

Research Article

Analysis of Unsteady Axisymmetric Squeezing Fluid Flow with Slip and No-Slip Boundaries Using OHAM

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In this manuscript, An unsteady axisymmetric flow of nonconducting, Newtonian fluid squeezed between two circular plates is studied with slip and no-slip boundaries. Using similarity transformation, the system of nonlinear partial differential equations is reduced to a single fourth order ordinary differential equation. The resulting boundary value problems are solved by optimal homotopy asymptotic method (OHAM) and fourth order explicit Runge-Kutta method (RK4). It is observed that the results obtained from OHAM are in good agreement with numerical results by means of residuals. Furthermore, the effects of various dimensionless parameters on the velocity profiles are investigated graphically.

1. Introduction

The squeezing of an incompressible viscous fluid between two parallel plates is an essential type of flow that is frequently observed in many hydro dynamical tools and machines. In food industries, squeezing flows have several applications particularly in chemical engineering [1, 2]. Compression and injection molding, polymer processing, and modeling of lubrication system are some practical examples of squeezing flows. The modeling and analysis of squeezing flow has started in nineteenth century and continues to receive significant attention due to its vast applications in biophysical and physical sciences. The initial work in squeezing flows has been done by Stefan [3], who developed an ad hoc asymptotic solution of Newtonian fluids. An explicit solution of the squeeze flow, considering inertial terms, has been established by Thorpe and Shaw [4]. However, P. S. Gupta and A. S. Gupta [5] proved that the solution set up by [4] fails to satisfy the boundary conditions. Considering fluid inertia effects, Elkouh [6] studied the squeeze film between two plane annuli. Verma [7] and Singh et al. [8] have conducted Numerical solutions of the squeezing flow between parallel plates. Leider and Bird [9] performed theoretical analysis for squeezing flow of power-law fluid between parallel disks.

Analytic solution for the squeezing flow of viscous fluid between two parallel disks with suction or blowing effect has been proposed by Domairry and Aziz [10]. Islam et al. [11] studied Newtonian squeezing fluid flow in a porous medium channel. Ullah et al. [12] discussed the Newtonian fluid flow with slip boundary condition keeping MHD effect into account. Siddiqui et al. [13] investigated the unsteady squeezing flow of viscous fluid with magnetic field. Apart from the mentioned researchers, other prominent scholars have conducted various theoretical and experimental studies of squeezing flows [14–17].

The difference between fluid and boundary velocity is proportional to the shear stress at the boundary. The dimension of proportionality constant is length, which is known as slip parameter. In fluids with elastic character, slip condition has great importance [18]. It has many applications in medical sciences, for instance, polishing artificial heart valves [19]. There are various situations in which no-slip boundary condition is inappropriate. Some of these situations include polymeric liquids when the weight of molecule is high, flow on multiple interfaces, fluids containing concerted suspensions, and thin film problems. The general boundary condition which shows the fluid slip at the wall was initially proposed by Navier [20]. Recently, Ebaid [21] studied

the effect of magnetic field in Newtonian fluid in an asymmetric channel with wall slip conditions.

Most of scientific incidents are modeled by nonlinear partial or ordinary differential equations. In literature, we have variety of perturbation techniques which can solve nonlinear boundary value problems analytically. But the limitations of these techniques are based on the assumption of small parameters. Detailed review of these methods is given by He [22]. In recent times, the ideas of Homotopy and Perturbation have been combined together. Liao [23] and He [24, 25] have done the primary work in this regard. In series of papers, Marinca with various scholars used OHAM to find the approximate solution of nonlinear differential equations arising in heat transfer, steady flow of a fourth-grade fluid, and thin film flow [26–28].

In this work, OHAM is used to analyze an unsteady squeezing fluid flow between two circular nonrotating disks with slip and no-slip boundary conditions. In addition, movement of the circular plates is considered to be symmetric about the axial line and the fluid is considered to be Newtonian, incompressible and viscous. Sections 2 and 3 include the description and mathematical formulation of the problem. Sections 4, 5, and 6 present the basic theory of OHAM and its application in case of no-slip and slip boundaries. Results and discussions are given in Section 7 while conclusions are mentioned in Section 8.

2. Description of the Problem

The unsteady axisymmetric squeezing flow of incompressible Newtonian fluid with density ρ , viscosity μ and kinematic viscosity ν , squeezed between two circular plates having speed $v_w(t)$ is considered. It is assumed that at any time t , the distance between two circular plates is $2s(t)$. It is also assumed that r -axis is the central axis of the channel while z -axis is taken normal to it. Plates move symmetrically with respect to the central axis $z = 0$ while the flow is axisymmetric about $r = 0$. The longitudinal and normal velocity components in radial and axial directions are $u_r(r, z, t)$ and $u_z(r, z, t)$, respectively. The geometrical interpretation of the problem is given in Figure 1.

3. Mathematical Formulation

The governing equations of motion are

$$\begin{aligned} \nabla \cdot \mathbf{U} &= 0, \\ \rho \left[\frac{\partial \mathbf{U}}{\partial t} + (\mathbf{U} \cdot \nabla) \mathbf{U} \right] &= \rho \mathbf{f} + \nabla \cdot \mathbf{T}, \end{aligned} \quad (1)$$

where

$$\begin{aligned} \mathbf{T} &= -p\mathbf{I} + \mu \mathbf{A}_1, \\ \mathbf{A}_1 &= \nabla \mathbf{U} + (\nabla \mathbf{U})^t, \end{aligned} \quad (2)$$

and \mathbf{U} is the velocity vector, p is the pressure, \mathbf{f} is the body force, \mathbf{T} is the Cauchy stress tensor, \mathbf{A}_1 is the Rivlin-Ericksen

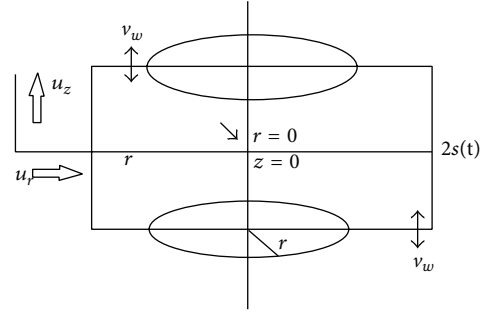


FIGURE 1: Geometrical interpretation of the problem.

tensor, and μ is the coefficient of viscosity. Now we formulate the unsteady two-dimensional flow. Let us assume that

$$\mathbf{U} = [u_r(r, z, t), 0, u_z(r, z, t)], \quad (3)$$

and introduce the vorticity function $\Omega(r, z, t)$ and generalized pressure $h(r, z, t)$ as

$$\Omega(r, z, t) = \frac{\partial u_z}{\partial r} - \frac{\partial u_r}{\partial z}, \quad (4)$$

$$h(r, z, t) = \frac{\rho}{2} [u_r^2 + u_z^2] + p. \quad (5)$$

Equations (1) are reduced to

$$\frac{\partial u_r}{\partial r} + \frac{u_r}{r} + \frac{\partial u_z}{\partial z} = 0,$$

$$\frac{\partial h}{\partial r} + \rho \left(\frac{\partial u_r}{\partial t} - u_z \Omega \right) = -\mu \frac{\partial \Omega}{\partial z}, \quad (6)$$

$$\frac{\partial h}{\partial z} + \rho \left(\frac{\partial u_z}{\partial t} + u_r \Omega \right) = \frac{\mu}{r} \frac{\partial}{\partial r} (r\Omega).$$

The boundary conditions on $u_r(r, z, t)$ and $u_z(r, z, t)$ are

$$\begin{aligned} u_r(r, z, t) &= 0, \quad u_z(r, z, t) = v_w(t) \quad \text{at } z = s \\ \frac{\partial}{\partial z} u_r(r, z, t) &= 0, \quad u_z(r, z, t) = 0 \quad \text{at } z = 0, \end{aligned} \quad (7)$$

where $v_w(t) = ds/dt$ is the velocity of the plates. The boundary conditions (7) are due to symmetry at $z = 0$ and no-slip at the upper plate when $z = s$. If we introduce the dimensionless parameter

$$\eta = \frac{z}{s(t)}. \quad (8)$$

Equations (4) and (6) transforms to

$$\Omega(r, z, t) = \frac{\partial u_z}{\partial r} - \frac{1}{s} \frac{\partial u_r}{\partial \eta}, \quad (9)$$

$$\frac{\partial u_r}{\partial r} + \frac{u_r}{r} + \frac{1}{s} \frac{\partial u_z}{\partial \eta} = 0, \quad (10)$$

$$\frac{\partial h}{\partial r} + \rho \left(\frac{\partial u_r}{\partial t} - u_z \Omega \right) = -\frac{\mu}{s} \frac{\partial \Omega}{\partial \eta}, \quad (11)$$

$$\frac{1}{s} \frac{\partial h}{\partial \eta} + \rho \left(\frac{\partial u_z}{\partial t} + u_r \Omega \right) = \frac{\mu}{r} \frac{\partial}{\partial r} (r\Omega). \quad (12)$$

The boundary conditions on u_r and u_z are

$$\begin{aligned} u_r = 0, \quad u_z = v_w(t) \quad \text{at } \eta = 1 \\ \frac{\partial u_r}{\partial \eta} = 0, \quad u_z = 0 \quad \text{at } \eta = 0. \end{aligned} \quad (13)$$

After eliminating the generalized pressure between (11) and (12), we obtained

$$\rho \left[\frac{\partial \Omega}{\partial t} + u_r \frac{\partial \Omega}{\partial r} + \frac{u_z}{s} \frac{\partial \Omega}{\partial \eta} - \frac{u_r}{r} \Omega \right] = \mu \left[\nabla^2 \Omega - \frac{\Omega}{r^2} \right], \quad (14)$$

where ∇^2 is the Laplacian operator.

Defining velocity components as [5]

$$\begin{aligned} u_r = -\frac{r}{2s(t)} v_w(t) g'(\eta), \\ u_z = v_w(t) g(\eta) \end{aligned} \quad (15)$$

we see that (10) is identically satisfied and (14) becomes

$$\frac{d^4 g}{d\eta^4} + R \left[(\eta - g) \frac{d^3 g}{d\eta^3} + 2 \frac{d^2 g}{d\eta^2} \right] - Q \frac{d^2 g}{d\eta^2} = 0, \quad (16)$$

where

$$R = \frac{sv_w}{v}, \quad Q = \frac{s^2}{vv_w} \frac{dv_w}{dt}. \quad (17)$$

Here both R and Q are functions of t but we consider R and Q constants for similarity solution. Since $v_w = ds/dt$, Integrate first equation of (17), we get

$$s(t) = (Wt + S)^{1/2}, \quad (18)$$

where W and S are constants. The plates move away from each other symmetrically with respect to η when $W > 0$ and $S > 0$. Also the plates approach to each other and squeezing flow exists with similar velocity profiles when $W < 0$, $S > 0$, and $s(t) > 0$. From (17) and (18) it follows that $Q = -R$. Then (16) becomes

$$\frac{d^4 g}{d\eta^4} + R \left[(\eta - g) \frac{d^3 g}{d\eta^3} + 3 \frac{d^2 g}{d\eta^2} \right] = 0. \quad (19)$$

Using (13) and (15) we determine the boundary conditions in case of no-slip and slip at the upper plate as follows:

$$\begin{aligned} g(1) = 1, \quad g'(1) = 0 \\ g(0) = 0, \quad g''(0) = 0 \end{aligned} \quad \text{(No-slip at the wall)} \quad (20)$$

$$\begin{aligned} g(1) = 1, \quad g'(1) = \gamma g''(1) \\ g(0) = 0, \quad g''(0) = 0 \end{aligned} \quad \text{(Slip at the wall)}. \quad (21)$$

4. Basic Theory of OHAM [26, 29–32]

Let us apply OHAM to the following differential equation:

$$\mathfrak{F}[v(x)] + f(x) + \aleph[v(x)] = 0, \quad B\left(v, \frac{dv}{dx}\right) = 0, \quad (22)$$

where x represents an independent variable, $v(x)$ is unknown function and $f(x)$ is known function. B , \aleph , \mathfrak{F} are boundary, nonlinear, and linear operators, respectively.

According to OHAM, we construct Homotopy $\Phi(x, p)$: $\mathbb{R} \times [0, 1] \rightarrow \mathbb{R}$ which satisfies

$$\begin{aligned} (1-p) [\mathfrak{F}(\Phi(x, p)) + f(x)] \\ = h(p) [\mathfrak{F}(\Phi(x, p)) + f(x) + \aleph(\Phi(x, p))], \\ B\left(\Phi(x, p), \frac{\partial \Phi(x, p)}{\partial x}\right) = 0, \end{aligned} \quad (23)$$

where $x \in \mathbb{R}$ and $p \in [0, 1]$ is an embedding parameter, $h(p)$ is a nonlinear auxiliary function for $p \neq 0$, $h(0) = 0$ and $\Phi(x, p)$ is an unknown function. Clearly, when $p = 0$ and $p = 1$, it holds that $\Phi(x, 0) = v_0(x)$ and $\Phi(x, 1) = \tilde{v}(x)$, respectively.

Thus, as p varies from 0 to 1, the solution $\Phi(x, p)$ approaches from $v_0(x)$ to $\tilde{v}(x)$.

We choose the auxiliary function $h(p)$ in the form of

$$h(p) = \sum_{k=0}^m p^k C_k, \quad (24)$$

where C_k are convergence controlling constants to be determined.

To obtain an approximate solution, we expand $\Phi(x, p, C_i)$ in a Taylor series about p as follows:

$$\Phi(x, p, C_i) = v_0(x) + \sum_{k=1}^m v_k(C_1, C_2, \dots, C_k) p^k. \quad (25)$$

Substituting (25) into (23) and equating the coefficients of like powers of p , we obtain the following equations.

The zeroth-order problem is

$$\mathfrak{F}[v_0(x)] + f(x) = 0, \quad B\left(v_0, \frac{dv_0}{dx}\right) = 0. \quad (26)$$

First-order problem is

$$\mathfrak{F}[v_1(x)] + f(x) = C_1 \aleph_0[v_0(x)], \quad B\left(v_1, \frac{dv_1}{dx}\right) = 0. \quad (27)$$

Second-order problem is

$$\begin{aligned} \mathfrak{F}[v_2(x)] + \mathfrak{F}[v_1(x)] \\ = C_2 \aleph_0[v_0(x)] + C_1 \{\mathfrak{F}[v_1(x)] + \aleph_1[v_0(x), v_1(x)]\}, \\ B\left(v_2, \frac{dv_2}{dx}\right) = 0. \end{aligned} \quad (28)$$

The general equations for $v_k(x)$ are given by

$$\begin{aligned} & \mathfrak{F}[v_k(x)] - \mathfrak{F}[v_{k-1}(x)] \\ &= C_1 \aleph_0[v_0(x)] \\ &+ \sum_{i=1}^{k-1} C_i \{ \mathfrak{F}[v_{k-i}(x)] \\ &+ \aleph_{k-i}[v_0(x), v_1(x), \dots, v_{k-1}(x)] \}, \\ & B\left(v_k, \frac{dv_k}{dx}\right) = 0, \\ & k = 2, 3, \dots, \end{aligned} \quad (29)$$

where the coefficient of p^m in the expansion of $\aleph(\Phi(x, p))$ about p is $\aleph_m[v_0(x), v_1(x), \dots, v_{m-1}(x)]$.

$$\begin{aligned} & \aleph(\Phi(x, p, C_i)) \\ &= \aleph_0[v_0(x)] + \sum_{m=1}^m \aleph_m[v_0(x), v_1(x), \dots, v_{m-1}(x)] p^m. \end{aligned} \quad (30)$$

It is noted that the convergence of the series (25) depends upon C_k . For convergence at $p = 1$, the m th order approximation \tilde{v} is

$$\tilde{v}(x, C_1, C_2, \dots, C_m) = v_0(x) + \sum_{j=1}^m v_j(x, C_1, C_2, \dots, C_j). \quad (31)$$

Substituting (31) in (22), the expression for residual is

$$\begin{aligned} & \mathfrak{R}(x, C_1, C_2, \dots, C_m) \\ &= \mathfrak{F}[\tilde{v}(x, C_1, C_2, \dots, C_m)] + f(x) \\ &+ \aleph[\tilde{v}(x, C_1, C_2, \dots, C_m)]. \end{aligned} \quad (32)$$

If $\mathfrak{R} = 0$, then \tilde{v} will be the exact solution but usually this does not happen in nonlinear problems.

There are various methods to find the optimal values of C_i , $i = 1, 2, \dots$. We apply the method of least square and Galerkin's method in the following manner:

In method of least square

$$J(x, C_1, C_2, \dots, C_m) = \int_a^b \mathfrak{R}^2(x, C_1, C_2, \dots, C_m) dx. \quad (33)$$

Minimizing $J(x, C_1, C_2, \dots, C_m)$, we have

$$\frac{\partial J}{\partial C_i} = 0, \quad i = 1, 2, \dots, m. \quad (34)$$

In Galerkin's method, we solve the following system for C_i ($i = 1, 2, \dots, m$):

$$\int_a^b \mathfrak{R} \frac{\partial \tilde{v}}{\partial C_i} dx = 0, \quad i = 1, 2, \dots, m. \quad (35)$$

To find appropriate C_i ($i = 1, 2, \dots, m$), we choose a and b in the domain of the problem. Approximate solution of order m is well-determined with these known constants.

5. Application of OHAM in Case of No-Slip Boundary

Using (19) and (20) various order problems are as follows:
Zeroth-order problem

$$\begin{aligned} & v_0^{(iv)}(\eta) = 0, \\ & v_0(0) = 0, \quad v_0''(0) = 0, \quad v_0(1) = 1, \quad v_0'(1) = 0. \end{aligned} \quad (36)$$

First-order problem

$$\begin{aligned} & v_1^{(iv)}(\eta) = 3C_1 R v_0''(\eta) + C_1 R \eta v_0'''(\eta) - C_1 R v_0(\eta) v_0'''(\eta) \\ &+ v_0^{(iv)}(\eta) + C_1 v_0^{(iv)}(\eta), \\ & v_1(0) = 0, \quad v_1''(0) = 0, \quad v_1(1) = 0, \quad v_1'(1) = 0. \end{aligned} \quad (37)$$

Second-order problem

$$\begin{aligned} & v_2^{(iv)}(\eta) = 3C_1 R v_1''(\eta) - C_1 R v_1(\eta) v_0'''(\eta) + C_1 R \eta v_1'''(\eta) \\ &- C_1 R v_0(\eta) v_1'''(\eta) + v_1^{(iv)}(\eta) + C_1 v_1^{(iv)}(\eta), \\ & v_2(0) = 0, \quad v_2''(0) = 0, \quad v_2(1) = 0, \quad v_2'(1) = 0. \end{aligned} \quad (38)$$

Third-order problem

$$\begin{aligned} & v_3^{(iv)}(\eta) = 3C_1 R v_2''(\eta) - C_1 R v_2(\eta) v_0'''(\eta) \\ &- C_1 R v_1(\eta) v_1'''(\eta) + C_1 R \eta v_2'''(\eta) \\ &- C_1 R v_0(\eta) v_2'''(\eta) + v_2^{(iv)}(\eta) \\ &+ C_1 v_2^{(iv)}(\eta), \\ & v_3(0) = 0, \quad v_3''(0) = 0, \quad v_3(1) = 0, \quad v_3'(1) = 0. \end{aligned} \quad (39)$$

Fourth-order problem

$$\begin{aligned} & v_4^{(iv)}(\eta) = 3C_1 R v_3''(\eta) - C_1 R v_3(\eta) v_0'''(\eta) \\ &- C_1 R v_2(\eta) v_1'''(\eta) - C_1 R v_1(\eta) v_2'''(\eta) \\ &+ C_1 R \eta v_3'''(\eta) - C_1 R v_0(\eta) v_3'''(\eta) \\ &+ v_3^{(iv)}(\eta) + C_1 v_3^{(iv)}(\eta), \\ & v_4(0) = 0, \quad v_4''(0) = 0, \quad v_4(1) = 0, \quad v_4'(1) = 0. \end{aligned} \quad (40)$$

By considering fourth-order solution, we have

$$\tilde{v}(\eta) = v_0(\eta) + v_1(\eta) + v_2(\eta) + v_3(\eta) + v_4(\eta). \quad (41)$$

The residual of the problem is

$$\mathfrak{R} = \frac{d^4 \tilde{v}(\eta)}{d\eta^4} + R \left[(\eta - \tilde{v}(\eta)) \frac{d^3 \tilde{v}(\eta)}{d\eta^3} + 3 \frac{d^2 \tilde{v}(\eta)}{d\eta^2} \right]. \quad (42)$$

We apply Galerkin's method to find constant C_1 as follows:

$$\int_0^1 \Re \frac{\partial \bar{v}}{\partial C_1} dx = 0. \quad (43)$$

Solving (43) and keeping $R = 0.1$, we get

$$C_1 = 1.01328. \quad (44)$$

Using above value of C_1 , the approximate solution is

$$\begin{aligned} \bar{v}(\eta) = & \frac{1}{2} (3\eta - \eta^3) \\ & + \frac{1}{560} (3.74914\eta - 7.39694\eta^3 + 3.54648\eta^5 \\ & \quad + 0.101328\eta^7) \\ & + \frac{1}{776160} (95.6941\eta - 430.222\eta^3 + 514.14\eta^5 \\ & \quad - 122.33\eta^7 - 55.3411\eta^9 - 1.94053\eta^{11}) \\ & + \frac{1}{565045} (2544.14\eta + 14364.4\eta^3 - 37116.4\eta^5 \\ & \quad + 25023.2\eta^7 - 8133.38\eta^9 + 2599.01\eta^{11} \\ & \quad + 696.10\eta^{13} + 22.962\eta^{15}) \\ & + \frac{1}{722737} (1.53702\eta - 1.87989 \times 10^8 \eta^3 \\ & \quad + 1.93991 \times 10^8 \eta^5 + 8.28837 \times 10^7 \eta^7 \\ & \quad - 8.03587 \times 10^7 \eta^9 - 2.92844 \times 10^7 \eta^{11} \\ & \quad + 1.67506 \times 10^7 \eta^{13} - 9.66217 \times 10^6 \eta^{15} \\ & \quad - 1.6529 \times 10^6 \eta^{17} - 48038.9\eta^{19}). \end{aligned} \quad (45)$$

6. Application of OHAM in Case of Slip Boundary

Using (19) and (21) different order problems are as follows. Zeroth-order problem

$$\begin{aligned} u_0^{(iv)}(\eta) &= 0, \\ u_0(0) = 0, \quad u_0''(0) = 0, \quad u_0(1) = 1, \quad u_0'(1) &= \gamma u_0''(1). \end{aligned} \quad (46)$$

First-order problem

$$\begin{aligned} u_1^{(iv)}(\eta) &= 3C_1 R u_0''(\eta) + C_1 R \eta u_0'''(\eta) - C_1 R u_0(\eta) u_0'''(\eta) \\ & \quad + u_0^{(iv)}(\eta) + C_1 u_0^{(iv)}(\eta), \\ u_1(0) = 0, \quad u_1''(0) = 0, \quad u_1(1) = 0, \quad u_1'(1) &= \gamma u_1''(1). \end{aligned} \quad (47)$$

Second-order problem

$$\begin{aligned} u_2^{(iv)}(\eta) &= 3C_1 R u_1''(\eta) - C_1 R u_1(\eta) u_0'''(\eta) \\ & \quad + C_1 R \eta u_1'''(\eta) - C_1 R u_0(\eta) u_1'''(\eta) \\ & \quad + u_1^{(iv)}(\eta) + C_1 u_1^{(iv)}(\eta), \\ u_2(0) = 0, \quad u_2''(0) = 0, \quad u_2(1) = 0, \quad u_2'(1) &= \gamma u_2''(1). \end{aligned} \quad (48)$$

Third-order problem

$$\begin{aligned} u_3^{(iv)}(\eta) &= 3C_1 R u_2''(\eta) - C_1 R u_2(\eta) u_0'''(\eta) \\ & \quad - C_1 R u_1(\eta) u_1'''(\eta) + C_1 R \eta u_2'''(\eta) \\ & \quad - C_1 R u_0(\eta) u_2'''(\eta) + u_2^{(iv)}(\eta) \\ & \quad + C_1 u_2^{(iv)}(\eta), \\ u_3(0) = 0, \quad u_3''(0) = 0, \quad u_3(1) = 0, \quad u_3'(1) &= \gamma u_3''(1). \end{aligned} \quad (49)$$

Fourth-order problem

$$\begin{aligned} u_4^{(iv)}(\eta) &= 3C_1 R u_3''(\eta) - C_1 R u_3(\eta) u_0'''(\eta) \\ & \quad - C_1 R u_2(\eta) u_1'''(\eta) - C_1 R u_1(\eta) u_2'''(\eta) \\ & \quad + C_1 R \eta u_3'''(\eta) - C_1 R u_0(\eta) u_3'''(\eta) \\ & \quad + u_3^{(iv)}(\eta) + C_1 u_3^{(iv)}(\eta), \\ u_4(0) = 0, \quad u_4''(0) = 0, \quad u_4(1) = 0, \quad u_4'(1) &= \gamma u_4''(1). \end{aligned} \quad (50)$$

By considering fourth-order solution, we have

$$\tilde{u}(\eta) = \sum_{i=0}^4 u_i(\eta, C_1). \quad (51)$$

The residual of the problem is

$$\zeta = \frac{d^4 \tilde{u}(\eta)}{d\eta^4} + R \left[(\eta - \tilde{u}(\eta)) \frac{d^3 \tilde{u}(\eta)}{d\eta^3} + 3 \frac{d^2 \tilde{u}(\eta)}{d\eta^2} \right]. \quad (52)$$

We apply Galerkin's method to find constant C_1 as follows:

$$\int_0^1 \zeta \frac{\partial \tilde{u}}{\partial C_1} dx = 0. \quad (53)$$

Solving (53) and taking $R = 0.2$ and $\gamma = 1$, we get

$$C_1 = -1.06872. \quad (54)$$

TABLE 1: OHAM solutions along with residuals for various R in case of no-slip boundary.

η	$R = 0.1$		$R = 0.3$		$R = 0.5$	
	Solution	Residual	Solution	Residual	Solution	Residual
0.0	0.	0.	0.	0.	0.	0.
0.1	0.150158	5.37334×10^{-11}	0.151534	-6.69283×10^{-9}	0.152999	-6.23412×10^{-8}
0.2	0.297237	3.14675×10^{-10}	0.299827	1.66025×10^{-9}	0.302582	6.58388×10^{-8}
0.3	0.438170	8.51847×10^{-10}	0.441661	2.33504×10^{-8}	0.445373	3.42092×10^{-7}
0.4	0.569900	1.51431×10^{-9}	0.573869	3.93945×10^{-8}	0.578082	4.93942×10^{-7}
0.5	0.689397	1.90824×10^{-9}	0.693354	2.81614×10^{-8}	0.697548	2.42092×10^{-7}
0.6	0.793661	1.33301×10^{-9}	0.797122	-3.19654×10^{-8}	0.800780	-6.53046×10^{-7}
0.7	0.879734	-1.59255×10^{-9}	0.882300	-2.21911×10^{-7}	0.885004	-3.23415×10^{-6}
0.8	0.944705	-1.02814×10^{-8}	0.946167	-8.84707×10^{-7}	0.947702	-1.2206×10^{-5}
0.9	0.985722	-3.446×10^{-8}	0.986180	-3.21268×10^{-6}	0.986659	-4.41008×10^{-5}
1.0	1.	-1.03509×10^{-7}	1.	-1.11826×10^{-5}	1.	-1.54022×10^{-4}

Using above value of C_1 , the approximate solution is

$$\begin{aligned}
\tilde{u}(\eta) = & \frac{1}{2} (3\eta + \eta^3) \\
& + \frac{1}{4480} (-113.284\eta + 151.758\eta^3 - 38.9012\eta^5 \\
& \quad + 0.427486\eta^7) \\
& + \frac{1}{248372} (-156189.\eta + 273825.\eta^3 - 160808.\eta^5 \\
& \quad + 45952.6\eta^7 - 2814.27\eta^9 + 34.5387\eta^{11}) \\
& + \frac{1}{723257} (-9.83844\eta + 1.149 \times 10^8 \eta^3 \\
& \quad - 3.35388 \times 10^7 \eta^5 + 4.04185 \times 10^7 \eta^7 \\
& \quad - 2.68964 \times 10^7 \eta^9 + 3.65673 \times 10^6 \eta^{11} \\
& \quad - 157538.\eta^{13} + 1724.2\eta^{15}) \\
& + \frac{1}{370042} (-1.97195 \times 10^{13} \eta + 4.25372 \times 10^{13} \eta^3 \\
& \quad - 2.94213 \times 10^{13} \eta^5 + 6.06765 \times 10^{12} \eta^7 \\
& \quad - 1.39445 \times 10^{12} \eta^9 + 2.47846 \times 10^{12} \eta^{11} \\
& \quad - 5.97188 \times 10^{11} \eta^{13} + 5.08263 \times 10^{10} \eta^{15} \\
& \quad - 1.62422 \times 10^9 \eta^{17} + 1.52182 \times 10^7 \eta^{19}). \tag{55}
\end{aligned}$$

7. Results and Discussions

In this article we considered the unsteady axisymmetric flow of nonconducting, incompressible Newtonian fluid between two circular plates. The resulting nonlinear boundary value problems are solved with OHAM and fourth-order Runge-Kutta method using Mathematica 7.0.

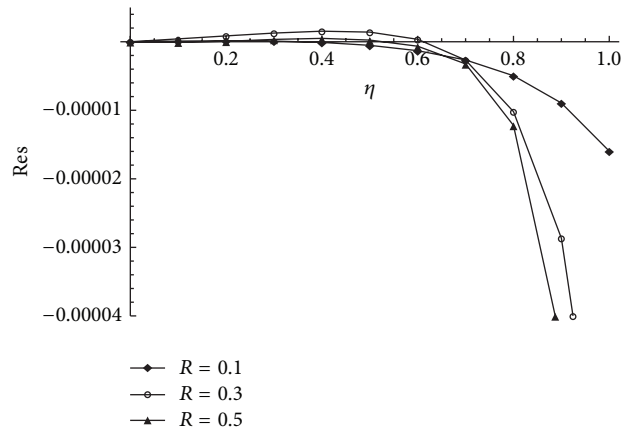


FIGURE 2: OHAM residuals at various values of R in case of no-slip boundary.

Tables 1, 3, and 5 reflect OHAM solutions along with residuals in case of no-slip and slip boundaries for various values of Reynolds number R and slip parameter γ . Also, Tables 2, 4, and 6 represent RK4 solutions along with residuals in case of no-slip and slip boundaries for various values of R and γ . All the tables demonstrate that results obtained using OHAM are in agreement with RK4 by means of residuals. In addition to above mentioned tables, Table 7 shows the comparison of solutions obtained from OHAM and RK4 for various values of Reynolds number R .

Furthermore, Figures 2, 3, and 4 indicate the OHAM residuals in case of no-slip and slip boundaries for various values of R and γ .

The effect of Reynolds number R on velocity profiles in case of no-slip boundary is shown in Figure 5. In these profiles we varied R as $R = 0.1, 1, 2, 3$ and observed that the normal velocity is increased with the increase of Reynolds number (Figure 5(a)). It is also noted that the normal velocity monotonically increases from $\eta = 0$ to $\eta = 1$ for fixed positive value of R at a given time. Figure 5(b) describes the impact of R on the longitudinal velocity in case of no-slip boundary. It

TABLE 2: RK4 solutions along with residuals for various R in case of no-slip boundary.

η	$R = 0.1$		$R = 0.3$		$R = 0.5$	
	Solution	Residual	Solution	Residual	Solution	Residual
0.0	0.	2.88535×10^{-7}	0.	9.66906×10^{-5}	0.	5.30549×10^{-4}
0.1	0.150158	3.88278×10^{-8}	0.151534	5.71393×10^{-6}	0.152999	3.04600×10^{-5}
0.2	0.297237	-9.97789×10^{-9}	0.299827	-1.41434×10^{-6}	0.302582	-7.52772×10^{-6}
0.3	0.438170	2.93767×10^{-9}	0.441661	3.95997×10^{-7}	0.445373	2.10296×10^{-6}
0.4	0.569900	-7.51436×10^{-10}	0.573869	-1.15203×10^{-7}	0.578082	-6.18081×10^{-7}
0.5	0.689397	-4.71705×10^{-10}	0.693354	-9.6761×10^{-9}	0.697548	-2.95916×10^{-8}
0.6	0.793661	2.23004×10^{-9}	0.797122	1.4593×10^{-7}	0.800780	7.14133×10^{-7}
0.7	0.879734	-7.18245×10^{-9}	0.882300	-4.86272×10^{-7}	0.885004	-2.39245×10^{-6}
0.8	0.944705	2.68744×10^{-8}	0.946167	1.77796×10^{-6}	0.947702	8.70664×10^{-6}
0.9	0.985722	-1.11599×10^{-7}	0.986180	-7.28952×10^{-6}	0.986659	3.56157×10^{-5}
1.0	1.	-2.71683×10^{-6}	1.	-1.47695×10^{-4}	1.	6.90088×10^{-4}

TABLE 3: OHAM solutions along with residuals for various values of R in case of slip boundary.

η	$R = 0.2$		$R = 0.3$		$R = 0.4$	
	Solution	Residual	Solution	Residual	Solution	Residual
0.0	0.	0.	0.	0.	0.	0.
0.1	0.072692	3.18345×10^{-8}	0.071220	3.15621×10^{-7}	0.069593	1.74626×10^{-6}
0.2	0.147091	-1.72789×10^{-8}	0.144268	-9.14579×10^{-8}	0.141147	-1.13148×10^{-7}
0.3	0.224893	-1.96995×10^{-7}	0.220953	-1.66461×10^{-6}	0.216599	-7.79061×10^{-6}
0.4	0.307773	-4.94482×10^{-7}	0.303048	-4.29173×10^{-6}	0.297832	-2.07401×10^{-5}
0.5	0.397370	-7.99437×10^{-7}	0.392277	-6.99917×10^{-6}	0.386657	-3.41643×10^{-5}
0.6	0.495283	-8.5784×10^{-7}	0.490289	-7.5499×10^{-6}	0.484784	-3.70689×10^{-5}
0.7	0.603056	-2.1053×10^{-7}	0.598654	-1.91141×10^{-6}	0.593805	-9.6958×10^{-6}
0.8	0.722172	1.87065×10^{-6}	0.718841	1.62936×10^{-5}	0.715176	7.91082×10^{-5}
0.9	0.854042	6.40576×10^{-6}	0.852211	5.59717×10^{-5}	0.850196	2.72708×10^{-4}
1.0	1.	1.46076×10^{-5}	1.	1.27671×10^{-4}	1.	6.22242×10^{-4}

TABLE 4: RK4 solutions along with residuals for various values of R in case of slip boundary.

η	$R = 0.2$		$R = 0.3$		$R = 0.4$	
	Solution	Residual	Solution	Residual	Solution	Residual
0.0	0.	4.12179×10^{-6}	0.	7.56765×10^{-6}	0.	3.62897×10^{-6}
0.1	0.072692	1.74999×10^{-7}	0.071220	2.16125×10^{-7}	0.069593	-3.49994×10^{-7}
0.2	0.147091	-4.21503×10^{-8}	0.144268	-4.97423×10^{-8}	0.141147	9.53266×10^{-8}
0.3	0.224893	1.12883×10^{-8}	0.220953	1.22294×10^{-8}	0.216598	-3.0735×10^{-8}
0.4	0.307773	-3.52272×10^{-9}	0.303048	-4.30187×10^{-9}	0.297832	7.2493×10^{-9}
0.5	0.397370	7.80684×10^{-10}	0.392276	3.06668×10^{-9}	0.386657	8.46409×10^{-9}
0.6	0.495283	1.10391×10^{-9}	0.490289	-5.28586×10^{-9}	0.484783	-3.36828×10^{-8}
0.7	0.603056	-4.35033×10^{-9}	0.598654	1.54159×10^{-8}	0.593805	1.06816×10^{-7}
0.8	0.722172	1.44198×10^{-8}	0.718841	-6.05873×10^{-8}	0.715175	-3.98519×10^{-7}
0.9	0.854042	-5.53933×10^{-8}	0.852211	2.59233×10^{-7}	0.850196	1.65518×10^{-6}
1.0	1.	-1.97434×10^{-7}	1.	7.96168×10^{-6}	1.	3.89126×10^{-5}

is experienced that this component of velocity decreases near the wall but increases near the central axis of the channel.

The effect of Reynolds number R on velocity profiles in case of slip boundary is depicted in Figure 6. In these profiles, we fixed slip parameter $\gamma = 1$ and varied Reynolds number R as $R = 0.2, 0.6, 1, 1.5$. It is noted that the normal velocity decreases as the Reynolds number increases (Figure 6(a)). It is also observed that longitudinal velocity decreases near

the central axis of the channel but increases near the walls when R increases (Figure 6(b)).

Figure 7 demonstrates the effect of slip parameter γ on the velocity profiles. After fixing Reynolds number $R = 0.3$ we varied γ as $\gamma = 0.6, 0.7, 0.8, 1$. We find that normal velocity increases as γ increases. It is also noted that longitudinal velocity decreases near the walls but increases near central axis of the channel.

TABLE 5: OHAM solutions along with residuals for various values of γ in case of slip boundary.

η	$\gamma = 0.5$		$\gamma = 0.6$		$\gamma = 0.7$	
	Solution	Residual	Solution	Residual	Solution	Residual
0.0	0.	0.	0.	0.	0.	0.
0.1	-0.00880011	-1.07933×10^{-6}	0.0336596	-7.54858×10^{-8}	0.0522402	-7.74445×10^{-9}
0.2	-0.010881	-2.2445×10^{-6}	0.0714091	-1.73419×10^{-7}	0.1074223	-2.51485×10^{-8}
0.3	0.000449012	-3.45224×10^{-6}	0.117324	-3.00407×10^{-7}	0.168479	-5.68899×10^{-8}
0.4	0.0318278	-4.41058×10^{-6}	0.175449	-4.32397×10^{-7}	0.238322	-9.8056×10^{-8}
0.5	0.0898133	-4.47787×10^{-6}	0.249785	-5.00627×10^{-7}	0.319832	-1.29675×10^{-7}
0.6	0.18086	-2.60114×10^{-6}	0.344278	-3.77978×10^{-7}	0.415852	-1.13733×10^{-7}
0.7	0.311298	2.65136×10^{-6}	0.462801	1.30706×10^{-7}	0.529175	1.20785×10^{-8}
0.8	0.487312	1.28583×10^{-5}	0.609145	1.28166×10^{-6}	0.662538	3.36724×10^{-7}
0.9	0.714929	2.91822×10^{-5}	0.787012	3.34515×10^{-6}	0.818613	9.67763×10^{-7}
1.0	1.	5.14019×10^{-5}	1.	6.49074×10^{-6}	1.	2.00176×10^{-6}

TABLE 6: RK4 solutions along with residuals for various values of γ in case of slip boundary.

η	$\gamma = 0.5$		$\gamma = 0.6$		$\gamma = 0.7$	
	Solution	Residual	Solution	Residual	Solution	Residual
0.0	0.	2.04594×10^{-5}	0.	7.34794×10^{-6}	0.	3.56291×10^{-6}
0.1	-0.00880012	7.72953×10^{-7}	0.0336596	3.21066×10^{-7}	0.0522402	1.63598×10^{-7}
0.2	-0.0108811	-1.8406×10^{-7}	0.0714091	-7.75305×10^{-8}	0.1074223	-3.96814×10^{-8}
0.3	0.000448983	4.82747×10^{-8}	0.117324	2.08509×10^{-8}	0.168479	1.0753×10^{-8}
0.4	0.0318277	-1.54235×10^{-8}	0.175449	-6.43999×10^{-9}	0.238322	-3.28063×10^{-9}
0.5	0.0898132	5.14031×10^{-9}	0.249785	1.21029×10^{-9}	0.319832	4.50154×10^{-10}
0.6	0.18086	-6.51866×10^{-10}	0.344278	2.64494×10^{-9}	0.415852	1.84079×10^{-9}
0.7	0.311298	-1.86837×10^{-9}	0.462801	-9.88382×10^{-9}	0.529175	-6.51979×10^{-9}
0.8	0.487312	-1.33003×10^{-9}	0.609145	3.37336×10^{-8}	0.662538	2.27322×10^{-8}
0.9	0.714929	2.66400×10^{-8}	0.787012	-1.32232×10^{-7}	0.818613	-9.05714×10^{-8}
1.0	1.	5.55277×10^{-6}	1.	-1.1671×10^{-6}	1.	-1.1767×10^{-6}

TABLE 7: Comparison of OHAM and RK4 solutions for various R in case of slip and no-slip boundary.

η	In case of no-slip boundary [RK4 Solution – OHAM Solution			In case of slip boundary [RK4 Solution – OHAM Solution		
	$R = 0.1$	$R = 0.3$	$R = 0.5$	$R = 0.2$	$R = 0.3$	$R = 0.4$
	0.	0.	0.	0.	0.	0.
0.0	0.	0.	0.	0.	0.	0.
0.1	2.33147×10^{-15}	1.62249×10^{-10}	2.41725×10^{-9}	8.44379×10^{-10}	7.90896×10^{-9}	4.1479×10^{-8}
0.2	9.49241×10^{-14}	3.14228×10^{-10}	4.67809×10^{-9}	1.6672×10^{-9}	1.55832×10^{-8}	8.15527×10^{-8}
0.3	3.82361×10^{-13}	4.46143×10^{-10}	6.63065×10^{-9}	2.44889×10^{-9}	2.28102×10^{-8}	1.18952×10^{-7}
0.4	9.13492×10^{-13}	5.47932×10^{-10}	8.11705×10^{-9}	3.1663×10^{-9}	2.93539×10^{-8}	1.52339×10^{-7}
0.5	1.65451×10^{-12}	6.07476×10^{-10}	8.95202×10^{-9}	3.77514×10^{-9}	3.48026×10^{-8}	1.79574×10^{-7}
0.6	2.42317×10^{-12}	6.09434×10^{-10}	8.91445×10^{-9}	4.18241×10^{-9}	3.8327×10^{-8}	1.96532×10^{-7}
0.7	2.86218×10^{-12}	5.36833×10^{-10}	7.77928×10^{-9}	4.22088×10^{-9}	3.84569×10^{-8}	1.96009×10^{-7}
0.8	2.52039×10^{-12}	3.78563×10^{-10}	5.4278×10^{-9}	3.65208×10^{-9}	3.31085×10^{-8}	1.67861×10^{-7}
0.9	1.20232×10^{-12}	1.54202×10^{-10}	2.18716×10^{-9}	2.24454×10^{-9}	2.02732×10^{-8}	1.02385×10^{-7}
1.0	1.26281×10^{-16}	2.53545×10^{-16}	2.93337×10^{-17}	1.7436×10^{-14}	4.92715×10^{-14}	3.8179×10^{-14}

8. Conclusions

In this article, we find the similarity solution for unsteady axisymmetric squeezing flow of incompressible Newtonian fluid between two circular plates. We observed that the similarity solution exists only when distance between the plates varies as $(Wt + S)^{1/2}$, and squeezing flow occurs when

$W < 0, S > 0$ and $(Wt + S) > 0$. The key findings of the present analysis are as follows:

In case of no-slip at boundary;

- (i) It has been found that increase in Reynolds number R increases the normal velocity.

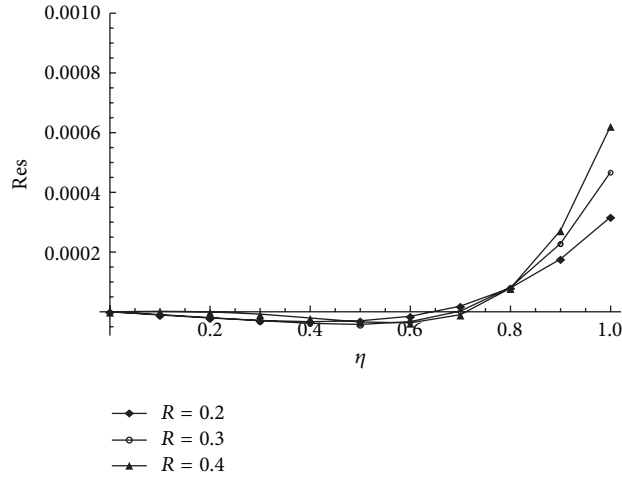


FIGURE 3: OHAM residuals at various values of R in case of slip boundary.

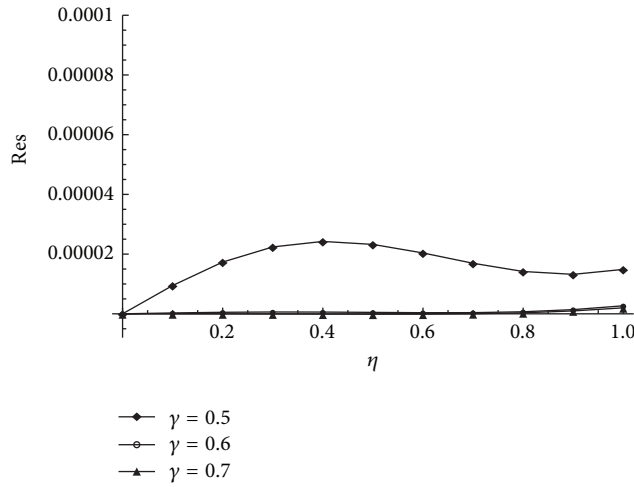


FIGURE 4: OHAM residuals at various values of γ in case of slip boundary.

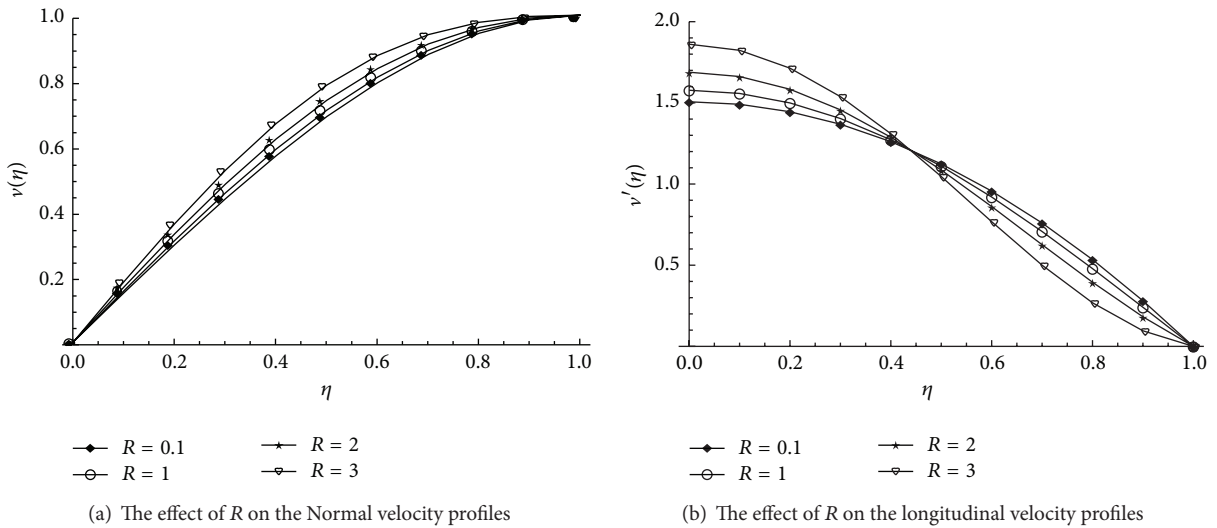


FIGURE 5: Velocity profiles for various values of $R = 0.1, 1, 2, 3$ in case of no-slip boundary.

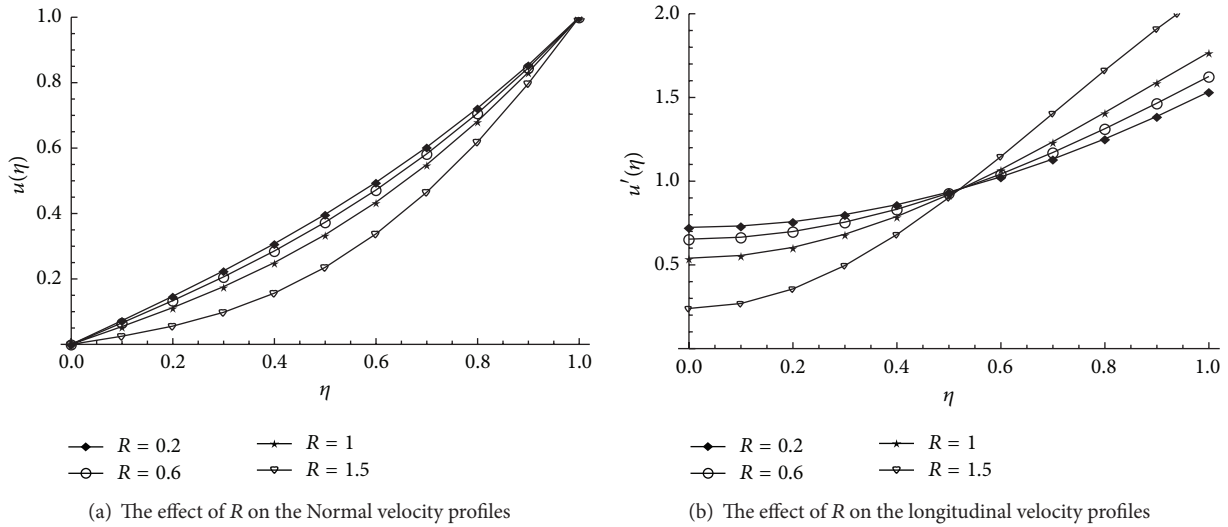


FIGURE 6: Velocity profiles for various values of $R = 0.2, 0.6, 1, 1.5$ fixing $\gamma = 1$ in case of slip boundary.

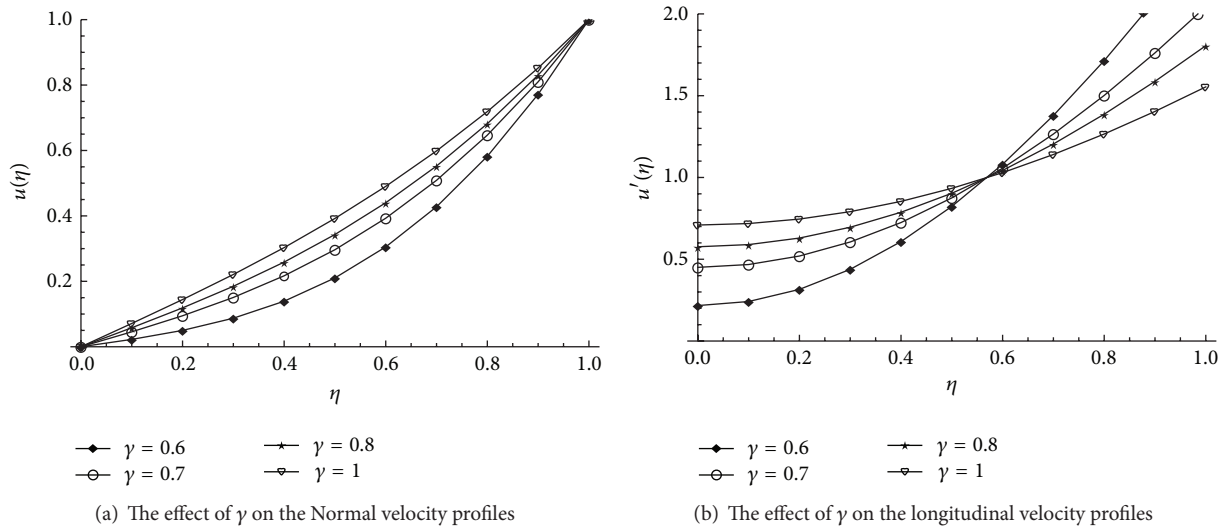


FIGURE 7: Velocity profiles for various values of $\gamma = 0.6, 0.7, 0.8, 1$ fixing $R = 0.3$ in case of slip boundary.

- (ii) It has been observed that normal velocity increases monotonically from $\eta = 0$ to $\eta = 1$ for fixed positive value of R at a given time.
- (iii) It has been seen that longitudinal velocity decreases near the walls and increases near the central axis of the channel.

longitudinal velocity decreases near the walls and increases near the central axis of the channel.

- (iii) It has been investigated that Reynolds number R and slip parameter γ have opposite effects on the normal and longitudinal velocity components.

In case of slip at boundary;

In case of slip versus no-slip boundary;

- (i) It has been noted that after fixing slip parameter γ and varying the Reynolds number R , the normal velocity profile decreases with the increase in R . Also the longitudinal velocity increases near the walls but decreases near the central axis of the channel.
- (ii) It has been examined that for a fixed Reynolds number R when we vary slip parameter γ , the normal velocity increases with the increase in γ . Also the

- (i) It has been observed that Reynolds number R has opposite behavior on the normal velocity in case of slip and no-slip boundaries.
- (ii) It has been also noticed that Reynolds number R has opposite effect on the longitudinal velocity near the central axis of the channel, while near the wall longitudinal velocity increases in case of slip boundary and decrease in no-slip boundary. This is in conformance to [33].

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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