



# GreenHouse gas Observations of the Stratosphere and Troposphere (GHOST): an airborne shortwave-infrared spectrometer for remote sensing of greenhouse gases

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**Abstract.** GHOST is a novel, compact shortwave-infrared grating spectrometer, designed for remote sensing of tropospheric columns of greenhouse gases (GHGs) from an airborne platform. It observes solar radiation at medium to high spectral resolution (better than 0.3 nm), which has been reflected by the Earth's surface using similar methods to those used by polar-orbiting satellites such as the JAXA GOSAT mission, NASA's OCO-2, and the Copernicus Sentinel-5 Precursor. By using an original design comprising optical fibre inputs along with a single diffraction grating and detector array, GHOST is able to observe CO<sub>2</sub> absorption bands centred around 1.61 and 2.06 μm (the same wavelength regions used by OCO-2 and GOSAT) whilst simultaneously measuring CH<sub>4</sub> absorption at 1.65 μm (also observed by GOSAT) and CH<sub>4</sub> and CO at 2.30 μm (observed by Sentinel-5P). With emissions expected to become more concentrated towards city sources as the global population residing in urban areas increases, there emerges a clear requirement to bridge the spatial scale gap between small-scale urban emission sources and global-scale GHG variations. In addition to the benefits achieved in spatial coverage through being able to remotely sense GHG tropospheric columns from an aircraft, the overlapping spectral ranges and comparable spectral resolutions mean that GHOST has unique potential for providing validation opportunities for these platforms, particularly

over the ocean, where ground-based validation measurements are not available. In this paper we provide an overview of the GHOST instrument, calibration, and data processing, demonstrating the instrument's performance and suitability for GHG remote sensing. We also report on the first GHG observations made by GHOST during its maiden science flights on board the NASA Global Hawk unmanned aerial vehicle, which took place over the eastern Pacific Ocean in March 2015 as part of the CAST/ATTREX joint Global Hawk flight campaign.

## 1 Introduction

The Paris Agreement (2015) describes a framework for mitigating global anthropogenic greenhouse gas (GHG) emissions. The success of this agreement lies in our ability to monitor progress on nationally determined contributions (NDCs) that describe country emission targets (Article 13 of the Paris Agreement). This will be achieved by global stock takes every 5 years from 2023 (Article 14). The Paris Agreement emphasizes, in particular, the requirement of independent verification of emissions or monitoring independent data. One approach to independently assessing GHG emis-

sions is to monitor atmospheric concentrations of GHGs. Atmospheric GHGs vary over a range of temporal and spatial scales, reflecting variations due to their sources, sinks, and atmospheric transport. Here, we describe the calibration and performance of a new airborne remote-sensing GHG instrument that seeks to fill the spatial measurement gap between ground-based remote-sensing instruments and satellite data. Data from this airborne instrument have the potential to link emissions from small-scale (< 1 km) sources to the global-scale atmospheric GHG variations that are currently observed by both ground-based networks and satellite instruments.

A large number of atmospheric GHG measurements are collected daily across the globe. Each type of atmospheric GHG measurement has its advantages and disadvantages. Global-scale in situ measurement networks were designed to precisely and accurately observe large-scale changes in atmospheric GHGs (e.g. NOAA ESRL, <https://www.esrl.noaa.gov/>, last access: 29 August 2018). They provide invaluable information on baseline values, and records are typically collected over many decades. These have recently been supplemented by smaller, denser networks within individual countries (Henne et al., 2016; Palmer et al., 2018) and in some cases within individual cities whose purpose is to quantify national, regional, and local GHG emissions (Bréon et al., 2015; Davis et al., 2017). Similar in situ instruments are installed on atmospheric research aircraft (Pitt et al., 2016; O'Shea et al., 2013) and in some instances commercial aircraft (Brenninkmeijer et al., 2007; Matsueda et al., 2002). These measurement platforms allow the study of vertical gradients but are typically deployed for short durations or over limited spatial domains, although there are notable exceptions. Data collected by commercial aircraft represent valuable knowledge of variations in the upper troposphere along air corridors but also provide vertical profiles during airport ascents and descents. In addition to these in situ observations, temporary networks of portable upward-looking Fourier transform spectrometers (Gisi et al., 2012) have been used to constrain GHG emissions on a local scale by making integrated column measurements of GHGs from different locations around a city (Hase et al., 2015; Viatte et al., 2017).

Satellite column observations of CO<sub>2</sub> and CH<sub>4</sub> with the precision necessary to determine their surface emissions are now available (Crisp et al., 2017; Kuze et al., 2009; Buchwitz et al., 2015; Feng et al., 2017). Because of the stringent measurement requirements (precisions of < 1 ppm for CO<sub>2</sub> and < 5 ppb for CH<sub>4</sub>) reflecting the small fractional variations introduced by surface sources and sinks, systematic errors of a few percent in the column amount can, if not properly characterized, compromise the usefulness of the inferred GHG fluxes (Chevallier et al., 2014; Feng et al., 2016). To help characterize these errors a global intercalibrated network of upward-looking Fourier transform spectrometers has been established to validate the space-borne data (Wunch et al., 2011). Nevertheless these data provide global coverage, sub-

ject to clouds and elevated aerosol loading, but at exclusively one local time of the day with a typical repeat frequency of a few days. The integrated column measurement can help to overcome these weaknesses: a column measurement at any one time and location is a superposition of sources and sinks from upwind regions at different times of day (Palmer et al., 2008). This does, however, make interpretation of the column non-trivial, and consequently it would be difficult with current measurement techniques, even if properly integrated through intercalibration efforts, to address the objectives of the Paris Agreement given the importance of city and point emission sources.

Aircraft remote-sensing instruments are particularly well suited for mapping out small-scale gradients in GHGs, enabling repeated observations over large point sources and diffuse sources and providing a link between ground-based in situ measurements and space-borne observations. The Airborne Research Interferometer Evaluation System (ARIES) is a Fourier transform spectrometer (FTS), which is regularly flown on the UK FAAM (Facility for Airborne Atmospheric Measurements) BAe-146 atmospheric research aircraft. Recent work has developed the capability to retrieve thermal infrared (TIR) CH<sub>4</sub> columns that have helped to map distributions of CH<sub>4</sub> gradients over the UK (Illingworth et al., 2014; Allen et al., 2014). The German Methane Airborne MAPper (MAMAP) is a two-channel near- and/or shortwave-infrared (NIR/SWIR) grating spectrometer (Gerilowski et al., 2011; Krings et al., 2011) that was designed to fly on a range of aircraft. MAMAP has illustrated the usefulness of airborne technology to map CH<sub>4</sub> and CO<sub>2</sub> emissions from coal mines, landfill sites, and a North Sea bubble blow-out plume (Krings et al., 2013; Krautwurst et al., 2017; Gerilowski et al., 2015). CHARM-F (CO<sub>2</sub> and CH<sub>4</sub> Remote Monitoring-Flugzeug) is an integrated-path differential-absorption lidar (Amediek et al., 2017) that serves as the airborne demonstrator for the DLR-CNES MERLIN (Methane Remote Sensing Lidar Mission) concept. CHARM-F simultaneously measures CO<sub>2</sub> and CH<sub>4</sub> columns and has flown on the German HALO (High Altitude and Long Range Research Aircraft). The potential for using airborne hyperspectral imagers such as the NASA Airborne Visible-Infrared Spectrometer – Next Generation (AVIRIS-NG) to detect and quantify localized anthropogenic sources of CH<sub>4</sub> has also been demonstrated recently (Thompson et al., 2015). A further NASA instrument, called CARVE-FTS (Carbon in Arctic Reservoirs Vulnerability Experiment FTS), has been used to observe GHG fluxes from an aircraft over Alaska (Dupont et al., 2012).

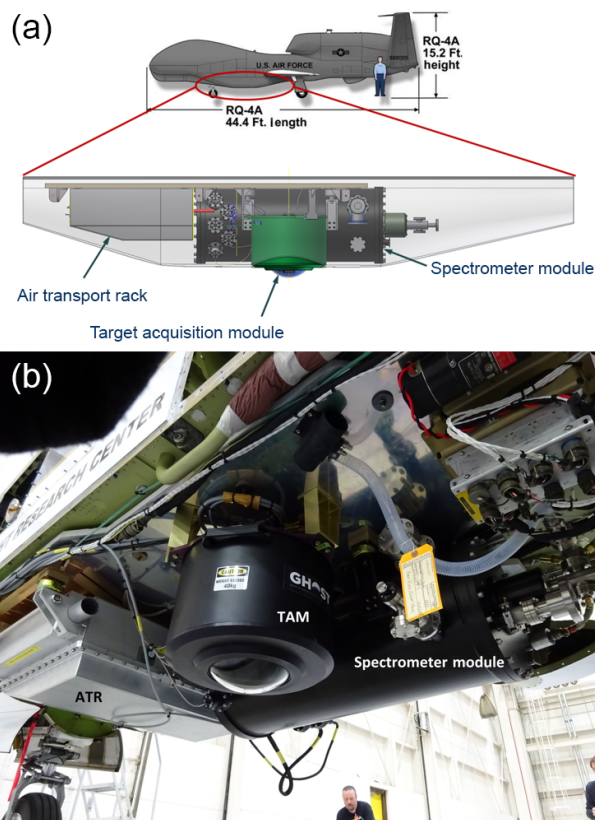
In this paper we describe the GreenHouse gas Observations of the Stratosphere and Troposphere (GHOST) shortwave-infrared (SWIR) grating spectrometer. The principal advantage of the GHOST design (described in Sect. 2) is that it is able to image four different spectral bands using a single diffraction grating and detector array, thus saving on space and weight compared with an equivalent instrument using a separate grating and detector for each band. This ex-

tent of wavelength coverage at high spectral resolution, and subsequently the number of different gases that can be observed, is unique for an airborne remote sensing instrument. As well as the instrument design we also show the first set of results from GHOST science flights on board the NASA Global Hawk, which took place during the CAST-ATTREX flight campaign, and describe the methods behind their production from raw GHOST data. Section 3 describes the laboratory measurements used to perform radiometric and spectral calibration on GHOST and assesses its performance. In Sect. 4 we outline the involvement of GHOST in CAST-ATTREX, which was based at NASA Armstrong in California during early 2015. Finally, we present the first GHOST flight results (along with the optimal estimation method used to retrieve them from the calibrated radiance spectra) in Sect. 5 and summarize the paper in Sect. 6.

## 2 The GHOST instrument

The optical design behind GHOST was developed by the STFC (Science and Technology Facilities Council) Astronomy Technology Centre during two design studies, both funded by the UK Centre for Earth Observation Instrumentation (<http://ceoi.ac.uk/>, last access: 29 August 2018), which demonstrated reductions in size and weight of SWIR Earth observation spectrometers by using technology originally developed for astronomy instruments. The optics use a combination of blocking filters and multiple grating orders to provide spectra from several high-resolution bands from across a wide range of wavelengths. As well as the size and weight advantages, the optical fibre feed to the spectrometer provides flexibility in the mechanical layout of the subsystems on different aircraft, thermo-mechanical isolation, and the possibility of optically isolated calibration light input to the spectrometer.

The GHOST instrument, initially designed to meet the strict engineering requirements for installation on the NASA Global Hawk unmanned aerial vehicle (UAV), takes advantage of an optical fibre feed system to split the optics into two units: the target acquisition module (TAM) and the spectrometer module. Figure 1 shows how these two components were mounted on a pallet on the underside of the Global Hawk, along with the air transport rack (ATR), which houses the electronics and support equipment for the instrument. In this section we discuss each of these three components in turn. A block diagram showing an overview of how the three components work together within the GHOST instrument system is given in Fig. 2.

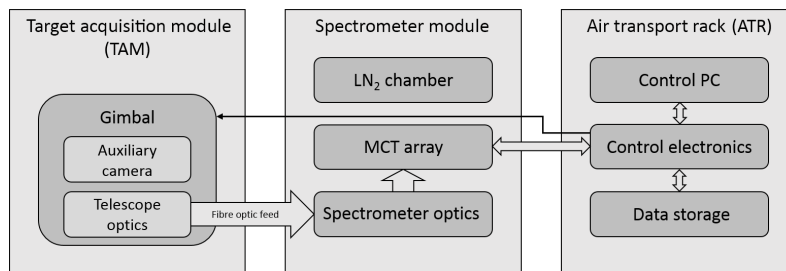


**Figure 1.** (a) Layout of the three main GHOST components mounted in the lower instrument bay of the NASA Global Hawk. (b) Photograph taken from below showing the GHOST installation on the Global Hawk.

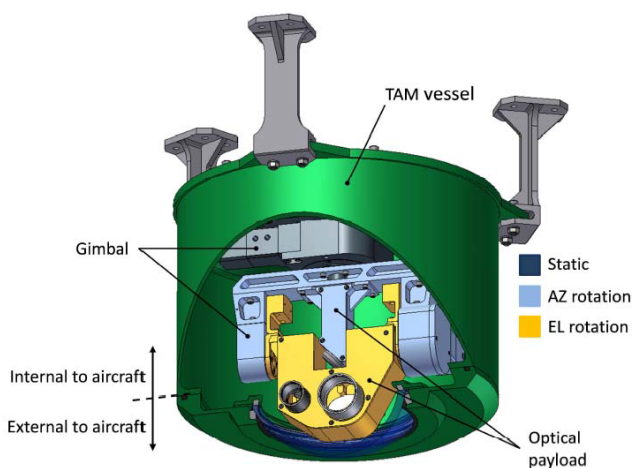
### 2.1 The target acquisition module (TAM)

The function of the TAM is to direct sunlight which has passed down through the atmosphere and then been reflected back upwards by the Earth's surface, onto an optical fibre bundle which transfers the light into the spectrometer module. To achieve this, the TAM has to be able to acquire light from any angle of rotation and up to  $70^\circ$  away from nadir, depending on the solar zenith angle. A custom off-axis telescope arrangement is used and mounted to a custom Newmark GM-6 gimbal (see Fig. 3).

A fold mirror reflects the light path along the elevation axis of the gimbal, through a depolarizing unit and onto a second fold mirror that directs the light path along the rotation axis (see Fig. 4). Mounted centrally along this axis are the pre-fibre optics (a field stop and lenses) and the fibre bundle mounting point. A field stop of diameter 2.6 mm is used to define the range of angles from which light will be accepted into the fibres, such that it observes reflected light from a surface footprint  $1^\circ$  in diameter. The optics create a pupil image on the end of the fibre bundle such that the light is both concentrated onto the fibres and evenly distributed between them. The field stop defines the range of



**Figure 2.** Block diagram showing the three main components of the GHOST instrument (described in Sect. 2) and how they interact with one another.



**Figure 3.** Cut-away model of the TAM showing the gimbal, payload, and the edge of the dome (in dark blue). The light-blue component rotates about the azimuthal axis, whilst the yellow component rotates about the axis of elevation. The TAM is 513 mm tall including the legs and has a diameter of 555 mm including the feet.

angles that will be accepted into the fibres, which is set to an angle of  $\pm 6.67^\circ$  (numerical aperture  $NA = 0.11$ ). In order to avoid misalignment between the main optical ray defined by these apertures and the mechanical axis of the gimbal (which would introduce a shift in pointing angle which varies with gimbal position), we required that the end of the fibre bundle, the coupling lens, and the field stop aperture should be centred on the rotation axis of the gimbal to within  $50\mu\text{m}$ . In the focus direction (along the optical axis), they should be positioned to within an accuracy of  $200\mu\text{m}$ . The intersection of the two mechanical axes of the gimbal must lie within  $50\mu\text{m}$  of the surface of fold mirror 2 (see Fig. 4), whilst the angle of this mirror must also be correct to within  $0.1^\circ$ .

By using a design which employs movable optics to transfer the observed light onto a static fibre bundle, we minimize the potential for deterioration of the measured signal caused by movement and bending of the fibres. The gimbal also carries a wide-field panchromatic camera with a field of view extending beyond that of the spectrometer input. The camera

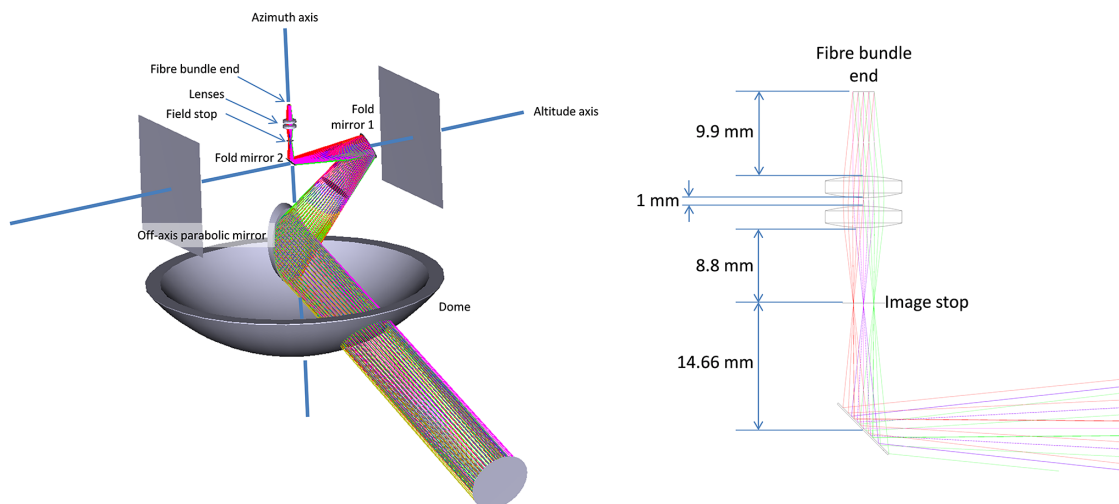
is used to help interpret the science data, e.g. by identifying when the spectrometer field of view is cloud-free.

The light enters the TAM through a dome whose centre of curvature has been placed at the centre of curvature of the gimbal to reduce differential aberrations across the gimbal range. Originally the whole bottom face of the TAM vessel was designed to be external to the aircraft, since the vessel was intended as an environmentally benign environment for the gimbal and the optics, with internal heaters and the potential for dry gas flushing. The TAM is pressurized to 3 psi above local ambient conditions to minimize the diffusion of water vapour into the optical system. The vessel also included a number of fiducial measurement points which were used to ascertain alignment and location of the optics, both in the lab and on the aircraft. The final installation was more enclosed and left only the dome itself protruding from the underside of the Global Hawk.

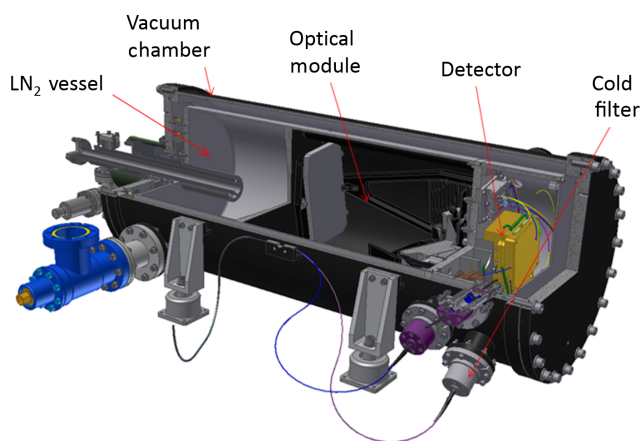
The optical fibre bundle which passes the received light onto the spectrometer module is made up of 35 multimode fibres, each with a  $0.365\text{ mm}$  core, encased in a stainless steel outer sheath for protection. At the spectrometer end the bundle of 35 fibres is split into five smaller bundles (one for each spectral band; see Sect. 2.2) comprising seven fibres each, with the choice of fibres kept as spatially random as possible to ensure that a similar sampling of the aperture is passed into each bundle. The light from each of the bundles is transmitted into the (cold) spectrometer through a window and an order-sorting filter, which minimizes the out-of-band light and is finally coupled into a cold fibre bundle.

## 2.2 The spectrometer module

Inside the spectrometer module there are three major sections: an end section that contains the optical entry points, cold fibres, and the detector box; a middle section containing the spectrometer optics; and a section where the cryogen tank is situated (see Fig. 5). All of the spectrometer module internal components are cooled to 80 K, which has the effect of reducing the thermal background, the dark current on the detector, and any thermo-mechanical instabilities. The decision to use liquid nitrogen for cooling rather than a closed cycle cooler is based primarily on the need to minimize vi-



**Figure 4.** Optical path diagram showing how the optical components of the TAM direct the observed light into the optical fibre.



**Figure 5.** GHOST spectrometer module showing the front end compartment, the main spectrometer optics area, and the liquid nitrogen cryogenic vessel. The cylinder containing these components is 1064 mm long and 440 mm in diameter. Taking into account the fittings external to the cylinder, the space occupied is 1406 mm long, 758 mm wide, and 440 mm tall.

brations, both for this instrument and for other instruments mounted on the same aircraft. Cryogenic cooling has the additional benefits of requiring no electrical power, being very reliable (compared with using mechanical cooling which relies on moving components), and using little extra space for external electronics.

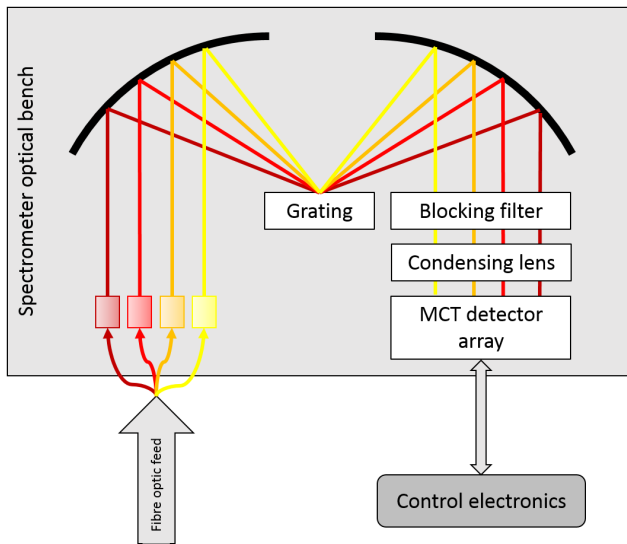
We summarize the spectrometer optical design schematically in Fig. 6. Observed light is brought into the spectrometer optics using cold fibre bundles as mentioned in Sect. 2.1. The optical part of the spectrometer module comprises four major components: the inlet slits, fold mirror, camera mirror, and grating (see Fig. 7). The  $f/5$  focused beam from the input slits is reflected by the fold mirror onto one side

of the curved camera mirror. The collimated beam is then reflected again by the fold mirror onto the grating, which disperses the light from each band into a number of spectrally resolved images, each produced by a different order of diffraction. The dispersed light is reflected again by the fold mirror on to the other side of the camera mirror, after which the converging beam is reflected once more by the fold mirror and passed through cylindrical output lenses that concentrate the spectral images onto the detector. The major innovation in this design is the use of multiple grating orders: through the choice of orders and positioning of the input slits, multiple high-resolution spectral bands can be selected from a wide overall wavelength range and conveniently placed onto the output plane. In the GHOST spectrometer we use a 60 grooves  $\text{mm}^{-1}$  blazed grating supplied by Richardson Gratings, with a blaze angle of  $28.7^\circ$  corresponding to a blaze wavelength of  $16\mu\text{m}$ . For spectral bands 1 through to 4 (Table 1) we use diffraction orders 13, 10, 8, and 7. The grating and orders were chosen to minimize the spread of input slit offsets (along the dispersion direction at the entrance to the spectrometer) required to image all of the bands onto the detector, using Band 2 as the reference point. The spread was calculated for diffraction orders up to 18, with the result that using diffraction order  $n = 10$  for Band 2 minimized the need to shift the input slits for the other bands. We then selected an appropriate grating by requiring that the blaze wavelength be as close to  $n\lambda$  for Band 2 as possible.

The spectral images are recorded by a mercury cadmium telluride (MCT) detector, which is mounted just behind the optics baseplate. The detector used is a Raytheon Vision Systems VIRGO2K detector with  $2048 \times 2048$   $20\mu\text{m}$  pixels, which has high quantum efficiency (typically greater than 80% across the broad spectral range), low dark current, and low read noise (less than 20 e rms in a correlated double sample frame). The measured dark current at liquid nitrogen tem-

**Table 1.** Target gases, spectral range, spectral resolution, and signal-to-noise ratio (SNR) design requirements for each band. The goal (threshold in brackets) values are given for resolution and SNR. The SNR requirements listed here assume an integration time of 1 sec.

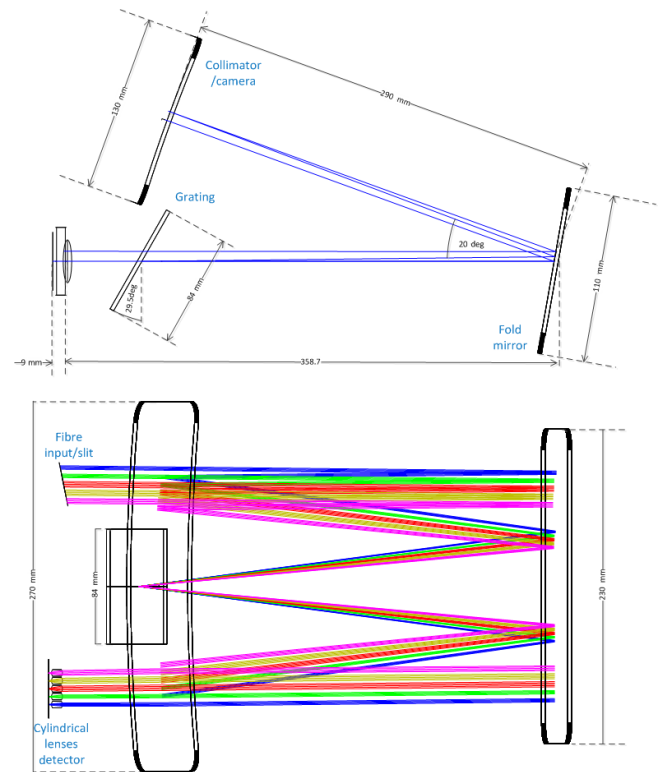
Band	Target gases	Spectral range ( $\mu\text{m}$ )	Resolution (nm)	SNR
1	O <sub>2</sub>	1.25–1.29	0.1 (0.1)	200 (150)
2	CH <sub>4</sub> , CO <sub>2</sub>	1.59–1.675	0.25 (0.3)	100 (80)
3	CO <sub>2</sub>	2.04–2.095	0.15 (0.3)	150 (100)
4	CO, CH <sub>4</sub> , H <sub>2</sub> O / HDO ratio	2.305–2.385	0.25 (0.3)	100 (80)



**Figure 6.** Block diagram showing a simple overview of the GHOST spectrometer optical layout.

perature (80 K) is less than  $1 \text{ e s}^{-1} \text{ pixel}^{-1}$ . During flight we use heaters and a platinum resistor (for feedback) to hold the detector temperature at a slightly warmer 98 K, ensuring that the detector temperature remains stable to within a few tens of mK via the feedback mechanism (the increased stability is achieved in this way at the expense of a higher dark current; see Sect. 3.2). Prior to installation of the detector array into the spectrometer module, we measured the average signal gain for each pixel to be  $4.26 \text{ e count}^{-1}$ .

The spectrometer has been designed to measure high-resolution spectral radiances over four wavelength bands, which we have chosen to coincide with spectral absorption features of the atmospheric gases we are interested in. The design requirements for the four bands are listed in Table 1, whilst Fig. 8 shows the absorption spectra of the most important gases in each band. When defining the requirements for the spectral resolution and signal-to-noise ratio we determined threshold values, which indicate the minimum acceptable performance, along with goal values which represent the desired performance level. In the final design a fifth band, a duplicate of Band 2 (the most important band for meeting our science objectives), was incorporated to provide redun-

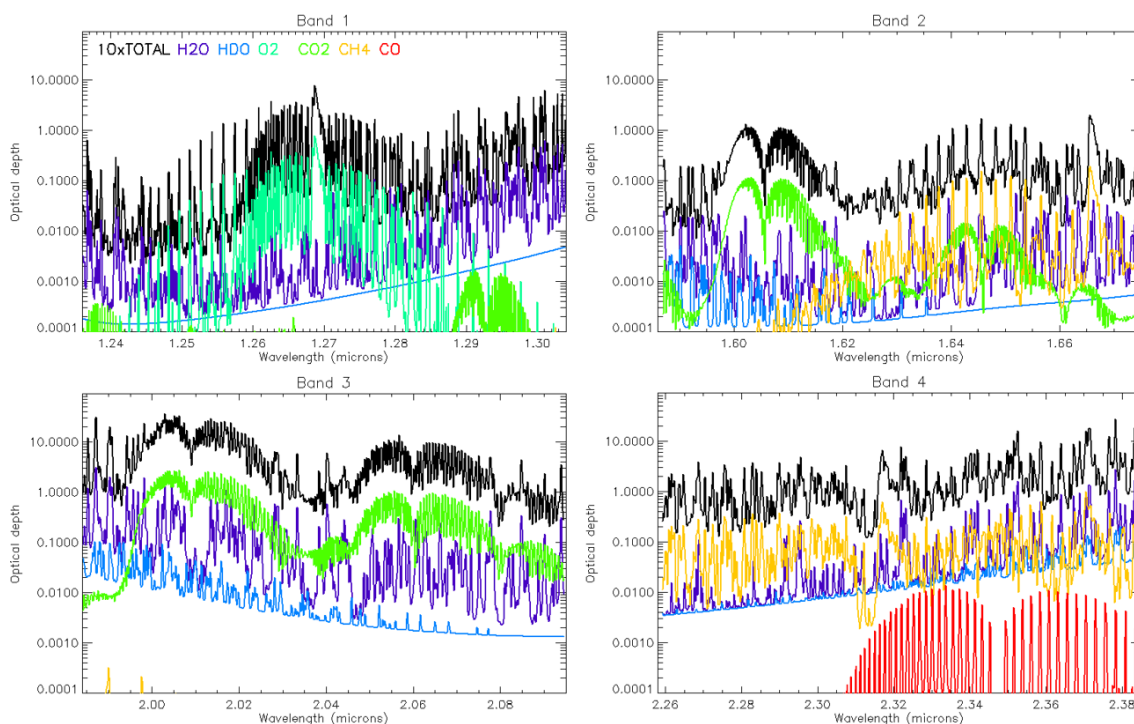


**Figure 7.** Elevation and plan view of the spectrometer showing the major dimensions, which allows it to fit into the cryostat optical module as shown in Fig. 5. The different coloured ray traces in the plan view diagram correspond to light from each of the five optical fibre bundles.

dancy in case the original Band 2 did not meet the spectral and radiometric requirements.

### 2.3 Data handling and control

The detector read-out system is an ARC (Astronomical Research Camera) controller attached to an industrial PC running Linux. The software system is the UK-ATC's UCam product, which has been widely used with astronomy instruments across the world for the last 10 years. The detector operates in an “integrate while read” mode, a non-destructive read-out mode in which pixels can be sampled as many times as required whilst integrating the signal. At 300 kHz pixel



**Figure 8.** Optical depth spectra for each of the four GHOST spectral bands listed in Table 1, calculated assuming a midlatitude reference atmosphere and a viewing angle of  $20^\circ$  off nadir. The different colours correspond to the contributions towards the total optical depth from each species considered. The total optical depth spectrum for each band (shown in black) is multiplied by 10 to make it easier to see on the logarithmic scale.

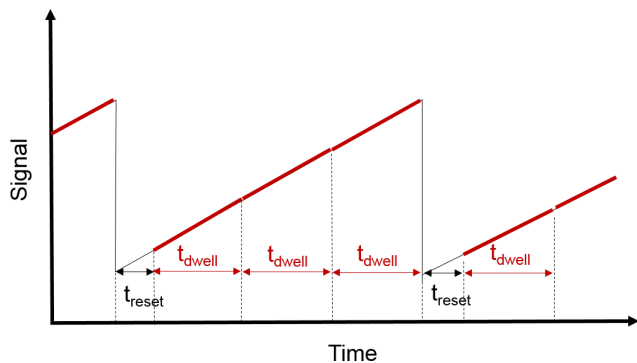
rate, using all 16 amplifier channels, it takes about 0.91 s to read out the entire detector. Since we are only imaging a fraction of the array, we reduce the read-out time by skipping the rows we do not need. By reading out only 300 of the 2048 detector rows (60 rows for each of the five bands), we reduce the read-out time to 0.115 s. In order to maximize the on-source integration time, an up-the-ramp read-out mode has been implemented where the array is read out a set number of times following a reset (see Fig. 9). Both the number of read-outs between resets and the dwell time between read-outs are programmable, and we set them such that the signal level prior to a reset is below the level at which the detector is saturated. Taking the difference between any two reads in a frame which is free from the reset noise and the offset.

The electronics for the read-out system are contained in the ATR, procured from Elma Electronic in the UK, which provides a temperature- and pressure-controlled environment. All data from the system (science data frames, auxiliary pictures, temperatures, positional information, etc.) are stored on a solid-state disk in time-tagged netCDF files. The system provides TCP (Transmission Control Protocol) and UDP (User Datagram Protocol) command and control access via a 100BASE-T port as well as real time data access (over TCP only). The software system is designed with robustness in mind, and a long campaign of simulated operations en-

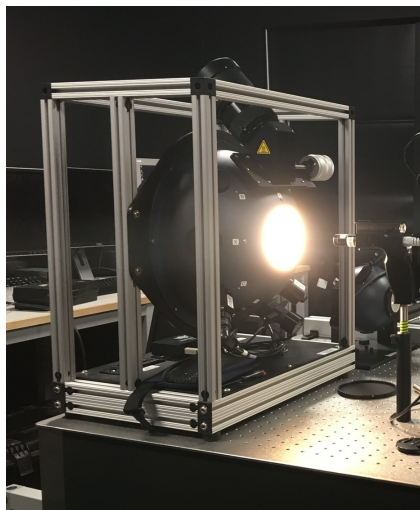
sured that the system would continue taking meaningful data under almost all conditions and, for extreme eventuality, provided a hard reboot facility.

### 3 Calibration and performance of GHOST

In this section, we describe the procedures and measurements used for the radiometric and spectral calibration of the GHOST instrument, and provide a summary of the spectrometer performance based on the calibration results. We perform the majority of the calibration measurements using a 0.3 m internal diameter integrating sphere with 0.1 m diameter output port from Labsphere (Fig. 10), provided by the NERC Field Spectroscopy Facility (FSF). The integrating sphere produces a spatially uniform light source via multiple internal reflections off the inner Spectrafect coating, which completely illuminates the GHOST field of view when positioned at a distance of 1 m from the TAM. The integrating sphere used has four input ports in addition to the output port: three ports housing quartz tungsten halogen (QTH) lamps (two internal to the sphere and one external), and one port allowing the use of alternative light sources (such as the emission lamps used for spectral calibration, as described in Sect. 3.3) with the sphere. The two internal QTH lamps have output powers of 35 and 75 W, whilst the 150 W external



**Figure 9.** The sampling scheme used by the GHOST detector, where we sample the array “up-the-ramp”. In this example we show three reads of the array subset per exposure. Time  $t_{\text{reset}} = 0.115$  s is required to perform a destructive read-out and reset of the array subset. A non-destructive read-out is then performed every  $t_{\text{dwell}}$  seconds. The number of reads and their duration are determined by the instrument operator.

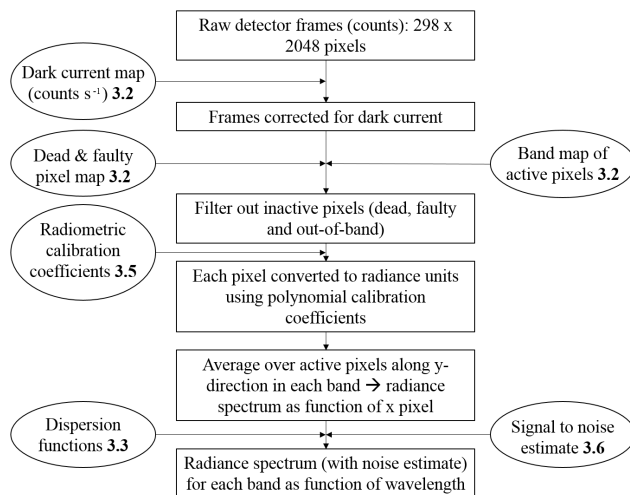


**Figure 10.** Photograph of the NERC FSF integrating sphere, with the 150 W external lamp and variable aperture mechanism visible just above the output port (photograph by Chris MacLellan, NERC FSF).

QTH lamp is mounted behind a mechanical variable aperture which allows fine adjustment of the output luminance. We use measurements of the 150 W external lamp for the radiometric calibration described in Sect. 3.5. An internally mounted photodiode provides measurements of the output luminance at a frequency of 1 Hz.

### 3.1 Processing of GHOST measurements into radiance spectra

A number of steps are required to process the raw detector frame data measured by GHOST into radiometrically and spectrally calibrated radiance spectra, which are then suitable



**Figure 11.** Diagram illustrating the steps and inputs involved during the processing of GHOST data into calibrated radiance spectra. The numbers in bold contained in each of the inputs refer to the corresponding section number.

for use in retrieval algorithms used to obtain concentrations of target trace gases (as described in Sect. 5.1). We summarize these steps in Fig. 11. The ellipses in the diagram indicate the inputs required, which we obtain during the instrument characterization and calibration described later in this section, whilst the rectangles show each separate processing step in the procedure. The raw detector frames at the start of the process are obtained by taking the final non-destructive read-out in a sequence and then subtracting the first read-out after the previous reset (see Fig. 9). The difference between these two read-outs removes the offset and reset noise as described in Sect. 2.3.

### 3.2 Dark current measurement and identification of inactive pixels

Prior to the spectral and radiometric calibration measurements, we need to characterize certain aspects of the detector array performance. These include the detector dark current (for each pixel on the array), the identification of the pixels that are illuminated on the detector array by each spectral band image, and the location on the array of dead, hot, or otherwise faulty pixels which are excluded from further analysis.

We evaluate the dark current (the residual current which flows through a photosensitive device in the absence of incident photons) by averaging over exposures taken with no light entering the system, resulting in a dark current map in units of digital counts per second. The mean dark current measured in each band is listed in Table 2. These values are higher than the  $0.25 \text{ counts s}^{-1}$  that would be achieved if the detector were operated at liquid nitrogen temperature (80 K; see Sect. 2.2). However, we consider it more advantageous to



**Table 2.** Mean dark current measured for each GHOST spectral band (see Sect. 3.2) with the detector at flight temperature (98 K). The standard deviations given represent the spatial variability of dark current within each band.

Band	Mean dark current (counts s <sup>-1</sup> )	Standard deviation (counts s <sup>-1</sup> )
1	2.855	1.187
2A	2.375	1.060
2B	2.698	1.145
3	2.505	1.021
4	3.025	1.379

keep the detector slightly warmer but at a stable temperature (and known dark current, which can then be subtracted more easily) than to minimize the dark current at the expense of temperature stability. The “darkness” required for this measurement is achieved by disconnecting the optical fibres from the spectrometer module. The dark exposures are also used to identify hot pixels, defined as pixels which return a fully saturated response independently of the amount of light incident on them. We flag all pixels with mean measured responses above a threshold value as hot pixels, and apply a threshold standard deviation to filter out pixels which are “hot” intermittently, as the pixel response to dark input should not vary significantly over time.

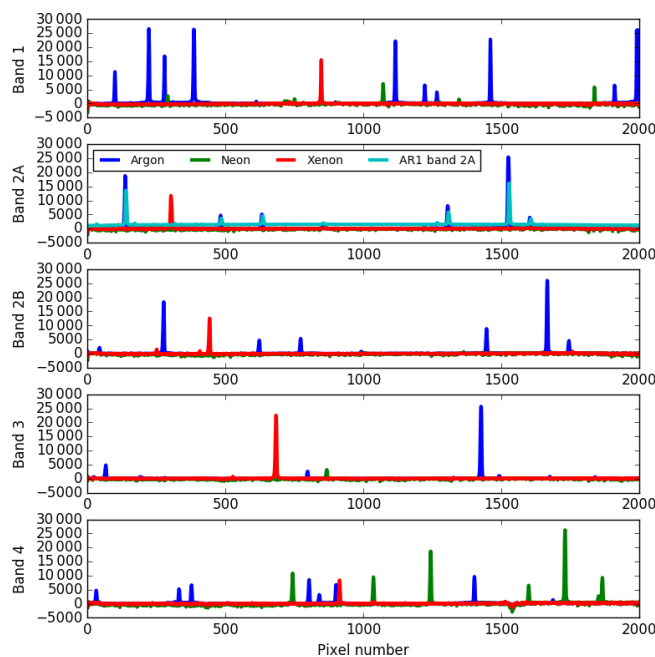
We identify dead pixels, pixels which show no response when light is incident on them, using exposures where a white light source is observed. For this purpose we use the integrating sphere described earlier with a quartz tungsten halogen lamp as the observed target. All pixels with measured mean responses below a threshold value are flagged as dead pixels. We also use the same measurements to produce a map of the image of each spectral band on the detector array, which is then used to determine the pixels included when processing the measured images into radiance spectra (see Sect. 3.1). The pixels forming the band map are identified on a column-by-column basis. In each column, the 20 pixels with the highest value when illuminated (excluding hot and dead pixels) are considered to be “in-band” for the purposes of processing the images into spectra. By taking the mean of the 20 in-band pixels in each column during the processing stage (as described in Sect. 3.1), we are able to obtain a better signal-to-noise ratio for the final calibrated spectra.

### 3.3 Spectral calibration

The aim of the spectral calibration is to determine a relation between the pixel number along the horizontal axis of the detector array and the wavelength of light incident on that pixel, following dispersion of the input light by the reflection grating. To obtain these relations for each of the five bands we use measurements of emission lamp spectra, where the wavelengths of the emission lines are well known, to evaluate

**Table 3.** Measurements used for the spectral calibration of GHOST (see text in Sect. 3.3).

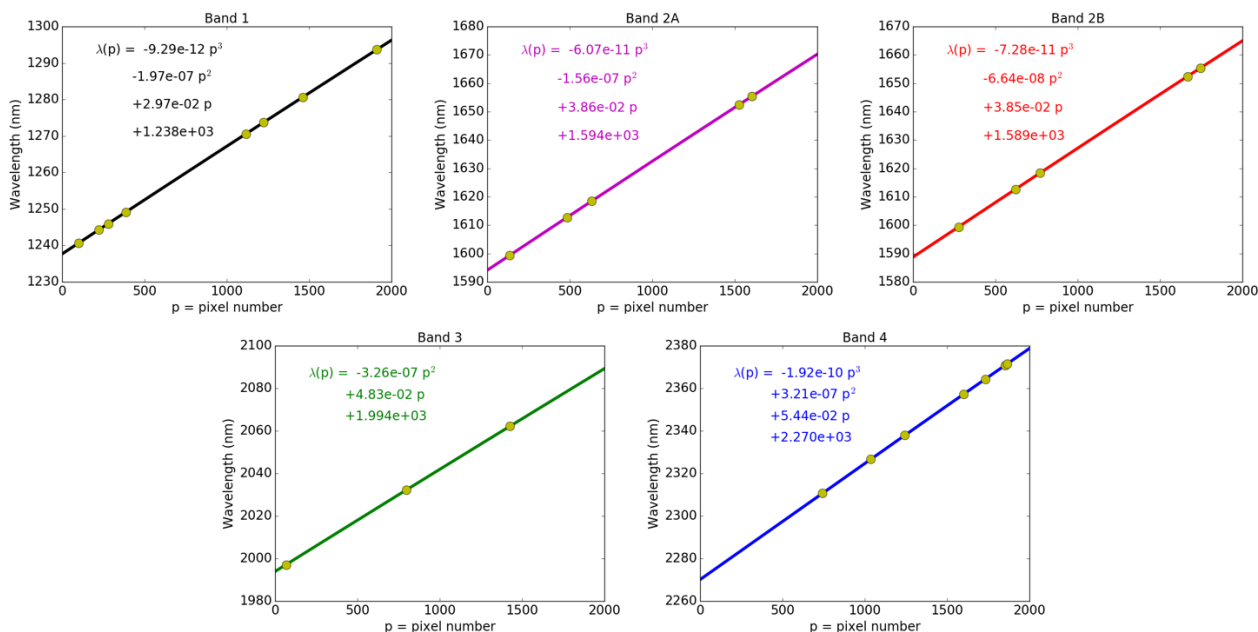
Measurement	Exposures	Reads per exposure	Dwell per read (ms)
Argon pen-style lamp	100	12	10 000
Neon pen-style lamp	40	12	20 000
Xenon pen-style lamp	40	12	10 000
AR1 argon lamp (Band 2A fibre input only)	40	30	1000



**Figure 12.** Measurements of emission lamp spectra for each GHOST band, shown as a digital detector response in counts as a function of the horizontal pixel number. The colours correspond to the different emission lamps listed in Table 3.

the wavelength of pixels corresponding to the emission line centres. Figure 12 shows the emission lamp spectra measured by GHOST that we used for the spectral calibration. We use argon, neon, and xenon pen-style emission lamps (belonging to the NERC FSF) in conjunction with the integrating sphere to produce spectrally discrete light sources which fill the GHOST field of view. The measurements we made for the spectral calibration are listed in Table 3.

We then fit a third-order polynomial which returns the wavelength of each emission line as a function of pixel number, giving us a dispersion function for each band. We locate the positions of the line centres in pixel space by first fitting and subtracting any continuum signal in the spectrum and then fitting an asymmetric Gaussian function to each emission peak greater than a threshold value. We finally obtain the dispersion functions by polynomial fitting of the emission line wavelengths listed in the National Institute of Stan-



**Figure 13.** Dispersion functions calculated for GHOST bands 1, 2A, 2B, 3, and 4. Argon emission lines are used for all except Band 4, where neon emission lines are used instead. We used neon for Band 4 because the identification of which measured line corresponds to which line listed in the NIST database was much less ambiguous than for argon in this wavelength range.

dards and Technology database (NIST, Kramida et al., 2017) to their corresponding locations in pixel space for each band, as shown in Fig. 13.

### 3.4 Estimate of instrument line shape functions

The instrument line shape (ILS) function is a representation of how a monochromatic light source is observed by the spectrometer and is an important parameter for calculating the simulated measured spectra used in retrieval algorithms (see Sect. 5.1). In the absence of a genuinely monochromatic source such as a laser, we use measurements of the emission lamps described in Sect. 3.3 with the assumption that the emission lines produced are sufficiently narrow in wavelength, so that they may be considered to be “monochromatic” for our purposes.

To obtain the ILS functions for GHOST we first take emission lamp spectra shown in Fig. 12 and apply the spectral and radiometric calibrations described in Sects. 3.3 and 3.5 respectively. Once the background continuum signal has been subtracted, three emission lines in each band are selected (such that they are representative of the band wavelength range), extracted, and normalized. The part of the spectrum extracted for each line covers a wavelength range of  $\pm 0.4\text{nm}$  centred on the maximum. Figure 14 shows the extracted ILS functions for Band 2A. During the forward-model calculation described in Sect. 5.1, we interpolate between the extracted instrument line shapes to estimate the ILS for each pixel. The interpolation method we use is performed in two steps: firstly, a linear interpolation is used to

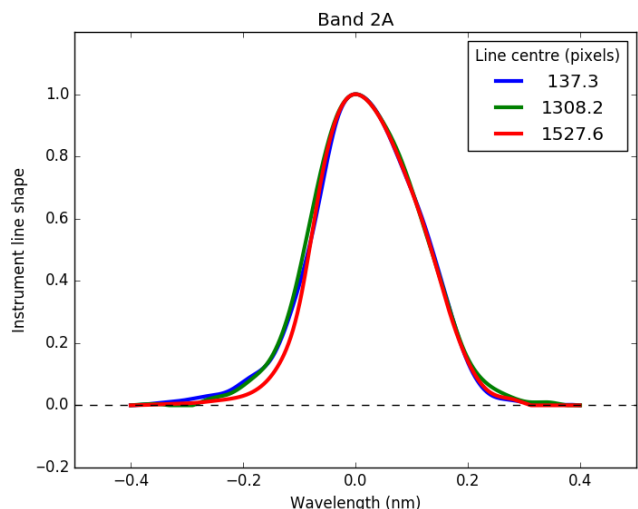
determine the line shape centred on each wavelength pixel; then, each pixel-specific line shape is interpolated in  $\log(\delta\lambda)$  space to determine how it maps onto the neighbouring pixels.

### 3.5 Radiometric calibration

The objective of the radiometric calibration is to determine the relationship between the digital detector array response and the spectral radiance (in SI units) incident on the GHOST fore-optics housed in the TAM, on a pixel-by-pixel basis. We use the NERC FSF integrating sphere (described previously at the beginning of Sect. 3.3) to produce a spatially uniform light source filling the GHOST field of view. The 150 W external QTH lamp is used in conjunction with a mechanical variable aperture to produce high-, mid-, and low-level luminances for each band (listed in Table 4). We choose the luminances such that each band has the following:

- the full dynamic range of the in-band pixels is covered between the three luminance levels, and
- there is some overlap in the dynamic range covered by measuring each luminance level; i.e. the final three to four read-outs in exposures of the low-level luminance output return a similar signal to the first three to four read-outs in exposures of the mid-level luminance output.

For each set of measurements we only connect the optical fibre input for the target band, to avoid saturation of the more optically sensitive bands (bands 2A and 2B being the most



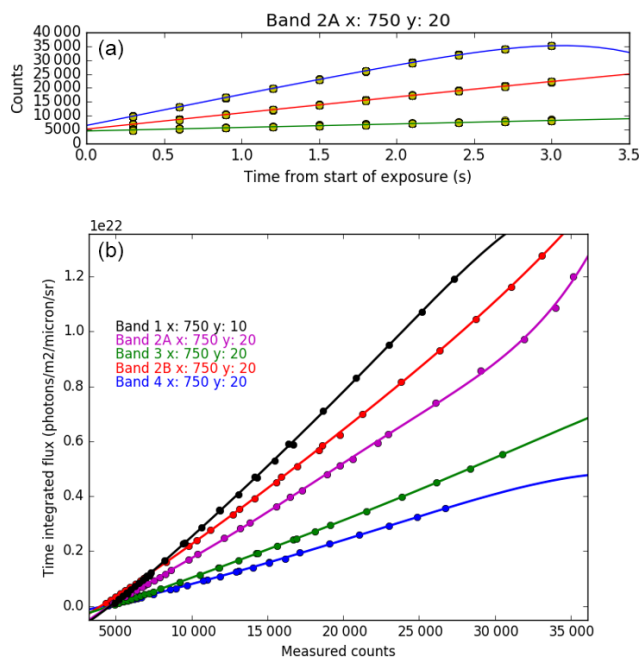
**Figure 14.** Instrument line shapes for Band 2A estimated from argon emission lamp measurements. The numbers in the legend give the location in pixel space for each emission line (see second panel of Fig. 12).

**Table 4.** Measurements of the NERC FSF integrating sphere used for the radiometric calibration of GHOST. The external 150 W lamp was used with a variable aperture to produce the output luminances listed.

Band	High luminance	Mid luminance	Low luminance
1	7218.14 cd m <sup>-2</sup>	3597.69 cd m <sup>-2</sup>	719.14 cd m <sup>-2</sup>
2A	1007.56 cd m <sup>-2</sup>	500.79 cd m <sup>-2</sup>	100.48 cd m <sup>-2</sup>
2B	1002.77 cd m <sup>-2</sup>	500.89 cd m <sup>-2</sup>	100.19 cd m <sup>-2</sup>
3	1398.78 cd m <sup>-2</sup>	699.92 cd m <sup>-2</sup>	140.21 cd m <sup>-2</sup>
4	1796.94 cd m <sup>-2</sup>	899.96 cd m <sup>-2</sup>	180.15 cd m <sup>-2</sup>
Number of detector exposures		100	
Number of reads per exposure		10	
Dwell time for each read (ms)		300	

sensitive) when the measured input light reaches the high end of the dynamic range of the less sensitive bands (particularly Band 1). The upper panel of Fig. 15 shows how the measured signal (averaged over 100 exposures) for a single pixel in Band 2A increases with time for each of the three luminances. The signal is read from the detector array 10 times per exposure, with each read-out represented by a yellow circle on the plot.

We use a calibration curve supplied with the integrating sphere to estimate the spectral radiance output (in photons s<sup>-1</sup> m<sup>-2</sup> μm<sup>-1</sup> sr<sup>-1</sup>) from the luminance measured by the internal photodiode. Assuming that the integrating sphere output is constant with time, we then obtain the time-integrated spectral flux for a single pixel as a function of the signal (in counts) measured by that pixel, as shown in the lower panel of Fig. 15. The GHOST calibration curves, shown here for a single pixel in each band, are derived by



**Figure 15.** (a) Measurements of the integrating sphere at three different luminances (blue: high luminance, red: mid luminance, green: low luminance – luminance values are listed in Table 4) from a single Band 2A pixel (pixel number 750 along the x axis, 20 along the y axis within the band). (b) Radiometric calibration curve fitted to the integrating sphere observations for a single pixel (pixel numbers listed in the legend) in each of the five GHOST bands.

fitting a fifth-order polynomial to 30 data points. These comprise data from 10 read-outs (averaged over 100 exposures) of each of the three luminances measured using each band. Calibration coefficients describing the fifth-order polynomial fit are calculated for every in-band pixel, and subsequently used in producing radiometrically calibrated radiance spectra from the GHOST flight measurements as described in Sect. 3.1. The calibration curves also illustrate the signal level at which the detector response begins to show particularly non-linear behaviour; this is at measured signals of around 26 000 counts and above for the pixels shown.

### 3.6 Summary of GHOST spectrometer performance

Table 5 summarizes the spectral performance of the GHOST spectrometer, specifically the wavelength range, spectral resolution, and spectral sampling for each band, which we evaluate using the dispersion functions obtained in Sect. 3.3.

The spectral resolution varies slightly across each band, as the wavelength does not increase linearly with pixel number. We estimate the range of spectral resolutions for each band by taking the narrowest and widest full width half maxima (FWHM) in pixels, obtained through the asymmetric Gaussian fits to the emission lines, and multiplying them by the spectral sampling (the gradient of the dispersion function,

**Table 5.** Spectral performance of the GHOST spectrometer, as determined from the wavelength calibration measurements described in Sect. 3.3. The ranges of spectral resolution and sampling are obtained from the minimum and maximum fitted full width half maxima of the emission lines measured for each band.

Band	Lower $\lambda$ (nm)	Upper $\lambda$ (nm)	Range (nm)	Resolution (nm)	Sampling (pixels)
1	1237.67	1296.26	58.59	0.107–0.148	3.675–5.005
2A	1594.03	1671.02	76.99	0.219–0.246	5.825–6.545
2B	1588.75	1664.97	76.22	0.179–0.202	4.746–5.276
3	1993.92	2089.27	95.35	0.258–0.264	5.394–5.577
4	2270.11	2378.73	108.62	0.250–0.280	4.630–5.126

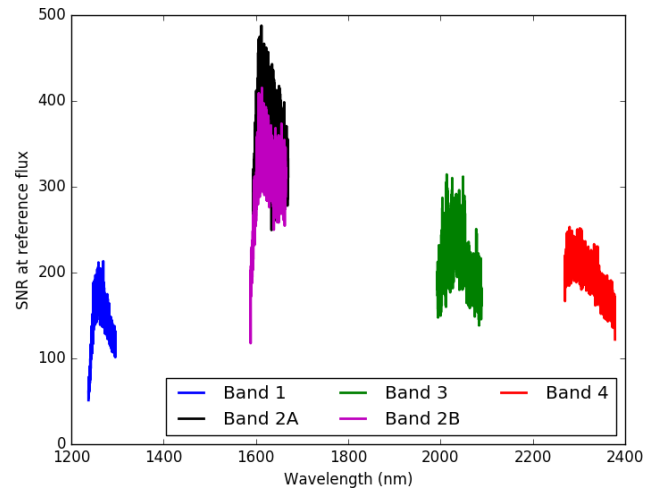
$d\lambda/dp$  where  $p$  is the pixel number) evaluated at the locations of those line centres. Band 2B has a slightly higher spectral resolution than Band 2A (around 0.19 nm resolution compared with around 0.23 nm), though unlike Band 2A its spectral range does not extend as far as the CH<sub>4</sub> Q-branch at 1667 nm.

GHOST's radiometric performance is evaluated by using the signal-to-noise ratio (SNR). We evaluate the SNR on a pixel-by-pixel basis by fitting fourth-order polynomials to both the mean measured signal and the standard deviation of a combined data set comprising the high and low luminance sets of measurements (see Table 4) for each active pixel as a function of the input radiative flux. The ratio between these two polynomials then gives the SNR as a function of the observed radiative flux. The active pixels in each column are finally averaged to obtain the SNR spectrum as a function of wavelength.

Figure 16 shows the estimated SNR for reference input radiances and integration times representative of the observation during the Global Hawk flights, whilst Table 6 shows the mean, minimum and maximum SNR for each band under these assumptions. Bands 2A and 2B have the highest SNRs of the five GHOST bands, with mean values of about 370 and 310. The other bands have lower SNR values, but are still sufficiently high (around 140 to 210) to be useful for trace gas column retrievals. The SNR spectrum is also used as an input by the retrieval algorithm, which requires an estimate of the uncertainty in the measured spectrum at each wavelength (see Sect. 5.1).

#### 4 GHOST flights on board the NASA Global Hawk

In February and March 2015, the GHOST instrument was installed and flown on the NASA Global Hawk aircraft (Naftel, 2014) based at NASA Armstrong Flight Research Centre in Edwards, California. The Global Hawk is an unmanned aircraft which is designed for high-altitude (up to 20 km) and long-endurance flight, and flown remotely by pilots based on the ground at NASA Armstrong. These characteristics make the Global Hawk platform well suited for atmospheric science applications which demand observations on a regional



**Figure 16.** Estimate of GHOST SNR for each band derived from integrating sphere measurements, assuming radiances typical of Global Hawk flight observations (Table 6). See text in Sect. 3.6 for details.

(as opposed to local) scale from altitudes well above the troposphere.

GHOST flew on the Global Hawk as part of a series of flights jointly supported by the NERC Co-ordinated Airborne Studies of the Tropics (CAST, Harris et al., 2017) and the NASA Airborne Tropical Tropopause Experiment (ATTREX, Jensen et al., 2017) projects. In this section we describe the installation of GHOST onto the Global Hawk and provide an overview of the three Global Hawk flights which took place during the joint CAST-ATTREX deployment in February and March 2015.

##### 4.1 Installation and operation of GHOST on board the Global Hawk

Following initial verification, testing, and calibration at the UK Astronomy Technology Centre, the GHOST instrument was shipped to the NASA Armstrong site (California, USA) in early January 2015. Prior to its integration onto the Global Hawk aircraft, GHOST was required to undergo three major testing periods: electronics and communications, representative environment (pressure and temperature), and mechan-

**Table 6.** Radiometric performance of the GHOST spectrometer, as determined from the calibration measurements described in Sect. 3.5. The reference radiances are in units of photons  $s^{-1} m^{-2} \mu m^{-1} sr^{-1}$  and are typical of the spectral radiance levels observed during the Global Hawk flights (e.g. see Fig. 19).

Band	Reference radiance	Minimum SNR	Mean SNR	Maximum SNR
1	$2.5 \times 10^{20}$	51.3	142.2	213.3
2A	$1.5 \times 10^{20}$	244.0	367.9	487.9
2B	$1.5 \times 10^{20}$	117.7	308.2	415.5
3	$4.0 \times 10^{19}$	138.5	211.1	314.5
4	$2.5 \times 10^{19}$	122.0	193.9	253.2

ical stability (vibrational). These tests were performed and checked by qualified NASA engineers, with assistance from the GHOST team, as a prerequisite to the instrument receiving permission to fly; NASA has the ability to self-qualify the aircraft and instruments it flies.

Electronics and communications testing was performed both on a lab bench using a test rig simulating the Global Hawk's communications channels, and also on the airfield concourse using the VHF (very high frequency) and X-Band communications systems once the instrument was installed on the aircraft. These tests ensured that the power drawn by the system did not exceed limits, that valid log packets were transmitted during operations, that all communications were correct (ports used and packet contents) and that, in extremis, the system could be remotely power cycled and return to operational mode. The communications system uses two basic protocols: a high rate system (over X-band) that provides TCP/IP (internet protocol) communications as one would expect on the ground, and a low rate system (over VHF) that provides very limited, multicast-UDP communications. The specifications for instruments to fly on the Global Hawk requires that full control must be possible using only this system, the data transmission rate which can be as low as a few hundred bytes every 10 s.

The pressure and temperature testing was performed in an environmental chamber designed to simulate operation under a wide range of temperatures and pressures. The entire GHOST system was installed on the floor of the chamber, then put through a series of pressure and temperature profiles, with pressures ranging from 1013 down to 56 hPa (corresponding to altitudes from sea level up to 20 km) and temperatures from 328 to 208 K. The tests lasted up to 4 h and some of the profiles were extremely rapid, demonstrating the instrument's ability to survive a rapid descent from 20 km to near sea level in a few minutes. During these tests the instrument was operational and was tested to ensure that its operational power stayed within limits, with the heaters and heat exchanger in the ATR being the main power-consuming components of the system.

The vibrational test was performed on each of three orthogonal axes (two horizontal and one vertical) but, owing to the size and weight of the instrument, the ATR, TAM, and spectrometer module units were tested separately. The testing was again performed with the system operational, although the array was not in an operational mode and was not powered up until the vibration test was complete. The vibrational specifications used were based on scenarios where forces up to several Newtons per kilogram were applied, despite the Global Hawk typically operating in a very stable and benign environment. The exact values for the pressure, temperature, and vibrational loading are solely for NASA's use and are not publicly available.

Once all the tests were completed the three sections of GHOST were integrated into the lower instrument bay of the Global Hawk (Fig. 1) on a specially designed pallet. A final combined system test (CST) on the ground with all instruments operational confirmed that GHOST was flight ready. At 15:03 UTC on 26 February the Global Hawk took off and embarked on a range flight, climbing to 19 km and then following a race track circuit to the north of Edwards Air Force Base for 6.6 h, landing at 21:38 UTC (Fig. 17). The GHOST system operated continuously and, since the high rate data communications was available for the majority of the flight, data could be transferred back in near real time for assessment. The flight demonstrated that all systems were functioning correctly, the gimbal in the TAM was tracking the solar glint spot (or remaining at nadir) as commanded and the spectrometer output was stable and consistent with expectations. Subsequently, the header data from this and subsequent science runs demonstrated that the internal temperatures (the spectrometer and the array) were stable to better than 0.1 K of the set point, and that the liquid cryogen cooling system could keep the spectrograph cold for a 20+ h flight.

#### 4.2 CAST-ATTREX flights during February and March 2015

During February and March 2015, the Global Hawk flew on three occasions as part of the CAST-ATTREX campaign. These comprised a range flight over the desert neighbouring Edwards in southern California (a test of all of the instrument and communications systems on board the Global Hawk prior to any long-range flying, as described in Sect. 4.1), and two science flights over the Pacific Ocean. These flights are summarized briefly in Table 7, whilst the flight paths are shown in Fig. 17.

The goal of the ATTREX project was to investigate the physical processes occurring in the tropical tropopause layer (TTL, Jensen et al., 2017), located between 13 and 19 km in altitude. The project exploited the unique capabilities of the Global Hawk platform to make observations of stratospheric humidity and composition. This is reflected in the instrument payload that flew with GHOST on board the Global Hawk, which included in situ sensors for water



**Figure 17.** CAST-ATTREX Global Hawk flight paths in February and March 2015: 26 February 2015 in yellow (range flight), 5 March in green (science flight), and 10 March in red (science flight).

**Table 7.** Summary of Global Hawk flights which took place under the CAST-ATTREX project during February and March 2015.

Date (UTC)	Take-off time, UTC (local)	Duration	Description
26 February 2015	15:00 (07:00)	6.6 h	Range flight over desert and mountainous regions close to Edwards, CA.
5 March 2015	04:00 (20:00)	21 h	Science flight over tropical eastern Pacific targeting profiles through the tropical tropopause layer. About 10 h of cloud-free daylight conditions on the return leg were suitable for GHOST observations.
10 March 2015	17:00 (10:00)	11.5 h	Science flight over eastern Pacific targeting clear skies for GHOST observations. The southbound flight leg was specifically located and timed to coincide with an OCO-2 overpass, whilst GOSAT also passed over the measurement region around the same time.

vapour, ice crystals, and ozone, as well as an air sampling system for post-flight laboratory analysis of chemical composition.

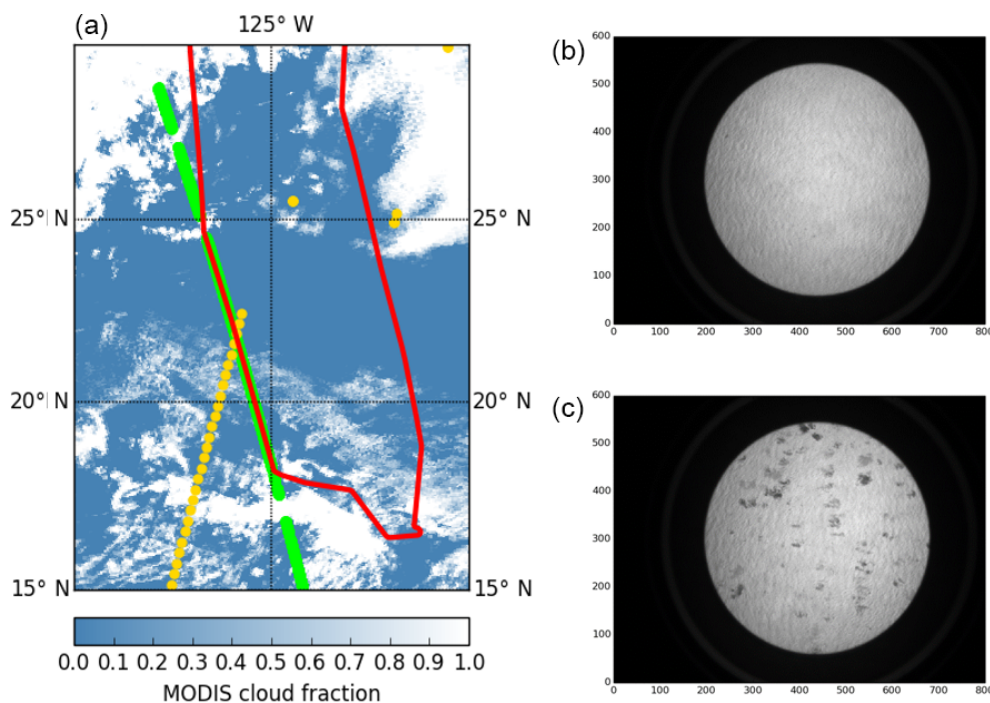
The CAST project (Harris et al., 2017) had similar objectives, looking at atmospheric composition and structure in the tropics. The 2015 Global Hawk flights, operated jointly with ATTREX, met the project objectives to demonstrate two new technologies for airborne atmospheric measurements: GHOST and an ice crystal imaging probe called AIITS (the Aerosol Ice Interface Transition Spectrometer, Stopford et al., 2015). The two CAST instruments therefore had opposing requirements for atmospheric conditions during flight, as GHOST requires the sky to be as cloud-free as possible for optimal results, whereas the AIITS team would benefit from flying through cloud as much as possible to fully test their instrument. The two science flights listed in Table 7 each address one of these two requirements, with a large proportion of the 5 March 2015 flight dedicated to vertical profiling through the TTL.

The flight on 10 March 2015, on the other hand, was tailored towards the requirements of GHOST (cloud-free skies during daylight hours). One of the flight legs was designed

to coincide both spatially and temporally with an overpass of the NASA OCO-2 (Orbiting Carbon Observatory, Crisp et al., 2017; Eldering et al., 2017) satellite during cloud-free conditions as shown in Fig. 18, providing an opportunity for comparison of the two data sets. In Sect. 5 we focus on this segment of the 10 March flight when presenting the first set of results from the GHOST spectrometer. This part of the flight also coincided with a GOSAT (Greenhouse Gases Observing SATellite, Kuze et al., 2009) overpass of the region, with the sounding locations shown in yellow in Fig. 18.

## 5 First GHOST results from the CAST-ATTREX Global Hawk flights

This section describes the first in-flight results obtained from the GHOST spectrometer, taken during the CAST-ATTREX 10 March 2015 Global Hawk flight. The first part of this section outlines the optimal estimation method used to estimate GHG concentrations from the measured spectra, including steps taken to allow for a systematic channelling effect observed in the data, whilst the second part presents the results themselves and assesses their quality.



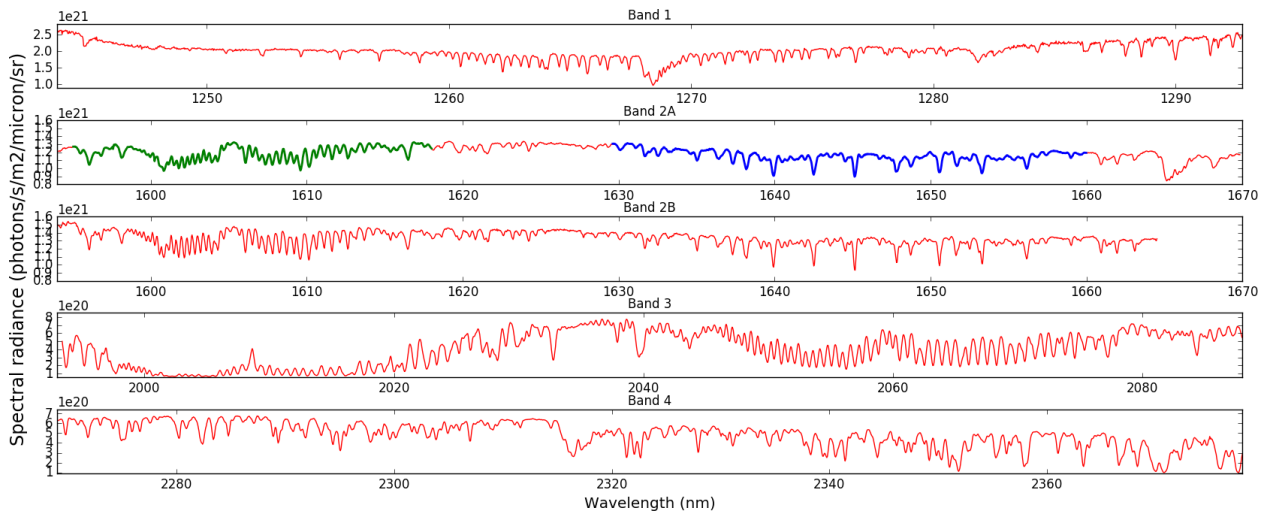
**Figure 18.** (a) 10 March Global Hawk flight path (red) plotted with sample locations of OCO-2 (green) and GOSAT (yellow) soundings. The blue–white colour scale shows the cloud fraction retrieved from MODIS (Moderate Resolution Imaging Spectroradiometer) observations. (b, c) Images from the GHOST visible camera taken during the OCO-2 overpass. Panel (b) shows cloud-free conditions towards the beginning of the flight leg, whilst (c) shows sparse cloud cover encountered towards the end of the flight leg.

### 5.1 Retrieval of GHG total column observations from GHOST spectra

The calibrated GHOST spectra (an example of a radiance spectrum recorded during this flight is shown in Fig. 19) have been analysed using the University of Leicester full physics retrieval algorithm. This algorithm uses an iterative retrieval scheme based on Bayesian optimal estimation (Rodgers, 2000) to estimate a set of atmospheric, surface, and instrument parameters, referred to as the state vector, from the radiance spectra measured by GHOST via calls to a forward model and an inverse method. The forward model describes the physics of the measurement process and relates measured radiances to the state vector. It consists of a radiative transfer (RT) model coupled to a model of the solar spectrum to calculate the monochromatic spectrum of light that originates from the sun, passes through the atmosphere, reflects from the Earth's surface or scatters from molecules or particles in the atmosphere, and is measured by the instrument (Boesch et al., 2006, 2011). We use output from two re-analysis models as the a priori estimate of the atmospheric state: the Copernicus Atmosphere Monitoring Service (CAMS, Bergamaschi et al., 2007, 2009) for CH<sub>4</sub> profiles as a function of pressure, and CarbonTracker (CT2016, Peters et al., 2007, with updates documented at <http://carbontracker.noaa.gov>, last access: 29 August 2018) for similar profiles of CO<sub>2</sub>, H<sub>2</sub>O, and temperature.

The forward model of the retrieval algorithm employs the LIDORT radiative transfer model (Spurr, 2008), which we use to calculate the upwelling spectral radiance at the height of the aircraft. The monochromatic spectrum is then passed through the instrument model where it is convolved with the instrument line shape function to simulate the measured radiances at the appropriate spectral resolution. The inverse method employs the Levenberg–Marquardt modification of the Gauss–Newton method to find the estimate of the state vector with the maximum a posteriori probability, given the measurement (Connor et al., 2008).

Here, we only present results from a fit to the CO<sub>2</sub> and CH<sub>4</sub> spectral bands in Band 2A (coloured green and blue respectively in Fig. 19) to infer the ratio of CO<sub>2</sub> to CH<sub>4</sub>, according to the proxy retrieval approach (Parker et al., 2011; Frankenberg et al., 2006). The advantage of this approach is the reduced sensitivity to aerosols due to a cancellation of the aerosol effects in the retrieved CO<sub>2</sub> and CH<sub>4</sub> columns, so subsequently aerosols do not have to be considered for the retrieval. In using the proxy method, we assume that very similar distributions of light paths contribute to the observed spectra at the absorption wavelengths of both the gas of interest and its proxy for the total air column, introducing the requirement that we use spectrally neighbouring fitting windows. In addition, the method assumes that our measurement exhibits equivalent sensitivity to both gases at the heights at



**Figure 19.** Example of sun-glint radiance spectra measured by GHOST during the 10 March 2015 Global Hawk flight, with solar zenith angle (SZA) of  $36.8^\circ$ . The fit windows we use in Sect. 5.1 to retrieve  $\text{CO}_2$  and  $\text{CH}_4$  from Band 2A are highlighted in green and blue respectively.

which the greatest deviations from the expected light path occur as a result of scattering (Frankenberg et al., 2006). The retrieved state vector elements are listed in Table 8. In future, we plan to also adopt a full-physics retrieval approach where aerosol parameters are retrieved together with  $\text{CO}_2$  by a simultaneous fit to the  $\text{O}_2$  band (Band 1), the weak  $\text{CO}_2$  (or  $\text{CH}_4$ ) band (Band 2) and the strong  $\text{CO}_2$  band (Band 3).

During our initial attempts to run the retrieval algorithm on the flight spectra, we noticed a persistent systematic spectral oscillation in the spectral residuals. On revisiting the calibration measurements taken in the laboratory, a similar spectral oscillation was found when taking the difference between spectra measured with and without the TAM included in the optical chain (Appendix A). When light is transmitted by two parallel surfaces, a sinusoidal interference pattern as a function of wavelength is produced. The period of the oscillation at a given wavelength is proportional to the distance between the two surfaces, and the refractive index of the medium between them. Analysis of the period of the oscillation observed in each band suggested that an air gap 0.2 mm thick could be the source of the interference pattern. Of the optical components within the TAM we identified the depolarizer as the most likely cause, since it includes an air gap of the correct thickness to produce the periodicity of oscillations observed in the GHOST spectra. To resolve this issue, in September 2017 we fitted GHOST with a replacement depolarizer which does not include an air gap and therefore does not introduce any spectral interference.

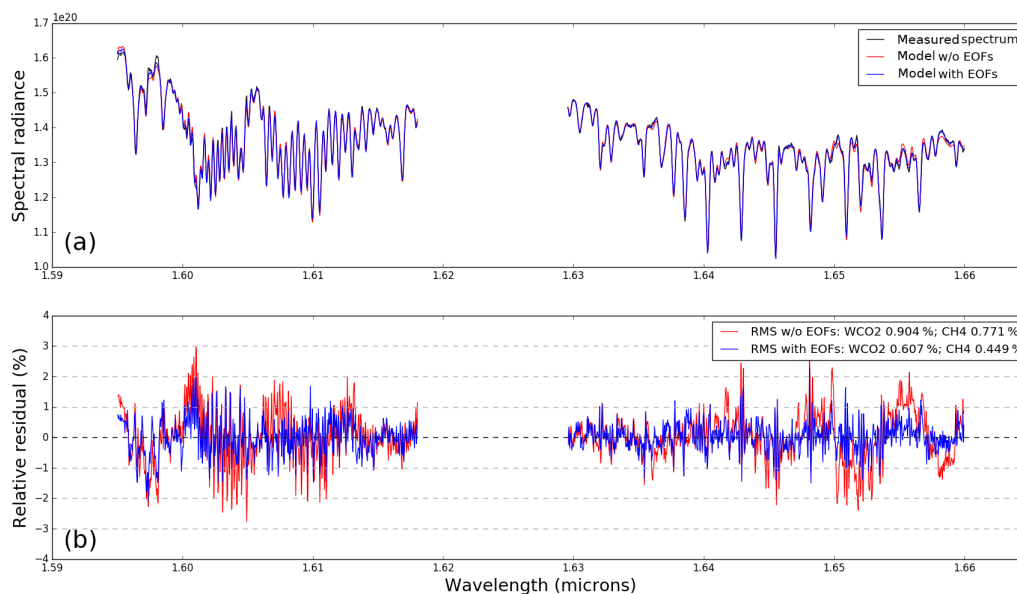
In our analyses of flight data recorded before the depolarizer was replaced, we have to take into account this systematic spectral effect. We do this by using the whole GHOST Global Hawk data set to calculate empirical orthogonal functions (EOFs) describing the variability in the spectral fit residuals obtained during the initial retrieval process (follow-

ing the method used in OCO-2 retrievals, JPL, 2015, to account for systematic errors in the measured spectra). We then run the retrieval algorithm again, this time incorporating into the fit the three EOFs accounting for the most variability in the spectral residuals. Three extra parameters are added to the state vector, which are scaling factors applied to each of the EOFs before they are added to the forward model spectrum. The improvement in the spectral fit is clearly demonstrated by the spectral residuals shown in Fig. 20, where the red and blue spectra show the residuals obtained without and with EOFs included in the retrieval. In the example shown, including the EOFs in the spectral fit reduces the rms residuals by 33 % and 42 % in the  $\text{CO}_2$  and  $\text{CH}_4$  fit windows.

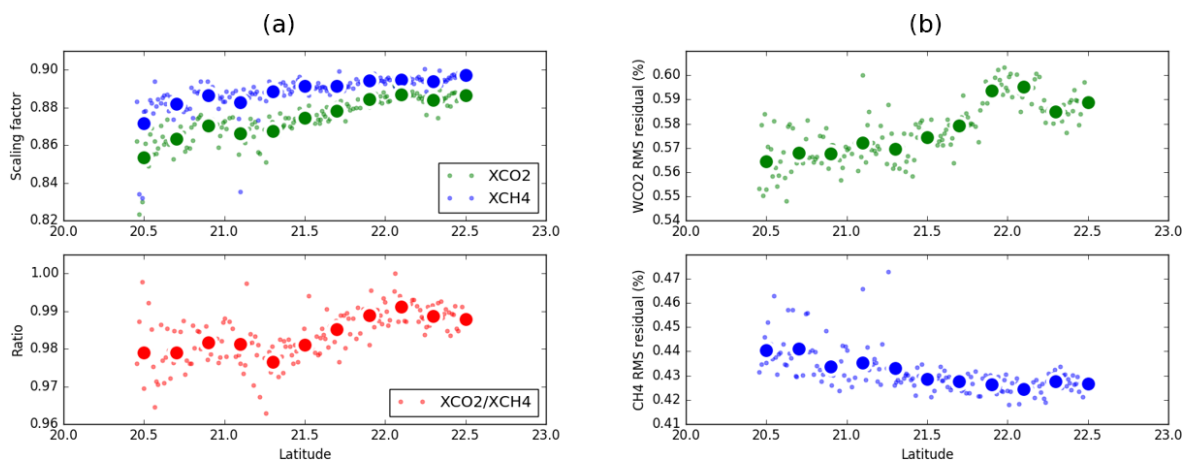
## 5.2 First retrieval results from GHOST spectra

We use this retrieval method to obtain our first set of results for  $\text{XCO}_2$  and  $\text{XCH}_4$  from a set of GHOST flight spectra, which were measured during the 10 March 2015 Global Hawk flight described in Sect. 4. We focus in particular on the 218 spectra observed from 21:54 UTC onwards during the OCO-2 and GOSAT overpasses. On applying quality filters based on thresholds for the number of algorithm iterations and the  $\chi^2$  value of the residual, 175 observations remain. We choose the threshold for the number of iterations before achieving convergence to be seven (i.e. convergence on a solution must take place after six iterations or fewer), based on the identification of outlying data points in histograms of the output retrieval metrics and results. In addition we apply a  $\chi^2$  minimum threshold value of 1.0, since values below 1.0 indicate an unphysical result (Rodgers, 2000). The left panel of Fig. 21 shows how the retrieved  $\text{XCO}_2$  (green),  $\text{XCH}_4$  (blue) and ratio (red) values vary along this leg of the flight, whilst the right panels show how the rms resid-





**Figure 20.** Example spectral fit residuals for the Band 2A CO<sub>2</sub> (left) and CH<sub>4</sub> (right) fit windows, using a sun-glint spectrum measured during the 10 March 2015 Global Hawk flight. The measured and optimized forward modelled spectra (both with and without EOFs included in the retrieval algorithm) are plotted in (a), whilst (b) shows the spectral fit residuals in each case (modelled – measured) as a percentage of the measured spectrum.



**Figure 21.** (a) Scatter plots for the Band 2A retrieved XCO<sub>2</sub> (green) and XCH<sub>4</sub> (blue) scaling factors, along with the ratios (red), from spectra measured during the OCO-2 overpass of the 10 March 2015 Global Hawk flight. (b) Scatter plot of rms residual for the Band 2A CO<sub>2</sub> (green) and CH<sub>4</sub> (blue) fit windows. The data are averaged into 0.2° latitude bins (the average for each bin is indicated by the larger circles).

ual values behave for the quality-filtered retrievals. This metric, along with the  $\chi^2$  values (not shown), indicate that the spectral fits of the CH<sub>4</sub> window using the OCO retrieval algorithm are superior to those of the CO<sub>2</sub> window.

The range of values covered by the ratio between the two scaling factors, as shown by the red data points in Fig. 21, is of the order of 1.5%. When applied to the prior total column concentration of CO<sub>2</sub> via the proxy retrieval method described in Sect. 5.1, this corresponds to a variation in XCO<sub>2</sub> along this flight leg of around 6 ppm. This is greater than that

seen over the same latitude range in both the OCO-2 observations and the CarbonTracker atmospheric model, which both indicate a spread in XCO<sub>2</sub> values of around 1.5 ppm. The variability in the scaling factor ratio is driven more by the retrieved CO<sub>2</sub> scaling factor than that of CH<sub>4</sub>, as can be seen from the top-left panel of Fig. 21. The divergence of the CO<sub>2</sub> scaling factor from the CH<sub>4</sub> scaling factor also results in a negative bias compared with the OCO-2 data and the CarbonTracker model output, which varies from 2 ppm up to around 8 ppm along the flight leg. Given that OCO-2 makes obser-

**Table 8.** Description of the state vector.

Quantity	Number of elements	Description
CH <sub>4</sub>	1	Scaling factor (no units) applied to a priori vertical profile
CO <sub>2</sub>	1	
H <sub>2</sub> O	1	
HDO	1	
Temperature	1	Shift (°K) added to a priori vertical profile.
Albedo	5	Coefficients of fourth-order polynomial describing surface albedo (no units) as a function of pixel number.
Dispersion	5	Coefficients of fourth-order polynomial describing wavelength (m) as a function of pixel number.
Zero level	1	Wavelength-independent scaling factor (no units), applied to radiance spectrum and then added to the approximate effect of stray light in the instrument.
EOFs	3	Wavelength-independent scaling factors (no units) applied to empirical orthogonal functions (see text in Sect. 5.1), which are then added to the spectrum to account for spectral systematic errors.

vations at a higher spatial density than GHOST (because of its 8 pixel cross-track imaging capability), we would expect OCO-2 data to be more representative of the variability in XCO<sub>2</sub> along the overpass compared with GHOST. We can conclude from this that the change in discrepancy between the two data sets along the flight track is unlikely to be a result of spatial changes in XCO<sub>2</sub> that OCO-2 could be missing as a result of mismatches in spatial resolution and location.

When using the proxy retrieval method, we are assuming that the two spectral ranges used are close enough in wavelength space that any systematic errors are eliminated when taking the ratio. However, this would not work (and could subsequently introduce the observed divergence in scaling factors obtained from the two spectral ranges used) in the presence of an instrumental error or effect which has sufficient wavelength dependence within the wavelength ranges observed by GHOST. Examples of these include unaccounted-for stray light incident on that part of the detector, or a wavelength-dependent error in the radiometric calibration. Whilst we are still investigating the underlying cause of this bias, we anticipate that an improved understanding of stray light effects in the instrument through ongoing laboratory measurements will help us to correct for the observed bias, as will comparison of retrieval results from future GHOST flights with those from ground-based validation sites.

## 6 Summary

GHOST is a new shortwave-infrared grating spectrometer, which employs a unique compact design to optimize the science benefits provided (with regards to wavelength ranges covered and spectral resolution) given the small size of its op-

tical payload. As described in Sect. 2, this has been achieved by adapting advances in optical technology originally designed for astronomy applications, namely the use of fibre bundles to transfer light from the fore-optics into the spectrometer, and the imaging of multiple spectral bands onto a single detector array with a single diffraction grating. Through the laboratory testing and calibration discussed in Sect. 3, we have demonstrated that the GHOST radiometric and spectral performance is suitable for retrieving total column concentrations of greenhouse gases from the measured shortwave-infrared spectra.

The CAST-ATTREX Global Hawk flight campaign in January–March 2015 (Sect. 4) was our first opportunity to operate GHOST on board an aircraft. Following extensive engineering and communications testing at NASA Armstrong, GHOST was successfully integrated into the Global Hawk aircraft and flew for the first time on 26 February 2015. During the campaign, GHOST took part in three flights on board the Global Hawk for a total duration of approximately 39 h, maintaining vacuum and thermal stability throughout up to altitudes of 20 km above sea level. Data from the 10 March 2015 flight are analysed in Sect. 5, which shows for the first time greenhouse gas retrievals from spectra measured in-flight by GHOST.

This paper has introduced the GHOST instrument, and shown its potential for airborne greenhouse gas remote sensing through initial results from its first science flights. Our future plans for this data set include applying a full physics retrieval to the measured spectra (as discussed in Sect. 5.1), which will allow for a more like-for-like comparison with the OCO-2 measurements during the 10 March 2015 overpass. In addition to the CAST-ATTREX Global Hawk flights we have also flown GHOST over the UK on board the NERC Air-

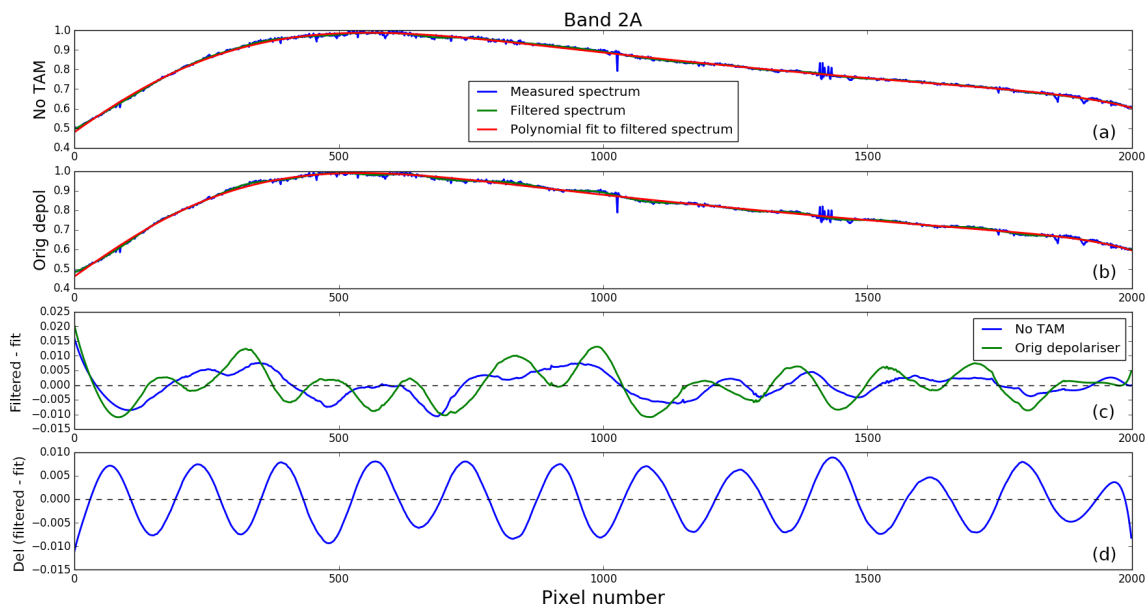
borne Research Facility (ARF) Dornier 228 aircraft in April and May 2015, targeting emissions hot spots. Future plans include analysis of this data set, as well as data from further flights supported by the ARF which took place in June 2018. These flights will investigate how multi-angle views of a scene can improve the retrieval accuracy through better representation of scattering effects in the atmosphere, as well as targeting ground-based remote sensing instruments in the UK, which can be used for validation of the GHOST results. Future flights (including those completed in 2018) will benefit from a new depolarizer unit, which has now been installed in the TAM, eliminating the spectral oscillations that affected previous measurements (see Appendix A). In addition we are working on further calibration measurements prior to these flights, which will include characterization of stray light effects and will enhance our understanding of the instrument (for example, explaining the different spectral radiances observed in bands 2A and 2B as seen in Fig. 19), therefore

improving our ability to retrieve GHG concentrations from the measured spectra. GHOST is also suitable for more dedicated intercomparison studies with greenhouse gas observing satellites, including the Sentinel-5 Precursor, which observes CH<sub>4</sub> using a similar wavelength range to GHOST's Band 4. We anticipate that GHOST will prove to be a valuable tool for regional and local-scale studies of the atmospheric greenhouse gas budget, in addition to acting as an airborne technology demonstrator for future satellite missions.

*Data availability.* GHOST flight data will be made available via the UK Centre for Environmental Data Analysis archive (<http://catalogue.ceda.ac.uk>, last access: 10 September 2018) once the whole data set has been fully processed. The raw data and processing code in their current form can be accessed by contacting Neil Humpage.

### Appendix A: Observation of depolarizer interference effect in laboratory measurements

The effect of the depolarizer discussed in Sect. 5.1 on GHOST Band 2A measurements is shown in Fig. A1. We perform measurements with the TAM removed from the optical chain by decoupling the optical fibre bundle from the TAM and feeding it directly into the output port of the integrating sphere. This results in observed intensities that are not identical, since the incoming light is no longer being focused onto the fibre bundle by the TAM fore-optics. To allow for this, we scale the two spectra such that the maximum value in each is equal to 1. We then apply a noise filter and perform a polynomial fit to isolate the background signal. The bottom panel shows the difference between the two measurements once these parts of the spectra are removed, leaving behind only the spectral effect of the depolarizer. Note that these are uncalibrated measurements: the radiometric calibration coefficients obtained from the integrating sphere measurements (Sect. 3.5) were obtained with the TAM in place, so are only applicable in that configuration.



**Figure A1.** Uncalibrated Band 2A measurements of integrating sphere output. **(a)** Spectrum measured without the TAM in place (blue), which is then noise filtered (green) and approximated by a polynomial (red); **(b)** is the same as **(a)** but with the TAM in place; **(c)** difference between noise-filtered spectrum and the polynomial fit in each of the two cases; and **(d)** difference between the two residuals shown in **(c)**, isolating the effect of the depolarizer on the spectrum.

*Author contributions.* NH prepared the manuscript (with contributions from all co-authors), performed the calibration measurements, developed the data processing methodology and code, operated the instrument during the NASA Armstrong flight campaign, and produced the first retrieval results shown here. HB and PIP defined the science requirements that guided the GHOST instrument design, and reviewed the manuscript prior to its initial submission. The retrieval algorithm used in this work was originally developed by HB. The introduction section of the manuscript was drafted by PIP. AV developed the instrument data handling and control software, supported the Global Hawk deployment (particularly testing of the communication links between instrument, aircraft, and ground), and drafted the instrument description section. PPB co-ordinated the design and build of GHOST at UK-ATC, as well as organizing and supporting the NASA Armstrong flight campaign. MW was the lead optical engineer, responsible for designing the spectrometer concept and other optical components of the instrument. DP and JS were the lead mechanical engineers on the GHOST project and also supported the testing and deployment of GHOST on the Global Hawk at NASA Armstrong. NB developed the detector control software used by the instrument.

*Competing interests.* The authors declare that they have no conflict of interest.

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