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The analysis of clay materials for use in a ceramic studio

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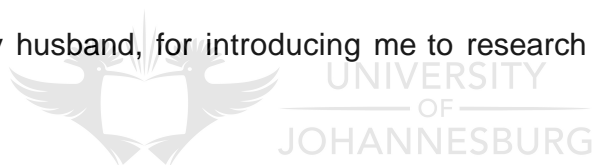
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ABSTRACT.

The research project entitled: *The Analysis of Clay Materials for use in a Ceramic Studio* was undertaken in order to give a quantitative base to the understanding of clay materials and their role in clay bodies. The project consists of analysing the clay materials as they are supplied, using technically sophisticated equipment. A set of data for each of the nine chosen clays was assembled and then correlated for easier comparison.

The clay materials were then mixed into clay bodies using a set proportion in order that a comparison of the nine clay bodies could be made and related to the data assembled for the clay materials.

The data collected, as well as the ceramic calculations used in the research project were entered into the "Insight" Ceramic software programme for use in the studio. This data base will be the foundation for ongoing research into ceramic materials.



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CHAPTER 1

INTRODUCTION AND RESEARCH OBJECTIVES

This research project was undertaken in the Ceramic Division of the Department of Three Dimensional Design TWR., in order to give a quantitative base to the understanding of clay used in the Department. This project analyses the clay materials as they are supplied, using sophisticated technology gives quantitative results that can be correlated with the known requirements of the clay bodies. The clay mining companies and distributors should be able to supply an updated analysis of the clay materials with every batch supplied but it is only in rare instances that this is in fact given. This lack of information is one of the prime reasons for undertaking this research project.

Ceramics is peculiar in the field of Art and Design in that it is essential to understand the technology of clay both in its unfired state and as a component of a ceramic body if there is to be control of the final product. This is of particular importance in a Technikon where technology and its transfer are vital to the structure of the Programme. All the distinguishing features of good design and formal aesthetics are taught as well as a variety of production techniques and surface treatments, but, if the quality of the finished ware is not technically sound the product is seriously diminished in worth.

The quest for quality is of paramount importance in South Africa at this time as the current employment route is leading towards small businesses producing limited numbers of up-market, designed objects for both the local buyer and export. Ceramics is ideally suited to small batch production but only if the number of rejects can be kept to a minimum by stringent material controls. The information collected in this project should be regularly updated and be made available to production potters who have ventured into the self-employment territory. The information will be stored in the form of a Data Base (2.6) designed for the easy access to the composition of the materials as well as to the calculations required for the formulation of the materials into clay bodies by all interested parties.

The clay bodies used to date have generally been supplied in pre-mixed form from one of the large ceramic supply companies. These materials have served a purpose in giving freedom to the students and staff of the Ceramic Division to

develop form, style and concept without too large an output of energy in the area of material research. However these clay bodies have proved to be the cause of problems that need to be addressed. It therefore becomes imperative that a clay body that is controlled and regularly tested should be formulated and mixed for use in the Ceramic Division. In this way the properties could be prioritised and adjusted to specific requirements. The information gathered in the course of this research project will be used for the formulation of the clay body.

Pottery making is one of the oldest techniques known to man. Sherds have been found from ancient civilisations in Asia dating back to 6500BC. It is the extraordinary properties of plasticity and sintering, making it possible to form the clay and then to render it permanent by firing, that has attracted man to this material. Clay vessels made for domestic uses such as carrying water, the storage of supplies and cooking pots have been produced by agrarian communities for centuries. Ritual vessels, for both secular and devout ceremonies were frequently made from clay, carefully and meaningfully crafted then decorated, endowing them with a spirit of creativity. The clay used for these vessels was selected for colour and workability and dug from riverbeds and prepared according to the traditions of the region. These preparations were tested empirically by the potters and the knowledge passed down through generations of crafts people. Even today traditional potters usually make use of materials within a limited radius of their workplace although they may combine materials in order to alter the properties of the body.

The concept of combining clays from different regions in order to fabricate a predetermined clay body was common practice in China as early as the Sung Dynasty (AD 960-1279). The potters of Jingdezhen combined the local ball clay with a particular clay from 'Gaolin', meaning High Mountain, to the North-East. A further important additive was 'petuntse', the colloquial name for a prepared crushed pegmatite. The three materials combined, produced a White, translucent porcelain that was the envy of the civilized world. Enormous quantities of porcelain wares were made for export to Europe, Asia and Africa. The Portuguese were the first to trade in these wares, later the Dutch East India Company brought shiploads of porcelain to Europe where they were coveted by the gentry and envied by the potters. This competition led to considerable research into white clay bodies in Europe and throughout the Western world. It was not until 1710 that true porcelain was made at Meissen. White tin glazed

majolica wares were produced in imitation of the Chinese porcelain until this discovery.

In the Eighteenth Century the Industrial Revolution and the resultant new middle class desired tableware of a high standard but, the imported wares were expensive. This newly opened market made the importation and blending of clays a viable proposition. Josiah Wedgwood for example built a canal to enable the transport of white clay from Devon to his factory, Etruria, in Stoke on Trent. His development and production of Creamware successfully competed with the imported porcelain. Today the importation and blending of clay in England and Europe is a highly sophisticated and scientifically controlled process guaranteeing a supply of clay to the manufacturer with a constant composition.

Post modernism's re-introduction of the use of brighter colours and decorative surfaces, after the constraints of minimalism and functionalism dictated by the Modernist movement in the 1950's and 1960's, required the development of white, low firing bodies. These bodies have to be fine-grained and low in iron to show off the coloured surface, and capable of maturing below 1200°C, as many of the available ceramic colours burn out at this temperature. The clays found in South Africa tend to be iron bearing, so, in order to produce a white body the clay materials must be blended in calculated proportions. It is essential to know accurately the composition of the various materials in order to perform this task. The materials required are readily available but are not always consistent in composition or tested regularly. These variations can cause faults such as dunting of the body or crazing in the glaze. This research project provides accurate means of examining clay materials in order to prevent such problems from occurring. It should be noted that this information and the means of formulating a clay body can be used to develop any required ceramic body, fired in any temperature range.

The Ceramic Design programme presented at the TWR is essentially art-and-design based, teaching visually literate students the techniques and technology necessary to make quality ceramic wares. It was therefore felt that the data generated by this project should be visually meaningful as well as quantitatively accurate in order for the data to be of use in the production studio. It was for this reason that the Scanning Electron Microscope with EDAX analyser was chosen as the prime analytical tool to study the clay materials. Photographs of the morphology and graphs of the properties of the clays would make the differences

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in these materials visually apparent when studied in conjunction with the analytical data. The stereo-microscope with a camera attachment was used in order to reproduce the colour of the clay which is often of significant importance:

As a final comparative method of characterising the nine clay materials chosen for the investigation, the materials were mixed as "clay bodies" with a set proportion of feldspar and silica to give a standard. These bodies were then tested by throwing with them on the wheel in order to compare their plasticity as well as other physical properties. This comparison of the materials as components of "clay bodies" was related to the characterisation of the individual clay materials.

1.2 CLAY MATERIALS

Info
Clay can be defined as a fine grained earthy mineral, made up of hydrous aluminium silicates, plus residual fragments of other minerals and colloidal matter^[2]. Clay displays plasticity when wet, green strength when dry and is converted to a rock-like mass when fired to a high temperature.

kaolins
Kaolinite is the most common member of the clay group^[2] and is the major component of the white primary or residual clays remaining on the site of their formation, known as kaolin or china-clay. Kaolinite is formed as the result of the weathering and decomposition of acid igneous rocks such as granite. Large amounts of the resultant, finely ground weathered material are transported, usually by water, over long distances and deposited in river beds and lakes, resulting in sedimentary ball clays that are plastic due to the finely ground particles, but usually soiled due to the pick-up of other fine particles such as iron, titanium and manganese and chemically altered due to the ion exchange that occurs en route.

The structure of the clay mineral is dependent on the mineralogy of the parent rock and the sequence in which the weathering occurs. If the weathering is such that the potash and magnesia are rapidly removed, kaolinite is formed. If the potash and magnesia remain in the weathering zone, smectite and illite are formed. Likewise kaolinite is formed from basic igneous rocks if the magnesia is

removed as soon as it is released, or smectite is formed[2]. Further weathering of the sediments follows the same pattern as for the acid igneous rocks[2].

Kaolin
Clay minerals have been classified into eight groups according to their crystal layer type, the layer charge and the type of interlayer unit. [2][3][4][5] To the ceramist making wares from clay, the three important minerals are Kaolinite, a species of the Kaolinite group, Montmorillonite of the Smectite group and Illite of the Mica group.

The clay minerals are hydrous layer-silicates, part of the larger family of phyllosilicates. "The structure of kaolinite (the most ordered of the clay minerals) is made up of two layers. One layer consists of silicon and oxygen ions in which each silicon ion is at the centre of a tetrahedron formed by four oxygen ions. The other layer consists of aluminium and hydroxyl ions, the hydroxyls forming the corners of an octahedron. When the two layers are combined a layer of kaolinite is formed." [3] These minute hexagonal plate-like crystals compress into concertina-like stacks. This form of crystal structure is known as a 1:1 layer.

Montmorillonite is composed of the same basic constituents as kaolinite but the ratio of silica : alumina is doubled. The layer of aluminium and hydroxyl ions is sandwiched between two silicon and oxygen layers known as a 2:1 layer. Illite is also of this 2:1 layer formation.

Most physical properties of clay minerals can be related either to the very small size and plate-like form of the individual particles or to the significant surface charge associated with these particles. [5]

There is a certain amount of ionic substitution in the clay minerals, particularly in the dis-ordered, form of Montmorillonite. As the substitution involves the replacement of cations by another ion of lower valency, the clay structure becomes negatively charged. Positive ions, e.g. K^+ , Na^+ , Mg^{2+} , Ca^{2+} and H^+ are absorbed on the edges of the clay mineral, or in the layers, these ions are loosely held in the structure and can in turn be exchanged [3].

Clay mineral crystals lie within the colloidal range and therefore have colloidal properties and do not obey the ordinary sedimentation laws. Instead the particles are capable of remaining suspended in water and have, the ability to absorb cations and anions and retain them in an exchangeable state. [2] Water

molecules become attached to the positive and negative crystal sites that are exposed when the **crystal** is fractured. This pore-water between the flakes is one of the contributing factors affecting the plasticity of **clay**.^[6] The alkalis **found** in the clay materials are bonded to the kaolin platelets by the surface charge of the **crystals**. They can readily be replaced by one another thus affecting the stacking of the platelets and causing either flocculation or deflocculation depending on the charge.

The particle size distribution of a material cannot be conveyed by a single fineness figure, especially in the colloidal range of particles. Only those particles less than **2 μ m** e.s.d. (equivalent size diameter) are considered to be **clay**. This is a geological convention but can give comparative information to ceramists. The varied shapes of clay particles, from platelets to tubes, makes the measurement of size particularly difficult. More than one method is usually needed and the problem of compatibility of the results must be considered^[2]. The use of the laser diffraction method of particle sizing used in this project can be used as a comparative value. A mix of particle sizes in a clay body gives the best plasticity as the packing density improves. This also improves the green strength of the wares made from the clay.^{[2][3][4][5]}

The effect of heat on clay minerals resulting in sintering and ultimately vitrification is indirectly the result of this finely divided state of the particles. When the minimum temperature is reached to initiate solid state intercrystallisation without actually reaching the melting point of the individual body components a lattice arrangement is formed^[4]. "During firing the kaolin takes part in a series of reactions which lead to the formation of a glass-rich phase that forms the vitreous bond in the ceramic body."^[2]

The combined effect of these properties result in a unique and irreplaceable material that will continue to be utilised by mankind for the production of objects for ritualistic, domestic and structural uses.

1.3 FUNCTION OF THE CONSTITUENT OXIDES IN CLAY MATERIAL

The constituent oxides in a clay material individually affect the final ceramic structure. The commonly occurring materials are discussed in this section.

Note: The formula for the *Ideal clay Substance* is $Al_2O_3 \cdot 2SiO_2 \cdot 2H_2O$ [4][2], therefore, the theoretical weight % expressed in oxides is:-

SiO₂: 46.51 %.

Al₂O₃: 39.53%

H₂O: 13.95%

This theoretical composition can be used to give an indication of the amount and type of impurities in the clay material. Kaolinite of this composition does not occur naturally.[2]

The structural formula of kaolinite can be written



a) Silica(SiO₂)

Silica (SiO₂) is the most abundant oxide found on the earth's crust. It forms silicates with other oxides. Most ceramic raw materials are silicates e.g. clay, feldspar, talc.

Silica occurs in clay in the free state as quartz or combined in the structure of minerals. The effect of free silica in a clay is to reduce the plasticity, drying shrinkage and dry strength. Upon heating, free silica forms cristobolite and tridymite, two phases that contribute to the control of reversible thermal expansion and contraction of the fabricated clay body which is related to the glaze fit. Quartz is converted to cristobolite at 1470°C but with the addition of a flux, in particular lime, the reaction can occur sooner. Cristobolite is also derived from the break up of the kaolinite lattice. The silica content in a fabricated body can be between 70% and 75%[2].

b) Alumina (Al₂O₃)

Alumina occurs as combined alumino-silicates. High alumino content is associated with a high kaolinite content.[2]

c) Iron Oxide (Fe_2O_3) and Titania (TiO_2)

These two oxides determine the colour of the clay. The combination of the two oxides should be less than **2%** for the body to fire white.[2]

Titania is a white mineral but it enhances the staining power of Iron oxide.

Iron oxide can react with silicates and alumino-silicates to form "compounds that flux in the 11 000e range.

d) Lime (CaO) and Magnesia (MgO)(Alkali Earth Oxide)

These two oxides act as fluxes in low-fired clay bodies, forming eutectics and reducing the vitrification temperature. The alkali earths (Lime in particular) react with the silica in the clay body forming glass in a similar way to the feldspars but with a softening and melting range shorter than the feldspars. They are usually added in small amounts as the proportion of flux is higher than in Feldspars[3].

The presence of the alkali earths in a clay material can affect the plasticity. The small, multicharged ions can assist in the build-up of the water structure on the edge of a kaolinite crystal[6].

Lime may act as a weak bleaching agent on iron.

Alkali earths can be used in the development of shock proof bodies and also in bodies requiring low shrinkage.

e) Alkali oxides (K_2O and Na_2O)

These oxides occur in the minerals feldspar and mica. They are powerful fluxes and combine with the silica and alumina during firing to form glasses of complex composition. The presence of potash and soda has a marked influence on the reversible thermal expansion and contraction of the fired body. Alkalies reduce the refractiveness and vitrification temperature of the clay.

Note on Loss on Ignition (LOI)

This is associated with the loss of **hydroxyl** ions in the clay structure (water of crystallization) as well as the loss of any organic matter that is present in the clay material.

1.4 PROJECT PLAN

The **project** consists of the following three stages:

1.4.1. *Visual Information*

To examine the morphology and structure of the surfaces of the clays used in the studio on a microscopic scale and to present them photographically.

To record the variations in colour from one clay to another

1.4.2 *Clay analysis*

To examine the clays used in the studio and record their physical properties and composition for inclusion in a Data Base.

The interrogative techniques used to develop the Data Base are:

1.4.2.1 Physical measurements.

1.4.2.2 Chemical analyses.

1.4.3 *Clay body*

To fabricate "clay bodies" from the chosen clay materials in order to assess the physical properties of the clay materials in this form.

CHAPTER 2

MATERIALS AND EXPERIMENTAL TECHNIQUES.

The rationale on the choice of materials and their preparation for analysis as well as the techniques used for the analyses are presented in this chapter. Some of the analytical techniques rely on results obtained from previous measurements in which case an explanation of the sequence of analysis is given. It should be noted that the term *clay material* is used for the "as supplied" clay, whereas the term *clay body* implies that the materials have been mixed into a clay body in combination with other materials.

2.1 CHOICE OF CLAYS

The clays in regular use in the Ceramic Division of the Technikon Witwatersrand were chosen to be tested in this project. These clays are commercially available and used for clay application by the students and staff. Occasionally a different clay will be introduced into the laboratory for research-based reasons such as a project on porcelain or white earthenware. Usually the choice is based on the required physical properties of the clay. Up to now the recommendation of the clay supplier has been the main criterion for the selection.

In the time span of this research project, two of the chosen clays, Western Province 8all Clay and 813, have been re-ordered. Samples from both the old and the new bags of clays have been analysed to show the variation in properties over a period of time.

CLAYS EXAMINED

Sail clays

A Clay (Fire clay)
813
C.Clay
Moss clay
PXX High cast (imported)
Western Province Ball Clay

Kaolins

G1 Kaolin
Serena Kaolin
S Kaolin

2.2 SAMPLE LABELING AND FIRING TEMPERATURES

The samples prepared for microscopic study, chemical analysis and the physical tests were labeled as shown in Table 2.1 according to the temperatures at which they were fired. These temperatures were chosen to closely match those used in the studio. As is usual in a working studio the glazes and clay bodies are formulated to mature at a specific temperature to simplify the firing schedule and to make sure that the kilns are fired full of wares as the cost per item must be accounted for.

Sample label	Firing Temp.	Orton cone number.	Firing Type
A	Unfired		
8	1000 ⁰ C	06 (999 ⁰ C)	Bisque temp.
C	1100 ⁰ C	03 (1101 ⁰ C)	Glaze temp.
0	1200 ⁰ C	4-5 (1 186 ⁰ C-1 196 ⁰ C)	Glaze Temp.

This system of firing and sample labeling has been used throughout the project. The A, or unfired sample was dried to 1100C in order to rid it of pore water. In the samples for the SEM this is necessary for the carbon coating to adhere to the surface and in the samples for the shrinkage and absorption tests it ensured that the Wet to Dry shrinkage was complete. The sample was not fired.

2.2.1 Samples for the microscopic studies and chemical analyses.

The microscopic studies were carried out by scanning electron microscopy (SEM) and the chemical analyses by energy dispersive X-ray analysis (EOAX). The samples examined on the SEM/EOAX were the A and 0 samples. To examine all four of the samples for each of the clay materials proved to be too time consuming and expensive. The results from the A and 0 samples were close, or even the same therefore it was assumed that the other two samples (8 & C) would also give very similar results.

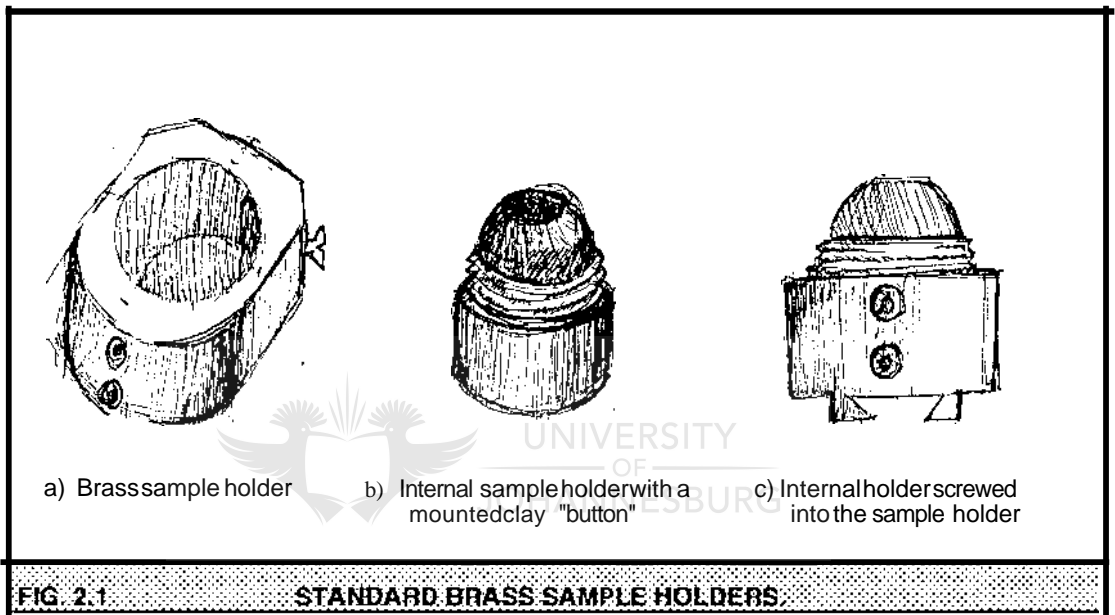
2.2.2 Samples for the physical tests

Samples fired to the four temperatures given in Table 2.1 were used for the physical tests. Where needed for the shrinkage and absorption tests, an additional sample was made and fired to 600⁰C. This is the temperature at which ceramic change becomes irreversible. The clay material is converted to a ceramic. The hydroxyl groups (OH) are removed from the clay lattice and the absorbed water is removed from the fractured ends of the clay lattice-[7] (Section 1.2) This additional sample gave insight into the sintering properties of the clay materials.

2.3 METHOD OF SAMPLE PREPARATION

2.3.1 Samples for the Scanning Electron Microscope (SEM)

The requirements for samples for the SEM were examined. It is essential that the sample fit into standard brass holders (Fig.2.1) and that the top surface of the sample be flush with the top of the holder so that the electron beam strikes the surface at 90° and the sample position is known. The internal holder (Fig. 2.1) should be firmly tightened with the grub screw.



2.3.1.1 First set of samples

a) The very first samples made were broken from a larger test piece. These irregularly shaped shards proved difficult to mount correctly. An attempt to mount a small clay fragment in a bakelite plug made conductive by the inclusion of iron, proved unsuccessful as the sample continued to "charge" when in the microscope, due to the accumulation of secondary electrons on the surface of the sample.

2.3.1.2 Second set of samples

a) A Plaster of Paris mold was made in the shape of an egg box to form the samples into the correct shape to fit into the brass sample holder. The clays were wet mixed and then dried in this mold before firing. Four samples of each clay were made. The rounded side of the clay "buttons" was ground flat on a marble slab to obtain a suitable surface for analysis. If the surface is left rough the electron beam is scattered in

scattered in many directions, and information is lost. Besides this the depth of penetration of the beam would not be the same at different orientations of the surface with respect to the beam, so secondary electrons and X-rays from different depths would be received, which would make it impossible to compare data from different samples.

b) The samples were carbon coated with the assistance of the Electron Microscope Unit of the University of the Witwatersrand. This coating makes the sample conductive thereby preventing the surface of the clay from "charging up" whilst being examined in the SEM.

c) The build up of charge on the surface of the samples proved to be considerable, especially on the A (unfired) samples, in spite of the carbon coating. It is essential to cover the samples with sufficient DAG, a suspension of graphite powder in acetone, in order to lead the charge to earth, leaving uncovered, (but coated with carbon) the area to be analysed.

2.3.2 Samples for the physical tests

There is a large number of books and publications giving techniques of clay evaluation and testing.[2][4][7J[a] The purpose of this research is to identify the techniques necessary for the evaluation and testing of clays in a studio situation.

The Physical Tests carried out were the following: (4)

- a) Shrinkage
- b) Water Absorption
- c) Loss on Ignition (LOI)
- d) Plasticity
- e) Particle size
- f) Colour comparison

The samples for the physical tests were prepared from the same clays as those prepared for examination in the SEM.

2.3.2.1 Method of sample preparation

art kilogram of clay was mixed with water to form a workable, plastic clay.

b) The clay was wedged thoroughly and formed into suitable test pieces for the tests described in 2.4.2.1.

c) Samples of the clay in powder form were prepared for particle size tests to be conducted at the Dept. Chemical Engineering University of Witwatersrand. (courtesy of Prof. Moys)

2.3.3. Samples for the "Clay Body II tests

Clay materials are seldom used in their found state but are mixed with other materials to form clay bodies with the required properties for their particular use. In order to obtain a normalised assessment of the clay materials they were mixed into "clay bodies" and tested (Table 3.32) (Chapter 4).

a) The nine clay materials listed in 2.1 were combined with Feldspar and Silica in the following proportions and formed into "clay bodies".

Clay material	50
Silica	30
Feldspar	<u>20</u>
	100

b) The clay was wedged thoroughly and formed into suitable test pieces for the tests described in 2.4.2.1 .

c) Samples of feldspar and silica were analysed in the SEM/EDAX (Appendix E) in order to include their composition into the Materials Definition Table included in the "Insight" Ceramic Chemistry software programme (2.6.2).

2.4 EXPERIMENTAL TECHNIQUES

2.4.1 Scanning Electron Microscope (SEM) and Energy Dispersive X-ray Analysis (EDAX)

2.4.1.1 Basic Principles of the SEM/EDAX [9]

The SEM/EDAX was selected as the instrument of analysis as the imaging of the surface and the chemical analysis of the individual clay materials can be performed simultaneously. This complied with the project aiming at visual and analytical characterization of the clays.

The SEM produces an image from the sample being examined as a result of the impingement of a finely focused electron beam onto its surface. The instrument basically consists of three groups of components: the electron optical column, the vacuum system including the specimen chamber and stage and the EDAX signal detection and display systems. The electron gun is usually a heated hairpin, tungsten filament. The electrons from the stream emitted from the gun are focused as they travel down the electron column by electromagnetic lenses which focus the beam to a diameter less than 100 Angstrom when it strikes the sample surface. The beam is scanned by electromagnetic scanning coils in synchronisation with the cathode-ray display tubes. When the beam impinges on the sample, secondary and backscattered electrons, X-radiation, and cathodoluminescence are emitted[9]. For this research project the secondary electrons were used to image the surface (with occasional use of backscattered electrons) and the X-radiation was used to analyse the chemical composition of the samples.

The secondary electrons that are emitted from the surface of the sample when it is impacted by a primary electron beam travel in all directions. However, since secondary electrons have relatively low energies, about 20 electron volts, essentially all of the secondary electrons, regardless of the direction in which they are emitted, are easily attracted to a collector mesh that has a positive potential of about 200 volts. This means that all spots on the sample surface will be included in the final image. However, it also means that secondary electrons produced by either primary or backscattering (Le. reflected) electrons striking other parts of the microscope, for example the objective lens, will also contribute to the final image. It has been estimated that about 30% of the final image is derived from extraneous interactions of this type. This phenomenon unfortunately creates noise in the image. Since all the secondary electrons entering the collector at any instant come from the small spot on the sample where the primary beam is striking, there is no need to focus the emitted

secondary electrons. Behind the collector is an aluminium coated light pipe which is excited with a potential of about 12.5 kV. This pipe is a solid rod made of specially doped plastic. Electrons that strike the end of the light pipe penetrate the thin aluminium coating and excite electron-hole pairs in the light pipe. These combine to produce photons which travel through the light pipe to a photomultiplier which produces a current. Any electrons that happen to travel away from the photomultiplier will be reflected by the aluminium coating and their motion reversed towards the photo multiplier. The current produced by the photomultiplier is amplified and used to modulate the intensity on a cathode ray tube which creates the final image.

The resolution and the depth of field of an SEM are the features that permit both the peaks and valleys normally encountered on a rough surface to be imaged in focus even at relatively high magnification. (Although the surfaces of the samples were ground flat, at the high magnifications used they appeared as rough surfaces). The contrast observed on the secondary electron image on the cathode ray tube is dependent primarily on the topography of the surface. A small variation in the angle between the primary electron beam and the surface of the sample where it strikes causes considerable variation in the brightness of the final image. Sharp edges or corners appear brighter than adjoining regions of the sample because their geometry causes greater quantities of secondary electrons to be emitted from them [9].

The energy dispersive X-ray analyser (EDAX) analyses the X-rays that are emitted from the spot where the electron beam strikes the sample. These X-rays have wavelengths characteristic of the elements contained in this precise area in an intensity proportional to their quantity which is measured by the spectrometer. A quantitative chemical analysis is possible by comparing the wavelengths and the intensity with known standards. The mineral standards for this project were loaned by Mintek and installed into the analytical programme linked to the EDAX (Appendix D) The use of the SEM/EDAX proved to be an efficient, accessible technique for obtaining the composition of clay materials for use in the Ceramic Division, TWA.

2.4.1.2 Procedure for Analysis of Clays

The procedure for the analysis of the clay samples was developed with the assistance of the Electron Microscope Unit at the University of Witwatersrand(10).

a) The samples were prepared as described in paragraph 2.3.1.

b) The samples were analysed using a Co standard that calibrates the energy scale. A sample of pure Co is permanently mounted at the side of the standard brass holder where it can be accessed and analysed

between each of the sample analyses. The zero strobe is set on, or as close as possible to, zero. The Cobalt K line should fall on 6.9242 keV. Any displacement was calibrated and corrected.

c) Mineral standards selected to closely correlate with the minerals commonly found in clay were used with the permission of MINTEK. The virtual or theoretical standards and the mineral standards available could not be calibrated adequately to give accuracy for elements such as sodium and magnesium which appear low on the atomic scale. A list of the standards used appear in (Appendix D).

d) The microscope was focused on the Co standard at 39mm working distance (WD) and x2000 magnification. The count rate was set on 1900 cps varying the Probe Current for adjustment. The Gun Alignment Tilt was checked at regular intervals to minimise drift. The Co standard was analysed between each two sample analyses in order to ensure the correct calibration. This process was repeated for each sample. The spectrum, a stoichiometric analysis giving the oxide percentage of the elements and an apparent concentration analysis giving the concentration of the various elements in the clay material were recorded for each sample.

e) The data were collected with ZAF correction [10] (Appendix D)

i.e. correcting for:-

Z = Atomic number

A = Absorption

F = Fluorescence

2.4.1.3 Correlation of clay data.

The clay data acquired from the SEMIEDAX were collected in these forms:-

a) computer generated analysis sheets giving the concentration of the elements in atomic percent. (Appendix D)

b) computer generated analysis sheets giving the stoichiometrically normalised analysis i.e. the oxide concentration in weight percent or molar percent (Appendix D).

c) Spectra of the above analyses.

d) Photographs of the samples at selected magnifications.

The calculations required for the analysis and comparison of clay materials are discussed in section 2.5 under clay evaluation & calculations. The visual information obtained is reported in Chapter 3 together with the physical data of the materials. The data collected in the course of this project has been stored in the form of a data base accessible to the Ceramic Division (Section 2.6)

2.4.2 Physical Tests

2.4.2.1 Linear Shrinkage. Water Absorption. Loss on Ignition. Colour and Particle Size(4)(11)

a) Linear Shrinkage

The clay material was prepared as discussed in 2.3.3.1, rolled into flat slabs and cut into rectangular samples. A 10cm line was inscribed onto each sample before firing to the required temperatures (Table 2.1). The shrinkage was measured from the shortening of the inscribed line for each of these temperatures. The wet-to-fired shrinkage is shown in the charts for each of the nine clay materials.(Chapter 3) and in (Chapter4) wet-to-fired linear shrinkage is given by:-

$$[(\text{wet length} - \text{fired length}) / \text{wet length}] \times 100\%$$

b) Water Absorption.

The samples were prepared as discussed in 2.3.3.1 and fired to the required temperatures. (Table 2.1)

The fired samples were weighed (D), placed in a saucepan and boiled for five hours, wiped dry and weighed again (S). The % water absorption is calculated by the formula

$$[(\text{Soaked wt} - \text{Dry wt}) / \text{Dry wt.}] \times 100 = \% \text{ Water Absorption}$$

The information gained from this test gives insight into the fluxing rate of the clay material. Graphs of the results of test a) and b) are included in the information on individual clays (Chapter 3) and in (Chapter 4).

c) Loss on Ignition:

100 grams of each clay was formed into a flattened disc which was allowed to dry for 24 hours, weighed (this weight will be indicated as (a) and the weights measured subsequently will be indicated as (b) and (e)) and then heated to 1100C in order to drive off the pore water. The sample was then weighed again. (b)

The sample was fired to 1000⁰C and re-weighed.(c) The difference between (b) and (e) is the *Loss on Ignition. (LOI)*

100 - (a) = Weight of water of plasticity in a 100 gm sample.

(a) - (b) = Weight of pore water in a 100 gm sample

$LO = (b) - (c)$

The result of the LOI test is included in the ultimate analysis calculation (2.5.1.1).

d) Colour. ,

The flat samples used in (c) were each photographed by means of the stereo-microscope at the Schonland Research Centre, University of the Witwatersrand. (Chapter 3)

e) Particle Size Test.

The "Malvern mastersizer" laser diffraction instrument was chosen as the method of analysis as it is capable of measuring colloidal particles accurately.

The Laser Diffraction particle size analyser in the Dept. of Civil Engineering, University of the Witwatersrand was used for these test, by courtesy of Prof. Moys.

The basic principles of operation are as follows:-

the clay material is dispersed in water by stirring and ultrasound. The clay particles are then passed through a laser beam. When the light beam is interrupted by particles which are of varying diameters, a series of diffraction light ring patterns are formed. Each light ring is spaced radially at a distance which is uniquely related to a particular particle size. If a photosensitive detector is then placed in the path of the diffraction patterns, and the detector output scanned, digitised and programmed in a micro-computer, then the size distribution of the particles can be determined.[4][12]

The percentage of particles less than 2 μm is given in the analyses of the individual clay materials (Chapter 3) and further analyses in (Chapter 4) The complete particle size analyses can be found in Appendix C

2.4.2.2 Plasticity Tests(2)(4)

Clay materials are not often used in their found state but are combined into a clay body for manufacture. This test was therefore performed on the standard "clay bodies" that were mixed from the chosen clay materials in order to obtain a realistic result..

Plasticity has been defined as "That property which enables a material to be changed in shape without rupturing by the application of an external force and to retain that shape when the force is removed or reduced below a certain value."(4)

The factors affecting plasticity are:-

- a) water content
- b) size, shape and composition of the particles
- c) electrolyte content
- d) history and preparation methods of the clay.

The "clay body" was prepared as described above (2.3.3).

The throwing test was divided into two sections.

- i) A 500gm ball of clay was thrown into a cylinder 8cm in diameter. The height was measured.
- ii) A 500gm ball of the clay was thrown in any form that the potter found suitable for the particular "clay body".

The results were recorded on an increasing scale rated from 1-5 (Table 3.32) and in (Chapter 4).

2.5 CLAY EVALUATION & CALCULATIONS

2.5.1 Clay analysis

The proportion of elements present in the clay material samples were determined by EDAX (204.1) making use of a Cobalt standard. The composition was obtained as % element, atomic % and oxide% and the formula of the material. An example of the computer analysis is shown in (Table 2.2.) The oxide % is calculated stoichiometrically from the % elements and the atom %. It is convention to report the composition of silicates (oxides) in terms of the total oxides however this is a theoretical calculation assuming that all the elements are oxides and that the percentage weight added to the % elements is oxygen alone. The elemental analysis is more correct as the oxide (stoichiometric) basis could be interpreted as conveying the concept that the material is a physical mix of oxides. In fact the oxide minerals consist of a regular packing of oxygen atoms of the O-sublattice with the interstices filled with metallic or amphoteric elements in stoichiometric proportions [15].

2.5.1.1 Ultimate analysis

The chemical analysis given in terms of percentage composition. of oxides[4]

The Ultimate Analysis was carried out as follows:-

two areas from each sample were analysed and the average of the two sets of results was taken as the composition of the sample. For the purpose of this project the atomic % analysis (Table 2.2 Co1A) was entered into the data base ultimate analysis calculation table (Table 2.3). A description of the method of calculation appears below Table 2.3.

Alternatively the average of the two stoichiometric results (Table 2.2 Co1.6) could be used to obtain the ultimate analysis.

TABLE 2.2 EXAMPLE OF THE ANALYSIS PRINT-OUT FROM THE LINK PROGRAMME OF THE EDAX

WPBC(2) 0 (1 200 ⁰ C)						
1	2	3	4	5	6	7
Spectrum:						
Last elmt by STOICH..NORMALISED						
ELMT	ZAF	%ELMT	ATOM.%		%OXIDE	FORMULA
NaK : 2	1.000	.178	.160	Na2O1	.240	.005
MgK : 2	1.014	.368	.315	Mg1O1	.610	.010
AlK : 2	.939	18.774	14.382	Al2O3	35.474	.454
SiK : 2	.775	26.667	19.400	Si1O2	56.403	.613
KK : 2	.990	2.280	1.205	K 2O1	2.746	.035
CaK : 2	.978	.274	.141	Ca1O1	.384	.004
TiK : 2	.981	.996	.430	TiO2	1.661	.014
MnK : 2	.873	.083	.031	Mn1O1	.108	.001
FeK : 2	.890	1.660	.614	Fe2O3	2.374	.019
OK : 0	.000	49.020	63.323			2.000
TOTAL		100.000	100.000		100.000	1.156

Column Description

- 1) Element (K line)(2 = Link Programme giving the mineral standards 2.4.1.3
- 2) ZAF Correction. See 2.4.1.2 (AppendixD).
- 3) % Element by weight.
- 4) Atomic % of Elements
- 5) Oxides of the elements assumed to be present.
- 6) % oxides stoichiometrically calculated.
- 7) Formula of the clay.

TABLE 2.3 EXAMPLE OF THE ULTIMATE ANALYSIS CALCULATION

C CLAY A (Unfired)							
1	2	3	4	5	6	7	8
	Atomic % of Elements			Molecular content *		Oxide content	
	Analysis 1	Analysis 2	Average	Number of Molecules	Total Mol Weight	OxideWt +LOI	OxideWt% +LOI
Si (S102)	23.32	23.26	23.29	23.29	1,399.73	68.06	63.90
Al (A1203)	9.90	10.16	10.03	5.02	51 1.53	24.87	23.35
Fe (Fe203)	0.27	0.27	0.27	0.14	21.55	1.05	0.98
Ti (Ti02)	0.35	0.24	0.30	0.30	23.57	1.15	1.08
K (K20)	1.54	1.66	1.60	0.80	75.36	3.66	3.44
Na (Na20)	0.15	0.19	0.17	0.09	5.27	0.26	0.24
Ca (CaO)	0.22	0.15	0.19	0.19	10.38	0.50	0.47
Mg (MgO)	0.25	0.17	0.21	0.21	8.46	0.41	0.39
Mn(Mn02)	0.02	0.00	0.01	0.01	0.87	0.04	0.04
OXYGEN	63.97	63.89	63.93				
LOI						6.50	6.10
Total	99.99	99.99	99.99		2,056.72	106.50	100.00

Note * =Molecular content of oxides in 100 atoms of clay.

●=LOI was measured for the same clay fired to 1000°C

Column Description

- 1) Elements in oxides being analysed
- 2) Atomic % taken from Column 4 Table2.2 (First analysis)
- 3) Atomic % taken from Column 4 Table 2.2 (Second analysis)
- 4) Average of Columns 2 & 3
- 5) Number of molecules of the oxides per 100 atoms of clay.
- 6) Column 5 multiplied by the molecular weight of the oxide of the element.
- 7) Mass of oxides (in weight %) and mass lost on ignition by 100 weight units of clay material.
- 8) Normalised results of column 7. These results are used for the Rational Analysis calculation (Table 2.4)

2.5.1.2 Rational Analysis or Proximate analysis or Calculated mineralogy.

The approximate amounts of mineralogical constituents present in the clay material calculated from the ultimate analysis. [4]

The calculation of the Rational analysis from the Ultimate analysis was first introduced by Seger in 1876. It is now understood that this calculation does not take the mineralogical composition of the clay materials into account. It is therefore not totally accurate, but nevertheless is of importance to the studio potter as an empirical method for the comparison of clay materials[8]. Some clays have their fluxing oxides present as mica and some as feldspar. Both the Feldspar convention and the Mica convention{4} calculations have been included in Table 2.4 One or other result would be used depending upon the mineralogical composition of the clay. The Feldspar convention, assuming that the clay material is felspathic, is usually used in the studio situation,

a) The feldspar convention which assumes that all the alkali oxides are present as soda feldspar and potash feldspar. The total of the K_2O and Na_2O should be low (2-4%)[4]

b) The mica convention assumes that all the alkali oxides are present as soda mica or potash mica.

It is therefore necessary to know whether feldspar or mica is present in the clay material. X-ray diffraction is the most usual source of this information recorded in published literature on the composition of clay materials. Other clay minerals that may be present in the clay material such as smectite, chlorite, vermiculite and pyrophyllite will not appear in the results on account of the assumption on which the calculations are based but may have an influence on the properties of the clay. [2]

A derivation of the calculations can be found in (Appendix A). A concise explanation of the calculations can be found below Table 2.4.

TABLE 2.4 EXAMPLE OF RATIONAL ANALYSIS [9] (C CLAY A)				
FELDSPAR CONVENTION				
MATERIAL	ENTRY	FACTOR	RESULT	
total alkalis	3.68	*5.92	21.79	%Feldspar
Feldspar	21.79	*0.183	3.99	Al ₂ O ₃ in Felds (a)
Feldspar	21.79	*0.647	14.10	SiO ₂ in Felds (b)
Al ₂ O ₃	23.35	"-a"*2.53	49.00	% Clay subst. (c)
Clay subst.	49.00	*0.463	22.68	SiO ₂ in Clay (d)
SiO ₂	63.90	"-(b+d)"	27.12	% silica
% WATER IN THE CLAY: % ORGANIC MATTER				
Clay Subst.	49.00	*0.140	6.86	Loss:H ₂ O in Clay
LOI	6.10	-H ₂ O in clay	000	Loss: CO ₂ etc.
MICA CONVENTION				
K ₂ O	3.44	*8.47	29.14	Potash Mica
Na ₂ O	0.24	*12.32	2.96	Soda Mica
Potash Mica	29.14	*0.384	11.19	Al ₂ O ₃ in K Mica (e)
Potash Mica	29.14	*0.452	13.17	SiO ₂ in K Mica (f)
Soda Mica	2.96	*0.4	1.18	Al ₂ O ₃ in Na Mica (g)
Soda Mica	2.96	*0.471	1.39	SiO ₂ in Na Mica (h)
Al ₂ O ₃	23.35	-(e+g)*2.53	27.8	Clay subst.
Clay subst.	27.8	*0.465	12.9	SiO ₂ in Clay (i)
SiO ₂	63.90	-(f+h+i)	35.91	Free Silica

Description of Columns

- 1) Material whose content must be determined. The information is taken either from the Ultimate analysis (Table 2.3) or from the results obtained in the calculation. The data from the "A" sample (as supplied) are used.
- 2) The data from column 8 of the Ultimate analysis is entered into this column. The entry column is completed as the calculation progresses. e.g. the Feldspar content in this column is taken from the result of the calculation described by the first line.
- 3) In the calculation column the symbols used are *derived* from the MACRO computer programme
 * = X : " " = Not included in the formula.
 Letters are used to explain the sequence of the calculations.

The calculation carried out according to *The Feldspar Convention* [4]

$$\begin{aligned} \text{Total alkalis} \times 5.92 &= \% \text{ feldspar} \\ \% \text{ Feldspar} \times 0.183 &= \% \text{ A1203 in feldspar} \\ \% \text{ Feldspar} \times 0.647 &= \% \text{ SiO}_2 \text{ in feldspar} \\ (\text{Total \% A1203} - \% \text{ A1203 in feldspar}) \times 2.53 &= \% \text{ clay substance} \\ \% \text{ Clay substance} \times 0.465 &= \% \text{ SiO}_2 \text{ in clay} \\ \text{Total \% SiO}_2 - (\% \text{ SiO}_2 \text{ in clay} + \% \text{ SiO}_2 \text{ in feldspar}) &= \% \text{ silica} \end{aligned}$$

The calculation carried out for *% Water in the clay*

$$\begin{aligned} \% \text{ Clay substance} \times 0.140 &= \text{loss due to water in the clay molecule.} \\ (\text{LOI} - \text{loss due to water in clay}) &= \text{loss due to organic matter.} \end{aligned}$$

The calculation carried out according to *The Mica convention* [4]

$$\begin{aligned} \% \text{ K}_2\text{O} \times 8.47 &= \% \text{ potash mica} \\ \% \text{ Na}_2\text{O} \times 12.32 &= \% \text{ soda mica} \\ \% \text{ Potash mica} \times 0.384 &= \% \text{ A1203 in potash mica} \\ \% \text{ Potash mica} \times 0.452 &= \% \text{ SiO}_2 \text{ in potash mica} \\ \% \text{ Soda mica} \times 0.400 &= \% \text{ A1203 in soda mica} \\ \% \text{ Soda mica} \times 0.471 &= \% \text{ SiO}_2 \text{ in soda mica} \\ (\text{Total \% A1203} - \% \text{ A1203 in micas}) \times 2.53 &= \% \text{ clay substance} \\ \% \text{ Clay substance} \times 0.465 &= \% \text{ SiO}_2 \text{ in clay} \\ \text{Total \% SiO}_2 - (\% \text{ SiO}_2 \text{ in clay} + \% \text{ SiO}_2 \text{ in mica}) &= \% \text{ free silica} \end{aligned}$$

4) The result of the calculation. The bold data is used for comparison of clays.

A full explanation of the above calculation is found in (Appendix A)
The explanation for use of the Data Base is given in Section 2.6.

2.5.2 The composition of the clay material.

The composition of the clay material and ultimately the clay body can be assessed from the above calculations. Tables of the data, compiled from the results of the ultimate analyses and the rational analyses, as well as additional comparative information, can be found in Chapter 4.

2.6 DATA BASE

2.6.1 *Purpose 01 the Data Base*

The information gathered in the course of this research project and any data that may be collected in the future must be collated in order to make it useful to the Ceramic Division, TWA.

2.6.2 *Description 01 the Data Base*

The computer software programme used for the purpose of storing the data is "INSIGHT Ceramic Calculations and Recipe Management Software for the Glaze, Clay and Glass sciences"(14)

The "inslght" programme does not contain calculations for the rational analysis of clays. Therefore the calculation Tables 2.3 and 2.4 were installed on a computer Macro worksheet that is accessible to the Illnsight" programme.

The materials entered in the Illnsight" Materials Definition Table (MDT) are American and Canadian but the table can be expanded to include additional materials.

In order to obtain the ultimate or chemical analysis and the rational analysis of a clay body using the "inslght" programme, the following steps must be followed:-

- a) the chemical composition of the clay materials examined must be entered into the MDT making the analysis available for the theoretical blending of clay bodies (Table 2.5).
- b) the materials can be recalled from the MDT and theoretically blended in the required quantities (Table 2.6).
- c) The ultimate analyses and the formulae of the resultant clay bodies are obtained for comparative purposes.
- d) The rational analysis can be calculated using the ultimate analysis (Table 2.7. See also Table 2.4) for additional comparison.

An explanation of Table 2.5 and 2.6 appears after the tables.

Table 2.5		
EXAMPLE OF CLAY ENTERED INTO THE MATERIALS DEFINITION TABLE		
MOSS CLAY MATERIAL		
	A	B
SiO ₂		65.39%
Al ₂ O ₃ ...		26.83%
Fe ₂ O ₃		1.58%
TiO ₂ ..		1.36%
K ₂ O.		4.30%
Na ₂ O.		.24%
CaO		.03%
MgO		.24%
MnO		.02%
	94.31	100%
(LOI)	(5.70%)	
	E	F
	FORMULA	ANALYSIS
CaO	.00	.03%
MgO	.02	.23%
K ₂ O	.17	4.06%
Na ₂ O	.01	.23%
Fe ₂ O ₃	.04	1.49%
MnO	.00	.02%
TiO ₂	.06	1.28%
*Al ₂ O ₃	1.00	25.30%
SiO ₂	4.14	61.66%
COSTIKG 0		
L.O.I. 5.70%		
RATIO 4.14		
EXPAN 5.90		
WEIGHT 403.20		

Table 2.6		
EXAMPLE OF CLAY MATERIAL BLENDED IN A CLAY BODY.		
MOSS CLAY BODY		
	C	D
Moss Clay	50	50%
SA Silica	30	30%
SA KFelds	20	20%
	100	100%
<p>The analyses for SA Silica and SA K Feldspar are included (Appendix E)</p>		
	G	H
	FORMULA	ANALYSIS
CaO	.00	.02%
MgO	.02	.12%
K ₂ O	.32	5.13%
Na ₂ O	.02	.26%
Fe ₂ O ₃	.03	.81%
MnO	.00	.01%
TiO ₂	.05	.68%
*Al ₂ O ₃	1.00	17.49%
SiO ₂	7.33	75.48%
COSTIKG 0		
L.O.I. nfa *		
RATIO 7.33		
EXPAN 5.75		
WEIGHT 583.05		

The information gained from the "Insight" programme is:-

a) .The clay recipe in *Standard Formula calculation* Shown in Table 2.5.and 2.6.

Column A: The ultimate analysis, calculated from the EDAX data This is, in effect, the "recipe" of the clay material. The LOI is entered in the programme and is accounted for in the calculation.

Column B: The ultimate analysis (recipe) including the LOI expressed as a percentage.

Column C: The clay body recipe

Column D: The recipe expressed as a percentage.

Column E: The formula of the clay in which the oxide mix is expressed according to the relative numbers of molecule types^[14]. This information can give insight into the molecular structure responsible for the firing behavior. The formula can be adjusted to show a single material or a group of materials as unity. In the case of clay it is convention to give Al_2O_3 as unity. This allows for comparison of materials.

Column F: The formula is multiplied by the atomic weight of each oxide and then brought to a percentage. In this instance it is similar to the ultimate analysis entered in Column A as the clay material is not blended. The LOI is not included.

Column G: The formula of the clay body.

Column H: The analysis of the clay body. This information can be entered into the rational analysis calculation (Table 2.4.)

.b)The *Detail Formula calculation* giving a detailed break down of materials into relative numbers of molecule types, or a *Mix ticket* giving the mixing instructions according to batch.size, An example is not included of these two calculations as it is the same information as that in Column H in different format.

c) The "cost" has not yet been programmed.

d) The LOI taken from the results of the physical tests.

e) The Ratio of Silica to Alumina.

f) The thermal expansion of the clay theoretically calculated by the "Insight" programme.

g) The Molecular weight of the formula.

CHAPTER 3

RESULTS OF CLAY MATERIAL ANALYSIS

The results of the research into the composition of clay materials are included in this chapter. The analysis and summary of each of the nine clay materials is shown separately. It should be noted that the summary includes conclusions that will be repeated in Chapter 4 in order to make this chapter a complete reference of the clay materials. Details on the calculations included in this chapter are given in Appendix A, on the results of the physical tests in Appendix C, and the raw data from EDAX and ultimate and rational analyses can be found in Appendix D. The comparative tables of the results of the analyses are included in Chapter 4.

It should be noted in the Water Absorption and Linear Shrinkage tables that although the temperature is DoC the sample has in fact been fully dried to 110°C to rid the clay of the pore water and to complete the wet to dry shrinkage.

When giving the chemical composition of clays it is convention to list them as oxides and to include loss on ignition (LOI). In analysis done on calcined samples (e.g. Sample D) the LOI value is given. In such cases the analysis is adjusted to total 100 weight units.

It should be noted that the *clay table* and *spectrum* do not show the same information. The *clay table* shows the calculated ultimate analysis (Table 2.3) of the clay material in terms of the component oxides. The *spectrum* shows the relative amounts of elements in one of the two samples included in the ultimate analysis.

As the Rational analysis is based on the assumed mineralogical composition of the clay material (2.5.1.2) and as the results from the A and D samples proved to be similar, only the results of the A sample are included in the results for comparative purposes.

As a final comparative technique the nine clay materials chosen were combined with feldspar and silica in a known proportion and formed into clay bodies (2.3.3). The reason for this final comparison is that clay is seldom used in its found state but rather blended, to form a required body for use in the studio (1.1). These resultant clay bodies could be compared both quantitatively and empirically. The results of the plasticity tests appear in this chapter. The comparative table of the Ultimate analyses of the clay bodies can be found in Chapter 4 (Table 4.2).

BALL CLAY ✓

3.1. A-CLAY

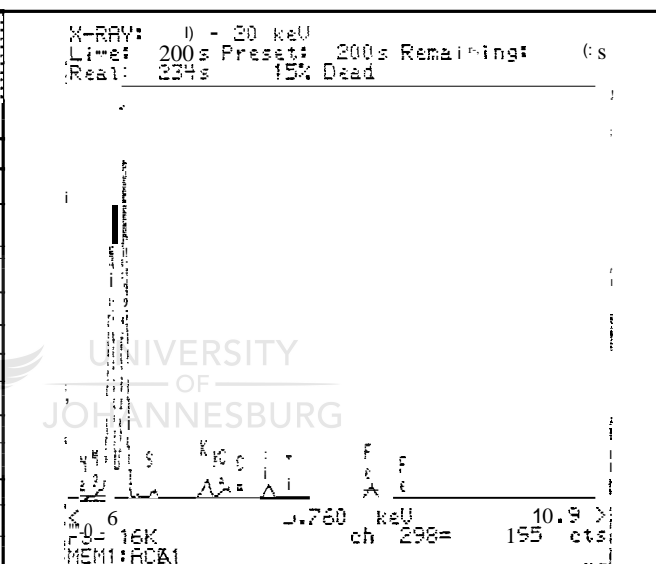
3.1.1. *Origin and Mineralogy*

"A" clay occurs in the Vereeniging region. It is mined and supplied in an unaltered state.

3.1.2 *Clay analysis*

The Ultimate and Rational analyses were carried out from the data collected on the SEM./EDAX (2.5.1) (Appendix D). The results of the Ultimate analysis of A-Clay A can be found in (Table 3.1) and D in (Table 3.4) The results of the Rational analysis of A-Clay A can be found in (Table 3.5).

TABLE & SPECTRUM 3.1 COMPOSITION OF A-CLAY A	
Oxide	Oxide Wt %
SiO ₂	46.02
Al ₂ O ₃	34.07
Fe ₂ O ₃	3.53
TiO ₂	2.18
K ₂ O	1.37
Na ₂ O	0.20
CaO	0.91
MgO	0.50
MnO	0.07
SO	0.58
LOI	10.6
Total	100.00



A -CLAY A

Magnification X 2000

The individual hexagonal flat platelets can be seen. (Ch. 1)

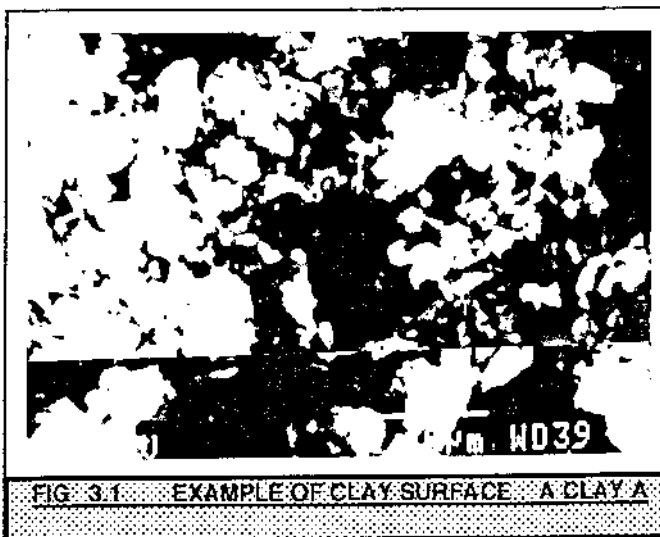
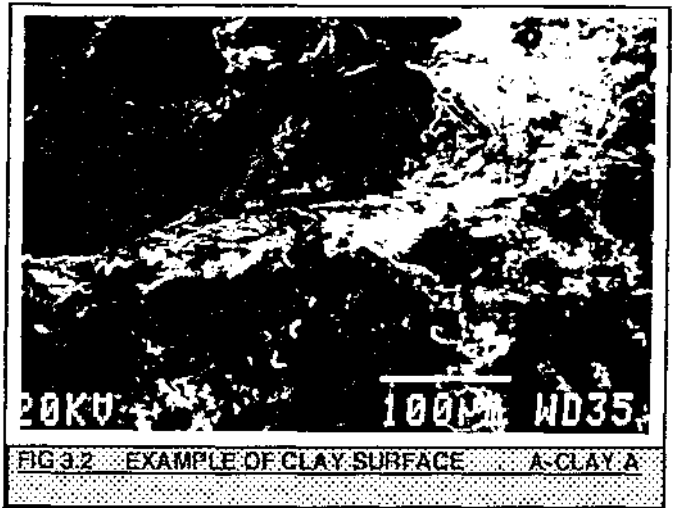


FIG 3.1 EXAMPLE OF CLAY SURFACE A-CLAY A

A-CLAY A

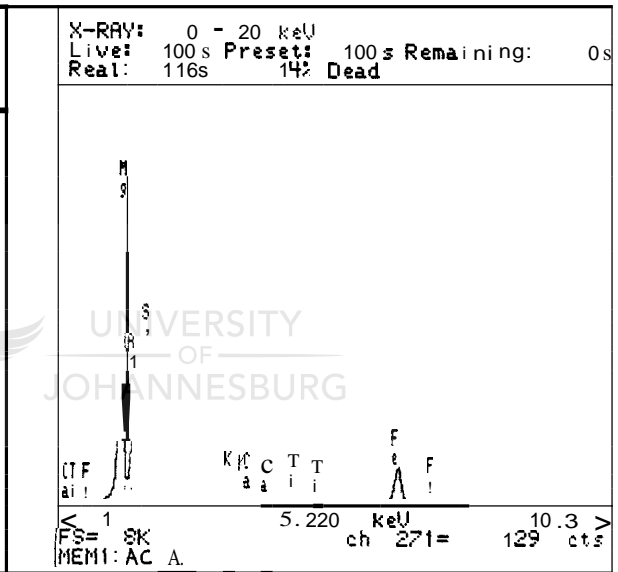
Magnification X 1160

This micrograph shows an individual, magnesium rich, particle
 These isolated particles proved to be quite common in this clay.
 Needle-like particles can be seen around the magnesium particle.



SPECTRUM 3.2
A-CLAY A

Composition of the particle indicated in Fig 3.2



SPECTRUM 3.3

This spectrum shows the composition of a particle found in A-Clay. This particle is high in Fe and proved to be common in this clay material.

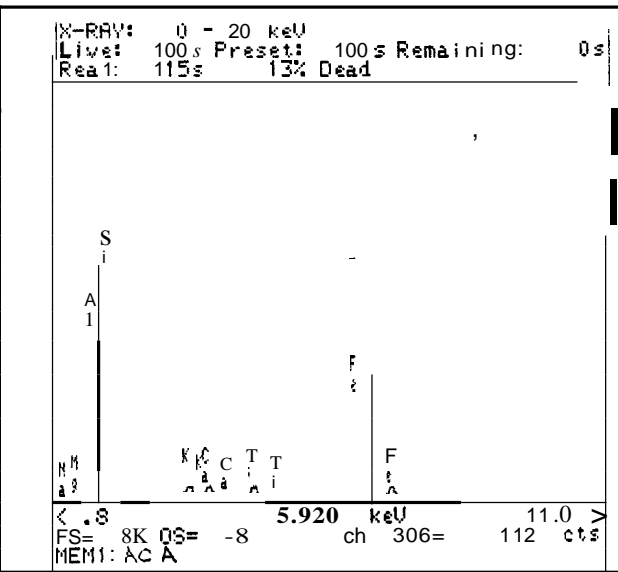


TABLE & SPECTRUM 3.4 COMPOSITION OF A-CLAY D	
Oxide	OxideWt. %
SiO2	49.82
Al2O3	33.57
Fe2O3	1.68
TiO2	1.93
K2O	1.01
Na2O	0.07
CaO	0.35
MgO	0.38
MnO	0.02
SO	0.58
LOI	10.6
Total	100.00

X-RAY: 0 - 20 keV
 Live: 100s Preset: 100s Remaining: 0s
 Real: 174s 43% Dead

FS= 32K MEM1: AC_D 4.860 keV 10.0 >
 ch 253= 711 cts

A-eLAYD

Magnification X 600

This is a micrograph of the surface of the clay fired to 1200°C

Large well fluxed particles can be seen. These particles are also visible in FIG 3.5



FIG 3.3 EXAMPLE OF CLAY SURFACE A-CLAY D

A-CLAY D

Magnification X 1200

This micrograph of the crack in FIG 3.3 shows "ligaments" of fluxed material preventing the crack from splitting open.

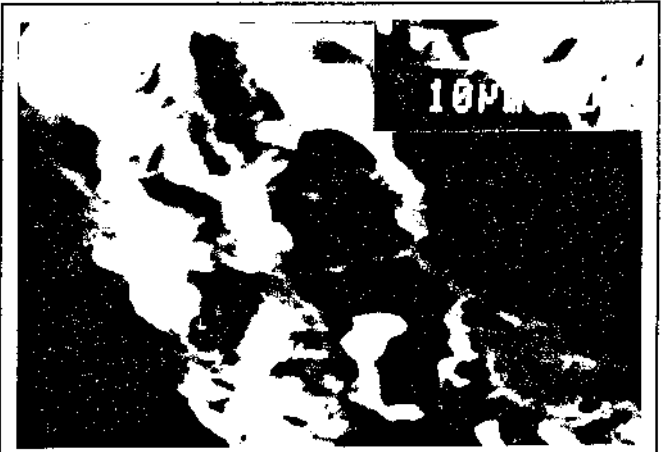


FIG 3.4 EXAMPLE OF CLAY SURFACE A-CLAY D

TABLE 3.5 RATIONAL ANALYSIS	
A-CLAY A	
FELDSPAR CONVENTION	
Material	Weight %
Feldspar	9.12
Clay substance	81.06
Free Silica	2.10
MICA CONVENTION	
Potash mica	11.43
Soda Mica	2.34
Clay substance	71.81
Free Silica	5.87
% WATER IN CLAY :	
% ORGANIC MATTER	
Loss :H ₂ O in Clay	11.35
Loss: CO ₂ etc.	0

The data in Table 3.5 is the result of the Rational Analysis calculation (Table 2.4)

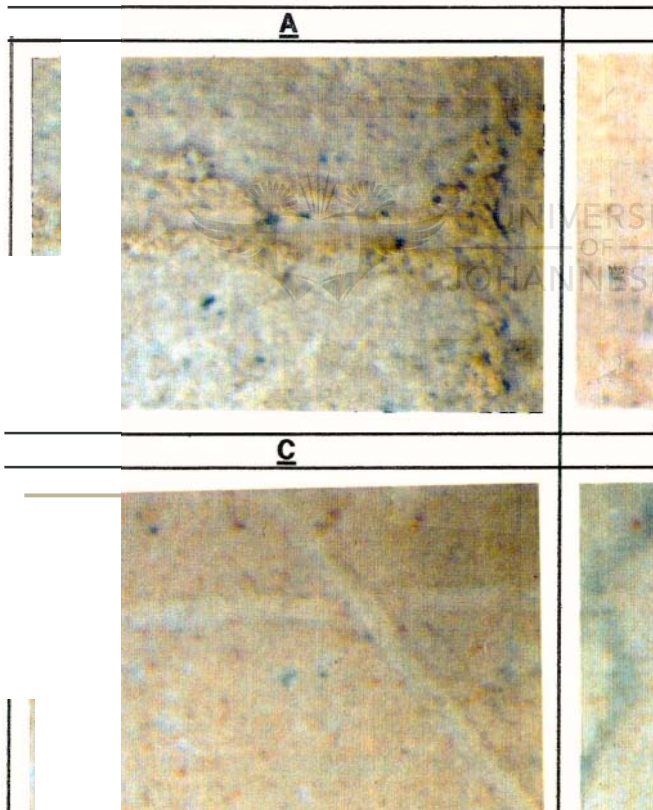


FIG 3.5
PHOTOGRAPHS OF THE SURFACE OF THE CLAY MATERIAL X 80 (Table 2.1)

3.1.3 Clay Properties

3.1.3.1 Water Absorption and Linear Shrinkage

A-CLAY



The results of the linear shrinkage and absorption tests (2.4.2) are shown in this chart.

There is no value for the absorption test for A-Clay A as the sample is unfired and disintegrates in water.

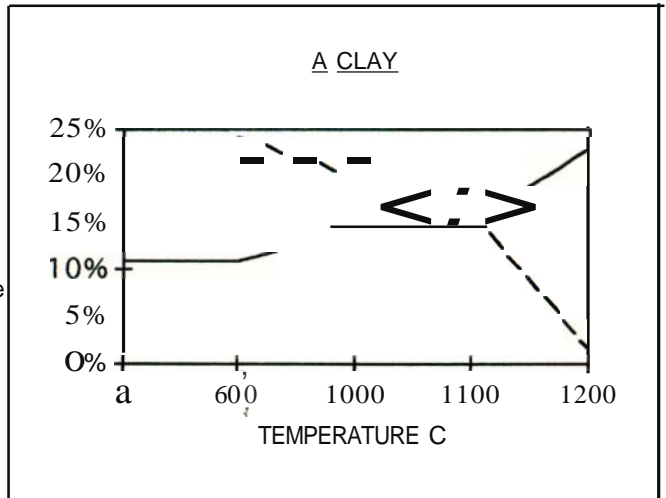


FIG 36 ABSORPTION & SHRINKAGE

3.1.3.2 Colour

A-CLAY

Photograph of A -CLAY fired to the selected temperatures. The change in colour can be clearly seen.

The colour at 1100oC (C) is the palest.



FIG 37 COLOUR OF THE A-CLAY SURFACE

3.1.3.3 Particle Size

2 microns is the upper grain-size limit for materials to be classified as clay. [2] 2.4.2.3

PARTICLE SIZE

The peak in the size distribution is at 20 μm and 3.9% of the particles are less than 2 microns in size .(Appendix C)

3.1.4 Summary and Preliminary Evaluation

A-clay is a plastic fire-clay from the clayfields of Vereeniging and Van der Bijl Park. **Fire-clays** are suitable for making oven ware.

A-clay has 5.71 % combined Fe+Ti (Table 3.1) The requirement for whiteware is 2% (2.5.2.1) With additions of Feldspar and Silica to make up a clay body. this clay could be useful for a slightly off-white ware fired to 1100°C The titanium content is the highest of all the clays tested (Table 4.1). This will enhance the staining power of the iron in the clay material.

The % particles below 2 microns is low (3.1.3.3) with the peak at the largest value in the particle size valuation at 20µm indicating that there is a fairly high proportion of large clay particle but a spread of particle sizes making the clay material very plastic when formed into a clay body. This clay material is high in Alkaline earths (Table 4.1 b) (1.2) a contributing factor to plasticity. (6)

The Alumina content is the highest among the selected clays materials making the material refractory. This will minimise the shrinkage and increase the firing range (Table 4.1).

The total of the fluxes = 3.0% (Table 4.1). The clay fluxes strongly after 1100°C (FIG 3.5) The fluxing begins in small isolated pinheads (FIG 3.5)

Along with the fluxing the colour changes. (FIG 3.7)

BALL CLAY

3.2 B13 BALL CLAY

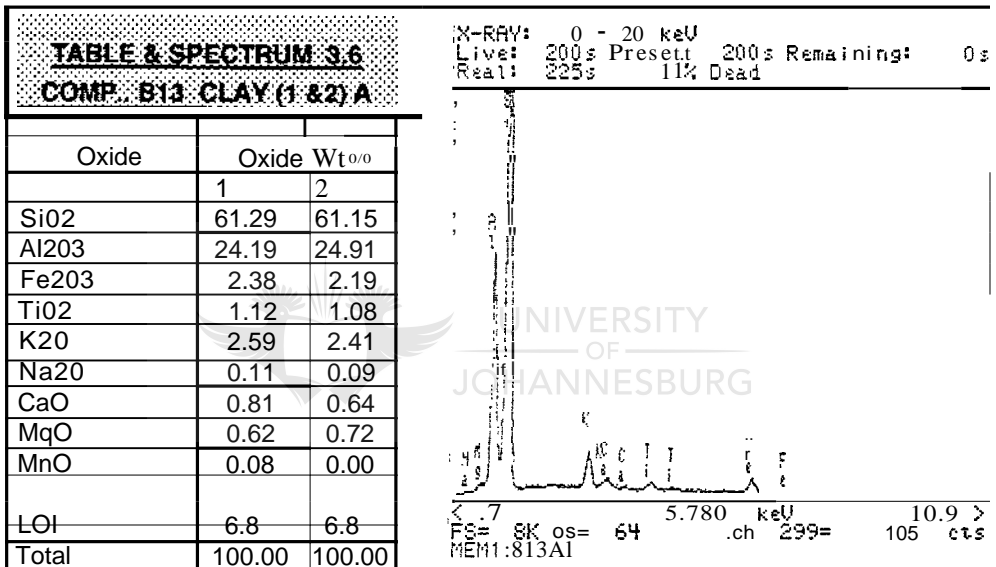
3.2.1 Origin and Mineralogy

The clay deposit is on the farm 8uffelsfontein in the Riversdale district. The material consists mainly of kaolinite, illite and quartz,110j

3.2.2 Clay Analysis

The Ultimate and Rational analyses were carried out using the data collected by the SEM./EDAX (2.5.1). The results of the Ultimate analysis of 813 Clay A can be found in (Table 3.6) and D in (Table 3.7). The results of the Rational analysis can be found in (Table 3.8).

Two samples of the clay were analysed as a new batch of clay was brought into the studio. (3.2.4)



813 CLAY A

Magnification X 2000

The individual hexagonal flat platelets can be seen. (1.2) This photo is taken of a rough patch where the particles are separate.

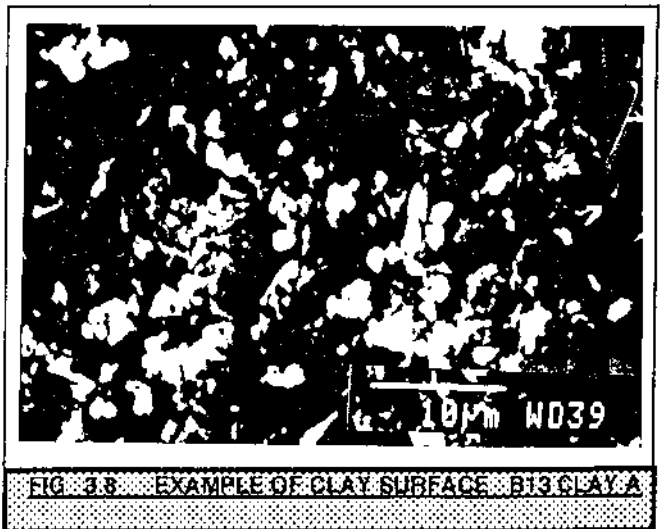
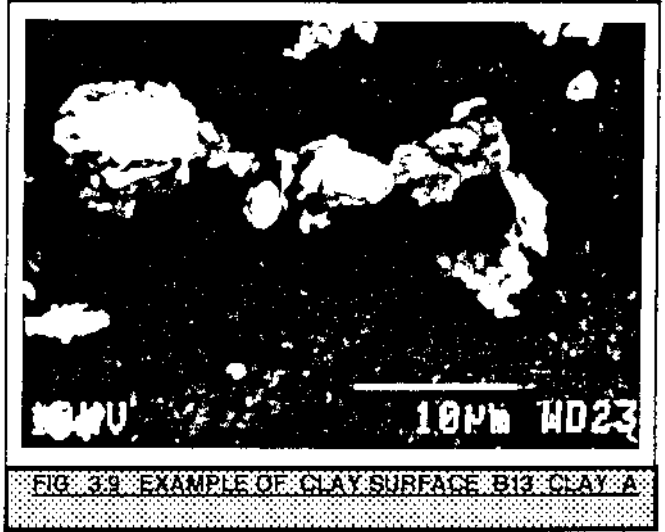


FIG 3.3 EXAMPLE OF CLAY SURFACE B13 CLAY A

813 CLAY A

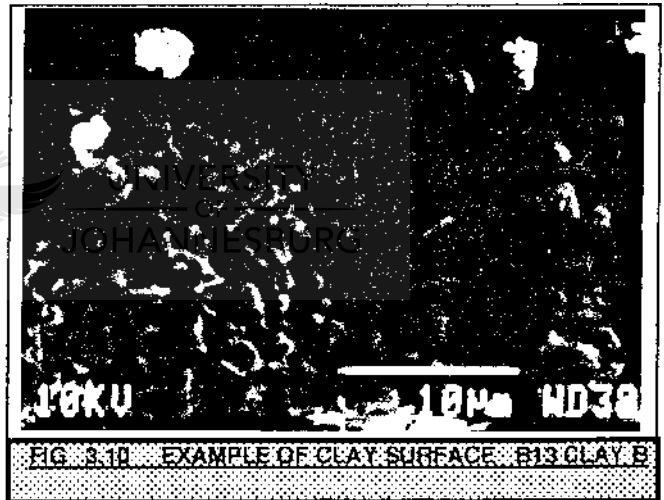
Magnification X 2000

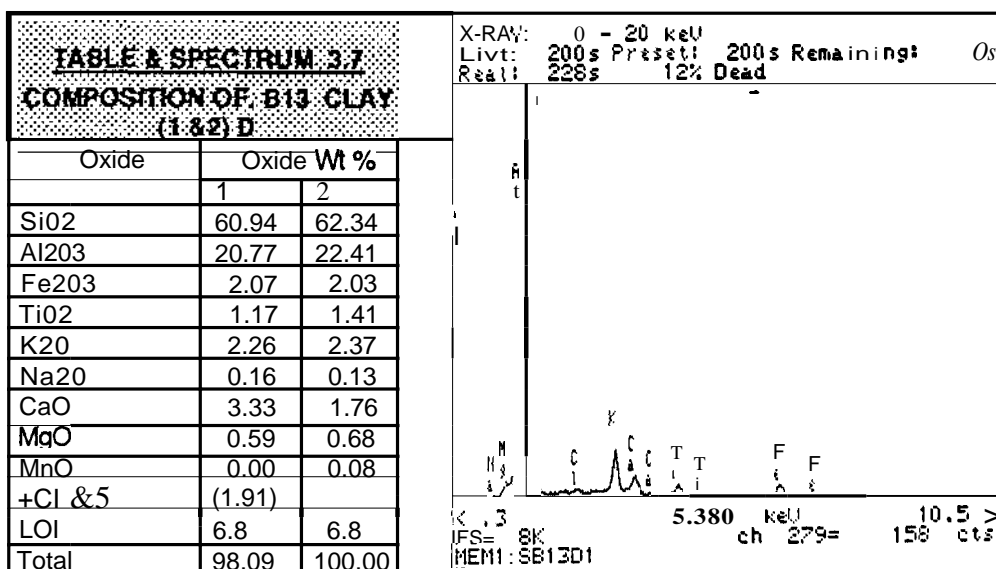
Sample of 813 A in powder form.
The flat flaky nature of the
particles is shown.

**813 CLAY B**

Magnification X 2200

This is the only example of a
B sample in the SEM.
The particles are still separated
and unchanged in form after
firing at this temperature.
(Table 2.1)

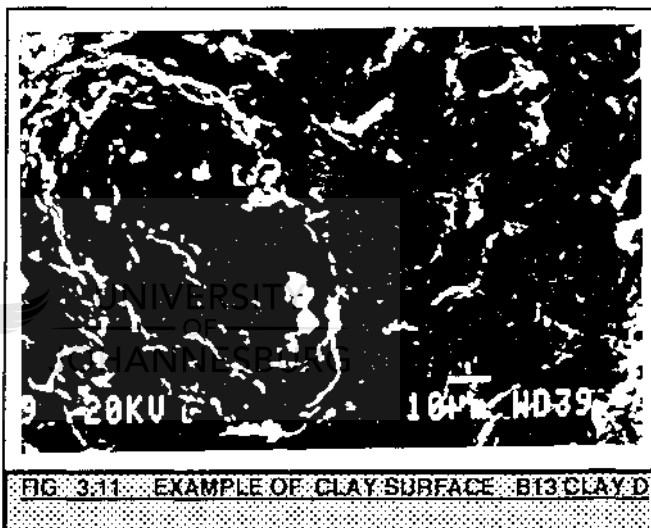




813 CLAY D

Magnification X 600

The sintered surface with separate particles is shown in this micrograph



813 CLAY D

Magnification X 600

The sintered surface of the clay material can be seen .

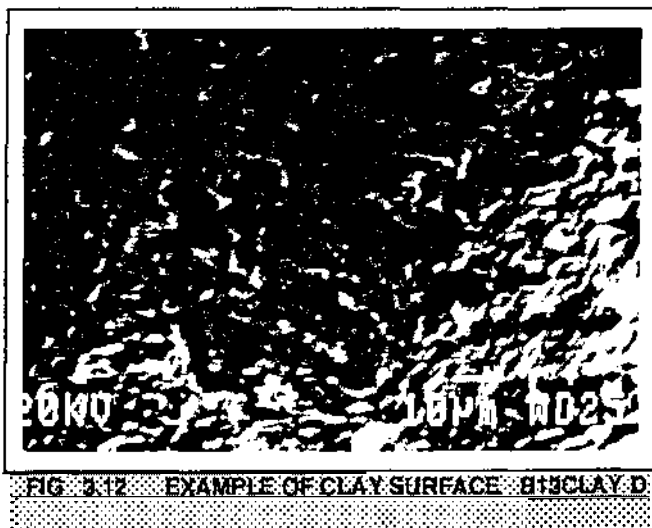


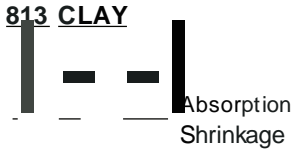
TABLE 3.8. RATIONAL ANALYSIS	
B13 CLAY(2) A	
FELDSPAR CONVENTION	
Material	Weight Percentage
Feldspar	15.98
Clay substance	53.8
Free Silica	26.04
MICA CONVENTION	
Potash mica	21.43
Soda Mica	1.23
Clay substance	37.69
Free Silica	32.05
% WATER IN CLAY: % ORGANIC MATTER	
Loss H ₂ O in Clay	7.53
Loss: CO ₂ etc.	0

The data in Table 3.3 is the result of the Rational Analysis calculation (Table 2.4)



3.2.3 Clay Properties

3.2.3.1 Water Absorption and Linear Shrinkage



The results of the linear shrinkage and absorption tests (2.4.2) are shown in this chart. The temperatures are those shown in Table 2.1. There is no value for the B13-A absorption test as the sample is unfired and disintegrated in water.

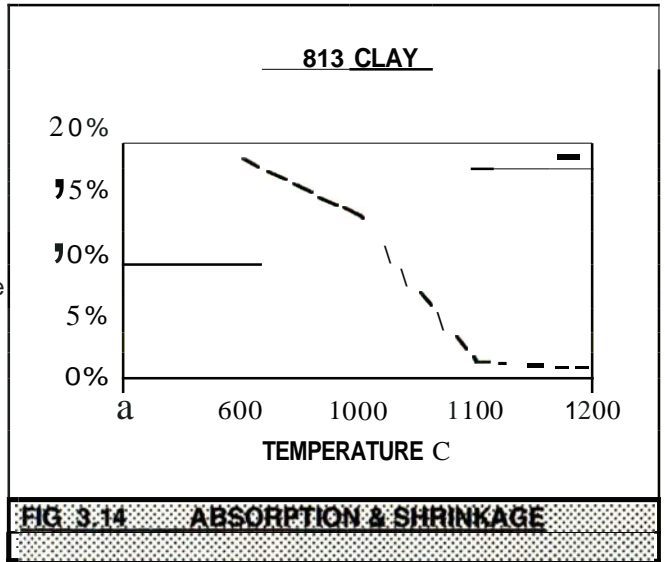


FIG 3.14 ABSORPTION & SHRINKAGE

3.2.3.2 Colour

813 CLAY

Photograph of B13 CLAY fired to the selected temperatures. The change in colour can be clearly seen.

The colour at 1100°C (C) is the palest. At 1200°C the colour is a yellow/green.

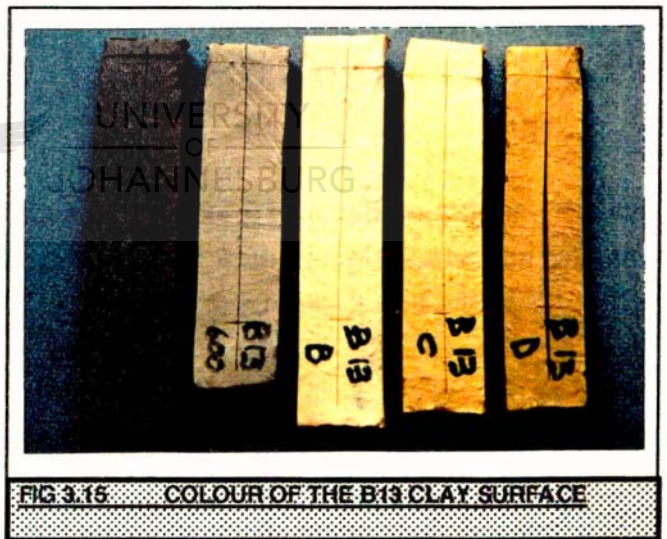


FIG 3.15 COLOUR OF THE B13 CLAY SURFACE

3.2.3.3 Particle Size

2 microns is the upper grain-size limit for materials to be classified as clay. (2.4.2.3)

PARTICLE SIZE	The peak in the size distribution is from 2µm to 7µm and 16.2% of the particles are less than 2 µm in size (Appendix C)
----------------------	---

3.2.4 Summary and Preliminary evaluation.

B 13 is a commonly used clay supplied by G&W Base Minerals.

On examination the clay appears fine particled but highly speckled.

(FIG 3.13) The clay content is high 16.2% of the particles are below $2\mu\text{m}$ in size (3.2.3.3)

The clay mixed into a clay body was of average plasticity.

The Fe+Ti content is 3.2%. When combined with feldspar and silica to form a clay body the white wares requirement of 2% would be met. The clay has a characteristic green tinge at fluxing temperatures.(3.15) Fluxing occurs giving a biscuit-like surface.

Separate particles of iron, chromium, titanium and calcium were identified in the material.

The absorption curve shows that vitrification is almost complete by 11 aaoe and the shrinkage is minimal from e to D. Le. 11 00VC - 12aOoe (Fig 3.14)

When comparing the two clay samples of B13 it was found that the iron content in sample 1 is almost .2% higher than sample 2 and the total flux content in sample 1 is 13.3% higher than in sample 2.and 44% higher than the supplier's analysis states. (Appendix B)

BALL CLAY

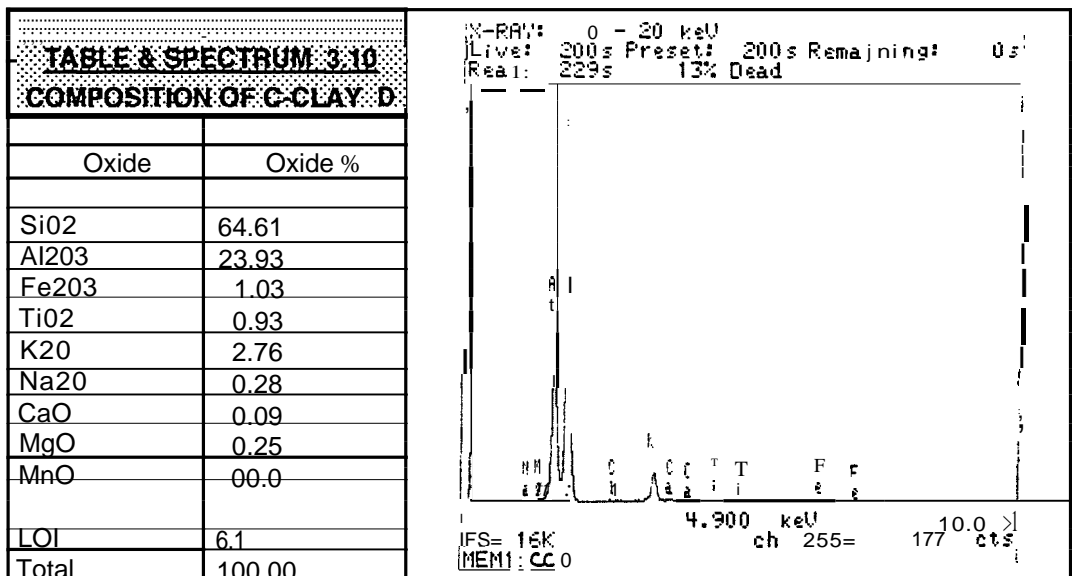
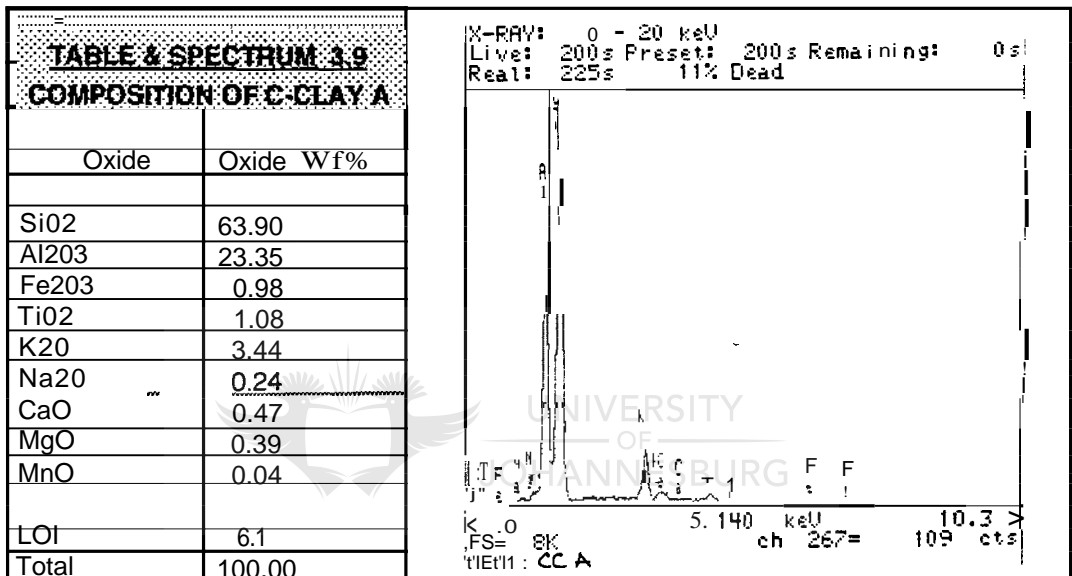
3.3 C-CLAY

3.3.1 Origin and Mineralogy

C-Clay (Crous clay) is mined at Peyneskraal in the Grahamstown district. The material consists mainly of illite with a small amount of kaolinite[11]

3.3.2 Clay Analysis

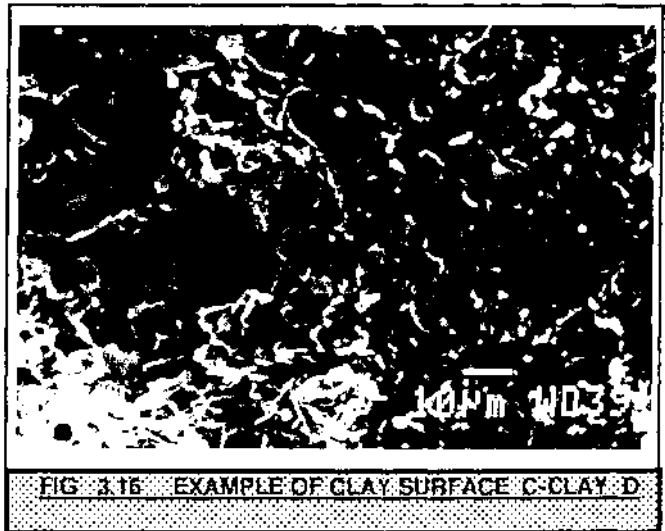
The Ultimate and Rational analyses were carried out using the data collected on the SEM IEDAX (2.5.1)(Appendix D)The results of the ultimate analysis of C-clay A can be found in (Table 3.9) and D in (Table 3.10) The results of the Rational analysis of C-Clay can be found in (Table 3.12)



c-eLAV 0

Magnification X 600

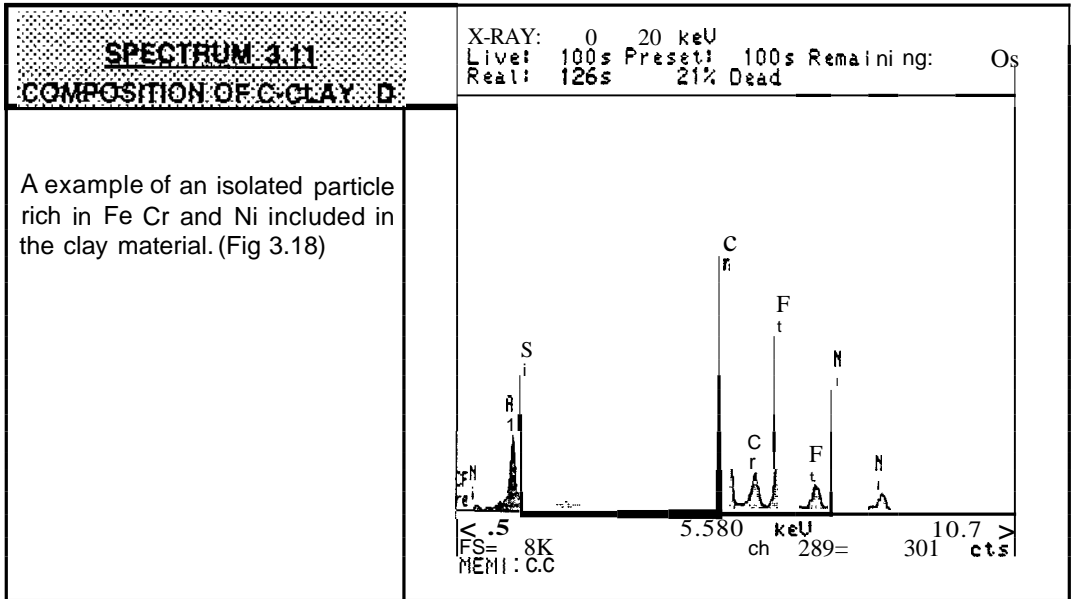
The individual hexagonal flat platelets can be seen. (1.2)
The particles are beginning to sinter and coagulate.

**C-eLAVD**

Magnification X 2000

The individual particles have run together forming a lattice on the surface.





c-eLAY D

Magnification X 600

The particle of Cr,Fe and Ni can be seen resting on the surface. the surrounding clay is sintered and congealed.(Spectrum 3.11)

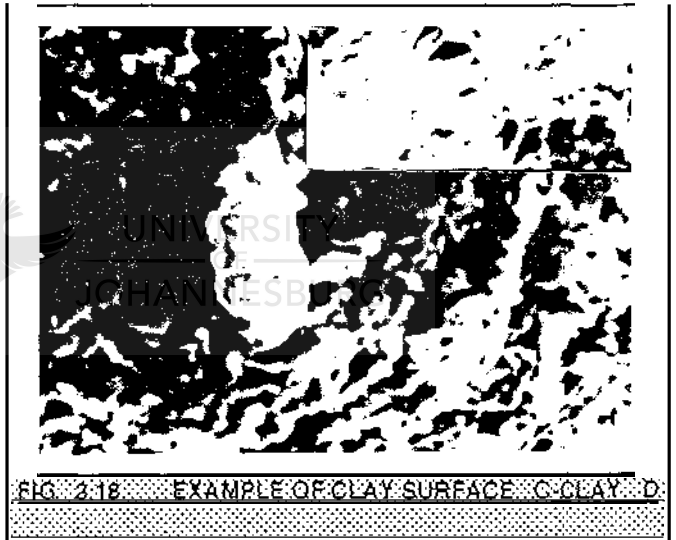


TABLE 3.12 RATIONAL ANALYSIS	
G-CLAY A	
FELDSPAR CONVENTION	
Material	Weight%
Feldspar	21.76
Clay substance	48.99
Free Silica	27.12
MICA CONVENTION	
Potash mica	29.14
Soda Mica	2.96
Clay substance	27.78
Free Silica	36.42
WATER IN CLAY : %ORGANIC MATTER	
Loss :H ₂ O in Clay	6.86
Loss: CO ₂ etc.	0

The data in Table 3.12 is the result of the Rational Analysis calculation (Table 2.4)

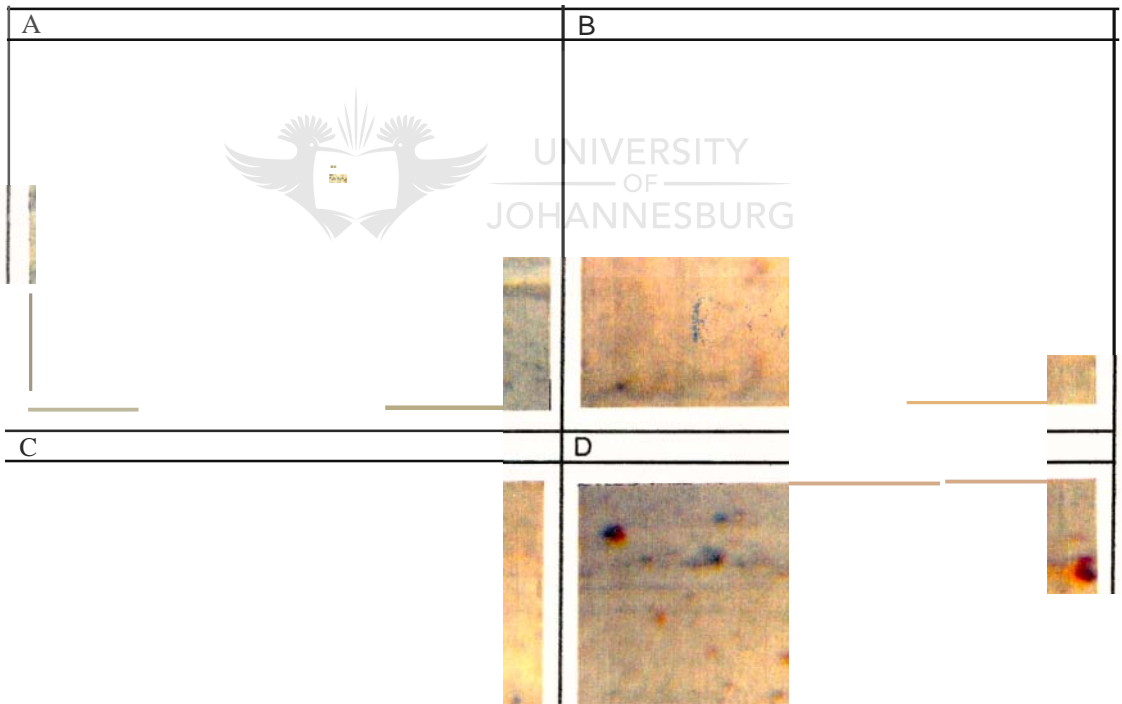


FIG 3.19
PHOTOGRAPHS OF THE SURFACE OF THE CLAY MATERIAL X 80 (Table 2.1)

3.3.3 Clay Properties

3.3.3.1 Water Absorption and Linear Shrinkage

C-CLAY



The results of the linear shrinkage and absorption tests (2.4.2) are shown in this chart.

There is no (A) or 600°C value for the absorption test as these samples disintegrated in water.

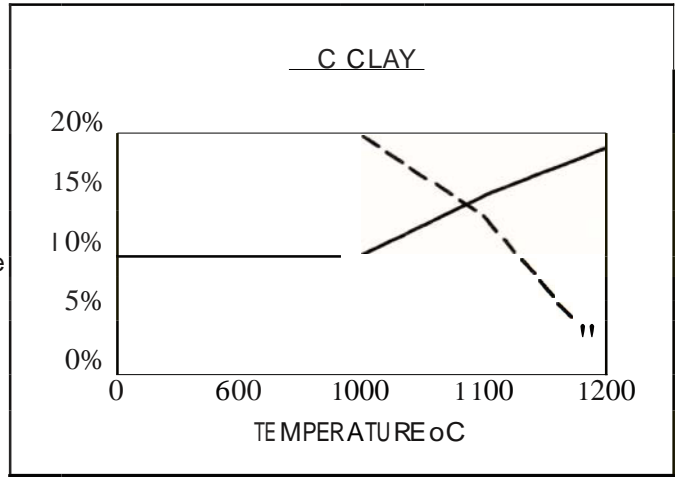


FIG 3.20 ABSORPTION & SHRINKAGE

3.3.3.2 Colour

C-CLAY

Photograph of C-CLAY fired to the selected temperatures.

This is a light coloured clay, even at high temperatures.



FIG 3.21 COLOUR OF C-CLAY SURFACE

3.3.3.3 Particle Size

2 microns is the upper grain-size limit for materials to be classified as clay. [2] 2.4.2.3

PARTICLE SIZE	The peak in the size distribution is at 8µm and 7.4 % of the articles are less than 2 µm in size. (Appendix c)
----------------------	--

3.3.4 Summary and Preliminary evaluation.

C-Clay is among the whitest of the clays tested. The combined **Fe+Ti** value is 2.06% (Table 4.1 a) making it a suitable whiteware clay but the clay displays a tendency to dilate when combined in a clay body and the plasticity is mediocre. (3.32)

The Silica content is the highest of the tested clays and the Alumina the lowest. (FIG 4.1)

The total flux content is 4.58% which is high. The result of this can be seen in the total vitrification of the clay at 1200°C (FIG 3.20) but the clay was not sintered at 600°C causing the sample to disintegrate when boiled for the water absorption test.

The fluxing occurs in "chains" over the surface of the material. (FIG 3.17)



BALL CLAY

3.4 MOSS CLAY

3.4.1 Origin and Mineralogy

The deposit is on the farm Collingham in the Grahamstown district. The material consists mainly of kaolinite, illite and quartz with a little pyrophyllite and feldspar.^[10]

3.4.2 Clay Analysis

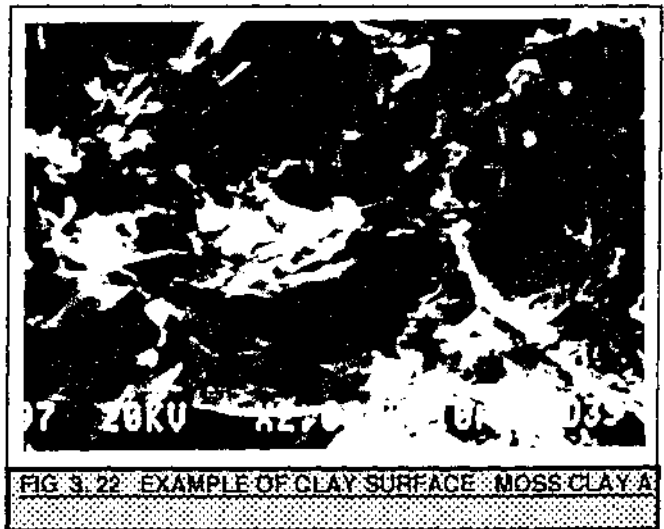
The Ultimate and Rational analyses were carried out using the data collected on the SEM./EDAX (2.5.1) (Appendix D). The results of the Ultimate analysis of Moss clay A can be found in (Table 3.13) and D in (Table 3.14). The results of the Rational analysis of Moss clay A can be found in (Table 3.16)

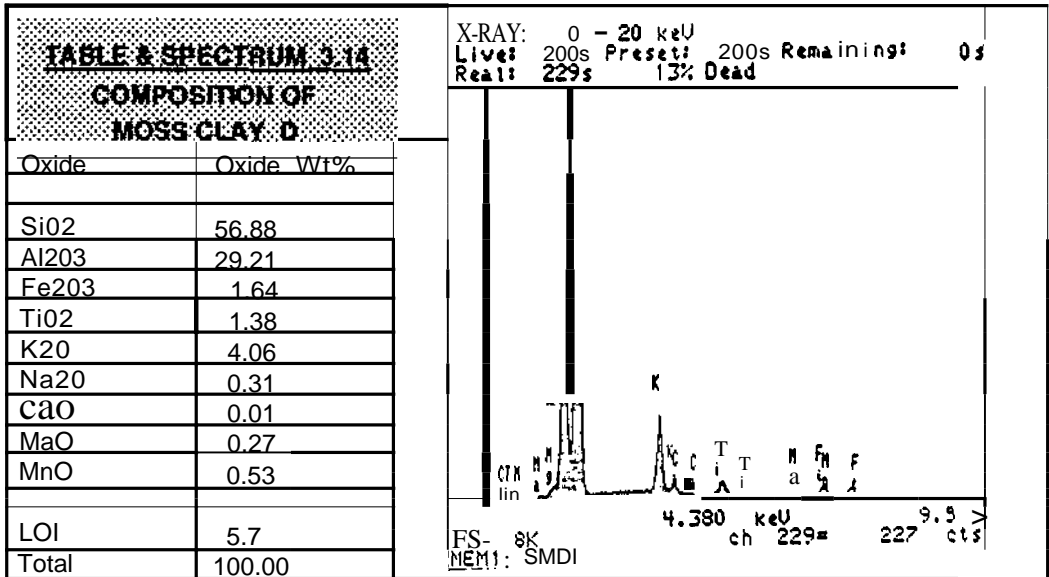
TABLE & SPECTRUM 3.13 COMPOSITION OF MOSS CLAY A	
Oxide	Oxide Wt %
SiO ₂	61.67
Al ₂ O ₃	25.30
Fe ₂ O ₃	1.49
TiO ₂	1.28
K ₂ O	4.06
Na ₂ O	0.23
CaO	0.03
MgO	0.23
MnO	0.02
LOI	5.7
Total	100.00

MOSS CLAY A

Magnification X2000

The individual hexagonal flat platelets can be clearly seen. (1.2)





MOSSCLAY 0

Magnification X 3500

The individual hexagonal flat platelets can be seen.

Moss clay exhibited the well known "stack of cards" structure

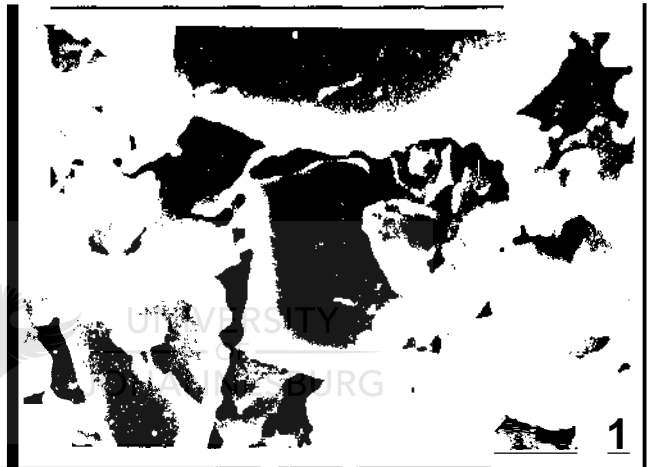


FIG. 3.23. EXAMPLE OF CLAY SURFACE. MOSS CLAY D

MOSS CLAY 0

Magnification X 3500

The individual hexagonal flat platelets can be seen stacked on edge.

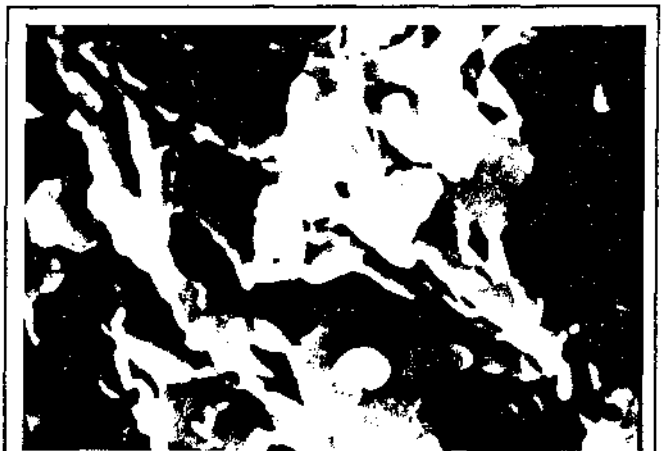
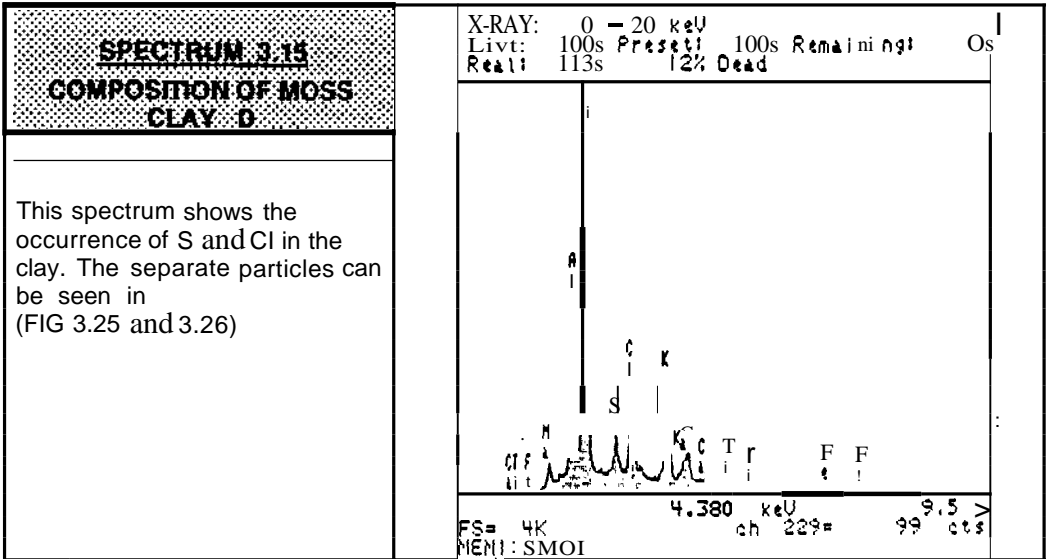


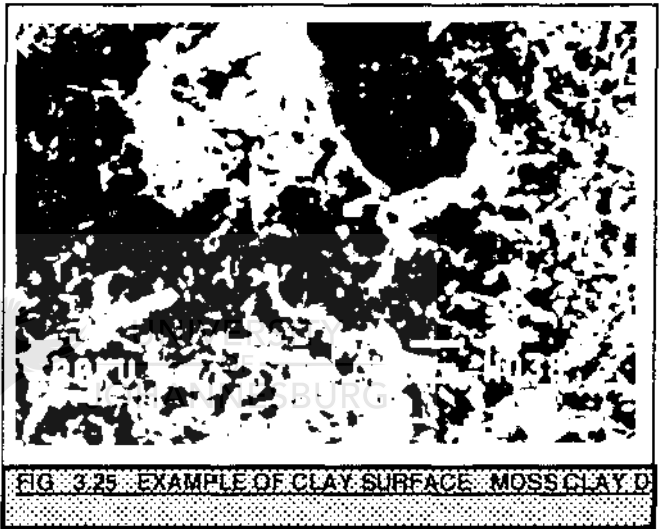
FIG. 3.24. EXAMPLE OF CLAY SURFACE. MOSS CLAY D



MOSS CLAY 0

Magnification X 750

The white particle can be seen on the surface of the clay. See (Spectrum 3.15)



MOSSCLAY D

Magnification X 1500

This is an enlargement of FIG 3.25 . The string like attachments of the sintered particles can be seen

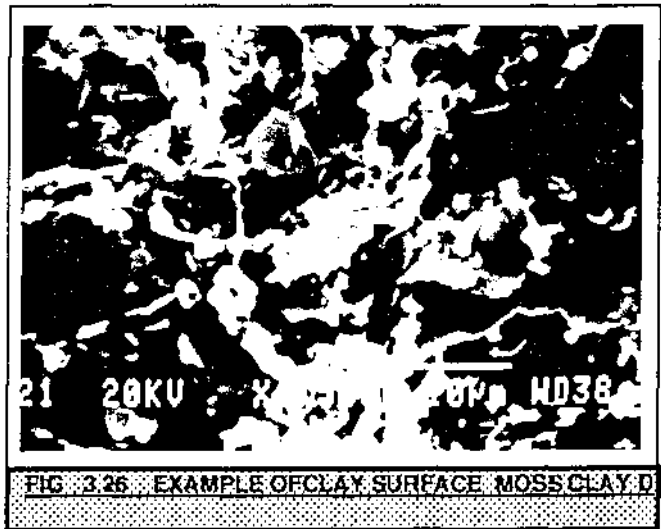


TABLE 3.16. RATIONAL ANALYSIS	
MOSS CLAY A	
FELDSPAR CONVENTION	
Material	Weight %
Feldspar	25.40
Clay substance	52.25
Free Silica	21.04
MICA CONVENTION	
Potash mica	34.39
Soda Mica	2.83
Clay substance	27.73
Free Silica	31.90
% WATER IN CLAY:	
% ORGANIC MATTER	
Loss H ₂ O in Clay	7.31
Loss: CO ₂ etc.	0

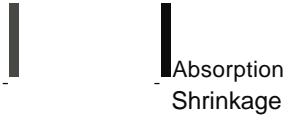
The data in Table 3.16 is the result of the Rational Analysis calculation (Table 2.4)



3.4.3 Clay Properties

3.4.3.1 Water Absorption and Linear Shrinkage

MOSS CLAY



The results of the linear shrinkage and absorption tests (2.4.2) are shown in this chart.

There is no (A) value for the absorption test

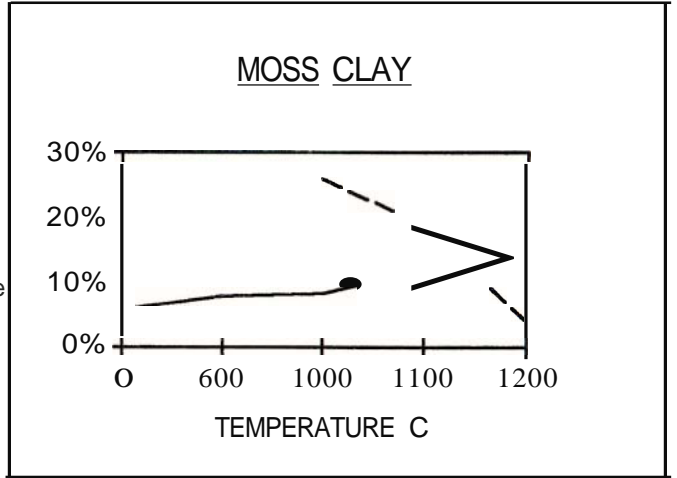


FIG 3.28 ABSORPTION & SHRINKAGE

3.4.3.2 Colour

MOSS CLAY

Photograph of A CLAY fired to the selected temperatures. the change in colour can be clearly seen.

The colour at 1100GC (C) is the palest.

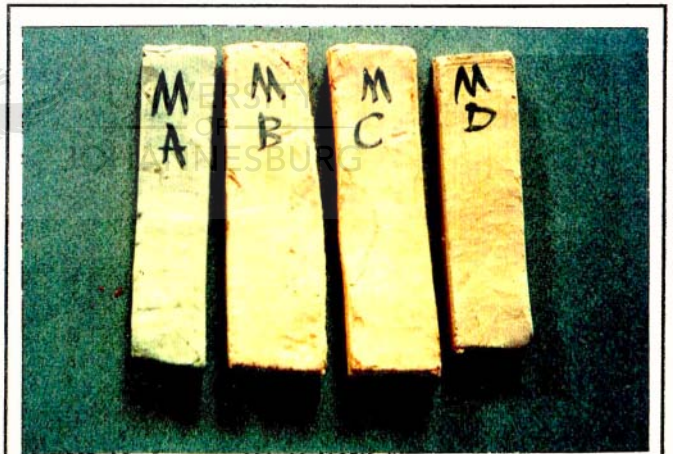


FIG 3.29 COLOUR OF THE MOSS CLAY SURFACE

3.4.3.3 Particle Size

2 microns is the upper grain-size limit for materials to be classified as clay. 12.4.2.3

PARTICLE SIZE

The peak in the size distribution is at 8.5µm and 5.1 % of the particles are less than 2 microns in size A endix C

3.4.4 *Summary and Preliminary evaluation.*

Moss clay is a readily available clay supplied by G & W Base Minerals.

This clay is close to fluxing point at 1200⁰C but is still absorbent at 1100⁰C.(Fig 3.28)

The particle size test showed that the peak at the largest value of the particle size valuation is below 10 μ m and there is an even spread of particle sizes. Although a low proportion of particles was clay material, in the throwing test this clay proved to be very plastic and firm to throw with.

Moss clay exhibits a matrix of varying sized particles.(FIG 3.22) and a non- compacted surface different to any of the other clay materials.

The combined Fe + Ti content is 2.77 %(Table 4.1) making it a possible clay for whitewares as this content will be less than 2% after blending, even in high proportions.

The total fluxes are 4.57% which is the highest along with C Clay (Table 4.1a) The particles show a spider-like fluxing pattern over the surface of the material at 1200C.

BALL CLAY

3.5 PXX BALL CLAY

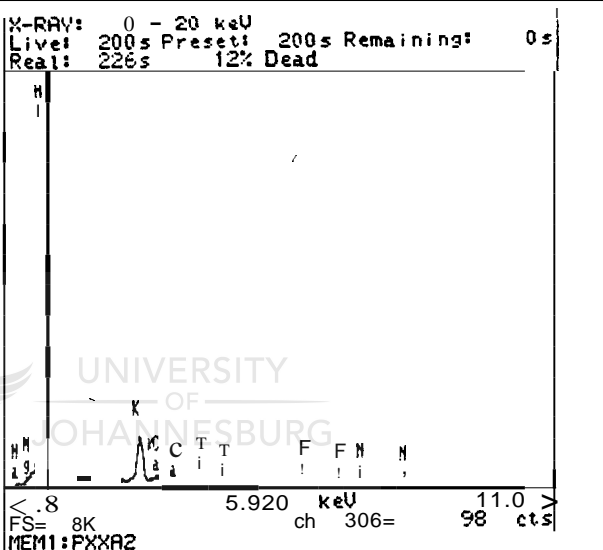
3.5.1 Origin and Mineralogy

PXX is an imported Ball clay. Origin and mineralogy unknown

3.5.2 Clay analysis

The Ultimate and Rational analyses were carried out using the data collected on the SEM IEDAX (2.5.1) (Appendix D). The results of the Ultimate analysis of PXX-clay A can be found in (Table 3.17) and D in (Table 3.18). The results of the Rational analysis of Pxx-Clay A can be found in (Table 3.19).

TABLE 3.17 COMPOSITION OF PXX CLAY A	
Oxide	Oxide WT%
SiO ₂	53.29
Al ₂ O ₃	32.62
Fe ₂ O ₃	1.04
TiO ₂	0.97
K ₂ O	2.62
Na ₂ O	0.15
CaO	0.22
MgO	0.43
MnO	0.03
LOI	8.60
Total	100.0

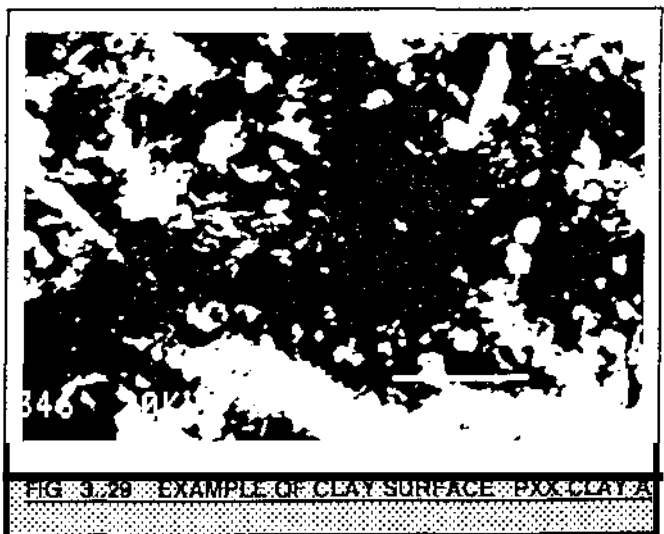


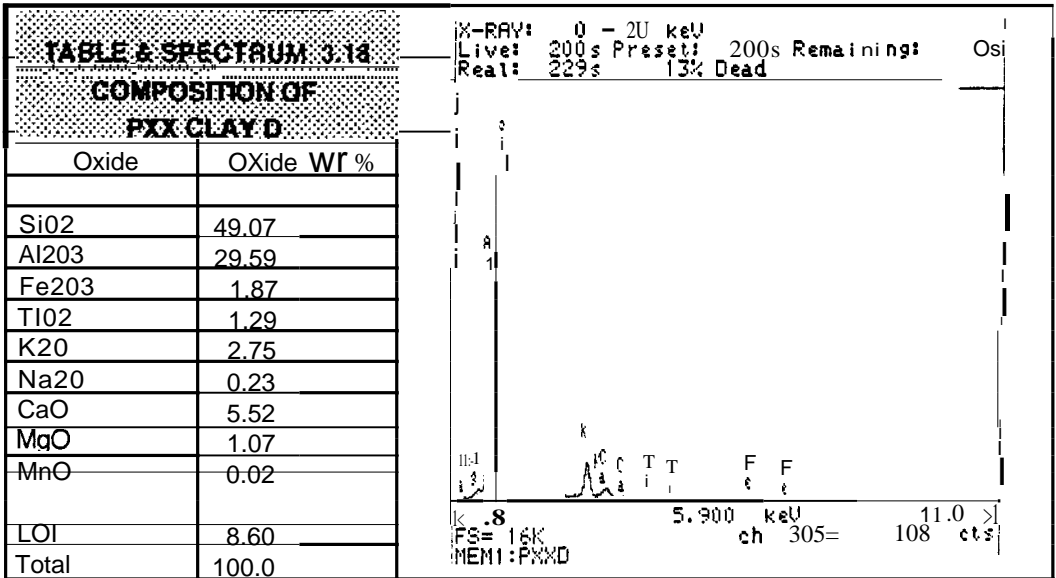
PXXCLAY A

Magnification X 2000

The individual hexagonal flat platelets can be seen.

The clay is homogeneous.





NOTE: The CaO in this sample is higher than in the other samples analysed

PXXCLAY 0

Magnification X 1000

The sintered surface.



PXX CLAY 0

Magnification X 12

The round sponge like particles can be seen.

The particles are of the same composition as the surrounding material.



3.5.4 Summary and Preliminary evaluation.

PXX Bait Clay is an imported clay used for white throwing and slip casting bodies. It was analysed in this project for comparison.

PXX Ball Clay is white at all temperatures (FIG 3.34) The combined Fe+Ti content is 2.01% which falls easily within the 2% white wares limit.

(Table 4.1)

The fluxing on the surface occurs in pinheads similar to those seen in the Kaolins

The total fluxes equal 3.45% (Table 4.1). The clay is close to vitrification at 11aoc and the shrinkage is between 15% - 20%.(Fig 3.33)

This clay proved to be very plastic when formed into a clay body and thrown on the wheel.(Table 3.32) The clay content of the material is high, 74.85% as can be noted in (Table 4.3) The particle size distribution is evenly spread without any particular peak(Appendix C).



BALL CLAY

3.6 WESTERN PROVINCE BALL CLAY

3.6.1 Origin and Mineralogy

Western Province Ball Clay is mined near Kraaifontein in the Stellenbosch district. The material consists mainly of kaolinite with some quartz. The organic matter content is very high.^[10]

3.6.2 Clay Analysis.

The Ultimate and Rational analyses were carried out using the data collected on the SEM IEDAX (2.5.1)(Appendix D).The results of the Ultimate analysis of WPBC-A can be found in (Table 3.20) and D in (Table 3.21).The results of the Rational analysis of WPBC-A can be found in (Table 3.22)

TABLE & SPECTRUM 3.20 COMPOSITION OF WPBC A		
Oxide	Oxide Wt%	
	1	2
SiO2	50.64	50.97
Al2O3	32.16	31.70
Fe2O3	1.73	1.74
TiO2	1.58	1.64
K2O	1.15	1.13
Na2O	0.08	0.06
CaO	0.19	0.18
MaO	0.58	0.59
MnO	0.00	0.10
LOI	11.90	11.90
Total	100.01	100.00

WPBC CLAY A

Magnification X 2000

The individual hexagonal flat platelets can be seen.

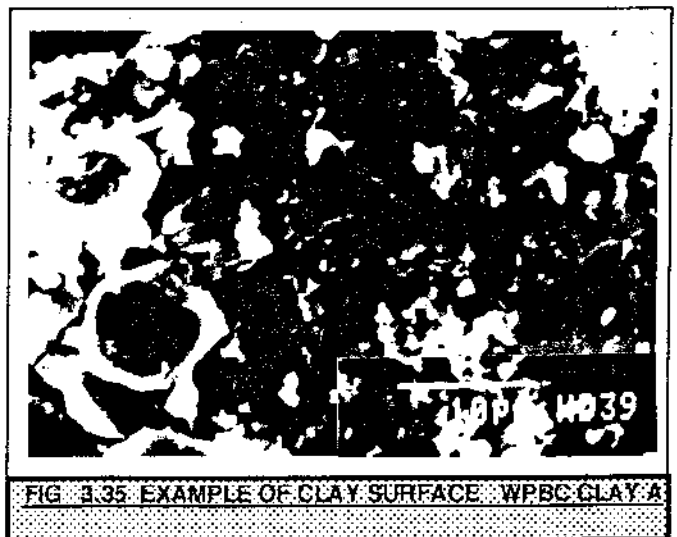
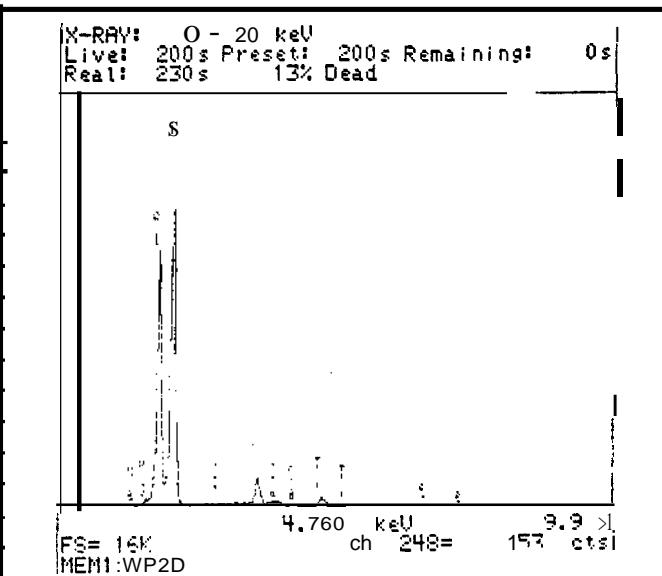


FIG 3.35 EXAMPLE OF CLAY SURFACE WPBC CLAY A

**TABLE 3.21
COMPOSITION OF WPBC D**

Oxide	OxideWt%	
	1	2
SiO2	56.29	49.18
Al2O3	26.75	31.44
Fe2O3	1.61	1.98
TiO2	1.52	1.51
K2O	1.19	2.44
Na2O	0.13	0.28
CaO	0.13	0.42
MgO	0.39	0.73
MnO	0.08	0.12
LOI	11.9	11.9
Total	100.0	100.0



WPBC CLAY D

Magnification X 2000

The surface is sintered and has a lattice-like appearance

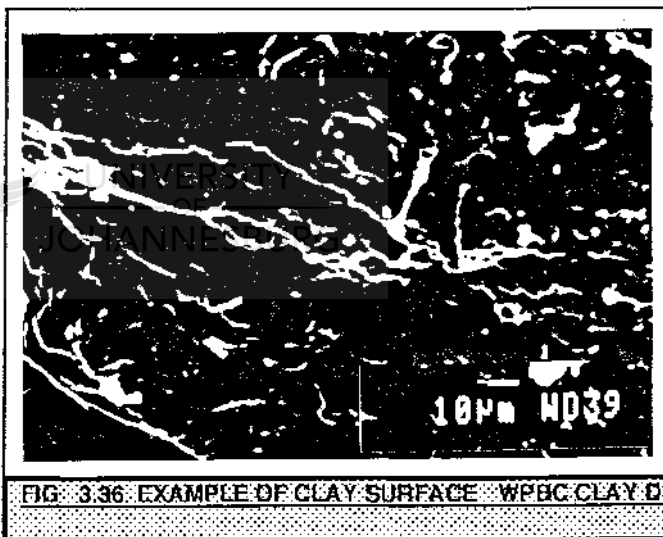
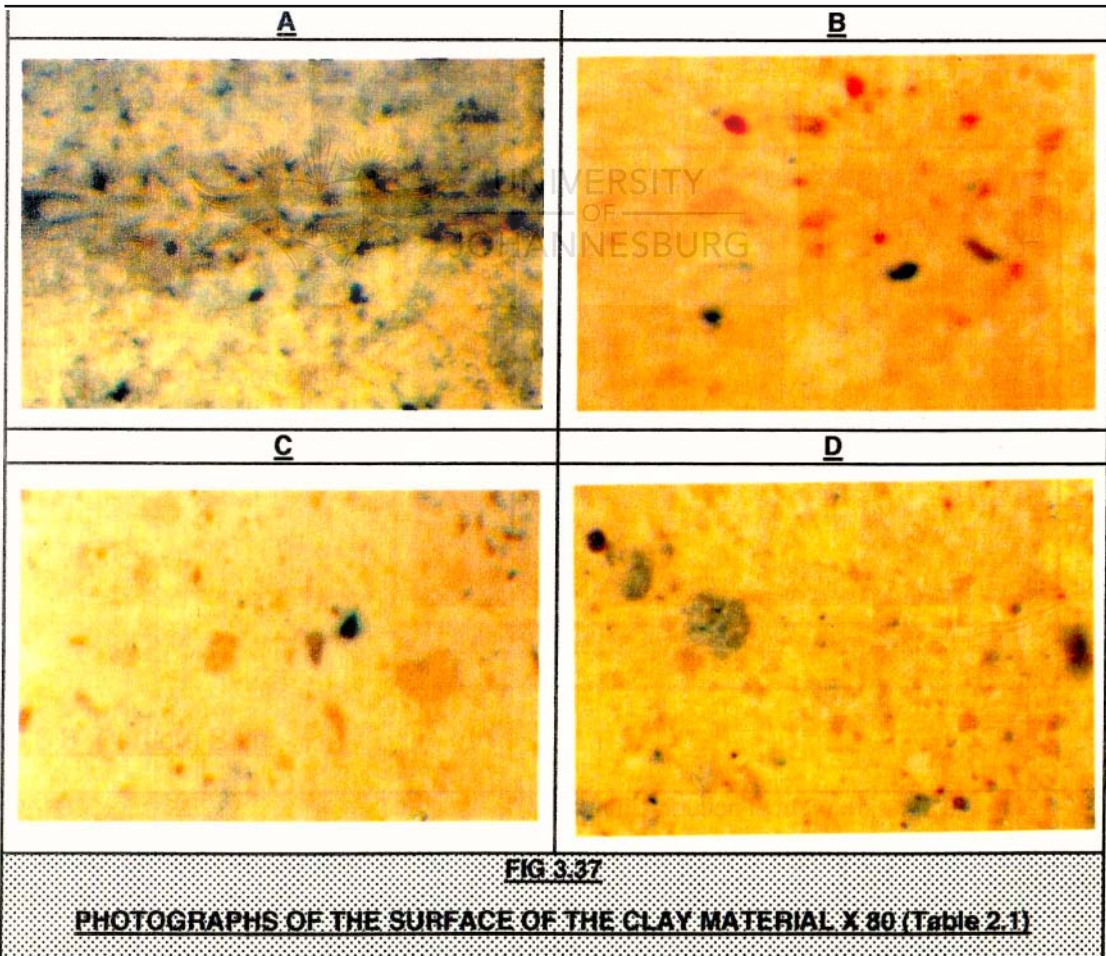


FIG. 3.36. EXAMPLE OF CLAY SURFACE WPBC CLAY D

TABLE 3.22 RATIONAL ANALYSIS		
WPBC A (1&2)		
FELDSPAR CONVENTION		
	1	2
Material	Weight Percentage	
Feldspar	7.28	7.04
Clay substance	77.99	76.94
Free Silica	9.82	10.79
MICA CONVENTION		
Potash mica	9.74	9.57
Soda Mica	0.99	0.74
Clay substance	70.90	70.13
Free Silica	12.80	13.69
100 WATER IN CLAY: %ORGANIC MATTER		
Loss H ₂ O in Clay	10.92	10.77
Loss: CO ₂ etc.	0.98	1.13

The data in Table 3.22 is the result of the Rational Analysis calculation (Table 2.4)



3.6.3 Clay Properties

3.6.3.1 Water Absorption and Linear Shrinkage

WPBC



The results of the linear shrinkage and absorption tests (2.4.2) are shown in this chart.

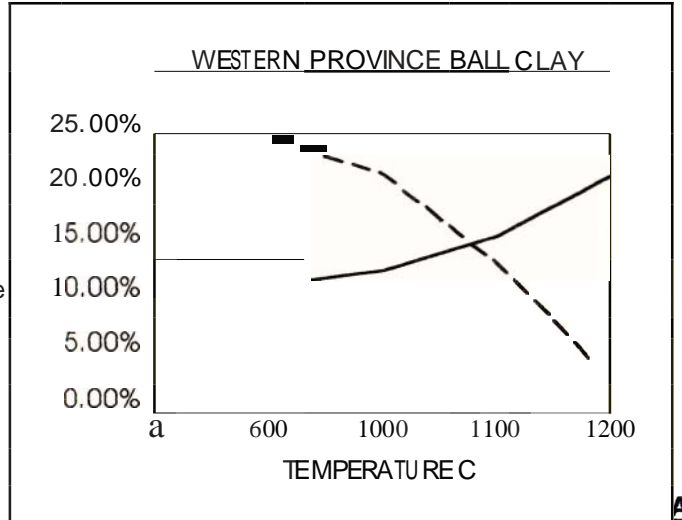


FIG 3.38 ABSORPTION & SHRINKAGE

3.6.3.2 Colour

WPBC

Photograph of WPBC fired to the selected temperatures. The change in colour can be clearly seen.

The typical gray of high carbon ball clays is evident in A. The body darkens when fired above 1100°C

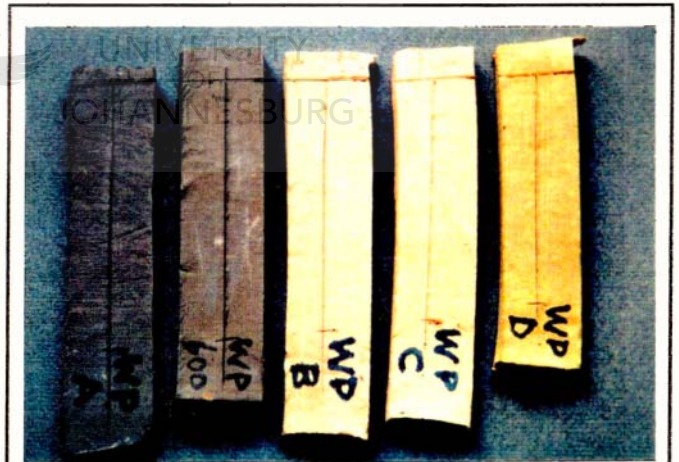


FIG 3.39 COLOUR OF THE CLAY SURFACE WPBC

3.6.3.3 Particle Size

PARTICLE SIZE	The peak of the size distribution is at 20µm and 7.9% of the particles are less than 2µm in size (Appendix C)
----------------------	---

3.6.4 Summary and Preliminary evaluation.

Western Province Ball Clay is supplied by G & W Base Minerals. It is plastic **when** blended in a clay body and with A-clay proved to be the most plastic of the chosen clays. (Table 3.32)

Two samples of this clay were analysed as a new order was brought into the studio. The two orders proved to be very similar in composition. (Table3.20)

The combined Fe + Ti content of this clay is fairly high - 3.38% (Table 4.1a) -but it could be used as a constituent of a clay body in which the other materials are pale in colour.

The Potash content was 38% higher in the EDAX analysis than in the suppliers analysis. (Appendix B)

WPBC is low in fluxes.- 2.06% As a result of this the water absorption is high e.g.. 25% at 600⁰ C (Fig.3.38). The material is high in clay substance 76.94% as can be seen in the Rational analysis (Table 3.2.2)(Table 4.3)



KAOLIN ✓

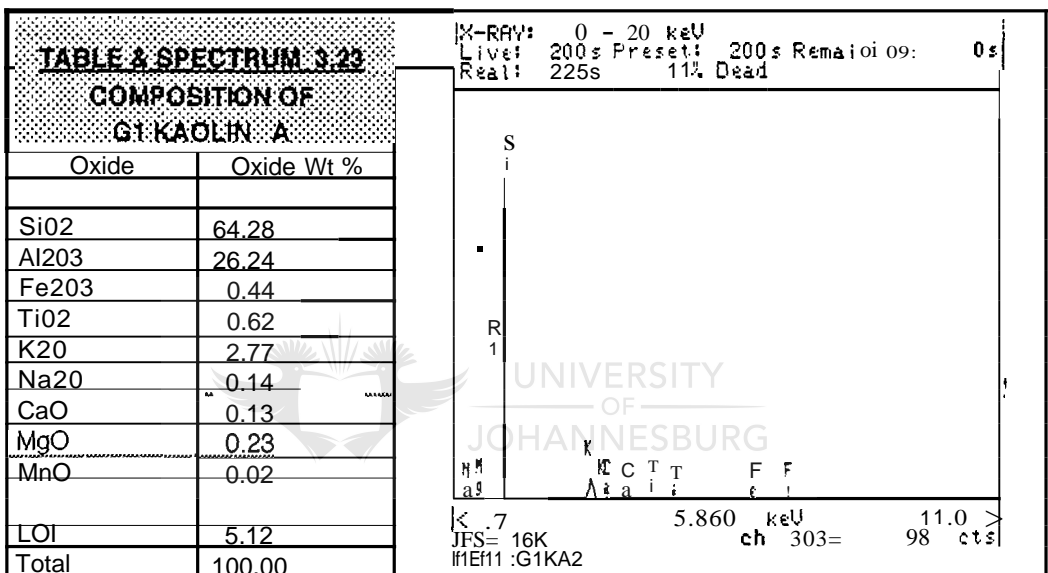
3.7 G1 KAOLIN

3..7.1 *Origin and Mineralogy*

The deposit is on the farm Zyferfontein in the Grahamstown district. The material consists mainly of kaolinite and illite.^{f10]}

3.7.2 *Clay Analysis*

The Ultimate and Rational analyses were carried out using the data collected on the SEM IEDAX (2.5.1) (Appendix D) the results of the Ultimate analysis of G1 Kaolin-A can be found in (Table 3.23) and 0 in (Table 3.24). The results of the Rational analysis of G1 Kaolin-A can be found in (Table 3.25).

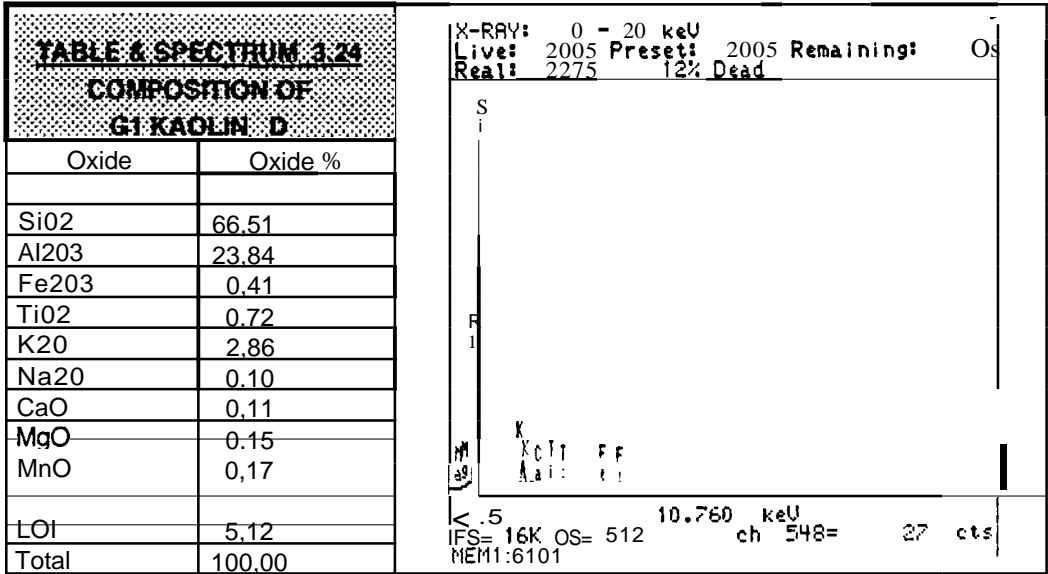
G1 KAOLIN A

Magnification X 2000

Stacked platelets can be seen.



FIG. 3.20. EXAMPLE OF CLAY SURFACE: G1 KAOLIN A



G1 KAOLIN 0

Magnification X 2000

The pinheads of fluxed clay material can be seen, The analysis shows that there is no difference in composition in inclusions.

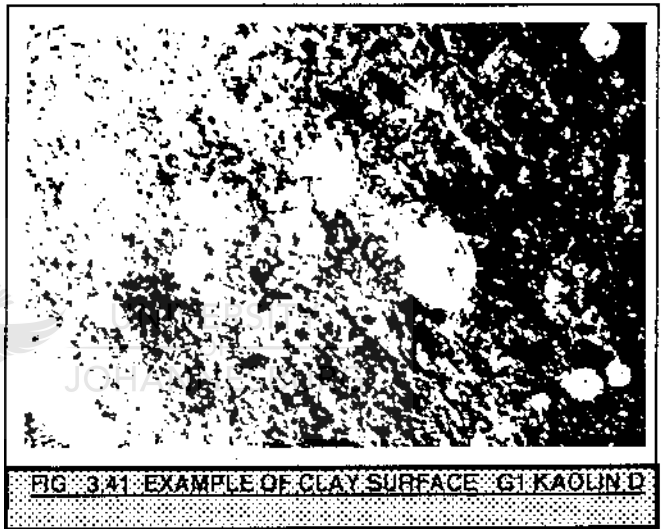


TABLE 3.25 RATIONAL ANALYSIS	
G1 KAOLIN A	
FELDSPAR CONVENTION	
Material	Weight Percentage
Feldspar	17.23
Clay substance	58.41
Free Silica	26.09
MICA CONVENTION	
Potash mica	23.46
Soda Mica	1.72
Clay substance	41.85
Free Silica	33.40
% WATER IN CLAY:	
% ORGANIC MATTER	
Loss H ₂ O in Clay	8.18
Loss: CO ₂ etc.	0

The data in Table 3.25 is the result of the Rational Analysis calculation (Table 2.4)

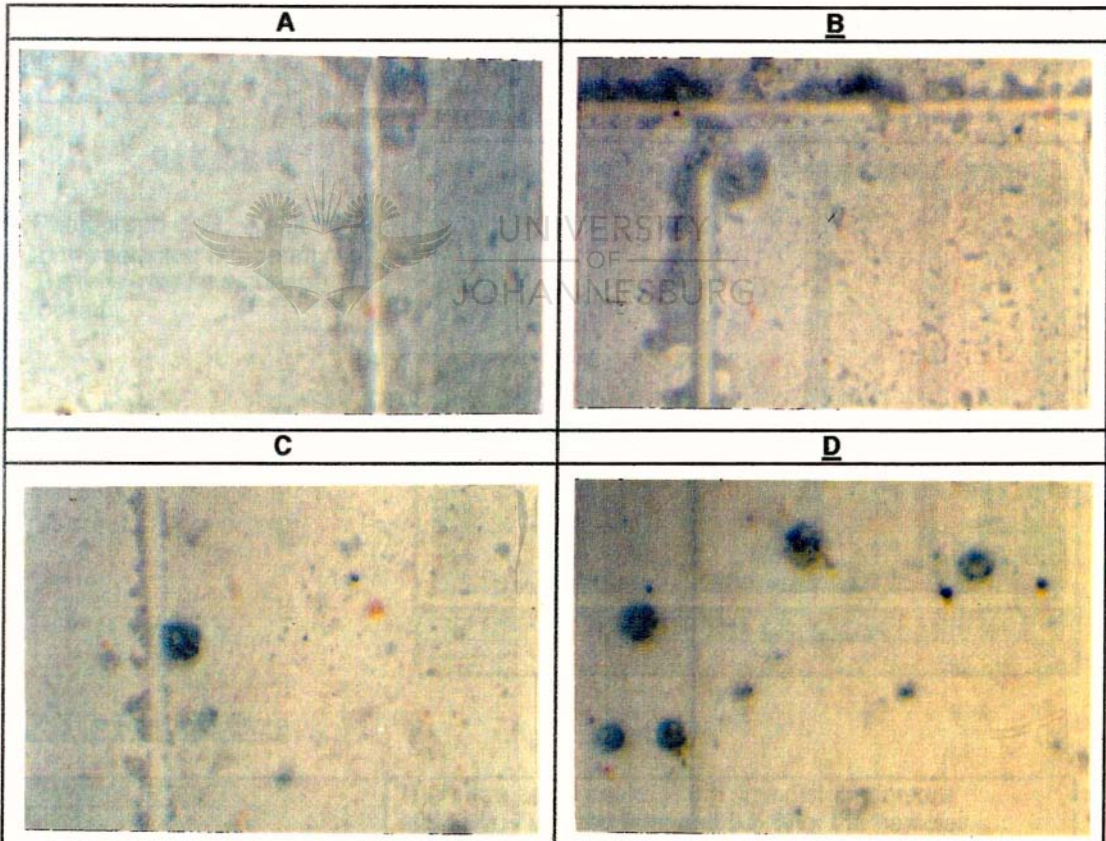


FIG 3.42

PHOTOGRAPHS OF THE SURFACE OF THE CLAY MATERIAL X 80 (Table 2.1)

3.7.3 Clay Properties

3.7.3.1 Water Absorption and Linear Shrinkage

G1 KAOLIN



The results of the linear shrinkage and absorption tests (2.4.2) are shown in this chart.

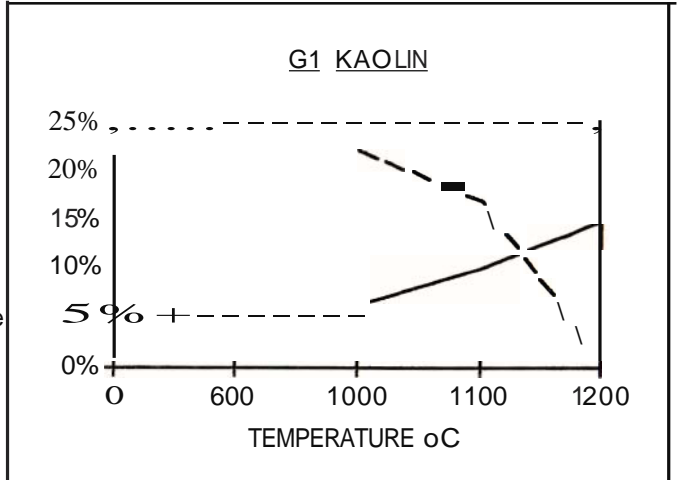


FIG 3.43 ABSORPTION & SHRINKAGE G1 Kaolin

3.7.3.2 Colour

G1 KAOLIN

Photograph of G1 KAOLIN fired to the selected temperatures. There is very little change in colour.

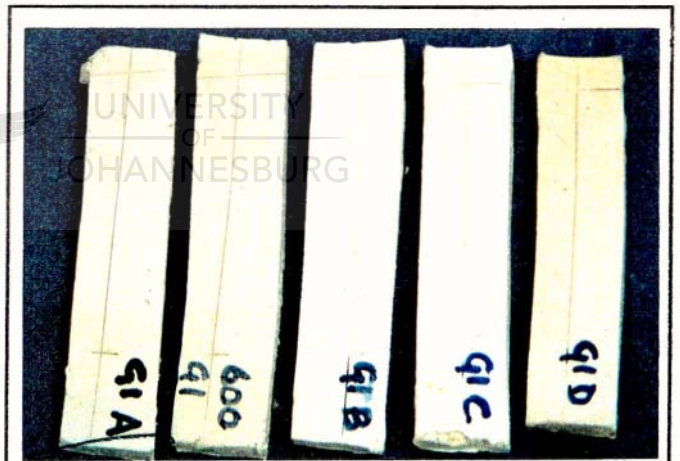


FIG 3.44 COLOUR OF THE G1 KAOLIN SURFACE

3.7.3.2 Particle Size

PARTICLE SIZE	The three equal peaks in the size distribution are at 3.5µm, 7µm and 9µm and 9.5 % of the particles are less than 2 µm in size.(Appendix C)
----------------------	---

3.7.4 Summary and Preliminary evaluation.

G1 Kaolin is a widely used clay material both for clay bodies and for glazes. The clay is supplied by G & W Base Minerals

The proportion of flux - 3.39%- is high for a kaolin causing the material to flux and vitrify at 1200°C. (FIG3.43)

The clay substance" in G1 Kaolin is low 58.41% for a kaolin and the Feldspar content high 17.23% as is the free silica content 26.09% (Table4.3) which should be taken into account when blending a clay body using this material as this combination may cause dunting of the wares due to an excess of free silica in the body.

The Fe + Ti content is well below the 2% limit for whitewares.



KAOLIN

3.8 SERINA KAOLIN

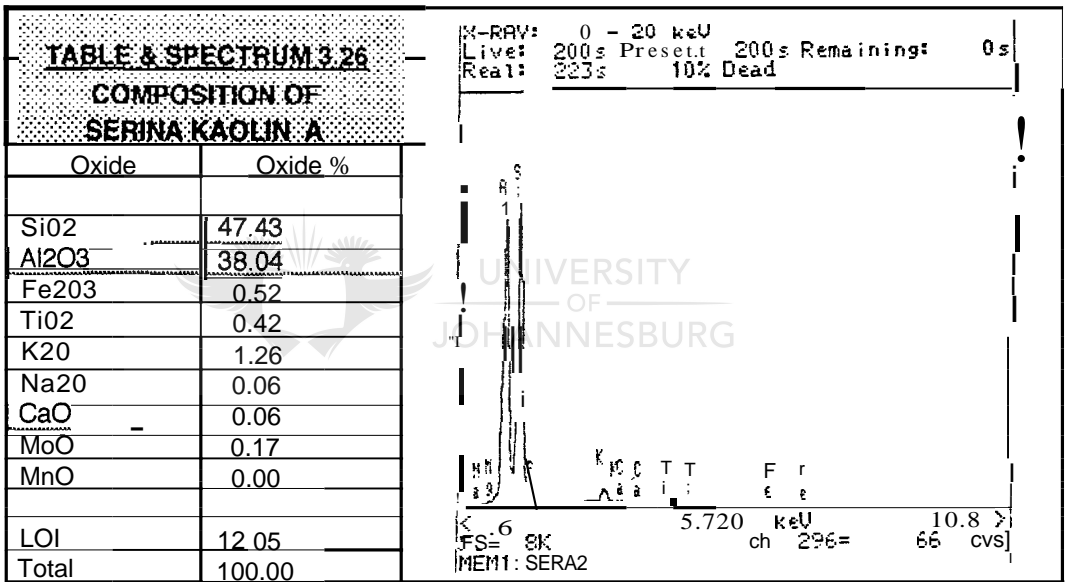
3.8.1 Origin and Mineralogy

Serina Kaolin is mined at Brakkloof in the Kommetjie-Fischoek valley on the Cape Peninsula.

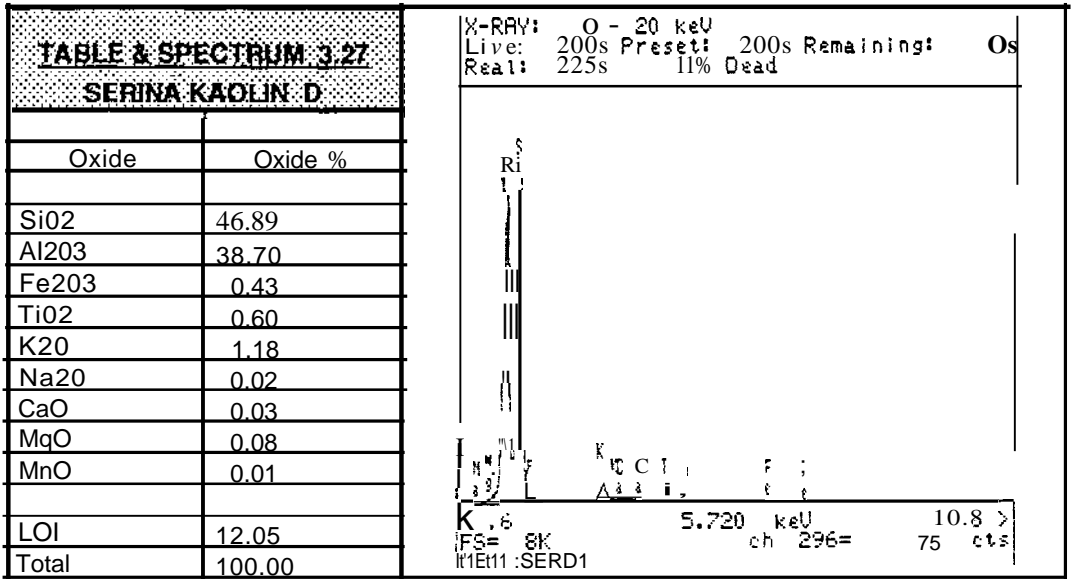
The Cape kaolins are formed *in situ* by weathering and hydrothermal action. The residual material consists mainly of kaolinite, quartz and mica with occasional inclusions of halloysite, and smectite-illite[2]

3.8.2 Clay Analysis

The Ultimate and Rational analyses were carried out using the data from the SEMEDAX (2.5.1) (Appendix D). The results of the Ultimate analysis of Serina Kaolin-A can be found in (Table 3.26) and 0 in (Table 3.7). The results of the Rational analysis of Serina Kaolin-A can be found in (Table 3.28).



NOTE: There is no micrograph of Serina Kaolin A (Fig 3.45) as the surface of the clay became "charged up", by the electron beam, in spite of the precautions taken, making it impossible to focus on the surface of the sample.(2.3.1)



SERINA 0

Magnification X 2000

There is no sintering of the surface. The material is truly refractory

Platelets are evident in the clay structure.

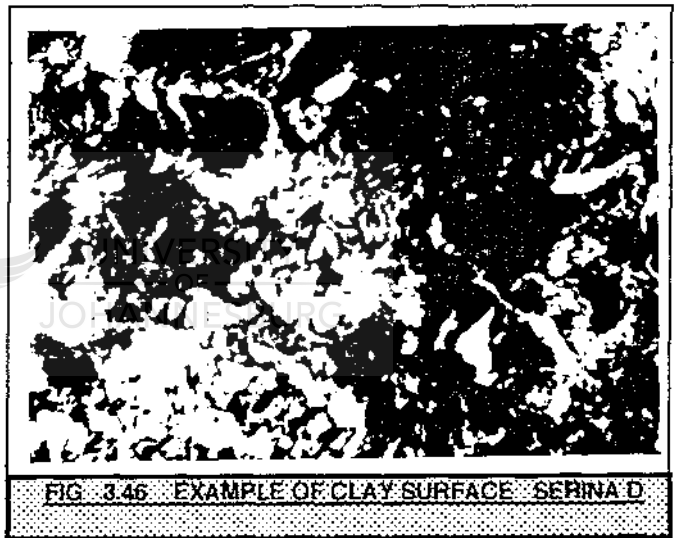


FIG 3.46 EXAMPLE OF CLAY SURFACE SERINA D

TABLE 3.28 RATIONAL ANALYSIS	
SERINA KAOLIN A	
FELDSPAR CONVENTION	
Material	Weight Percentaae
Feldspar	7.81
Clay substance	92.63
Free Silica	-0.51
MICA CONVENTION	
Potash mica	10.67
Soda Mica	0.74
Clay substance	85.12
Free Silica	2.67
% WATER IN CLAY :	
%ORGANIC MATTER	
Loss :H ₂ O in Clay	12.97
Loss: CO ₂ etc.	0

The data in Table 3.28 is the result of the Rational Analysis calculation (Table 2.4)

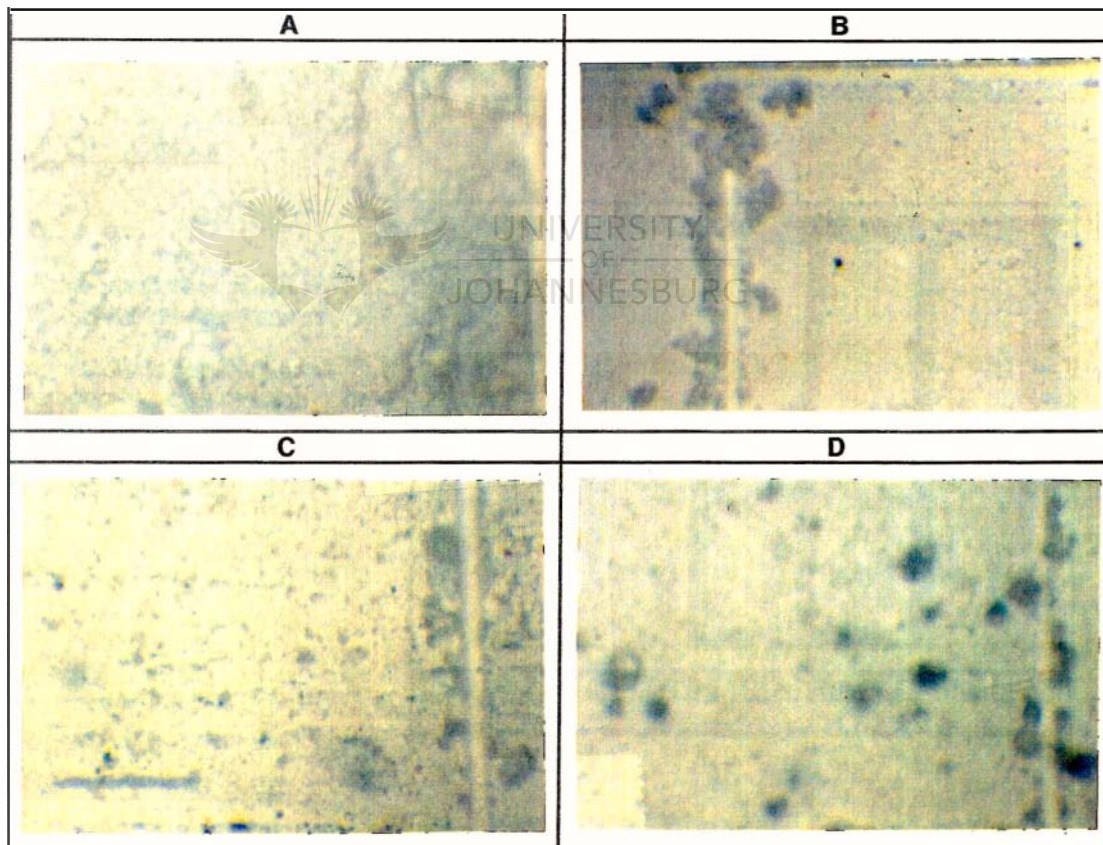
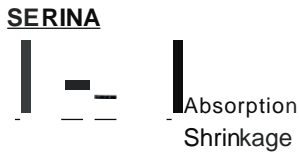


FIG 3.47

PHOTOGRAPHS OF THE SURFACE OF THE CLAY MATERIAL X 80 (Table 2.1)

3.8.3 Clay Properties

3.8.3.1 Water Absorption and Linear Shrinkage



The results of the linear shrinkage and absorption tests (2.4.2) are shown in this chart.

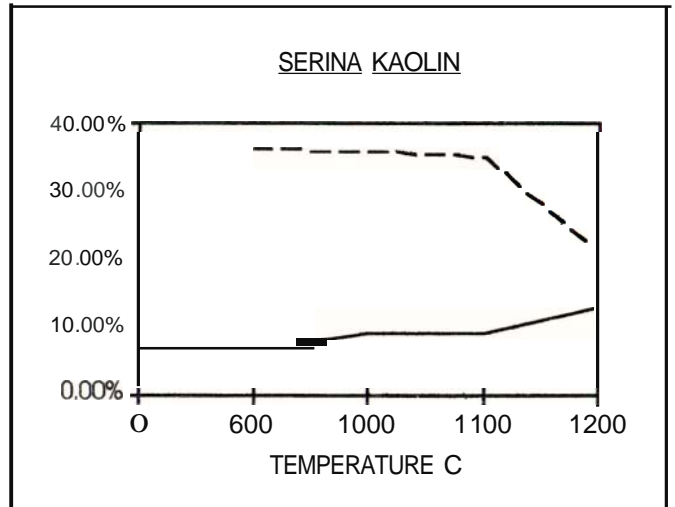


FIG 3.48 ABSORPTION & SHRINKAGE

3.8.3.2 Colour

SERINA

Photograph of SERINA fired to the selected temperatures.

the colour is constant at all temperatures as the Iron content is virtually nil.



FIG 3.49 COLOUR OF THE CLAY SURFACE SERINA

3.8.3.3 Particle Size

2 microns is the upper grain -size limit for materials to be classified as clay[2] 2.4.2.3

PARTICLE SIZE	The peak in the size distribution is at 7µm and 7% of the particles are less than 2 µm in size. (Appendix C)
----------------------	--

3.8.4 Summary and Preliminary evaluation

Serina kaolin is mined and supplied by Serina (Pty) Ltd.

The kaolin is pure and refractory and easily beneficiated as the impurities are large enough to sieve out. The clay content is 92.63%. (Table 4.3) Serina Kaolin falls the closest of the clays tested to the theoretical composition of kaolinite:-

SiO₂ . 46.54 Al₂O₃ 39.50 H₂O . 13.96

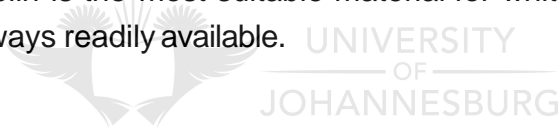
Composition of Serina Kaolin:-

SiO₂ . 47.43 Al₂O₃ . 38.04 LOI . 12.05

The shrinkage of Serina is low after the water of plasticity is removed (FIG.3.48)

The absorption curve does not approach the 0 line as the material is exceedingly refractory and retains absorbency. The peak at the largest value in the particle size valuation is below 10µm.

Serina kaolin is the most suitable material for whitewares and porcelain but is not always readily available.



KAOLIN

3.9 S. KAOLIN

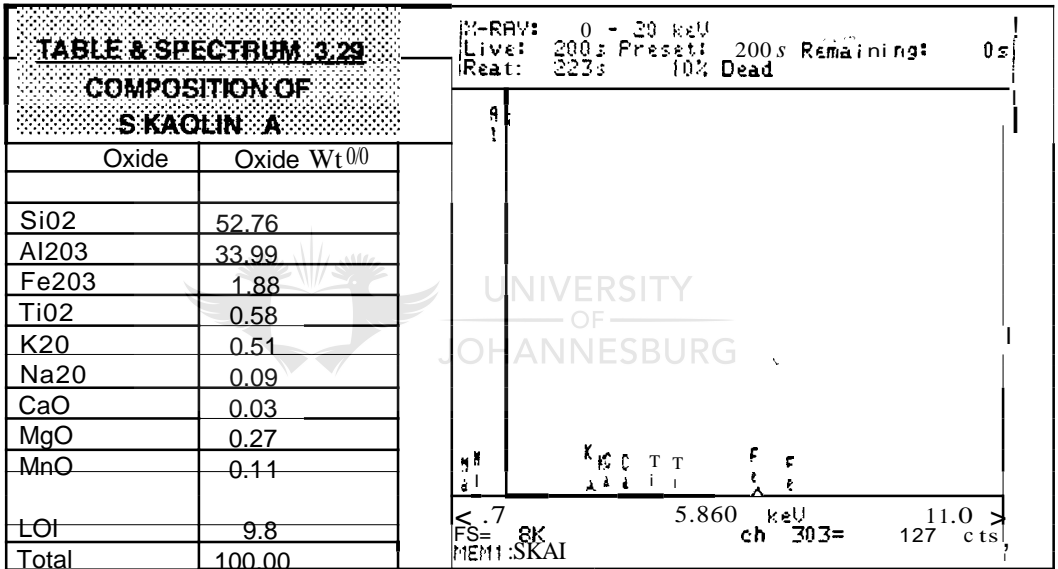
3.9.1 Origin and Mineralogy

The deposit of S.Kaolin is in the Mossel Bay district on the farm Rondeheuwel.

The material consists mainly of kaolinite with some quartz and mtca.PI

3.9.2. Clay Analysis

The Ultimate and Rational analyses were carried out using the data collected on the SEM IEDAX (2.5.1)(Appendix D). The results of the Ultimate analysis of S-Kaolin-A can be found in (Table3.29) and D in (Table3.30). the results of the Rational analysis of S-Kaolin Acan be found in (Table 3.31



SKAOLIN

Magnification X 2000

The individual hexagonal flat platelets can be seen.

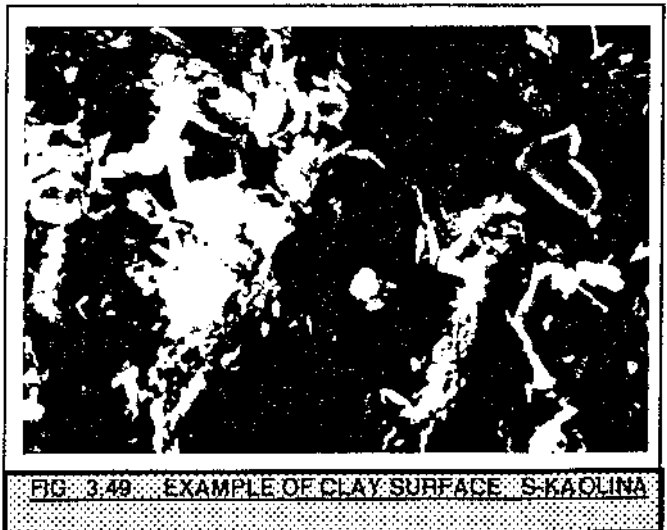
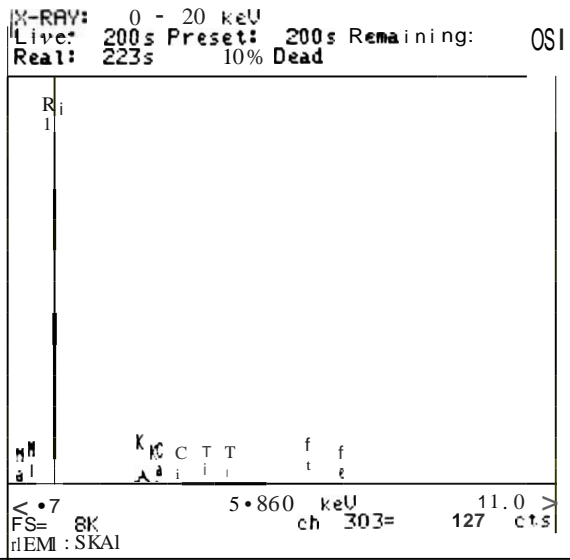


TABLE & SPECTRUM 3.30
COMPOSITION OF S-KAOLIN D

Oxide	Oxide Wt %
SiO ₂	50.81
Al ₂ O ₃	36.27
Fe ₂ O ₃	1.42
TiO ₂	0.60
K ₂ O	0.64
Na ₂ O	0.06
CaO	0.06
MgO	0.35
MnO	0.00
LOI	9.8
Total	100.00



S KAOLIN D

Magnification X 2000

The individual hexagonal flat platelets can be seen. The separate particles that appear on the surface do not differ in composition from the main body of material.

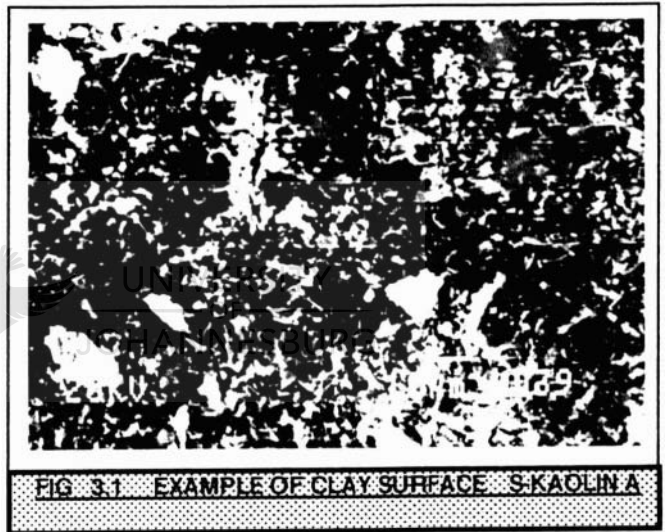


TABLE 3.31 RATIONAL ANALYSIS	
S KAOLIN A	
FELDSPAR CONVENTION	
Material	Weight Percentage
Feldspar	3.55
Clay substance	84.35
Free Silica	11.41
MICA CONVENTION	
Potash mica	5.42
Soda Mica	0.74
Clay substance	79.65
Free Silica	10.98
% WATER IN CLAY: %ORGANIC MATTER	
Loss: H ₂ O in Clay	11.81
Loss: CO ₂ etc.	0

The data in Table 3.3 t is the result of the Rational Analysis calculation (Table 2.4)

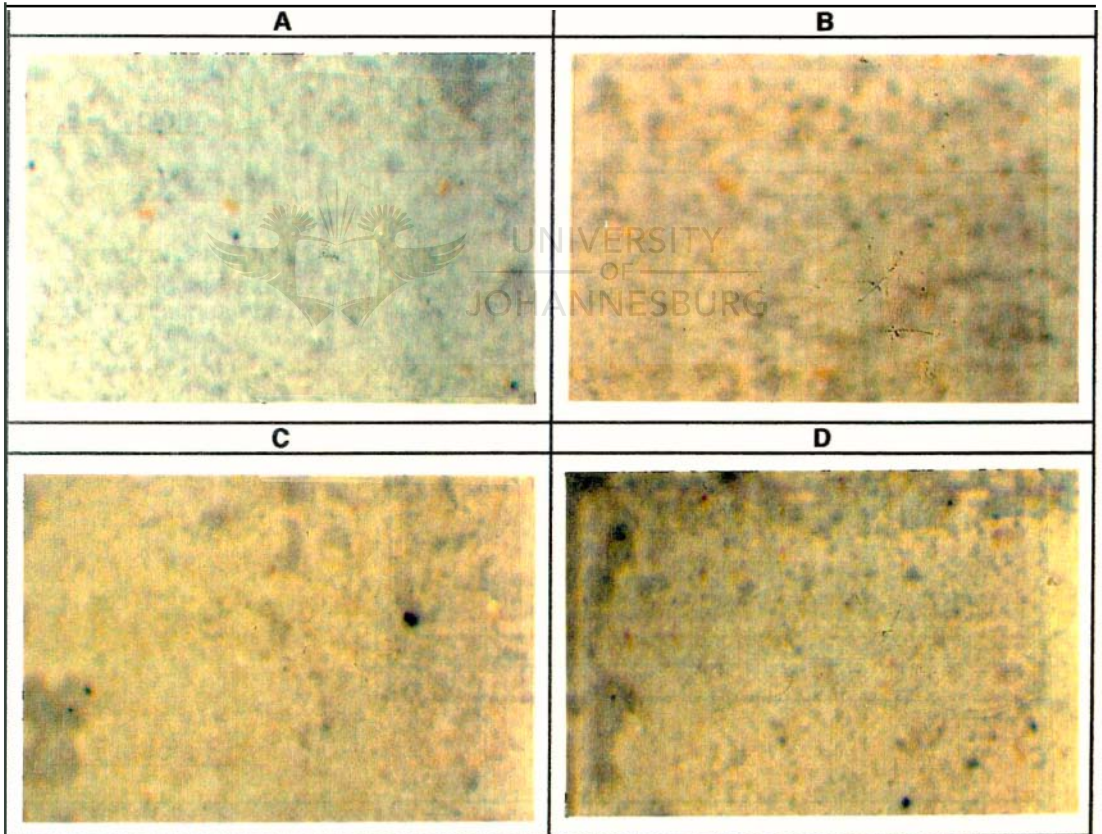


FIG 3.51
PHOTOGRAPHS OF THE SURFACE OF THE CLAY MATERIAL X 80 (Table 2.1)

3.9.3 Clay Properties

3.9.3.1 Water Absorption and Linear Shrinkage

S.KAOLIN



The results of the linear shrinkage and absorption tests (2.4.2) are shown in this chart. There is no (A) value for the absorption test

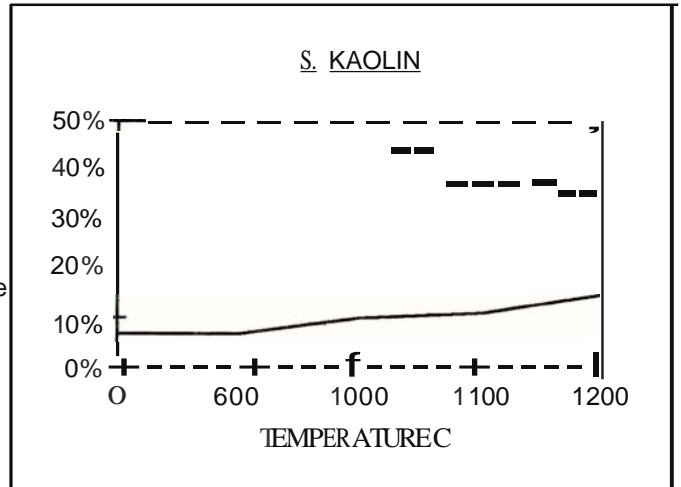


FIG 3.52 ABSORPTION & SHRINKAGE

3.9.3.2 Colour

SKAOLIN

Photograph of S KAOLIN fired to the selected temperatures. The change in colour can be clearly seen.

The colour at 1100° C (C) is the palest.



FIG 3.53 EXAMPLE OF CLAY SURFACE S-KAOLIN

3.9.3.3 Particle Size

PARTICLE SIZE

The peak in the size distribution is at 11.5µm and 1.7% of the particles are less than 2µm in size. (Appendix C)

3.9.4 Summary and Preliminary evaluation.

S Kaolin is, a refractory material that begins to flux at 1000°C but is far from vitrification at 1200°C . Craters appear in the surface as the material begins to flux.(Fig 3.51)

S Kaolin is a white material with very little plasticity when blended into a clay body (Table 3.37) The peak at the largest value in the particle size valuation is at $20\mu\text{m}$ indicating that the particles are generally of a larger diameter than the other clay materials.

S Kaolin is closer to a pure kaolin than G1 Kaolin but not as pure as Serina kaolin.

S Kaolin is suitable as the kaolin component in a clay body but is no longer obtainable.



3.10.1 Clay body Analysis.

3.10.1.1 Plasticity.

As a final comparative technique the nine clay materials chosen were combined with feldspar and silica in a known proportion and formed into clay bodies (2.3.3). The reason for this final comparison is that clay is seldom used in its found state but rather blended to form a required body for use in the studio (1.1). As stated in the introduction to this Chapter, the Ultimate analysis and the Rational analysis of the Clay bodies appear in Chapter 4

(Table 3.32) is compiled from the information obtained from three potters, each represented by a symbol (x, 0, 0) in the table. The clay bodies were prepared as described (2.3.3) and tested (2.4.2.2.) Each potter was given 500gms. of each of the prepared clay bodies which were thrown on the wheel and assessed for plasticity and workability. This is qualitative information as there is no definitive method of measuring plasticity but the information is never-the-less valuable as the experience of the potters chosen is considerable and the information can be comparatively applied.

The two clays identified by all three potters as being particularly plastic and easy to throw were A-clay and Western Province ball clay.

Moss clay was placed on the chart as being between *Good* and *Excellent*.

813 and PXX were similarly placed above *OK* but not outstanding.

C-clay was low on the scale as a plastic throwing clay possibly due to the low Alumina content in the clay material. (Table 4.2)

The three kaolins were understandably low in plasticity as the larger particles found in kaolins lower the plasticity and the green strength of a clay body. [4]

TABLE 3.32 RESULTS OF THE THROWING TEST FOR PLASTICITY							
CLAY	CYL HGT	1 BAD	2 OK	3 GOOD	4 VGOOD	5 EXCEL	COMMENTS
1 A CLAY	10.0 14.0 13.4				X 0 0		Wet. Good tooth Moisture too high Firm, Did not absorb water.
2 B13	9.75 10.5 13.5		0 0		X		Good tooth. Smooth Sticky to wedge Slimy to throw Rubbery; pleasant colour; no form.
3 C CLAY	9.25 11.40 11.4	0		X 0			Spongy and dilated. Slimy, flabby. too wet. Stiff and floppy.
4 PXX	9.75 15.50 13.0		0		X	0	Firm. good tooth Very good. Hard and dry.
5 MOSS	9.00 13.3 13.3			0	0	X	Firm and Strong. High water absorption; dry Smooth; floppy; Slimy. Hard when stretched then flops.
6 WPBC	9.00 16.80 14.6				X 0 0		Dense. Similar to 613 Sticky -too wet Slim and smooth. Easy to throw.
7 G1 KAOLIN	9.75 9.50 11.0	0	X 0				Wet / Dry cheesy Wet and short. Stiff and noooov Thirstv.
8 S KAOLIN	8.75 9.50 9.30	0 0	X				Less cheesy but no tooth Very short; sticky No binder; would not throw. (V bad)
9 SERINA	9.25 12.00 10.7	0 0	X				Less cheesy No tooth Short, sticky. Creamy; better than 7

CHAPTER 4

CORRELATION OF INFORMATION AND DISCUSSION.

The tables presented in this chapter include correlations of the results in Chapter 3 as well as additional tables prepared to assist in the comparison of the nine chosen clay materials and the "clay bodies" and thereby to identify the similarities and differences.

4.1 ULTIMATE ANALYSIS

The information in Tables 4.1 and 4.2 is compared in Tables 4.1 a and 4.2a in order to simplify the choice of clay to be used in a clay body. The tables show the Ultimate Analyses of the clay materials and the clay bodies. The proportion of the materials blended in a clay body can be adjusted using the INSIGHT software programme (2.6), and the Data Base.

1) The silica and alumina ratings show the clays in order according to the quantities of silica and alumina present in the bodies.

The amount of silica is an indirect indication of the behavior of the final clay body. Part of the SiO_2 becomes available as amorphous SiO_2 when clay breaks down, while SiO_2 as quartz is more refractory because of the larger particle size. In earthenware clay it can be considered a filler.

Al_2O_3 forms mullite and takes part in the glassy phase of the clay vitrification process. The quantity of alumina can be used as an indication of the clay fraction in the Rational Analysis.

2) The $\text{Fe}+\text{Ti}$ gives the total of these two materials which must be less than 2% when combined in a white clay body, Although the titanium is itself almost white, it enhances the staining power of the iron causing the clay body to be off-white. With the addition of silica and feldspar, or any other filler, to a clay body the proportion of the $\text{Fe} + \text{Ti}$ is reduced. The result of this can be seen when comparing Table 4.2 (Clay material) with table 4.3 (Clay body).

3) The value of total fluxes is important to determine the vitrification and the thermal expansion of clay bodies. The thermal expansion of the clay materials is **theoretically** calculated by means of the Data Base.(Table 2.6)

4) The total of the secondary fluxes or alkali earth oxides gives information on the type of flux present in the clay. These fluxes are important for throwing clays as they can affect plasticity by altering the structure of the pore water layer[6]. The Ca reacts with the silica forming a glass at a relatively low temperature and thereby lowering the fluxing point of the clay body.

TABLE 4.1 TABLE OF THE ULTIMATE ANALYSIS OF BALL CLAYS AND KAOLINS

Oxide	A Clay	B13 Oay	C Clay	Moss Clay	PXX Ball cl	W.P.B.C lay	G1 Kaolin	Serena	S Kaolin
SiO ₂	46.02	61.29	63.90	61.67	53.29	50.64	64.28	47.43	52.76
Al ₂ O ₃	34.07	24.19	23.35	25.30	32.62	32.16	26.24	38.04	33.99
Fe ₂ O ₃	3.53	2.38	0.98	1.49	1.04	1.73	0.44	0.52	1.88
TiO ₂	2.18	1.12	1.08	1.28	0.97	1.58	0.62	0.42	0.58
K ₂ O	1.37	2.59	3.44	4.06	2.65	1.15	2.77	1.26	0.51
Na ₂ O	0.20	0.11	0.24	0.23	0.15	0.08	0.14	0.06	0.09
CaO	0.91	0.81	0.47	0.03	0.22	0.19	0.13	0.06	0.03
MgO	0.50	0.62	0.39	0.23	0.43	0.58	0.23	0.17	0.27
MnO	0.07	0.08	0.04	0.02	0.03	0.00	0.02	0.00	0.11
Sulphur	0.55								
LOI	10.6	6.8	6.1	5.7	8.60	11.90	5.12	12.05	9.8
TOTAL	100.0	100.00	100.00	100.00	100.01	100.00	100.00	100.00	100.00

TABLE 4.1a

Silica Rating	6	3	1	2	4	5	1	3	2
Al. Rating	1	5	6	4	2	3	3	1	2
Fe+Ti	5.71	3.5	2.04	2.77	2.01	3.31	1.06	.94	2.46
Total Fluxes	3.0	4.21	4.58	4.57	3.45	2.00	3.29	1.55	1.01
Ca+Mg+Mn	1.41	1.5	.9	.28	.68	.77	.43	.23	.41

TABLE 4.2 TABLE OF THE ULTIMATE ANALYSIS OF CLAY BODIES									
Oxide	A Clay	B13 Oay	C Clay	Moss Oay	PXX Ball cl	W.P.B.C lav	G1 Kaolin	Serena	S Kaolin
SiO ₂	74.06	75.73	76.63	75.48	71.74	72.08	76.60	70.46	72.07
Al ₂ O ₃	19.69	17.02	18.07	17.49	21.72	21.70	17.93	24.86	22.33
Fe ₂ O ₃	1.55	1.28	.39	.81	.15	.97	.27	.33	1.04
TiO ₂	.80	.60	1.05	.68	.79	.86	.34	.24	.32
K ₂ O	3.33	4.40	3.26	5.13	4.69	3.75	4.45	3.81	3.97
Na ₂ O	.17	.20	.31	.26	.76	.19	.21	.18	.05
CaO	.24	.41	.17	.02	.10	.10	.07	.03	.02
MgO	.16	.32	.11	.12	.05	.31	.12	.09	.14
MnO	0	00	00	.01	00	.05	.01	00	.06
TOTAL	100.00	100.00	100	100.00	100.00	100.00	100.00	100.00	100.00

TABLE 4.2a COMPARATIVE INFORMATION									
Silica Ratio	4	2	1	3	6	5	1	3	2
Al. Ratio	3	6	4	5	1	2	3	1	2
Fe+Ti	2.53	1.77	1.44	1.49	.94	1.55	.61	.57	1.36
Total Fluxes	3.9	5.33	3.85	5.53	5.61	4.35	4.86	4.11	4.24
Ca+Mg+Mn	0.4	0.73	0.28	0.14	0.15	0.16	0.2	0.12	0.16

4.2 RATIONAL ANALYSES

The Rational analysis of the ball clays and kaolins is shown in Table 4.3 and the Rational analysis of the clay bodies in Table 4.4.

The variation in the quantities of component materials can be clearly seen. The comparison of the clays illustrates the importance of knowing this information before substituting one clay material for another in order to retain the required proportions of Clay substance, Free silica and Feldspar or Mica in a clay body. Comparisons such as these are useful when deciding on the clay material to be included in a clay body. The recipe for the clay body can be calculated using the Insight programme and the calculations in the Data base. By adjusting the quantities of the various materials the proportions can be maintained.

In this project both the Feldspar and the Mica convention have been used for the assessment of the clay materials because the mineralogy of the clays had not been established directly. It could have been established by X-Ray diffraction if funds had been available. The mineralogical evaluations of the clay materials are referenced from scientific publications specialising in this technique. [2][5][15][16].

The Feldspar convention is referred to in the discussion as it is the convention most frequently used in the studio situation, but the calculations based on both conventions are installed in the data base.

Material	A Clay	B13 Clay	C Clay	MOSS Clay	PXX Clay	W.P.B. Clay.	G1 Kaolin	Serena	S Kaolin
Feldspar	8.22	15.98	21.76	25.40	16.58	7.28	17.23	7.81	3.55
Clay Subst	82.40	53.80	48.99	52.25	74.85	77.99	58.41	92.63	84.35
Free silica'	2.55	26.04	27.12	21.04	7.91	9.82	26.09	-0.5	11.41
Potash Mica	11.60	21.43	29.14	34.39	23.29	9.74	23.46	10.67	5.42
Soda Mica	2.46	1.23	2.96	2.83	2.83	0.99	1.72	0.74	0.74
Clay Subst	72.45	37.69	27.78	27.73	57.03	70.90	41.85	85.12	79.65
Free Silica	5.31	32.05	36.42	31.90	14.91	12.80	33.40	2.67	10.98
H2O in Clay	11.35	7.53	6.86	7.31	10.46	10.92	8.18	12.97	11.81
LOI	10.60	6.80	6.10	5.70	8.60	11.90	5.10	12.05	9.80

Material	A Clay	B13 Clay	C Clay	MOSS Clay	PXX Clay	W.P.B. Clay.	G1 Kaolin	Serena	S Kaolin
Feldspar	20.72	27.23	21.13	31.91	32.26	23.32	27.59	23.62	23.80
Clay subst	40.22	30.45	35.95	29.76	40.02'	44.10	32.59	51.96	45.48
Free silica	42.03	43.95	46.31	41.06	32.34	36.57	43.66	31.02	35.59
Potash Mica	28.21	37.27	27.61	43.45	39.72	31.76	37.69	32.27	33.65
Soda Mica	2.09	2.46	3.82	3.20	9.36	2.34	2.59	2.22	0.62
Clay Subst	20.29	4.36	15.03	0.00	6.88	21.67	5.69	29.30	21.55
Free Silica	50.58	55.70	55.36	54.89	46.17	46.54	55.70	41.20	46.54

4.3 SHRINKAGE AND ABSORPTION

The information shown in (Fig.4.1 and 4.2) was collated from the results of the shrinkage and absorption experiments (ChapterS) (Appendix C).The values for the individual clays materials are shown in the charts in the clay characterisation section. (Chapter3)

The clay bodies were submitted to the same test procedure as the clay materials and the results are presented in (Fig.4.3 and 4.4). The purpose of these clay body tests is to illustrate the changes that occur when materials are blended.

The linear shrinkage of the clay materials (Table 4.1) follows a shrinkage "pattern", with the wet to dry shrinkage being between 5% and 12% at 100⁰C (in fact the samples were dried to 1100C to ensure that the pore water had been driven off) and the shrinkage at 1200⁰C falling between 12.5% and 22.5%. The three kaolins show the least shrinkage and the most plastic of the clays (A-clay and WPBC) (Table 3.32) show the greatest shrinkage.

In comparison the linear shrinkage of the clay bodies (Table 4.3) shows B13 Ball clay with the highest shrinkage followed by the remainder of the ball clays. Serena and S-kaolin predictably show the least shrinkage as they have a high clay substance level.(Table 4.5). The percentage linear shrinkage of the clay bodies, ranging between 9% and 16%.at 1200⁰C ,is considerably lower than the clay materials shrinkage due to the silica and feldspar which act as fillers at this temperature. The shrinkage of the clay bodies is slightly less at the lower temperatures than that of the clay materials.

The tables of %water absorption show the wt.% water in a fired sample after boiling for 5 hours as described in Chapter 2. The porosity of ceramic materials is an .Indlcatlon of the state of flux that the body reached in the firing process. This can range from a highly porous earthenware to a totally vitrified porcelain with 0% absorption. The % water absorption is dependent on the composition of the material and the temperature of the firing.

The water absorption pattern (FIG. 4.2) of the clay materials fall into three distinct zones which are repeated in the clay body absorption charts (Fig 4.4) but with changes in the participant clays.

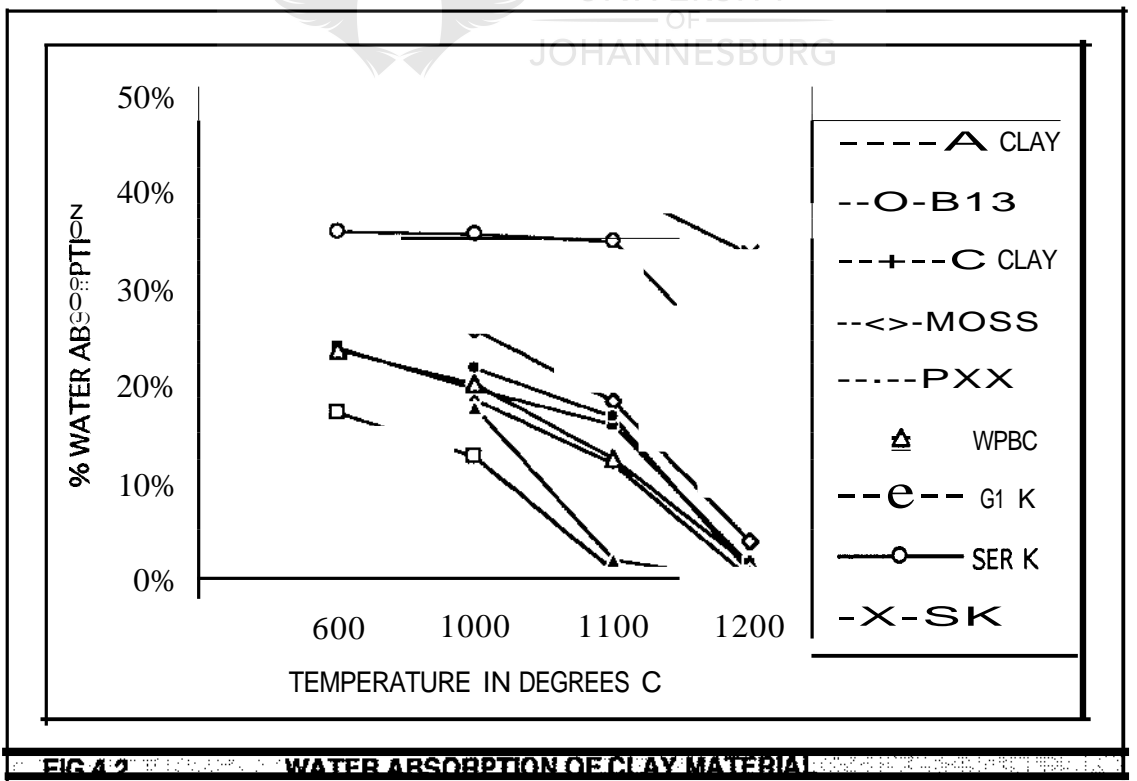
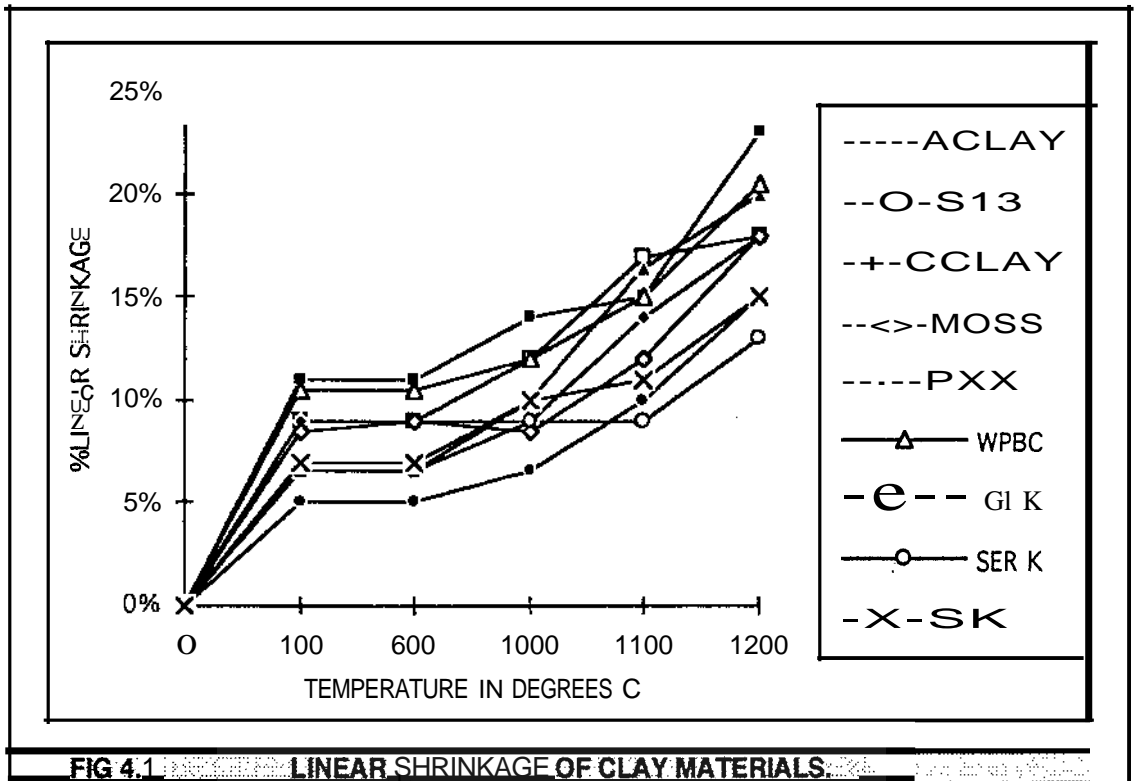
The clay material zones are:-

- 1) PXX **clay** and the 813 clay fluxing below 1000⁰ C.
- 2) the rest of the ball clays and the G1 Kaolin fluxing below 1200⁰C,
- 3) Serena and S- kaolins not approaching the fluxing point.

In comparison the clay body zones are:-

- 1) WP8C and Moss clay with 5% absorbency at 11 000C and slightly less at 1200⁰C.
- 2) the remainder of the ball clays plus G1 Kaolin ranging from 12%-17% absorption at 11 000C and between 0%-5% at 1200⁰C.
- 3) Serena and S-Kaolin not approaching the fluxing point.





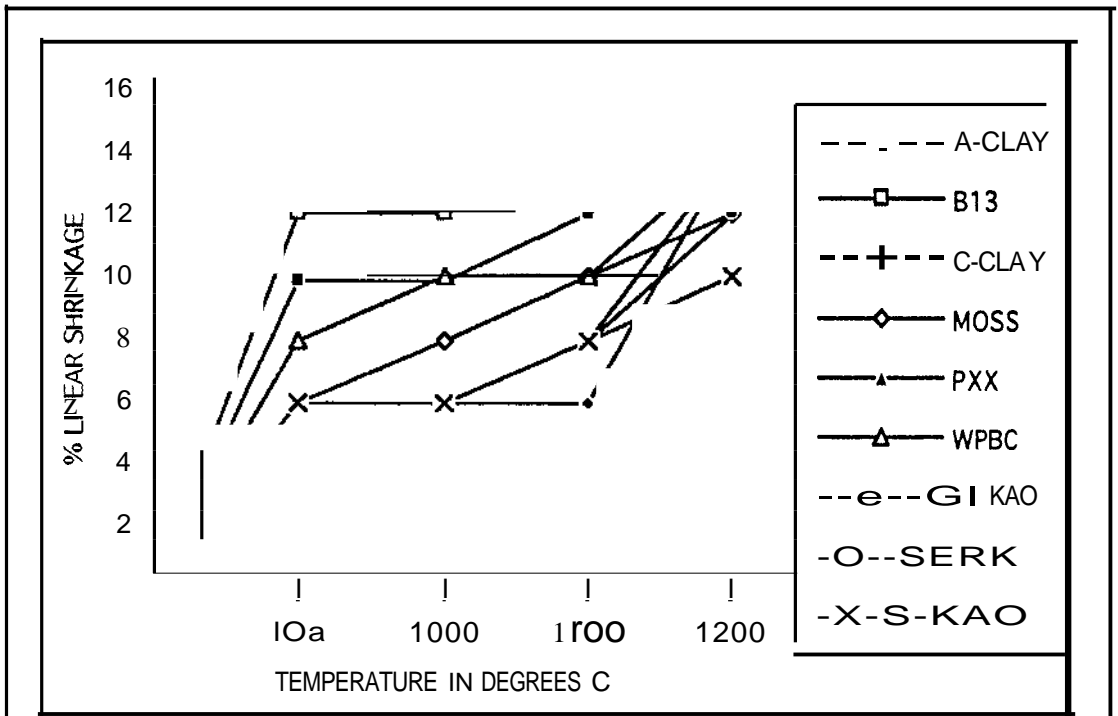


FIG. 4.3 LINEAR SHRINKAGE OF CLAY BODIES

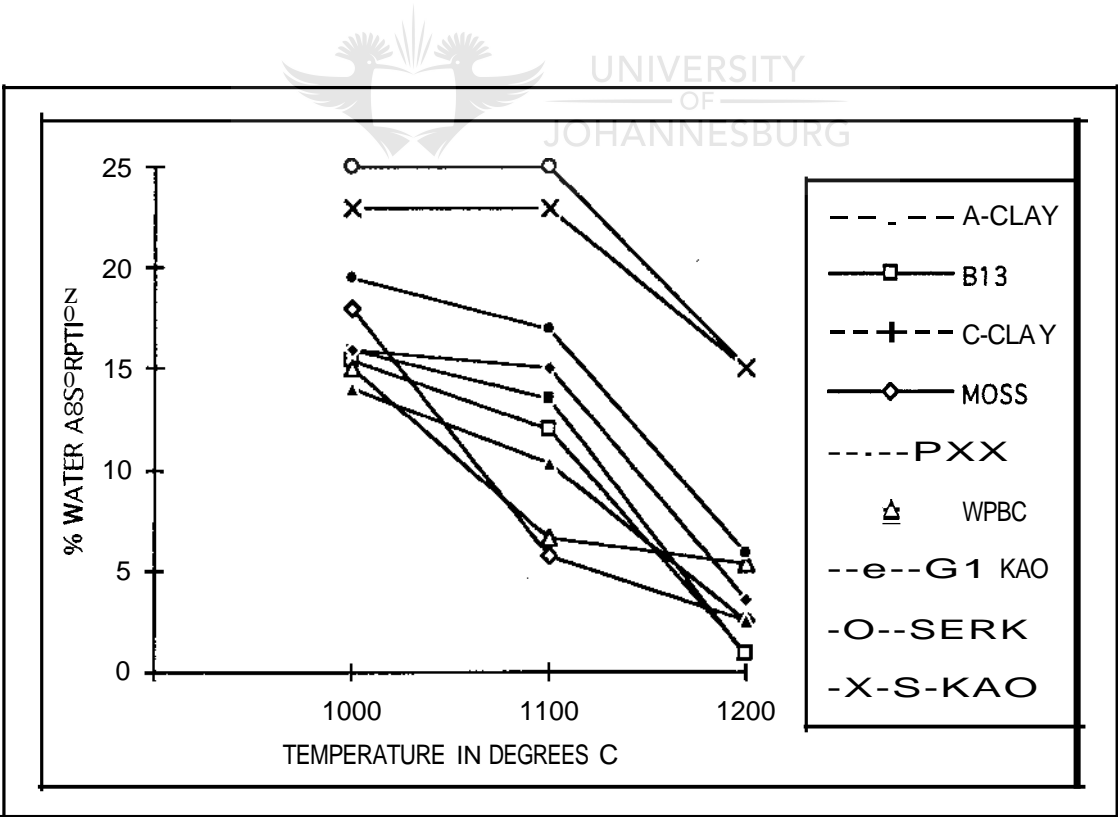


FIG. 4.4 % WATER ABSORPTION OF CLAY BODIES

4.4 PARTICLE SIZE

The particle size of the nine chosen clay materials was tested using the laser diffraction method on a Malvern "Microsizer" by courtesy of Prof. Moys, Dept. Chemical Engineering, Univ. of Witwatersrand. The data sheets and charts can be found in Appendix C.

It should be noted that particle size analysis is dependent on several parameters such as type of dispersant, method of analysis etc. and should be seen as a comparative method of assessing clay materials.

Particle size is of great importance to the plasticity of clay materials. As has been discussed in (1.2) a mix of particle sizes in a clay body gives the best plasticity as the packing density of the particles improves as does the green strength.

The following chart shows three series of data selected from the Malvern data sheets.

Fig 4.5 shows the % particles less than $2\mu m$ equivalent size diameter (e.s.d.) giving the percentage clay in the material.^[2] This is a geological size division of particles and the results should be seen as a comparative assessment of clay materials.

Fig 4.6 shows the peak of the particle size distribution chart giving the size of the particles that are present in the clay material in the highest percentage.

Fig 4.7 Shows the specific surface area in square meters of one gram of clay material. The smaller the average particles are the larger the surface area will be.

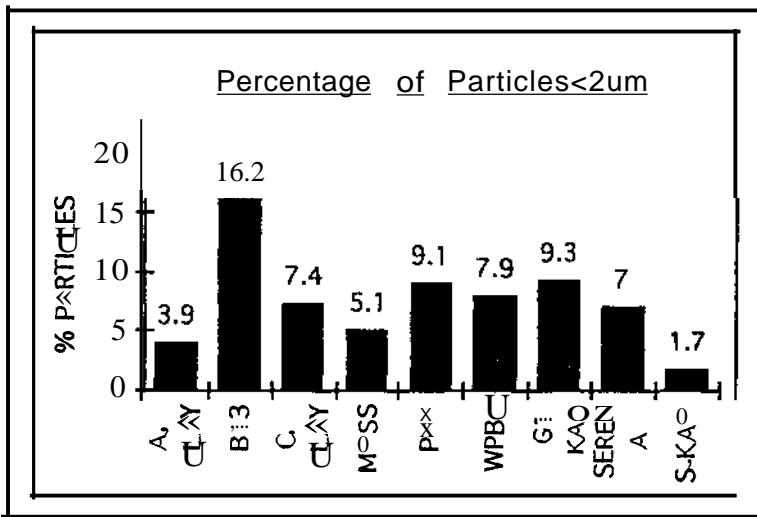


FIG. 4.5

PARTICLE SIZE CHARTS

Fig 4.5 shows the percentage particles less than 2µm in size. This can be used to compare the quantity of colloidal particles present in the clay material.

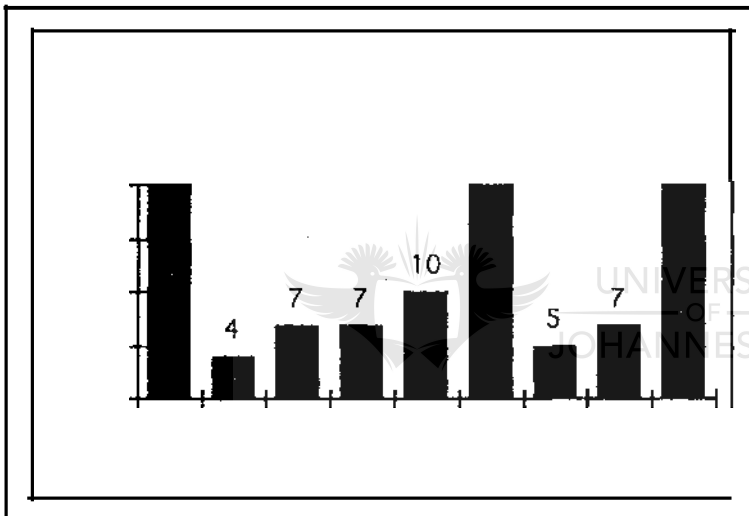


FIG 4.6

Fig 4.6 gives an indication of the proportion of the coarser particles in the clay material. The chart shows the size of the particles present in the largest proportion.

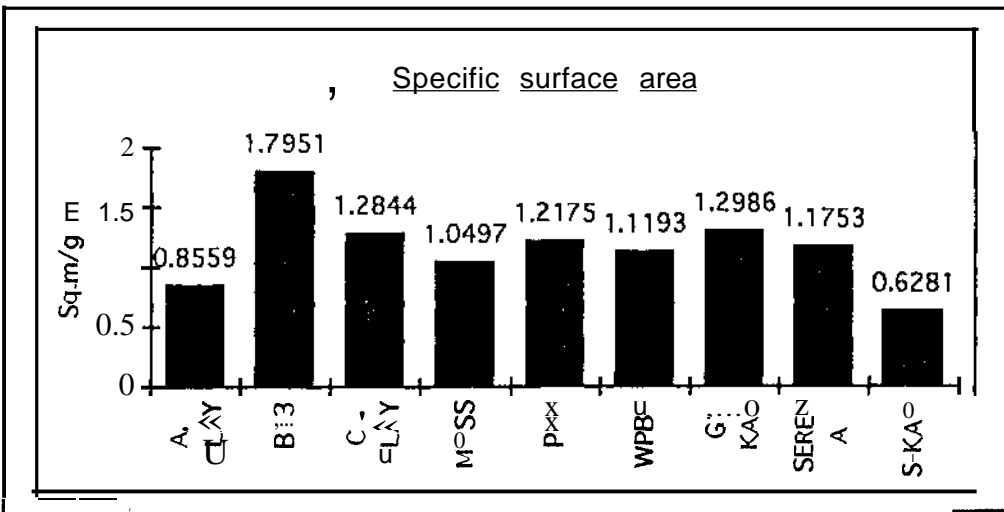


FIG4.7

Fig 4.7 gives an indication of the overall fineness of the material.

4.5 DISCUSSION

The charts and tables presented in this chapter can be compared and analysed, giving both qualitative and quantitative information on the properties of the nine clay materials and clay bodies.

✚ For a clay body to be of use to a ceramist, whether a manufacturer or a studio potter, the required properties of the body **must be considered.** For instance, in the Ceramic Division, TWR, two types of whiteware are required:

1) a body for decorative art wares and **fancy tableware**. These wares frequently need more than a bisque firing followed by a glaze firing. Often a second glaze firing as well as a lustre or on-glaze firing is needed for the desired glaze effect and a non-vitrified body is necessary to prevent dunting in the last firing. The clay should be plastic in order to be thrown and have good green strength in order that the final surface treatment can be performed without fear of breaking. The choice of clays for inclusion in such a body should not approach the vitrification point at the regular firing temperature of the studio (1186°C) and should have a low silica content to avoid dunting. The ware should be white in order to enhance the colours applied to the surface.

2) a body for production wares that complies with the requirements for whitewares. The ware should be just short of vitrification at the chosen firing temperature in order to give mechanical strength and the body / glaze fit should be good to prevent delayed crazing. This body should be plastic for quick production throwing and preferably be compatible with a slip-ware body in order that sets, combining the two techniques, can be produced. (This thesis does not cover the Subject of slipcasting bodies, but the information can be used for their assessment).

In both these cases, as in most others, the properties of workability and plasticity, colour, firing range and vitrification of the ware are of prime importance. It must be noted that any clay body can be formulated using the information supplied in this Data Base.

The information gained from the plasticity tests performed on the clay bodies shows that A Clay and Western Province Ball Clay (WPBC) are consistently the most plastic and easy to throw: On the particle size charts both these clays show a fair percentage of particles less than $2\mu\text{m}$ in size and a peak of particle size distribution at $20\mu\text{m}$ indicating a wide range of particle sizes.

If the similarities between these two clays are followed, it shows that they have the lowest % of total fluxes of all the chosen clays (Table 4.2) and are the lowest in free silica (Table 3.3). Both these clays are also among those with the highest combined iron and titanium content. If these two clays were combined in a white body that has properties as mentioned above (4.5), A-clay, WPBC and other white materials would have to be carefully balanced for the combined iron and titanium content to be less than 2% in order that the final clay body fire white.

The introduction of Moss clay in the place of A-clay would be more suitable for a whiteware body. After firing the clay body samples to 1000°C and 1200°C there was an indiscernible lightening of the A-clay in spite of the reduction in combined Fe+Ti to 2.53% (Table 4.2) but the WPBC and Moss clay fired considerably lighter at 1100°C and slightly lighter at 1200°C .

It should be noted that neither Moss clay nor WPBC are fully fluxed at 1200°C (Fig 4.4) making them useful clays for extending the vitrification range of a clay body without reducing the plasticity as would occur with the addition of kaolin. These two clays had the lowest absorption rate at 1100°C making them extremely useful clays for inclusion in whitewares intended to fire at temperatures below 1200°C . There seems to be no outstanding factor to explain the phenomena e.g. excess low temperature fluxes such as Na_2O or CaO (Table 4.2).

813 clay shows the highest percentage of colloidal particles of all the clay materials tested (Fig 4.5), and the highest specific surface area (Fig 4.7) but the peak of particle size distribution fell below $5\mu\text{m}$ (Fig 4.6) caused the body to be sticky to throw on the wheel (Table 3.32). This could be attributed to the fact that the range of particle sizes is too small.

On examination under the microscope 813 clay material appeared fine particled but highly speckled (Fig.3.13). Separate particles of iron, chrome, titanium and calcium were identified which are the probable cause of the characteristic green tinge of 813 at firing temperatures above 1100°C . Examination of the fired clay body samples of

this clay show an indiscernible lightening of the clay body after the addition of silica and feldspar although the combined Fe+Ti content is 1.7% (Table 4.2).

813, together with PXX clay, are the most vitrified of the clay materials at 1100°C (Fig.4.2) but with the addition of feldspar and silica to form a clay body the vitrification point was raised considerably (Fig 4.4). PXX is a useful white clay of average plasticity (Table 3.32). The clay fired lighter after the addition of silica and feldspar to the clay body but it is not superior in any way and it is doubtful that it should be used in the place of the local clay materials.

As has been stated in Chapter 3, C-Clay is among the whitest of the ball clays tested with a low combined Fe+Ti content of 2.06% (Table 4.1a) but the clay shows a tendency to dilate when combined in a clay body giving the clay body a low rating in the empirical throwing test (Table 3.32). This clay could be introduced in small quantities to a clay body as a whitener. Neither the shrinkage nor the water absorption rates are excessive.

The addition of kaolin to a clay body is usual to increase the refractory materials and reduce the shrinkage of the clay body. Kaolin will also act to lighten the body. Of the three kaolins tested, Serena is far superior to the other two. As mentioned in Chapter 3 (3.8.4) this kaolin falls the closest of all the materials tested to the theoretical composition of kaolinite.

The silica content in Serena and S-Kaolin is low and high in G1 Kaolin. The fluxes follow the same pattern. S-Kaolin is the third clay material of those tested to exhibit a peak of particle size distribution at 20µm (Fig 4.6) but a low percentage of the fine particles (Fig 4.5) and a low specific surface area (Fig 4.7) suggest that it is a coarse, non-plastic material.

It is questionable whether G1 Kaolin should be considered a Kaolin or placed with the ball clays. Its analytical similarity to 813 clay is remarkable.

The information that can be gained from the correlation of data as is shown in this chapter, can assist in the choice of clays for specific bodies. For the two bodies outlined above (4.5) the choice of clay materials would be Moss clay and WP8C for their colour but more specifically for their fluxing power at 1100°C. As has been previously mentioned (1.2) for a body to have strength it should be just short of

vitriification: Both of these clays comply with this requirement. With the addition of Serena kaolin, feldspar and silica, a suitable body could be formulated. The second whiteware body might need the addition of a secondary flux to bring the fired body closer to vitriification point.

The data base and the comparative tables of clays can be updated with each new batch of clay brought into the studio. In this way the Ceramic Division of the TWR could establish a useful, comprehensive record of the composition and physical properties of the clay materials in use.



CHAPTER 5

CONCLUSIONS AND SUGGESTIONS.

The analyses and tests performed on the nine selected clay materials show the range of properties to be found in a handful of clay materials, a minute sample of all the clays round on Earth.

The clay mining companies and distributors should be able to supply an updated analysis of the clay materials with every batch supplied. It is only in rare instances that this is in fact given. This lack of information was one of the prime reasons for undertaking this research project. The available suppliers analyses can be found in Appendix B. A comparison of the EDAX data and the suppliers analysis shows that there are variations in composition, both greater and smaller. The analysis for Serena Kaolin, the most stable of the clay materials, is almost identical in the two analyses giving validation to the EDAX as an analytical tool. Generally the Al_2O_3 shows very little variation between the two analyses, the silica shows more but the Iron content and the fluxes vary considerably in percentage composition..

The techniques laid out in this thesis can be used for testing any clay materials. As has been mentioned, the data should be frequently updated in order to be aware of changes in the composition of the clays in use and thus avert problems before any quantity of ware has been manufactured using material of unknown composition.

The Insight ceramic software programme combined with the ultimate and rational analyses calculations has proved to be efficient and accessible to the students of the Division. As long as the students have available the results from the analyses and the physical tests described here, they may enter them in the programme and "mix" the available clays theoretically, down to the final adjustments, until they obtain the clay body most suited to the type of ware required. This will eliminate the trials and errors of the past and, subsequently, the waste of time and materials.

Alternately, as discussed in detail in section 4.5, the potential of each new clay as a component of clay bodies can be assessed by means of the "Insight" programme by simply entering its chemical analyses in the programme and testing all possible recipes of clay bodies including the new clay material. As a result of this project, therefore, it will be much easier now to venture into new recipes.

Another important achievement of this work is that it has led to a better understanding of the behavior of each clay. As has been discussed in section 4.5,

the behavior can be explained quite consistently in terms of composition and the rational analyses, particle size, fluxing temperature and colour. With further research into other clay materials: a useful body of information can be collected and made available to the students and staff of the Ceramic Division, TWA.

As far as suggestions are concerned, the main one is that the present knowledge of clays should be completed by X-ray diffraction analysis, perhaps in collaboration with another research group, which would lead to knowledge of the mineralogical composition of the clays. This would give another comparative means of assessing the physical properties and workability of the clay materials as well as the ability to determine whether the rational analysis should be based on the feldspar or mica convention.



APPENDICES

APPENDIX A

Rational Analysis

Copied from Whitewares Production, Testing and Quality Control
by W. Ryan and C. Radford. Page 158 - 162

Example

SiO ₂	61.30
Al ₂ O ₃	20.20
Fe ₂ O ₃	3.40
TiO ₂	0.20
MgO	0.24
CaO	0.34
Na ₂ O	1.05
K ₂ O	2.35
loss	10.90

To Calculate the Rational Analysis of a Clay

FELSPAR CONVENTION

- (1) Using this convention it is assumed that the alkalis (K₂O and Na₂O) are derived entirely from feldspars.

1 molecule K₂O ≡ 1 molecule potash feldspar

≡ K₂O·Al₂O₃·6SiO₂

94 parts K₂O ≡ 556 parts potash feldspar

1 part K₂O ≡ $\frac{556}{94}$ parts potash feldspar

= 5.92 potash feldspar or orthoclase

A similar calculation for soda spar (albite)

Na₂O·Al₂O₃·6SiO₂

yields a factor of 8.45. However, it is common practice to take the sum of the percentage of K₂O and Na₂O and to use the factor of 5.92 to convert these oxides to mineral feldspar. This treatment should only be applied to clays when the total alkalis are small (2-4%) and the amount of K₂O is approximately twice the Na₂O content.

Considering the ultimate analysis quoted at the beginning of the chapter,

(K₂O 2.35 + Na₂O 1.05) = 3.40 total alkali content

3.40 × 5.92 = 20.13% feldspar

- (2) (a) 1 molecule K₂O·Al₂O₃·6SiO₂ ≡ 1 molecule Al₂O₃

556 ≡ 102

1 part feldspar ≡ $\frac{102}{556}$ parts Al₂O₃

= 0.183 Al₂O₃

20.13 × 0.183 = 3.68 parts Al₂O₃
in feldspar

- (b) Similarly,

556 feldspar ≡ 6 × 60 SiO₂

1 feldspar ≡ $\frac{360}{556}$ SiO₂

= 0.647 SiO₂

20.13 × 0.647 = 13.02 parts SiO₂
in feldspar

$$\begin{aligned}
 (3) \quad & \text{Total Al}_2\text{O}_3 = 20.20 \text{ (ref. ultimate analysis)} \\
 & \text{-Al}_2\text{O}_3 \text{ in felspar} = -3.68 \\
 & \quad \quad \quad 16.52 = \text{Al}_2\text{O}_3 \text{ in clay substance} \\
 & 1 \text{ molecule Al}_2\text{O}_3 \equiv 1 \text{ molecule Al}_2\text{O}_3 \cdot 2\text{SiO}_2 \cdot 2\text{H}_2\text{O} \\
 & \quad \quad \quad 102 \equiv 258 \\
 & 1 \text{ part Al}_2\text{O}_3 \equiv \frac{258}{102} \text{ parts clay substance} \\
 & \quad \quad \quad = 2.53 \text{ clay substance} \\
 \therefore & 16.52 \times 2.53 = \underline{41.79\% \text{ clay substance}}
 \end{aligned}$$

$$\begin{aligned}
 (4) \quad & 1 \text{ molecule Al}_2\text{O}_3 \cdot 2\text{SiO}_2 \cdot 2\text{H}_2\text{O} \equiv 2 \text{ molecules SiO}_2 \\
 & \quad \quad \quad 258 \equiv 2 \times 129 \\
 & 1 \text{ clay substance} \equiv \frac{129}{258} \text{ SiO}_2 \\
 & \quad \quad \quad = 0.465 \text{ SiO}_2 \\
 & \text{SiO}_2 \text{ in clay substance} = 41.79 \times 0.465 \\
 & \quad \quad \quad = 19.43\% \text{ SiO}_2 \text{ in clay substance}
 \end{aligned}$$

$$\begin{aligned}
 \text{Free quartz} &= \text{Total SiO}_2 \\
 & \quad \quad \quad - (\text{SiO}_2 \text{ in clay substance} - \text{SiO}_2 \text{ in felspar}) \\
 &= 61.30 - (19.43 + 13.02) \\
 &= \underline{28.85\% \text{ free quartz}}
 \end{aligned}$$

Summary

$$\begin{aligned}
 & \text{Total alkalis} \times 5.92 = \underline{\% \text{ felspar}} \\
 & \text{Felspar} \times 0.183 = \underline{\text{Al}_2\text{O}_3 \text{ in felspar}} \\
 & \text{Felspar} \times 0.647 = \underline{\text{SiO}_2 \text{ in felspar}} \\
 & (\text{Total Al}_2\text{O}_3 - \text{Al}_2\text{O}_3 \text{ in felspar}) \times 2.53 = \underline{\% \text{ clay substance}} \\
 & \text{Clay substance} \times 0.465 = \underline{\% \text{ SiO}_2 \text{ in clay}} \\
 & \text{Total SiO}_2 - (\text{SiO}_2 \text{ in clay} + \text{SiO}_2 \text{ in felspar}) = \underline{\% \text{ quartz}}
 \end{aligned}$$

Further information can be obtained from the percentage loss-on-ignition. The first step is to calculate the loss due to the chemically combined water in the clay molecule.

$$\begin{aligned}
 1 \text{ molecule Al}_2\text{O}_3 \cdot 2\text{SiO}_2 \cdot 2\text{H}_2\text{O} &\equiv 2 \text{ molecules H}_2\text{O} \\
 & \quad \quad \quad 258 = 2 \times 129 \\
 1 \text{ part clay} &\equiv \frac{36}{258} \text{ parts water} \\
 &= 0.140 \text{ part water} \\
 41.78 \times 0.140 &= 5.83 \text{ loss due to H}_2\text{O in clay molecule} \\
 (\text{Total loss} - \text{loss due to H}_2\text{O in clay}) &= \text{loss due to organic matter, CO}_2, \text{ etc.} \\
 (10.90 - 5.83) &= \underline{5.07\% \text{ loss due to organic matter, CO}_2, \text{ etc.}}
 \end{aligned}$$

MICA CONVENTION

The mica convention is concerned with the minerals
 . potash mica ($K_{20.3}Al_{203.6}Si_{102.2}H_{20}$)
 and soda mica ($Na_{20.3}Al_{203.6}Si_{102.2}H_{20}$)

Using the ultimate analysis from the previous example:

$$(1) \quad 1 \text{ molecule } K_{20} \equiv 1 \text{ molecule } K_{20.3}Al_{203.6}Si_{102.2}H_{20}$$

$$94 \equiv 796$$

$$1 \text{ part } K_{20} \equiv \frac{796}{94} \text{ parts mica}$$

$$1 \text{ part } K_{20} = 8.47 \text{ parts potash mica}$$

Similarly the factor for converting Na₂₀ content to soda mica = 12.32.

$$K_{20} = 2.35\% \text{ (ref. ultimate analysis)}$$

$$2.35 \times 8.47 = \text{potash mica} \equiv 19.91\%$$

$$\text{and } 1.05 \times 12.32 = \text{soda mica} \equiv 12.93\%$$

$$(2) \quad 1 \text{ molecule potash mica} \equiv 3 \text{ molecules } Al_{203}$$

$$796 \equiv 306$$

$$306$$

$$1 \equiv \frac{306}{796}$$

$$\therefore 1 \text{ part potash mica} \equiv 0.384 \text{ parts } Al_{203}$$

$$19.91 \times 0.384 = 7.64 = Al_{203} \text{ in potash mica}$$

$$1 \text{ molecule potash mica} \equiv 6 \text{ molecules } Si_{102}$$

$$796 \equiv 6 \times 60$$

$$360$$

$$1 \equiv \frac{360}{796}$$

$$1 \text{ part potash mica} \equiv 0.452 \text{ parts } Si_{102}$$

$$\therefore 19.91 \times 0.452 = 9.00 = Si_{102} \text{ in potash mica}$$

Similarly for soda mica:

$$12.93 \times 0.400 = 5.17 = Al_{203} \text{ in soda mica}$$

$$12.93 \times 0.471 = 6.09 = Si_{102} \text{ in soda mica}$$

$$(3) \quad \text{Total } Al_{203} \text{ (ref. ultimate analysis)} = 20.20$$

$$- Al_{203} \text{ in micas } (7.64 + 5.17) = 12.81$$

$$Al_{203} \text{ in clay substance} = 7.39$$

$$7.39 \times 2.53 = 18.69\% \text{ clay substance}$$

$$(4) \quad Si_{102} \text{ in clay} = 18.69 \times 0.465 = 8.69$$

$$Si_{102} \text{ in clay} + Si_{102} \text{ in micas} = (8.69 + 9.00 + 6.09)$$

$$= 23.78$$

$$\therefore \text{Free quartz} = 61.30 - 23.78 = 37.52\%$$

The final rational analysis is:

Potash mica	19.9
Soda mica	12.9
Clay substance	18.7
Quartz	37.5
Organic matter, CO ₂ , etc., by difference	6.9
Fe ₂₀₃	3.4
TiO ₂	0.2
MgO	0.2
CSO	0.3

Summary

$$K_{20} \times 8.47 = \text{potash mica}$$

$$Na_{20} \times 12.32 = \text{soda mica}$$

$$\text{Potash mica} \times 0.384 = Al_{203} \text{ in potash mica}$$

$$\text{Potash mica} \times 0.452 = Si_{102} \text{ in potash mica}$$

$$\text{Soda mica} \times 0.400 = Al_{203} \text{ in soda mica}$$

$$\text{Soda mica} \times 0.471 = Si_{102} \text{ in soda mica}$$

$$(\text{Total } Al_{203} - Al_{203} \text{ in micas}) \times 2.53 = \text{clay substance}$$

$$\text{Clay substance} \times 0.465 = Si_{102} \text{ in clay}$$

$$\text{Total } Si_{102} - (Si_{102} \text{ in clay} + Si_{102} \text{ in micas}) = \text{Free quartz}$$

APPENDIX B

Chemical Analy\$es supplied by the distributors

CLAY TYPE	C CLAY	B13 CLAY	WPBC	PXX	A CLAY	KAOLIN GI	KAOLIN S	SERENA K
SiO ₂	56.8	58.9	48.5	54.5	55.85	65.5	53	47
AL ₂ O ₃	23.6	24.9	31.6	33.5	28.9	22.5	31	37.5
Fe ₂ O ₃	0.6	2.5	2.2	0.2	2.88	0.6	1.5	0.6
rTiO ₂	1.8	0.9	1.4	1.5	1.5	0.5	0.9	0.68
MgO	0.2	0.3	0.5	0.1	0.3	0.1	0.1	0.18
CaO	0.3	0.2	0.16	0.2	0.45	0.04	0.1	0.1
Na ₂ O	0.3	0.4	0.1	1.2	0.05	0.6	0.2	0.3
K ₂ O	0.35	1.4	0.7	3.2	0.4	3.6	0.2	0.8
MnO				0.01				
LOI	6.7	9	12.9	5.4	10.6	5.7	11.7	13.3



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APPENDIX C**RESULTS OF THE PHYSICAL TESTS****Loss On Ignition**

Clay	A Clay	813	C Clay	Moss	Pxx	WPBC	G1 Kaol.	Selina	S Kaolin
Drywt	73	70	71.5	70	78	69.5	75.	75.	73.25
110°C	72.4	74.5	69	67	73	65.5	72.5	69.25	67.00
1000°C	61.10	67.7	64.8	63.2	66.7	57.7	68.8	60.9	60.4
LOI	10.9	6.8	6.1	5.7	8.6	11.9	5.1	12.05	9.8

Water of plasticity; Linear shrinkage; Water absorption.**CLAY MATERIAL**

CLAY TYPE	C CLAY B13	WPBC	PXX	A CLAY	G1 K	SK	SER K	MOSS	
WATER OF PLASTICITY	38%	40%	42%	35%	44%	36%	47%	52%	45%
LIN. SHRINKAGE									
A	9%	9%	10.50%	6.50%	11%	5%	7%	6.50%	8.5%
600	9%	9%	10.50%	6.50%	11%	5%	7%	6.50%	6%
B	9%	12%	12%	10%	14%	6.50%	10%	9%	8.5%
C	14%	17%	15%	16.50%	15%	10%	11%	9%	12%
0	18%	18%	20.50%	20%	23%	15%	15%	13%	18%
ABSORPTION									
A									
600		17.60%	23.90%		24.20%			36.20%	
B	18.90%	13.10%	20.50%	18.10%	20%	22.10%	46.00%	35.90%	26%
C	12.20%	1.40%	12.80%	2.40%	16.20%	16.90%	40.90%	35.10%	18.7%
0	0.50%	0.70%	1.85%	0.20%	1.70%	1.10%	33.80%	21.10%	4.10%

CLAY BODIES

% LINEAR SHRINKAGE (WET-FIRED)									
	A-CLAY	813	C-CLAY	MOSS	PXX	WP8C	G1 KAO	SER K	S-KAO
W	0	0	0	0	0	0	0	0	0
0	9.9	12	6	6	6	8	6	6	6
1000	9.9	12	6	8	6	10	6	6	6
1100	12	14	6	10	8	10	8	8	8
1200	14	16	14	12	14	14	12	10	10

% WATER ABSORPTION									
	A-CLAY	813	C-CLAY	MOSS	PXX	WP8C	G1 KAO	SER K	S-KAO
1000	16	15.5	16	18	14	15	19.5	25	23
1100	13.5	12	15	5.7	10.3	6.6	17	25	23
1200	0.7	0.9	3.6	2.5	2.5	5.3	5.9	15	15



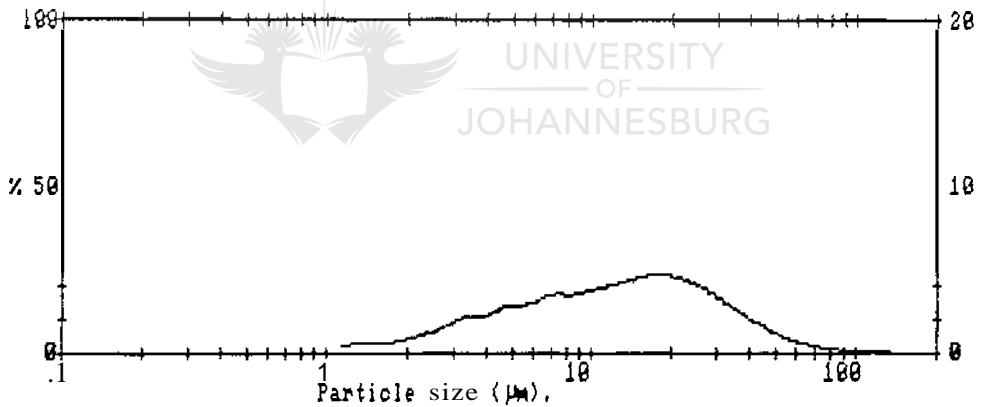
Particle size Analysis

A clay

MALVERN MASTERSIZER S2.01 Date 01-01-1980 Time 01:34

SAMPLE NO: 1 - AC

Dispersant Water
 Additives None
 Ultrasound Max
 PUIP speed 80%
 Stir speed 80%
 Notes



Upper Size	% in	Lower Size	% under	Upper Size	% in	Lower Size	% under
600	0.0	600	100	31.0	6.7	25.5	79.6
492	0.0	492	100	25.5	8.0	20.9	71.6
404	0.0	404	99.9	20.9	8.6	17.1	63.0
333	0.0	333	99.9	17.1	8.3	14.1	54.6
272	0.0	272	99.9	14.1	7.7	11.6	46.9
224	0.0	224	99.8	11.6	7.1	9.48	39.8
183	0.0	183	99.8	9.48	6.5	7.78	33.3
151	0.0	151	99.7	7.78	6.3	6.39	28.9
124	0.0	124	99.5	6.39	5.5	5.24	21.4
101	0.0	101	99.3	5.24	5.1	4.38	16.3
83.3	0.0	83.3	99.0	4.38	4.2	3.53	12.2
68.3	0.0	68.3	98.8	3.53	3.8	2.98	8.4
56.1	0.0	56.1	97.1	2.98	2.7	2.38	5.7
46.0	0.0	46.0	94.9	2.38	1.8	1.95	3.9
37.8	0.0	37.8	91.4	1.95	1.3	1.66	2.6
		31.0	86.3	1.66	1.2	1.32	1.4

Result source=Salpe
Record No. = 0
Focal length = 300 II.
Presentation = 0903
Volume distribution
Beal length = 2.0 II.
Obscuration = 0.2892
Volume Cone. = 0.6239 %
Residual = 0.113%
Model indp
D(Y.B.S) = 12.52 II
DI(9.9) = 35.68 III
DI(3.1) = 3.17 III
DI(4.3) = 15.89 III
DI(3.2) = 7.94 III
Span = 2.6
Spec. surf. area
0.8559 sq.l./gl.

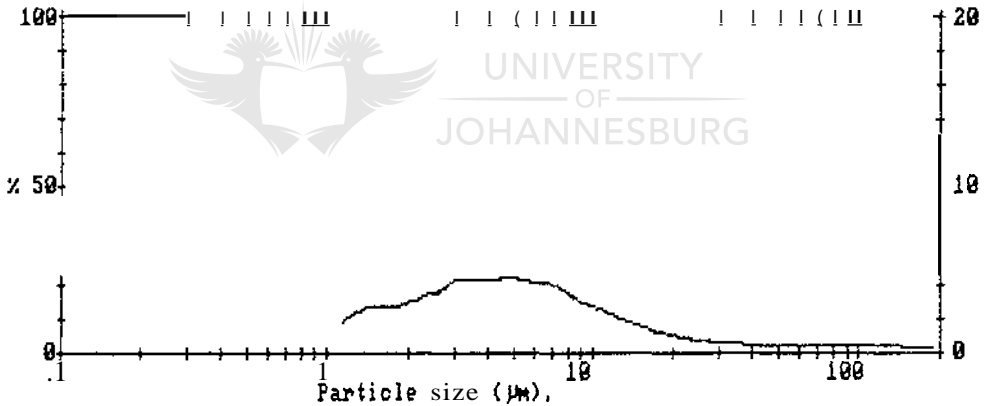
Particle size Analysis

8 13 8all clay

MALVERN MASTERSIZER S2.01 Date 01-01-1980 Time 00:13

SAMPLE NO: 2 - 813

Dispersant Water
 Additives None
 Ultrasound Max
 PUIP speed 80%
 Stir speed 80%
 Notes



Upper Size	% in	Lower Size	% under	Upper Size	% in	Lower Size	% under
600	0.0	492	100	31.0	1.3	25.5	90.3
492	0.0	404	100	25.5	1.6	20.9	88.7
404	0.0	332	100	20.9	2.2	17.1	86.5
332	0.1	272	99.9	17.1	2.8	14.1	83.7
272	0.2	224	99.7	14.1	3.8	11.6	79.9
224	0.4	183	99.3	11.6	4.9	9.48	75.1
183	0.6	151	98.7	9.48	6.4	7.78	69.1
151	0.8	124	98.0	7.78	7.7	6.39	61.6
124	0.9	101	97.1	6.39	8.0	5.24	53.6
101	0.8	83.3	96.3	5.24	8.3	4.30	45.3
83.3	0.9	68.3	95.4	4.30	8.0	3.53	37.3
68.3	0.9	55.1	94.5	3.53	7.1	2.90	29.3
55.1	0.9	45.0	93.6	2.90	6.0	2.38	22.2
45.0	0.9	37.8	92.7	2.38	5.2	1.95	16.2
37.8	1.1	31.0	91.6	1.95	5.1	1.60	10.9
				1.60	5.1	1.32	5.9

Result source=Sample
 Record No. = 0
 Focal length = 300 II.
 Presentation = 0903
 Volume distribution
 Deal length = 2.0 II.
 Obscuration = 0.1853
 Volume Cone. = 0.0094 %
 Residual = 0.375%
 Model indp
 D(v,0.5) = 4.81 µm
 Div(0.9) = 24.33 µm
 Div(0.1) = 1.55 µm
 O14.3) = 18.14 µm
 O13.2) = 3.70 µm
 Span = 4.7
 Spec. surf. area
 1.7951 sq.l./gl.

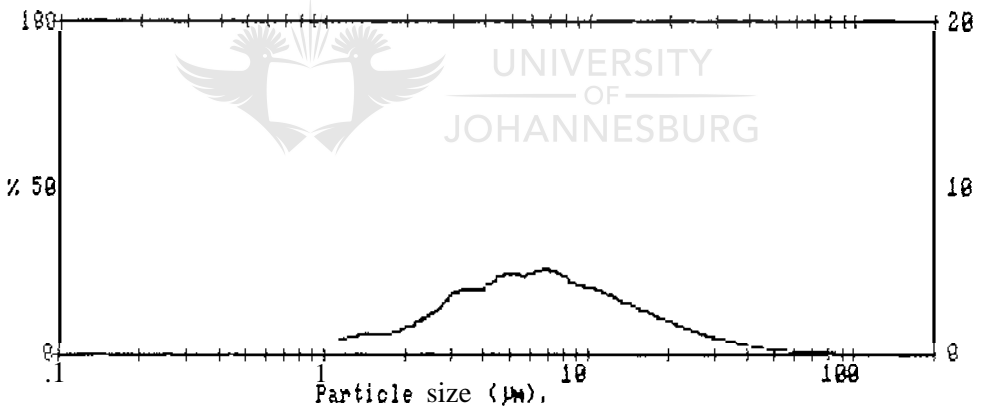
Particle size Analysis

C-Clay

MALVERN MASTERSIZER S2.01 Date 01-01-1980 Time 00:24

SAMPLE NO: 3 - CCLAY

Dispersant Water
 Additives None
 Ultrasound Max
 Pu.p speed 80%
 Stir speed 80%
 Notes



Upper Size	% in	Lower Size	% under	Upper Size	% in	Lower Size	% under
600	1.1	492	98.9	31.0	2.1	25.5	99.8
492	1.1	404	97.8	25.5	3.0	20.9	87.8
404	0.8	332	97.2	20.9	4.0	17.1	83.8
332	0.2	272	96.8	17.1	5.1	14.1	78.7
272	0.1	224	96.8	14.1	6.2	11.6	72.5
224	0.1	183	96.8	11.6	7.3	9.4	65.1
183	0.1	151	96.7	9.4	8.2	7.7	56.9
151	0.1	124	96.6	7.7	9.3	6.3	47.6
124	0.1	101	96.6	6.3	8.9	5.2	38.7
101	0.1	83.3	96.4	5.2	8.7	4.3	30.0
83.3	0.1	68.3	96.2	4.3	7.3	3.5	22.7
68.3	0.0	56.1	95.9	3.5	7.0	2.9	15.8
56.1	0.0	46.0	95.3	2.9	5.0	2.3	10.8
46.0	0.0	37.8	94.4	2.3	3.4	1.9	7.4
37.8	1.4	31.0	92.9	1.6	2.3	1.3	2.6

Result source=Salpe
Record No. = 0
Focal length = 300 II.
Presentation = 0903
Volume distribution
Mean length = 2.0 I**
Obscuration = 0.2327
Volume Cone. = 0.0176 %
Residual = 0.165 %
Model indep
D(v,0.5) = 6.72 µm
D(v,0.9) = 23.95 µm
Q(v,0.1) = 2.23 µm
Q(4,3) = 12.41 µm
Q(3,2) = 5.15 µm
Span = 3.2
Spec. surf. area
1.2844 sq.l./gl.

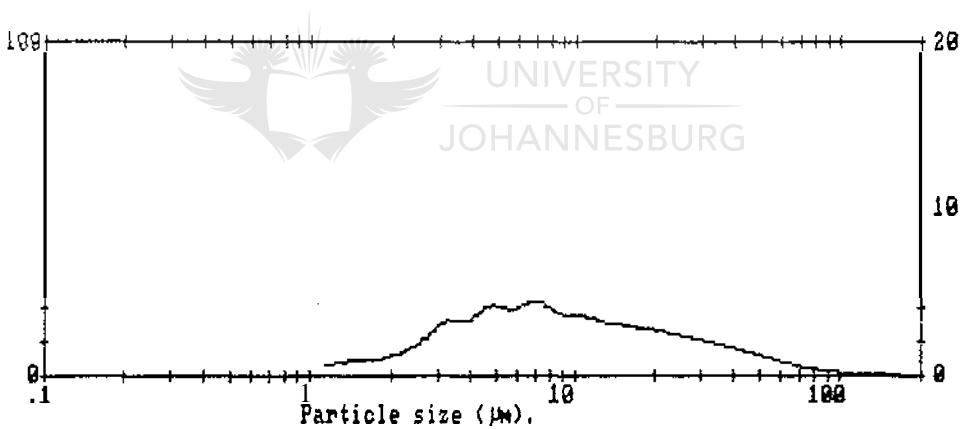
Particle size Analysis

Moss Clay

MALVERN MASTERSIZER S2.91 Date 01-01-1980 Time 00:44

SAMPLE NO: 5 - MOSS

Dispersant Water
 Additives None
 Ultrasound Max
 PUIP speed 80%
 Stir speed 80%
 Notes



Upper Size	% in	Lower Size	% under	Upper Size	% in	Lower Size	% under
600	1.3	600		4.1	25.5	81.3	
492	0.6	404		4.7	20.9	76.6	
404	0.2	332		5.1	17.1	71.4	
332	0.1	272		5.5	14.1	65.9	
272	0.1	224		6.0	11.6	59.9	
224	0.1	183		6.5	9.48	53.4	
183	0.1	151		6.9	7.78	46.5	
151	0.1	124		8.0	6.39	38.5	
124	0.1	101		7.4	5.24	31.1	
101	0.1	83.3		7.5	4.30	23.6	
83.3	0.1	68.3		6.1	3.53	17.5	
68.3	1.5	56.1		5.8	2.90	11.6	
56.1	2.2	46.8		4.0	2.38	7.6	
46.8	2.0	37.8		2.5	1.95	5.1	
37.8	3.6	31.0		1.7	1.60	3.4	
				1.6	1.32	1.8	

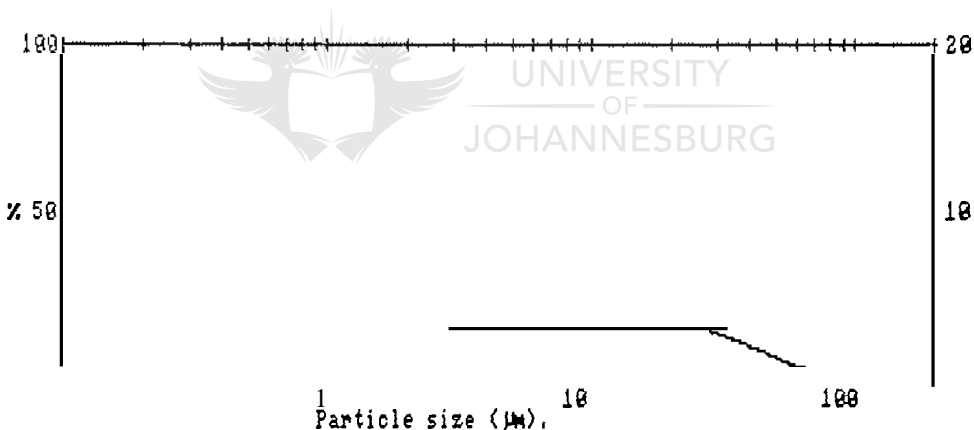
Particle size Analysis

PXX ball clay

MALVERN MASTERSIZER S2.01 Date 01-01-1980 Time 00:34

SAMPLE NO: 4 - PXX

Dispersant Water
 Additives None
 Ultrasound Max
 Pulp speed 80%
 Stir speed 80%
 Notes



Upper Size	% in	Lower Size	% under	Upper Size	% in	Lower Size	% under
600	0.6	600	100	31.0	5.3	25.5	79.6
492	0.3	492	99.4	25.5	5.8	20.9	73.8
404	0.2	404	99.0	20.9	5.9	17.1	67.9
332	0.1	332	98.9	17.1	5.7	14.1	62.2
272	0.1	272	98.8	14.1	5.5	11.6	56.7
224	0.1	224	98.7	11.6	5.5	9.48	51.2
183	0.1	183	98.7	9.48	5.6	7.78	45.6
151	0.1	151	98.6	7.78	5.0	6.39	39.6
124	0.1	124	98.4	6.39	5.9	5.24	33.7
101	0.2	101	98.2	5.24	5.9	4.30	27.8
83.3	0.4	83.3	97.8	4.30	5.4	3.53	22.3
68.3	0.8	68.3	96.9	3.53	5.2	2.96	17.1
56.1	1.5	56.1	95.5	2.96	4.4	2.38	12.7
46.0	2.4	46.0	93.0	2.38	3.5	1.95	9.1
37.8	3.6	37.8	89.5	1.95	2.9	1.60	6.2
	4.6	31.0	84.9	1.60	2.8	1.32	3.4

Result source=Salple
 Record No. = 0
 Focal length = 300 mm.
 Presentation = 0.03
 Volume distribution
 Beal length = 2.0 mm.
 Obscuratfon = 0.2887
 Volume Cone. = 0.8336 %
 Residual = 0.122 %
 Model indp
 D(Y,0.5) = 9.08 µm
 D(y,0.9) = 38.80 µm
 D(y,0.1) = 2.06 µm
 D(4,3) = 14.99 µm
 D(3,2) = 5.57 µm
 Span = 4.0
 Spec. surf. area = 1.2175 Sq.1./gI.

Particle size Analysis

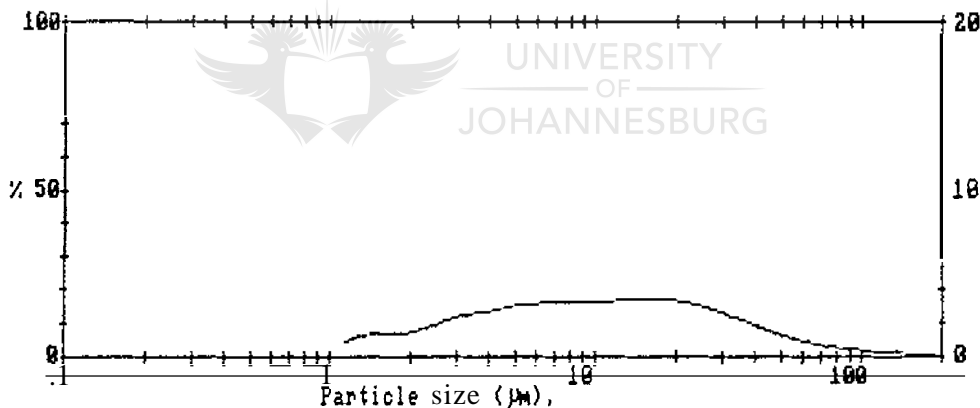
Western Province Ball Clay

MALEVERN

MASTERSIZER S2.01 Date 01-01-1980 Time 00:55

SAMPLE NO: 6 - WABC

Dispersant Water
 Additives None
 Ultrasound Max
 PUMP speed 80%
 Stir speed 80%
 Notes



Upper Size	% in	Lower Size	% under	Upper Size	% in	Lower Size	% under	Result source-Salple
600	0.0	600	100	31.0	5.1	25.5	78.8	Record No. = 0
492	0.0	492	99.8	25.5	5.8	20.9	73.0	Focal length = 300 mm
404	0.0	404	99.6	20.9	6.3	17.1	66.7	Presentation = 0.03
332	0.0	332	99.5	17.1	6.4	14.1	60.4	Volume distribution
272	0.0	272	99.3	14.1	6.2	11.6	54.1	Beam length = 2.0 II.
224	0.0	224	99.1	11.6	6.2	9.48	47.9	Obscuration = 0.2255
183	0.0	183	98.8	9.48	6.1	7.78	41.8	Volume Cone = 0.0194 %
151	0.0	151	98.5	7.78	6.1	6.39	35.7	Residual = 0.105 %
124	0.0	124	98.0	6.39	5.9	5.24	29.8	Model indp
101	0.0	101	97.4	5.24	5.5	4.38	24.3	D(v,0.5) = 10.13 µm
83.3	0.0	83.3	96.6	4.38	4.9	3.53	19.4	DIY(0.9) = 42.01 µm
68.3	0.0	68.3	95.4	3.53	4.6	2.90	14.8	DIY(0.1) = 2.24 µm
56.1	0.0	56.1	93.8	2.90	3.8	2.38	11.0	D[4,3] = 16.59 µm
46.0	0.0	46.0	91.4	2.38	3.1	1.95	7.9	D[3,2] = 6.09 µm
37.8	0.0	37.8	88.1	1.95	2.5	1.60	5.4	Span = 3.9
		31.0	83.9	1.60	2.4	1.32	3.0	Spec. surf. area = 1.1193 sq.1.Jgl.

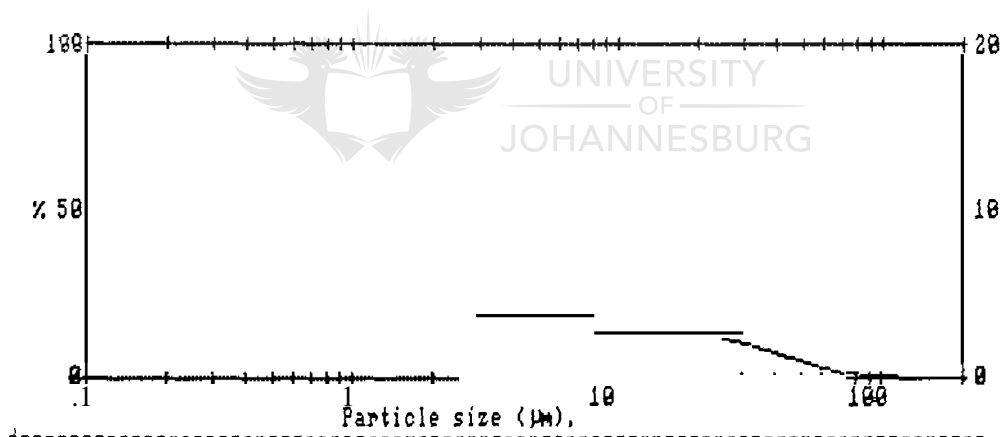
Particle size Analysis

G1 Kaolin

MALVERN MASTERSIZER S2.91 Date 01-01-1988 Time 91:25

SAMPLE NO: 9 - 61 K

Dispersant Water
 Additives None
 Ultrasound Max
 PUMP speed 80%
 Stir speed 80%
 Notes .



Upper Size	% in	Lower Size	% under	Upper Size	% in	Lower Size	% under
600	2.0	600	100	31.0	4.0	25.5	82.6
492	0.0	492	98.0	25.5	4.5	28.9	78.1
404	0.0	404	97.3	20.9	4.7	17.1	73.3
332	0.0	332	97.0	17.1	4.9	14.1	68.5
272	0.0	272	96.9	14.1	5.1	11.6	63.4
224	0.0	224	96.9	11.6	5.4	9.48	58.0
183	0.0	183	96.8	9.48	5.8	7.78	52.1
151	0.0	151	96.8	7.78	6.9	6.39	45.3
124	0.0	124	96.7	6.39	6.8	5.24	38.5
101	0.0	101	96.6	5.24	7.2	4.30	31.3
83.3	0.6	83.3	96.3	4.30	6.5	3.53	24.8
68.3	1.1	68.3	95.7	3.53	6.5	2.90	18.3
56.1	1.8	56.1	94.6	2.90	5.1	2.38	13.2
46.0	2.7	46.0	92.7	2.38	3.9	1.95	9.3
37.8	3.4	37.8	90.0	1.95	3.1	1.60	6.2
		31.0	86.6	1.60	2.9	1.32	3.3

Result source=Sample
 Record No. = 0
 Focal length = 300 II.
 Presentation = 0903
 Volume distribution
 Beam length = 2.0 II.
 Obscurahon = 0.3253
 Volume Cone. = 0.8255 %
 Residual = 0.108 %
 Model indp
 Div.(1.5) = 7.30 µm
 Div.(8.9) = 37.68 µm
 Div.(0.1) = 2.83 µm
 D(14.3) = 16.19 µm
 D(3.2) = 5.15 µm
 Span = 4.9
 Spec. surf. area = 1.2986 sq.1./gl.

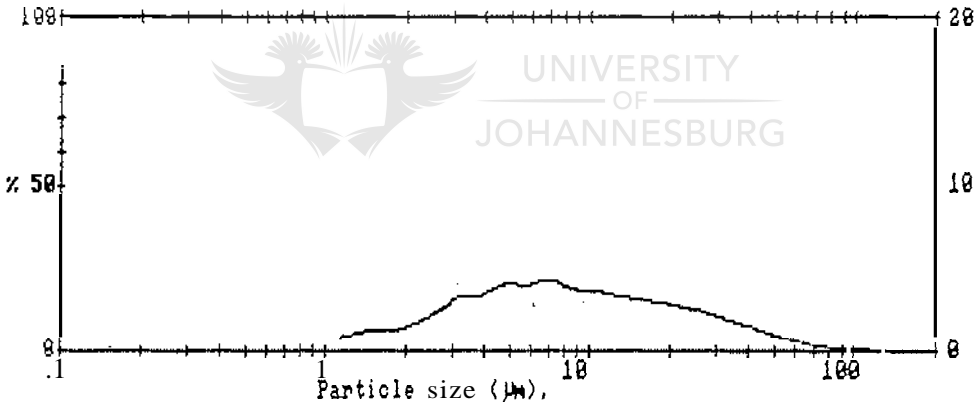
Particle size Analysis

Serena Kaolin

MALVERN MASTERSIZER S2.01 Date 01-01-1980 Time 01:04

SAMPLE NO: 7 - SER-

Dispersant Water
 Additi Yes None
 Ultrasound Max
 PUIP speed 80%
 Stir speed 80%
 Notes



Upper Size	% in	Lower Size	% under	Upper Size	% in	Lower Size	% under	Result
600	0.7	492	99.3	31.0	4.1	25.5	84.7	Result source=Sample
492	0.4	404	98.9	25.5	4.8	20.9	79.9	Record No. = 0
404	0.1	332	98.8	20.9	5.4	17.1	74.5	Focal length = 300 II.
332	0.1	272	98.7	14.1	5.7	14.1	68.8	Presentation = 0903
272	0.0	224	98.7	11.6	6.1	11.6	62.7	Volume distribution
224	0.0	183	98.6	9.48	6.6	9.48	56.1	Beam length = 2.0 II.
183	0.1	151	98.6	7.78	7.0	7.78	49.2	Obscuration = 0.2210
151	0.1	124	98.5	6.39	7.7	6.39	41.4	Volume Cone. = 0.0182 %
124	0.1	101	98.3	5.24	7.4	5.24	34.0	Residual = 0.118%
101	0.1	83.3	98.0	4.30	7.3	4.30	26.7	Model indp
83.3	0.1	68.3	97.5	3.53	6.2	3.53	20.5	D(v, 0.5) = 7.95 µm
68.3	1.0	56.1	96.5	2.90	5.9	2.90	14.6	D(1, 0.9) = 32.95 µm
56.1	1.7	46.0	94.8	2.38	4.4	2.38	10.2	D(1, 0.1) = 2.36 µm
46.0	2.5	37.8	92.2	1.95	3.1	1.95	7.0	D(1, 3) = 12.90 µm
37.8	3.4	31.0	88.9	1.60	2.3	1.60	4.7	D(1, 2) = 5.69 µm
				1.60	2.2	1.52	2.5	Span = 3.8
								Spec. surf. area = 1.1753 sq.../g1.

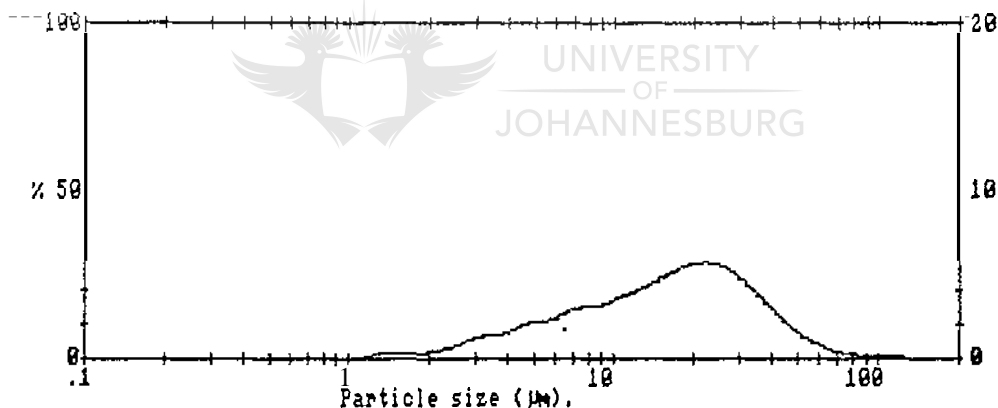
Particle size Analysis

S-Kaolin

MALVERN MASTERSIZER S2.IU Date 01-01-1980 Time 01:14

SAMPLE NO: 8 - S K

Dispersant Water
 Additives None
 Ultrasound Max
 PUIP speed 80%
 Stir speed 80%
 Notes



Upper Size	% in	lower Size	% under:	Upper Size	% in	lower Size	% under:
600	0.1	492	99.9	31.0	9.4	25.5	72.8
492	0.0	404	99.9	25.5	10.5	20.9	62.3
404	0.0	332	99.9	20.9	10.1	17.1	52.2
332	0.0	272	99.8	17.1	9.0	14.1	43.2
272	0.0	224	99.8	14.1	7.7	11.6	35.5
224	0.0	183	99.7	11.6	6.7	9.48	28.8
183	0.1	151	99.7	9.48	5.8	7.78	23.0
151	0.1	124	99.5	7.78	5.4	6.39	17.6
124	0.2	101	99.4	6.39	4.3	5.24	13.3
101	0.3	83.3	99.0	5.24	3.9	4.38	9.4
83.3	0.7	68.3	98.4	4.38	2.8	3.53	6.6
68.3	1.4	56.1	97.0	3.53	2.5	2.90	4.1
56.1	2.7	46.0	94.3	2.90	1.5	2.38	2.6
46.0	4.8	37.8	89.5	2.38	0.9	1.95	1.7
37.8	7.3	31.0	82.2	1.95	0.6	1.60	1.1
				1.60	0.5	1.32	0.6

Result source=Sample
Record No. = 111
Focal length = 300 II.
Presentation = 0903
Volume distribution
Beal length = 2.0 II.
Obscuration = 0.2558
Volume Cone. = 0.0423 %
Residual = 0.174%
Model indep
D(y,0.5) = 16.40 µm
D(v,0.9) = 38.47 µm
D(v,0.1) = 4.45 µm
D(4.3) = 18.85 µm
D(3.2) = 10.79 µm
Span = 2.1
Spec. surf. area = 0.6281 sq.1./g1.

APPENDIX D**SEMIEDAX*****Standards used for EDAX analysis.***

The MINTEK standards used were:

Si - 23	SiO ₂
Al- 5	Al ₂ O ₃
Fe - 18	Fe ₂ O ₃ P
Ti - 2	TiO ₂ P
Mg-1	MgOP
Si -12	CaOP
Si - 33	Na ₂ O _p
Mn-4	Mn ₃ O ₄
Si - 28	K ₂ O _p



Explanation of ZAF correction

Z .The atomic number correction is required on account of two phenomena - electron backscattering and electron retardation, both of which depend on the average atomic number of the sample. If there is a difference between the average atomic number of the sample and that of the standard, an atomic number correction is necessary.

Variables affecting the Z correction are: operating voltage, take off angle and the mass absorption factor for the element of interest.

A The absorption correction is required since the x-rays produced by the electron beam are created at some non-zero depth in the sample, and they must pass through the sample on the way to the detector. On this journey, some of the X-rays undergo absorption due to interactions with the atoms of the various elements in the sample. Thus the intensity of the X-ray radiation finally reaching the detector is reduced in magnitude.

Variables affecting the A correlation are : respective mass absorption coefficients, the critical excitation voltage E_c for K, L and M radiation from the element and the mean atomic number and mean atomic weight of the sample.

F The fluorescent correction is necessary if the energy of the X-ray peak from one element is sufficient to excite X-rays secondarily from another element. Thus more X-rays from the second element are generated than would have been produced by electron excitation alone.

CLAY MATERIAL ANALYSES

The stoichiometric analyses of the nine selected clay materials are presented in this section. The *ATOM%* column of the EDAX analysis was entered into the Ultimate analysis data base calculation (Chapter2).The Ultimate analysis for each clay material was entered into the Rational analysis data base calculation. The results of all three analyses are included in this appendix.



EDAX ANALYSIS

A-CLAY

Sample A 1

Specimen spectrum,
ACD1

FILENAME: ACD1
LIVETIME(spec.)= 200

ENERGY RES AREA
1.6 84.06 114853
TOTAL AREA= 287104

FIT INDEX= .82

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.185	.087
MgK	2	.426	.109
AlK	2	24.010	.187
SiK	2	23.730	.141
K K	2	1.463	.065
CaK	2	.792	.056
TiK	2	1.537	.077
MnK	2	.044	.071 * < 2 Sigma*
FeK	2	2.737	.113
S K	0	.360	.044

... [3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: ACD1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 .987	.147	.133	Na2O1	.198 .004
MgK	2 1.005	.334	.284	Mg1O1	.553 .009
AlK	2 .933	20.241	15.550	Al2O3	38.247 .492
SiK	2 .759	24.585	18.140	Si1O2	52.591 .571
K K	2 .991	1.161	.615	K 2O1	1.399 .019
CaK	2 .985	.632	.327	Ca1O1	.885 .010
TiK	2 .985	1.227	.531	Ti1O2	2.047 .017
MnK	2 .875	.040	.015	Mn1O1	.051 .000
FeK	2 .892	2.414	.896	Fe2O3	3.451 .028
S K	0 .733	.386	.249	S 1O1	.578 .008
O K	0 .000	48.834	63.260		2.000
TOTAL		100.001	100.000	100.001	1.162

EDAX ANALYSIS

A-CLAY

SampleA2Specimen spectrum,
ACD2

FILENAME: ACD2

LIVETIMEC(spec.)= 200

ENERGY	RES	AREA
1.4	83.41	117362
TOTAL AREA=		191190

FIT INDEX= .67

ELMT		APP.CONC	ERRORCWT%)
NaK	2	.140	.068
MgK	2	.273	.084
AlK	2	15.228	.147
SiK	2	'14.63'1	.1'11
K K	2	1.129	.055
CaK	2	.663	.049
TiK	2	1.37'1	.069
MnK	2	.D39	.061* < 2 Sigma*
FeK	2	2.282	.1'0'1
S K	0	.293	.036

... C 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM=.00 COSINE=1.000

Spectrum: ACD2

Last elmt by STOICH., NORMALISED

ELMT	ZAF	%ELMT	ATOM.%		%OXIDE	FORMULA
NaK	2	.967	.177	Na20'1	.238	.005
MgK	2	.989	.336	Mg'101	.557	.009
AlK	2	.922	20.093	Al203	37.966	.493
SiK	2	.756	23.546	Si102	50.370	.555
K K	2	.995	1.380	K 201	1.663	.023
CaK	2	.988	.8'17	Ca101	1.144	.014
TiK	2	.987	1.690	Ti'102	2.820	.023
MnK	2	.875	.055	Mn'101	.071	.001
FeK	2	.893	3.1'12	Fe203	4.449	.037
S K	0	.738	.483	S 101	.724	.010
0 K	0	.000	48.3'12			2.000
TOTAL		100.001	100.000		100.001	1.171

EDAX ANALYSIS

A-CLAY

Sample D 1

CO calibration,
SCOACD1

FILENAME:SCOACD1

LIVETIME= 200 I/P= 1883 cps

ENERGY	RES	AREA
.2	84.45	113522
6931.1	157.55	162801
TOTAL AREA=		376625 GF= 50.048

Specimen spectrum,
SACD1

FILENAME:SACD1

LIVETIME(spec.)'= 200

ENERGY	RES	AREA
.2	83.60	116211
TOTAL AREA=		243178

FIT INDEX= .55

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.086	.071* < 2 Sigma*
MgK	2	.333	.087
AlK	2	19.636	.156
SiK	2	20.338	.120
K K	2	1.041	.049
CaK	2	.298	.039
TiK	2	-1.302	.061
MnK	2	.025	.052* < 2 Sigma*
FeK	2	1.192	.076

••• C 3 ZAF'SJ

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20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SACD1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 1.011	.083	.074	Na201	.112 .002
MgK	2 1.024	.316	.267	Mg101	.525 .008
AlK	2 .946	20.224	15.398	Al203	38.213 .484
SiK	2 .764	25.920	18.955	Si102	55.447 .596
K K	2 .988	1.026	.539	K 201	1.236 .017
CaK	2 .983	.295	.151	Ca101	.413 .005
TiK	2 .983	1.290	.553	Ti102	2.152 .017
MnK	2 .873	.028	.011	Mn101	.036 .000
FeK	2 .890	1.304	.480	Fe203	1.865 .015
O K	0 .000	49.513	63.571		2.000
TOTAL		100.000	100.000	100.000	1.146

EDAX ANALYSIS

A-CLAY

Sample O2

Specimen spectrum,
SCOACD2FILENAME:SACD2
LIVETIME(spec.)= 200

ENERGY	RES	AREA
.3	83.12	115846
TOTAL AREA=		244409

FIT INDEX= .49

ELMT	APP.CONC	ERROR(WT%)
NaK 2	.034	.070* < 2 Sigma*
MgK 2	.214	.086
AlK 2	19.243	.155
SiK 2	20.955	.121
K K 2	.867	.048
CaK 2	.279	.038
TiK 2	1.324	.061
MnK 2	.005	.052* < 2 Sigma*
FeK 2	1.222	.077

... 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM=.00 COSINE=1.000

Spectrum: SCOACD2

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	1.009	.032	.029	Na2O1	.044 .001
MgK 2	1.024	.203	.172	Mg1O1	.337 .005
AlK 2	.948	19.770	15.040	Al2O3	37.357 .472
SiK 2	.769	26.525	19.381	Si1O2	56.742 .608
K K 2	.987	.855	.449	K 2O1	1.030 .014
CaK 2	.983	.276	.141	Ca1O1	.386 .004
TiK 2	.983	1.311	.562	Ti1O2	2.187 .018
MnK 2	.873	.005	.002	Mn1O1	.007 .000
FeK 2	.890	1.337	.491	Fe2O3	1.911 .015
O K 0	.000	49.686	63.734		2.000
TOTAL		100.000	100.000	100.000	1.138

ULTIMATE ANALYSIS TABLES

A-CLAY

A CLAY A (Unfired)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	18.14	17.51	17.83	17.83	1,071.34	51.47	46.02
Al(Al ₂ O ₃)	15.55	15.56	15.55	7.78	793.25	38.11	34.07
Fe(Fe ₂ O ₃)	0.90	1.16	1.03	0.52	82.19	3.95	3.53
Ti (TiO ₂)	0.53	0.74	0.63	0.63	50.66	2.43	2.18
K (K ₂ O)	0.62	0.74	0.68	0.34	31.86	1.53	1.37
Na (Na ₂ O)	0.13	0.16	0.15	0.07	4.56	0.22	0.20
Ca (CaO)	0.33	0.43	0.38	0.38	21.12	1.01	0.91
Mg (MgO)	0.28	0.29	0.29	0.29	11.55	0.55	0.50
Mn(MnO ₂)	0.02	0.02	0.02	0.02	1.56	0.08	0.07
S (SO ₂)	0.25	0.32	0.28	0.28	13.47	0.65	0.58
OXYGEN	63.26	63.08	63.17				
LOI						11.85	10.60
Total	100.00	100.00	100.00		2,081.57	111.85	100.00

A CLAY D (1200°C)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	18.96	19.38	19.17	19.17	1,152.00	55.72	49.82
Al(Al ₂ O ₃)	15.40	15.04	15.22	7.61	776.17	37.54	33.57
Fe(Fe ₂ O ₃)	0.48	0.49	0.49	0.24	38.74	1.87	1.68
Ti (TiO ₂)	0.55	0.56	0.56	0.56	44.54	2.15	1.93
K (K ₂ O)	0.54	0.45	0.49	0.25	23.27	1.13	1.01
Na (Na ₂ O)	0.07	0.03	0.05	0.03	1.60	0.08	0.07
Ca (CaO)	0.15	0.14	0.15	0.15	8.19	0.40	0.35
Mg (MgO)	0.27	0.17	0.22	0.22	8.85	0.43	0.38
Mn(MnO ₂)	0.01	0.00	0.01	0.01	0.56	0.03	0.02
S (SO ₂)			0.00	0.28	13.47	0.65	0.58
OXYGEN	63.57	63.73	63.65				
LOI						11.85	10.60
Total	100.00	100.00	100.00		2067.39	111.85	100.00

RATIONAL ANALYSIS TABLE

A-CLAY

RATIONAL ANALYSIS (A Clay A)				
FELDSPAR CONVENTION				
MATERIAL	ENTRY	FACTOR	IRESULT	
Total alkalis	1.39	*5.92	/8.22	%Feldspar
Feldspar	8.22	*0.183	1.50	Al ₂ O ₃ in Felds (a)
Feldspar	8.22	*0.647	5.32	SiO ₂ in Felds (b)
Al ₂ O ₃	34.07	"-a"*2.53	182.4	% Clay subst. (c)
Clay subst.	82.4	*0.463	38.15	SiO ₂ in Clay (d)
SiO ₂	46.02	"-(b+d)"	12.55	% Free silica
% WATER IN THE CLAY: % ORGANIC MATTER				
Clay Subst.	82.4	*0.140	/11.53	Loss:H ₂ O in Clay
LOI	10.60	"(-H ₂ O in clay)"	0.00	Loss: CO ₂ etc
MICA CONVENTION				
K ₂ O	1.37	*8.47	111.60	%Potash Mica
Na ₂ O	0.20	*12.32	12.46	%Soda Mica
Potash Mica	11.60	*0.384	4.45	Al ₂ O ₃ in K Mica (e)
Potash Mica	11.60	*0.452	5.24	SiO ₂ in K Mica (f)
Soda Mica	2.46	*0.4	0.98	Al ₂ O ₃ in Na Mica (g)
Soda Mica	2.46	*0.471	1.58	SiO ₂ in Na Mica (h)
Al ₂ O ₃	34.07	-(e+g)*2.53	172.45	%Clay subst.
Clay subst.	72.45	*0.465	33.89	SiO ₂ in Clay (i)
SiO ₂	46.02	"-(f+h+i)"	15.31	%Free Silica

EDAX ANALYSIS

813 Ball Clay

Sample 1 A1

CO calibration.

FILENAME:SC01

SC01

LIVETIME= 200 I/P= 2434 cps

ENERGY	RES	AREA
.3	85.81	112178
6923.2	159.88	210775
TOTAL AREA= 486828 GF= 49.991		

Specimen spectrum,

FILENAME:813A1 FILE DOES NOT EXIST

Spectrum from Analyser, File or Real-time processor: File ?S

Specimen spectrum,

FILENAME:S813A1

SB13A1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
.4	84.16	115484
TOTAL AREA= 279523		

.....
FIT INDEX= .59

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.057	.052* < 2 Sigma*
MgK	2	.398	.067
AlK	2	11.034	.112
SiK	2	22.317	.106
K K	2	1.744	.048
CaK	2	.452	.035
TiK	2	.494	.044
MnK	2	-.029	.044* < 2 Sigma*
FeK	2	1.174	.065
..[2 ZAF'SJ			



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20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SB13A1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 .998	.067	.060	Na2O1	.090 '1.002
MgK	2 1.014	.455	.385	Mg1O1	.754 .012
AlK	2 .940	13.601	10.370	Al2O3	25.699 .324
SiK	2 .824	31.353	22.961	Si1O2	67.071 .717
K K	2 .985	2.050	1.079	K 2O1	2.470 .034
CaK	2 .975	.538	.276	Ca1O1	.752 .009
TiK	2 .978	.585	.251	Ti1O2	.976 .008
MnK	2 .871	.000	.000	Mn1O1	.000 .000
FeK	2 .889	1.531	.561	Fe2O3	2.188 .018
O K	0 .000	49.821	64.055		2.000
TOTAL		100.001	100.000	100.001	1.122

EDAX ANALYSIS

B13 Ball Clay**Sample 1 A2**

Specimen spectrum,
SB13A2

FILENAME: SB13A2

LIVETIME(spec.)= 200

ENERGY RES AREA
.5 84.18 115427
TOTAL AREA= 267184

.....
FIT INDEX= .41

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.067	.05-1 * < 2 Sigma*
MgK	2	.393	.066
AlK	2	-1-1.279	.111
SiK	2	19.977	.101
K K	2	4.815	.048
CaK	2	.349	.034
TiK	2	.651	.046
MnK	2	-.004	.044* < 2 Sigma*
FeK	2	-1.278	.066

..1 2 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SB-13A2

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%		%OXIDE	FORMULA
NaK	2 .993	.082	.074	Na20'1	.111	.002
MgK	2 '1.0'10	.475	.403	Mg'10-1	.787	.0-13
AlK	2 .936	14.689	11.233	Al203	27.756	.352
SiK	2 .812	30.00-1	22.036	Si-102	64.177	.690
K K	2 .987	2.242	1.183	K 201	2.700	.037
CaK	2 .976	.436	.225	Ca'101	.6'10	.007
TiK	2 .979	.8-11	.349	Ti-102	'1.353	.011
MnK	2 .872	.000	.000	Mn-10-1	.000	.000
FeK	2 .889	1.753	.648	Fe203	2.506	.020
0 K	0 .000	49.5'12	63.849			2.000
TOTAL		100.00'1	'100.000		'100.001	1.132

EDAX ANALYSES

S13 *Sail Clay*

Sample 1 01

Specimen spectrum,
S813D1

FILENAME:Se.13AD1

LIVETIME(spec.)= 200

ENERGY RES AREA
.B B5.31 116174

TOTAL AREA= 222152

Peak at 2.62 keV omitted?

FIT INDEX= .52

ELMT	APP.CONC	ERROR(Wr,,)
NaK 2	.144	.060
MgK 2	.396	.077
AlK 2	10.393	.128
SiK 2	24.139	.127
K K 2	1.911	.057
CaK 2	.711	.045
TiK 2	.595	.052
MnK 2	.064	.053* < 2 Sigma*
FeK 2	1.178	.078

•• [2 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: S813D1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	"ELMT	ATOM."	%OXIDE	FORMULA
NaK 2	.993	.162	.145	Na201	.218 .005
MgK 2	1.00B	.437	.371	Mg101	.725 .012
AlK 2	.937	12.335	9.422	Al203	23.308 .294
SiK 2	.B36	32.103	23.552	Si102	6B.675 .735
K K 2	.9B6	2.154	1.135	K 201	2.595 .035
CaK 2	.975	.811	.417	Ca101	1.135 .013
TiK 2	.977	.677	.291	Ti102	1.129 .009
MnK 2	.B71	.0B2	.031	Mn101	.106 .001
FeK 2	.8BB	1.475	.544	Fe203	2.109 .017
0 K 0	.000	49.763	64.093		2.000
TOTAL		.99.999	100.000	99.999	1.120

EDAX ANALYSIS

B13BallClay

Sample 1 02

CO calibration,

FILENAME:SC02

LIVETIME= 200 I/P= 1790 cps

ENERGY	RES	AREA
1.1	83.94	113661
6929.7	157.86	154713
TOTAL AREA=		358002 GF=' 50.032

Specimen spectrum,

FILENAME:SB13D2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.2	82.72	116571
TOTAL AREA=		220938

FIT INDEX= .47

ELMT	APP. CONC	ERROR(WT%)
NaK 2	.112	.061* < 2 Sigma*
MgK 2	.348	.080
AlK 2	9.999	.128
SiK 2	23.326	.127
K K : 2	1.817	.058
CaK 2	2.270	.059
TiK 2	.665"	.054
MnK 2	-.045	.052* < 2 Sigma*
FeK 2	1.256	.078
ClK : 0	.134	.034
S K 0	.339	.035
•• C 2 ZAF'SJ		


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20."00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	.982	.127	.114	Na2O1	.171 .004
MgK 2	1.000	.386	.330	Mg1O1	.640 .010
AlK 2	.932	11.903	9.171	Al2O3	22.491 .288
SiK 2	.839	30.855	22.834	Si1O2	66.005 .714
K K : 2	.991	2.034	1.082	K 2O1	2.451 .034
CaK 2	.977	2.577	1.337	Ca1O1	3.606 .042
TiK 2	.973	.758	.329	Ti1O2	1.265 .010
MnK 2	.870	.000	.000	Mn1O1	.000 .000
FeK 2	.888	1.570	.584	Fe2O3	2.245 .018
ClK : 0	.795	.188	.110	Cl1O2	.357 .003
S K 0	.735	.511	.332	S 1O1	.767 .010
O K 0	.000	49.087	63.777		2.000
TOTAL		99.996	100.000		99.996 1.136

EDAX ANALYSIS

B13 Ball ClaySample 2 A1Specimen spectrum,
B13A1

FILENAME: 8'13A'1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.6	84.52	117692
TOTAL AREA=		162748

Peak at 2.60 keV omitted?
FIT INDEX= .37

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.070	.049* < 2 Sigma*
MgK	2	.248	.06'1
AlK	2	8.'192	.106
SiK	2	4'4. 423	.097
K K	2	'1.472	.048
CaK	2	.305	.035
TiK	2	.406	.045
MnK	2	.040	.046* < 2 Sigma*
FeK	2	'1.0L13	.068
..C 2 ZAF'SJ			

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE='1.000

Spectrum: B13A1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 .988	.119	.107	Na2O1 .160	.003
MgK	2 1.005	.413	.352	Mg1O1 .686	.01-1
AlK	2 .934	'14.673	'1'1.250	Al2O3 27.725	.353
SiK	2 .81'1	29.745	2'1.906	Si1O2 63.63'1	.687
K K	2 .988	2.492	'1.3'19	K 2O1 3.002	.04'1
CaK	2 .975	.524	.270	Ca'1O1 .733	.008
TiK	2 .979	.694	.300	Ti1O2 '1.'157	.009
MnK	2 .872	.077	.029	Mn1O1 .099	.001
FeK	2 .890	-1.963	.727	Fe2O3 2.806	.023
O K	0 .000	49.300	63.74'1		2.000
TOTAL		'100.000	'100.000	'100.000	'1.'138

EDAX ANALYSIS

B13 Ball Clay**Sample 2 A2**

Specimen spectrum,
B13A2

FILENAME: 8'13A2

LIVETIME(spec.)= 200

ENERGY RES AREA
1.5 84.62 117334
TOTAL AREA= 177666

.....
FIT INDEX= .40

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.033	.050* < 2 Sigma*
MgK	2	.262	.064
AlK	2	7.931	.107
SiK	2	17.464	.105
K K	2	1.388	.048
CaK	2	.466	.038
TiK	2	.487	.046
MnK	2	.018	.046* < 2 Sigma*
FeK	2	.952	.067

..[ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.00

Spectrum: B13A2

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 .991	.050	.045	Na2O1	.067 .001
MgK	2 1.009	.393	.334	Mg1O1	.652 .0'10
AlK	2 .938	12.792	9.775	Al2O3	24.171 .305
SiK	2 .832	31.750	23.303	Si1O2	67.920 .727
K K	2 .987	2.128	-1.122	K 2O1	2.564 .035
CaK	2 .975	.723	.372	Ca1O1	1.011 .012
TiK	2 .978	.753	.324	Ti1O2	1.256 .010
MnK	2 .871	.031	.012	Mn1O1	.041 .000
FeK	2 .888	1.621	.598	Fe2O3	2.318 .019
O K	0 .000	49.757	64.115		2.000
TOTAL		99.999	100.000	99.999	1.119

EDAXANALYSIS

B13 Ball ClaySample 2 02Specimen spectrum,
S813D2

FILENAME:S13D2813D2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
.9	85.43	116518
TOTAL-AREA=		216002

FIT INDEX= .49

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.042	.060* < 2 Sigma*
MgK	2	.387	.078
AlK	2	10.807	.128
SiK	2	22.23[1	.122
K K	2	1.80B	.056
CaK	2	1.628	.053
TiK	2	.979	.057
MnK	2	.024	.051* < 2 Sigma*
FeK	2	1.232	.077

.C ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM=0.00 COSINE=1.000

Spectrum: S813D2

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 .983	.048	.044	Na2O1 .065	.001
MgK	2 1.003	.437	.373	Mg1O1 .724	.012
AlK	2 .933	13.114	10.082	Al2O3 24.780	.316
SiK	2 .826	30.446	22.480	Si1O2 65.130	.704
K K	2 .992	2.063	1.094	K 2O1 2.485	.034
CaK	2 .979	1.883	.974	Ca1O1 2.634	.031
TiK	2 .976	1.135	.491	Ti1O2 1.893	.015
MnK	2 .871	.031	.012	Mn1O1 .040	.000
FeK	2 .888	1.570	.583	Fe2O3 2.244	.018
O K	0 .000	49.270	63.867		2.000
TOTAL		99.997	100.000	99.997	1.131

ULTIMATE ANALYSIS

813 Ball Clay .

B13 CLAY A (Sarnole 1) (Unfired)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (5102)	21.91	23.30	22.60	22.60	1,358.53	65.76	61.29
Al (Al2O3)	11.25	9.78	10.51	5.26	536.14	25.95	24.19
Fe (Fe2O3)	0.73	0.60	0.66	0.33	52.87	2.56	2.38
Ti (TiO2)	0.30	0.32	0.31	0.31	24.93	1.21	1.12
K (K2O)	1.32	1.12	1.22	0.61	57.49	2.78	2.59
Na (Na2O)	0.11	0.05	0.08	0.04	2.36	0.11	0.11
Ca (CaO)	0.27	0.37	0.32	0.32	18.01	0.87	0.81
Mg (MgO)	0.35	0.33	0.34	0.34	13.82	0.67	0.62
Mn (MnO2)	0.03	0.01	0.02	0.02	1.78	0.09	0.08
oxygen	63.74	64.12	63.93				
LOI						7.30	6.80
Total	100.00	100.00	100.00		2 065.92	107.30	100.00

B13 CLAY D (sample 1)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (5102)		22.83	11.42	11.42	686.16	65.39	60.94
Al (Al2O3)		9.17	4.59	2.29	233.86	22.29	20.77
Fe (Fe2O3)		0.58	0.29	0.15	23.30	2.22	2.07
Ti (TiO2)		0.33	0.16	0.16	13.14	1.25	1.17
K (K2O)		1.08	0.54	0.27	25.48	2.43	2.26
Na (Na2O)		0.11	0.06	0.03	1.77	0.17	0.16
Ca (CaO)		1.34	0.67	0.67	37.50	3.57	3.33
Mg (MgO)		0.33	0.17	0.17	6.65	0.63	0.59
Mn (MnO2)		0.00	0.00	0.00	0.00	0.00	0.00
Cl (ClO2)		0.11	0.11	0.11	5.67	0.54	0.50
S (SO)		0.33	0.33	0.33	15.87	1.51	1.41
oxygen		63.78	31.89				
LOI						7.30	6.80
Total		100.00	50.22		1,049.41	107.30	100.00

ULTIMATE ANALYSIS

B13 Ball Clay .

B13 CLAY (Sample 2) (Unfired)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (SiO ₂)	22.96	22.04	22.50	22.50	1,352.16	65.62	61.15
Al (Al ₂ O ₃)	10.37	11.23	10.80	5.40	550.88	26.73	24.91
Fe (Fe ₂ O ₃)	0.56	0.65	0.61	0.30	48.36	2.35	2.19
Ti (TiO ₂)	0.25	0.35	0.30	0.30	23.97	1.16	1.08
K (K ₂ O)	1.08	1.18	1.13	0.57	53.27	2.59	2.41
Na (Na ₂ O)	0.06	0.07	0.07	0.03	2.08	0.10	0.09
Ca (CaO)	0.28	0.23	0.25	0.25	14.05	0.68	0.64
Mg (MgO)	0.39	0.40	0.39	0.39	15.88	0.77	0.72
Mn (MnO ₂)	0.00	0.00	0.00	0.00	0.00	0.00	0.00
LOI						7.30	6.80
Total	100.00	100.00	100.00		2 060.64	107.30	100.00

B13 CLAY (Sample 2) (1200oC)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (SiO ₂)	23.55	22.48	23.02	23.02	1,383.26	66.89	62.34
Al (Al ₂ O ₃)	9.42	10.08	9.75	4.88	497.30	24.05	22.41
Fe (Fe ₂ O ₃)	0.54	0.58	0.56	0.28	44.97	2.17	2.03
Ti (TiO ₂)	0.29	0.49	0.39	0.39	31.24	1.51	1.41
K (K ₂ O)	1.14	1.09	1.11	0.56	52.49	2.54	2.37
Na (Na ₂ O)	0.15	0.04	0.09	0.05	2.93	0.14	0.13
Ca (CaO)	0.42	0.97	0.70	0.70	39.02	1.89	1.76
Mg (MgO)	0.37	0.37	0.37	0.37	14.99	0.72	0.68
Mn (MnO ₂)	0.03	0.01	0.02	0.02	1.87	0.09	0.08
LOI						7.30	6.80
Total	100.00	100.00	100.00		2 068.07	107.30	100.00

RATIONAL ANALYSIS

813 8a/I Clay .

RATIONAL ANALYSIS (813 Clay. A SAMPLE 1)			
FELDSPAR CONVENTION			
MATERIAL	NTRY	FACTOR	IREULTI
ITotal alkalis	2.70	*5.92	115.98 1%Feldspar
Feldspar	15.98	*0.183	2.92 Al2O3 in Felds (a)
Feldspar	15.98	*0.647	10.34 SiO2 in Felds (b)
Al2O3	24.19	"-a"*2.53	153.80 1% Clay subst. (c)
Clay subst.	53.80	*0.463	24.91 SiO2 in Clay (d)
SiO2	61.29	"-(b+d)"	126.04 1% silica
% WATER IN THE CLAY: % ORGANIC MATIER			
Clay Subst.	3.80	*0.140	17.53 ILoss:H2O in Clay
LOI	.80	"(-H2O in clay)"	0 Iloss C02 etc
MICA CONVENTION			
K2O	2.53	*8.47	121.43 1%Potash Mica
Na2O	0.10	*12.32	11.23 1%Soda Mica
Potash Mica	21.43	*0.384	8.23 Al2O3 in K Mica (e)
Potash Mica	21.43	*0.452	9.69 SiO2 in K Mica (f)
Soda Mica	1.23	*0.4	0.49 Al2O3 in Na Mica (g)
Soda Mica	1.23	*0.471	0.58 SiO2 in Na Mica (h)
Al2O3	23.62	" - (e+g)*2.53	137.691%Clay subst.
Clay subst.	37.69	*0.465	17.53 SiO2 in Clay (i)
SiO2	59.84	"-(f+h+i)"	32.05 1% Free Silica

EDAX ANALYSIS

G-ClaySample A1

The data in Sample A1 and A2 was calculated using the Apparent concentration and not the stoichiometric analyses. The oxide weight was calculated for each molecule of material in the analysis and the total brought to a percentage.

Specimen spectrum,

FILENAME: SCCA'1

LIVETIME(spec.)= :200

ENERGY RES AREA
 .3 82.98 117598
 TOTAL AREA= 182472

Peak at 2.30 keV omitted?
 FIT INDEX= '1.20

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.194	.065
MgK	2	.307	.083
AlK	2	11.502	.137
SiK	2	19.861	.122
K K	:2	2.056	.059
CaK	2	.299	.041
TiK	2	.600	.052
MnK	2	.038	.050* < 2 Sigma*
FeK	2	.508	.065

••• C 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

All elmts analysed

ELMT	ZAF	%ELMT	ATOM.%
NaK	2 1.460	.133	.423
MgK	2 1.332	.230	.695
AlK	:2 1.138	10.105	27.480
SiK	2 .802	24.784	64.734
K K	:2 .905	2.272	4.263
CaK	:2 .901	.332	.608
TiK	2 .936	.641	.982
MnK	2 .859	.044	.058
FeK	:2 .882	.576	.756
TOTAL		39.116	100.000

EDAX ANALYSIS

e-c/ay

SampleA2

Specimen spectrum,

FILENAME:SCCA2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
.2	83.35	118177
TOTAL AREA= 176572		

.....

FIT INDEX= 1.25

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.235	.064
MgK	2	.201	.080
AlK	2	11.336	.135
SiK	2	18.822	.119
K K	2	2.124	.059
CaK	2	.198	.039
TiK	2	.386	.049
MnK	2	-.006	.050* < 2 Sigma*
FeK	2	.484	.067

.... C 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM=F 00 COSINE=1.000

Spectrum:

All elmts analysed

ELMT		ZAF	%ELMT	ATOM.%
NaK	2	1.475	.159	.531
MgK	2	1.339	.150	.474
AlK	2	1.146	9.895	28.126
SiK	2	.798	23.596	64.422
K K	2	.904	2.351	4.611
CaK	2	.898	.221	.422
TiK	2	.935	.412	.660
MnK	2	.860	.000	.000
FeK	2	.882	.548	.753
TOTAL			37.332	100.000

EDAX ANALYSIS

C-ClaySample 01

CO calibration,

FILENAME:SC02

LIVETIME= 200 I/P= 1823 cp

ENERGY	RES	AREA
1.3	84.88	114315
6928.8	157.53	157210
TOTAL AREA=		364511 GF=' 50.024

Specimen spectrum,

FILENAME:SCCD1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.4	83.74	116832
TOTAL AREA=		226914

FIT INDEX= .89

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.241	.065
MgK	2	.188	.080
AlK	2	12.890	.139
SiK	2	23.464	-127
K K	2	2.373	.061
CaK	2	.062	.038* < 2 Sigma*
TiK	2	.588	.054
MnK	2	.004	.053* < 2 Sigma*
FeK	2	.828	.071
... [3 ZAF'SJ			

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE='1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 1.011	.256	.229	Na2O1	.345 .007
MgK	2 1.020	.198	.168	Mg1O1	.329 .005
AlK	2 .948	14.625	11.132	Al2O3	27.634 .348
SiK	2 .818	30.831	22.541	Si1O2	65.954 .706
K K	2 .985	2.592	1.361	K 2O1	3.122 .043
CaK	2 .972	.068	.035	Ca1O1	.096 .001
TiK	2 .977	.648	.278	Ti1O2	1.080 .009
MnK	2 .871	.005	.002	Mn1O1	.007 .000
FeK	2 .888	1.003	.369	Fe2O3	1.434 .012
O K	0 .000	49.774	63.887		2.000
TOTAL		100.000	100.000	100.000	1.131

EDAX ANALYSIS

*C-Clay*Sample D2

Specimen spectrum;

FILENAME:SCCD2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.5	83.19	116061
TOTAL AREA=		234406

FIT INDEX= .55

ELMT		APP.CONC	ERROR(WT%)	
NaK	2	.185	.063	
MgK	2	.120	.080*	< 2 Sigma*
AlK	2	11.205	.135	
SiK	2	26.932	.134	
K K	2	2.142	.059	
CaK	2	.069	.038*	< 2 Sigma*
TiK	2	.502	.052	
MnK	2	-.006	.053*	<, 2 Sigma*
FeK	2	.446	.066	
. -I 2 ZAF'SJ				

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 1.018	.191	.170	Na2O1	.258 .005
MgK	2 1.027	.123	.103	Mg1O1	.204 .003
AlK	2 .954	12.343	9.346	Al2O3	23.323 .291
SiK	2 .845	33.513	24.374	Si1O2	71.690 .758
K K	2 .981	2.295	1.199	K 2O1	2.764 .037
CaK	2 .970	.075	.038	Ca1O1	.105 .001
TiK	2 .975	.541	.231	Ti1O2	.903 .007
MnK	2 .870	.000	.000	Mn1O1	.000 .000
FeK	2 .887	.528	.193	Fe2O3	.755 .006
0 K	0 .000	50.393	64.345		2.000
TOTAL		100.002	100.000	100.002	1.108

ULTIMATE ANALYSIS

c-Clay

C CLAY A (Unfired)							
	Atomic % of Elements			Molecular content *		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (5102)	23.32	23.26	23.29	23.29	1,399.73	68.06	63.90
Al (Al2O3)	9.90	10.16	10.03	5.02	511.53	24.87	23.35
Fe (Fe2O3)	0.27	0.27	0.27	0.14	21.55	1.05	0.98
Ti (TiO2)	0.35	0.24	0.30	0.30	23.57	1.15	1.08
K (K2O)	1.54	1.66	1.60	0.80	75.36	3.66	3.44
Na (Na2O)	0.15	0.19	0.17	0.09	5.27	0.26	0.24
Ca (CaO)	0.22	0.15	0.19	0.19	10.38	0.50	0.47
Mg (MgO)	0.25	0.17	0.21	0.21	8.46	0.41	0.39
Mn (MnO2)	0.02	0.00	0.01	0.01	0.87	0.04	0.04
oXYGEN	63.97	63.89	63.93				
LOI						6.50	6.10
Total	99.99	99.99	99.99		2,056.72	106.50	100.00

C CLAY D (12000C)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (5102)	22.54	24.37	23.46	23.46	1,409.71	68.81	64.61
Al (Al2O3)	11.13	9.35	10.24	5.12	522.19	25.49	23.93
Fe (Fe2O3)	0.37	0.19	0.28	0.14	22.42	1.09	1.03
Ti (TiO2)	0.28	0.23	0.25	0.25	20.33	0.99	0.93
K (K2O)	1.36	1.20	1.28	0.64	60.29	2.94	2.76
Na (Na2O)	0.23	0.17	0.20	0.10	6.18	0.30	0.28
Ca (CaO)	0.04	0.04	0.04	0.04	2.05	0.10	0.09
Mg (MgO)	0.17	0.10	0.14	0.14	5.46	0.27	0.25
Mn (MnO2)	0.00	0.00	0.00	0.00	0.09	0.00	0.00
oXYGEN	63.89	64.35	64.12				
LOI						6.50	6.10
Total	100.00	100.00	100.00		2,048.72	106.50	100.00

RATIONAL ANALYSIS**C-Clay**

RATIONAL ANALYSIS (C CLAY A)				
FELDSPAR CONVENTION				
MATERIAL	ENTRY	FACTOR	RESULT	
frotaI alkalis	3.68	*5.92	121.79	I%Feldspar
Feldspar	21.79	*0.183	3.99	Al2O3 in Felds (a)
Feldspar	21.79	*0.647	14.10	SiO2 in Felds (b)
Al2O3	23.35	"-a"*2.53	148.99	I% Clay subst. (c)
Clay subst.	48.99	*0.463	22.68	SiO2 in Clay (d)
SiO2	63.90	"-(b+d)"	127.12	I% silica
% WATER IN THE CLAY: % ORGANIC MATTER				
Clay Subst.	48.99	*0.140	16.86	ILoss:H2O in Clay
LOI	6.10	"(H2Oinclay)"	0.00	ILoss: CO2 etc
MICA CONVENTION				
K2O	3.44	*8.47	29.14	I%Potash Mica
Na2O	0.24	*12.32	12.96	I% soda Mica
Potash Mica	29.14	*0.384	11.19	Al2O3 in K Mica (e)
Potash Mica	29.14	*0.452	13.17	SiO2 in K Mica (f)
Soda Mica	2.96	*0.4	1.18	Al2O3 in Na Mica (g)
Soda Mica	2.96	*0.471	1.39	SiO2 in Na Mica (h)
Al2O3	23.35	"(e+g)*2.53	127.78	I%Clay subst.
Clay subst.	27.78	*0.465	12.92	SiO2 in Clay (i)
SiO2	63.90	"-(f+h+i)"	136.42	I%Free Silica

EDAX ANALYSIS

*Masse/sy*Sample A1

The data in Sample A1 and A2 was calculated using the Apparent concentration and not the stoichiometric analyses. The oxide weight was calculated for each molecule of material in the analysis and the total brought to a percentage.

Specimen spectrum,

FILENAME: SMA1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.1	83.65	116411
TOTAL AREA= 231603		

FIT INDEX= .80

ELMT		APP.CONG	ERROR(WT%)
NaK	2	.23'1	.065
MgK	2	.152	.080* < 2 Sigma*
AlK	2	13.937	.138
SiK	2	20.972	.118
K K	2	2.795	.06:2
CaK	2	.0'18	.037* < 2 Sigma*
TiK	2	.822	.054
MnK	2	.026	.049* < 2 Sigma*
FeK	2	.7'17	.068

.••E 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

SpectrLlm:

All elmts analysed

ELMT		ZAF	%ELMT	ATOM.%
NaK	2	1.442	.160	.456
MgK	2	1.320	.115	.3'10
AlK	2	1.136	12.266	29.692
SiK	2	.784	26.749	62.'192
K K	2	.909	3.076	5.139
CaK	2	.900	.020	.033
TiK	2	.939	.875	1.193
MnK	2	.861	.031	.036
FeK	2	.883	.8'11	.949
TOTAL			44.'105	100.000

EDAX ANALYSIS

*Masse/sy*SampleA2Specimen spectrum,
CO calibration,

FILENAME:

FILENAME: SCO1

LIVETIME= 200 I/P= 1916 cps

ENERGY	RES	AREA
1.0	84.48	113327
6929.2	157.56	165063
TOTAL AREA=		383240 GF= 50.029

Specimen spectrum,

FILENAME:SMA2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.1	83.47	116548
TOTAL AREA=		220401

FIT INDEX= '1.04

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.216	.063
MgK	2	.182	.078
AlK	2	'13.355	.135
SiK	2	'19.569	.115
K K	2	2.7'10	.061
CaK	2	.008	.036* 0(2 Sigma*
TiK	2	.494	.050
MnK	2	-.020	.050* < 2 Sigma*
FeK	2	.945	.070

••• C 3 ZAF'SJ

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20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

All elmts analysed

ELMT		ZAF	%ELMT	ATOM.%
NaK	2	'1.430	.151	.453
MgK	2	1.312	.139	.393
AlK	2	'1.130	'11.820	30.164
SiK	2	.778	25.151	61.646
K K	2	.908-	2.983	5.253
CaK	2	.899	.009	.016
TiK	2	.939	.526	.756
MnK	2	.862	.000	.000
FeK	2	.884	'1.069	1.318
TOTAL			4'1.849	'100.000

EDAX ANALYSIS

*Moss Clay*Sample 01

CO calibration,

.FILENAME: SCO1

LIVETIME= 200 I/P= 1908 cps

ENERGY	RES	AREA
.8	84.26	113346
6929.5	158.72	165794
TOTAL AREA=		381636 GF= 50.033

Specimen spectrum,

FILENAME: SMD1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
.9	83.37	116150
TOTAL AREA=		232820

FIT INDEX= 3.33

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.226	.064
MgK	2	.177	.078
AlK	2	13.964	.137
SiK	2	19.755	.116
K K	2	3.007	.064
CaK	2	.011	.038* < 2 Sigma*
TiK	2	.808	.055
MnK	2	.552	.063
FeK	2	.953	.074

... [3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE='1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 .994	.255	.230	Na2O1	.343 .007
MgK	2 1.008	.196	.168	Mg1O1	.325 .005
AlK	2 .939	16.664	12.818	Al2O3	31.488 .405
SiK	2 .795	27.841	20.568	Si1O2	59.558 .650
K K	2 .990	3.401	1.805	K 2O1	4.097 .057
CaK	2 .973	.013	.006	Ca1O1	.018 .000
TiK	2 .980	.924	.400	Ti1O2	1.541 .013
MnK	2 .873	.709	.268	Mn1O1	.915 .008
FeK	2 .890	1.200	.446	Fe2O3	1.716 .014
0 K	0 .000	48.798	63.291		2.000
TOTAL		100.000	100.000	rqn.coo	1.160

EDAX ANALYSIS

Masse/sy

Sample D2

Specimen spectrum,

FILENAME:SMD2

LIVETIME{spec.}= 200

ENERGY RES AREA
 1.2 83.24 117204
 TOTAL AREA= 202795

FIT INDEX= .66

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.183	.058
MgK	2	.119	.072* < 2 Sigma*
AlK	2	11.556	.126
SiK	2	17.398	.108
K K	2	2.817	.061
CaK	2	.006	.036* < 2 Sigma*
TiK	2	.615	.051
MnK	2	-.004	.052* < 2 Sigma*
FeK	2	.835	.072

••[2 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2	1.005	.217	.325	Na2O1 .007
MgK	2	1.016	.132	.256	Mg1O1 .004
AlK	2	7.45	12.382	30.508	Al2O3 .391
SiK	2	.803	21.079	61.214	Si1O2 .665
K K	2	.989	1.990	4.529	K 2O1 .063
CaK	2	.970	.005	.012	Ca:1O1 .000
TiK	2	.977	.359	1.386	Ti1O2 .011
MnK	2	.872	.000	.000	Mn1O1 .000
FeK	2	.889	.459	1.772	Fe2O3 .014
O K	0	.000	63.378		2.000
TOTAL		100.003	100.000	100.003	1.156

••[2 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

ULTIMATE ANALYSIS**Moss Clay**

MOSS CLAY A (UNFIRED)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (SiO ₂)	22.54	22.39	22.47	22.47	1,350.15	65.39	61.67
Al (Al ₂ O ₃)	10.76	10.96	10.86	5.43	553.86	26.83	25.30
Fe (Fe ₂ O ₃)	0.34	0.48	0.41	0.21	32.72	1.58	1.49
Ti (TiO ₂)	0.43	0.27	0.35	0.35	27.97	1.35	1.28
K (K ₂ O)	1.86	1.91	1.89	0.94	88.78	4.30	4.06
Na (Na ₂ O)	0.17	0.16	0.17	0.08	5.12	0.25	0.23
Ca (CaO)	0.01	0.01	0.01	0.01	0.56	0.03	0.03
Mg (MgO)	0.11	0.14	0.13	0.13	5.04	0.24	0.23
Mn (MnO ₂)	0.01	0.00	0.01	0.01	0.43	0.02	0.02
oxygen	63.76	63.67	63.72				
LOI						6.04	5.70
Total	99.99	99.99	99.99		2 064.62	106.04	100.00
MOSS CLAY D(1200oC)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (SiO ₂)	20.57	21.08	20.82	20.82	1,251.49	60.32	56.88
Al (Al ₂ O ₃)	12.82	12.38	12.60	6.30	642.60	30.97	29.21
Fe (Fe ₂ O ₃)	0.45	0.46	0.45	0.23	36.11	1.74	1.64
Ti (TiO ₂)	0.40	0.36	0.38	0.38	30.32	1.46	1.38
K (K ₂ O)	1.81	1.99	1.90	0.95	89.37	4.31	4.06
Na (Na ₂ O)	0.23	0.22	0.22	0.11	6.93	0.33	0.31
Ca (CaO)	0.01	0.01	0.01	0.01	0.31	0.01	0.01
Mg (MgO)	0.17	0.13	0.15	0.15	6.05	0.29	0.27
Mn (MnO ₂)	0.27	0.00	0.13	0.13	11.64	0.56	0.53
oxygen	63.29	63.38	63.33				
LOI						6.04	5.70
Total	100.00	100.00	100.00		2 074.82	106.04	100.00

RATIONAL ANALYSIS

Moss Clay

RATIONAL ANALYSIS (Moss clay A)				
FELDSPAR CONVENTION				
MATERIAL	ENTRY	FACTOR	RESULT	1
rrotal alkalis	4.29	*5.92	125.40	l%Feldspar
Feldspar	25.40	*0.183	4.65	Al ₂ O ₃ in Felds (a)
Feldspar	25.40	*0.647	16.43	SiO ₂ in Felds (b)
Al ₂ O ₃	25.30	"-a"*2.53	152.25	1% Clay subst. (c)
Clay subst.	52.27	*0.463	24.20	SiO ₂ in Clay (d)
SiO ₂	61.67	"-(b+d)"	121.04	1% silica
% WATER IN THE CLAY: % ORGANIC MATTER				
Clay Subst.	52.27	*0.140	17.31	lLoss:H ₂ O in Clay
LOr	5.70	"(H ₂ Oinclay)"	0.00	lLoss: CO ₂ etc
MICA CONVENTION				
K ₂ O	4.06	*8.47	134.39	lPotash Mica
Na ₂ O	0.23	*12.32	12.83	lSoda Mica
Potash Mica	34.39	*0.384	13.21	Al ₂ O ₃ in K Mica (e)
Potash Mica	34.39	*0.452	15.54	SiO ₂ in K Mica (f)
Soda Mica	2.83	*0.4	1.13	Al ₂ O ₃ in Na Mica (g)
Soda Mica	2.83	*0.471	1.33	SiO ₂ in Na Mica (h)
Al ₂ O ₃	25.30	"(e+g)*2.53	127.73	[Clay subst.
Clay subst.	27.73	*0.465	12.90	SiO ₂ in Clay (i)
SiO ₂	61.67	"-(f+h+i)"	131.90	lFree Silica

EDAX ANALYSIS

Pxx Ball Clay .

Sample A1

CO calibration, FILENAME:SC02
 PXXA1 LIVETIME= 200 I/P= 1650 cps
 ENERGY RES AREA
 1.2 88.54 113706
 6929.6 158.13 141690
 TOTAL AREA= 329915 GF= 50.030

Specimen spectrum, FILENAME:PXXA1
 PXXA1 LIVETIMECspec.)= 200
 ENERGY RES AREA
 1.4 86.45 117266
 TOTAL AREA= 178083

FIT INDEX= .50

ELMT	APP.CONC	ERRORCWT%
NaK 2	.104	.068* < 2 Sigma*
MgK 2	.288	.084
AlK 2	14.790	.147
SiK 2	17.843	.119
K K 2	1.942	.059
CaK 2	.139	.039
TiK 2	.544	.053
MnK 2	-.016	.052* < 2 Sigma*
FeK 2	.586	.068

... [3 ZAF'SJ



20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

SpectrLlm: PXXA1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	1.023	.122	.109	.164	Na2O1 .003
MgK 2	1.032	.335	.283	.556	Mg101 .009
AlK 2	.952	18.665	14.203	35.269	Al2O3 .448
SiK 2	.781	27.429	20.046	58.676	Si102 .632
K K 2	.986	2.365	1.242	2.849	K 201 .039
CaK 2	.974	.172	.088	.240	Ca101 .003
TiK 2	.978	.668	.286	1.114	Ti102 .009
MnK 2	.872	.000	.000	.000	Mn101 .000
FeK 2	.889	.792	.291	1.132	Fe203 .009
0 K 0	.000	49.452	63.452		2.000
TOTAL		100.000	100.000	100.000	1.152

EDAX ANALYSIS

*Pxx Ball Clay*SampleA2Specimen spectrum,
PXXA1

FILENAME:PXXA2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.3	85.14	117090
TOTAL AREA= 178198		

FIT INDEX= .55

ELMT	APP.CONC	ERROR(WT%)
NaK 2	.108	.069* < 2 Sigma*
MgK 2	.199	.085
AlK 2	15.074	.149
SiK 2	17.447	.118
K K 2	2.004	.059
CaK 2	.136	.038
TiK 2	.492	.051
MnK 2	.029	.052* < 2 Sigma*
FeK 2	.591	.067

... [3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM=0.00 COSINE="1.000

Spectrum: PXXA1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	1.023	.128	.114	Na2O1	.172 .004
MgK 2	1.032	.232	.196	MgO1	.385 .006
AlK 2	.953	19.102	14.543	Al2O3	36.094 .459
SiK 2	.778	27.087	19.807	SiO2	57.944 .625
K K 2	.986	2.454	1.289	K2O1	2.956 .041
CaK 2	.974	.169	.087	CaO1	.237 .003
TiK 2	.978	.608	.261	TiO2	1.011 .008
MnK 2	.872	.040	.015	MnO1	.052 .000
FeK 2	.889	.802	.295	Fe2O3	1.147 .009
O K 0	.000	49.378	63.393		2.000
TOTAL		100.000	100.000	100.000	1.155

EDAX ANALYSIS

Pxx Ball Clay

Sample 0 1

CO calibration,

FILENAME:SC02

LIVETIME= 200 '1/P= 1616 cps

ENERGY	RES	AREA
1.5	86.12	113918
6929.2	158.96	138934
TOTAL AREA=		323234 GF= 50.025

Specimen spectrum,
PXXD

FILENAME:PXXD

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.3	82.91	116118
TOTAL AREA=		226015

FIT INDEX= .52

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.186	.079
MgK	2	.679	.101
AlK	2	17.981	.168
SiK	2	22.884	.136
K K	2	3.349	.073
CaK	2	•-/22	.050
TiK	2	.807	.060
MnK	2	.031	.055* < 2 Sigma*
FeK	2	1.012	.080

...[3 ZAF/SJ



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20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: PXXD

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 '1.0'10	•'170	.153	Na20'1	.230 .005
MgK	2 '1.022	.6'16	.524	Mg'10'1	1.021 .0'17
AlK	2 .94'1	17.708	'13.574	Al203	33.46'1 .430
SiK	2 .786	26.986	19.867	Si102	57.727 .629
K K	2 .990	3.'132	'1.657	K 20'1	3.773 .052
CaK	2 .973	.687	.354	Ca101	.96'1 .0'11
TiK	2 .976	.766	.331	Ti102	'1.277 .0'10
MnK	2 .872	.033	.0'13	Mn101	.043 .000
FeK	2 .889	'1.055	.391	Fe203	'1.508 .0'12
0 K	0 .000	48.848	63.'138		2.000
TOTAL		'100.000	'100.000	'100.000	1.168

EDAX ANALYSIS

Pxx Ball Clay

Sample 02

Specimen spectrum,
PXXD

FILENAME:PXXD2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.4	84.48	115634
TOTAL AREA=		273219

FIT INDEX= '1.00

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.218	.078
MgK	2	.900	•'10'1
AlK	2	'17.429	•'165
SiK	2	21.042	•'13'1
K K	2	2.198	.072
CaK	2	8.965	•'105
TiK	2	1.026	.070
MnK	2	-.017	.071* < 2 Sigma*
FeK	2	'1.846	.106
...[3 ZAF'SJ			

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: PXXD

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2	.960	.197	Na20'1	.265 .006
MgK	2	.983	.795	Mg'10'1	1.3'17 .022
AlK	2	.912	'16.57'1	Al203	31.3'12 .42'1
SiK	2	.784	23.262	Si'102	49.762 .567
K K	2	'1.0'16	1.876	K 20'1	2.260 .033
CaK	2	.992	7.839	Ca10'1	10.969 .134
TiK	2	.966	•92'1	Ti'102	1.536 .0'13
MnK	2	.869	.000	Mn'10'1	.000 .000
FeK	2	.888	'1.804	Fe203	2.579 .022
O K	0	.000	46.736		82.153 2.000
TOTAL		'100.001	100.000	'100.00'1	1.218

ULTIMATE ANALYSIS

Pxx Ball Clay .

PXX BALL CLAY A (Unfired)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (5102)	20.05	19.81	19.93	19.93	1,197.58	58.30	53.29
Al (Al2O3)	14.20	14.54	14.37	7.19	733.02	35.69	32.62
Fe (Fe2O3)	0.29	0.29	0.29	0.15	23.30	1.13	1.04
Ti (TiO2)	0.29	0.26	0.27	0.27	21.85	1.06	0.97
K (K2O)	1.24	1.29	1.27	0.63	59.61	2.90	2.65
Na (Na2O)	0.11	0.11	0.11	0.06	3.46	0.17	0.15
Ca (CaO)	0.09	0.09	0.09	0.09	4.91	0.24	0.22
Mg (MgO)	0.28	0.20	0.24	0.24	9.65	0.47	0.43
Mn (MnO2)	0.00	0.02	0.01	0.01	0.65	0.03	0.03
oxygen	63.45	63.39	63.42				
LOI						9.40	8.60
Total	100.00	100.00	100.00		2,054.03	109.40	100.01

PXX BALL CLAY 0 (12000C)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (5102)	19.87	17.62	18.74	18.74	1,126.51	53.68	49.07
Al (Al2O3)	13.57	13.07	13.32	6.66	679.40	32.37	29.59
Fe (Fe2O3)	0.39	0.69	0.54	0.27	43.01	2.05	1.87
Ti (TiO2)	0.33	0.41	0.37	0.37	29.56	1.41	1.29
K (K2O)	1.66	1.02	1.34	0.67	63.07	3.01	2.75
Na (Na2O)	0.15	0.18	0.17	0.08	5.19	0.25	0.23
Ca (CaO)	0.35	4.16	2.26	2.26	126.67	6.04	5.52
Mg (MgO)	0.52	0.70	0.61	0.61	24.56	1.17	1.07
Mn (MnO2)	0.01	0.00	0.01	0.01	0.56	0.03	0.02
oxygen	63.14	62.15	62.65				
LOI						9.40	8.60
Total	100.00	100.00	100.00		2,098.55	109.40	100.01

NB The Ca is very high in this spectrum.

RATIONAL ANALYSIS

Pxx Ball Clay .

RATIONAL ANALYSIS (PXX Ball Clay A)			
FELDSPAR CONVENTION			
MATERIAL	ENTRY	FACTOR	RESULT
rrotal alkalis	2.80	*5.92	116.58 I%Feldspar
Feldspar	16.58	*0.183	3.03 Al ₂ O ₃ in Felds (a)
Feldspar	16.58	*0.647	10.73 SiO ₂ in Felds (b)
Al ₂ O ₃	32.62	"-a"*2.53	174.85 1% Clay subst. (c)
Clay subst.	74.85	*0.463	34.66 SiO ₂ in Clay (d)
SiO ₂	53.29	"-(b+d)"	17.91 1% Free silica
% WATER IN THE CLAY: % ORGANIC MATTER			
Clay Subst.	24.94	*0.140	/10.48 ILoss:H ₂ O in Clay (e)
LOI	8.60	"-(e)"	0 ILoss: CO ₂ etc
MICA CONVENTION			
K ₂ O	2.75	*8.47	/23.29 IPotash Mica
Na ₂ O	0.23	*12.32	12.83 ISoda Mica
Potash Mica	23.29	*0.384	8.94 Al ₂ O ₃ in K Mica (e)
Potash Mica	23.29	*0.452	10.53 SiO ₂ in K Mica (f)
Soda Mica	2.83	*0.4	1.13 Al ₂ O ₃ in Na Mica (g)
Soda Mica	2.83	*0.471	1.33 SiO ₂ in Na Mica (h)
Al ₂ O ₃	32.62	"(e+g)*2.53	/57.03 [Clay subst.
Clay subst.	57.03	*0.465	26.52 SiO ₂ in Clay (i)
SiO ₂	53.29	"-(f+h+i)"	114.91/Free Silica

EDAX ANALYSIS

*Western Province Ball Clay*Sample 1 A 1

CO calibration,

FILENAME: SCQZ

LIVETIME= 200 I/P= 1841 cps

ENERGY	RES	AREA
.1	83.79	113348
6932.8	156.88	158655
TOTAL AREA=		368138 GF= 50.061

Specimen spectrum,

FILENAME:SWPBCA1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
.5	82.77	118332
TOTAL AREA=		173057

FIT INDEX= .42

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.037	.060* < 2 Sigma*
MgK	2	.292	.074
AlK	2	13.080	.130
SiK	2	14.619	.103
K K	2	.778	.044
CaK	2	.106	.033
TiK	2	.856	.054
MnK	2	-.028	.047* < 2 Sigma*
FeK	2	.911	.070
...[3 ZAF'SJ			


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20.00 kV TILT= .00 ELEV=40.0o AZIM= .00 COSINE=1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 '1.008	.052	.047	Na2O1 .070	.001
MgK	2 '1.023	.400	.338	Mg1O1 .663	.011
AlK	2 .944	'19.433	'14.792	Al2O3 ' 36.7'19	.465
SiK	2 .771	26.606	'19.452	Si1O2 56.9'15	.611
K K	2 .987	1.105	.581	K 2O1 '1.332	.018
CaK	2 .982	.151	.078	Ca1O1 .2'12	.002
TiK	2 .983	'1.222	.524	Ti'1O2 2.038	.016
MnK	2 .873	.000	.000	Mn1O1 .000	.000
FeK	2 .890	'1.435	.528	Fe2O3 2.052	.017
O K	0 .000	49.596	63.66'1		2.000
TOTAL		'100.000	'100.000	'100.000	'1.142

EDAX ANALYSIS

Western Province Ball Clay .

Sample 1 A 2

Specimen spectrum,

FILENAME:SWPBCA2

LIVETIME(spec.)= 200

ENERGY RES AREA
 .2 83.43 117339
 TOTAL AREA= 193750

FIT INDEX= .24

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.063	.064* < 2 Sigma*
MgK	2	.334	.080
AlK	2	14.850	.139
SiK	2	17.156	.111
K K	2	.853	.045
CaK	2	.124	.035
TiK	2	.750	.053
MnK	2	-.005	.048* < 2 Sigma*
FeK	2	.954	.069

••• ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

SpectrLlm:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	1.014	.076	.068	.102	Na2O1 .002
MgK	1.026	.398	.335	.659	Mg1O1 .011
AlK	.946	19.198	14.582	36.276	Al2O3 .458
SiK	.774	27.132	19.794	58.040	Si1O2 .621
K K	.986	1.058	.555	1.275	K 2O1 .017
CaK	.981	.154	.079	.216	Ca1O1 .002
TiK	.982	.934	.400	1.558	Ti1O2 .013
MnK	.873	.000	.000	.000	Mn1O1 .000
FeK	.890	1.311	.481	1.875	Fe2O3 .015
O K	.000,	49.739	63.707		2.000
TOTAL		100.000	100.000	100.000	1.139

EDAX ANALYSIS

*Western Province Ball Clay*Sample 2 A 1

CO calibration,

FILENAME:SC02

LIVETIME= 200 I/P= '177'1 cps

ENERGY	RES	AREA
1.2	84.62	114103
6927.9	158.91	154072
TOTAL AREA=		354205 GF= 50.018

Specimen spectrum,

FILENAME: SWP2A'1

LIVETIME(soec.)= 200

ENERGY	RES	AREA
1.4	83.05	117374
TOTAL AREA=		191581

FIT INDEX= .42

ELMT	APP.CONC	ERROR(WT%)
NaK 2	.046	.066* < 2 Sigma*
MgK 2	.308	.083
AlK 2	'14.974	.143
SiK 2	17.583	•'114
K K 2	.869	.047
CaK 2	.100	.036
TiK 2	.914	.056
MnK 2	.020	.050* < 2 Sigma*
FeK 2	'1.0'14	.073

... [3 ZAF'SJ



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20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE='1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	'1.0'10	.055	.049	Na2O1	.002
MgK 2	'1.024	.360	.304	Mg'101	.010
AlK 2	.945	'18.987	14.436	Al2O3	.453
SiK 2	.775	27.188	19.855	Si102	58.'16'1
K K 2	.986	'1.056	.554	K 201	1.272
CaK 2	.98'1	•'122	.063	Ca'10'1	•'17'1
TiK 2	.983	'1.114	.477	Ti102	1.859
MnK 2	.873	.028	.0'10	Mn101	.036
FeK 2	.890	1.366	.502	Fe203	1.953
O K 0	.000	49.723	63.750		2.000
TOTAL		'100.000	100.000	'100.000	'1.'137

EDAXANALYSIS

*Western Province Ball Clay*Samole 2 A2

Specimen spectrum,

FILENAME:SWP2A:2

LIVETIME(spec.)= :200

ENERGY	RES	AREA
1.2	83.27	118293
TOTAL AREA=		173716

FIT INDEX= .51

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.035	.062* < 2 Sigma*
MgK	2	.345	.078
AlK	2	'13.598	.135
SiK	2	15.701	.108
K K	2	.798	.045
CaK	2	•-125	.033
TiK	2	.827	.054
MnK	2	.074	.050* < 2 Sigma*
FeK	2	.945	.073

••• C 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM=5.00 COSINE=1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%		%OXIDE	FORMULA
NaK	2 1.008	.046	.041	Na2O	.062	.001
MgK	2 1.022	.447	.377	MgO	.741	.012
AlK	2 .943	19.104	'14.540	Al2O3	36.097	.457
SiK	2 .773	:26.907	'19.669	SiO2	57.559	.618
K K	2 .987	'1.072	.563	K2O	'1.291	.018
CaK	2 .982	•169	.086	CaO	.236	.003
TiK	2 .983	'1.114	.478	TiO2	1.859	.015
MnK	2 .873	•112	.042	MnO	.144	.001
FeK	2 .890	1.406	.517	Fe2O3	2.010	.016
O K	0 .000	49.624	63.687			2.000
TOTAL		100.000	100.000		100.000	'1.140

EDAX ANALYSIS

*Western Province Ball Clay*Samle 201

CO calibration,

FILENAME:SC02

LIVETIME= 200 I/P= 1759 cps

ENERGY	RES	AREA
.7	84.80	114321
6925.7	158.23	152958
TOTAL AREA=		351810 GF= 50.006

Specimen spectrum,

FILENAME:SWP2D

LIVETIMEC(spec.)= 200

ENERGY	RES	AREA
.7	82.93	116115
TOTAL AREA=		236256

FIT INDEX= .78

ELMT		APP.CONC	ERRORCWT%)
NaK	2	.186	.074
MgK	2	.390	.093
AlK	2	18.442	.160
SiK	2	21.372	.126
K K	2	2.360	.062
CaK	2	.281	.D43
TiK	2	1.022	.060
MnK	2	.076	.055* < 2 Sigma*
FeK	2	1.546	.085

...[3 ZAF'SJ



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20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 1.000	.178	.160	Na2O1	.240 .005
MgK	.2 1.014	.368	.313	Mg1O1	.610 .010
AlK	2 .939	18.774	14.382	Al2O3	35.474 .454
SiK	2 .775	26.367	19.400	Si1O2	56.403 .613
K K	2 .990	2.280	1.205	K 2O1	2.746 .038
CaK	2 .978	.274	.141	Ca1O1	.384 .004
TiK	2 .981	.996	.430	Ti1O2	1.661 .011
MnK	.2 .873	.083	.031	Mn1O1	.108 .001
FeK	2 .890	1.660	.614	Fe2O3	2.374 .019
O K	0 .000	49.020	63.323		2.000
TOTAL		100.000	100.000	100.000	1.158

EDAX ANALYSIS

*Western Province Ball Clay*Sample 2 02

Specimen spectrum,

FILENAME:SWP2D2

LIVETIME(spec.)= 200

ENERGY RES AREA
 .9 83.50 117186
 TOTAL AREA= 209380

FIT INDEX:: .71

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.271	.070
MgK	2	.595	.088
AlK	2	16.395	.150
SiK	2	18.385	.117
K K	2	2.119	.060
CaK	2	.370	.041
TiK	2	.962	.059
MnK	2	.077	.054* < 2 Sigma*
FeK	2	1.226	.079

•••: 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 1.004	.292	.263	Na2O1	.394 .008
MgK	2 1.015	.635	.540	Mg1O1	1.053 .017
AlK	2 .935	18.995	14.556	Al2O3	35.892 .461
SiK	2 .771	25.835	19.015	Si1O2	55.267 .602
K K	2 .991	2.318	1.225	K 2O1	2.792 .039
CaK	2 .978	.410	.211	Ca1O1	.574 .007
TiK	2 .981	1.063	.459	Ti1O2	1.773 .015
MnK	2 .873	.095	.036	Mn1O1	.123 .001
FeK	2 .890	1.492	.552	Fe2O3	2.133 .017
O K	0 .000	48.865	63.142		2.000
TOTAL		100.000	100.000	100.000	1.167

ULTIMATE ANALYSIS

Western Province Ball Clay I

WESTERN PROVINCE BALL CLAY D (Sample 1)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	19.45	19.79	19.62	19.62	1,179.34	57.47	50.64
Al(Al ₂ O ₃)	14.79	14.58	14.69	7.34	749.04	36.50	32.16
Fe(Fe ₂ O ₃)	0.53	0.48	0.50	0.25	40.26	1.96	1.73
Ti (TiO ₂)	0.52	0.40	0.46	0.46	36.91	1.80	1.55
K (K ₂ O)	0.58	0.56	0.57	0.28	26.75	1.30	1.15
Na (Na ₂ O)	0.05	0.07	0.06	0.03	1.78	0.09	0.08
Ca (CaO)	0.08	0.08	0.08	0.08	4.40	0.21	0.19
Mg (MgO)	0.34	0.34	0.34	0.34	13.56	0.66	0.58
Mn(MnO ₂)	0.00	0.00	0.00	0.00	0.00	0.00	0.00
OXYGEN	63.66	63.71	63.68				
LOI						13.50	11.90
Total	100.00	100.00	100.00		2.052.05	113.50	100.01

WESTERN PROVINCE BALL CLAY D (Sample 1)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	20.53	22.71	21.62	21.62	1,299.27	63.89	56.29
Al(Al ₂ O ₃)	12.90	11.31	12.11	6.05	617.38	30.36	26.75
Fe(Fe ₂ O ₃)	0.55	0.38	0.47	0.23	37.15	1.83	1.61
Ti (TiO ₂)	0.47	0.42	0.44	0.44	35.20	1.73	1.52
K (K ₂ O)	0.66	0.51	0.58	0.29	27.53	1.35	1.19
Na (Na ₂ O)	0.11	0.09	0.10	0.05	3.07	0.15	0.13
Ca (CaO)	0.05	0.06	0.06	0.06	3.09	0.15	0.13
Mg (MgO)	0.26	0.19	0.23	0.23	9.09	0.45	0.39
Mn(MnO ₂)	0.05	0.00	0.02	0.02	1.96	0.10	0.08
OXYGEN	63.93	64.34	64.13				
LOI						13.50	11.90
Total	99.50	100.00	99.75		2 033.72	113.50	100.01

ULTIMATE ANALYSIS

Western Province Ball Clay I

WESTERN PROVINCE BALL CLAY A (Sample 2)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	19.86	19.67	19.76	19.76	1,187.70	57.85	50.97
Al(Al ₂ O ₃)	14.43	14.54	14.49	7.24	738.79	35.98	31.70
Fe(Fe ₂ O ₃)	0.5e	0.52	0.51	0.25	40.66	1.98	1.74
Ti (TiO ₂)	0.48	0.48	0.48	0.48	38.15	1.86	1.64
K (K ₂ O)	0.55	0.56	0.56	0.28	26.31	1.28	1.13
Na (Na ₂ O)	0.05	0.04	0.05	0.02	1.40	0.07	0.06
Ca (CaO)	0.06	0.09	0.07	0.07	4.18	0.20	0.1a
Mg (MgO)	0.30	0.38	0.34	0.34	13.72	0.67	0.59
Mn(MnO ₂)	0.01	0.04	0.03	0.03	2.26	0.11	0.10
OXYGEN	63.75	63.69	63.72				
LOI						13.50	11.90
Total	100.00	100.00	100.00		2053.15	113.50	100.01

WESTERN PROVINCE BALL CLAY D (Sample 2)							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	19.40	19.02	19.21	19.21	1,154.37	55.82	49.18
Al(Al ₂ O ₃)	14.38	14.56	14.47	7.23	737.87	35.68	31.44
Fe(Fe ₂ O ₃)	0.61	0.55	0.58	0.29	46.52	2.25	1.98
Ti (TiO ₂)	0.43	0.46	0.44	0.44	35.52	1.72	1.51
K (K ₂ O)	1.21	1.23	1.22	0.61	57.23	2.77	2.44
Na (Na ₂ O)	0.16	0.26	0.21	0.11	6.56	0.32	0.28
Ca (CaO)	0.14	0.21	0.18	0.18	9.87	0.48	0.42
Mg (MgO)	0.31	0.54	0.43	0.43	17.19	0.83	0.73
Mn(MnO ₂)	0.03	0.04	0.03	0.03	2.91	0.14	0.12
OXYGEN	63.32	63.14	63.23				
LOI						13.50	11.90
Total	100.00	100.00	100.00		2068.03	113.50	100.01

RATIONAL ANALYSIS

Western Province Ball Clay I

RATIONAL ANALYSIS WPBC A (sample 1)				
FELDSPAR CONVENTION				
MATERIAL		FACTOR	RESULT	
Total alkalis	1.23	*5.92	17.28	1%Feldspar
Feldspar	7.28	*0.183	1.33	Al ₂ O ₃ in Felds (a)
Feldspar	7.28	*0.647	4.71	SiO ₂ in Felds (b)
Al ₂ O ₃	32.16	"-a"*2.53	177.99	1% Clay subst. (e)
Clay subst.	77.99	*0.463	36.11	SiO ₂ in Clay (d)
SiO ₂	50.64	"-(b+d)"	19.82	1% Free silica
% WATER IN THE CLAY: % ORGANIC MATTER				
Clay Subst.	76.94	*0.140	110.92	Loss:H ₂ O in Clay (e)
LOI	11.90	"(-e)"	1.20	Loss; CO ₂ etc
MICA CONVENTION				
K ₂ O	1.15	*8.47	19.74	1%Potash Mica
Na ₂ O	0.08	*12.32	10.99	1%Soda Mica
Potash Mica	9.74	*0.384	3.74	Al ₂ O ₃ in K Mica (e)
Potash Mica	9.74	*0.452	4.40	SiO ₂ in K Mica (f)
Soda Mica	0.99	*0.4	0.39	Al ₂ O ₃ in Na Mica (g)
Soda Mica	0.99	*0.471	0.46	SiO ₂ in Na Mica (h)
Al ₂ O ₃	32.16	"-(e+g)*2.53	170.90	1%Clay subst,
Clay subst.	70.90	*0.465	32.97	SiO ₂ in Clay (i)
SiO ₂	50.64	"-(f+h+i)"	12.80	1%Free Silica

RATIONAL ANALYSIS

Western Province Ball Clay I

RATIONAL ANALYSIS WPBC A (sample 2)				
FELDSPAR CONVENTION				
MATERIAL		FACTOR	RESULT	
Total alkalis	1.19	*5.92	17.04	1%Feldspar
Feldspar	7.04	*0.183	1.29	Al ₂ O ₃ in Felds (a)
Feldspar	7.04	*0.647	4.55	SiO ₂ in Felds (b)
Al ₂ O ₃	31.70	"-a"*2.53	176.94	1% Clay subst. (c)
Clay subst.	76.94	*0.463	35.62	SiO ₂ in Clay (d)
SiO ₂	50.97	"-(b+d)"	110.79	1% Free silica
% WATER IN THE CLAY: % ORGANIC MATTER				
Clay Subst.	76.94	*0.140	110.77	Loss:H ₂ O in Clay (e)
LOI	11.90	"(e)"	1.20	Loss: CO ₂ etc
MICA CONVENTION				
K ₂ O	1.13	*8.47	19.57	1%Potash Mica
Na ₂ O	0.06	*12.32	10.74	1%Soda Mica
Potash Mica	9.57	*0.384	3.68	Al ₂ O ₃ in K Mica (e)
Potash Mica	9.57	*0.452	4.33	SiO ₂ in K Mica (f)
Soda Mica	0.74	*0.4	0.30	Al ₂ O ₃ in Na Mica (g)
Soda Mica	0.74	*0.471	0.35	SiO ₂ in Na Mica (h)
Al ₂ O ₃	31.7	"-(e+g)*2.53	170.13	1%Clay subst,
Clay subst.	70.13	*0.465	33.6	SiO ₂ in Clay (i)
SiO ₂	50.97	"-(f+h+i)"	113.69	1%Free Silica

EDAX ANALYSIS

G1 Kaolin

Sample A 1

Data file values:

SNO= 107.49 SN1=-2.4341

CO calibration,

FILENAME:SC02

LIVETIME= 200 I/P= 1616 cps

ENERGY	RES	AREA
1.5	86.12	113918
6929.2	158.96	138934
TOTAL AREA=		323234 GF= 50.025

Specimen spectrum,

FILENAME: G1K1

G1K1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
-1.5	84.69	117157
TOTAL AREA=		181433

FIT INDEX= .53

ELMT		APP.CONC	ERROR (WT%)
NaK	2	.105	.065* < 2 Sigma*
MgK	2	.125	.081* < 2 Sigma*
AlK	2	11.692	•-140
SiK	2	21.926	•131
K K	2	2.036	.060
CaK	2	.084	.038
TiK	2	.216	.049
MnK	2	-.015	.052* < 2 -Sigma*
FeK	2	.229	.061

...L 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: G1K1

Last, elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 1.029	.122	.109	Na2O1	.165 .003
MgK	2 1.036	.144	.121	Mg1O1	.239 .004
AlK	2 .959	14.573	11.028	Al2O3	27.536 .344
SiK	2 .824	31.808	23.119	Si1O2	68.044 .722
K K	2 .981	2.481	1.295	K 2O1	2.988 .040
CaK	2 .969	.103	.053	Ca1O1	.144 .002
TiK	2 .974	.265	.113	Ti1O2	.442 .004
MnK	2 .870	.000	.000	Mn1O1	.000 .000
FeK	2 .887	.309	.113	Fe2O3	.442 .004
O K	0 .000	50.195	64.050		2.000
TOTAL		100.000	100.000	100.000	1.123

EDAX ANALYSIS

G1 Kaolin

SampleA2Specimen spectrum,
G1K1

FILENAME: G1KA2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.4	84.68	117377
TOTAL AREA= 174362		

FIT INDEX= .56

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.078	.064* < 2 Sigma*
MgK	2	.122	.080* < 2 Sigma*
AlK	2	11.613	.139
SiK	2	21.405	.129
K K	2	1.926	.059
CaK	2	.077	.037
TiK	2	.421	.050
MnK	2	.018	.050* < 2 Sigma*
FeK	2	.255	.059
... [3 ZAF'SJ			

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: G1K1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%		%OXIDE	FORMULA
NaK	2	1.025	.093	.082	Na2O1	.125 .003
MgK	2	1.034	.143	.121	Mg101	.238 .004
AlK	2	.958	14.692	11.129	Al2O3	27.761 .347
SiK	2	.822	31.542	22.948	Si102	67.475 .716
K K	2	.982	2.376	1.242	K 201	2.862 .039
CaK	2	.970	.096	.049	Ca101	.134 .002
TiK	2	.975	.524	.223	Ti102	.874 .007
MnK	2	.870	.025	.009	Mn101	.033 .000
FeK	2	.887	.348	.127	Fe2O3	.498 .004
O K	0	.000	50.160	64.069		2.000
TOTAL		100.000	100.000		100.000	1.122

EDAX ANALYSIS

G1 Kaolin

Sample 0 1

Specimen spectrum,
G1D1.

FILENAME: G1D1

LIVETIME(spec.)= :200

ENERGY	RES	AREA
1.5	86.04	.117250
TOTAL AREA= 185479		

FIT INDEX= .50

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.08:2	.063* < 2 Sigma*
MgK	2	.083	.079* < 2 Sigma*
AlK	2	'10.952	.137
SiK	2	22.947	.132
K K	2	2.232	.062
CaK	2	.077	.039* < 2 Sigma*
TiK	2	.466	.053
MnK	2	-.040	.053* < 2 Sigma*
FeK	2	.286	.062
..I	2	ZAF'SJ	

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: G1D1

Last elmt by STOICH.,NORMALISE[I

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 1.021	.094	.084	Na2O1	.127 .003
MgK	2 1.031	.095	.080	Mg1O1	.157 .002
AlK	2 .957	'13.494	'10.232	Al2O3	25.497 .319
SiK	2 .835	32.43'1	23.621	Si1O2	69.377 .736
K K	2 .982	2.680	'1.402	K 2O1	3.229 .044
CaK	2 .969	.094	.048	Ca1O1	.131 .001
TiK	2 .974	.564	.241	Ti1O2	.94'1 .008
MnK	2 .B70	.000	.000	Mn1O1	.000 .000
FeK	2 .887	.381	.139	Fe2O3	.544 .004
O K	0 .000	50.'171	64.152		2.000
TOTAL		'100.004	'100.000	'100.004	'1.118

EDAX ANALYSIS

G1 Kaolin

Sample D2

Specimen spectrum,

FILENAME: G1D2

LIVETIME(spec.)= 200

ENERGY RES AREA
 1.6 85.27 116653
 TOTAL AREA= 210400

FIT INDEX= .34

ELMT	APP.CONC	ERROR(WT%)
NaK 2	.067	.068* < 2 Sigma*
MgK 2	.099	.085* < 2 Sigma*
AlK 2	12.490	.147
SiK 2	27.576	.144
K K 2	2.269	.063
CaK 2	.067	.040* < 2 Sigma*
TiK 2	.330	.053
MnK 2	-.013	.054* < 2 Sigma*
FeK 2	.202	.063

.... [3 ZAF/SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum:

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	1.027	.066	.058	Na2O1	.088
MgK 2	1.036	.096	.081	Mg1O1	.160
AlK 2	.961	13.151	9.938	Al2O3	24.850
SiK 2	.839	33.229	24.119	Si1O2	71.083
K K 2	.980	2.341	1.221	K 2O1	2.820
CaK 2	.969	.070	.036	Ca1O1	.098
TiK 2	.974	.343	.146	Ti1O2	.571
MnK 2	.870	.000	.000	Mn1O1	.000
FeK 2	.887	.230	.084	Fe2O3	.329
O K 0	.000	50.474	64.318		2.000
TOTAL		100.000	100.000	100.000	1.110

ULTIMATE ANALYSIS

G1 Kaolin

G1 KAOLIN A							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysist	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	23.12	22.95	23.03	23.03	1,384.31	67.75	64.28
Al(Al ₂ O ₃)	11.03	11.13	11.08	5.54	565.00	27.65	26.24
Fe(Fe ₂ O ₃)	0.11	0.13	0.12	0.06	9.58	0.47	0.44
Ti (TiO ₂)	0.11	0.22	0.17	0.17	13.42	0.66	0.62
K (K ₂ O)	1.30	1.24	1.27	0.63	59.75	2.92	2.77
Na (Na ₂ O)	0.11	0.08	0.10	0.05	2.96	0.14	0.14
Ca (CaO)	0.05	0.05	0.05	0.05	2.86	0.14	0.13
Mg (MgO)	0.12	0.12	0.12	0.12	4.88	0.24	0.23
Mn(MnO ₂)	0.00	0.01	0.00	0.00	0.39	0.02	0.02
OXYGEN	64.05	64.07	64.06				
LOI						5.40	5.12
Total	100.00	100.00	100.00		2,043.15	105.40	100.00

G1 KAOLIN 0							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	23.62	24.12	23.87	23.87	1,434.59	70.10	66.51
Al(Al ₂ O ₃)	10.23	9.94	10.09	5.04	514.34	25.13	23.84
Fe(Fe ₂ O ₃)	0.14	0.08	0.11	0.06	8.90	0.43	0.41
Ti (TiO ₂)	0.24	0.15	0.19	0.19	15.46	0.76	0.72
K (K ₂ O)	1.40	1.22	1.31	0.66	61.77	3.02	2.86
Na (Na ₂ O)	0.08	0.06	0.07	0.04	2.20	0.11	0.10
Ca (CaO)	0.05	0.04	0.04	0.04	2.36	0.12	0.11
Mg (MgO)	0.08	0.08	0.08	0.08	3.24	0.16	0.15
Mn(MnO ₂)	0.00	0.08	0.04	0.04	3.65	0.18	0.17
OXYGEN	64.14	64.32	64.23				
LOI						5.40	5.12
Total	99.99	100.09	100.04		2046.50	105.40	100.00

RATIONAL ANALYSIS

G1 Kaolin

RATIONAL ANALYSIS G1 KAOLIN					
FELDSPAR CONVENTION					
MATERIAL	ENTRY	FACTOR	RESULT	1	
Total alkalis	2.91	*5.92	117.23	1%Feldspar	
Feldspar	17.23	*0.183	3.15	Al2O3 in Felds	(a)
Feldspar	17.23	*0.647	11.15	SiO2 in Felds	ib)
Al2O3	26.24	"a"*2.53	158.41	1% Clay subst.	c
Clay subst.	58.41	*0.463	27.04	SiO2 in Clay	Id
SiO2	64.28	"(b+d)"	126.09	1% silica	
% WATER IN THE CLAY: % ORGANIC MATTER					
Clay Subst.	58.41	*0.140	18.18	Loss:H2O in Clay E)	
LOI	5.10	"(- e)"	0.00	Loss: CO2 etc	
MICA CONVENTION					
K2O	2.77	*8.47	123.46	1% Potash Mica	
Na2O	0.14	*12.32	11.72	1%Soda Mica	
Potash Mica	23.46	*0.384	9.01	Al2O3 in K Mica	(e)
Potash Mica	23.46	*0.452	10.60	SiO2 in K Mica	(f)
Soda Mica	1.72	*0.4	0.69	Al2O3 in Na Mica	(g)
Soda Mica	1.72	*0.471	0.81	SiO2 in Na Mica	(h)
Al2O3	26.24	"(e+g)	141.85	1% Clay substance	
		2.53			
Clay subst.	41.85	*0.465	19.46	SiO2 in Clay (i)	
SiO2	64.28	"(f+h+)	133.40	1% Free Silica	

EDAX ANALYSIS

serena Kaolin

Sample A 1

CO calibration, FILENAME:SC02
 SC02 LIVETIME= 200 I/P= 1682 cps

ENERGY	RES	AREA
1.2	92.56	113328
6927.6	164.06	145778

TOTAL AREA= 336374 GF= 50.016

Specimen spectrum, FILENAME: SERD1 = SER A 1
 SERD1 LIVETIME(spec.)= 200

ENERGY	RES	AREA
.7	97.64	116341

TOTAL AREA= 128785

.....
 FIT INDEX= .41

ELMT	APP.CONC	ERROR(WT%)
NaK 2	.047	.060* < 2 Sigma*
MgK 2	.049	.072* < 2 Sigma*
AlK 2	12.890	.132
SiK 2	10.910	.095
K K 2	.689	.043
CaK 2	.033	.031* < 2 Sigma*
TiK 2	.164	.041
MnK 2	-.026	.044* < 2 Sigma*
FeK 2	.236	.053

..C 3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SERD1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	'1.0"1'6	.078	.069	Na201	.105 .002
MgK 2	'1.05'1	.08'1	.068	Mg-10-1	-.134 .002
AlK 2	.966	22.968	-17.344	Al203	43.399 .547
SiK 2	.748	25.099	-18.205	Si102	53.692 .575
K K 2	.983	'1.206	.629	K 201	1.453 .020
CaK 2	.977	.058	.029	Ca-10-1	.08-1 .00-1
TiK 2	.980	.:289	-.123	Ti102	.482 .004
MnK 2	.873	.000	.000	Mn-101	.000 .000
FeK 2	.890	.457	.167	Fe203	.654 .005
0 K 0	.000	49.764	63.367		2.000
TOTAL		100.000	-100.000	-100.000	-1 .156

EDAXANALYSIS

*Serena Kaolin*Sample A2Specimen spectrum,
SERA2FILENAME: SERA2 = **A2.**
LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.1	93.48	117433
TOTAL AREA=		114281

FIT INDEX= .52

ELMT		APP.CONC	ERROR(WTX)
NaK	2	.0'10	.057* < 2 Sigma*
MgK	2	.087	.070* < 2 Sigma*
AlK	2	11.752	.126
SiK	2	'10.'122	.09'1
K K	2	.610	.039
CaK	2	.0'18	.028* < 2 Sigma*
rn:	2	.'148	.038
MnK	2	.001	.041* < 2 Sigma*
FeK	2	.'176	.047

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SERA2

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK	2 '1.048	.0'17	.0'15	Na2O1	.023 .000
MgK	2 '1.053	.'156	.130	Mg1O1	.258 .004
AlK	2 .966	22.806	'17.208	Al2O3	43.093 .543
SiK	2 .750	25.322	'18.35'1	Si1O2	54.'168 .579
K K	2 .983	'1.164	.606	K 2O1	1.402 .019
CaK	2 .977	.035	.0'18	Ca1O1	.049 .001
TiK	2 .979	.283	.120	Ti1O2	.473 .004
MnK	2 .873	.002	.00'1	Mn1O1	.002 .000
FeK	2 .889	.372	.'135	Fe2O3	.531 .004
0 K	0 .000	49.843	63.416		2'000
TOTAL		'100.000	'100.000	'100.000	1.'154

EDAX ANALYSIS

Serena Kaolln

Sample 0 1

Specimen spectrum,
SERD2FILENAME:SERD2 = D1
LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.4	89.63	116815
TOTAL AREA= 193222		

FIT INDEX= 1.21

ELMT	APP.CONC	ERROR(WT%)
NaK 2	.026	.075* < 2 Sigma*
MgK 2	-.188	.091* < 2 Sigma*
AlK 2	20.072	.166
SiK 2	16.690	.116
K K 2	.983	.051
CaK 2	.046	.037* < 2 Sigma*
TiK 2	.302	.050
MnK 2	-.024	.052* < 2 Sigma*
FeK 2	.249	.061

..C 3 ZAF'SJ

20.00 kV TLLT= .00 ELEV=40.00 AZIM=.00 COSINE=1.000

Spectrum: SERD2

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA	
NaK 2	1.049	.028	.025	Na2O1	.037	.001
MgK 2	1.054	.000	.000	Mg1O1	.000	.000
AlK 2	.969	23.234	17.530	Al2O3	43.901	.553
SiK 2	.747	25.061	18.161	Si1O2	53.610	.573
K K 2	.983	1.122	.584	K 2O1	1.351	.018
CaK 2	.977	.053	.027	Ca1O1	.074	.001
TiK 2	.979	.346	.147	Ti1O2	.576	.005
MnK 2	.873	.000	.000	Mn1O1	.000	.000
FeK 2	.889	.314	.114	Fe2O3	.449	.004
O K 0	.000	49.843	63.413			2.000
TOTAL		100.000	100.000	100.000		1.154

EDAX ANALYSIS

*Serena Kaolin***Sample 02**Specimen spectrum,
SERD3FILENAME: SERD3 = D2.
LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.3	90.26	116940
TOTAL AREA=		158706

FIT INDEX= .46

ELMT		APP.CONC	ERROR	CWT(%)
NaK	2	.010	.067*	< 2 Sigma*
MgK	2	.092	.08-1*	< 2 Sigma*
AlK	2	-17.083	•-150	
SiK	2	-13.996	.-106	
K K	2	.827	.045	
CaK	2	-.006	.033*	< 2 Sigma*
TiK	2	.350	.046	
MnK	2	.0-1-1	.047*	< 2 Sigma*
FeK	2	.25-1	.057	

... (3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM=.00 COSINE=L 000

Spectrum: SERD3

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%		%OXIDE	FORMULA
NaK	2 -1.046	.0-12	.0-1-1	Na2O1	.016	.000
MgK	2 -1.053	•116	.097	Mg1O1	•192	.003
AlK	2 .966	23.33'1	17.6-15	Al2O3	44.084	.556
SiK	2 .745	24.790	-17.977	Si-102	53.030	.567
K K	2 .983	-1.110	.578	K 201	1.337	.0-18
CaK	2 .978	.000	.000	Ca-1O1	.000	.000
TiK	2 .980	.47-1	.200	Ti1O2	.785	.006
MnK	2 .873	.0-17	.006	Mn1O1	.021	.000
FeK	2 .890	.373	•'136	Fe2O3	.533	.004
O K	0 .000	49.78'1	63.379			2.000
TOTAL		100.000	-100.000		'100.000	1.156

ULTIMATE ANALYSIS

serena Kaolin

SERINA KAOLIN A							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (5102)	18.21	18.35	18.28	18.28	1,098.51	53.93	47.43
Al(Al ₂ O ₃)	17.34	17.21	17.28	8.64	881.05	43.25	38.04
Fe(Fe ₂ O ₃)	0.17	0.14	0.15	0.08	12.05	0.59	0.52
Ti (TiO ₂)	0.12	0.12	0.12	0.12	9.71	0.48	0.42
K (K ₂ O)	0.63	0.61	0.62	0.31	29.08	1.43	1.26
Na (Na ₂ O)	0.07	0.02	0.04	0.02	1.30	0.06	0.06
Ca (CaO)	0.03	0.02	0.02	0.02	1.32	0.06	0.06
Mg (MgO)	0.07	0.13	0.10	0.10	3.99	0.20	0.17
Mn(MnO ₂)	0.00	0.00	0.00	0.00	0.04	0.00	0.00
OXYGEN	63.37	63.42	63.39				
LOI						13.70	12.05
Total	100.00	100.00	100.00		2037.08	113.70	100.00

SERINA KAOLIN 0							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide + LOI	Oxide %
Si (5102)	18.16	17.98	18.07	18.07	1,085.95	53.31	46.89
Al(Al ₂ O ₃)	17.53	17.62	17.57	8.79	896.20	44.00	38.70
Fe(Fe ₂ O ₃)	0.11	0.14	0.13	0.06	9.98	0.49	0.43
Ti (TiO ₂)	0.15	0.20	0.17	0.17	13.86	0.68	0.60
K (K ₂ O)	0.58	0.58	0.58	0.29	27.37	1.34	1.18
Na (Na ₂ O)	0.03	0.01	0.02	0.01	0.56	0.03	0.02
Ca (CaO)	0.03	0.00	0.01	0.01	0.76	0.04	0.03
Mg (MgO)	0.00	0.10	0.05	0.05	1.95	0.10	0.08
Mn(MnO ₂)	0.00	0.01	0.00	0.00	0.26	0.01	0.01
OXYGEN	63.41	63.38	63.40				
LOI						13.70	12.05
Total	100.00	100.00	100.00		2036.88	113.70	100.00

RATIONAL ANALYSIS*serena Kaolin .*

RATIONAL ANALYSIS SERINA A			
FELDSPAR CONVENTION			
MATERIAL		FACTOR	IREULTI
Total alkalis	1.32	*5.92	/7.81 /%Feldspar
Feldspar	7.81	*0.183	1.43 Al ₂ O ₃ in Felds (a)
Feldspar	7.81	*0.647	5.05 SiO ₂ in Felds (b)
Al ₂ O ₃	38.04	"-a"*2.53	192.63 1% Clay subst. (c)
Clay subst.	92.63	*0.463	42.89 SiO ₂ in Clay (d)
SiO ₂	47.43	"-(b+d)"	1-0.51 1% silica
% WATER IN THE CLAY: % ORGANIC MATTER			
Clay Subst.	92.63	*0.140	112.97 ILoss:H ₂ O in Clay (e)
LOI	12.05	"(-e)"	I _{toss} : CO ₂ etc
MICA CONVENTION			
K ₂ O	1.26	*8.47	110.67 IPotash Mica
Na ₂ O	0.06	*12.32	10.74 [soda Mica
Potash Mica	10.67	*0.384	4.10 Al ₂ O ₃ in K Mica (e)
Potash Mica	10.67	*0.452	4.82 SiO ₂ in K Mica (f)
Soda Mica	0.74	*0.4	0.30 Al ₂ O ₃ in Na Mica (g)
Soda Mica	0.74	*0.471	0.35 SiO ₂ in Na Mica (h)
Al ₂ O ₃	38.04	"-(e+g)*2.53	185.12 [Claysubst.
Clay subst.	85.12	*0.465	39.58 SiO ₂ in Clay (i)
SiO ₂	47.43	"-(f+h+i)"	12.67 IFree Silica

EDAX ANALYSIS

5-Ksolln

Sample A 1

CO calibration,
SiK1

FILENAME:SCO'1

LIVETIME= 200 I/P= '1639 cps

ENERGY	RES	AREA
1.4	85.71	114300
6928.7	157.71	141292
TOTAL AREA=		327714 GF= 50.022

Specimen spectrum,
SKA1

FILENAME:SKA1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.4	84.21'	118427
TOTAL AREA=		150743

FIT INDEX:: .3'1

ELMT	APP.CONC	ERROR(WT%)
NaK 2	.071	.063* < 2 Sigma*
MgK 2	.126	.076* < 2 Sigma*
AlK 2	13.989	.140
SiK 2	13.915	.106
K K 2	.439	.042
CaK 2	.027	.034* < 2 Sigma*
TiK 2	.271	.048
MnK 2	.095	.052* < 2 Sigma*
FeK 2	1.006	.074
... 3 ZAF'SJ		

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SKA1

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	1.015	.100	.089	Na2O1	.135 .003
MgK 2	1.027	.175	.147	Mg101	.290 .005
AlK 2	.950	20.997	15.924	Al2O3	39.675 .501
SiK 2	.759	26.144	19.044	Si102	55.927 .599
K K 2	.984	.636	.333	K 201	.766 .010
CaK 2	.981	.039	.020	Ca101	.054 .001
TiK 2	.984	.392	.167	Ti102	.654 .005
MnK 2	.874	.154	.057	Mn101	.199 .002
FeK 2	.891	1.609	.589	Fe2O3	2.300 .019
0 K 0	.000	-49.755	63.629		2.000
TOTAL		100.000	100.000	100.000	1.143

EDAX ANALYSIS

*8-Kaolln*SampleA2Specimen spectrum,
SKA2

FILENAME: SKA2

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.5	84.23	118149
TOTAL AREA= 151767		

FIT INDEX= .24

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.036	.063* < 2 Sigma*
MgK	2	.135	.077* < 2 Sigma*
AlK	2	'12.92.7	•'138
SiK	2	15.98'1	•'112
K K	2	.207	.038
CaK	2	.00'1	.033* < 2 Sigma*
TiK	2	.278	.048
MnK	2	-.008	.049* < 2 Sigma*
FeK	2	.837	.070
... [3 ZAF'SJ			

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SKA2

Last elmt by STOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%		%OXIDE	FORMULA
NaK	2 '1.02'1	.049	.044	Na2O1	.066	.00'1
MgK	2 '1.032	•'182	.152	Mg'101	.302	.005
AlK	2 .954	18.874	'14.244	Al2O3	35.663	.445
SiK	2 .779	28.554	20.697	Si102	6'1.082	.646
K K	2 .981	.294	'153	K 201	.355	.005
CaK	2 .980	.002	.00'1	Ca'10'1	.003	.000
TiK	2 .982	.394	.168	Ti102	.657	.005
MnK	2 .873	.000	.000	Mn101	.000	.000
FeK	2 .890	'1.310	.477	Fe2O3	1.872	.015
O K	0 .000	50.34'1	64.064			2.000
TOTAL		'100.000	100.000		100.000	1.122

EDAX ANALYSIS

5-Kaolln

Sample 0 1

Specimen spectrum,
SKD1

FILENAME: SKD1

LIVETIME(spec.)= 200

ENERGY	RES	AREA
1.6	84.89	114935
TOTAL AREA=		271362

FIT INDEX= .56

ELMT		APP.CONC	ERROR(WT%)
NaK	2	.079	.088* < 2 Sigma*
MgK	2	.368	.108
AlK	2	27.200	.195
SiK	2	26.443	.146
K K	2	.906	.056
CaK	2	.064	.044* < 2 Sigma*
TiK	2	.635	.063
MnK	2	-.081	.064* < 2 Sigma*
FeK	2	1.486	.092
...	3	ZAF'SJ	

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SKD1

Last elmt by STOICH.,NORMALISED

ELMT		ZAF	%ELMT	ATOM.%		%OXIDE	FORMULA
NaK	2	1.025	.057	.051	Na2O1	.077	.002
MgK	2	1.035	.266	.223	Mg1O1	.440	.007
AlK	2	.953	21.299	16.119	Al2O3	40.245	.507
SiK	2	.757	26.063	18.945	Si1O2	55.754	.596
K K	2	.984	.688	.359	K 2O1	.828	.011
CaK	2	.981	.049	.025	Ca1O1	.069	.001
TiK	2	.983	.482	.206	Ti1O2	.804	.006
MnK	2	.874	.000	.000	Mn1O1.	.000	.000
FeK	2	.890	1.246	.456	Fe2O3	1.782	.014
O K	0	.000	49.850	63.617			2.000
TOTAL			100.000	100.000		100.000	1.144

EDAX ANALYSIS

5-Kaolln**Sample D2**Specimen spectrum,
SKD2

FILENAME: SKD2

LIVETIMECspec.)= 200

ENERGY	RES	AREA
1.5	85.55	116385
TOTAL AREA= 225754		

FIT INDEX= .54

ELMT	APP.CONC	ERRORCWT%)
NaK 2	.045	.082* < 2 Sigma*
MgK 2	.234	.100
AlK 2	22.874	.180
SiK 2	22.693	.136
K K 2	.551	.049
CaK 2	.046	.039* < 2 Sigma*
TiK 2	.339	.054
MnK 2	-.073	.056* < 2 Sigma*
FeK 2	.962	.077

••• [3 ZAF'SJ

20.00 kV TILT= .00 ELEV=40.00 AZIM= .00 COSINE=1.000

Spectrum: SKD2

Last elmt by 8TOICH.,NORMALISED

ELMT	ZAF	%ELMT	ATOM.%	%OXIDE	FORMULA
NaK 2	1.033	.039	.035	Na2O1	.001
MgK 2	1.042	.200	.167	Mg101	.005
AlK 2	.959	2-1.253	16.034	Al2O3	.503
SiK 2	.760	26.602	19.276	Si102	.605
K K 2	.982	.500	.260	K 2O1	.008
CaK 2	.980	.042	.021	Ca101	.001
TiK 2	.982	.308	.131	TiO2	.004
MnK 2	.873	.000	.000	Mn101	.000
FeK 2	.890	.963	.351	Fe2O3	.011
O K 0	.000	50.094	63.726		2.000
TOTAL		100.000	100.000	100.000	1.138

ULTIMATE ANALYSIS

5-Kaolin

S KAOLIN A							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	19.04	20.70	19.87	19.87	1,194.22	58.49	52.76
Al(Al ₂ O ₃)	15.92	14.24	15.08	7.54	769.28	37.68	33.99
Fe(Fe ₂ O ₃)	0.59	0.48	0.53	0.27	42.53	2.08	1.88
Ti (TiO ₂)	0.16	0.17	0.17	0.17	13.18	0.65	0.58
K (K ₂ O)	0.33	0.15	0.24	0.12	45	0.56	0.51
Na (Na ₂ O)	0.09	0.04	0.07	0.03	2.06	0.10	0.09
Ca (CaO)	0.02	0.00	0.01	0.01	0.59	0.03	0.03
Mg (MgO)	0.15	0.15	0.15	0.15	6.02	0.30	0.27
Mn(MnO ₂)	0.06	0.00	0.03	0.03	2.48	0.12	0.11
OXYGEN	63.63	64.06	63.85				
LOI						10.86	9.80
Total	99.99	100.00	100.00		2 041.82	110.86	100.00

S KAOLIN 0							
	Atomic % of Elements			Molecular content		Oxide content	
	Analysis 1	Analysis 2	Average	Molecules	Mol weight	Oxide +LOI	Oxide %
Si (SiO ₂)	18.95	19.28	19.11	19.11	1,148.54	56.32	50.81
Al(Al ₂ O ₃)	16.12	16.03	16.08	8.04	819.90	40.21	36.27
Fe(Fe ₂ O ₃)	0.46	0.35	0.40	0.20	32.20	1.58	1.42
Ti (TiO ₂)	0.21	0.13	0.17	0.17	13.46	0.66	0.60
K (K ₂ O)	0.36	0.26	0.31	0.15	14.58	0.71	0.64
Na (Na ₂ O)	0.05	0.04	0.04	0.02	1.33	0.07	0.06
Ca (CaO)	0.03	0.02	0.02	0.02	1.29	0.06	0.06
Mg (MgO)	0.22	0.17	0.20	0.20	7.86	0.39	0.35
Mn(MnO ₂)	0.00	0.00	0.00	0.00	0.00	0.00	0.00
OXYGEN	63.62	63.73	63.67				
LOI						10.86	9.80
Total	100.00	100.00	100.00		2039.16	110.86	100.00

RAIIONAI ANALYSIS

5-Kaolln

RATIONAL ANALYSIS (S KAOLIN A)				
FELDSPAR CONVENTION				
MATERIAL	ENTRY	FACTOR	IRESULTI	
Total alkalis	0.60	*5.92	13.55	I%Feldspar
Feldspar	3.55	*0.183	0.65	Al2O3 in Felds (a)
Feldspar	3.55	*0.647	2.30	SiO2 in Felds (b)
Al2O3	33.99	"-a"*2.53	184.35	I% Clay subst. (c)
Clay subst.	84.35	*0.463	39.05	SiO2 in Clay (d)
SiO2	52.76	"-(b+d)"	'11.41	I% silica
% WATER IN THE CLAY: % ORGANIC MATTER				
Clay Subst.	32.35	*0.140	'11.81	ILoss:H2O in Clay (e)
LOI	9.80	"(- e)"	5.27	[toss: CO2 etc
MICA CONVENTION				
K2O	0.64	*8.47	15.42	I%Potash Mica
Na2O	0.06	*12.32	10.74	I%Soda Mica
Potash Mica	5.42	*0.384	2.08	Al2O3 in K Mica (e)
Potash Mica	5.42	*0.452	2.45	SiO2 in K Mica (f)
Soda Mica	0.74	*0.4	0.30	Al2O3 in Na Mica (g)
Soda Mica	0.74	*0.471	0.35	SiO2 in Na Mica (h)
Al2O3	36.27	"-(e+g)*2.53	179.65	I%Clay subst,
Clay subst.	79.65	*0.465	37.04	SiO2 in Clay (i)
SiO2	50.81	"-(f+h+i)"	'10.98	I% Free silica

APPENDIX E**DATA BASE**

The Ultimate analysis of the clay bodies was calculated by means of the "Insight" ceramic software programme. The results are presented in this appendix.



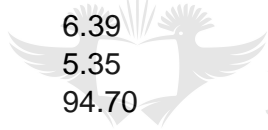
INSIGHT RECIPE CALCULATIONS.*A clay body*

A CLAY BODY

A CLAY.....	50.00	50.00%
SA SILICA.....	30.00	30.00%
SA POTASH FELDSPAR..	20.00	20.00%
		100.00

FORMULA & ANALYSIS

CaO ..	.00	.24%
MgO ..	.00	.16%
K2O ..	.03	3.33%
Na2O .	.00	.17%
Fe2O3..	.01	1.55%
TiO2...	.01	.80%
Al2O3..	.18	19.69%
SiO2...	1.17	74.06%
RATIO	6.39	
EXPAN	5.35	
WEIGHT	94.70	



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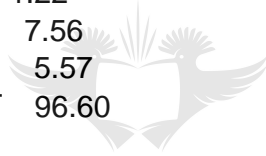
INSIGHT RECIPE CALCULATIONS.**813 Ball Clay Body**

B13 BALL CLAY BODY

B13 Ball Clay.....	50.00	50.00%	
SA SiLiCA.....	30.00	30.00%	
SA POTASH FELDSPAR..	20.00		20.00%
			100.00

FORMULA & ANALYSIS

CaO ..	.01	.41%
MgO ..	.01	.32%
K2O ..	.05	4.40%
Na2O ..	.00	.20%
Fe2O3..	.01	1.28%
MnO ..	.00	.04%
TiO2 .	.01	.60%
Al2O3..	.16	17.02%
SiO2...	1.22	75.73%
RATIO	7.56	
EXPAN	5.57	
WEIGHT	96.60	



INSIGHT RECIPE CALCULATIONS.***C*Claybody**

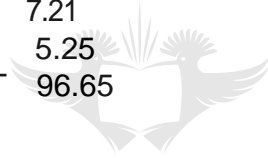
C Clay body

C CLAY.....	50.00	50.00%
SA SiLiCA.....	30.00	30.00%
SA POTASH FELDSPAR..	20.00	20.00%

100.00

FORMULA & ANALYSIS

CaO....	.00	.17%
MgO....	.00	.11%
K ₂ O....	.03	3.26%
Na ₂ O...	.00	.31%
Fe ₂ O ₃ ..	.00	.39%
TiO ₂01	1.05%
Al ₂ O ₃ ..	.17	18.07%
SiO ₂ ...	1.23	76.63%
RATIO	7.21	
EXPAN	5.25	
WEIGHT	96.65	



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INSIGHT RECIPE CALCULATIONS.***PXX Ball claybody***

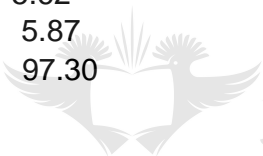
PXX BALL CLAY BODY

PXX BALL CLAY.....	50.00	50.00%
SA SiLiCA.....	30.00	30.00%
SA POTASH FELDSPAR..	20.00	20.00%

100.00

FORMULA & ANALYSIS

CaO .	.00	.10%
MgO .	.00	.05%
K2O ..	.05	4.69%
Na2O ..	.01	.76%
Fe2O3..	.00	.15%
TiO2...	.01	.79%
Al2O3..	.21	21.72%
SiO2...	1.16	71.74%
RATIO	5.62	
EXPAN	5.87	
WEIGHT	97.30	



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INSIGHT RECIPE CALCULATIONS.***Moss Clay body***

MOSS CLAY BODY

Moss Clay.....	50.00	50.00%
SA SILICA.....	30.00	30.00%
SA POTASH FELDSPAR..	20.00	20.00%
	100.00	

FORMULA & ANALYSIS

CaO ..	.00	.02%
MgO ..	.00	.12%
K2O ..	.05	5.13%
Na2O .	.00	.26%
Fe2O3..	.00	.81%
MnO .	.00	.01%
TiO2 .	.01	.68%
Al2O3..	.17	17.49%
SiO2...	1.22	75.48%
RATIO	7.33	
EXPAN	5.75	
WEIGHT	97.15	



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INSIGHT RECIPE CALCULATIONS.

Western Province Ball clay body

Western Province ball clay Body

WPBC.	50.00	50.00%
SA,SILICA.....	30.00	30.00%
SA POTASH FELDSPAR..	20.00	20.00%

100.00

FORMULA & ANALYSIS

CaO ..	.00	.10%
MgO ..	.01	.31%
K ₂ O ..	.04	3.75%
Na ₂ O .	.00	.19%
Fe ₂ O ₃ ..	.01	.97%
MnO ..	.00	.05%
TiO ₂ .	.01	.86%
Al ₂ O ₃ ..	.20	21.70%
SiO ₂ ...	1.13	72.08%
RATIO	5.65	
EXPAN	5.47	
WEIGHT	94.05	



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INSIGHT RECIPE CALCULATIONS.**G1 *Kaolin body'***

G1 Kaolin Body

G1 KAOLIN.....	50.00	50.00%
SA SILICA.....	30.00	30.00%
SA POTASH FELDSPAR..	20.00	20.00%

100.00

FORMULA & ANALYSIS

CaO....	.00	.07%
MgO....	.00	.12%
K2O....	.05	4.45%
Na2O...	.00	.21%
Fe2O3..	.00	.27%
MnO....	.00	.01%
TiO2...	.00	.34%
Al2O3..	.17	17.93%
SiO2...	1.24	76.60%
RATIO	7.26	
EXPAN	5.46	
WEIGHT	97.44	



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INSIGHT RECIPE CALCULATIONS.***Serina Kaolin body***

SERINA BODY

Serina.....	50.00	50.00%
SA SiLiCA.....	30.00	30.00%
SA POTASH FELDSPAR..	20.00	20.00%

100.00

FORMULA & ANALYSIS

CaO .	.00	.03%
MgO .	.00	.09%
K2O ..	.04	3.81%
Na2O .	.00	.18%
Fe2O3..	.00	.33%
TiO2...	.00	.24%
Al2O3..	.23	24.86%
SiO2...	1.10	70.46%
RATIO	4.82	
EXPAN	5.45	
WEIGHT	93.98	



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INSIGHT RECIPE CALCULATIONS.***S Kaolin body .***

S KAOLIN BODY

S Kaolin .	50.00	50.00%
SA SILICA. .	30.00	30.00%
POTASH FELDSPAR...	20.00	20.00%

100.00

FORMULA & ANALYSIS

CaO....	.00	.02%
MgO....	.00	.14%
K2O....	.04	3.97%
Na2O...	.00	.05%
Fe2O3..	.01	1.04%
MnO....	.00	.06%
TiO2...	.00	.32%
Al2O3.. "	.21	22.33%
SiO2...	1.14	72.07%

COST/KG .04

RATIO 5.49

EXPAN 5.44

WEIGHT 95.07



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EDAX ANALYSES

The analyses of SA Silica and SA K Feldspar are entered in the INSIGHT Materials Data Table (MDT).

Sa Silica Analysis

sa silica

Na20.....	.02	.02%
Si02.....	97.38	97.38%
Al203.....	1.93	1.93%
Fe203.....	.15	.15%
K20.....	.46	.46%
Ti02.....	.05	.05%

100.00

FORMULA & ANALYSIS

K20 .	.26	.46%
Na20 ..	.02	.02%
Fe203..	.05	.15%
Ti02...	.04	.05%
*Al203..	1.00	1.93%
Si02...	85.60	97.38%

COST/KG .04

RATIO 85.60

EXPAN 3.72

WEIGHT 5274.25



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Sa Potash Feldspar

SA POTASH FELDSPAR

Na20 .	.65	.65%
Si02 ..	66.43	66.44%
Al203 ..	18.83	18.83%
K20 .	14.08	14.08%

99.99

FORMULA & ANALYSIS

K20 ..	.81	14.08%
Na20 .	.06	.65%
*Al203..	1.00	18.83%
Si02...	6.00	66.44%

COST/KG .08

RATIO 6.00

EXPAN 8.42

WEIGHT 541.58