



# Pressure-Related Universal Previtreous Behavior of the Structural Relaxation Time and Apparent Fragility

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The report presents the evidence for the hypothetically "universal" previtreous behavior of the pressure related apparent fragility:  $m_T(P) \propto 1/(P^* - P)$ , where  $P^*$  is the extrapolated singular pressure. This finding was the basis for deriving the "model-free" dependence for the pressure evolution of the structural relaxation time:  $\tau(P) = \tau_o^P (P^* - P)^{-\Psi}$ . All these led to the new way of testing the dynamic crossover phenomenon via  $1/m_T(P)$  vs. Pplot. Finally, the behavior of electric conductivity in the previtreous domain is discussed. The experimental evidence covers 8\*OCB (liquid crystal), EPON 828 (resin), diisobutyl phthalate, and propylene carbonate (low molecular weight liquids). Experiments were carried up to extreme  $P \sim 2.2$  GPa, in the "bulk" measurement capacitor. This report also contains a summary of existing descriptions of the pressure evolution of structural relaxation time or viscosity on approaching the glass transition.

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# INTRODUCTION

The glass transition remains the grand challenge of the condensed matter physics and material engineering (Kennedy, 2005; Berthier and Ediger, 2016; Kremer and Loidl, 2018; Royall et al., 2018; Tong and Tanaka, 2018). Decades of research yielded the excellent experimental and theoretical evidence, based on increasingly sophisticated approaches (Donth, 2007; Berthier and Ediger, 2016; Kremer and Loidl, 2018; Royall et al., 2018; Tong and Tanaka, 2018). However, the long-awaited cognitive breakthrough is still elusive. Notable problems appear even for the hallmark feature of the previtreous dynamics: the super-Arrhenius (*SA*) evolution of viscosity  $\eta$  (*T*) or the structural (*primary, alpha*) relaxation time  $\tau$  (*T*) (Ngai, 2011; Berthier and Ediger, 2016; Kremer and Loidl, 2018; Royall et al., 2018). The general *SA* relation has the following form (Donth, 2007; Ngai, 2011):

$$\tau(T) = \tau_0 exp\left(\frac{E_a(T)}{RT}\right) \tag{1}$$

where P = 0.1MPa,  $T > T_g$ ,  $T_g$  is for the glass temperature and R means the gas constant;  $E_a(T)$  denotes the apparent, temperature dependent, activation energy. This is related to the SA behavior. For the domain where for  $E_a(T) = E_a = const$ , one obtains the basic Arrhenius (A) relation. A similar relation describes  $\eta(T)$  changes.

The prefactor  $\tau_0$  denotes the terminal value at the infinite temperature, for which  $\tau_0 = 10^{-14}s$  is most often assumed. It is correlated with "infinite" temperature studies or the estimation the time scale of atomic vibrations,  $\tau_0 = h/kT$  (Donth, 2007; Ngai, 2011). However, when considering various glass formers ranging from low molecular weight liquids to liquid crystals and plastic crystals  $10^{-17}s < \tau_0 < 10^{-10}s$  is evidenced (Drozd-Rzoska and Rzoska, 2006; Lunkenheimer et al., 2010; Martinez-Garcia et al., 2013).

The isothermal compressing constitutes the alternative path of approaching the glass transition. It offers unique possibilities of decoupling phenomena overlapping under atmospheric pressure, the selective focus on the free volume related properties or revealing the impact of phenomena "hidden" under pressure (Roland et al., 2005, 2008; Drozd-Rzoska et al., 2008a,b; Rzoska et al., 2010; Floudas et al., 2011; Kondrin et al., 2012; Rzoska, 2017).

The relation for describing the pressure-viscosity behavior was first proposed by Barus (*B*) via the relation  $\eta$  (*P*)  $\propto exp(\alpha P)$ ,  $\alpha = const$ , (Barus, 1893). For describing the complex dynamics in the previtreous domain, one can consider the super-Barus (*SB*) relation, with the pressure dependent coefficient  $\alpha$  (*P*):

$$\tau(P) = \tau_0^P exp(\alpha(P) \times P) = \tau_0^P exp\left(\frac{V_a(P)}{RT}P\right)$$
(2)

where T = const,  $P < P_g$ , and  $P_g$  is for the glass (vitrification) pressure;  $V_a$  (*P*) denotes the apparent activation volume (Roland et al., 2005, 2008; Rzoska et al., 2010; Floudas et al., 2011; Rzoska, 2017);  $\tau_{ref.} = \tau_0^P$  is the reference prefactor.

The prefactor in *SB* Equation (2) can be approximated by the relaxation time under atmospheric pressure for the selected isotherm. Consequently, it ranges between  $10^{-10}s$  and 10s for the same glass former (Drozd-Rzoska et al., 2008a,b; Rzoska, 2017). The general *SA-SB* formula can be obtained linking Equations (1, 2) (Roland et al., 2005; Floudas et al., 2011):

$$\tau (T, P) = \tau (T) \exp\left(\frac{PV_a}{RT}\right) = \tau_0 \exp\left(\frac{E_a(T) + PV_a(P)}{RT}\right) (3)$$

where  $T > T_g$  and  $P < P_g$ . The similar relation occurs for  $\eta(T, P)$  changes.

Following Equation (3), the isobaric temperature evolution is described by:

$$\tau (T) = \left[\tau_0 exp\left(\frac{PV_a(P)}{RT}\right)\right] exp\left(\frac{E_a(T)}{RT}\right)$$
$$= \tau_{ref.} exp\left(\frac{E_a(T)}{RT}\right)_p$$
(4)

where P = const.

Equation (4) coincides with the SA Equation (1) for P = 0, yielding  $\tau_{ref.} = \tau_0$ . In practice, such isobar can be approximated by temperature studies under atmospheric pressure ( $P \approx 0.1MPa$ ). It is notable that in high-pressure studies the pressure stabilization and determination hardly (if

at all) reaches  $\pm 0.2$ *MPa*. For studies under moderate and high pressures Equation (4) suggest the more complex form of the prefactor.

Previtreous temperature changes of  $\tau(T)$  or  $\eta(T)$  are inherently associated with the "Angell plot," recognized as the hallmark picture for the glass transition physics (Angell, 1985; Böhmer et al., 1993; Donth, 2007; Ngai, 2011; Berthier and Ediger, 2016; Kremer and Loidl, 2018; Royall et al., 2018; Tong and Tanaka, 2018). It enables the common presentation of the previtreous dynamics for different glass formers via the normalized plot  $log_{10}\tau(T)$  or  $log_{10}\eta(T)$  vs.  $T_g/T$ , assuming  $\tau$   $(T_g) = 10^2 s \text{ or } \eta$   $(T_g) = 10^{13} Poise$  (Angell, 1985; Böhmer et al., 1993). This plot led to the concept of fragility as the metric of the SA dynamics:  $m = m_P(T_g) = \left[ d \log_{10} \tau(T) / d(T_g/T) \right]_{T=T_g}$ being one of the key concepts of the glass transition physics (Berthier and Ediger, 2016; Kremer and Loidl, 2018; Royall et al., 2018; Tong and Tanaka, 2018). In the Angell plot, the basic Arrhenius behavior manifests as the straight line for which  $m = m_{\min}$  =  $log_{10}\tau(T_g) - log_{10}\tau_0 = 16$ , assuming  $\tau_0 = 10^{-14} s$  (Böhmer et al., 1993). For the isothermal, pressure related previtreous behavior the plot  $log_{10}\tau$  (P) or  $log_{10}\eta$  (P) vs.  $P/P_g$  has been indicated as the counterpart of the Angell plot, leading to the pressure related fragility  $m_T(P_g) = m^P =$  $\left[ d \log_{10} \tau (P) / d \left( P / P_g \right) \right]_{P=P_g}$  (Roland et al., 2005; Rzoska et al., 2010; Floudas et al., 2011). However, for such plots, one obtains a "fan" of curves for the same glass former, due to the fact that  $log_{10}\tau_{ref.}$  ranges between -10 and 1 for different tested isotherms. For the basic Barus behavior  $(V_a(P) = V_a =$ const in the given domain of pressures) the "minimal" fragility  $m_{\min}^{P} = log_{10}\tau (P_g) - log_{10}\tau_{ref.}$  can range between 1 and 12, for an arbitrary glass former. To remove the inconsistency between temperature and pressures paths it was proposed to take into account that a solid/liquid can be isotropically stretched down to the absolute stability limit spinodal ( $P_{SL} < 0$ ), hidden under negative pressures (Lukacs and Martinas, 1990; Sciortono et al., 1995; Imre et al., 1998, 2002). Notable is the experimental evidence of the smooth passing P = 0, from the "positive" to the negative pressures domains in glass-forming liquids (Angell and Qing, 1989; Imre et al., 2002). Consequently, the plot  $log_{10}\tau$  (P) vs.  $\Delta P = P - P_{SL}$  as the pressure counterpart of the "Angell plot" was proposed (Drozd-Rzoska, 2005; Drozd-Rzoska et al., 2007, 2008b). This resulted in the approximately constant prefactor:  $\tau_{ref.} = \tau (P_S) \sim 10^{-11} s$  and then the "universal" minimal fragility  $m_{\min}^p \sim 13$ . All these led to the new definition of the apparent fragility  $m_T^{\Delta P}$ , which can be linked to the "old" one as follows:

$$m_T^{\Delta P} = \frac{d \log_{10} \tau (P)}{d \left( \Delta P / \Delta P_g \right)} = \Delta P_g \frac{d \log_{10} \tau (P)}{d \left( \Delta P \right)} = \frac{\Delta P_g}{P_g} \frac{d \log_{10} \tau (P)}{d \left( P / P_g \right)}$$
$$= \frac{\Delta P_g}{P_g} m_T (P) \tag{5}$$

where  $\Delta P = P - P_{SL}$ ,  $\Delta P_g = P_g - P_{SL}$  and  $P \le P_g$ 

General SA and SB equations for portraying experimental data cannot be used directly, because of unknown forms of the apparent activation energy and activation volume dependences.

Consequently, "replacement equations" are used (Donth, 2007; Ngai, 2011; Kremer and Loidl, 2018; Royall et al., 2018; Tong and Tanaka, 2018). For temperature studies under the atmospheric pressure the dominant role plays the Vogel-Fulcher-Tammann (VFT) equation (Vogel, 1921; Fulcher, 1925; Tammann, 1925; Donth, 2007; Ngai, 2011; Kremer and Loidl, 2018; Royall et al., 2018; Tong and Tanaka, 2018):

$$\tau (T) = \tau_0 exp\left(\frac{D_T T_0}{T - T_0}\right) \tag{6}$$

where  $T > T_g$  and the VFT singular temperature  $T_0 < T_g$ ;  $D_T$  is the fragility strength related to the fragility via  $D_T = m_{\min}^2 ln10/(m - m_{\min})$  (Böhmer et al., 1993). In the physics of polymers the Williams-Landel-Ferry (WLF) relation, the parallel of Equation (6), is used (Williams et al., 1955; Donth, 2007; Ngai, 2011).

Originally, the VFT equation was introduced empirically (Vogel, 1921; Fulcher, 1925; Tammann, 1925) and subsequently derived as the output "checkpoints" of significant glass transition models. One can recall here the free volume model (Turnbull and Cohen, 1961; Betancourt et al., 2015; Hao, 2015), Adam-Gibbs entropic models (Adam and Gibbs, 1965; Schneider et al., 1999; Dudowicz et al., 2006), random first-order transition (RFOT) theory (Wolyness and Lubchenko, 2013; Lerner and Bouchbinder, 2018), and Tanaka's "critical" model (Tanaka et al., 2010; Tong and Tanaka, 2018). The hypothetical "universal" meaning of the VFT for the previtreous behavior results from the enormous experimental evidence (Rzoska et al., 2010; Berthier and Ediger, 2016; Kremer and Loidl, 2018; Royall et al., 2018; Tong and Tanaka, 2018). Notwithstanding, significant objections against its fundamental validity appeared in the last two decades:

- (i) One of the key arguments for the uniqueness of the VFT description is the empirical coincidence between the VFT singular temperature  $T_0$  and the Kauzmann temperature  $T_K$ (Kauzmann, 1948), i.e., the "dynamic" and "thermodynamic" estimations of the ideal glass transition temperature (Berthier and Ediger, 2016; Kremer and Loidl, 2018). However, there is clear evidence that  $0.8 < T_0/T_K < 2.2$  (Tanaka, 2003; Martinez-Garcia et al., 2014).
- (ii) The root-mean-square residual analysis showed the prevalence of other than VFT relations for portraying τ (T) or η (T) experimental data, tested for several "popular" low molecular weight liquids and polymeric glass formers (Richert, 2000; Hecksher et al., 2008; Lunkenheimer et al., 2010; Zheng and Mauro, 2017).
- (iii) The linearized derivative-based and distortions-sensitive analysis showed a clear preference for the critical like portrayal in the ultraviscous domain close to  $T_g$ :  $\tau$  (T) =  $\tau'_0(T T_C)^{-\varsigma}$ , where  $T_C < T_g$  and the exponent 8.5 <  $\varsigma < 15$ , for glass forming liquid crystals, plastic crystals and also polystyrene, xylitol, propanol,... (Drozd-Rzoska and Rzoska, 2006; Drozd-Rzoska et al., 2010; Martinez-Garcia et al., 2013).
- (iv) The case-sensitive analysis of the apparent activation energy index  $I_{DO}(T) = -dlnE_a(T)/dlnT =$

 $[dE_a/E_a]/[dT/T]$  (Dyre and Olsen, 2004) questioned the general validity of the VFT/WLF portrayal (Hecksher et al., 2008; McKenna, 2008; Martinez-Garcia et al., 2013, 2014; Martinez-Garcia et al., 2015).

The empirical critique of the VFT equation led to the development and success of alternative model relations. One can recall the MYEGA (Waterton-Mauro) equation (Mauro et al., 2009), Avramov-Milchev model relation (Avramov and Milchev, 1998), Schmidtke-Petzold-Kahlau-Hofmann-Rössler scaling relation (Schmidtke et al., 2012) or Elmatad-Garrahan-Chandler model dependence (Elmatad et al., 2009).

The discussion of the pressure (isothermal) previtreous behavior often recalls studies by Johari and Whalley (JW) in superpressed glycerol as the reference (Johari and Whalley, 1972), which introduces the following relation:

$$\tau(P) = \tau_{ref.} exp\left(\frac{J}{P_0 - P}\right) \tag{7}$$

where J = const,  $P < P_g$  and  $T \sim 20^{\circ}C$ ; the extrapolated singular pressure  $P_0 > P_g$ .

Measurements were carried out using the broadband dielectric spectroscopy up to frequency f = 105 KHz, for pressures P < 5.3GPa (Johari and Whalley, 1972). Extreme pressure studies were possible only via the anvil-cell highpressure technique, inherently associated with a minimal pressurized volume and then very small measurements capacitor with the micrometric gap between its plates (Roland et al., 2005; Rzoska et al., 2010; Floudas et al., 2011). The qualitative development of the broadband dielectric spectroscopy (BDS) which occurred four decades ago enabled the scan of hundreds of frequencies ranging from microHz to few GHz with the resolution of 5-6 relevant digits (Kremer and Schönhals, 2003). Consequently, BDS has become the basic tool for studying the inherently multi-time scale complex dynamics in glass forming systems (Kremer and Schönhals, 2003; Berthier and Ediger, 2016; Kremer and Loidl, 2018; Royall et al., 2018). Notwithstanding, the application of BDS for high-pressure studies is limited to frequencies f < 10MHz: approaching the GHz frequency range remains the future challenge (Roland et al., 2005; Rzoska et al., 2010; Floudas et al., 2011). In the year 1998, the application of new BDS facilities and the new design of the measurement capacitors (Rzoska et al., 2018) enabled obtaining the highresolution  $\tau$  (P) experimental data for ultraviscous glycerol compressed up to 0.35 GPa (for  $T \sim 260K$ ). Their analysis showed the limited adequacy of Equation (7) and the fair portrayal via the empirical relation (Paluch et al., 1998):

$$\tau(P) = \tau_{ref.} exp\left(\frac{J(P)}{P_0 - P}\right) = \tau_{ref.} exp\left(\frac{D_P P}{P_0 - P}\right), \quad (8)$$

where  $D_P$  is the fragility strength for the pressure path; the prefactor  $\tau_{ref.}$  has the same meaning as in *SB* Equation (2).

Equation (8) was "designed" to enable approximations via JW Equation (7) or via the basic Barus relation, in properly selected

"terminal" ranges of pressures. It is worth stressing that the JW Equation (7) cannot be reduced to the basic Barus form. The extension of Equation (8) into the negative pressures domain requires the substitution mentioned above:  $P \rightarrow \Delta P = P - P_{SL}$  (Drozd-Rzoska, 2005; Drozd-Rzoska et al., 2007, 2008a,b):

$$\tau (P) = \tau_{SL} exp\left(\frac{D_P^{SL} \Delta P}{P_0 - P}\right)$$
(9)

where  $D_P^{SL}$  is the corrected by the impact of the stability limit (*SL*) pressure fragility strength.

This relation is associated with four fitted coefficients, i.e., more than the optimal number of three adjustable parameters (Donth, 2007; Ngai, 2011; Kremer and Loidl, 2018). The number of fitted parameters in Equation (9) can be reduced by the direct estimation of  $P_{SL} < 0$  pressure, but this constitutes the extreme experimental challenge (Imre et al., 2002). Notwithstanding, one can support the analysis via Equations (8, 9) by the distortion-sensitive and derivative-based analysis of experimental data, yielding (Drozd-Rzoska, 2005; Drozd-Rzoska et al., 2007; Drozd-Rzoska et al., 2008a,b):

$$\left[\frac{dln\tau (P)}{dP}\right]^{-1/2} = (D_P P_0)^{-1/2} P_0 - (D_P P)^{-1/2} P = A + BP$$
(10a)

$$\left[\frac{dln\tau (P)}{dP}\right]^{-1/2} = \left[D_P^{SL} (P_0 - P_{SL})\right]^{-1/2} P_0$$
$$-\left[D_P^{SL} (P_0 - P_{SL})\right]^{-1/2} P = A + BP$$
(10b)

where Equation (10a) is linked to Equation (8) and Equation (10b) to Equation (9).

Relations (8) and (9) are associated with the same value of PVFT singular pressure  $P_0$  but different fragility strengths:  $D_P^{SL} = D_P [(P_0 - P_{SL})/P_0]$  (Drozd-Rzoska et al., 2008a,b). Equations 10a,b offer the estimation of key parameters in Equations (8, 9) via the simple linear regression fit, supporting the final non-linear analysis of experimental data.

In the last three decades Equation (8), due to its simplicity and the link to fragility via the fragility related coefficient  $D_P$ , has become the key tool for describing  $\tau(P)$  and  $\eta(P)$ experimental data in compressed glass-forming systems (Roland et al., 2005; Rzoska et al., 2010; Floudas et al., 2011; Rzoska, 2017; White and Lipson, 2018). Despite this success, there are still no theoretical models deriving Equation (8), often recalled as the pressure counterpart of the VFT relation: the PVFT equation (Roland et al., 2005; Floudas et al., 2011). In the opinion of the author, the latter name can be justified by the fact that it is possible to transform the VFT Equation (6) into the PVFT Equation (8) via the simple substitution T = A/P :  $\tau(T) = \tau_0 exp [D_T T_0/(T - T_0)]$  $\rightarrow$ =  $\tau_0 exp \left[ D_T \left( A/P_0 \right) / \left( (A/P) - (A/P_0) \right) \right]$  $\tau_0 exp [D_T (A/P_0)/((AP_0 - AP)/P_0P)] =$ 

 $= \tau_0 exp [D_T P/(P_0 - P)]$ . The latter suggest the coincidence between  $\tau_0, D_T$  in the VFT Equation (6) and  $\tau_0, D_P$  in the PVFT Equation (8), but in practice they differ very strongly.

However, the coincidence between these coefficient appears when considering the substitution  $T = A/\Delta P$  into the VFT equation (6), what leads to the corrected PVFT Equation (9). In the opinion of the author this can be considered as the argument for the only "effective" validity of the basic PVFT Equation (8).

However, such a simple link leads to the question that if significant problems with describing  $\tau$  (*T*) or  $\eta$  (*T*) experimental data via the VFT equation [issues (i)–(iv)] also extends for the PVFT/ (corrected PVFT) dependences applied for describing  $\tau$  (*P*) or  $\eta$  (*P*) SB behavior?

It is notable that the relation similar to Equation (8) was reported in 1963 by Roelands et al. (1963):  $\eta_0 \exp(\alpha_0 P/(1+R_3 P))$ , where  $R_3$  and  $\alpha_0$  are  $\eta(P)$ = constants, for describing viscosity changes in lubricating (1993) introduced the dependence oils. Kovarski  $\tau(P) = \tau_0 \exp \left[ \frac{PV^0}{RT} \left( 1 + \frac{P}{c} \right) \right]$ , where  $V^0$  and c are constants, to portray relaxation time changes in vitrifying polymers. There is also a set of other dependences proposed for portraying  $\tau$  (P) or  $\eta$  (P) behavior in the previteous domains, for instance, given by the Avramov-Milchev (Avramov, 2005), the free volume (Roland et al., 2005; Rzoska et al., 2010; Floudas et al., 2011) or the Adam-Gibbs (Roland et al., 2005; Floudas et al., 2011) models. However, they require more than three fitted parameters which inherently limits their application.

When testing the previtreous behavior in the extended range of pressures and temperatures the existence of two dynamical domains associated with the dynamical crossover occurring at  $(T_B, P_B)$  was discovered. It was first reported by Stickel et al. (1995), basing on the analysis of  $\tau$  (T) experimental data and later by Casalini et al. (2003) for  $\tau$  (P) and  $\eta$  (P) experimental data in the previtreous domain. They discovered such phenomenon applying  $\Phi_P$  (T) =  $\left[ d \log_{10} \tau (T)/d (1/T) \right]^{-1/2}$  vs. 1/T (Stickel et al., 1995) and  $\Phi_T$  (P) =  $\left[ d \log_{10} \tau (P)/d (P) \right]^{-1/2}$  vs. P (Casalini et al., 2003) plots, respectively.

These relations can be derived linking the *SA* Equation (1) with the VFT Equation (6) and the SB Equation (2) with the PVFT Equation (8), focusing on the "linear presentation" of results (see Equations 10a,b).

Notable, that such way of analysis analysis assume a priori the validity of VFT (Equation 6) and PVFT (Equation 8) relations, in both dynamical domains. At least for the temperature path the critical-like portrayal  $\tau$  (T)  $\propto$   $\left(T - T_C^{MCT}\right)^{-\varphi}$ , with  $\varphi$  = 1.5-3 and  $T_B \sim 1.2T_g$ , derived within the Mode-Coupling-Theory (MCT) is expected in the high temperature dynamical domain  $(T > T_B)$ , i.e., (Götze and Sjögren, 1995; Mallamace et al., 2010; Ngai, 2011). Studies focused on MCT-type behavior are usually based on  $\tau^{1/\varphi}$  vs. T plot, showing the empirical coincidence  $T_B \approx T_C^{MCT}$  (Mallamace et al., 2010; Ngai, 2011). and the occurrence in the high temperature dynamical domain for  $T > T_C^{MCT} + 10K$  (Mallamace et al., 2010; Rzoska et al., 2010; Ngai, 2011). Following refs. (Roland et al., 2005; Floudas et al., 2011; Ngai, 2011) one can coincide the high temperature dynamical (isobar, atmospheric pressure) with the low-pressure dynamical domain (isotherm): the preliminary evidence for the MCT-type behavior for the pressure path  $\tau$  (P)  $\propto$  ( $P_C^{MCT} - P$ )

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and  $P_C^{MCT} \sim P_B$  was reported in Patkowski et al. (2003). The dynamical crossover  $(T_B, P_B)$  is indicated as the onset of the secondary relaxation or the emergence of the translationalorientational decoupling (Roland et al., 2005; Roland, 2008, 2010; Floudas et al., 2011; Ngai, 2011) showed experimentally the timescale invariance of  $\tau$  ( $T_B$ ,  $P_B$ ) for the given glass former. Novikov and Sokolov (2003) basing on the Stickel et al. (1995) analysis for 28 different glass formers suggested the hypothetical "magic universality" of the dynamic crossover time scale  $\tau$  (T<sub>B</sub>) =  $10^{-7\pm1}s$ , later evidenced also under pressure (Casalini and Roland, 2004; Roland et al., 2005; Floudas et al., 2011). However, this concept has been questioned due to the evidence of notable discrepancies for a few glass formers (Ding and Sokolov, 2006; Ngai, 2011; Mallamace et al., 2014). One should stress that the critical-like behavior mentioned in issue (iii) above was associated with the low-temperature domain (close to  $T_{\sigma}$ ) and has no links to the MCT critical-like behavior associated with the high-temperature domain for  $T >> T_g$ . Notable, that the existence of two dynamical domains was also confirmed beyond BDS studies (Wu et al., 2009; Hoffman et al., 2017; Bartoš et al., 2018). Generally, the dynamical crossover phenomenon is associated with the crossover from the ergodic to the nonergodic (ultraviscous, ultraslow) domain on approaching the glass transition (Roland et al., 2005; Floudas et al., 2011; Ngai, 2011), Stickel et al. (1995), and Casalini et al. (2003).

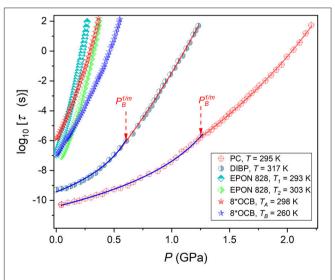
This report presents the evidence for the presumably universal long-range previtreous changes of the pressure related apparent fragility. This "anomaly" led to the "model-free" derivation of the critical-like relation for the pressure evolution of the primary/structural relaxation time. All these led to new conclusions for the dynamic crossover phenomenon. Finally, the extension of results for the electric conductivity and related properties is considered.

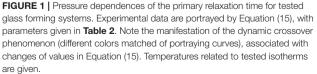
# **EXPERIMENTAL**

This report presents the results of high-pressure studies, up to  $P \sim 2.2$  GPa, of the structural relaxation time in glass forming liquid crystalline 8\*OCB (isooctyloxycyanobiphenyl) (Pawlus et al., 2010), epoxy resin EPON 828 (Rzoska and Drozd-Rzoska, 2011) and two low-molecular-weight liquids diisobutyl phthalate (DIBP) (Paluch et al., 1996) and propylene carbonate (PC) (Drozd-Rzoska et al., 2008a,b). For 8\*OCB and EPON 828 results are presented for two isotherms. In each case, studies were carried out between the atmospheric pressure (P = 0.1MPa) and  $P_g(T)$ , for time-scales ranging between  $\tau$   $(T_g, P_g) = 100s$  and  $\tau \sim 10^{-7}s$ . The latter is associated with existing limitations in high-pressure experimental studies to frequencies f < 10MHz.(Roland et al., 2005; Rzoska et al., 2010; Floudas et al., 2011). To overcome this problem for PC and DIBP,  $\tau$  (P) experimental data were matched with scaled electric conductivity  $\sigma$  (*P*) data. The scaling of  $\tau$  (*P*) and  $\tau_{\sigma}$  (*P*)  $\propto$  $1/\sigma$  (P) experimental data was possible because the low-pressure dynamical domain obeys the translational-orientational coupling  $\tau$  (*T*, *P*)  $\sigma$  (*T*, *P*) = const (Starzonek et al., 2015). Studies were carried out in the measurement capacitor with the macroscopic gap between the capacitor's plates d = 0.2 mm. For the applied measurement of voltage U = 1V, the electric field intensity E =5kV/m. So far, for studies in the challenging GPa domain, the microscopic gap was used. However, for instance for the  $20\mu m$  gap one obtains E = 5 MV/m, which is the value where nonlinear phenomena are essential (Rzoska and Drozd-Rzoska, 2011; Richert, 2018). The scheme of the applied capacitor is presented in ref. (Rzoska et al., 2018). One of the critical problems in high-pressure studies is the separation between the tested sample and the pressure transmitted medium (Plexol in the given case). For the results presented, the transmission of pressure to the tested sample took place via the deformation of the Teflon film (Rzoska et al., 2018). All samples before measurements were degassed prior to measurements. Studies were carried out using the impedance analyzer Novocontrol BDS model 2015. The primary relaxation time was determined from the peak relaxation time of dielectric loss curves  $\tau = 1/2\pi f_{peak}$ . The electric conductivity was estimated from the low-frequency part of the BDS spectrum using the relation  $\sigma = (2\pi f) \varepsilon''(f)$  (Kremer and Schönhals, 2003; Rzoska et al., 2010). The pressure chamber was surrounded by the special jacket enabling fluid flow from the thermostat with external liquid circulation, V = 25 L total volume and the temperature control  $\sim 0.02K$ . The pressure was exerted and controlled via the computer controlled pump.

# **RESULTS AND DISCUSSION**

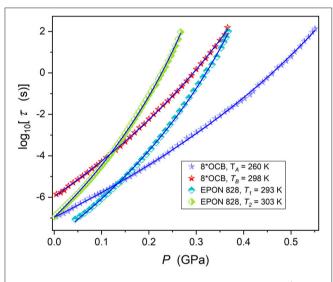
**Figures 1**, **2** show the pressure evolution of the structural relaxation time for tested glass forming systems in the previtreous domain. They are a liquid crystal (8\*OCB), epoxy resin (EPON 828) and two low molecular weight liquids: diisobutyl phthalate (DIBP) and propylene carbonate (PC). For 8\*OCB and EPON





828 results are given for two isotherms. **Figure 2** shows the supplementary, "focused," presentation of results from **Figure 1**. This is associated with qualitatively different available ranges of pressures in tested systems: each glass forming system could be studied between the atmospheric pressure and the glass transition pressure.

Values of glass pressures for each tested isotherm are given in **Table 1**. It is notable that high-resolution  $\tau$  (*P*) results for pressures well-above 1 GPa and with "bulk parameters" of the measurements capacitor are still hardly available (Roland et al., 2005; Rzoska et al., 2010; Floudas et al., 2011; Rzoska, 2017). The apparent fragility can be determined from  $\tau$  (*P*) experimental



**FIGURE 2** | Pressure dependences of the primary relaxation time in 8<sup>\*</sup>OCB and EPON 828, for two isotherms. Experimental data are portrayed by Equation (15), with parameters given in **Table 2**. Temperatures related to tested isotherms are given.

data using the relation (Roland et al., 2005; Floudas et al., 2011):

$$m_T(P) = \frac{d \log_{10} \tau(P)}{d \left(P/P_g\right)} \tag{11}$$

where  $0.1MPa < P < P_g$ , T = const: see also Equation (5).

The experimental pressure evolutions of the apparent fragility in tested glass formers, based on empirical data from **Figures 1**, **2** and Equation (11), are presented in **Figures 3**, **4**. The applied scale,  $[m_T(P)]^{-1}$  vs. *P*, reveals the simple and hypothetically universal form of the previtreous behavior in the high pressure (*HP*) domain, adjacent to  $P_g$ :

$$\frac{1}{m_T(P)} = a_{HP} + b_{HP}P \to m_T(P) = \frac{A_{HP}}{P^* - P}$$
(12)

where  $P_B^{1/m} < P < P_g$  and  $P^* > P_g$ ; the singular pressure is estimated via the condition  $1/m_T \left(P_g^*\right) = 0$ . A similar behavior occurs for the low pressures (*LP*) domain  $P < P_B$ :

$$\frac{1}{m_T(P)} = a_{LP} + b_{LP}P \to m_T(P) = \frac{A_{LP}}{P_B^* - P}$$
(13)

where  $P_B^{1/m} < P_B^* < P_g$  and the singular pressure is estimated as  $1/m_T (P_B^*) = 0$ .

The dynamical crossover pressure  $P_B^{1/m}$  is defined as the intersection of lines described by Equations (12, 13), for *HP* and *LP* domains, respectively. Linking Equations (11) and Equations (12, 13) one obtains:

$$d\log_{10}\tau(P) = \frac{d(P/P_g)}{aP+b}$$
(14)

Subsequently, the integration of Equation (14) yields the relation:

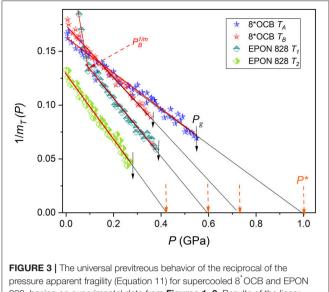
$$\tau(P) = \tau_{0P} \left( P^* - P \right)^{-\Psi} \tag{15}$$

for the ultraviscous *HP* domain  $P_B^{1/m} < P < P_g$ , with  $P^* = P_g + \Delta P_g^*$  and  $1/m_T (P^*) = 0$ .

**TABLE 1** Results of the linear regression fit for the reciprocal of apparent fragility  $m_T(P)$ : see Equations (12, 13).

|                         | Relation     | $\frac{1}{m_T(P)} = aP + b; aP + b \neq 0$ Values of fitted parameters |                  |                             |          |                                     |  |
|-------------------------|--------------|--|------------------|-----------------------------|----------|-------------------------------------|--|
|                         |              |  |                  |                             |          |                                     |  |
|                         |              | ∆Prange [GPa]  | а                | P* [GPa]remote<br>(#)/close | Pg [GPa] | P <sup>1/m</sup> <sub>B</sub> [GPa] |  |
| Glass forming materials | DIIB         | $\Delta P_{remote}$ 0.01÷0.66<br>$\Delta P_{close}$ 0.60÷1.25          | -0.415<br>-0.039 | <sup>(#)</sup> 0.73<br>2.56 | 1.23     | 0.54                                |  |
|                         | PC           | $\Delta P_{remote}$ 0.02÷1.26<br>$\Delta P_{close}$ 1.2÷2.21           | -0.24<br>-0.03   | <sup>(#)</sup> 1.56<br>3.56 | 2.22     | 1.06                                |  |
|                         | EPON 828 (1) | $\Delta P_{remote}$ 0.02÷0.1<br>$\Delta P_{close}$ 0.09÷0.39           | -1.25<br>-0.33   | <sup>(#)</sup> 0.92<br>0.59 | 0.28     | 0.09                                |  |
|                         | EPON 828 (2) | 0.01 ÷ 0.27  | -0.30            | 0.42                        | 0.39     |                                     |  |
|                         | 8*OCB (2)    | 0.01 ÷ 0.55  | -0.24            | 0.73                        | 0.55     |                                     |  |
|                         | 8*OCB (1)    | 0.01 ÷ 0.38  | -0.16            | 1.00                        | 0.365    |                                     |  |

 $\Delta P_{range} = |P_r - P_g|$ ,  $P_r$  denotes the terminal pressure;  $\Delta P_{close}$ - close to  $P_g$ , related to the (ultra)slow relaxation;  $\Delta P_{ramote}$ - remote from  $P_g$ , related to the "fast" dynamical domain.



pressure apparent tragility (Equation 11) for supercooled 8 OCB and EPON 828, basing on experimental data from **Figures 1**, **2**. Results of the linear regression fit (Equations 12, 13) in **Table 1** are collected. Solid arrows indicate the glass transition. The dashed (orange) arrows show singular pressures  $P_g^*, P_B^*$ . For the "high temperature" isotherm for EPON 828, the dynamic crossover pressure  $P_g'$  is also indicated.

For the *LP* dynamical domain, remote (*R*) from the glass pressure:

$$\tau (P) = \tau_{0P}^{R} (P_{B}^{*} - P)^{-\Psi^{R}}$$
(16)

for  $P < P_B^{1/m}$ ,  $P_B^* = P_B^{1/m} + \Delta P_B^*$  and  $1/m_T (P_B^*) = 0$ . Linking Equations (15, 16) and Equation (11) one can

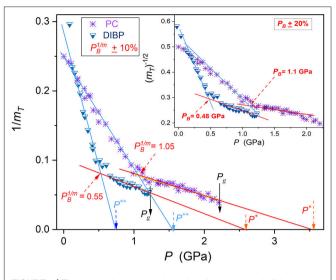
Linking Equations (15, 16) and Equation (11) one can obtain relations enabling the estimation of power exponent from  $1/m_T$  (*P*) vs. *P* plots, i.e., via the simple linear regression fit:

$$\Psi = ln10 \frac{\Delta P_g^*}{P_g} m_T \left( P_g \right) \tag{17}$$

$$\Psi^R = ln 10 \frac{\Delta P_B^*}{P_B^{1/m}} m_T \left( P_B^{1/m} \right)$$
(18)

Power exponents depends on the fragilities,  $m_{\rm T} (P_g)$ ,  $m_{\rm T} (P_B^{1/m})$ , and the relative values of discontinuities  $\Delta P_g^*/P_g$ ,  $\Delta P_B^*/P_B^m$ ), respectively. **Tables 1**, **2** present results of analysis of the apparent fragility via Equations (12, 13) and the relaxation time via Equations (15, 16). Graphically, the solid curves in **Figures 1**, **2** support the validity of the discussed description.

**Figure 4** presents the pressure evolution of the reciprocal of the apparent fragility  $1/m_T$  (*P*) and in the inset the dependence  $(m_T)^{-1/2}$  vs. *P*, for the same set of data. The latter is directly linked to the Casalini et al. (2003) plot developed for estimating the dynamic crossover pressure  $P_B$ , namely:  $[m_T(P)]^{-1/2} = (P_g)^{-1/2} [d \log_{10} \tau(P)/dP]^{-1/2} = (P_g)^{-1/2} \Phi_T(P)$ . As mentioned in the Introduction, the Casalini et al. (2003)  $\Phi_T(P)$  plot assumes *a priori* the validity of the



**FIGURE 4** | The universal previtreous behavior of the reciprocal of the pressure apparent fragility for super-pressed propylene carbonate and diisobutyl phthalate, based on experimental data from **Figure 1**. Results of the linear regression fit (Equations 15, 16) are collected in **Table 1**. The solid arrows indicated glass transition pressures, and the dashed (orange) arrows extrapolated singular pressures  $P_g^* = P_g + \Delta P_g^*$  and  $P_B^* = P_B^{1/m} + \Delta P_B^*$ . Dynamical crossover pressures  $P_B^{1/m}$  are indicated.

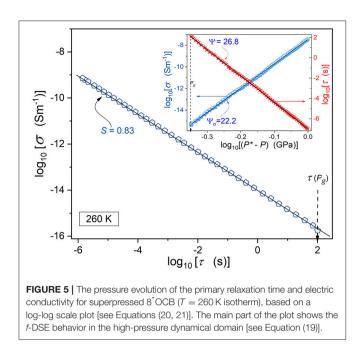
**TABLE 2** | Results of fitting of experimental data  $\tau$  ( $P \rightarrow P_g$ ), for the primary (structural) relaxation time via Equations (15, 16).

|                         | Relation     | $\ln\tau(\mathbf{P}) = \ln\tau_{\mathbf{0P}} - \Psi \times \ln\left(\mathbf{P}^* - \mathbf{P}\right)$ |   |                                       |                          |  |  |
|-------------------------|--------------|---|---|---------------------------------------|--------------------------|--|--|
|                         |              | Values of fitted parameters   |   |                                       |                          |  |  |
|                         |              | $\Delta P_{range} [GPa]$  | $\textit{In}\left(\tau_{\textit{OP}}\left[\boldsymbol{s}\right]\right)$ | Ψ                                     | <b>P*</b> [ <b>GP</b> a] |  |  |
| erials                  | DIIP         | $\Delta P_{remote}$ 0.01÷0.60<br>$\Delta P_{close}$ 0.56÷1.24   | -10.00<br>13.53   | 5.4 <sub>4</sub><br>55.2 <sub>0</sub> | 0.78<br>2.66             |  |  |
| Glass forming materials | PC           | $\Delta P_{remote}$ 0.05÷1.26<br>$\Delta P_{close}$ 1.21÷2.21   | -8.94<br>4.09   | 7.1 <sub>9</sub><br>29.3 <sub>8</sub> | 1.61<br>3.42             |  |  |
| ormi                    | EPON 828 (1) | 0.05 ÷ 0.38   | -13.30  | 23.7 <sub>0</sub>                     | 0.60                     |  |  |
| SS f                    | EPON 828 (2) | 0.04÷ 0.33  | -15.00  | 23.9 <sub>0</sub>                     | 0.46                     |  |  |
| Gla                     | 8*OCB (2)    | 0.01 ÷ 0.37   | -9.60   | 26.8 <sub>0</sub>                     | 0.73                     |  |  |
|                         | 8*OCB (1)    | 0.01 ÷ 0.55   | -6.80   | 26.5 <sub>0</sub>                     | 1.02                     |  |  |

 $\Delta P_{range} = |P_r - P_g|, P_r \text{ denotes the terminal pressure; } \Delta P_{close} \text{ - close to} P_g, \text{ related to the (ultra)slow relaxation; } \Delta P_{remote} \text{ - remote from} P_g, \text{ related to the "fast" dynamical domain.}$ 

PVFT Equation (8) in both dynamical domains. Estimations of the dynamic crossover pressure by both mentioned methods (indicated as  $P_B$  and  $P_B^{1/m}$ , respectively) differs by ca. 10%. The arbitrariness of the estimation is more significant for the Casalini et al. (2003) type analysis presented in the inset. The analysis based on  $[m_T(P)]^{-1}$  vs. *P* plots yielded: for EPON 828 ( $P_B^{1/m} = 0.138GPa$ , and  $\tau_B = 4 \times 10^{-6}$ ), for DIIB ( $P_B^{1/m} = 0.544GPa$  and  $\tau_B = 2.3 \times 10^{-7}$ ) and PC ( $P_B^{1/m} = 1.075GPa$  and  $\tau_B = 2.5 \times 10^{-7}$ ).

Results presented above are associated with the primary relaxation time evolution, but they can also be applied for other



dynamic properties: viscosity, diffusion or electric conductivity. The shift from the low pressure (or high temperature) to the high pressure (low temperature) dynamical domain changes the translational-orientational coupling (Ngai, 2011; Starzonek et al., 2015): (*translational—orientational coupling*)  $\rightarrow P_B \rightarrow (translational—orientational decoupling). For the electric conductivity such behavior is associated with the Debye-Stokes-Einstein ($ *DSE*) and the fractional*DSE*(*f-DSE*) dependences (Starzonek et al., 2015):

$$\sigma(P) \tau(P) = C_{LP} \to P_B \to \sigma(P) [\tau(P)]^S = C_{HP}$$
(19)

where parameters  $C_{LP} = const$ ,  $C_{HP} = const$  and *S* denotes the *f*-DSE exponent, describing the decoupling. Linking Equations (15, 16, 19) one obtains for the high-pressure dynamical domain:

$$\sigma(P) = \frac{C}{\left[\tau_{0P}(P^* - P)^{-\Psi}\right]^S} = \sigma_{0P} \left(P^* - P\right)^{S\Psi} = \sigma_{0P} \left(P^* - P\right)^{\Psi_{\sigma}} (20)$$

The inset in **Figure 5** confirms the validity of the critical-like portrayal [Equations (15, 20)], using linearized plots:

$$log_{10}\tau (P) = log_{10}\tau_0^P - \Psi log_{10} (P^* - P) \text{ and } log_{10}\sigma (P)$$
  
=  $log_{10}\sigma_0^P + \Psi_\sigma log_{10} (P^* - P)$  (21)

Values of exponents S,  $\Psi$ ,  $\Psi_{\sigma}$  are given in the plot. The inset shows the *f*-DSE behavior for the same set of experimental data and the direct estimation of the "decoupling" exponent *S*. It is in fair agreement with the estimation from the inset  $S = \Psi_{\sigma}/\Psi$ , resulted from Equation (20).

# CONCLUSIONS

This report presents the evidence that the pressure related apparent fragility can show the "universal" pretransitional anomaly, both on approaching the glass transition pressure and the dynamic crossover pressure. The resulted linear pressure dependence of its reciprocal enables a simple and "model-free" estimation of the dynamic crossover pressure, also introducing new parameters associated with  $P_g$  and  $P_B$ : extrapolated singular pressures  $P_g^*$  and  $P_B^*$  and coupled "discontinuities" of transitions  $\Delta P_g^* = P_g^* - P_g$  and  $\Delta P_B^* = P_B^* - P_B$ . The obtained "pretransitional" anomalies of the apparent fragility served as a reference for deriving critical-like equations for portraying the  $\tau$  (P) evolution (Equations 15, 16). All parameters for these relations can be determined from  $1/m_T$  (P) the plot and based on the exact definition of the prefactor  $\tau_{0P}$ : it is equal to the relaxation time at  $P^* - P = 1$  GPa. Notable that the description via Equations (15, 16) extends into the negative pressures region. The obtained relation for  $\tau$  (P) has the critical-like form, associated with the power exponents  $\Psi$  ( $P_B^{1/m} < P < P_g$ ) and  $\Psi^R$  for the "remote" dynamical domain ( $P < P_B^{1/m}$ ). Notable, that  $\Psi >>$  $\Psi^R$ , which according to Equations (17, 18) may results from the difference between fragilities  $m_T(P_g) >> m_T(P_B^{1/m})$  visible in Figures 3, 4. On the other hand there is w very weak impact of the shift from one isotherm to another on values of power exponents.

The question arises if the critical-like behavior in the lowpressure domain is coupled to the MCT-type behavior. In the opinion of the author, the answer is negative: Equation (16) obeys up to the dynamical crossover pressure  $P_B$  and the singular pressure is located at  $P_B^* = P_B + \Delta P_B^*$ . For the MCT-type behavior, one should expect the singularity at  $P_C \approx P_B$ , with the critical-like description terminating well-above  $P_B$  (Götze and Sjögren, 1995; Mallamace et al., 2010; Ngai, 2011). Results presented in this report indicate the equal importance of the glass transition and the dynamical crossover between the ergodic domains, introducing the novel way of estimating the dynamical crossover loci between both domains. It yields slightly shifted estimations (denoted as  $P_B^{1/m}$ ) in comparison with the  $P_B$  values from Casalini et al. (2003) plot  $\Phi_T(P)$  plot, which assumes a priori the validity of the PVFT Equation (8). Notable, that relations developed in this report, including (15, 16), cover both dynamical domains and can also be applied for other dynamical properties. They are directly applied for the pressure evolution of viscosity  $\eta$  (P). For the electric conductivity or diffusion the impact of translational-orientational decoupling should be taken into account.

# AUTHOR CONTRIBUTIONS

The author confirms being the sole contributor of this work and has approved it for publication.

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**Conflict of Interest Statement:** The author declares that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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