# SCALING OF A WALL-STABILIZED HIGH-BETA STELLARATOR

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#### Abstract:

On the basis of the surface current model, the scaling of an m=1 wall-stabilized high-ß stellarator is discussed in terms of the compression ratio  $\kappa$ , aspect ratio A, helical distortions  $\delta_0$ ,  $\delta_1$ ,  $\delta_2$ , and  $\beta$ . The m=1, k=0 mode can be wall-stabilized for  $\kappa \simeq 2$ ,  $\delta_1 \simeq 1$ , A  $\simeq 200$ ,  $\beta \simeq 0.83$ ,  $\delta_0 \simeq 0.21$ ,  $\delta_2 \simeq 0.07$ . The number of periods around the torus is then  $n_0 \simeq 0.6$  A/ $\kappa^2$ .

## I. INTRODUCTION

In the ISAR T 1 experiment, the toroidal finite-ß MHD equilibrium characterized by zero toroidal net current is produced by superimposing stellarator fields of different  $\ell$ -numbers on the main (toroidal) magnetic field /2,4/. The combination of an  $\ell$ -fold helical field with lower amplitude  $\ell \pm 1$  helical fields of proper period and phase compensates the outward toroidal drift force acting on the plasma column. Equilibria of this type can be regarded as a generalized class of M & S-type equilibria with non-planar magnetic axis.

The stability calculations of the m=1 mode /1,4,5/ show that, in leading order, the  $\ell=1$  helical field is the most favorable one for creating a high-ß equilibrium which is stable to the m=1, k=0 mode. Therefore, magnetic field configurations with  $\ell=1$  corrugation fields in leading order and lower-amplitude  $\ell=0$  and/or  $\ell=2$  have been investigated in more detail with respect to the stability behaviour /3,5/. The available theories based on the surface-current model show that the m=1 mode (rigid gross displacement) can be stabilized if the stabilizing effect of the conducting wall is taken into account. In the following note, we will discuss the scaling of experiments in the high-ß stellarator geometry which are wall-stabilized to m=1, k=0 modes /b/ and we will estimate the optimum regimes using those formulas for the growth rate of the m=1, k=0 mode in an  $\ell=0,1,2$  system which have been derived from the surface current model /1,2,3,5/.

The small parameter, used in the theories just cited as an expansion parameter, is  $\varepsilon:=ha$  (a mean plasma radius,  $h=2\pi/L$  periodicity number of the  $\ell=1$  helical field). In addition to  $\varepsilon$ , we use the following parameters: the compression ratio  $\kappa=b/a$  (b mean wall radius) and the aspect ratio A=R a related to the plasma radius (R major torus radius). The toroidal equilibrium configuration has n periods around the major circumference. The parameter  $\varepsilon$  is then related to the aspect ratio by  $\varepsilon=n/A$ . The only parameter relating the quantities inside the plasma to those outside is  $\beta=2p/B$  (kinetic plasma pressure over magnetic pressure of the outside main magnetic field  $\beta=1$  and of lower-amplitude  $\beta=1$ , 2 fields produces a deformation of the plasma surface of the form

$$r = \alpha \left\{ 1 + \sum \delta_{\ell} \cos \left( \ell \theta - hz \right) \right\}, \ \ell = 0, 1, 2 \tag{1}$$

where  $\delta_{\,\ell}$  are the deformations in units of the mean plasma radius.

The marginal limit of the m=1 mode can be expressed in six dimensionless parameters as a condition (see below):

$$F(\delta_1, A, \kappa; \alpha, \eta, \beta) = 0.$$

The search for an optimal working range under this condition has to include technical and other arguments which will be briefly listed for the parameters  $\delta_1$ , A and  $\kappa$  in the following.

Firstly,  $\delta_1$  has to be small. The need for a small helical distortion  $\delta_1$  is imposed mainly for technical reasons. But the limit of the validity of the formulas for equilibrium and stability is also reached when  $\delta_1$  becomes too large. The aspect ratio A has to be not to large; this is a condition from the view of reactor considerations. For the compression ratio n one has to look for a large value to reduce the problems of shock heating.

It turned out that optimization of these three quantities ( $\delta_1 \rightarrow \min!$ ,  $A \rightarrow \min!$ ,  $\mu \rightarrow \max!$ ) with respect to the remaining quantities  $\alpha$ , n and  $\beta$  leads in every case to the identical set of values  $\alpha_0$ ,  $\alpha_0$ , and  $\beta_0$ . So the requirements imposed on  $\delta_1$ , A, and  $\mu$  can be met at the same time and we can restrict ourselves in the following to the minimization of  $\delta_1$ .

The optimum values of the distortions  $\oint_{\ell}$  will be determined for systems with  $\ell=0,1$  and with  $\ell=0,1,2$  corrugation fields. The amplitudes of the distortions of the plasma surface are given by the equilibrium conditions

$$\delta_{\circ}\delta_{1} = \frac{2 \wedge \alpha}{n^{2} (3-2\beta)} \tag{2}$$

$$\delta_{2}\delta_{1} = (1 - \alpha) \frac{2A}{n^{2}(2-\beta)}$$
 (3)

The parameter  $\alpha$  varies between 0 and 1 (0 <  $\alpha$   $\leq$  1) and parameterizes the relative contribution of the  $\ell$  = 0 and the  $\ell$  = 2 corrugation fields. An optimum value of  $\alpha$  will be derived lateron which depends only on  $\beta$ .

## II. SCALING OF THE $\ell = 0,1,2$ CORRUGATION FIELDS

For the case of superimposed  $\ell=0,1,2$  corrugation fields, the growth rate  $\gamma$  of the  $m=1,\ k=0$  mode (k wave number in longitudinal direction) is given by /3/

$$\gamma^{2} = \frac{V^{2} n^{2}}{A^{2} \alpha^{2}} \frac{\beta}{(1-\beta)} \left[ G_{0} \int_{0}^{2} + \frac{n^{2}}{A^{2}} G_{1} \int_{1}^{2} + G_{2} \int_{2}^{2} + G_{3} \int_{1}^{4} - \frac{\beta}{\varkappa^{4}} \int_{1}^{2} \right]$$
(4)

where  $V = B_i / (\mu_0 \rho)^{1/2}$  is the Alfvén velocity and  $B_o^2 / \mu_0 \rho = \frac{V^2}{(1-\beta)}$ .

The functions  $G_{\ell}$ ,  $\ell=0,1,2$  have been introduced in 1/2 (without a factor of 2):

$$G_0 = \frac{(3-2\beta)(1-\beta)}{(2-\beta)}$$
 (5a)

$$G_1 = \frac{(4-3\beta)(2-\beta)}{8(1-\beta)}$$
 (5b)

$$G_2 = \frac{1}{2}(2 - B)$$
 (5c)

$$G_3 = \frac{\beta^4}{32(2-\beta)} \tag{5d}$$

The last term in Eq.(4) is the stabilizing wall term proportional to  $\chi^{-4}$ . Therefore,  $\kappa$  should be small (e.g. 2) in order to achieve effective wall stabilization. The stabilizing effect arises from the induced helical dipole current. The unstable term  $G_3$  is neglected because it is small compared to  $G_1$  and it can be fully compensated when an elliptical deformation is introduced 5/.

The two essential points in using the  $\ell=1$  field in leading order (in contrast to the classical M & S configuration /7/ ) are

- a) there is no unstable term of order  $0(\pi^2 \int_1^2 /A^2)$ ,
- b) there exists a strong stabilizing term of order  $0(\pi^2 \delta_1^2/A^2 \chi^4)$

of the same order as the unstable terms if  $\chi^4$  is small enough.

The growth rate of the m=1,  $k \neq 0$  mode is smaller than that for k=0; therefore, the case  $k \neq 0$  will not be investigated.

With the help of (2) and (3) we eliminate  $\delta_0$  and  $\delta_2$  in Eq.(4) and carry out the optimization for marginal stability ( $\gamma^2=0$ ). In this case Eq.(4) can be explicitly solved for  $\delta_1$ 

$$\delta_{1}^{4} = \frac{4\alpha^{2}(1-\beta)/(3-2\beta) + 2(1-\alpha)^{2}}{(2-\beta)[\beta n^{4}/(\mu^{4}A^{2}) - 6_{1}n^{6}/A^{4}]}$$
(6)

We shall now minimize  $\delta_1$  with respect to  $n_{\mbox{\scriptsize ,}\alpha}$  , and ß in that order.

The function  $\delta_1^4$  has local minima with respect to n, $\alpha$ , and  $\beta$ . After minimizing with respect to n, one sees that the A-and  $\alpha$ -dependences are simply given by the factor  $\alpha^{12}/A^2$  in front of  $\delta_1^4$ .

Furthermore, the three parameters A,n and  $\varkappa$  occur in Eq.(6) as the two combinations  $n/(\varkappa \bigtriangleup^{1/2})$  and  $n/A^{2/3}$ . Now the quantity  $\delta_1^4$  has a minimum with respect to n for  $n=n_1$ , where  $n_1$  is given by

$$n_1(\beta) = N_1 A / n^2$$
,  $N_1 = (2\beta/3G_1)^{1/2}$ . (7)

There is precisely one solution  $n_1$  for the number of periods and this solution is always positive.

# II. 1. $\ell = 0, 1$ - system ( $\alpha = 1$ ) at the gain index entrice ( $\lambda$ ) pd at the

With Eqs.(6) and (7)  $\delta_1$  was calculated for  $\alpha = 1$ :

$$\int_{1, n} = D_n \mathcal{N}^3 / A^{1/2}$$
with  $D_n(\beta) = \left[ \frac{27(4-3\beta)^2(2-\beta)}{64\beta^3(1-\beta)(3-2\beta)} \right]^{1/4}$ 

(the index n indicates minimization with respect to n).

The function  $D_n(\beta)$  varies weakly in the region 0.5  $\leq \beta \leq$  0.9, assumes the minimum value of 1.71 for  $\beta = \beta_2 = 0.86$  (see Fig.1), and is infinite for  $\beta = 0$  and 1. The corresponding  $\ell = 0$  deformation of the plasma surface is calculated from Eq.(2):

$$(\delta_0 \delta_1)_n = D_0 \kappa^4/A$$

with

$$D_{o} = \frac{3(4-3\beta)(2-\beta)}{8\beta(1-\beta)(3-2\beta)}$$
 (9)

In the special case where  $\beta=\beta_2$  minimizes  $D_n$  above one obtains  $D_o(\beta_2)=3.94$ , which does not coincide with the minimum value of  $D_o$ . The  $\beta$ -dependence of the  $\ell=0$  distortion after minimizing  $\delta_1^4$  with respect to n is given by  $D_o(\beta)$ .

The function D is shown in Fig.2 (dashed curve).

Finally, after minimization of  $d_1$  with respect to n and  $\beta$  one gets:

$$\delta_{1,n\beta} = 1.71 \, \chi^3 / A^{1/2} \,. \tag{10}$$

Fig. 3 shows the curves  $\mathcal{H} = \mathcal{H}(A; \delta_{1, n, \beta})$  in a logarithmic A,  $\mathcal{H}$  - diagram (dashed curves); the parameter of these curves is  $\delta_{1, n, \beta}$  and assumes the values 0.25, 0.50, 1, 2,3. The region above the curves is the unstable region.

# II.2. $\ell = 0, 1, 2 - \text{system } (\alpha \neq 1)$

Next we minimize  $\delta_1^4$ , Eq.(6), with respect to  $\alpha$  and with respect to n. Consequently, with Eq.(7) we obtain from Eq.(6) the minimizing  $\alpha$ -value,  $\alpha_1$ , as a function of  $\beta$ :

$$\alpha_1 = \frac{(3-2\beta)}{(5-4\beta)} \tag{11}$$

which increases monotonically:  $3/5 \le \alpha_1 \le 1$ ;  $\alpha_1$  depends only on  $\beta$  and does not depend on the geometric parameters of the configuration. It follows from Eq.(11) that the minimum value of  $\alpha$  is at  $\beta = 0$  and is given by 0.6.

Consequently, a non-vanishing  $\ell=0$  distortion of the plasma surface is needed in the case of minimizing  $\delta_1^4$ , Eq.(6), with respect to n and  $\alpha$  at arbitrary  $\beta$ . Using the minimizing functions  $\bowtie_1$  and  $n_1$ , the ratio of the  $\ell=2$  distortion to the  $\ell=0$  distortion is then

$$\delta_2/\delta_0 = 2(1-\beta)/(2-\beta)$$
.

We see from this formula that the  $\ell=0,2$  distortions are approximately of the same magnitude for small  $\beta$  (e.g. for  $\beta=0.1$ :  $\delta_2/\delta_0=0.94$ ), and that the ratio  $\delta_2/\delta_0$  decreases monotonically to small values with increasing  $\beta$  (e.g. for  $\beta=0.9$ :  $\delta_2/\delta_0=0.18$ ).

Inserting in Eq.(6) the minimizing functions  $n_1$  and  $\alpha_1$ , one gets for  $\delta_1$ 

$$S_{1,n\alpha} = D_{n\alpha} \mathcal{H}^{3}/A^{1/2}$$
 (12)

$$D_{n \alpha} = D_n \alpha_1^{1/4} \tag{13}$$

(the index  $\pi\alpha$  indicates minimization with respect to n and  $\alpha$ ).

The function  $D_{\eta\alpha}$  is infinite for  $\beta=0,1$  and has a minimum value of 1.62 for  $\beta=0.83=\beta_0$ .

 $\delta_2/\delta_0$  for this minimizing  $\beta_0$  - value is 0.31. The minimum values of the functions  $D_n(\alpha=1)$  and  $D_{n\alpha}(\alpha=\alpha_1)$  differ little from each other (Fig.1). The fact that  $D_{n\alpha}$  varies slowly below  $\beta_0=0.83$  is important; therefore, the final scaling law (shown in Fig.3) hardly changes if a  $\beta$ -value different from the optimum value  $\beta_0$  is used  $\alpha_1/\beta_0=0.8=0.8=0.8$ 

The final scaling of  $\delta_1$  after minimization with respect to  $n_{\mbox{\scriptsize ,}\alpha}$  , ß is

$$\delta_{1, \eta \alpha \beta} = 1.62 \ \chi^{3} / A^{1/2} \,. \tag{14}$$

Let us now express  $n = n(A; \delta_{1, n \alpha \beta})$ . Fig. 3 then represents n = n(A) for different choises of  $\delta_{1, n \alpha \beta}$ . The stable A, n-region for the m=1, k=0 mode lies below these curves.

The  $\ell = 0, 2$  distortions have to be calculated from (2), (3), and are given by

$$(\delta_{o} \delta_{1})_{n \alpha} = d_{o} \mathcal{H}^{4}/A$$
,  $d_{o}(\beta) = D_{o} \alpha_{1}$ ,  $d_{o}(0.83) = 2.79$ ,

$$(S_2 S_1)_{n\alpha} = D_2 n^4/A$$
,  $D_2(\beta) = \frac{3(4-3\beta)}{4\beta(5-4\beta)}$ ,  $D_2(0.83) = 0.81$ .

The functions  $d_0$  and  $D_2$  are shown in Fig. 2. For the optimum case of  $\beta_0=0.83$ , the  $\ell=0$  distortion is roughly three times as large as the  $\ell=2$  distortion. If the  $\beta$ -value is increased above the optimum value  $\beta_0$ , the  $\ell=0$  distortion increases, while the  $\ell=2$  distortion decreases. If the  $\beta$ -value is decreased below the optimum  $\beta_0$ ,  $0.5 \pm \beta \pm \beta_0$ , the  $\ell=0$  distortion decreases and the  $\ell=2$  distortion increases, both slowly. The  $\ell=2$  distortion is always smaller than the  $\ell=0$  distortion.

#### II.3. Limiting curves for non-shaped vessel

Up to now we have minimized the  $\ell=1$  distortion of the plasma surface and have found the  $(\int_{1}^{\ell} A, \mathcal{K})$  triplets for the marginal stability of the m=1, k=0 mode. We now describe the conditions under which a smooth toroidal vacuum vessel or a helically shaped vessel is needed in order to produce a toroidal high- $\beta$  equilibrium with superimposed  $\ell=0,1,2$  fields which is wall-stabilized with respect to the m=1, k=0 mode.

The limiting curve in the A, n-diagram is to be calculated from the assumption that the distorted plasma column should lie within a non-shaped vessel, this fact being stated by

where  $r_{V}$  is the mean radius of the vessel and  $\Delta a$  is the total plasma distortion (for the estimate it is enough to take into account the  $\ell=1$  distortion). Inserting the non-dimensional parameters we get the relation

$$\delta_1 \leq \kappa \nu - 1 \tag{16}$$

where  $v = r_v/b$  is a measure of the wall thickness of the vessel; Eq.(16) gives the admissible  $\delta_1$  values as functions of  $\kappa$  for the case of a non-shaped vessel. Using Eq.(14)(i.e.  $\alpha = \alpha_o$ ) we get the limiting curve in the A, $\kappa$  - diagram:

$$A_1 = \frac{\chi^6 D^2}{(\nu \chi - 1)^2}$$
 (17)

with D = 1.62.

The limiting curve is shown in Fig.3: the curve (i) represents V = 1,  $\alpha = \alpha_0$ ; the curve (ii) represents V = 0.8,  $\alpha = \alpha_0$  which is more realistic.

The region to the right-hand side of the limiting curve is admissible if a non-shaped vessel is used. A depends strongly on  $\nu$ .

### III. CONCLUSIONS

The scaling of an m=1 wall-stabilized high- $\beta$  stellarator is discussed on the basis of the surface-current model. Scaling laws and curves in terms of the aspect ratio A, compression ratio  $\alpha$ , helical distortions  $\delta_{\ell}$  ( $\ell=0,1,2$ ), and  $\beta$  are given. The minimization of the  $\ell=1$  distortion of the plasma surface in the case of marginal stability was performed with respect to the number of periods (n) around the torus, the amplitudes of the helical  $\ell=0$  and  $\ell=2$  corrugation fields ( $\delta_0$ ,  $\delta_2$ ), and  $\delta$ . After minimization a possible choice of these parameters is  $\delta_0=0.21$ ,  $\delta_0=0.21$ ,  $\delta_0=0.07$ , where wall stabilization of the m=1, k=0 mode is effective.

In the case of no  $\ell=2$  distortion ( $\alpha=1$ ), the optimum  $\beta$ -value is  $\beta=0.86$  and the resulting scaling law is  $\delta_{1,\eta\beta}=1.71\,\mu^3/\Lambda^{1/2}$ , the number of periods is  $n_1=0.63\,\Lambda/\mu^2$ .

In the case of  $\alpha=\alpha_0$  ( $\ell=0,1,2$  corrugation fields), the optimum  $\beta$ -value is  $\beta_0=0.83$  and the resulting scaling law is  $\delta_{1,n\beta}=1.62 \, \frac{3}{4} \, \frac{1}{2}$  ( $\alpha_0=0.8$ ). The corresponding number of periods  $\alpha_0=0.66$  A/ $\alpha_0=0.66$  A/ $\alpha_0=0.66$  A/ $\alpha_0=0.86$  A/ $\alpha_$ 

In all cases of practical interest (A not to large) it is necessary to use a vacuum vessel which has a helical-toroidal shape.

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# Figure Captions

- Fig. 1: a) Function  $D_n = \left[ \frac{27(4-3\beta)^2}{(2-\beta)} \left( \frac{3}{64\beta^3} \left( \frac{3}{1-\beta} \right) \left( \frac{3-2\beta}{4} \right) \right]^{1/4}$  describing the  $\ell = 1$  ( $\ell = 1$ ) distortion  $\delta_{1,n} = \left( \frac{3}{2} \right) \sqrt{A} D_n$ .
  - b) Function  $D_{n\alpha} = D_n \left[ (3-2\beta) / (5-4\beta) \right]^{1/4}$ describing the  $\ell = 1$  ( $\alpha = \alpha_1$ ) distortion  $\delta_{1,n\alpha} = (\alpha^3 / \sqrt{A}) D_{n\alpha}$ .
- Fig.2: a) Function  $D_0 = 3(4-3\beta) (2-\beta)/8\beta(1-\beta) (3-2\beta)$  describing the  $\ell = 0$  distortion in the case of  $\alpha = 1$ :  $(\delta_0 \delta_1)_n = (\kappa^4/A) D_0$  (dashed curve optimized with respect to n).
  - b) Function  $d_0 = D_0(3-2\beta)/(5-4\beta)$  describing the  $\ell = 0$  distortion in case of  $\alpha = \alpha_1 : (\delta_0 \delta_1)_{n\alpha} = (\alpha^4/A) d_0$  (slight curve; optimized with respect to  $n, \alpha$ ).
    - c) Function  $D_2 = 3(4-3\beta)/4\beta(5-4\beta)$  describing the  $\ell=2$  distortion in case of  $\alpha = \alpha_1$ :  $(\delta_2\delta_1)_{n\alpha} = (\kappa^4/A)D_2$  (bold curve; optimized with respect to  $\alpha$ ,  $\alpha$ ). In all three cases  $\delta_1$  is parameter.
- Fig.3: Scaling law for marginal stability of the m=1, k=0 mode (rigid displacement; A aspect ratio with respect to plasma radius;  $\delta_1$  optimum  $\ell=1$  distortion).





