

Methanol and Ethanol Decomposition in Supercritical Water

By Walter Hack*, David A. Masten, and Steven J. Buelow

Photochemistry and Photophysics Group, CST-4, MS J567, Los Alamos National Laboratory, Los Alamos, NM 87545, USA

Dedicated to Prof. Dr. Michael Buback on the occasion of his 60th birthday

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The decomposition of CH₃OH and C₂H₅OH in supercritical water was studied in a flow reactor tube (Ni/Mo/Cr/Fe alloy) in the temperature range $597 \leq T/\text{K} \leq 797$ at a pressure of $p = 315$ bar for technical application of scH₂O for hazardous chemical waste destruction. The CH₃OH and C₂H₅OH concentrations in the liquid as a function of the residence times were determined by a Raman spectrometer.

The [CH₃OH] and [C₂H₅OH] resp. decay followed first order kinetics and a rate constant $k_1(653 \text{ K}) = 1.3 \times 10^{-2} \text{ s}^{-1}$ for CH₃OH and $k_2(653 \text{ K}) = 5.5 \times 10^{-2} \text{ s}^{-1}$ for C₂H₅OH was determined. The rate constant k_1 was found to be independent of the initial CH₃OH concentration in the mass fraction range $0.002 \leq x_m \leq 0.04$. The rate depended on the history of the reactor. Treatment with NH₄OH, C₂H₅OH or with H₂O₂ at $T = 653 \text{ K}$, did not change the rate. Treatment with HNO₃/H₂O₂, however, at $T = 838 \text{ K}$ reduced the rate by about a factor of 1000.

The Arrhenius-activation energy over the above temperature range was determined to be $E_A = 164 \text{ kJ/mol}$ for methanol and $E_A = 145 \text{ kJ/mol}$ for ethanol.

The major products from methanol decomposition were CH₄, H₂, and CO₂ as observed by gas chromatography and CH₄ and CO₂ by FTIR-spectrometry. No other products were found. The products were not effected by the pretreatment of the reactor wall. A non-radical mechanism, which explains the formation of only these products, will be discussed.

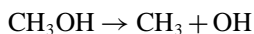
1. Introduction

Supercritical fluids are emphasized to be advantageous as solvents for chemical reactions. They provide a continuously tunable temperature and pressure range

* Corresponding author. Permanent address: Max-Planck-Institut für biophysikalische Chemie, Am Faßberg 11, 37077 Göttingen, Germany. E-mail: whack@gwdg.de

and thus optimum reactivity and selectivity conditions may be chosen. The tunability of the reaction medium provides the potential of establishing suitable combinations of solvent and transport properties. As pointed out by Buback, it is possible to carry out chemical reactions by exploiting the special properties of the compressed fluid phase [1].

Supercritical water (scH₂O) is an appropriate medium for the destruction of hazardous organic chemical waste. Partly oxidized hydrocarbons can be regarded as prototypes of such organic molecules the simplest of which is CH₃OH. For this reason the decomposition of methanol and ethanol is studied in sc water. In the gas phase, the decomposition of CH₃OH has been studied extensively, whereby the excited CH₃OH has been produced thermally in shock waves and flames, or chemically in the combination reaction CH₃ + OH, or in other chemical reactions like O(¹D) + CH₄ [2], or CH₂(\tilde{a}) + H₂O [3]. For the gas phase at low densities the decomposition into two radicals



is well accepted as the dominant initial step [4] which proceeds with an activation energy of $E_A = 334 \text{ kJ/mol}$ [5]. This might be different at liquid-like densities realized in supercritical water and it seems to be interesting to study the CH₃OH and C₂H₅OH decomposition under these conditions.

If supercritical water is used to destroy organic waste material, the small alcohols like methanol and ethanol might be regarded as a model compound to study the decomposition of H/C/O containing organic molecules. If water at high temperature and densities with significantly different physicochemical properties than H₂O at low temperature and pressures, is used as a solvent for synthesis reactions or destruction reactions, it is essential to know the stability of the organic compounds. If decomposition under supercritical conditions cannot be avoided, it is necessary to know the decomposition products and the intermediated, *i.e.*, the decomposition mechanism. For kinetic measurements also the decomposition rate has to be known. This study deals with some aspects with relevance to a technical and industrial use of scH₂O for a realisation of hazardous chemical waste destruction.

The decomposition of methanol [6, 7] and ethanol [8] in supercritical water have been studied with respect to the products, but no reaction rates were given. The decomposition of CH₃OH in supercritical water was observed as a side effect, when oxidizing CH₃OH either by O₂ [9] or by NO₃⁻ [10]. The rate constant for the methanol decomposition at $T = 817 \text{ K}$ was found to be $k = 3.1 \times 10^{-3} \text{ s}^{-1}$ [9]. The products of the CH₃OH decomposition were not reported. Moreover a slow hydro-thermolysis of methanol was observed in a static cell in supercritical water [7].

The aim of this work was to study the kinetics of the decomposition of CH₃OH \rightarrow prod (1) and C₂H₅OH \rightarrow prod (2) in supercritical water, *i.e.*; to determine the rate, the activation energy, and the decomposition products.

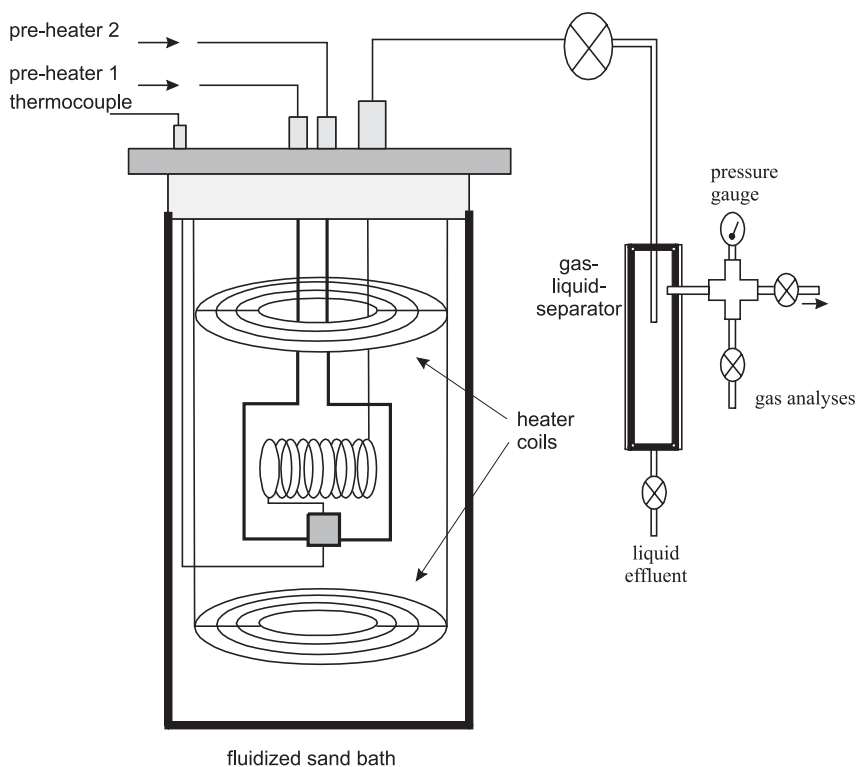


Fig. 1. Experimental apparatus: Tubular reactor in a fluidized sandbath.

2. Experimental

The experiments were performed in a hastelloy tube flow reactor (alloy C-276 (58% Ni; 16% Mo; 15% Cr; 5% Fe; 3.5% W and 2.5% Co)). The tube had an inner diameter of $\varnothing = 2.11$ mm. The reactor was heated in a fluidized sand bath as shown in Fig. 1 and described in detail in [10]. The liquid enters the reactor, which has a total volume of $V = 12.17$ ml and a surface to volume ratio $S/V = 1.9$ mm⁻¹, via one of two nearly symmetrical preheating tubes, which are connected to the flow reactor. At the end of the reactor there is a quenching section, which is cooled down to room temperature via water cooling. To study the reaction of two reactants, the mixing point (Fig. 1) is equivalent to reaction time zero. For a decomposition reaction, as studied in this work, the preheating time cannot be ignored. The volumes of preheating tubes are $V = 6.8$ ml each. It was assumed that after approximately 30% of the preheating length, the final temperature can be attained taking into account the region in which the temperature changes from room temperature to reactor temperature. The effect of preheating can be changed by varying the residence time in the

actor, pumping a constant amount of CH₃OH solution through one preheating tube and pure water through the other. The results were less reliable due to the change in initial CH₃OH concentration; but the above assumption could be verified. The uncertainty in the preheating section contributes to the uncertainty of the absolute value of the rate constant (see results section) but much less to the uncertainty of the activation energy.

The methanol/water and ethanol/water mixture was pumped into the reactor with two liquid chromatography feed pumps (Consta Metric 3200, LDC Analytical), which allowed a change of the total flow (v) in the range of $0.05 \leq v/\text{g s}^{-1} \leq 0.358$. The flow was determined by measuring the mass decrease of the liquid reservoir or the mass of liquid leaving the reactor in a given time.

Probes from the liquid leaving the reactor were taken and analyzed by Raman spectroscopy. The Raman apparatus has been described in detail elsewhere [11]. The probe was excited with the 488 nm line of a cw-Ar⁺-laser, the scattered light red shifted by 2857 cm⁻¹ was spectrally dispersed with a 0.6 m monochromator (Triplemate 1877 Spex Ind. Inc.) and detected with a CCD camera (ST-130 Princeton Instruments Inc.).

The gas products were analyzed either with a gas chromatograph (Hewlett Packard 5890 series II) or with an FTIR spectrometer (Perkin Elmer 1260X). The gas chromatograph was equipped with a capillary column (carboplat P 7 Chrom pak) and a thermal conductivity detector. Helium was used as a carrier gas, when CO₂, CO, CH₄, and other hydrocarbons were to be detected; in an independent experiment H₂ was detected with Ar as a carrier gas.

As reactants home-made de-ionized water was used and CH₃OH (99.94% EM Science) with the main impurity being H₂O (0.03%) and C₂H₅OH (99% EM Science) (impurity H₂O).

3. Results

3.1 Reaction rate

The rate constant for the reaction



in water under liquid and supercritical conditions was measured in the temperature range $597 \leq T/\text{K} \leq 719$. The initial concentration of CH₃OH in water was varied in the range $0.002 \leq x_m \leq 0.04$ (mass fraction) *i.e.* $0.001 \leq x \leq 0.0225$ (mole fraction). The pressure was kept in the region of $p = 315$ bar. All experimental data are summarized in Table 1. At $T \geq 797$ K the reaction was found to be so fast that only a lower limit of the rate constant was determined.

The residence time in the reactor was varied by the pumping speed, which was limited to about 0.18 g s⁻¹ for each pump. The residence time in the pre-

Table 1. CH₃OH decomposition. Experimental condition for all runs.

T [K]	P [bar]	CH ₃ OH $\times 10^{-3}$	$\rho(\text{H}_2\text{O}) \left[\frac{\text{g}}{\text{cm}^3} \right]$	Δt_{max} [s]	k_1 [10^{-3} s^{-1}]
597	313.2	5.87	0.716	244	1.3
623	315.4	5.60	0.646	211	2.7
653	312.5	1.25	0.543	199	13.0*
653	313.9	1.47	0.543	179	14.6
653	316.8	5.84	0.543	165	14.6
653	316.0	23.1	0.543	181	11.2
683	314.7	5.84	0.310	93.9	48.2
719	315.8	5.77	0.165	21.6	200

* surface oxidized by H₂O₂ treatment

heating tubes was taken into account by assuming that the final reactor temperature is reached after 30% of the preheating tube lengths. This assumption enters into the overall residence time and thus into the derived first order rate constant. The uncertainty of this assumption is responsible for the error bars given for the first order rate constant. The temperature dependence and thus the activation energy is much less effected by this correction.

The CH₃OH concentration in the liquid samples collected at the end of the reactor was analyzed by a Raman spectrometer. The spectrometer gave a linear dependence for the Raman signal as a function of [CH₃OH] for pure methanol samples. It has to be assumed that the Raman signal is not influenced by any of the products formed in the reaction. From the product analysis (see products) this assumption, however, appears valid.

The plots of $\ln \{[\text{CH}_3\text{OH}]/[\text{CH}_3\text{OH}]_0\}$ vs. residence times (whereby [CH₃OH] is the CH₃OH concentration at the exit and [CH₃OH]₀ the initial methanol concentration) yielded straight lines for all temperatures as shown in Fig. 2. From these data the rate constant at a given temperature, say $T = 653 \text{ K}$, was determined to be:

$$k_1(653 \text{ K}) = (1.3 \pm 0.3) \times 10^{-2} [\text{s}^{-1}].$$

The error is mainly due to the uncertainty of the residence time.

The activation energy for the methanol depletion is obtained from a plot of $\ln k_1$ vs. $1/T$ as shown in Fig. 3. A straight line is obtained, indicating an Arrhenius behaviour of the rate constant $k_1(T)$. The Arrhenius activation energy is found to be:

$$E_A = (167 \pm 20) \text{ kJ/mol}$$

in the temperature range $597 \leq T/\text{K} \leq 719$.

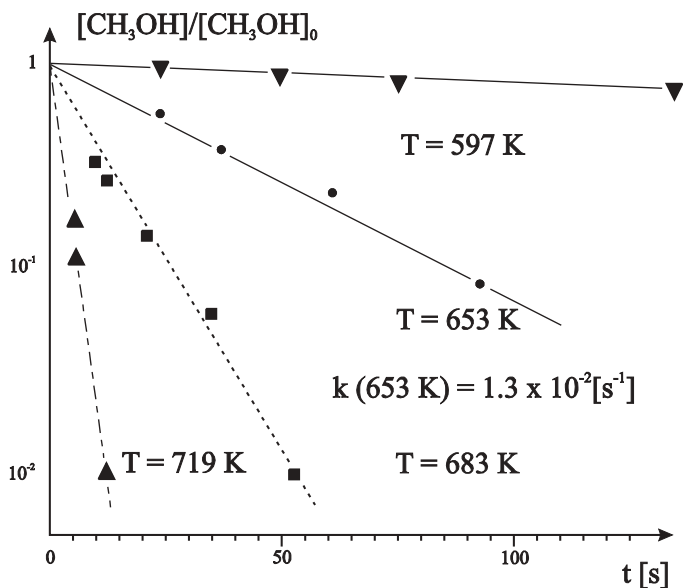


Fig. 2. First order decay of CH_3OH with residence time at different temperatures.

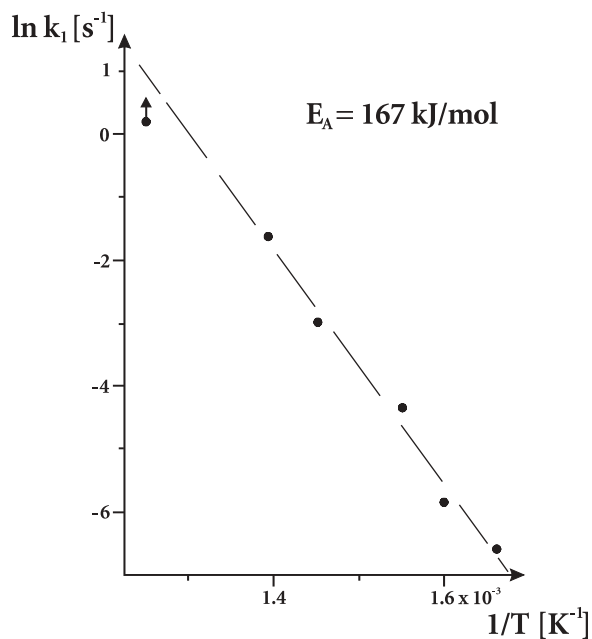


Fig. 3. Arrhenius plot for the methanol decomposition rate in supercritical water. The arrow indicates a lower limit at $k_1(789 \text{ K})$.

Table 2. C₂H₅OH decomposition. Experimental condition for all runs.

T [K]	P [bar]	$\text{CH}_3\text{OH} \times 10^{-3}$	$\rho(\text{H}_2\text{O}) \left[\frac{\text{g}}{\text{cm}^3} \right]$	$\Delta t_{\text{r,max}}$ [s]	k_2 [10^{-3} s^{-1}]
597	312.3	4.059	0.716	106.9	5.9
623	313.7	4.059	0.646	184.2	13.5
653	316.1	4.059	0.543	158.6	55.5
683	308.6	4.049	0.31	48.3	200
719	315.7	4.04	0.165	8.5	600

For one temperature ($T = 653 \text{ K}$) the initial concentration of CH₃OH was varied from $x = 1.42 \times 10^{-3}$ to $x = 2.3 \times 10^{-2}$; no effect of $[\text{CH}_3\text{OH}]_0$ on the rate constant was observed, which indicated that none of the initially formed products seem to react further with CH₃OH (see discussion).

For the reaction:



the rate constant was measured in the temperature range $597 \leq T/\text{K} \leq 719$. The experimental details are summarized in Table 2. The initial concentration was given as the mole fraction $x = 4.0 \times 10^{-3}$. The rate constant is about a factor of four higher than the rate constant of the decomposition of methanol at the same temperature, *e.g.*

$$k_2(653 \text{ K}) = (55 \pm 13) \times 10^{-3} \text{ s}^{-1}.$$

The rate constant increases with increasing temperature. The temperature dependence is shown in Fig. 4. An Arrhenius plot leads to a straight line and can be described by an activation energy of

$$E_A = (145 \pm 15) \text{ kJ/mol}$$

in the studied temperature range. This means that the rate for ethanol is faster than for methanol but with a smaller temperature dependence in the given temperature range.

3.2 Reaction products

The reaction products of the methanol decomposition were detected by gas chromatography and by FTIR spectrometry in the gas phase obtained in a gas liquid separator behind the quenching section. The liquid was analyzed for products by gas chromatography and liquid chromatography.

The amount of gas produced was determined by the pressure increase in a known volume in a given time.

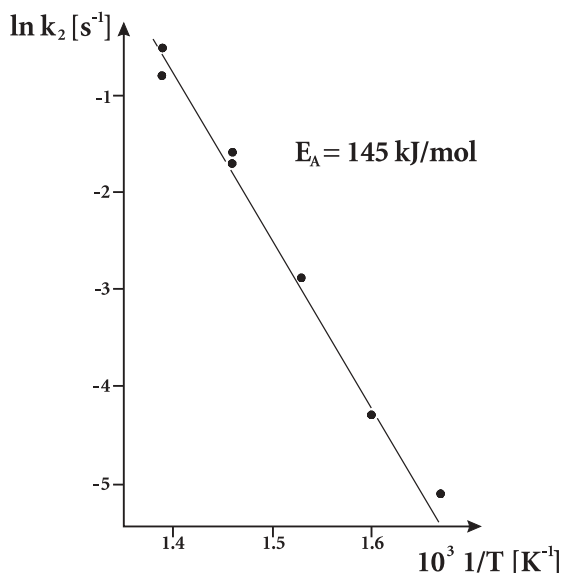


Fig. 4. Arrhenius plot for the ethanol decomposition rate in supercritical water.

The gas at a reactor temperature of $T = 653$ K consists mainly of H_2 ($x_{H_2} = 0.5$). The carbon is found as CH_4 ($x_{CH_4} = 0.33$) and CO_2 ($x_{CO_2} = 0.12$). The carbon balance was measured to be 94%, *i.e.*, more than 90% of the carbon initially bound in the CH_3OH is found as CH_4 or CO_2 . The gas product composition changes with temperature. At $T = 797$ K, the methane concentration is significantly lower ($x_{CH_4} = 2 \times 10^{-3}$) than at $T = 653$ K, whereas the mole fraction of H_2 is up to $x_{H_2} = 0.68$ and that of CO_2 to $x_{CO_2} = 0.32$ when the temperature was changed from $T = 653$ K to $T = 797$ K.

With the FTIR-spectrometer no further products were detected in the gas phase; in particular, no C_2 -containing compounds and no CO were found. In the liquid phase (at $T = 653$ K) CHOOH was detected. The detection method was not calibrated for CHOOH but the amount of CHOOH was small (estimation $[CHOOH]/[CH_3OH]_0 \cong 2 \times 10^{-4}$).

3.3 Reaction mechanism

Several experiments were done to determine the reaction mechanism and its dependence on the pretreatment of the wall.

The reaction was followed at very low initial CH_3OH concentrations and the reactor walls were treated in different ways by ethanol, hydrogen peroxide, and finally, by nitric acid/hydrogen peroxide.

It was observed that at the very low initial CH_3OH concentrations ($x_{CH_3OH} \leq 5.25 \times 10^{-5}$) the depletion rate was significantly lower than at higher

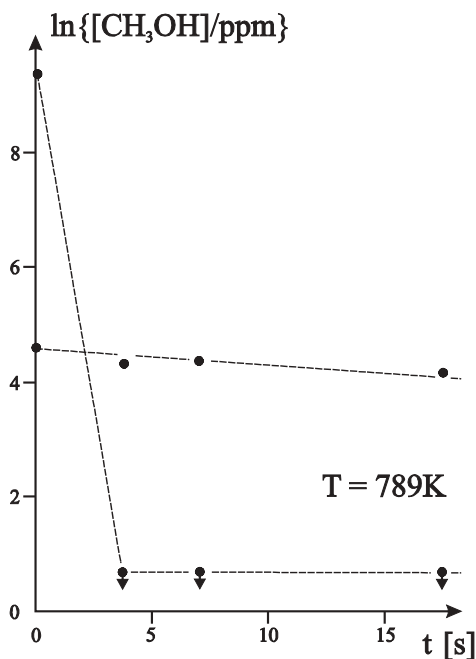


Fig. 5. Concentration profiles for CH_3OH at $T = 789\text{ K}$, $p = 316.5\text{ bar}$ (the straight lines are given to help to identify the measured points). $\downarrow = \text{CH}_3\text{OH}$ concentration below detection limit.

concentrations. At a temperature of $T = 798\text{ K}$ the CH_3OH concentration depleted to about 60% after the reaction time of 17 s. This observation is interpreted as a surface reaction, *i.e.*, $\text{CH}_3\text{OH}(\text{aq})$ reacts with $\text{CH}_3\text{OH}(\text{ad})$ (see discussion). The concentration-time profiles for an experiment with a high and a low initial concentration are shown in Fig. 5. The CH_3OH concentration drops below the detection limit within several seconds (in agreement with the lower limit of the rate constant given in Fig. 3) when starting with high CH_3OH initial concentrations. In the experiment with the low $[\text{CH}_3\text{OH}]_0$ value, the depletion of CH_3OH is much slower and the CH_3OH concentration stays at a much higher level. This behaviour is also explained by a heterogeneous mechanism (see discussion).

In order to study the surface effect on the rate constant, the reactor was treated with $\text{C}_2\text{H}_5\text{OH}$ at temperatures up to $T = 673\text{ K}$ for several hours before these measurements were done. For one experiment (see Table 1), the reactor was treated with H_2O_2 to oxidize the surface. The H_2O_2 (3 mass-% solution in H_2O) was pumped through the reactor for two hours at $T = 473\text{ K}$ and than for more than 4 hours at $T = 573\text{ K}$ at a pressure of $p \cong 300\text{ bar}$. After that, the reactor was left at room temperature filled with H_2O_2 solution, for more than a day. Before starting the experiment, the reactor was rinsed with

pure H₂O at $T = 653$ K. The rate constant for the methanol decomposition obtained after that treatment of the surface did not differ from the rate constants obtained under otherwise identical conditions (see Table 1). The reactor was heated with a solution of HNO₃ and H₂O₂ (1 molar each) at $T = 838$ K for about 1/2 h. After the treatment the reactor was rinsed with H₂O for several hours at $T = 650$ K. The HNO₃/H₂O₂ treatment changed the reactivity of the surface significantly. Even at the highest temperature $T = 798$ K, no CH₃OH depletion was detected; *i.e.*, the reaction rate dropped by more than a factor of 10³. This deactivation could not be influenced by washing the reactor with H₂O₂ or with an alkaline solution (like NH₄OH). The reactor was also passivated for the C₂H₅OH depletion reaction, *i.e.*, the C₂H₅OH reacted in the same way as CH₃OH. The reactivity of the surface was increased by washing the reactor with HCl. After a treatment with 0.1 molar HCl for about 0.75 h and rinsing with pure H₂O for several hours, a rate constant for the CH₃OH depletion of $k(750 \text{ K}) \cong 0.04 \text{ s}^{-1}$ was observed. This is more than a factor of 40 above the value obtained after the HNO₃/H₂O₂ treatment. These observations clearly indicate that the methanol decomposition is strongly catalyzed by the surface of the reactor.

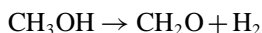
4. Discussion

The reaction

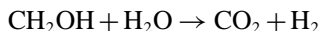


in supercritical water in a metal flow reactor proceeds at sufficient high (see below) concentrations in a first order reaction with an activation energy of $E_A = 167$ kJ/mol. This small activation energy, compared to that of the decomposition in the gas phase, indicates that a molecular mechanism rather than a radical mechanism is occurring. The decomposition is surface catalyzed: At high CH₃OH concentrations, which are sufficient to saturate the reactor surface with adsorbed methanol (CH₃OH (ad)), the reaction appears to be first order in CH₃OH. At CH₃OH concentrations below those necessary to saturate the surface, the reaction is no longer first order in CH₃OH and appears to be much slower. In order to explain this significant lower CH₃OH depletion rate, one has to assume that the methanol or one of the methanol decomposition products adsorbed at the wall is responsible for the CH₃OH depletion rate. This could be described as a reaction CH₃OH(ad) + CH₃OH(aq) → products. The CH₃OH concentration profiles observed for high and low initial methanol concentrations show that a reaction product of the methanol decomposition is adsorbed on the wall and reacts with methanol.

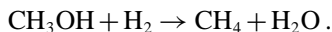
These heterogeneous reaction indicated that the mechanism can not be as simple as the three reactions:



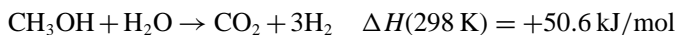
followed by:



and methane produced in the reaction:



These three reactions are sufficient to explain the observed products but they are not sufficient to describe the kinetic behaviour of the system. The overall reaction:



is endothermic and thus favored at higher temperatures as observed in the kinetic experiments.

The experiment, in which the CH_3OH decomposition was suppressed completely by changing the reactor surface, via $\text{HNO}_3/\text{H}_2\text{O}_2$ treatment, showed that the reaction is dominated by heterogeneous character. The change of the reactor surface would be explained by assuming that one of the alloy metals, which is responsible for the catalytic activity of the alloy, was specifically extracted from the surface. The HCl treatment renewed the surface by removing metal atoms unspecifically bringing back the catalytic activity.

Since the reaction (1) is a surface catalyzed reaction, it cannot simply be compared with data in other experiments unless the reactor surface and the pre-treatment of the reactor is described in detail.

The catalytic decomposition of methanol was studied in several publications [6, 7, 12–15]. The main products observed by Hirth and Franck [7], when they studied the decomposition of methanol in dense supercritical water at $T = 673 \text{ K}$ and $T = 773 \text{ K}$ at $p = 600 \text{ bar}$, were CO_2 , CH_4 and H_2 in the gas phase after expansion. In the liquid phase only methanol was found. The decomposition kinetics in the non-corrosive nickel alloy reactor, however, was very slow. After one hour the percentage of decomposed methanol was 3.8%. A temperature increase from $T = 673 \text{ K}$ to $T = 773 \text{ K}$ increased the methanol decomposition from 4.8 to 20.6%. These data correspond to a rate $k_1(773 \text{ K}) = 6.4 \times 10^{-5} \text{ s}^{-1}$ and an activation energy of $E_A = 78.6 \text{ kJ/mol}$.

In more recent experiments [6] which were done in a nickel-based alloy (Inconel 625) reactor in the temperature range $673 \leq T/\text{K} \leq 873$ at pressures from 25 to 45 MPa the methanol residence times (methanol conversion 99.9%) were in the range 3 to 100 s. The main component of the product gas was hydrogen with smaller amounts of carbon dioxide, carbon monoxide and methane.

It can be concluded that the kinetic decomposition behaviour of methanol in supercritical water strongly depends on the surface whereas the reaction

mechanism is less sensitive to the surface conditions. The decomposition rate varies for different reactor surfaces by two orders of magnitude whereas the reaction products are identical.

Acknowledgement

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