlines with $N_\theta \sim 50$ particles along each streamline, so a typical ring simulation uses about 5000 particles. Note though that the assignment of particles to a given streamline is merely labeling; particles are still free to wander over time in response to the ring's internal forces: gravity, pressure, and viscosity. But as the following will show, the simulated ring stays coherent and highly organized throughout the run, in the sense that particles on the same streamline do not pass each other longitudinally, nor do adjacent streamlines cross. Because the simulated ring stays so highly organized, there is no radial or transverse mixing of the ring particles, and the particles will preserve over time membership in their streamline.[4]

2.3.2. Ring Self-gravity

The concept of gravitating streamlines is widely used in analytic studies of ring dynamics (Goldreich & Tremaine 1979; Borderies et al. 1983a, 1986; Longaretti & Rappaport 1995; Hahn et al. 2009), and the concept is easily implemented in an *N*-body code. Because the simulated portion of the ring is narrow, its streamlines are all close in the radial sense. Consequently, the gravitational pull that one streamline exerts on a particle is dominated by the nearest part of the streamline, with that acceleration being quite insensitive to the fact that the more distant and unimportant parts of the perturbing streamline are curved. Therefore, the perturbing streamline can be regarded as a straight and infinitely long wire of matter whose linear density is $\lambda \simeq m_p N_\theta / 2\pi a$ to lowest order in the streamline's small eccentricity e, where m_p is the mass of a single particle. The gravitational acceleration that a wire of matter exerts on the particle is

$$A_g = \frac{2G\lambda}{\Delta}, \tag{19}$$

---

[4] But if the simulated ring is instead initialized with all particles on a given streamline having distinct (rather than common) values for a and e, then the resulting streamlines can appear ragged in longitude θ. And if that initial ring is sufficiently ragged or non-smooth, then that raggedness can grow over time as the particles a's and e's evolve independently. The main point is that the streamline model employed here succeeds when all streamlines are sufficiently smooth, and that is accomplished by initializing all particles in a given streamline with common a, e.

where Δ is the separation between the particle and the streamline. However, the particles in that streamline only provide N_θ discreet samplings of a streamline that is after all slightly curved over larger spatial scales. So to find the distance to nearest part of the perturbing streamline, the code identifies at every timestep the three perturbing particles that are nearest in longitude to the perturbed particle. A second-degree Lagrange polynomial is then used to fit a smooth continuous curve through those three particles (Kudryavtsev & Samarin 2013), and this polynomial provides a convenient method for extrapolating the perturbing streamline's distance Δ from the perturbed particle. This procedure is also illustrated in Figure 3, which shows that the radial and tangential components of that acceleration are

$$A_{g,r} \simeq A_g \tag{20a}$$

and
$$A_{g,\theta} \simeq -A_g v_r' / v_\theta' \tag{20b}$$

to lowest order in the perturbing streamline's eccentricity e', where v_r' and v_θ' are the radial and tangential velocity components of that streamline. Equation (20) is then summed to obtain the gravitational acceleration that all other streamlines exert on the particle.

To obtain the gravity that is exerted by the streamline that the particle inhabits, treat the particle as if it resides in a gap in that streamline that extends midway to the adjacent particles. The nearby portions of that streamline can be regarded as two straight and semi-infinite lines of matter pointed at the particle whose net gravitational acceleration is

$$A_g = 2G\lambda \left(\frac{1}{\Delta_+} - \frac{1}{\Delta_-} \right), \tag{21}$$

where Δ_+ and Δ_- are the particle's distance from its neighbors in the leading (+) and trailing (-) directions. The radial and tangential components of that streamline's gravity are

$$A_{g,r} \simeq A_g v_r / v_\theta \tag{22a}$$

and
$$A_{g,\theta} \simeq A_g, \tag{22b}$$

where v_r, v_θ are the perturbed particle's velocity components.

A major benefit of using Equation (19) to calculate the ring's gravitational acceleration is that there is no artificial gravitational stirring. This is in contrast to a traditional *N*-body model that would use discreet point masses to represent what is really a continuous ribbon of densely packed ring matter. Those gravitating point masses then tug on each other in amounts that vary rapidly in magnitude and direction as they drift past each other in longitude, and those rapidly varying tugs will quickly excite the simulated particles' dispersion velocity. As a result, the particles' unphysical random motions tend to wash out the ring's large-scale coherent forced motions, which is usually the quantity that is of interest. So, although Equation (19) is only approximate because it does not account for the streamline's curvature that occurs far away from a perturbed ring particle, Equation (19) is still much more realistic and accurate than the force law that would be employed in a traditional global *N*-body simulation of a planetary ring, which out of computational necessity would treat a continuous stream of ring matter as discreet clumps of overly massive gravitating particles.
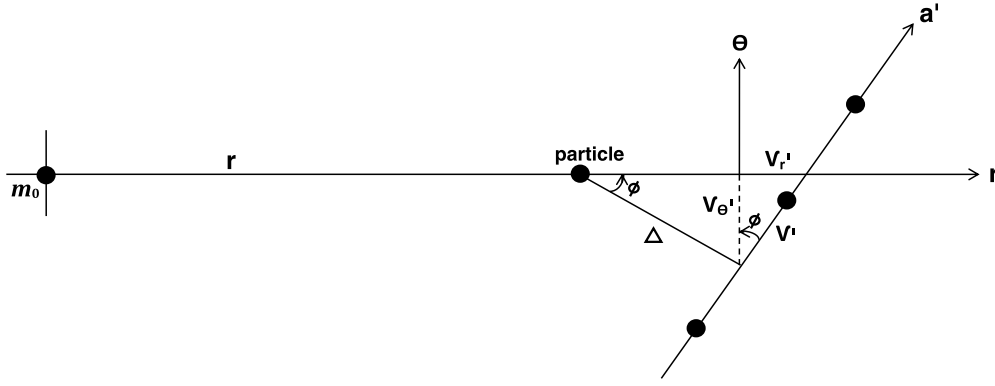
Figure 3. Particle lies at a distance r from the central mass m_0 and is perturbed by a streamline whose particles have semimajor axes a'. The shape of that streamline is determined by fitting a Lagrange polynomial to the three particles that are nearest in longitude, which is represented by the nearly straight curve a', with that polynomial then providing the streamline's distance Δ from the particle at r. The streamline's gravitational acceleration of that particle is $A_g = 2G\lambda/\Delta$, which has radial and tangential components $A_{g,r} = A_g \cos\phi$ and $A_{g,\theta} = -A_g \sin\phi$ where angle ϕ obeys $\sin\phi = v_r'/v' \simeq v_r'/v_\theta'$ and $\cos\phi = v_\theta'/v' \simeq 1$ to lowest order in the perturbing streamline's eccentricity e', so $A_{g,r} \simeq A_g$ and $A_{g,\theta} \simeq -A_g v_r'/v_\theta'$.

2.3.3. Ring Pressure

A planetary ring is very flat and its vertical structure will be unresolved in this model, so a 1D pressure p is employed here. That pressure p is the rate-per-length that a streamline segment communicates linear momentum to the adjacent streamline orbiting just exterior to it, with that momentum exchange being due to collisions occurring among particles on adjacent streamlines. So for a small streamline segment of length $\delta\ell$ that resides somewhere in the ring's interior, the net force on that segment due to ring pressure is $\delta f = [p(r - \Delta) - p(r)]\delta\ell$ since $p(r - \Delta)$ is the pressure or force-per-length exerted by the streamline that lies just interior and a distance Δ away from segment $\delta\ell$, and $p(r)$ is the force-per-length that segment $\delta\ell$ exerts on the exterior streamline. And since force $\delta f = A_p \delta m$ where $\delta m = \lambda \delta\ell$ is the segment's mass, the acceleration on a particle due to ring pressure is

$$A_p = \frac{\delta f}{\delta m} = \frac{p(r - \Delta) - p(r)}{\lambda} \simeq -\frac{\Delta}{\lambda}\frac{\partial p}{\partial r} = -\frac{1}{\sigma}\frac{\partial p}{\partial r} \quad (23)$$

since the ring's surface density $\sigma = \lambda/\Delta$.

Formulating the acceleration in terms of pressure differences across adjacent streamlines is handy because the model can then easily account for the large pressure drop that occurs at a planetary ring's edge, which can be quite abrupt when the ring's edge is sharp. For a particle orbiting at the ring's innermost streamline, the acceleration there is simply $A_p = -p(r)/\lambda$ since there is no ring matter orbiting interior to it so $p(r - \Delta) = 0$ there; likewise the acceleration of a particle in the ring's outermost streamline is $A_p = p(r - \Delta)/\lambda$. Pressure is exerted perpendicular to the streamline and hence it is predominantly a radial force, so by the geometry of Figure 3 the radial component of the acceleration due to pressure is $A_{p,r} \simeq A_p$ while the tangential component $A_{p,\theta} \simeq -A_p v_r/v_\theta$ is smaller by a factor of e, where v_r and v_θ are the perturbed particle's radial and tangential velocities. This accounts for the pressure on the particle due to adjacent streamlines.

The acceleration on the particle due to pressure gradients in the particle's streamline is simply $A_p = -(\partial p/\partial\theta)/(r\sigma)$. This acceleration points in the direction of the particle's motion, so the radial and tangential components of that acceleration are $A_{p,r} \simeq A_p v_r/v_\theta$ and $A_{p,\theta} \simeq A_p$.

Acceleration due to pressure requires selecting an equation of state (EOS) that relates the pressure p to the ring's other

properties, and this study will treat the ring as a dilute gas of colliding particles for which the 1D pressure is $p = c^2\sigma$ where c is the particles dispersion velocity. However, an alternate EOS exists for planetary rings, and that possibility is discussed in Section 4.2.

A simple finite difference scheme is used to calculate the pressure gradient in Equation (23) in the vicinity of particle i in streamline j that lies at longitude $\theta_{i,j}$. Lagrange polynomials are again used to evaluate the adjacent streamlines' planetocentric distances $r_{i,j-1}$ and $r_{i,j+1}$ along the particle's longitude $\theta_{i,j}$, so the pressure gradient at particle i in streamline j is

$$\left.\frac{\partial p}{\partial r}\right|_{i,j} \simeq \frac{p_{i,j+1} - p_{i,j-1}}{r_{i,j+1} - r_{i,j-1}}, \quad (24)$$

where the pressures in the adjacent streamlines $p_{i,j+1}$ and $p_{i,j-1}$ are also determined by interpolating those quantities to the perturbed particle's longitude $\theta_{i,j}$.

The surface density $\sigma_{i,j}$ in the vicinity of particle i in streamline j is determined by centering a box about that particle whose radial extent spans half the distance to the neighboring streamlines, so

$$\sigma_{i,j} = \frac{2\lambda_j}{r_{i,j+1} - r_{i,j-1}}. \quad (25)$$

If, however, streamline j lies at the ring's inner edge where $j = 0$, then the surface density there is $\sigma_{i,0} = \lambda_0/(r_{i,1} - r_{i,0})$ while the surface density at the outermost $j = N_r - 1$ streamline is $\sigma_{i,N_r-1} = \lambda_{N_r-1}/(r_{i,N_r-1} - r_{i,N_r-2})$.

2.3.4. Ring Viscosity

Viscosity has two types, shear viscosity and bulk viscosity. Shear viscosity is the friction that results as particles on adjacent streamlines collide as they flow past each other. The friction due to this shearing motion causes adjacent streamlines to torque each other, so shear viscosity communicates a radial flux of angular momentum through the ring. A particle on a streamline experiences a net torque and hence a tangential acceleration when there is a radial gradient in that angular momentum flux.

Also, if there are additional spatial gradients in the ring's velocities that cause ring particles to converge toward or diverge away from each other, then these relative motions will cause ring particles to bump each other as they flow past, which transmits momentum through the ring via the pressure forces discussed

above. However, the ring particles' viscous bulk friction tends to retard those relative motions, and that friction results in an additional flux of linear momentum through the ring. Any radial gradients in that linear momentum flux then results in a radial acceleration on a ring particle.

The 1D radial flux of the z component of angular momentum due to the ring's shear viscosity is derived in Appendix A:

$$F = -\nu_s \sigma r^2 \frac{\partial \dot{\theta}}{\partial r} \quad (26)$$

(see Equation (A16)), where ν_s is the ring's kinematic shear viscosity and $\dot{\theta} = v_\theta/r$ is the angular velocity. The quantity F is the rate-per-length that one streamline segment communicates angular momentum to the adjacent streamline orbiting just exterior, so the net torque on a streamline segment of length $\delta\ell$ is $\delta\tau = [F(r - \Delta) - F(r)]\delta\ell$, but $\delta\tau = r A_{\nu,\theta}\delta m$ where $\delta m = \lambda \delta\ell$ so the tangential acceleration due to the ring's shear viscosity is

$$A_{\nu,\theta} = \frac{F(r - \Delta) - F(r)}{\lambda r} = -\frac{1}{\sigma r}\frac{\partial F}{\partial r}. \quad (27)$$

Again this differencing approach is useful because it easily accounts for the large viscous torque that occurs at a ring's sharp edge since $A_{\nu,\theta} = -F(r)/\lambda r$ at the ring's inner edge and $A_{\nu,\theta} = F(r - \Delta)/\lambda r$ at the ring's outer edge.

Appendix B shows that the radial flux of linear momentum due to the ring's shear and bulk viscosity is

$$G = -\left(\frac{4}{3}\nu_s + \nu_b\right)\sigma\frac{\partial v_r}{\partial r} - \left(\nu_b - \frac{2}{3}\nu_s\right)\frac{\sigma v_r}{r} \quad (28)$$

(Equation (B7)), where ν_b is the ring's bulk viscosity. This quantity is analogous to a 1D pressure so the corresponding acceleration is

$$A_{\nu,r} = \frac{G(r - \Delta) - G(r)}{\lambda} = -\frac{1}{\sigma}\frac{\partial G}{\partial r} \quad (29)$$

in the ring's interior and $A_{\nu,r} = -G(r)/\lambda$ or $A_{\nu,r} = G(r - \Delta)/\lambda$ along the ring's inner or outer edges.

To evaluate the partial derivatives that appear in the flux Equations (26) and (28), Lagrange polynomials are again used to determine the angular and radial velocities $\dot{\theta}$ and v_r in the adjacent streamlines, interpolated at the perturbed particle's longitude, with finite differences used to calculate the radial gradients in those quantities.

2.3.5. Satellite Gravity

All ring particles are also subject to each satellite's gravitational acceleration, $A_s = Gm_s/\Delta^2$, where m_s is the satellite's mass and Δ is the particle–satellite separation. Satellites also feel the gravity exerted by all the ring particles, as well as the satellites' mutual gravitational attractions.

Also, once all of the accelerations of each ring particle and satellite are tallied, each body is then subject to the corresponding velocity kicks of steps (1) and (5) that are described just below Equation (8).

2.4. Tests of the Code

The N-body integrator developed here is called epi_int, which is shorthand for *epicyclic integrator*, and the following

briefly describes the suite of simulations whose known outcomes are used to test all of the code's key parts.

Forced motion at a Lindblad resonance. Numerous massless particles are placed in circular orbits at Mimas's $m = 2$ ILR. In this test, Mimas's initially zero mass is slowly grown to its current mass over an exponential timescale $\tau_s = 1.6 \times 10^4$ ring orbits, which excites adiabatically the ring particle's forced eccentricities to levels that are in excellent agreement with the solution to the linearized equations of motion, Equation (42) of Goldreich & Tremaine (1982). Similar results are also obtained for the particle's response to Janus's $m = 7$ ILR, which is responsible for confining the outer edge of Saturn's A ring. These simulations test the implementation of the integrator's kick-step-drift scheme as well as the satellite's forcing of the ring.

Precession due to oblateness. This simple test confirms that the orbits of massless particles in low-eccentricity orbits precess at the expected rate, $\tilde{\omega}(a) = \Omega - \kappa = (3/2)J_2(R_p/a)^2\Omega(a)$, due to planetary oblateness J_2.

Ringlet eccentricity gradient and libration. When a narrow eccentric ringlet is in orbit about an oblate planet, dynamical equilibrium requires the ringlet to have a certain eccentricity gradient so that differential precession due to self-gravity cancels that due to oblateness. And when the ringlet is composed of only two streamlines then this scenario is analytic, with the ringlet's equilibrium eccentricity gradient given by Equation (28b) of Borderies et al. (1983b). So to test epi_int's treatment of ring self-gravity, we perform a suite of simulations of narrow eccentric ringlets that have surface densities $40\,\mathrm{g\,cm^{-2}} < \sigma < 1000\,\mathrm{g\,cm^{-2}}$ with initial eccentricity gradients given by Equation (28b), and integrate over time to show that these pairs of streamlines do indeed precess in sync with no relative precession, as expected, over runtimes that exceed of the timescale for massless streamlines to precess differentially. And when we repeat these experiments with the ringlets displaced slightly from their equilibrium eccentricity gradients, we find that the simulated streamlines librate at the frequency given by Equation (30) of Borderies et al. (1983b), as expected.

Density waves in a pressure-supported disk. This test examines the model's treatment of disk pressure and uses a satellite to launch a two-armed spiral density wave at its $m = 2$ ILR in a non-gravitating pressure-supported disk. The resulting pressure wave has a wavelength and an amplitude that agree with Equation (46) of Ward (1986), as expected.

Viscous spreading of a narrow ring. In this test, epi_int follows the radial evolution of an initially narrow ring as it spreads radially due to its viscosity, and the simulated ring's surface density $\sigma(r, t)$ is in excellent agreement with the expected solution, Equation (2.13) of Pringle (1981).

3. SIMULATIONS OF THE OUTER EDGE OF SATURN'S B RING

The semimajor axis of the outer edge of Saturn's B ring is $a_{\mathrm{edge}} = 117568 \pm 4$ km, and that edge lies $\Delta a_2 = 12 \pm 4$ km exterior to Mimas's $m = 2$ ILR (Spitale & Porco 2010, hereafter SP10). Evidently, Mimas's $m = 2$ ILR is responsible for confining the B ring and preventing it from viscously diffusing outward and into the Cassini Division. Mimas's $m = 2$ ILR excites a forced disturbance at the ring-edge whose radius–longitude relationship $r(\theta)$ is expected to have the form $r(\theta, t) = a_{\mathrm{edge}} - R_m \cos m(\theta - \tilde{\omega}_m)$ where R_m is the epicyclic amplitude of the mode whose azimuthal wavenumber

is m and whose orientation at time t is given by the angle $\tilde{\omega}_m(t)$. This forced disturbance is expected to corotate with Mimas's longitude, and such a pattern would have a pattern speed $\dot{\tilde{\omega}}_m = d\tilde{\omega}_m/dt$ that satisfies $\dot{\tilde{\omega}}_m = \Omega_s$ where Ω_s is satellite Mimas's angular velocity.

SP10 have analyzed the many images of the B ring's edge that have been collected by the *Cassini* spacecraft, and they show that this ring-edge does indeed have a forced $m = 2$ shape that corotates with Mimas as expected. But they also show that the B ring's edge has an additional *free $m = 2$* pattern that rotates slightly faster than the forced pattern. SP10 also detect two additional modes, a slowly rotating $m = 1$ pattern as well as a rapidly rotating $m = 3$ pattern. These findings are confirmed by stellar occultation observations of the B ring's outer edge that also detect additional lower-amplitude $m = 4$ and $m = 5$ modes (Nicholson et al. 2012).

The following will use the N-body model to investigate the higher amplitude $m = 1, 2,$ and 3 modes seen at the B ring's edge. But keep in mind that only the $m = 2$ forced pattern has a known driver, namely, Mimas's $m = 2$ ILR, while the nature of the perturbation that launched the other three free modes in the B ring is quite unknown. So to study the B ring's behavior when those free modes are present, an admittedly ad hoc method is used. Specifically, the simulated ring particles' initial conditions are constructed in a way that plants a free $m = 1, 2,$ or 3 pattern at the simulated ring's edge at time $t = 0$. The N-body integrator then advances the system over time, which then reveals how those free patterns evolve over time. And to elucidate those findings most simply, the following subsections first consider the B ring's $m = 1, 2,$ and 3 patterns in isolation.

All simulations use a timestep $\Delta t = 0.2/2\pi = 0.0318$ orbit periods, so there are 31.4 timesteps per orbit of the simulated B ring, and nearly all simulations use oblateness $J_2 = 0.01629071$, which is the same value we used in previous work (Hahn et al. 2009).

Last, these simulations also zero the viscous acceleration that is exerted at the simulated B ring's innermost and outermost streamlines, to prevent them from drifting radially due to the ring's viscous torque. This is in fact appropriate for the simulation's innermost streamline, since in reality the viscous torque from the unmodeled part of the B ring should deliver to the inner streamline a constant angular momentum flux F that it then communicates to the adjacent streamline, so the viscous acceleration $A_{\nu,\theta} \propto \partial F/\partial r$ at the simulation's inner edge really should be zero. However, zeroing the viscous acceleration of outer streamline might seem like a slight-of-hand since it should be $A_{\nu,\theta} = F/\lambda r$ according to Section 2.3.4. But setting $A_{\nu,\theta} = 0$ is done because, if not, then the outermost streamline will slowly but steadily drift radially outward past Mimas's $m = 2$ ILR, which also causes that streamline's forced eccentricity to slowly and steadily grow as the streamline migrates. This happens because the model does not settle into a balance where the ring's positive viscous torque on its outermost streamline is opposed by a negative torque exerted by the satellite's gravity. We also note that the semi-analytic model of this resonant ring-edge, which is described in Hahn et al. (2009), also had the same difficulty in finding a torque balance. So to sidestep this difficulty, this model zeros the viscous acceleration at the outermost streamline, which keeps its semimajor axis static as if it were in the expected torque balance. This then allows us to compare simulations to the B ring's forced $m = 2$ pattern to that measured by the *Cassini* spacecraft. The validity of this approximation is also assessed below in Section 4.1.

3.1. The Forced and Free m = 2 Patterns

SP10 detect a forced $m = 2$ pattern at the B ring's outer edge that has an epicyclic amplitude $R_2 = 34.6 \pm 0.4$ km, and that forced pattern corotates with the satellite Mimas. They also detect a free pattern whose epicyclic amplitude is 2.7 km larger, so the forced and free patterns are nearly equal in amplitude, and the free pattern rotates slightly faster than the forced pattern by $\Delta\dot{\tilde{\omega}}_2 = 0.0896 \pm 0.0007$ deg day^{-1} (SP10). The radius–longitude relationship for a ring-edge that experiences these two modes can be written as

$$r(\theta, t) = a - R_2 \cos m(\theta - \theta_s) - \tilde{R}_2 \cos m(\theta - \tilde{\omega}_2), \quad (30)$$

where R_2 is the epicyclic amplitude of the forced pattern that corotates with Mimas whose longitude is $\theta_s(t)$ at time t, and $\tilde{R}_2$ is the epicyclic amplitude of the free pattern with $\tilde{\omega}_2(t)$ being the free pattern's longitude.

The N-body integrator `epi_int` is used to simulate the forced and free $m = 2$ patterns that are seen at the outer edge of the B ring, for simulated rings having a variety of initial surface densities σ_0. These simulations use $N_r = 130$ streamlines that are distributed uniformly in the radial direction with spacings $\Delta a = 5.13$ km, so the radial width of the simulated portion of the B ring is $w = (N_r - 1)\Delta a = 662$ km. Each streamline is populated with $N_\theta = 50$ particles that are initially distributed uniformly in longitude θ and in circular coplanar orbits. These simulations use a total of $N_r N_\theta = 6500$ particles, which is more than sufficient to resolve the $m = 2$ patterns seen here. These systems are evolved for $t = 41.5$ yr, which corresponds to 3.2×10^4 orbits, and is sufficient time to see the simulation's slightly faster free $m = 2$ pattern lap the forced $m = 2$ pattern several times. The execution time for these high resolution, publication-quality simulations is 1.5 days on a desktop PC, but sufficiently useful preliminary results from lower-resolution simulations can be obtained in just a few hours.

The B ring's viscosity is unknown, so these simulations will employ a value for the kinematic shear viscosity ν_s and bulk viscosity ν_b that are typical of Saturn's A ring, $\nu_s = \nu_b = 100$ cm^2 s^{-1} (Tiscareno et al. 2007). The simulated particles' dispersion velocity c is also chosen so that the ring's gravitational stability parameter $Q = c\kappa/\pi G\sigma_0 = 2$, since Saturn's main rings likely have $1 \lesssim Q \lesssim 2$ (Salo 1995). Mimas's mass is $m_s = 6.5994 \times 10^{-8}$ Saturn masses, and its semimajor axis a_s is chosen so that its $m = 2$ ILR lies $\Delta a_{\rm res} = 12.2$ km interior to the simulated B ring's outer edge. This model only accounts for the $J_2 = 0.01629071$ part of Saturn's oblateness, so the constraint on the resonance location puts the simulated Mimas at $a_s = 185577.0$ km, which is 38 km exterior to its real position.

Starting the ring particles in circular orbits provides an easy way to plant equal-amplitude free and forced $m = 2$ patterns in the ring. This creates a free $m = 2$ pattern that at time $t = 0$ nulls perfectly the forced $m = 2$ pattern due to Mimas. However, the free pattern rotates slightly faster than the forced pattern, so the ring's epicyclic amplitude varies between near zero and $\sim 2 R_2$ as the rotating patterns interfere constructively or destructively over time. This behavior is illustrated in Figure 4, which shows results from a simulation of a B ring whose undisturbed surface density is $\sigma_0 = 280$ g cm^{-2}. The wire diagrams show the ring's streamlines via radius versus longitude plots, with dots indicating individual particles, and the adjacent grayscale map shows the ring's surface density at that instant. Figure 4 shows snapshots of the system at five distinct times that span one cycle
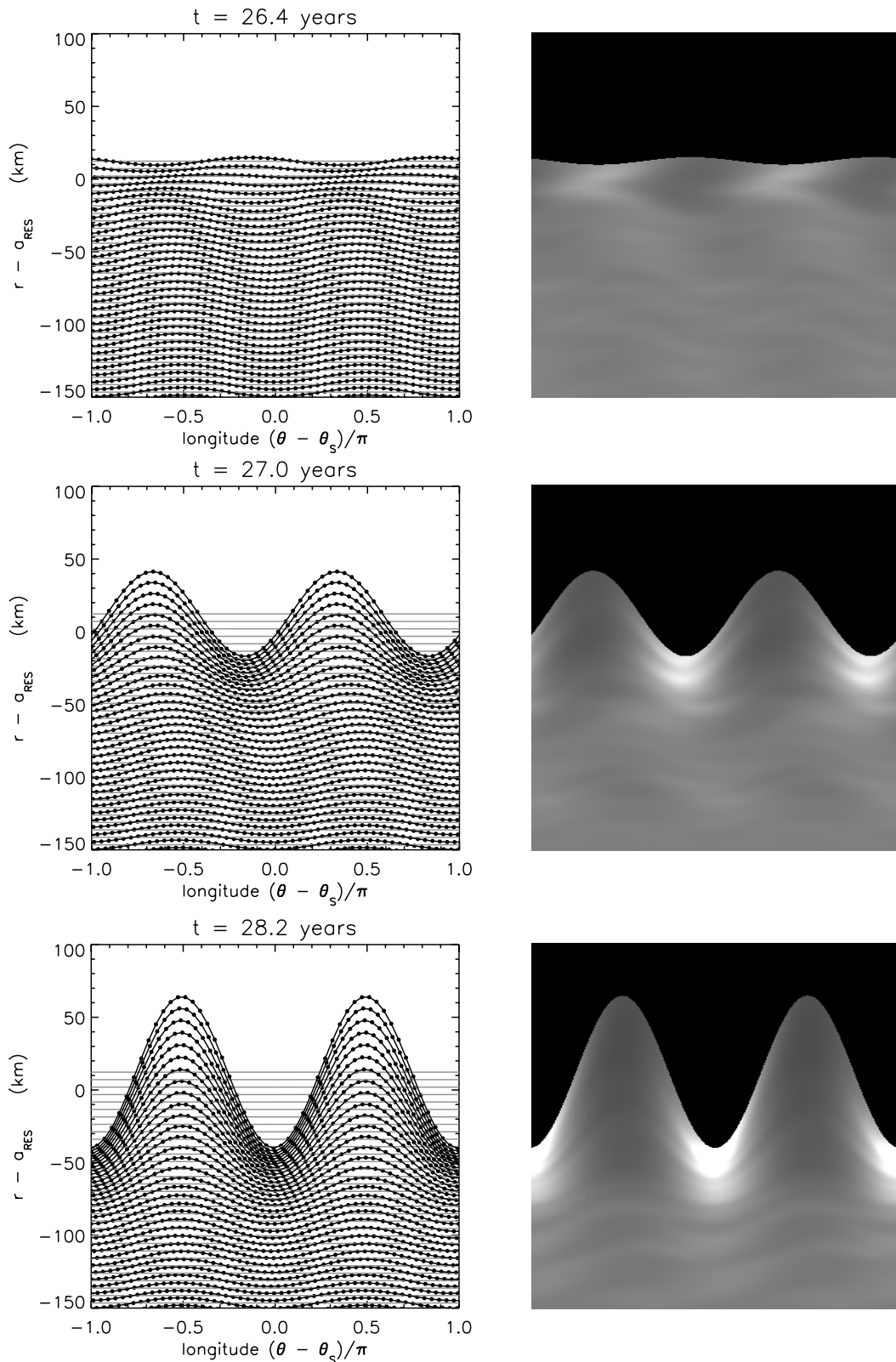
Figure 4. Five snapshots of a simulated B ring that is perturbed by Mimas's $m = 2$ ILR. The simulated ring has an undisturbed surface density $\sigma_0 = 280$ g cm^{-2}, with other model details provided in Section 3.1. Black curves show each distorted streamline via a radius vs. longitude plot, with the streamline's radial displacement measured along the vertical axis and longitude measured along the horizontal axis. Note that the simulated ring extends inward another 420 km beyond that shown here. All distances are measured relative to the resonance radius $a_{\rm res}$ and all longitudes are measured relative to satellite Mimas's longitude θ_s. Dots indicate the locations of all particles, and gray lines indicate their semimajor axes. The grayscale map shows the fractional variations in the ring's surface density σ/σ_0 scaled so that gray corresponds to an undisturbed region having $\sigma = \sigma_0$, black for regions where there is no ring matter, and white saturating in regions where the ring is overdense by at least two, $\sigma \geqslant 2\sigma_0$. Keep in mind that the particles sample the ring's surface density across an irregular grid, so to generate these grayscale maps, a spline is first fit to each streamline so that each is resampled along a regularly spaced grid in longitude θ. Then another set of splines is fit along each longitude to determine the radial distance $r(\theta)$ of each streamline along direction θ, which then allows the ring's surface density $\sigma(r, \theta)$ to be determined along a grid that is uniformly sampled in r, θ.
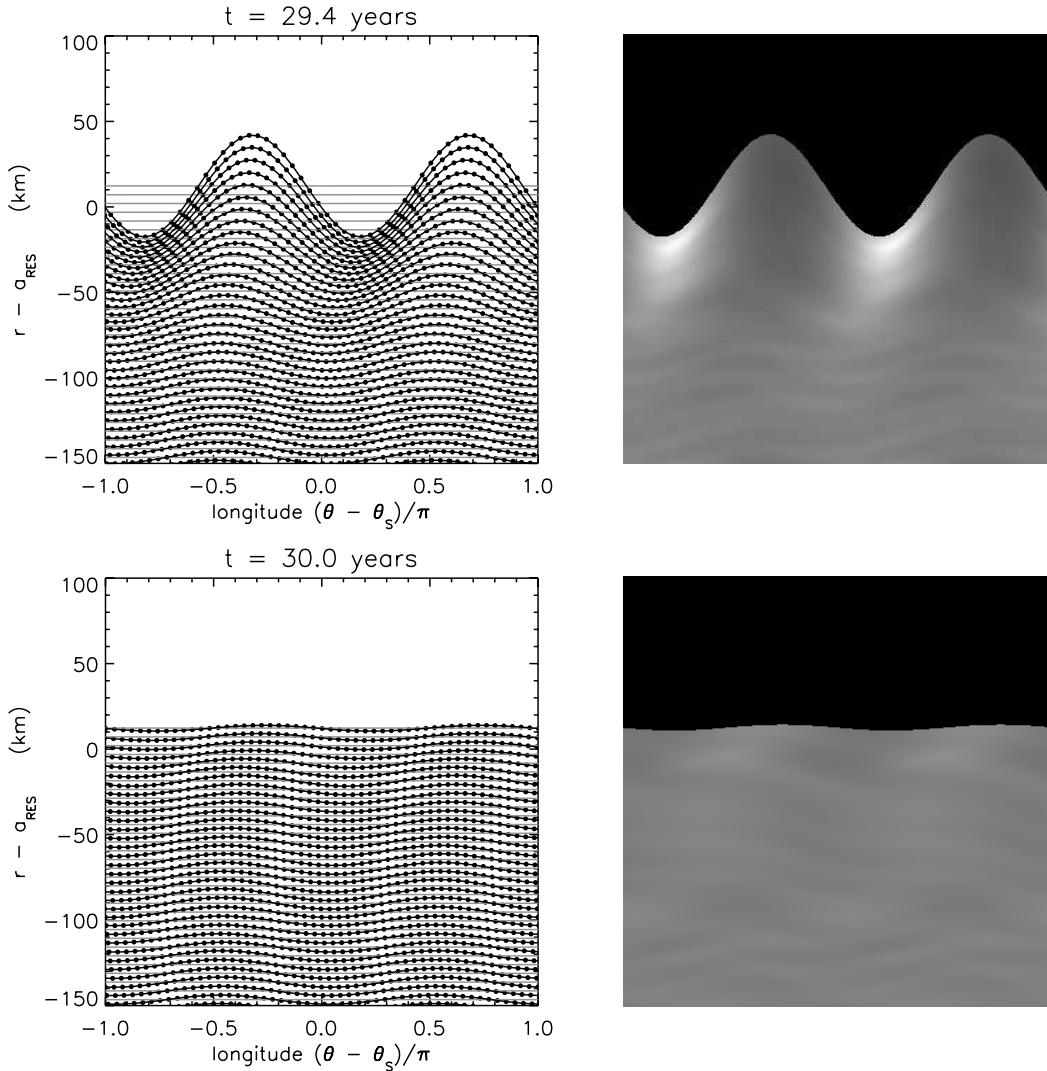
Figure 4. (Continued)

of the ring's circulation: at time $t = 26.4$ yr when the ring's outermost streamline is nearly circular due to the forced and free patterns being out of phase by nearly $180°/m = 90°$ and interfering destructively, to time $t = 28.2$ yr when the forced and free patterns are in phase and interfere constructively, to nearly circular again at time $t = 30.0$ yr.

The circulation cycle seen in Figure 4 repeats for the duration of the integration, which spans about 10 cycles. The gray lines in Figure 4 show the semimajor axes a of all particles on each streamline; note that all particles on a given streamline preserve a common semimajor axes, and this is also true of their eccentricities e. In the simulations shown here, the two orbit elements a and e do not vary with the particle's longitude θ. This, however, is distinct from the particles' angular orbit elements M and $\tilde{\omega}$, which do vary linearly with longitude θ along each streamline. Recall that the `epi_int` code does not in any way force or require particles to inhabit a given streamline. The streamline concept is only used when calculating the forces that all of the ring's streamlines exert on each particle, which the symplectic integrator then uses to advance these particles forward in time. Although a particle's e and a are in principle free to drift away from that of the other streamline-members, that does not happen in the simulations shown here; evidently the particles' a and e evolve slowly in the orbit-averaged sense, with

that time-averaged evolution being independent of longitude θ. This accounts for why all particles on the same streamline have the same evolution in a and e. This time-averaged evolution is also a standard assumption that is routinely invoked in analytic models of planetary rings (see *cf.* Goldreich & Tremaine 1979; Borderies et al. 1986; Hahn et al. 2009), and the simulations shown here confirm the validity of that assumption.

A suite of seven B ring simulations is performed for rings whose undisturbed surface densities range over $120\,\mathrm{g\,cm}^{-2} \leqslant \sigma_0 \leqslant 360\ \mathrm{g\ cm}^{-2}$. Results are summarized in Figure 5, which shows the forced epicyclic amplitude R_2 (solid curve) and the free epicyclic amplitude $\tilde{R}_2$ (dashed curve) from each simulation. These amplitudes are obtained by fitting Equation (30) to the simulated B ring's outermost streamline assuming that the free pattern there rotates at a constant rate, $\tilde{\omega}_2(t) = \tilde{\omega}_0 + \dot{\tilde{\omega}}_2 t$ where $\tilde{\omega}_0$ is the free pattern's angular offset at time $t = 0$ and $\dot{\tilde{\omega}}_2$ is the free mode's pattern speed. Equation (30) provides an excellent representation of the ring-edge's behavior over time, and that equation has four parameters, R_2, $\tilde{R}_2$, $\tilde{\omega}_0$, and $\dot{\tilde{\omega}}_2$, that are determined by least squares fitting. The observed epicyclic amplitude of the B ring's forced $m = 2$ component is $R_2 = 34.6 \pm 0.4$ km (SP10), and the gray bar in Figure 5 indicates that the outer edge of the B ring has a surface density
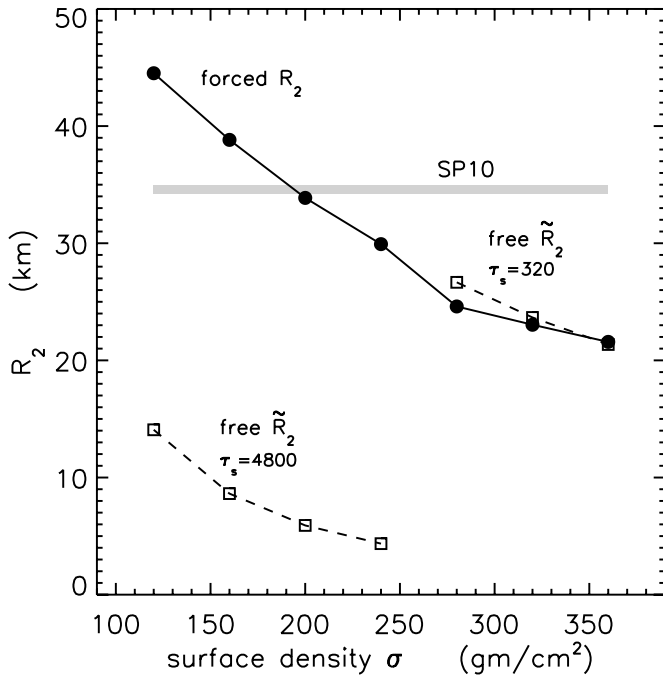
Figure 5. Solid curve is the epicyclic amplitude R_2 for the $m = 2$ pattern forced by Mimas, plotted vs. ring surface density σ_0 for the B ring simulations described in Section 3.1. The dashed curve gives the simulated ring's free epicyclic amplitude $\tilde{R}_2$. The gray bar is the ring's observed forced $m = 2$ epicyclic amplitude, from SP10; the bar's vertical extent, ± 0.35 km, spans the uncertainty in the observed R_2. In simulations with $\sigma_0 \leqslant 240$ g cm^{-2}, Mimas is grown to its current mass over timescales $\tau_s = 4800$ ring orbits, and simulations with $\sigma_0 \geqslant 280$ g cm^{-2} have $\tau_s = 320$ orbits.

of about $\sigma_0 = 195$ g cm^{-2}. And if we naively assume that the ring's surface density is everywhere the same, then its total mass of Saturn's B ring is about 90% of Mimas's mass.

Figure 5 also shows that the amplitude of the forced pattern R_2 gets larger for rings that have a smaller surface density σ_0, due to the ring's lower inertia, with the forced response varying roughly as $R_2 \propto \sigma_0^{-0.67}$. This also makes lighter rings more difficult to simulate, because their larger epicyclic amplitudes also causes the ring's streamlines to get more bunched up at periapse. For instance in the $\sigma_0 = 280$ g cm^{-2} simulation of Figure 4, the ring's edge at longitudes $\theta = \theta_s$ and $\theta = \theta_s \pm \pi$ are overdense by a factor of three at time $t = 28.2$ yr, which is when the force and free patterns add constructively. Streamline bunching in lighter rings is even more extreme, which is also more problematic, because streamlines that are too compressed can at times cross in these overdense sites, and the simulated ring's subsequent evolution becomes unreliable.

To avoid the streamline crossing that occurs in simulations of lower surface density, the model also grows the mass of Mimas exponentially over the timescale τ_s that takes values of 0.41 yr $\leqslant \tau_s \leqslant 6.2$ yr, with faster satellite growth ($\tau_s = 0.41$ yr or 320 B ring orbits) occurring in simulations of a heavy B ring having $\sigma_0 \geqslant 280$ g cm^{-2} and slower growth ($\tau_s = 6.2$ yr or 4800 B ring orbits) for the lighter $\sigma_0 \leqslant 240$ g cm^{-2} ring simulations. The satellite growth timescale τ_s controls the amplitude of the free pattern $\tilde{R}_2$, with the ring having a smaller free epicyclic amplitude $\tilde{R}_2$ when τ_s is larger; see the dashed curve in Figure 5. Indeed, when the satellite grows over a timescale $\tau_s \gg 6.2$ yr (i.e., $\tau_s \gg 4800$ orbits), the ring responds adiabatically to forcing by the slowly growing Mimas, and shows only a forced $m = 2$ pattern that corotates with Mimas,

with the free $m = 2$ pattern having a negligible amplitude. Consequently, only the $\sigma_0 = 280, 320$, and 360 g cm^{-2} simulations in Figure 5 are faithful in their attempt to reproduce a B ring whose free epicyclic amplitude $\tilde{R}_2$ is slightly larger than the forced amplitude R_2. However the lower-surface-density simulations have free patterns whose amplitudes are smaller than the forced patterns, and these simulated rings have outer edges whose longitude of periapse librate about Mimas's longitude, rather than circulate.

Also of interest here is the so-called radial depth of the $m = 2$ disturbance, $\Delta a_{e/10}$, which is defined as the semimajor axis separation between the ring's outer edge and the streamline whose mean eccentricity is one-tenth that of the edge's eccentricity. For these $m = 2$ simulations the radial depth is $\Delta a_{e/10} = 154$ km, so the radial width of the simulated part of the ring is $w = 4.3 \Delta a_{e/10}$.

3.1.1. Sensitivity to Resonance Location and Other Factors

The surface density σ_0 that is inferred from the amplitude of the ring's forced motion R_2 is very sensitive to the uncertainty in the ring's semimajor axis, which is $\delta a_{\rm edge}$. For example, when the B ring is simulated again but with its outer edge instead extending further out by $\delta a_{\rm edge} = 4$ km, those simulations show that the ring's forced amplitude R_2 is larger by about 6 km, which requires increasing σ_0 by $\delta\sigma_0 = 60$ g cm^{-2} so that the simulated R_2 is in agreement with the observed value. Similarly, when the simulated ring's edge is moved inward by $\delta a_{\rm edge} = 4$ km, the forced amplitude R_2 is smaller and the ring's surface density σ_0 must be decreased by $\delta\sigma_0$ to compensate. So the surface density of the B ring-edge is $\sigma_0 = 195 \pm 60$ g cm^{-2}, and this value represents the mean surface density of outer $\Delta a_{e/10} \simeq 150$ km that is most strongly disturbed by Mimas's $m = 2$ resonance. These results are also in excellent agreement with the semi-analytic model of Hahn et al. (2009), which calculated only the ring's forced motion.

However, these results are very insensitive to the model's other main unknown, the ring's viscosity ν. For instance, when we re-run the $\sigma_0 = 200$ g cm^{-2} simulation with the ring's shear and bulk viscosities increases as well as decreased by a factor of 10, we obtain the same forced response R_2. Therefore, these findings are insensitive to range of ring viscosities considered here, 10 cm^2 s$^{-1} < \nu < 1000$ cm^2 s^{-1}.

3.1.2. Free $m = 2$ Pattern

The dotted curve in Figure 6 shows the simulations' free $m = 2$ pattern speeds $\dot{\tilde{\omega}}_2$, which is also sensitive to the ring's undisturbed surface density σ_0. The purpose of this subsection is to illustrate how a free normal mode can also be used to determine the ring's surface density. Although these results will not be as definitive as the value of σ_0 that was inferred from the ring's forced pattern, due to a greater sensitivity to the observational uncertainties, the following illustrates an alternate technique that in principle can be used to infer the surface density of other rings, such as the many narrow ringlets orbiting Saturn that also exhibit free normal modes.

However, first note the models' large discrepancy with the observed free $m = 2$ pattern speed reported in SP10, which is the upper horizontal bar in Figure 6. This discrepancy is *not* due to the $\delta a_{\rm edge} = \pm 4$ km uncertainty in the ring-edge's semimajor axis, which makes the simulated ring particles' mean angular velocity uncertain by the fraction $\delta\Omega/\Omega = 1.5 \delta a_{\rm edge}/a_{\rm edge} \simeq 0.005\%$. We find empirically that the simulations' pattern speeds
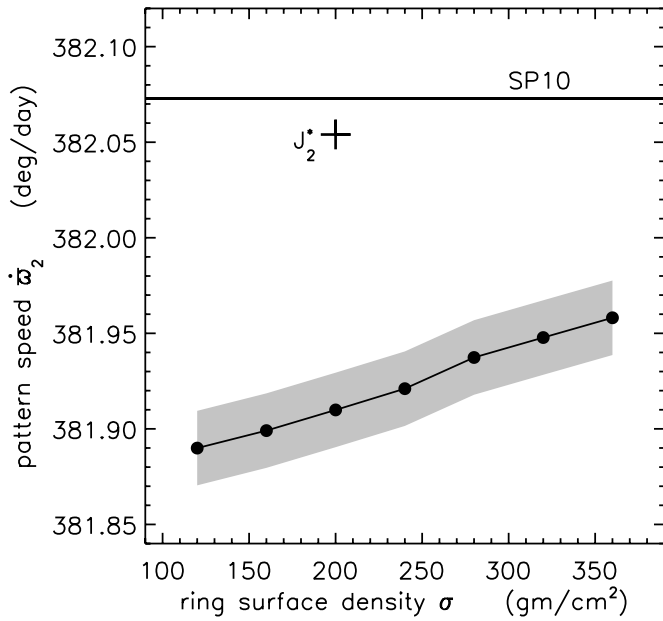
Figure 6. Curve with black dots is the pattern speed $\dot{\tilde{\omega}}_2$ for the simulated B ring's free $m = 2$ pattern. The vertical extent of the gray band indicates how these simulated results would change if the ring-edge's semimajor axis was altered by its observed uncertainty $\delta a_{edge} = \pm 4$ km. The horizontal line is the B ring's observed free $m = 2$ pattern speed $\dot{\tilde{\omega}}_2 = 382.0731 \pm 0.0007$ deg day^{-1}, from SP10, with its small uncertainty indicated by the line's thickness. The cross shows how the free pattern speed in the $\sigma_0 = 200$ g cm^{-2} simulation changes when J_2 is boosted by factor $f^\star = 1.0395013$ to $J_2^\star$.

Figure 7. Dots indicate the simulations' free $m = 2$ pattern speed relative to the force pattern speed, $\Delta \dot{\tilde{\omega}}_2 = \dot{\tilde{\omega}}_2 - \Omega_{sat}$, with the light gray indicating the uncertainty due to the $\delta a_{edge} = \pm 4$ km uncertainty in the ring-edge's semimajor axis. The dark gray indicates what would result if δa_{edge} were instead ± 1 km. The horizontal line is the B ring's observed $m = 2$ relative pattern speed from SP10, with the small uncertainty indicated by the line's thickness. The cross indicates that the free pattern's relative speed in the $\sigma_0 = 200$ g cm^{-2} simulation is unchanged when J_2 is boosted by factor $f^\star = 1.0395013$ to $J_2^\star$, and the white dot indicates the relative pattern speed when J_2 is instead set to zero. All simulations have Mimas's orbit configured so that its forced $m = 2$ inner Lindblad resonance lies 12.2 km interior to the semimajor axis of the B ring's outer edge.

are also uncertain by this fraction, so $\delta \dot{\tilde{\omega}}_2 \simeq 0.02$ deg day^{-1}, which is the vertical extent of the gray band around the simulated data in Figure 6.

Rather, this discrepancy is indirectly due to the absence of the J_4 and higher terms from the N-body simulations. To demonstrate this, repeat the $\sigma_0 = 200$ g cm^{-2} simulation with J_2 boosted slightly by factor $f^\star = 1.0395013$ so that the second zonal harmonic is $J_2^\star = f^\star J_2 = 0.016934294$. This increases the simulated B ring-edge's angular velocity slightly to $\Omega_{edge} = 758.8824$ deg day^{-1}, which is in fact the ring's true angular velocity at $a = a_{edge}$ when the higher order J_4 and J_6 terms are also accounted for.[5] And since Saturn's gravitational force there is $a_{edge}\Omega_{edge}^2$, this means that Saturn's gravity on the simulated particles at $r = a_{edge}$ is in fact the true value. Note that boosting J_2 to the slightly larger value $J_2^\star$ also requires bringing the simulated Mimas inward and just interior to its true semimajor axis by 2 km. Which speeds up both the forced and free pattern speeds, and is why this simulation's free $m = 2$ pattern speed $\dot{\tilde{\omega}}_2$, which is the cross in Figure 6, is in better agreement with the observed pattern speed. So the discrepancy between all the other simulated and observed pattern speeds $\dot{\tilde{\omega}}_2$ is due to those models' not accounting for the additional gravity that is due to the J_4 and higher terms in Saturn's oblate figure. Compensating for the absence of those oblateness effects requires altering the simulated satellite's orbits slightly, which in turn alters the forced and free pattern speeds slightly, but the following will show that these two patterns' *relative* speeds are
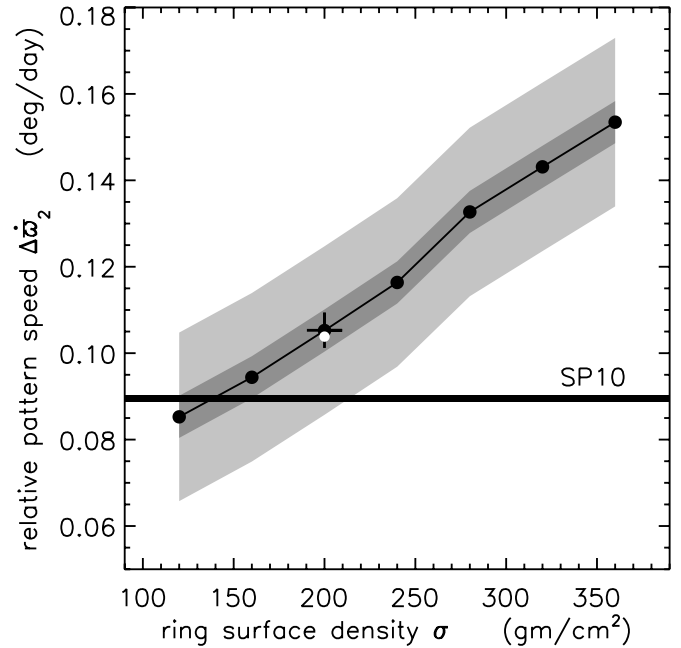
---

[5] This mean angular velocity is obtained using the physical constants given in the 2011 August 25 *Cassini* SPICE kernel file: $Gm_0 = 37940585.47323534$ km^3 s^{-2}, $J_2 = 0.016290787119$, $J_4 = -0.000934741301$, and $J_6 = 0.000089240275$.

quite insensitive to the particular value of J_2 and the absence of the J_4 and higher terms.

The best way to compare simulated to observed free $m = 2$ patterns is to consider the free $m = 2$ pattern speed relative to the forced pattern speed, which is the satellite's mean angular velocity Ω_{sat}. That frequency difference is $\Delta \dot{\tilde{\omega}}_2 = \dot{\tilde{\omega}}_2 - \Omega_{sat}$, and is plotted versus ring surface density σ_0 in Figure 7. Black dots are from the simulation and the light gray band indicates the $\delta \dot{\tilde{\omega}}_2 \simeq 0.02$ deg day^{-1} spread that results from the $\delta a_{edge} = \pm 4$ km uncertainty in the ring-edge's semimajor axis. The relatively large uncertainty in a_{edge} means that one can only conclude from Figure 7 that $\sigma_0 \lesssim 210$ g cm^{-2}. If, however, the uncertainty in a_{edge} were instead $\delta a_{edge} = \pm 1$ km, then the uncertainty in $\Delta \dot{\tilde{\omega}}_2$ would be four times smaller (darker gray band), which would have allowed us to determine the ring surface density with a much smaller uncertainty of only ± 20 g cm^{-2}. The lesson here is that if one wishes to use models of free patterns to infer σ_0 in, say, narrow ringlets, then one will likely need to know the ring-edge's semimajor axis with a precision of $\delta a_{edge} \simeq \pm 1$ km.

The cross in Figure 7 indicates that the free $m = 2$ pattern speed relative to the forced is unchanged when Saturn's oblateness is boosted to $J_2^\star$. Also, to demonstrate that this kind of plot is rather insensitive to oblateness effects, the white dot in Figure 7 shows that these relative pattern speeds change only very slightly even when J_2 is set to zero.

Note though that there will be instances where there is no forced mode with which to compare pattern speeds. In that case
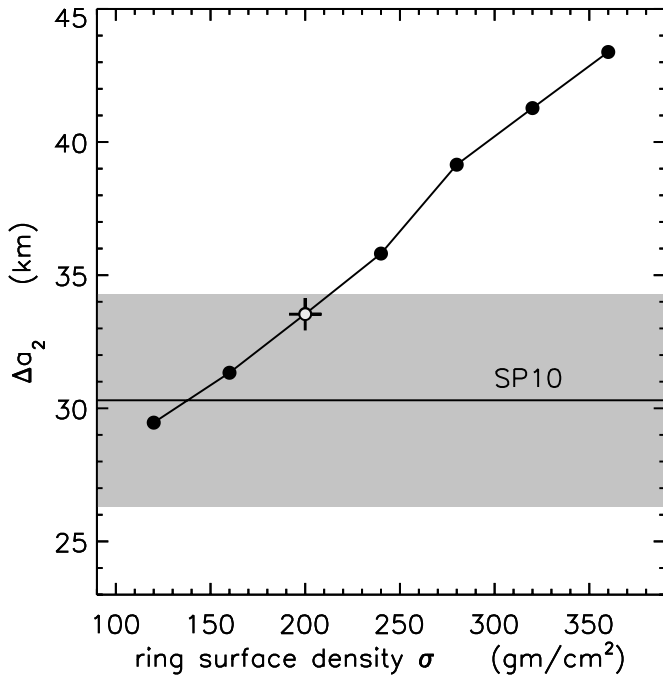
Figure 8. Equation (31) is solved for the radius $\tilde{a}_2$ of the inner Lindblad resonance that is associated with each of the simulated free $m = 2$ modes whose pattern speeds $\Omega_{ps} = \dot{\tilde{\omega}}_m$ are shown in Figure 6, with this figure showing the relative distance $\Delta a_2 = a_{\rm edge} - \tilde{a}_2$ of the ILR from the semimajor axis of the simulated B ring's outer edge. The observed value is $\Delta a_2 = 30.3 \pm 4$ km (SP10) whose uncertainty is indicated by gray band. The cross and the white dot indicate that the results are unchanged when the oblateness parameter takes values $J_2^\star$ and zero.

it will be convenient to convert the free pattern speed $\dot{\tilde{\omega}}_m = \Omega_{ps}$ into a radius by solving the Lindblad resonance criterion,

$$\kappa(r) = \epsilon m[\Omega(r) - \Omega_{ps}], \tag{31}$$

for the resonance radius $r = a_m$, where $\kappa(r)$ is the ring particles' epicyclic frequency (Equation (12b)), and $\epsilon = +1(-1)$ at an inner (outer) Lindblad resonance. So for the simulated B ring's free $m = 2$ mode, Equation (31) is solved for the radius $r = \tilde{a}_2$ of the $\epsilon = +1$ ILR that is associated with this mode. That quantity is to be compared to a nearby reference distance, which in this case would be the semimajor axis of the B ring's outer edge $a_{\rm edge}$. Results are shown in Figure 8, which shows the simulations' distance from the B ring's outer edge to the free $m = 2$ pattern's ILR, $\Delta a_2 = a_{\rm edge} - \tilde{a}_2$, plotted versus ring surface density σ_0. Heavier rings have a faster pattern speeds (Figures 6 and 7), and so the pattern's resonance resides at a higher orbital frequency $\Omega(r)$ and thus must lie further inward of the ring's outer edge in order to satisfy the resonance condition, Equation (31). Figure 8 has the same information content as Figure 7, which is why it also tells us that the B ring's outer edge has $\sigma_0 \lesssim 210$ g cm^{-2}. However, a plot like Figure 8 will also provide the best way to interpret the B ring's free $m = 3$ mode, which is examined below in Section 3.2.

Last, note that the free $m = 2$ patterns seen in these simulations persist for 3×10^4 orbits or 40 yr without any sign of damping, despite the ring's viscosity $\nu = 100$ cm^2 s^{-1}. This is illustrated in Figure 9, which plots the ring-edge's epicyclic amplitude over time for the nominal $\sigma_0 = 200$ g cm^{-2} simulation. Indeed we have also rerun this simulation using a viscosity that is 10 times larger and still saw no damping. These experiments reveal a possibly surprising result, that a
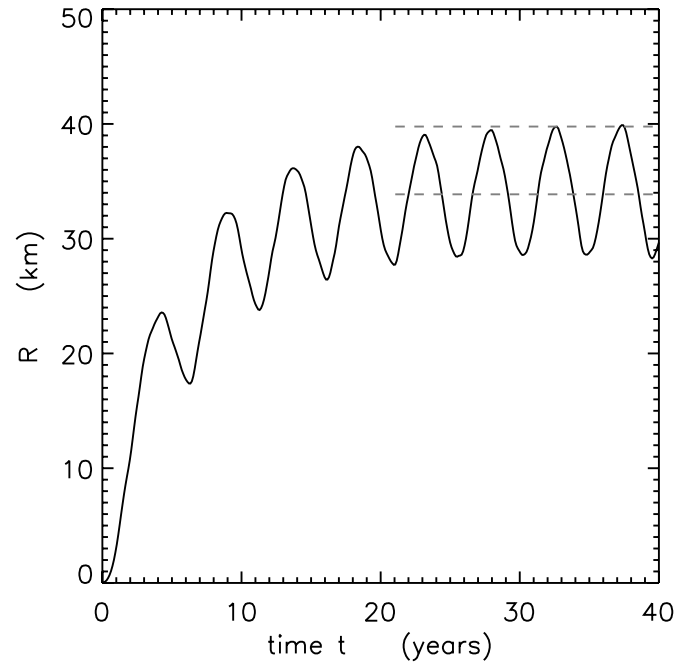

Figure 9. Epicyclic amplitude $R = |r - a|$ of the simulated B ring's outer edge over time t, from the $\sigma_0 = 200$ g cm^{-2} simulation shown in Figures 5–8, with Mimas's mass grown exponentially over a $\tau_s = 6.2$ yr timescale. The lower dashed line is the amplitude of the ring's forced response R_2 due to Mimas's resonant perturbation, and the upper dashed line is the sum of the amplitudes of the ring's forced + free response $R_2 + \tilde{R}_2$, obtained by fitting Equation (30) to the curve at times $t > 20$ yr.

free pattern can persist at a ring-edge for a considerable length of time, likely hundreds of years or longer, and Section 4.1 will show that this longevity is due to the viscous forces being several orders or magnitude weaker than the ring's other interval forces. Therefore, one possible interpretation of the free modes seen at the B ring and at other ring edges is that they are relics from past disturbances in Saturn's ring that may have happened hundreds or more years ago. This possibility is discussed further in Section 4.3.

3.2. The Free $m = 3$ Pattern

The B ring's free $m = 3$ mode has an epicyclic amplitude of $\tilde{R}_3 = 11.8 \pm 0.2$ km, a pattern speed $\dot{\tilde{\omega}}_3 = 507.700 \pm 0.001$ deg day^{-1}, and the ILR associated with this pattern speed lies $\Delta a_3 = 24 \pm 4$ km interior to the B ring's outer edge (SP10).

To excite a free $m = 3$ pattern at the ring-edge, place a fictitious satellite in an orbit that has an $m = 3$ ILR $\Delta a_3 = 24$ km interior to the ring's outer edge. Noting that the satellite Janus happens to have an $m = 3$ resonance in the vicinity, about 2000 km inward of the B ring's edge, these simulations use a Janus-mass satellite to perturb the simulated ring for about 1650 orbits (about 2 yr), which excites an $m = 3$ pattern at the ring's outer edge. The satellite is then removed from the system, which converts the pattern into a free normal mode, and epi_int is then used to evolve the now unperturbed ring for another 1.8×10^4 orbits (about 23 yr). Figure 10 plots the ring-edge's epicyclic amplitude, where it is shown that the free mode persists at the B ring's outer edge, undamped over time, despite the simulated ring's viscosity of $\nu = 100$ cm^2 s^{-1}.

A suite of such B ring simulations is performed, with ring surface densities 120 g cm$^{-2} \leqslant \sigma_0 \leqslant 360$ g cm^{-2} and all other parameters identical to the nominal model of Section 3.1 except
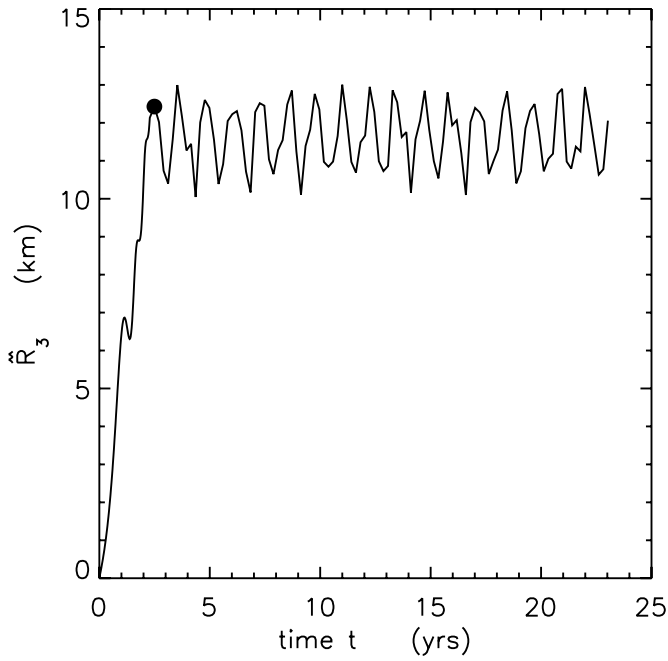
Figure 10. Epicyclic amplitude $\tilde{R}_3$ vs. time t for a simulated B ring having surface density $\sigma_0 = 200$ g cm^{-2} that is perturbed until time $t = 2.3$ yr (black dot) by a satellite whose $m = 3$ inner Lindblad resonance lies $\Delta a_{\rm res} = 24$ km interior to the ring's outer edge. The satellite's mass is Janus's, and the dot indicates the time when that satellite is removed from the system, which converts this $m = 3$ pattern into an unforced normal mode.

Figure 11. Distance $\Delta a_3 = a_{\rm edge} - \tilde{a}_3$ between the ring's outer edge and the inner Lindblad resonance associated with the free normal modes in the B ring simulations described in Section 3.2, plotted vs. ring surface density σ_0. The horizontal line is the observed distance with its uncertainty indicated by the gray band, from SP10. These simulations use $N_r = 100$ streamlines with $N_\theta = 60$ particles on each streamline, so the total number of particles is $N_r N_\theta = 6000$. The streamlines' radial separation is $\Delta a = 2.03$ km, and the total radial width of the simulated ring is $w = (N_r - 1)\Delta a = 203$ km.

where noted in Figure 11 caption. The pattern speed $\Omega_{ps} = \dot{\tilde{\omega}}_3$ of the $m = 3$ normal mode is then extracted from each simulation, with those speeds again being slightly faster in the heavier rings. Those pattern speeds are then inserted into Equation (31), which is solved for the radius of the ILR $\tilde{a}_3$, each of which lies a distance $\Delta a_3 = a_{\rm edge} - \tilde{a}_3$ inward of the ring's outer edge, and those distances are plotted in Figure 11 versus ring surface density σ_0. The simulated distances Δa_3 are compared to the observed edge-resonance distance reported in SP10, which indicates a ring surface density 160 g cm$^{-2} \leqslant \sigma_0 \leqslant 310$ g cm^{-2}. This finding is consistent with the results from the $m = 2$ patterns, but this constraint on σ_0 is again rather loose due to the $\delta a_{\rm edge} = \pm 4$ km uncertainty in the ring-edge's semimajor axis. However, our purpose here is to show how one might use models of free normal modes to infer the surface density of other rings and narrow ringlets, which again will likely require knowing the ring-edge's semimajor axis to ± 1 km or better.

Also note that the radial depth of this $m = 3$ disturbance is $\Delta a_{e/10} = 50$ km, about three times smaller than the radial depth of the $m = 2$ disturbance.

3.3. The Free m = 1 Pattern

The B ring's free $m = 1$ mode has an epicyclic amplitude of $\tilde{R}_1 = 20.9 \pm 0.4$ km and a pattern speed $\dot{\tilde{\omega}}_1 = 5.098 \pm 0.003$ deg day^{-1} that is slightly faster than the local precession rate, and the ILR that is associated with this pattern speed lies $\Delta a_1 = 253 \pm 4$ km interior to the B ring's outer edge (SP10). Several simulations of the B ring's $m = 1$ pattern are evolved for model rings having surface densities of 120 g cm$^{-2} \leqslant \sigma_0 \leqslant$ 360 g cm^{-2}. To excite the $m = 1$ pattern at the simulated ring's edge, again arrange a fictitious satellite's orbit so that its $m = 1$ ILR lies $\Delta a_1 = 253$ km interior to the B ring's edge, which is the site where the resonance condition (Equation (31)) is
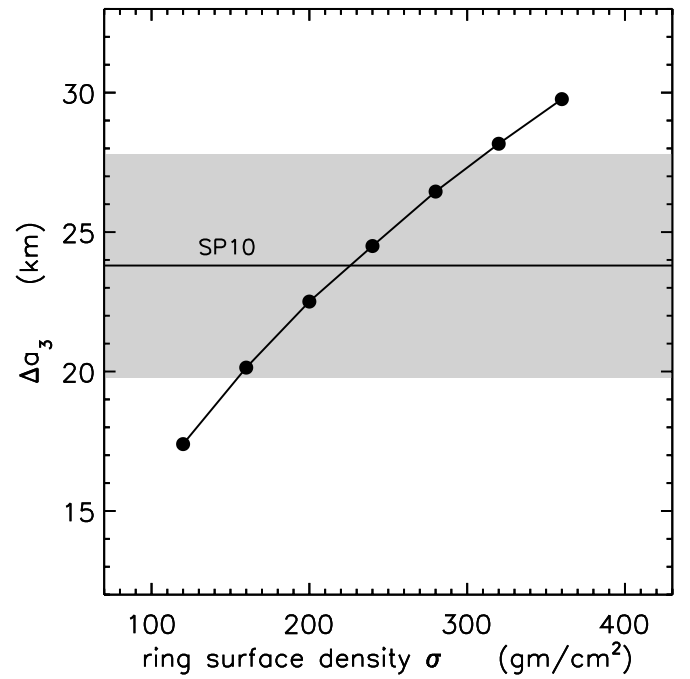
satisfied when the satellite's mean angular velocity matches the ring particles' precession rate, $\Omega_s = \dot{\tilde{\omega}} = \Omega_{ps}$. The simulated ring is perturbed by a satellite whose mass is about 20% that of Mimas, for 1.6×10^4 orbits or 21 yr, which excites a forced $m = 1$ pattern at the ring's edge that corotates with the satellite. The satellite is then removed, which converts the forced $m = 1$ pattern into a free pattern, and the ring is evolved for another 6.4×10^4 orbits or 83 yr. For each simulation the free pattern speed is measured, and Equation (31) is then used to convert the free pattern speed into a resonance radius $\tilde{a}_1$, which is displayed in Figure 12 that shows that resonance's distance from the ring's outer edge, $\Delta a_1 = a_{\rm edge} - \tilde{a}_1$. As the figure shows, the free $m = 1$ pattern rotates slightly faster in the heavier ring and thus the associated $m = 1$ ILR must lie further inward in order to satisfy the resonance condition $\Omega_{ps} = \dot{\tilde{\omega}} = (3/2)J_2(R_p/a)^2\Omega$. Again there is no damping of the free $m = 1$ pattern, which stays localized at the ring's outer edge over the simulation's 83 yr time span, despite the simulated ring's viscosity $\nu = 100$ cm^2 s^{-1}.

The radial depth of this $m = 1$ disturbance is much greater than the others, $\Delta a_{e/10} = 614$ km, which is about four times larger than the $m = 2$ disturbance. Comparing Figure 12 to Figures 8 and 11 also shows that the Lindblad resonance associated with the $m = 1$ disturbance lies about 10 times further from the ring-edge than the $m = 1$ and $m = 2$ resonances. Which is why the $m = 1$ simulation uses streamlines whose width Δa is $\sim 10\times$ larger, since a wider portion of the B ring-edge must be simulated in order to capture this disturbance's deeper reach into the B ring.

Note also that the ± 4 km uncertainty in this resonance's position relative to the B ring edge, which is entirely due to the uncertainty in the B ring-edge's semimajor axis, is in this case
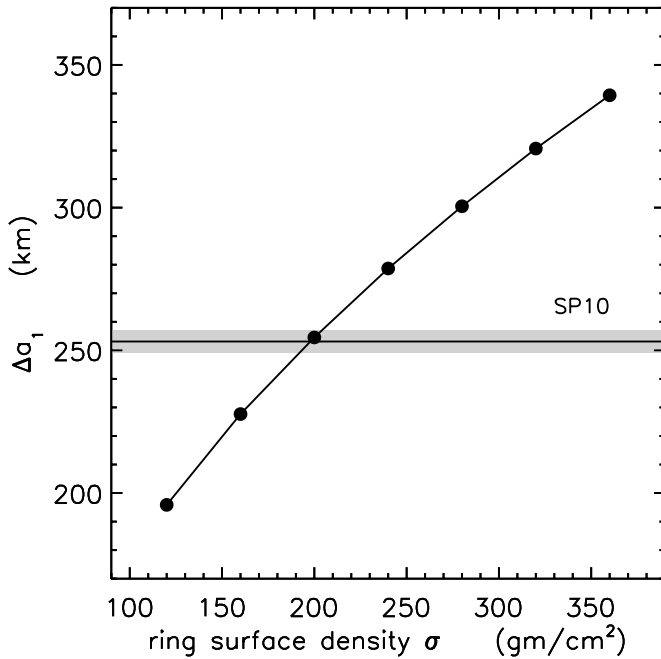
Figure 12. Distance $\Delta a_1 = a_{\text{edge}} - \tilde{a}_1$ between the ring's outer edge and the inner Lindblad resonance associated with the free normal models in the B ring simulations described in Section 3.3, plotted vs. ring surface density σ_0. The horizontal line is the observed distance with its uncertainty indicated by the gray band, from SP10. These simulations use $N_r = 100$ streamlines with $N_\theta = 30$ particles per streamline and $N_r N_\theta = 3000$ particles total. The streamlines' radial separation is $\Delta a = 24.6$ km, and the total radial width of the simulated ring is $w = (N_r - 1)\Delta a = 2435$ km.

relatively small, which is why the ring's free $m = 1$ mode can also be used to probe its surface density with some precision (unlike the free $m = 2$ and $m = 3$ modes), and is consistent with a B ring surface density of $\sigma_0 \simeq 200$ g cm^{-2}.

3.4. Convergence Tests

A number of simulations have also been performed, which repeat the ring simulations using various particle numbers N_r and N_θ and various widths w of the simulated ring. We find that the results reported here do not change significantly when the simulated ring is populated densely with enough particles, and when the radial width of the simulated B ring is sufficiently wide. Those convergence tests reveal that the number of particles along each streamline must satisfy $N_\theta \geqslant 20m$, that the radial width of each streamline should satisfy $\Delta a \leqslant 0.04\Delta a_{e/10}$, and that the total width of the simulated ring should satisfy $w > 4\Delta a_{e/10}$. All of the simulations reported here satisfy these requirements.

4. DISCUSSION

This section re-examines the model's treatment of viscous effects at the ring's edge and also describes related topics that will be considered in follow-up work.

4.1. The Ring's Internal forces

Figure 13 plots the accelerations that the ring's internal forces—gravity, pressure, and viscosity—exert on each ring particle. These accelerations are from the nominal $\sigma_0 = 200$ g cm^{-2} simulation that is described in Figures 5–9, and these accelerations are plotted versus each particle's distance from the ring's edge, so those forces obviously get larger closer to the ring's disturbed outer edge. But the main point of Figure 13 is that the
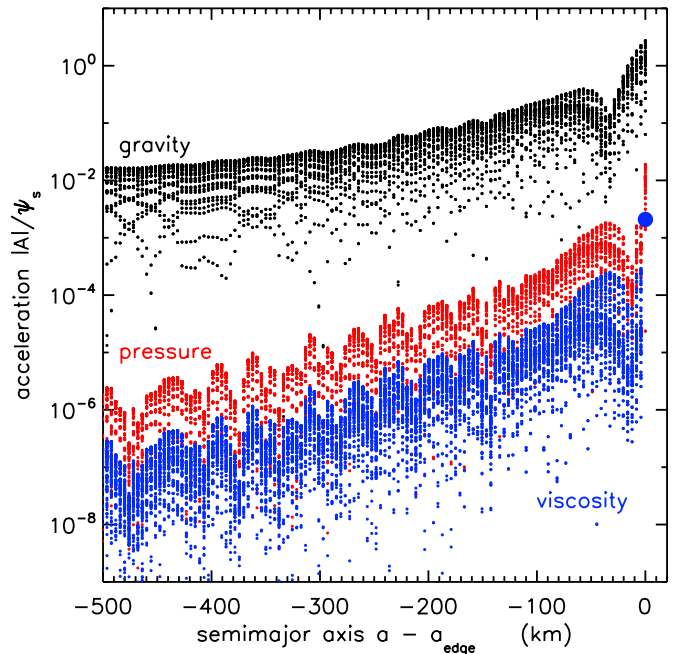

Figure 13. Magnitude of the acceleration $|A|$ due to ring self-gravity (black dots), pressure (red), and viscosity (blue) are plotted for every particle in the B ring simulation having $\sigma_0 = 200$ g cm^{-2} that is described in Figures 5–9. The ring's internal forces are excited by the satellite's periodic forcing, which is conveniently measured by the satellite's forcing function Ψ_s (see Equation (19) of Hahn et al. 2009), and these accelerations are displayed in units of Ψ_s. This figure also subtracts from the radial component of A its azimuthally averaged value since that quantity merely changes the orbital frequencies Ω and κ slightly without altering the ring's dynamics. Shown are these accelerations at time $t = 30.9$ yr when the simulated ring has settled into quasi equilibrium (see Figure 9). The accelerations are plotted vs. each streamline's semimajor axis distance from the ring's outer edge, $a - a_{\text{edge}}$, and these accelerations are periodic in longitude θ, which is why they span a range of values within each streamline. This simulation also has the viscous acceleration zeroed at the ring's outer edge, and the large blue dot on the right indicates the viscous acceleration that those particles at the ring's edge would otherwise have experienced; see Section 4.1 for details.

ring's self-gravity is the dominant internal force in the ring, exceeding the pressure force by a factor of ~100 at the ring's outer edge and by a larger factor elsewhere. Those pressure forces are also ~10 times larger than the ring's viscous forces. But recall that those simulations had zeroed the viscous acceleration that the ring exerts on its outermost streamline (Section 3), when that acceleration should instead be $A_{\nu,\theta} = F/\lambda r$ as indicated by the large blue dot at the right edge of Figure 13. Note though that the neglected viscous acceleration of the ring's edge is still ~1000 times smaller than that due to ring gravity and ~10 times smaller than that due to ring pressure. So this justifies neglecting, at least for the short-term $t \sim 100$ yr simulations considered here, the much smaller viscous forces at the ring's outer edge.

Nonetheless, this study's neglect of the small viscous force at the ring's outer edge implies that this model does not yet account for the B ring's radial confinement by Mimas's $m = 2$ ILR. So there appears to be some missing physics that will be necessary if one is interested in the ring's resonant confinement or the ring's long-term evolution over $t \gg 100$ yr timescales. The suspected missing physics is described below.

4.1.1. Unmodeled Effects: The Viscous Heating of a Resonantly Confined Ring-edge

The model's inability to confine the B ring's outer edge at Mimas's $m = 2$ ILR may be a consequence of the ring's

kinematic viscosity ν being treated here as a constant parameter everywhere in the simulated ring. Although treating ν as a constant is a simple and plausible way to model the effects of the ring's viscous friction, it might not be adequate or accurate if one wishes to simulate the resonant confinement of a planetary ring. This is because the ring's viscosity transports both energy and angular momentum radially outward through the ring. So if the ring's outer edge is to be confined by a satellite's mth Lindblad resonance, the satellite must absorb the ring's outward angular momentum flux, which it can do by exerting a negative gravitational torque at the ring's edge. But Borderies et al. (1982) show via a simple Jacobi-integral argument that resonant interactions only allow the satellite to absorb but a fraction of the energy that viscosity delivers to the ring-edge. Consequently the ring's viscous friction still delivers some orbital energy to the ring-edge where it accumulates and heats up the ring particles' random velocities c. Also, if collisions among particles are the main source of the ring's viscosity, then $\nu_s \simeq c^2\tau/2\Omega(1 + \tau^2)$ where $\tau \propto \sigma$ is the ring's optical depth (Goldreich & Tremaine 1982). In this case viscous heating would increase c as well as ν_s at the ring's edge. The enhanced dissipation there should also increase the angular lag ϕ between the ring-edge's forced pattern and the satellite's longitude (see Equation (83b) of Hahn et al. 2009). This will also be important because the gravitational torque that the satellite exerts on the ring-edge varies as $\sin\phi$ (Hahn et al. 2009), and that torque needs to be boosted if the satellite is to confine the spreading ring.

To model this phenomenon properly, the `epi_int` code also needs to employ an energy equation, one that accounts for how viscous heating tends to increase the ring particles' dispersion velocity c and viscosity ν_s nearer the ring's edge. The increased dissipation and the resulting orbital lag will allow the satellite to exert a greater torque on the ring which, we suspect, will enable the satellite to resonantly confine the simulated ring's outer edge. The derivation of this energy equation and its implementation in `epi_int` are ongoing, and those results will be reported on in a follow-up study.

4.2. An Alternate Equation of State

The EOS adopted here is appropriate for a dilute gas of colliding ring particles whose mutual separations greatly exceed their sizes. This should be regarded as a limiting case since ring particles can of course be packed close to each other in the ring. But Borderies et al. (1985) consider the other extreme limiting case, with close-packed particles that reside shoulder to shoulder in the ring. In that case the ring is expected to behave as an incompressible fluid whose volume density $\rho = \sigma/2h$ stays constant. So when some perturbation causes ring streamlines to bunch up and increases the ring's surface density σ, the ring's vertical scale height h also increases as ring particles are forced to accumulate along the vertical direction. This in turn increases the ring's pressure due to the larger gravitational force along the vertical direction.

Borderies et al. (1985) show that infinitesimal density waves in an incompressible disk are unstable and grow in amplitude over time. This phenomenon is related to the viscous overstability, and Longaretti & Rappaport (1995) show that it can distort a narrow eccentric ringlet's streamlines in a way that accounts for its $m = 1$ shapes. Borderies et al. (1985) also suggest that unstable density waves can be trapped between a Lindblad resonance and the B ring's outer edge, which might explain the normal modes seen there, and Spitale & Porco (2010) use this concept to estimate the ring's surface density there.

However, keep in mind that this instability only occurs when the ring particles are densely packed to the point of being incompressible, which requires the ring to be very thin and dynamically cold. We have shown here that the amplitude of the B ring's forced motions indicates that the ring-edge has a surface density $\sigma \simeq 200\,\mathrm{g\,cm}^{-2}$. So if this ring is incompressible and composed of icy spheres having a mean volume density of $\rho = \sigma/2h \simeq 0.5\,\mathrm{g\,cm}^{-3}$, this then requires a B ring thickness of only $h \sim 2$ m, which is rather thin compared to other estimates (Cuzzi et al. 2010). Similarly the ring particles' dispersion velocity c must be small compared to that expected for a dilute particle gas, so $c \ll (h\Omega \sim 0.3\,\mathrm{mm\,s}^{-1})$, which again is cold compared to all other estimates for Saturn's rings (Cuzzi et al. 2010). The upshot is that an incompressible EOS requires the ring to be very thin and dynamically cold, likely much colder and thinner than is generally thought. Consequently we are optimistic that the compressible EOS used here, $p = \sigma c^2$, is the appropriate choice for simulations of the outer edge of Saturn's B ring. Nonetheless in a follow-up investigation we do intend to encode the incompressible EOS into `epi_int`, to see if the BGT instability can account for the higher $m \geqslant 2$ free modes that are seen at the outer edge of the B ring and in many other narrow ringlets.

4.3. Impulse Origin for Normal Modes

The simulations of Section 3 used a fictitious temporary satellite to excite the free modes that occur at many Saturnian ring edges. These simulations used an admittedly ad hoc method—the sudden appearance and disappearance of a satellite—to excite these modes. Nonetheless, these models demonstrate that transient and impulsive events can excite normal modes at ring edges, and those simulations show that normal modes can persist at the ring's edge for hundreds of years after the disturbance has occurred. This suggests that an impulsive event in the recent past, perhaps an impact into Saturn's rings, might be responsible for exciting the normal modes that are seen at the outer edge of the B ring, as well as the normal modes that are also seen along the edges of several narrower ringlets (French et al. 2010; Hedman et al. 2010; French et al. 2011; Nicholson et al. 2012)

The possibility that normal modes are due to an impact is motivated by the discovery of vertical corrugations in Saturn's C and D rings (Hedman et al. 2007, 2011) and in Jupiter's main dust ring (Showalter et al. 2011). These vertical structures are spirals that span a large swath of each ring, and they are observed to wind up over time due to the central planet's oblateness. Evolving the vertical corrugations backward in time also unwinds their spiral pattern until some moment when the affected region is a single tilted plane. Unwinding the Jovian corrugation shows that this disturbance occurred very close to the date when the tidally disrupted comet Shoemaker-Levy 9 impacted Jupiter in 1994, which suggests an impact from a tidally disrupted comet as the origin of these ring-tilts (Showalter et al. 2011). However, a single sub-kilometer comet fragment cannot tilt a large $\sim 2 \times 10^5$ km wide planetary ring. But a disrupted comet can produce an extended cloud of dust, and if that disrupted dust cloud returns to the planet with enough mass and momentum, then it might tilt a ring that at a later date would be observed as a spiral corrugation.

However, the tidal disruption of comet about a low-density planet like Saturn is more problematic, because tidal disruption only occurs when the comet's orbit is truly close to parabolic and not too hyperbolic, and with periapse just above the planet's atmosphere (Sridhar & Tremaine 1992; Richardson et al. 1998).

However, it is easy to envision an alternate scenario that might be more likely, with a small kilometer-sized comet originally in a heliocentric orbit coming close enough to Saturn to instead strike the main A or B rings. This scenario is more probable because the cross-section available to orbits impacting the main rings is significantly larger than those resulting in tidal disruption. The impacting comet's considerably greater momentum will nonetheless carry the impactor through the dense A or B rings, but the collision itself is likely energetic enough to shatter the comet. And if that collision is sufficiently dissipative, then the resulting cometary debris will then stay bound to Saturn, and in an orbit that will return that debris back into the ring system on its next orbit. Small differences among the orbits of individual debris particles means that, when the debris encounters the rings again, that impacting debris will be spread across a much larger footprint on the ring, which presumably will allow any dense rings or ringlets to absorb the debris' mass and momentum in a way that effectively gives the ring particles there a sudden velocity kick $\Delta \mathbf{v}$ in proportion to the comet debris density ρ and velocity $\mathbf{v}_r$ relative to the ring matter. But if comet Shoemake-Levy 9's (SL9) impact with Jupiter is any guide, then impact by a cloud of comet debris could last as long as a week of time, which might tend to smear this effect out due to the ring's orbital motion. But that effect would be offset if the debris train's dust cloud is also rather clumpy, like the SL9 debris train was. Indeed, it is possible that this scenario might also account for the spiral corrugations of Saturn's C and D ring. It is also conceivable that an inclined cloud of impacting comet debris might also excite the vertical analog of normal modes—long-lived vertical oscillations of a ring's edge. This admittedly speculative scenario will be pursued in a follow-up study, to determine whether debris from an impact-disrupted comet can excite the normal modes seen at ring edges, and to determine the mass of the progenitor comet that would be needed to account for these modes' observed amplitudes.

5. SUMMARY OF RESULTS

We have developed a new *N*-body integrator that calculates the global evolution of a self-gravitating planetary ring as it orbits an oblate planet. The code is called `epi_int`, and it uses the same kick-drift-step algorithm as is used in other symplectic integrators such as SYMBA and MERCURY. However, the velocity kicks that are due to ring gravity are computed via an alternate method that assumes that all particles inhabit a discreet number of streamlines in the ring. The use of streamlines to calculate ring self-gravity has been used in analytic studies of rings (Goldreich & Tremaine 1979; Borderies et al. 1983a, 1986), and the streamline concept is easily implemented in an *N*-body code. A streamline is the closed path through the ring that is traced by particles having a common semimajor axis. All streamlines are radially close to each other, so the gravitation acceleration due to a streamline is simply that due to a long wire, $A = 2G\lambda/\Delta$ where λ is the streamline's linear density and Δ is the particle's distance from the streamline. This is very useful since particles are responding to the pull of smooth wires rather than discreet clumps of ring matter, so there is no gravitational scattering, which means that only a modest number of particles are needed, typically a few thousand, to simulate all $360°$ of a scalloped ring like the outer edges of Saturn's A and B ring. Only a few thousand particles are also needed to simulate linear as well as nonlinear spiral density waves, and execution times are just a few hours on a desktop PC.

Another distinction occurs during the particles' unperturbed drift step when particles follow the epicyclic orbit of Longaretti & Rappaport (1995) about an oblate planet, rather than the usual Keplerian orbit about a spherical planet. This effectively moves the perturbation due to the planet's oblate figure out of the integrator's kick step and into the drift step. The code also employs hydrodynamic pressure and viscosity to account for the transport of linear and angular momentum through the ring that arises from collisions among ring particles. Another convenience of the streamline formulation is that it easily accounts for the large pressure drop that occurs at a ring's sharp edge, as well as the large viscous torque that the ring exerts there. The model also accounts for the mutual gravitational perturbations that the ring and the satellites exert on each other. The `epi_int` code is written in IDL, and the source code is available for download at http://gemelli.spacescience.org/~hahnjm/software.html.

This integrator is used to simulate the forced response that the satellite Mimas excites at its $m = 2$ ILR that lies near the outer edge of Saturn's B ring. That resonance lies $\Delta a_2 = 12 \pm 4$ km inward of the ring's edge, and simulations show that the ring's forced epicyclic amplitude varies with the ring's surface density σ_0 as $R_2 \propto \sigma_0^{0.67}$. Good agreement with *Cassini* measurements of R_2 occurs when the simulated ring has a surface density of $\sigma_0 = 195 \pm 60$ g cm^{-2} (see Figure 5), where the uncertainty in σ_0 is dominated by the $\delta a_{\rm edge} = 4$ km uncertainty that Spitale & Porco (2010) find in the ring-edge's semimajor axis. This σ_0 is the mean surface density over that part of the B ring that is disturbed by this resonance, whose influence in the ring extends to a radial distance of $\Delta a_{e/10} \sim 150$ km from the B ring's outer edge. And if we naively assume that this surface density is the same everywhere across Saturn's B ring, then its total mass is about 90% of Mimas's mass.

Cassini observations reveal that the outer edge of Saturn's B ring also has several free normal modes that are not excited by any known satellite resonances. Although the mechanism that excites these free modes is uncertain, we are nonetheless able to excite free modes in a simulated ring via various ad hoc methods. For instance, a fictitious satellite's *m*th Lindblad resonance is used to excite a forced pattern at the ring edge. Removing that satellite then converts the forced pattern into a free normal mode that persists in these simulations for up to ~ 100 yr or $\sim 10^5$ orbits without any damping, despite the simulated ring having a kinematic viscosity of $\nu = 100$ cm^2 s^{-1}; see Figure 10 for one example.

Alternatively, starting the ring particles in circular orbits while subject to Mimas's $m = 2$ gravitational perturbation excites both a forced and a free $m = 2$ pattern that initially null each other precisely at the start of the simulation. But the forced pattern corotates with Mimas's longitude while the free pattern rotates slightly faster in a heavier ring, which suggests that a free mode's pattern speed can also be used to infer a ring's surface density σ_0. However, the free pattern speed is also influenced by the J_4 and higher terms in the oblate planet's gravity field, which are absent from this model which only accounts for the J_2 component. So the simulated pattern speed cannot be compared directly to the observed pattern speed; see Figure 6. To avoid this difficulty, the resonance condition (Equation (31)) is used to calculate the radius of the Lindblad resonance that is associated with the free normal mode. Plotting the distances of the simulated and observed resonances from the B ring's edge (Figures 8, 11, and 12) then provides a convenient way to compare simulations to observations of free modes in a way that is insensitive to the planet's oblateness.

Simulations of the B ring's free $m = 2$ and $m = 3$ patterns are consistent with *Cassini* measurements of the B ring's normal modes when the simulated ring-edge again has a surface density of $\sigma_0 \sim 200$ g cm^{-2}, which is a nice consistency check. But these particular measurements do not provide a tight constraint on the ring's σ_0 due to the fact that the $m = 2$ and $m = 3$ Lindblad resonances only lie $\Delta a_m \sim 25$ km from the outer edge of a ring whose semimajor axis a is uncertain by $\delta a_{\text{edge}} = 4$ km. However, the B ring's free $m = 1$ normal mode does lie much deeper in the ring's interior, $\Delta a_1 = 253 \pm 4$, so the uncertainty in its location is fractionally much smaller, and this normal mode does confirm the $\sigma_0 \simeq 200$ g cm^{-2} value that was inferred from simulations of the B ring's forced response R_2.

One of the goals of this study is to determine whether simulations of free modes can be used to determine the surface density and mass of a narrow ringlet. Such ringlets show a broad spectrum of free normal models over $0 \leqslant m \leqslant 5$ (French et al. 2010, 2011; Hedman et al. 2010; Nicholson et al. 2012), and the answer appears to be yes since free pattern speeds do increase with σ_0. However, Section 3.1.2 shows that the semimajor axes of the ringlet's edges likely need to be known to a precision of $\delta a_{\text{edge}} \sim 1$ km in order for a free mode to provide a useful measurement of the ringlet's σ_0.

The origin of these free modes, which are quite common along the edges of Saturn's broad rings and its many narrow ringlets, is uncertain. Borderies et al. (1985) show that, if a planetary ring's particles are packed shoulder to shoulder such that the ring behaves like an incompressible fluid, then that ring is unstable to the growth of density waves, a phenomenon also termed viscous overstability, and they suggest that the B ring's normal modes might be due to unstable waves that are trapped between a Lindblad resonance and the ring's edge. To study this further, we will in a follow-up study adapt `epi_int` to employ an incompressible equation of state, to see if the viscous overstability can in fact account for the free normal modes seen along the Saturnian ring edges.

Although the current version of `epi_int` does not account for the origin of these free modes, one can still plant a free mode along the edge of a simulated ring by temporarily perturbing a ring at a fictitious satellite's Lindblad resonance, and then removing that satellite, which creates an unforced mode that persists undamped at the ring-edge for more than $\sim 10^5$ orbits or ~ 100 yr despite the simulated ring having a kinematic viscosity of $\nu = 100$ cm^2 s^{-1}. Because this forcing is suddenly turned on and off, this suggests that any sudden or impulsive disturbance of the ring can excite normal modes, with those disturbances possibly persisting for hundreds or maybe thousands of years. And in Section 4.3, we suggest that the Saturnian normal modes might be excited by an impact with a collisionally disrupted cloud of comet dust. This is a slight variation of the scenario that Hedman et al. (2007) and Showalter et al. (2011) propose for the origin of corrugated planetary rings, and in a follow-up investigation we intend to determine whether such impacts can also account for the normal modes seen in Saturn's rings.

Last, we find that `epi_int`'s treatment of ring viscosity has difficulty accounting for the radial confinement of the B ring's outer edge by Mimas's $m = 2$ ILR. This model employs a kinematic shear viscosity ν_s that is everywhere a constant, which causes the simulation's outermost streamline to slowly but steadily drift radially outward, which in turn causes the ring's forced epicyclic amplitude R_2 to slowly grow over time and makes difficult any comparison to *Cassini*'s measurement of R_2. To sidestep this difficulty, the model zeros the torque that the simulated ring exerts on its outermost streamline, which does allow the ring to settle into a static configuration that can be compared to *Cassini* observations and yields a measurement of the ring's surface density σ_0. This approximate treatment is also examined in Section 4.1, which shows that the viscous acceleration of the ring-edge, had it been included in the simulation, is still orders of magnitude smaller than that due to ring self-gravity. So this study of the dynamics of the B ring's forced and free modes is not adversely impacted by this approximate treatment, but this does mean that the B ring's radial confinement is still an unsolved problem, and Section 4.1.1 suggests that this might be a consequence of treating ν_s as a constant. Borderies et al. (1982) show that viscosity's outward transport of energy should also heat the ring's outer edge and increase the ring particles' dispersion velocity c there. Also, if collisions among ring particles are the dominant source of ring viscosity, then $\nu_s \propto c^2$ and viscous dissipation would be enhanced at the ring edge, which in turn would increase the angular lag between the ring's forced response and the Mimas's longitude. That then would increase the gravitational torque that that satellite exerts on the ring-edge. Therefore, in a follow-up study we will modify `epi_int` to address this problem in a fully self-consistent way, to see if enhanced dissipation at the ring-edge also increases Mimas's gravitational torque there sufficiently to prevent the B ring's outer edge from flowing viscously beyond that satellite's $m = 2$ ILR.

APPENDIX A

The following calculates the flux of angular momentum that is communicated via a disk's viscosity. The disk is flat and thin and has a vertical half-width h and constant volume density ρ that is related to its surface density σ via $\rho = \sigma/2h$. The disk is assumed to be viscous, and its gravity is ignored here since this appendix is only interested in the angular momentum flux that is transported solely by viscosity.

The density of angular momentum in the disk is $\boldsymbol{\ell} = \mathbf{r} \times \rho \mathbf{v}$, and the vertical component along the $z = x_3$ axis is $\ell_3 = x_1 \rho v_2 - x_2 \rho v_1$ in Cartesian coordinates $x = x_1$ and $y = x_2$ where ρ and v_i are functions of position and time, so the time rate of change of ℓ_3 is

$$\frac{\partial \ell_3}{\partial t} = x_1 \frac{\partial}{\partial t}(\rho v_2) - x_2 \frac{\partial}{\partial t}(\rho v_1). \quad (A1)$$

The time derivatives in the above are Euler's equation,

$$\frac{\partial}{\partial t}(\rho v_i) = -\sum_{k=1}^{3} \frac{\partial \Pi_{ik}}{\partial x_k}, \quad (A2)$$

where Π_{ik} are the elements of the momentum flux density tensor

$$\Pi_{ik} = \rho v_i v_k + \delta_{ik} p - \sigma'_{ik} \quad (A3)$$

where p is the pressure and σ'_{ik} are the elements of the viscous stress tensor (Landau & Lifshitz 1987). Inserting Equation (A3)

into Equation (A1) yields

$$\frac{\partial \ell_3}{\partial t} = -x_1 \nabla \cdot \mathbf{\Pi}_2 + x_2 \nabla \cdot \mathbf{\Pi}_1, \qquad (A4)$$

where the vector

$$\mathbf{\Pi}_i = \sum_{k=1}^{3} \Pi_{ik} \hat{\boldsymbol{x}}_k \qquad (A5)$$

is the flux density of the i component of linear momentum and $\hat{\boldsymbol{x}}_k$ is the unit vector along the x_k axis. Equation (A4) can be rewritten as

$$\frac{\partial \ell_3}{\partial t} = -\nabla \cdot (x_1 \mathbf{\Pi}_2 - x_2 \mathbf{\Pi}_1) + \mathbf{\Pi}_2 \cdot \nabla x_1 - \mathbf{\Pi}_1 \cdot \nabla x_2, (A6)$$

but note that $\mathbf{\Pi}_1 \cdot \nabla x_2 - \mathbf{\Pi}_2 \cdot \nabla x_1 = \Pi_{21} - \Pi_{12} = \sigma'_{12} - \sigma'_{21} = 0$ since the viscous stress tensor is symmetric (Equation (A11)), so

$$\frac{\partial \ell_3}{\partial t} = -\nabla \cdot \boldsymbol{F}_3 \qquad (A7)$$

where

$$\boldsymbol{F}_3 = x_1 \mathbf{\Pi}_2 - x_2 \mathbf{\Pi}_1. \qquad (A8)$$

Integrating Equation (A7) over some volume V that is bounded by area A yields

$$\frac{\partial}{\partial t} \int_V \ell_3 dV = -\int_V \nabla \cdot \boldsymbol{F}_3 dV = -\int_A \boldsymbol{F}_3 \cdot d\boldsymbol{A} \quad (A9)$$

by the divergence theorem, so Equation (A9) indicates that $\boldsymbol{F}_3$ is the flux of the x_3 component of angular momentum out of volume V that is being transported by advection, pressure, and viscous effects.

This appendix is interested in the part of $\boldsymbol{F}_3$ that is due to viscous effects, which will be identified as $\boldsymbol{F}_3'$ and is obtained by replacing Π_{ik} in Equation (A3) with $-\sigma'_{ik}$ so

$$\boldsymbol{F}_3' = \left(x_2 \sigma'_{11} - x_1 \sigma'_{21}\right)\hat{\boldsymbol{x}}_1 + \left(x_2 \sigma'_{12} - x_1 \sigma'_{22}\right)\hat{\boldsymbol{x}}_2. \quad (A10)$$

This is the 2D flux of the x_3 component of angular momentum that is transported by the disk's viscosity whose horizontal components in Cartesian coordinates are $\boldsymbol{F}_3' = F_1'\hat{\boldsymbol{x}}_1 + F_2'\hat{\boldsymbol{x}}_2$ where $F_1' = x_2 \sigma'_{11} - x_1 \sigma'_{21}$ and $F_2' = x_2 \sigma'_{12} - x_1 \sigma'_{22}$. However, this appendix desires the radial component of $\boldsymbol{F}_3'$ at some site r, θ in the disk, which is $F_r' = F_1' \cos \theta + F_2' \sin \theta$.

The elements of the viscous stress tensor are (Landau & Lifshitz 1987)

$$\sigma'_{ik} = \eta \left(\frac{\partial v_i}{\partial x_k} + \frac{\partial v_k}{\partial x_i}\right) + \left(\zeta - \frac{2}{3}\eta\right) \delta_{ik} \nabla \cdot \boldsymbol{v}, \quad (A11)$$

where η is the shear viscosity, ζ is the bulk viscosity, and δ_{ik} is the Kronecker delta. Inserting this into F_r' and replacing $x_1 = r \cos \theta$ and $x_2 = r \sin \theta$ then yields

$$F_r' = -\eta r \left(\frac{\partial v_1}{\partial x_2} + \frac{\partial v_2}{\partial x_1}\right) \cos 2\theta + \eta r \left(\frac{\partial v_1}{\partial x_1} - \frac{\partial v_2}{\partial x_2}\right) \sin 2\theta. \tag{A12}$$

The horizontal velocities are $v_1 = v_r \cos \theta - v_\theta \sin \theta$ and $v_2 = v_r \sin \theta + v_\theta \cos \theta$ when written in terms of their radial

component v_r and tangential component $v_\theta = r\dot{\theta}$. The derivatives in Equation (A12) are

$$\frac{\partial v_1}{\partial x_1} = \left(\cos \theta \frac{\partial}{\partial r} - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta}\right) v_1$$
$$= \cos^2 \theta \frac{\partial v_r}{\partial r} - \sin \theta \cos \theta r \frac{\partial \dot{\theta}}{\partial r} + \frac{\sin^2 \theta}{r} v_r$$
$$- \frac{\sin \theta \cos \theta}{r} \frac{\partial v_r}{\partial \theta} + \frac{\sin^2 \theta}{r} \frac{\partial v_\theta}{\partial \theta}$$

$$\frac{\partial v_2}{\partial x_2} = \left(\sin \theta \frac{\partial}{\partial r} + \frac{\cos \theta}{r} \frac{\partial}{\partial \theta}\right) v_2$$
$$= \sin^2 \theta \frac{\partial v_r}{\partial r} + \sin \theta \cos \theta r \frac{\partial \dot{\theta}}{\partial r} + \frac{\cos^2 \theta}{r} v_r$$
$$+ \frac{\sin \theta \cos \theta}{r} \frac{\partial v_r}{\partial \theta} + \frac{\cos^2 \theta}{r} \frac{\partial v_\theta}{\partial \theta}$$

$$\frac{\partial v_1}{\partial x_2} = \left(\sin \theta \frac{\partial}{\partial r} + \frac{\cos \theta}{r} \frac{\partial}{\partial \theta}\right) v_1$$

$$\frac{\partial v_2}{\partial x_1} = \left(\cos \theta \frac{\partial}{\partial r} - \frac{\sin \theta}{r} \frac{\partial}{\partial \theta}\right) v_2, \qquad (A13)$$

when written in terms of cylindrical coordinates, and the combinations of derivatives in Equation (A12) are

$$\frac{\partial v_1}{\partial x_2} + \frac{\partial v_2}{\partial x_1} = \left(\frac{\partial v_r}{\partial r} - \frac{1}{r} \frac{\partial v_\theta}{\partial \theta} - \frac{v_r}{r}\right) \sin 2\theta$$
$$+ \left(\frac{\partial v_\theta}{\partial r} + \frac{1}{r} \frac{\partial v_r}{\partial \theta} - \frac{v_\theta}{r}\right) \cos 2\theta \quad (A14a)$$

$$\frac{\partial v_1}{\partial x_1} - \frac{\partial v_2}{\partial x_2} = \left(\frac{\partial v_r}{\partial r} - \frac{1}{r} \frac{\partial v_\theta}{\partial \theta} - \frac{v_r}{r}\right) \cos 2\theta$$
$$- \left(\frac{\partial v_\theta}{\partial r} + \frac{1}{r} \frac{\partial v_r}{\partial \theta} - \frac{v_\theta}{r}\right) \sin 2\theta. \quad (A14b)$$

Inserting these into Equation (A12) then yields a result that is thankfully much more compact,

$$F_r' = -\eta \left(r^2 \frac{\partial \dot{\theta}}{\partial r} + \frac{\partial v_r}{\partial \theta}\right) \simeq -\eta r^2 \frac{\partial \dot{\theta}}{\partial r}, \qquad (A15)$$

noting that the second term in Equation (A15) may be neglected since the azimuthal gradient is much smaller than the radial gradient for the disks considered here. This is the radial component of the disk's 2D viscous angular momentum flux density, so the 1D viscous angular momentum flux density is Equation (A15) integrated through the disk's vertical cross section:

$$F = \int_{-h}^{h} F_r' dx_3 = -v_s \sigma r^2 \frac{\partial \dot{\theta}}{\partial r} \qquad (A16)$$

where $v_s = \eta/\rho$ is the disk's kinematic shear viscosity.

APPENDIX B

The flux density of x_1-type momentum is $\mathbf{\Pi}_1$ (see Equation (A5)) while the flux density of x_2-type momentum is $\mathbf{\Pi}_2$, so the flux density of radial momentum is $\boldsymbol{G} = \cos \theta \mathbf{\Pi}_1 +$

$\sin\theta\,\boldsymbol{\Pi}_2$ and the radial component of this momentum flux density is

$$
\begin{aligned}
G_r = \boldsymbol{G} \cdot \hat{\boldsymbol{r}} &= (\cos\theta\Pi_{11} + \sin\theta\Pi_{21})\hat{\boldsymbol{x_1}} \cdot \hat{\boldsymbol{r}} \\
&+ (\cos\theta\Pi_{12} + \sin\theta\Pi_{22})\hat{\boldsymbol{x_2}} \cdot \hat{\boldsymbol{r}}
\end{aligned}
\tag{B1}
$$

$$
= \cos^2\theta\Pi_{11} + \sin\theta\cos\theta(\Pi_{12} + \Pi_{21}) + \sin^2\theta\Pi_{22}, \tag{B2}
$$

where $\hat{\boldsymbol{r}}$ is the unit vector in the radial direction. The part of that momentum flux that is transported solely by viscous effects will be called G'_r and is again obtained by replacing the Π_{ik} in the above with $-\sigma'_{ik}$:

$$
G'_r = -\cos^2\theta\sigma_{11} - \sin\theta\cos\theta\left(\sigma'_{12} + \sigma'_{21}\right) - \sin^2\theta\sigma'_{22} \tag{B3}
$$

$$
\begin{aligned}
= &-2\eta\left[\cos^2\theta\frac{\partial v_1}{\partial x_1} + \sin^2\theta\frac{\partial v_2}{\partial x_2} + \sin\theta\cos\theta\left(\frac{\partial v_1}{\partial x_2} + \frac{\partial v_2}{\partial x_1}\right)\right] \\
&-\left(\zeta - \frac{2}{3}\eta\right)\boldsymbol{\nabla} \cdot \boldsymbol{v}.
\end{aligned}
\tag{B4}
$$

Equations (A13) provide the combination

$$
\begin{aligned}
\cos^2\theta\frac{\partial v_1}{\partial x_1} + \sin^2\theta\frac{\partial v_2}{\partial x_2} &= \left(\frac{3}{4} + \frac{1}{4}\cos 4\theta\right)\frac{\partial v_r}{\partial r} \\
&- \frac{1}{4}\sin 4\theta\, r\frac{\partial\dot\theta}{\partial r} + \frac{1}{2r}\sin^2 2\theta\, v_r - \frac{1}{4r}\sin 4\theta\frac{\partial v_r}{\partial\theta} \\
&+ \frac{1}{2r}\sin^2 2\theta\frac{\partial v_\theta}{\partial\theta},
\end{aligned}
\tag{B5}
$$

and inserting this plus Equation (A14a) into Equation (B3) then yields

$$
G'_r = -\left(\frac{4}{3}\eta + \zeta\right)\frac{\partial v_r}{\partial r} - \left(\zeta - \frac{2}{3}\eta\right)\left(\frac{v_r}{r} + \frac{1}{r}\frac{\partial v_\theta}{\partial\theta}\right), \tag{B6}
$$

but the $\partial v_\theta/\partial\theta$ term is again neglected in the streamline approximation. This is the 2D radial momentum flux due to viscous transport, so the vertically integrated linear momentum flux due to viscosity is

$$
G = \int_{-h}^{h} G'_r\, dx_3 = -\left(\frac{4}{3}\nu_s + \nu_b\right)\sigma\frac{\partial v_r}{\partial r} - \left(\nu_b - \frac{2}{3}\nu_s\right)\frac{\sigma v_r}{r}. \tag{B7}
$$

REFERENCES

Borderies, N., Goldreich, P., & Tremaine, S. 1982, Natur, 299, 209
Borderies, N., Goldreich, P., & Tremaine, S. 1983a, AJ, 88, 1074
Borderies, N., Goldreich, P., & Tremaine, S. 1983b, Icar, 55, 124
Borderies, N., Goldreich, P., & Tremaine, S. 1985, Icar, 63, 406
Borderies, N., Goldreich, P., & Tremaine, S. 1986, Icar, 68, 522
Borderies-Rappaport, N., & Longaretti, P.-Y. 1994, Icar, 107, 129
Chambers, J. E. 1999, MNRAS, 304, 793
Cuzzi, J. N., Burns, J. A., Charnoz, S., et al. 2010, Sci, 327, 1470
Duncan, M. J., Levison, H. F., & Lee, M. H. 1998, AJ, 116, 2067
French, R. G., Marouf, E. A., Rappaport, N. J., & McGhee, C. A. 2010, AJ, 139, 1649
French, R. G., Nicholson, P. D., Colwell, J., et al. 2011, in EPSC-DPS Joint Meeting 2011 (Göttingen: Copernicus), 624
Goldreich, P., & Tremaine, S. 1979, AJ, 84, 1638
Goldreich, P., & Tremaine, S. 1982, ARA&A, 20, 249
Goldstein, H. 1980, Classical Mechanics (2nd ed.; Reading, MA: Addison-Wesley)
Hahn, J. M., Spitale, J. N., & Porco, C. C. 2009, ApJ, 699, 686
Hedman, M. M., Burns, J. A., Evans, M. W., Tiscareno, M. S., & Porco, C. C. 2011, Sci, 332, 708
Hedman, M. M., Burns, J. A., Showalter, M. R., et al. 2007, Icar, 188, 89
Hedman, M. M., Nicholson, P. D., Baines, K. H., et al. 2010, AJ, 139, 228
Kudryavtsev, L. D., & Samarin, M. K. 2013, Lagrange Interpolation Formula, Encyclopedia of Mathematics. http://www.encyclopediaofmath.org/index.php?title=Lagrange interpolation formula&oldid=17497
Landau, L. D., & Lifshitz, E. M. 1987, Fluid Mechanics (2nd ed.; Oxford: Elsevier)
Longaretti, P.-Y., & Rappaport, N. 1995, Icar, 116, 376
Melita, M. D., & Papaloizou, J. C. B. 2005, CeMDA, 91, 151
Nicholson, P. D., French, R. G., & M., H. M. 2012, contributed talk at AAS/DDA Conference, 1, 1
Pringle, J. E. 1981, ARA&A, 19, 137
Richardson, D. C., Bottke, W. F., & Love, S. G. 1998, Icar, 134, 47
Salo, H. 1995, Icar, 117, 287
Showalter, M. R., Hedman, M. M., & Burns, J. A. 2011, Sci, 332, 711
Shu, F. H. 1984, in IAU Colloq. 75: Planetary Rings, ed. R. Greenberg & A. Brahic (Tucson, AZ: Univ. Arizona Press), 513
Spitale, J. N., & Porco, C. C. 2010, AJ, 140, 1747
Sridhar, S., & Tremaine, S. 1992, Icar, 95, 86
Tiscareno, M. S., Burns, J. A., Nicholson, P. D., Hedman, M. M., & Porco, C. C. 2007, Icar, 189, 14
Ward, W. R. 1986, Icar, 67, 164