



UNIVERSITI PUTRA MALAYSIA

***FABRICATION AND EFFECT OF APPLIED FIELD STRESSES ON
STABILITY OF ZnO CERAMICS WITH CaMnO₃ AS ADDITIVE FOR
VARISTOR APPLICATION***

ISMAIL IBRAHIM LAKIN

FS 2015 78



**FABRICATION AND EFFECT OF APPLIED FIELD STRESSES ON
STABILITY OF ZnO CERAMICS WITH CaMnO₃ AS ADDITIVE FOR
VARISTOR APPLICATION**

By

ISMAIL IBRAHIM LAKIN

**Thesis Submitted to the school of Graduate Studies, Universiti Putra Malaysia,
in Fulfillment of the Requirements for the Degree of Master of Science.**

February 2014

COPYRIGHT

All materials contained within the thesis, including without limitation text, logos, icons, photographs and all other artwork, is copyright material of Universiti Putra Malaysia unless otherwise stated. Use may be made of any material contained within the thesis for non-commercial purposes from the copyright holder. Commercial use of material may only be made with the express, prior, written permission of Universiti Putra Malaysia.

Copyright © Universiti Putra Malaysia



DEDICATION

I hereby dedicate this thesis to the Almighty Allah who has been my help, sustainer, provider, guide, encouragement, keeper and my all in all throughout the course of my studies and also to my parents (Late Alhaji Ibrahim Lakin and Maimuna (Kande) Pate), whose prayers and support has kept me going. Finally to my brothers and sisters who are always by my side.



COPYRIGHT

UPM

Abstract of thesis presented to the Senate of Universiti Putra Malaysia in fulfillment of the requirement for the Degree of Master of Science

FABRICATION AND EFFECT OF APPLIED FIELD STRESSES ON STABILITY OF ZnO CERAMICS WITH CaMnO₃ AS ADDITIVE FOR VARISTOR APPLICATION

By

ISMAIL IBRAHIM LAKIN

February 2015

Chairman: Professor Azmi Zakaria, PhD

Faculty: Science

The major challenge in the continuing development of varistor has been to reduce the energy loss which is due to temperature and applied field stresses and to attain a good stability. The aims of this study are; to study the effect of CaMnO₃ (CMO) contents on nonlinearity coefficient (α) enhancement of ZnO based varistor ceramics; and secondly to study the nonlinear stability of this ceramic against DC electrical field and thermal stresses as function of CMO contents. The first aim has been carried out by synthesis of ZnO + xCMO ceramics by citrate gel coating technique, where x ranging from 3 – 7 mol% and sintered at various sintering times from 1 – 3 hrs. The prepared samples were characterized by using TG/DTA, EDX, SEM, XRD, and I-V measurements. The second aim was carried out by choosing the samples with best electrical properties subjecting them simultaneously to stresses of specific temperature and DC voltage over a certain period of time to study the degree of degradation. XRD analysis shows that the main phase in the material systems was ZnO while CMO as the secondary phase increase gradually with the increase of mol%, x. The TG/DTA analysis shows that, good quality of ZnO-CMO can be achieved at calcination temperature above 650 °C. Average density of the ceramics in all systems has the same trend where it decreases with the increase of doping level and sintering time. The maximum grain size was found to be 23.4 μm at the highest sintering time at 3 hrs at 7 mol% CMO doping level, as Mn is a strong grain enhancer. The SEM and EDX results verified that Ca and Mn were distributed within the grain as well as in the grain boundaries and triple point junctions. The value of α was found to increase with amount of CMO up to 5 mol% concentration. An optimum sintering time of 3 hrs for 5 mol% doping level gave the best α , attaining a value of 42.3 which represent a high protective function of ZnO varistor. The DC stress has caused a decrease in varistor voltage, α , and also an increase in leakage current. After exposure to DC and heat stresses for 18 hours, the varistor ceramics experienced a slight drop in nonlinearity. Thus, the varistor ceramic samples exhibited a high level of leakage current compared to samples before degradation which indicated they have been degraded or deteriorated. The degradation percentage was calculated in terms of changes in varistor parameters before and after stress. It showed that sample with 3 mol% CMO possess lowest degradation

percentage. From this result, it was found that samples fabricated at 3 hrs sintering time have the best microstructure and electrical properties.



Abstrak tesis yang dikemukakan kepada Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk Ijazah Master Sains

FABRIKASI DAN DEGRADASI ZnO + CaMnO₃ SERAMIK VARISTOR BERVOLTAN RENDAH

Oleh

ISMAIL IBRAHIM LAKIN

Februari 2015

Pengerusi: Professor Azmi Zakaria, PhD

Fakulti: Science

Cabaran utama dalam pembangunan berterusan varistor adalah merendahkan kehilangan tenaga yang mana bersabit dengan tegasan-tegasan suhu dan medan gunaan, dan untuk mendapatkan kestabilan tinggi. Tujuan kajian ini adalah; mengkaji kesan kandungan CaMnO₃ (CMO) keatas peningkatan pekali tak-linear (α) seramik varistor berdasarkan ZnO; dan keduanya mengkaji kestabilan tak-linear seramik ini terhadap tegasan-tegasan medan elektrik DC dan terma sebagai fungsi kepada kandungan CMO. Objektif pertama telah dilakukan dengan mensintesis seramik ZnO + xCMO menerusi teknik salutan gel sitrat, yang mana x mencangkup dari 3 – 7 mol% dan disinter pada pelbagai masa sinteran dari 1 – 3 jam. Sampel tersedia dicirikan dengan menggunakan TG/DTA, EDX, SEM, XRD, and pengukuran I-V. Manakala untuk objektif kedua, sampel dari sistem dengan ciri-ciri elektrik terbaik di kenakan secara serentak tegasan-tegasan suhu dan voltan DC spesifik menerusi satu kala masa untuk mengkaji darjah degradasi. Analisis XRD menunjukkan bahawa fasa utama dalam sistem bahan adalah ZnO manakala CMO sebagai fasa sekunder bertambah secara perlahan dengan pertambahan mol% x. Analisis TG/DTA menunjukkan bahawa, kualiti baik dari ZnO-CMO boleh dicapai pada suhu pengkalsinan melebihi 650°C. Ketumpatan purata dari seramik dalam semua sistem mempunyai trend yang sama dimana ia mengecil dengan bertambahan paras pendopan dan masa pensinteran. Saiz butir maksimum yang didapati adalah 23.4 μm pada masa pensinteran tertinggi pada 3 jam dan pada paras pendopan 7 mol% CMO, kerana Mn adalah penumbuh butiran. Hasil-hasil SEM dan EDX membuktikan bahawa Ca dan Mn adalah tertabur didalam butiran juga didalam sempadan butiran dan simpang titik tiga. Nilai α didapati bertambah dengan amaun CMO sehingga ke kepekatan 5 mol%. Masa persinteran optimum adalah 3 jam untuk paras pendopan 5 mol% memberikan α terbaik, mencapai nilai 42.3 yang mana mewakili fungsi perlindungan tinggi dari seramik varistor ZnO. Tegasan DC menyebabkan penurunan pada voltan varistor, α , dan juga pertambahan dalam arus bocor. Selepas pendedahan kepada tegasan DC dan suhu untuk selama 18 jam, seramik varistor mengalami penurunan kecil dalam ketak-linear. Jadinya, sampel varistor seramik menunjukkan paras tinggi arus bocor berbanding dengan sampel sebelum degradasi yang mana menunjukkan mereka telah terdegradasi atau merosot. Peratus degradasi dikira dalam sebutan dari perubahan dalam parameter varistor sebelum dan

selepas tegasan. Ia menunjukkan bahawa sampel dengan 3 mol% CMO mempunyai peratusan degradasi terendah. Daripada hasil ini, adalah didapati bahawa sampel difabrikasi pada masa sintaran 3 jam mempunyai mikrostruktur dan sifat-sifat elektrik terbaik.



ACKNOWLEDGEMENTS

In the name of Allah, the most gracious and the most merciful who has thought man by pen. All thanks to Allah who has given me the opportunity to see this day, the day I have been dreaming of, may the peace and blessings of Allah be upon his noble prophet Muhammad (SAW). First of all, I would like to use this opportunity to express my heartfelt thankfulness to my supervisor Prof. Dr. Azmi Zakaria for his support, advice, guidance, and encouragement which helped me towards achieving this goal. My sincere appreciation also goes to members of my supervisory committee; Assoc. Prof. Dr. Halimah Mohammed Kamari, and Dr. Raba'ah Syahidah Aziz for kind guidance and support towards the completion of this project.

I would like to use this opportunity to thank my mentors; Dr. Yadollah Abdollahi and Wan Rafizah binti Wan Abdullah for their help, support and understanding throughout my programme lastly my love (Asiya Hassan) thank you for being there for me spiritually.

I would also like to extend my sincere gratitude to Kaduna State University (KASU) for the sponsorship, my appreciation also goes to Universiti Putra Malaysia for the opportunity given to pursue my goals.

I certify that a Thesis Examination Committee has met on 16 February 2015 to conduct the final examination of Ismail Ibrahim Lakin on his thesis entitled "Fabrication and Effect of Applied Field Stresses on Stability of ZnO Ceramics with CaMnO₃ as Additive for Varistor Application" in accordance with the Universities and University Colleges Act 1971 and the Constitution of the Universiti Putra Malaysia [P.U.(A) 106] 15 March 1998. The Committee recommends that the student be awarded the Master of Science.

Members of the Thesis Examination Committee were as follows:

Abdul Halim b Shaari, PhD

Professor
Faculty of Sciences
Universiti Putra Malaysia
(Chairman)

Zainal Abidin b Talib, PhD

Professor
Faculty of Sciences
Universiti Putra Malaysia
(Internal Examiner)

Shahrom bin Mahmud, PhD

Associate Professor
School of Physics
Universiti Sains Malaysia
(External Examiner)



ZULKARNAIN ZAINAL, PhD

Professor and Deputy Dean
School of Graduate Studies
Universiti Putra Malaysia

Date: 15 April 2015

This thesis was submitted to the Senate of Universiti Putra Malaysia and has been accepted as fulfillment of the requirements for the degree of Master of Science. The members of the Supervisory Committee were as follows:

Azmi Zakaria, PhD

Professor,
Faculty of Science,
Universiti Putra Malaysia
(Chairman)

Halimah Mohammed Kamari, PhD

Professor,
Faculty of Science,
Universiti Putra Malaysia
(Member)

Raba'ah Syahidah Aziz, PhD

Senior Lecturer,
Faculty of Science,
Universiti Putra Malaysia
(Member)

BUJANG BIN KIM HUAT, PhD

Professor and Dean
School of Graduate Studies
Universiti Putra Malaysia

Date:

Declaration by graduate student

I hereby confirm that:

- This thesis is my original work;
- Quotations, illustrations and citations have been duly referenced;
- This thesis has not been submitted previously or concurrently for any other degree at any other institutions;
- Intellectual property from the thesis and copyright of the thesis are fully-owned by Universiti Putra Malaysia (Research) Rules 2012;
- Written permission must be obtained from supervisor and the office of Deputy Vice-Chancellor (Research and Innovation) before thesis is published (in the form of written, printed or in electronic form) including books, journals, modules, proceedings, popular writings, seminar papers, manuscripts, posters, reports, lecture notes, learning modules or any other materials as stated in the Universiti Putra Malaysia (Research) Rules 2012;
- There is no plagiarism or data falsification/fabrication in the thesis, and scholarly integrity is upheld as according to the Universiti Putra Malaysia (Graduate Studies) Rules 2003 (Revision 2012-2013) and the Universiti Putra Malaysia (Research) Rules 2012. Thesis has undergone plagiarism detection software.

Signature: ----- Date: -----

Name and Matric No.: Ismail Ibrahim Lakin GS36445

Declaration by Members of Supervisory Committee

This is to confirm that:

- the research conducted and the writing of this thesis was under our supervision;
- supervision responsibilities as stated in the Universiti Putra Malaysia (Graduate Studies) Rules 2003 (Revision 2012-2013) were adhered to.

Signature: _____

Name of
Chairman of
Supervisory
Committee: _____

Signature: _____

Name of
Member of
Supervisory
Committee: _____

Signature: _____

Name of
Member of
Supervisory
Committee: _____

TABLE OF CONTENTS

ABSTRACT	Page
	i
ABSTRAK	iii
ACKNOWLEDGEMENTS	v
APPROVAL	vi
DECLARATION	viii
LIST OF TABLES	xvi
LIST OF FIGURES	xvii
LIST OF ABBREVIATIONS	xx

CHAPTER

1 INTRODUCTION	1
1.1 Introduction	1
1.2 Varistor: Low Voltage varistor	1
1.3 Zinc Oxide Based Varistor	2
1.4 Zinc Oxide	4
1.5 Calcium Manganite	5
1.6 Sintering	6
1.7 Electrical Characteristics	9
1.7.1 Degradation – Electrical Relationship	10
1.7.2 Nonlinear Current- Voltage Characteristics	11
1.7.3 Nonlinear Coefficient	13
1.8 Research Problems	14
1.9 Objectives	15
1.10 Hypothesis	15
1.11 Scope of Research	15
2 LITERATURE REVIEW	16
2.1 Introduction	16
2.2 Structure of Zinc Oxide Based Low Voltage Varistor	16
2.3 Role of Additives	19
2.3.1 Varistor Formers	20
2.3.2 Varistor Enhancers	21
2.3.3 Varistor Highlighters	21
2.4 Degradation in ZnO	21
3 METHODOLOGY	24
3.1 Introduction	24
3.2 Sample Preparation	24
3.2.1 Synthesis of CMO	24
3.2.2 Characterizations	27
3.3 Preparation of Low Voltage ZnO Based Varistor Ceramics at Various CMO mol%	27
3.3.1 ZnO + xCMO	27
3.3.2 Raw Materials	27

3.3.3	Weighing	28
3.3.4	Mixing, Heating and Drying	28
3.3.5	Calcination	28
3.3.6	Grinding, Addition of Binder (PVA) and Drying	29
3.3.7	Pelletizing	29
3.3.8	Sintering	29
3.3.9	Sample Preparation for Scanning Electron Microscope and Energy Dispersive X-Ray Analysis	29
3.3.10	Sample preparation for Current density-Electric field Measurements	29
3.4	Characterizations	31
3.4.1	X-Ray Diffraction	31
3.4.2	Scanning Electron Microscope	32
3.4.3	Energy Dispersive X-Ray	32
3.4.4	Average Relative Density Measurements	32
3.4.5	Average Grain Size Measurements	33
3.4.6	Thermogravimetric and Differential Thermal analysis	33
3.5	Double Schottky Barrier Model	34
3.6	Degradation Test	36
3.6.1	Application DC and Thermal Stresses of Chosen System	36
3.6.2	Degradation Measurements of Chosen System	36
4	RESULTS AND DISCUSSION	37
4.1	Introduction	37
4.2	Morphological Studies of All Systems	37
4.2.1	CaMnO ₃ (CMO)	37
4.2.2	XRD Phase Determination	39
4.2.3	Average Grain Size Analysis	43
4.2.4	SEM Result for ZnO + xCMO	47
4.2.5	Energy Dispersive X-ray Analysis	52
4.2.6	Average Relative Density Analysis	56
4.2.7	Thermogravimetric and Differential Thermal analysis	59
4.3	Electrical studies	60
4.3.1	Nonlinear Current-Voltage Characteristics	60
4.3.2	Degradation Behaviour of Selected Varistor Ceramics	70
5	CONCLUSION	75
5.1	Conclusion	75
5.2	Recommendation for Future Research	76
	REFERENCES	77
	APPENDICES	84
	BIODATA OF STUDENT	92
	LIST OF PUBLICATIONS	93

LIST OF TABLES

Table		Page
1.1	Electrical Characteristics of ZnO Varistors.	10
4.1	The variation of E_b , α and J_L values for ZnO-CMO varistor ceramics sintered for 1 hour.	64
4.2	The variation of E_b , α and J_L values for ZnO-CMO varistor ceramics sintered for 2 hour.	67
4.3	The variation of E_b , α and J_L values for ZnO-CMO varistor ceramics sintered for 3 hour.	70
4.4	The variation of J-E characteristics parameters of ZnO varistor ceramics doped with various CMO content after DC accelerated aging stress.	72

LIST OF FIGURES

Figure		Page
1.1	Wurtzite structure of ZnO	5
1.2	Ideal cubic perovskite crystalline structure formula	6
1.3	Basic phenomena occurring during sintering under the driving force for sintering, $\Delta(\gamma A)$	7
1.4	Large pore during sintering, where A and B are grains	8
1.5	Elimination of pores by instantaneous filling with liquid	8
1.6	Elimination of the liquid pocket by grains growth toward the liquid pocket center upon prolong sintering	9
1.7	Nonlinear Current-Voltage Characteristics Regions	12
2.1	ZnO structure	20
2.2	SEM for the standard sample	23
3.1	Flow chart of CMO Preparation	25
3.2	The research flow chart of ZnO + CMO varistor ceramic	26
3.3	Flow chart for I-V measurement	31
3.4	Double Schottky barrier model	35
4.1	XRD patterns for CMO Sintered at 900 °C for 1 hr	38
4.2	SEM micrograph for CMO Sintered at 900 °C for 1 hr	38
4.3	TG/DTA curves of CMO powder heated in air at heating rate of 10 °C/min	39
4.4	XRD patterns for ZnO based ceramics at 1300 °C for 1 hr sintering time at different CMO doping concentration	40
4.5	Scale of Reference for CMO Peaks Diffraction	41
4.6	XRD patterns for ZnO based ceramics at 1300 °C for 2 hrs sintering time at different CMO doping concentration	42
4.7	XRD patterns for ZnO based ceramics at 1300 °C for 3 hrs sintering time at different CMO doping concentration	43
4.8	Variation of grain Size with CMO doping level for 1 hr sintering time	44
4.9	Variation of grain Size with CMO doping level for 2 hrs sintering time	45
4.10	Variation of grain Size with CMO doping level for 3 hrs sintering time	46
4.11	Overall average grain sizes with Duration	47
4.12	SEM micrographs for ZnO doped with (a) 3 (b) 4 (c) 5 (d) 6 (e) 7 mol% CMO sintered at 1300 °C for 1 hr sintering time	49
4.13	SEM micrographs for ZnO doped with (a) 3 (b) 4 (c) 5 (d) 6 (e) 7 mol% CMO sintered at 1300 °C for 2 hrs sintering time	50

4.14	SEM micrographs for ZnO doped with (a) 3 (b) 4 (c) 5 (d) 6 (e) 7 mol% CMO sintered at 1300 °C for 3 hrs sintering time	51
4.15	EDX micrographs and spectra of CMO doped Varistor ceramics at 1300 °C for 1 hr	53
4.16	EDX micrographs and spectra of CMO doped Varistor ceramics at 1300 °C for 2 hrs	54
4.17	EDX micrographs and spectra of CMO doped Varistor ceramics at 1300 °C for 3 hrs	55
4.18	Density variation with CMO doping level for 1 hr sintering time	57
4.19	Density variation with CMO doping level for 2 hrs sintering time	58
4.20	Density variation with CMO doping level for 3 hrs sintering time	59
4.21	Overall relative densities with Duration	59
4.22	TG/DTA curves of ZnO-CMO powder heated in air at heating rate of 10 °C/min.	60
4.23	J-E curve of varistor ceramics at five different CMO concentrations sintered for 1 hr	61
4.24	α curve of varistor ceramics at five different CMO concentrations sintered for 1 hr	62
4.25	The variation of varistor voltage with various CMO doping level sintered for 1 hr	63
4.26	The variation of leakage current density with various CMO doping level sintered for 1 hr	63
4.27	J-E curve of varistor ceramics at 5 different CMO concentrations sintered for 2 hrs	65
4.28	α curve of varistor ceramics at 5 different CMO concentrations sintered for 2 hrs	65
4.29	The variation of varistor voltage with various CMO doping level sintered for 2 hrs	66
4.30	The variation of leakage current density with various CMO doping level sintered for 2 hrs	66
4.31	J-E curve of varistor ceramics at five different CMO concentrations sintered for 3 hrs	68
4.32	α curve of varistor ceramics at five different CMO concentrations sintered for 3 hrs	68
4.33	The variation of varistor voltage with various CMO doping level sintered for 3 hrs	69
4.34	The variation of leakage current density with various CMO doping level sintered for 3 hrs	69
4.35	Leakage current of ZnO varistor ceramics during DC stress with various CMO contents. (a) 3 mol%, (b) 4 mol% (c) 5 mol% (d) 6 mol% and (e) 7 mol%	71

4.36	J-E characteristics behaviour of various CMO mol% added ZnO-based ceramics before and after applying DC accelerated aging stress; (a) 3 mol%, (b) 4 mol% (c) 5 mol% (d) 6 mol% and (e) 7 mol%	73
B.1	Chart for Pre-sintering process	90
B.2	Chart for sintering process	90
B.3	Replicate of the ImageJ method for the average grain size measurement	91



LIST OF ABBREVIATIONS

I	Current
V	Voltage
α	Nonlinear coefficient
K	Material constant
$^{\circ}\text{C}$	Degree celcius
$a=b=c$	Lattice constant of ZnO wurtzite structure
\AA	Angstrom
ρ	Resistivity
x	Doping level of dopant (mol %)
d	Spacing between the lattice planes in the crystals
Z	Atomic number
J_L	Leakage current density
I_L	Leakage current
V_{on}	Varistor Voltage
E_b	Breakdown voltage
V_T	Threshold voltage
θ	Angle of diffraction
λ	Wavelength of the X-ray (0.154nm for $\text{CuK}\alpha$)
ρ	Density
ρ_{water}	Density of water (1 gm^{-3})
W_{air}	Weight of pellet in air
W_{water}	Weight of pellet in water
I_1	1 mA
I_2	10 mA
V_1	Voltage corresponding to I_1
V_2	Voltage corresponding to I_2
$\rho_{\text{theoretical}}$	Theoretical density of ZnO

ΔE_b	Variation rate of breakdown voltage
$\Delta \alpha$	Variation rate of nonlinear coefficient
ΔI_L	Variation rate of leakage current
K_T	Degradation rate coefficient
Zn_n	Zinc



CHAPTER 1

INTRODUCTION

1.1 Introduction

In this chapter, Zinc Oxide (ZnO) varistor ceramic is being introduced and discussed in detail. This includes the application of ZnO and what makes them to be highly demanded and become the focus of interest of many researchers in the field of solid state semiconductor ceramic devices. The basic operation of ZnO varistor concern of how it works as electronic device in the field of circuit over voltage protection has been discussed. Lastly, research problems, scope of research and objectives of this present research work have been outlined in this section. This work focuses on effect of Calcium Manganite (CaMnO_3) as dopant on nonlinear coefficient (α), electrical properties, degradation and stability of ZnO varistor.

1.2 Varistor: Low Voltage varistor

A varistor is a device that exhibit non-ohmic behaviour with resistivity values dependent on the applied voltage. It is used as a protective device to regulate transient voltage surges of unwanted magnitudes by shunting them to the ground. The unwanted magnitudes refer to over voltage transients that damage the operating voltage of the equipment being protected. These transients are generated due to the phenomena internal to the equipment, or of atmospheric origin. Therefore, the transients are inherent in the electrical system (Das, 2010).

These excess energy and over voltage are hazardous to electrical appliances and electrical circuits. It can cause power system failures which can result in huge losses of product output. These transients occurs a few thousand times a year for a typical household and office premises. Nowadays, ZnO varistor plays a major role in preventing these power surges from causing power failures.

The varistor works in similar way as a back-to-back Zener diode and usually placed in parallel with circuits to protect them from voltage surges. A good protector would contain at least three varistors, two connected to the live wire and the other is connected to the neutral wire. The second varistor component can continue the protection service if the first varistor fails after many years of service. This is why several varistors are arranged in parallel to each other, so that it can survive for more than half a century under normal condition. Normally, varistors are usually connected close to the protected device and located at the incoming power lines before the power supply reaches the circuitry being protected for optimum protective performance. For offices and households, the normal power supply is 240 volts (rms). If a transient over voltage of 300 volts (rms) is transmitted through the household socket, the varistor will perform its action. The varistor will immediately detect the presence of the transients in nanoseconds speed, it will absorb most of the power voltage transients voltage energy and redirect (or shunt) the remaining transient energy to the ground.

A varistor is not a perfect conductor but when energy is absorbed by a varistor, the varistor becomes more conductive and therefore, its life expectancy increases exponentially as varistor rating is increased. The normal ratings of the varistor components are either 25 volts (rms) for low voltage varistor or 300 volts (rms) for high voltage varistor. A varistor failure can be avoided by significantly increasing varistor energy ratings by using a varistor of higher joules or by connecting more varistor devices in parallel. Discrete component varistor have rather high breakdown voltage (≈ 50 V), well above the safe applied voltage levels for silicon devices. For the past decades, the usual methods for producing low-voltage varistors involved either grinding down a conventional disk varistor or promoting large grains in the sintered material. Use of titanium dioxide (TiO_2) as additive to promote secondary recrystallization has been employed, but suffers from limited control over final grain size (Trontelj et al., 1986). The second method employs a pre-sintered pure ZnO substrate material into which varistor additives are diffused. This may either be from screen printed paste of the additives (Schwing and Hoffmann, 1981) or solid dopant layer sandwiched between two ZnO substrates (Selim et al., 1980). Both methods produce workable device but with small active area that limit the current capabilities.

To achieve lower voltage reliability, a method of producing thin varistor layers had been devised. Shohata et al., (1981) successfully fabricated multilayer varistor by tape casting or laminating process used to produce multilayer capacitors. This technique enable the production of extremely thin resistor layer of the order of $20 \mu\text{m}$ compared to the 0.5 mm achieved through die pressing. By reducing the number of grains between the electrodes, the varistor's breakdown voltage can be reduced to a lower limit of approximately 4 V. Meanwhile increasing the area of the varistor potentials increases current handling capabilities.

1.3 Zinc Oxide Based Varistor

ZnO based varistor is one of the success phenomena of solid state semiconductor ceramic devices and become the preferred approach technology predominantly in the field of circuit overvoltage protection. Varistor are defined as voltage dependent Resistor (VDR). The resistivity of ZnO varistor depends upon the applied voltages, where the resistivity is very high below the breakdown voltage (V_b) but becomes very low at voltages above V_b (Nahm, 2004). Therefore, the varistor is so-called voltage dependent resistor. V_b is the minimum voltages that cause a set of insulator to become conductor. ZnO varistors are widely used as valve electronic devices of lightning arrestors for protecting electrical power lines or as surges absorbers to protect electronic components against voltage surges. In summary, ZnO varistor is a ceramic semiconductor used to protect electrical and electronic systems against dangerous overvoltage surges, switching surges, electromagnetic transient surges, and electrostatic discharges (Nahm, 2005).

A varistor function is to conduct significantly increased current when voltage is excessive. Before the invention of the ZnO varistor, silicon carbide is widely used in protection system (SIMOES et al., 2006). Then, ZnO become commercial and attract more attention due to excellent nonlinear current – voltage (I-V) characteristics and their high energy withstanding capabilities. In less than 30 years of its discovery, the varistor now become widespread in the application of varistor as voltage surge

protectors in the electrical circuits (Bai et al., 1995). More than two billion of this kind of varistors have been manufactured by now and their popularity is rapidly increasing due to their low cost, high amazing versatility and ability to absorb large amount of energy (Bernik and Daneu, 2007). Moreover, due to their superior electrical properties, increasing number of ZnO varistors is now being used in automobiles.

This Metal Oxide Varistor (MOV) contains metal oxides such as small amount of bismuth, cobalt, manganese e.t.c that can affect the varistor properties in matrix with ZnO grains. ZnO ceramic alone cannot exhibit a nonlinear behaviour without doping the heavy elements with large ionic radii such as Ba, Pr, Bi etc (Nahm and Park, 2000). Currently, these ceramics are produced with minor addition of typically Bi₂O₃, Sb₂O₃, CoO, MnO₂, CaMnO₃, and Cr₂O₃.

The characteristics of varistor ceramics are closely related to the microstructure (Bernik and Daneu, 2007) where each dopant plays an important role to improve the non-ohmic properties of ZnO varistor. ZnO varistor exhibit high nonlinearity and stability with many additives (Nahm, 2003). In addition to nonlinearity, the electrical stability is technologically very important characteristics of ZnO varistors.

The relationship between the voltage across the terminals, V, and the current in the device, I, is typically expressed by

$$I = KV^\alpha. \quad (1.1)$$

where

K = constant

α = nonlinearity coefficient

The nonlinear I-V characteristics of ZnO varistors are attributed to a double Schottky barrier formed to the grain boundaries, which are essentially formed by the segregation of varistor forming oxides towards the ZnO grain boundaries.

The main properties of ZnO varistors are;

- a. High energy absorption capability ranging from a few joules for smaller models and up to thousands of kilojoules for larger models.
- b. ZnO can sense and clamp transients repeatedly, in thousands of times without being destroyed.
- c. ZnO varistor have superfast response to over voltage transients whereby they can sense and clamp transients in nanoseconds speed.
- d. High nonlinear coefficient values ranging from tenths to hundreds.
- e. Small size with various geometries and design.
- f. Low power loss of only 10 – 100 W/cm³.
- g. Long life span of more than 10 years.
- h. Highly versatile, it is applicable both in low voltage and mega voltage.

Regarding to the unique properties of ZnO listed above, lots of attention has been shifted to these ZnO varistors. Moreover, the collaboration between ZnO varistor and dopants are incredible phenomena in device civilization for industrial applications. A lot of work has been done on the ZnO varistor system and further investigations are still going on in order to enhance the varistor performances.

1.4 Zinc Oxide

Zinc Oxide (ZnO) is a polycrystalline solid material and it is widely used in the manufacturing of paints, plastics, glass, cement, rubber products, cosmetics, textiles, inks, soaps, pharmaceuticals, floor covering, batteries, adhesive and many other products. It is also used in the fields of UV devices, chemical and gas sensor, piezoelectric transducers, light emitting diodes, lasers (Eda, 1978) and varistors.

ZnO occurs as a white powder with a common name zinc white. ZnO is nearly insoluble in water but soluble in acids and alkalis. ZnO would change colour from white to yellow when it is heated. ZnO has a density of 5.606g/cm³ and with a melting point of 1975 °C. The resistivity of ZnO ranges from 1 to 100 Ωm, which corresponds to the electron concentration of the order of 10²¹-10²³ m⁻³. ZnO has several other favourable properties such as good transparency, high electron mobility, wide band gap and strong room temperature luminescence where those properties already used in heat protecting windows and electronic applications as thin film transistors and light emitting diodes.

ZnO is a group II -VI semiconducting compound because Zinc and Oxygen belongs to 2nd and 6th groups of the periodic table respectively. ZnO Oxide becomes a great interest for electronic and photonic devices it is also studied for a variety of applications. ZnO has a wide band gap of 3.37 eV at room temperature and large excitation binding energy of 60 MeV that are technologically important in the application for short wavelength optical devices such as ultraviolet, violet, blue light, emitting diodes and laser diodes. It is also important in the development of electronic and optoelectronic devices (Srinivasan and Kumar, 2008).

The advantages of wide band is higher breakdown voltage, ability to sustain large electric field, lower electronic noise and power operation that make ZnO as one of the most promising material for electronic applications. Pure ZnO is an n-type intrinsic semiconductor where the intricity is due to Zinc interstitial and oxygen deficiency. In commercial varistor, ZnO has to be doped with elements such as Co, Sb, Mn, Ni, Mg and Bi.

ZnO has a wurtzite structure as shown in Figure 1.1. The physical properties of ZnO are as follows;

- i) Perfect ZnO crystals exist in the hexagonal wurtzite structure,
- ii) The ZnO lattice type is hexagonally close packed in which oxygen atoms are arranged and half of the tetrahedral sites filled up by zinc atoms,
- iii) Zinc and oxygen atoms are tetrahedrally coordinated giving rise to equal positioning to each other,
- iv) The mean lattice constant of the wurtzite structure are $a = b = 3.257\text{Å}$ and $c = 5.213\text{Å}$ which gives a unit cell of volume 47.9Å³.

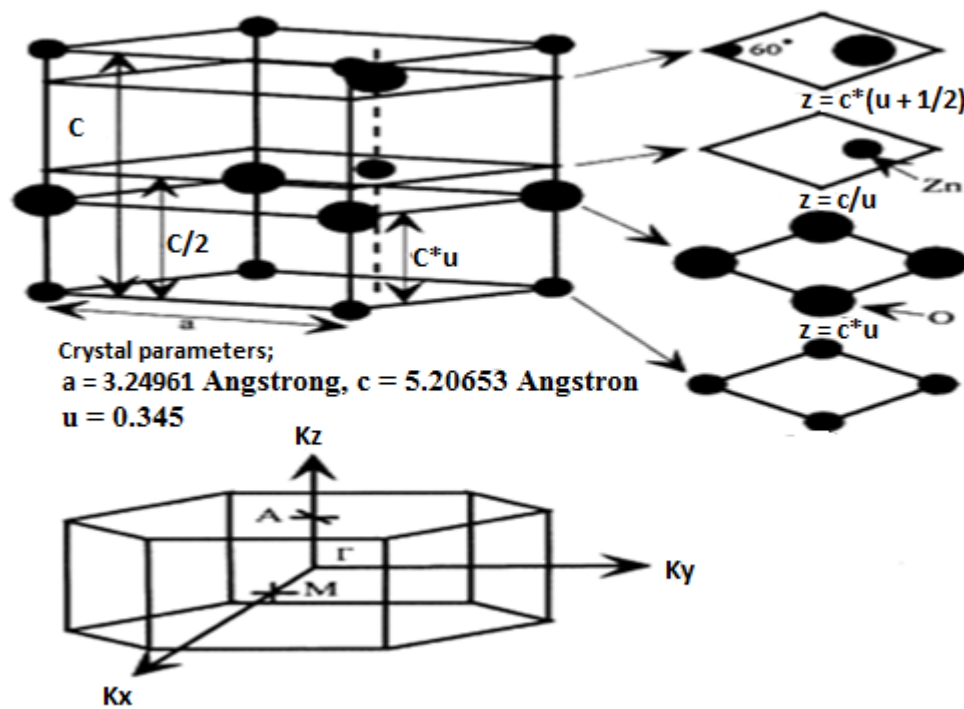


Figure 1.1: Wurtzite structure of ZnO (Oshikiri et al., 2001)

The ZnO structure is relatively open, all of the octahedral and half of the tetrahedral sites are empty. So, external dopants easily incorporate into the ZnO lattice (Mahan, 1983). Therefore dopants such as manganese (Mn) can easily occupy these empty sites and improve the nonlinear current – voltage characteristics in ZnO varistor by affecting the defect chemistry at the grain boundary (Han et al., 2002). There are different opinions about the dominant intrinsic defect that occur in the ZnO and have long been a subject of controversial discussion in the literature. The electron density measurements have shown that dominant defects are interstitial zinc ions. However, other investigations suggest that it is oxygen vacancies that predominate in pure ZnO.

1.5 Calcium Manganite

Calcium manganite (CMO) Transition metal oxides with perovskite-type structure are attractive materials for thermoelectric applications. The properties of these materials originate from strong interactions between the d-state electrons of the transition metal atoms (Alfaruq et al., 2012). Perovskite type manganates are well known for their high magnetoresistance which can be explained by double-exchange model. CMO is an antiferromagnetic insulator that was extensively studied in recent years, the mixed valence of Mn^{3+} and Mn^{4+} as function of the elemental composition strongly govern the physical properties (e.g thermoelectric properties) of manganates. An alternative way to modify the physical properties is by changing the

morphology of the samples, e.g., by creating low dimensional structures or nanostructures (Wiebe et al., 2001).

Early neutron diffraction experiments performed on stoichiometric CMO indicate an orthorhombic perovskite structure ($a = \sqrt{2}a_c$, $b = 2a_c$, $c = \sqrt{2}a_c$ where a_c = cell constant of cubic perovskite). And it is antiferromagnetic insulator with a Neel temperature (T_N) of 120K. CMO also exhibit a ferromagnetism below Neel temperature (Macchesney et al., 1967).

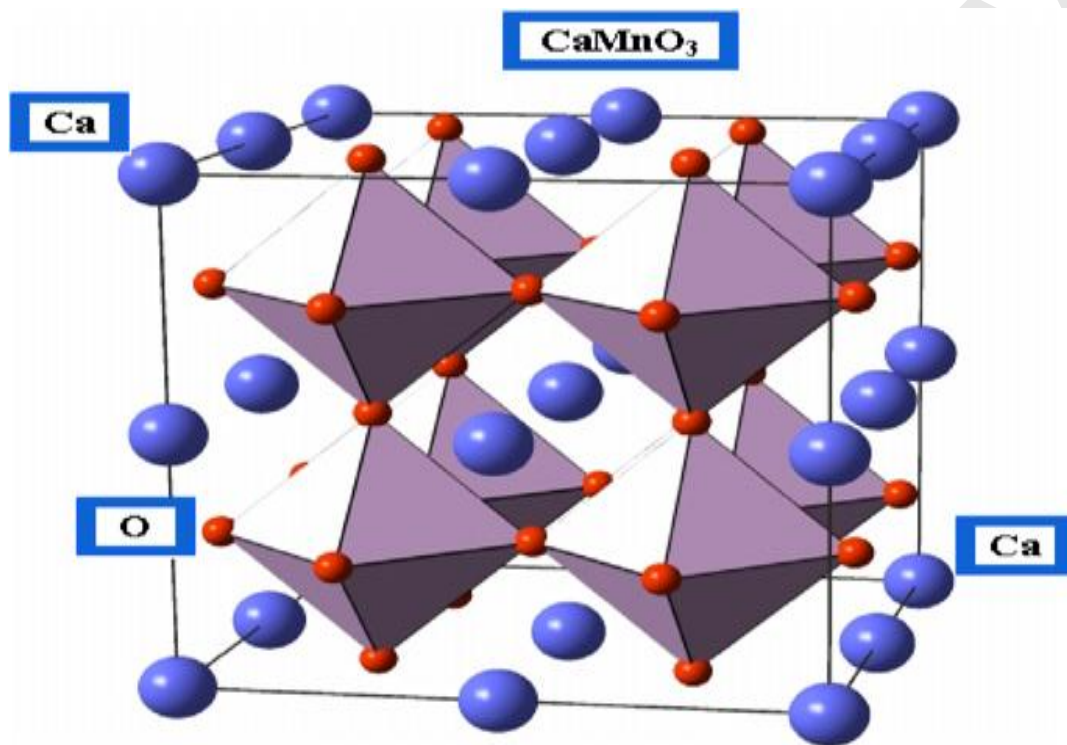


Figure 1.2: Ideal cubic perovskite crystalline structure formula (Hamdad and Bouhafs, 2010)

1.6 Sintering

Sintering is a method for making objects from powder, by heating the material until its particle adheres to each other. In other words it refers to powder compacting process by applying thermal treatment. Sintering is also a processing technique used to produce density-controlled materials and components from metals and ceramic powders by the use of thermal energy.

Sintering originated in the era of firing pottery. Since 1940's, sintering was studied fundamentally, scientifically and then, a remarkable in sintering science have been made. In the sintering step, there are various techniques and processing variables which can produce variations in the micro structure and results of the sintered body. In general, the aim of sintering is to produce sintered parts with reproducible and, if possible, designed microstructure through control of sintering variables.

Microstructure control including the control of grain size, sintered density, pores and also size and distribution of other phases. In most cases, the final aim of sintering is to control both densification and grain growth process (Figure 1.3).

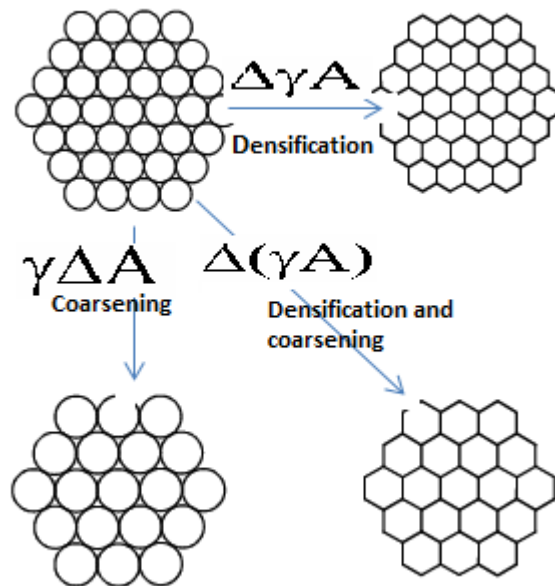


Figure 1.3: Basic phenomena occurring during sintering under the driving force for sintering, $\Delta(\gamma A)$

<http://v5.books.elsevier.com/bookscat/samples/9780750663854/4355-Kang-01.pdf>

Densification is the act of reducing porosity in a sample thereby making it dense. Grain growth is the process of grain boundary motion; hence increase the average grain size. A great change in microstructure properties is technologically important in order to produce a better varistor performance. Liquid phase sintering is a consolidation technique of powder compacts containing more than one component at the temperature above the solidus of the components in the presence of liquid. It is essential to have an amount of liquid phase that is large in size, a near complete solubility of the solid in the liquid, and wetting of the solid by the liquid for densification to occur. Densifications usually occur in the solid state during heating of powder mixture compact. Densification is derived from capillary pressure of the liquid phase located between the fine solid particles. A capillary pressure is developed when the liquid wets the solid particle and each space between the particles becomes a capillary. Liquid flows in to fine capillaries due to the capillaries pressure difference between the fine and coarse channels between solid particles and the solid particles can be redistributed by this liquid flow.

In final sintering stage, pores are present at grain boundary and particularly at triple junction and inhibit grain growth. During liquid phase sintering, most of the sites of particles melted and become pores because of liquid flow into fine capillary between solid particles. As sintering proceeds, elimination of pores and grain growth occur in the liquid matrix (Figure 1.5). The capillary pressure exerts on a particle hence, the solubility of the atoms in the particles increases in the matrix. When particles of different size are dispersed in liquid, material transport occurs from small to large

grains because of the difference in the solubility between the grains. The small grains dissolve and large grains grow further and therefore the average grain size increases (Figure 1.6).

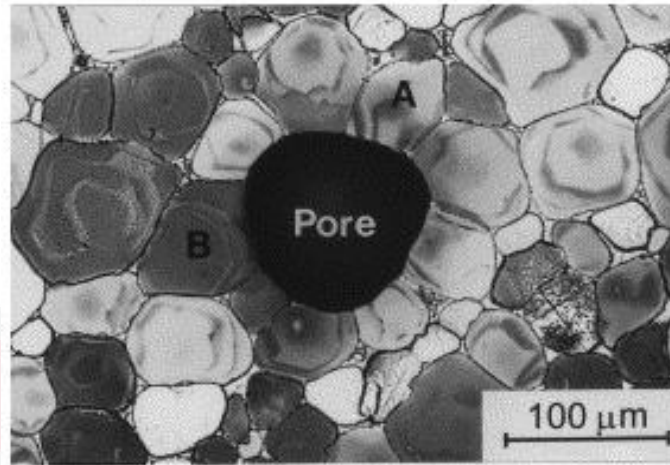


Figure 1.4: Large pore during sintering, where A and B are grains

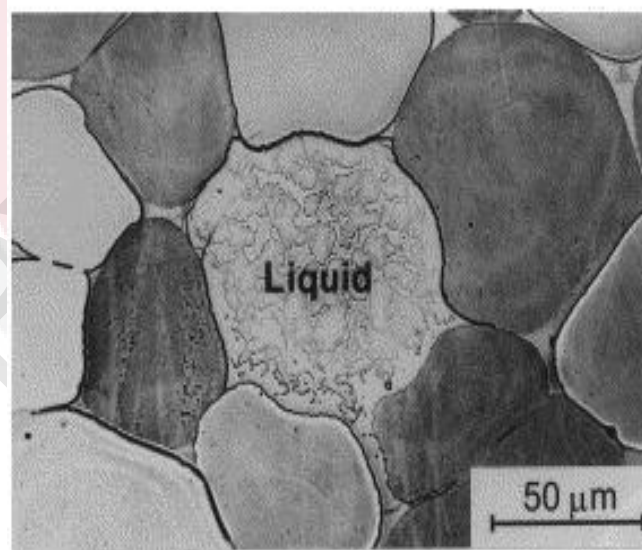


Figure 1.5: Elimination of pores by instantaneous filling with liquid

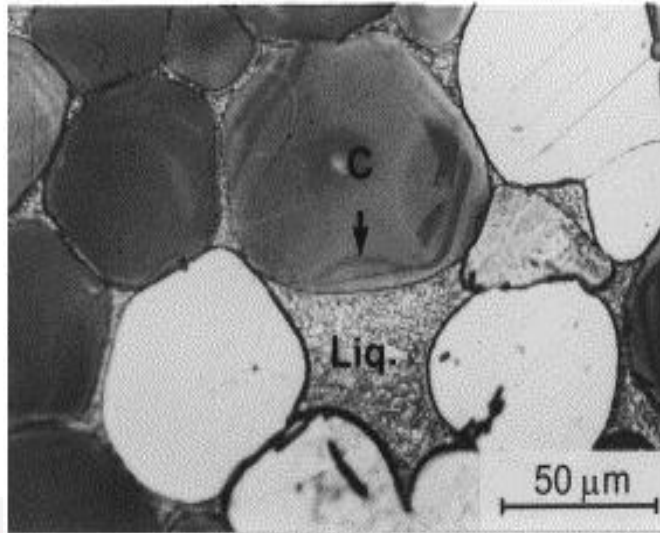


Figure 1.6: Elimination of the liquid pocket by grains growth toward the liquid pocket center upon prolong sintering. (Lee and Kang, 1998)

Grains growth happens due to the motion of the atoms across a grain boundary. Grain growth is divided into two parts, normal and abnormal grain growth. Normal grain growth is a simple and invariable distribution of relative grain size. Abnormal grain growth occurs by the formation of some exceptionally large grains in a matrix of fine grains and also due to the presence of large grains in the matrix, material containing second phase and also impurities of high concentration.

1.7 Electrical Characteristics

The combination properties of ZnO varistor such as nonohmic behaviour, large energy handling capabilities and their amazing versatility make them a very high demand protective device to regulate transient voltage surges of unwanted magnitudes. ZnO varistor have energy handling capabilities as high as 300 J/cm^3 . Some other investigators reported the achieving of energy handling capabilities up to 1000 J/cm^3 . Their ability to absorb or handle energy levels are important because most materials would vaporize if they are expose to energy levels even less than 100 J/cm^3 .

The very thin grain boundaries of ZnO varistor have amazingly high resistivity in the range of $10^8 - 10^{12} \Omega \cdot \text{cm}$ compared to ZnO grains which have the resistivity of $1-10 \Omega \cdot \text{cm}$. The difference between ZnO grain and ZnO boundary resistivity is the existence of electrostatic potential barrier located at the depletion layers inside the ZnO grain, very close to the grain boundaries. The concentrations of donors inside the depletion region create trap states that prevent the flow of charge carriers across the grain boundaries. Therefore, large potential barriers exist at the area close to the grain boundaries.

Table 1.1: Electrical Characteristics of ZnO Varistors

ZnO Varistor Characteristics	Electrical Characteristics Values
Depletion Layer Thickness	50-100 nm
Grain Boundary Resistivity	$10^8 - 10^{12} \Omega \cdot \text{cm}$
Grain resistivity	1 – 10 $\Omega \cdot \text{cm}$
Donor Concentration	$10^{17} / \text{cm}^3$
Interfacial Trap Density	$10^{14} / \text{cm}^2$
Nonlinear Voltage Range	1 V – 10 kV
Nonlinear Coefficient (α)	10 - 100
Energy Absorption Capability	100 – 300 J/cm^3
Response Time	5 -10 ns
Power Loss	10– 100 mW/cm^3

The very thin grain boundaries of ZnO varistor have amazingly high resistivity in the range of $10^8 - 10^{12} \Omega \cdot \text{cm}$ compared to ZnO grains which have the resistivity of 1-10 $\Omega \cdot \text{cm}$. The difference between ZnO grain and ZnO boundary resistivity is the existence of electrostatic potential barrier located at the depletion layers inside the ZnO grain, very close to the grain boundaries. The concentrations of donors inside the depletion region create trap states that prevent the flow of charge carriers across the grain boundaries. Therefore, large potential barriers exist at the area close to the grain boundaries.

1.7.1 Degradation – Electrical Relationship

ZnO based varistors are widely used to protect circuits against excessive transient voltages by incorporating them into the circuit in such a way that, when triggered, they will shunt the current created by the high voltage away from the sensitive components because of their extreme nonlinearity in their I-V characteristics. The chosen suitable additives are the main tools that are used to improve the nonlinear response and the stability of ZnO varistor ceramics (Eda, 1989). Therefore, the stability of ZnO based varistor ceramics against constant biases, AC and DC or voltage surge is recognized as one of crucial subjects to be investigated (Gupta, 1990). In practical application, ZnO varistors are always subjected to a continuous electrical stress, switching surge and lightning surge. If the stability against these stresses is poor, the application of such varistor is extremely limited even if the nonlinearity is high. The ZnO varistor begin to degrade due to the gradual increase in

leakage current with stress time. Eventually, they cause thermal runaway and loss of varistor function. Therefore, the stability of varistor is more important than any other varistor property. In addition to nonlinearity, the electrical stability is a technologically important characteristic of ZnO varistor. The stability of varistors can be estimated from the empirical equation: $I_L = I_{L0} + K_T t^{1/2}$. where K_T , is the degradation rate coefficient indicating the aging degree. The lower the K_T value, the better the stability.

1.7.2 Nonlinear Current- Voltage Characteristics

Due to the strong semiconducting behaviour of ZnO varistors, many prominent varistor scientists such as (Matsuoka 1971 and Clarke, 1999) have reported that the most important property of ZnO varistor is its nonlinear current-voltage (I-V) characteristics, as shown in Figure 1.7. Since ZnO varistors are manufactured with many voltage and current ratings, the diameter and its thickness values would have large variations, from a few millimetres to 400 millimetres in diameter and from micrometres to 40 centimetres in thickness. Consequently the current density-electric field (J-E) graph will also experience big variations in terms of its shape and turning points. Therefore if the varistor samples have large physical variations, it would be wise to report the current and voltage values with respect to a certain denominator; that is current is represented by current density J (amperes/cm²) while voltage is represented by electric field E (voltage/cm). However, if an analysis is focused on a certain model, say low – voltage models, then the current-voltage (I-V) characteristics do not vary that much; therefore it is relatively accurate if the common denominator is not used.

J-E curve has three characteristic regions which are the pre-breakdown region (the sleep mode), the breakdown region (triggered mode) and the upturn region (the high current zone).

Pre-Breakdown Region

In this low-current region, the ZnO varistor acts as an ohmic resistor. Current increases linearly with voltage and the resistivity (or resistance) can be directly calculated from the slope of the J-E Graph in Figure 1.7. This pre-breakdown region is the “**sleep mode**” of the varistor whereby the varistor action is not triggered and it does not interact with the normal operation of the electrical circuit being protected. This ohmic region normally ranges from a current density of 1 nA/cm² up to 0.1mA/cm², which is a variation of up to six orders of magnitude. With regard to varistor application, this pre-switch region refers to the region of operation in the absence of all over-voltage transients.

Another name of this pre-switch region is leakage region that corresponds to the presence of a small leakage current ((Kutty and Ezhilvalavan, 1996) and (Clarke, 1999)). For commercial use, this leakage current must be lower than 60 μ A/cm² in order to reduce to the watt loss of the circuit being protected.

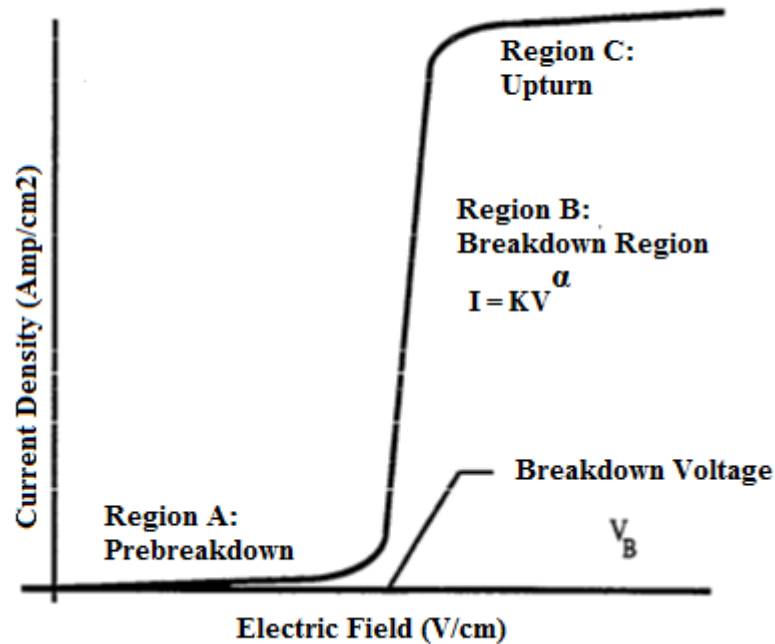


Figure 1.7: Nonlinear Current density-Electric field Characteristics Regions.
(Nies, 1989)

This watt loss can be regarded as an amount of energy stolen from the power supply during the normal operation of circuit, and this stolen energy would reduce the power efficiency of the circuit and also it can make the resistor to become hot.

Breakdown Region

In this current-voltage region, the ZnO varistor acts as a very good conductor and as a very effective power surge absorber. From the J-E graph in Figure 1.7, flat peak of the graph refers to the switched region; the flatter peak, the better the protective function of the varistor.

The breakdown region, also called the nonlinear region, has one critical point known as switch-on voltage (V_{on}). It is also known as threshold Voltage or onset voltage. The switched-on voltage (V_{on}) is the voltage at which the varistor action is triggered. One intriguing fact about the switch-on voltage (V_{on}) is that, it is conveniently chosen to be 0.5 mA/cm² current density or the voltage at 1mA. This chosen voltage (V_{1mA}) is found to be a convenient measuring parameter for varistor manufacturers to compare ZnO varistors of different voltage ratings. Another reason for choosing V_{1mA} as the critical parameter is that, most ZnO varistors exhibit the minimum nonlinearity at current value of about 1 mA. V_{on} must be at least 20% higher than the steady-state voltage of the normal operation of the circuit being protected by the varistor. This more than 20% voltage requirement is set by varistor manufacturers

and varistor buyers. If the switch-on voltage is less than 20%, there will a danger of premature triggering of the varistor action that can cause harm to the circuit.

If the incoming supply voltage to the circuit suddenly increases to a dangerous level, that is more than 20%, then the varistor action of the ZnO varistor will be “switched on”. When the varistor senses over voltage, it becomes highly conductive and conducts the large quantity of current from the transient; thus preventing the damaging over-voltage from reaching the circuitry.

The current-voltage (I-V) characteristics in this nonlinear region do not obey Ohm’s law because the resistivity (ρ) of the varistor changes at different voltage values. For both the pre-switch and switched regions, the electrical characteristics of the ZnO varistor is controlled by the ZnO grain boundaries. Grain boundary resistivity, Grain boundary potential barrier, depletion layers and interfacial trap states are the grain boundary phenomena that contribute to the electrical characteristics of ZnO varistor.

Upturn Region

The upturn region is also called high-current region due to the high impulse current that the ZnO varistor has to endure. Because the ZnO grains becomes the controlling parameter that determine how the current-voltage characteristics response to transient surges, where the grain boundary potential barrier is completely removed by the large electric fields from the transients.

Referring to Figure 1.7, the onset of the upturn region also called E_{upon} can also be written as V_{upon} . The upturn onset electric field (E_{upon}) occurs at about $100\text{A}/\text{cm}^2$ current density; and for low- voltage varistors, it may be about $1\text{A}/\text{cm}^2$ current density. One unique characteristic about the high current region is that the ZnO varistor becomes more ohmic as the current/voltage increases, in which the current density-electric field (J-E) graph appears like a straight line.

Another crucial property of this high current region is that, the high current surges can cause permanent damage, physically and electrically on ZnO varistor; which almost means that the electrical properties are no longer reversible. In most cases, the electrical properties of the ZnO varistor become worse after every encounter with a high current transient surge. But luckily enough, high current surges do not occur regularly since they are cause by lightning and serious power faults.

The upturn region can extend up to a few thousands amperes/ cm^2 current density or until the ZnO device is physically destroyed. For low-voltage varistors, the upturn region ranges from $0.1\text{ A}/\text{cm}^2$ to $100\text{A}/\text{cm}^2$ current density. Higher voltage varistor models can withstand higher level current surges up to one million amperes.

1.7.3 Nonlinear Coefficient

The nonlinear coefficient (α) is the most important property of the varistor because it is the heart of the varistor action that provides the protection against over-voltage transient surges (Wang et al., 2008). Over-voltage transient triggers the varistor to transform from a highly resistive state ($\rho \sim 10^{12}\ \Omega.\text{cm}$) into a highly conductive state

($\rho < 10$) in just a few nanoseconds, thus short-circuiting the incoming transient into the varistor device.

The higher the nonlinear coefficient value, the better the protection function of the varistor. The nonlinear coefficient equation is derived from the current – voltage (I-V) characteristics in switched region (Figure 1.7). The transformation from a highly resistive into a highly conductive state is made possible by the highest value of nonlinear coefficient of ZnO varistor.

The majority carriers (electrons) are rich with kinetic energy which allow them to cross the potential barrier at the grain boundary, thus gives the highest value of nonlinear coefficient. ZnO gives the highest value of nonlinear coefficient (α) if compared with any other varistor materials; this property makes ZnO the best choice for protection. Older varistor materials such as silicon carbide and selenium have much lower α value which explains why they are totally replaced with ZnO varistors. Pure resistors should have α value equal to 1 because referring to equation 1.1, if $\alpha = 1$ the equation becomes $I = KV$ which is the equation of straight line that agrees with Ohm's law. Here K is constant that is known as reciprocal of resistance, that is $K = 1/R$.

1.8 Research Problems

In operation, ZnO varistor materials are often subjects to various stresses such as continuous leakage current and resultant heat that can affect their performances. It has been found that the effect of applied field stresses on the stability of ZnO varistor ceramics can be taken care-off by the introduction of small amount of metal oxides as additives in the system. To develop a high performance of ZnO ceramics, small amount of CMO is added to ZnO system where this additive improves the stability of ZnO varistor.

Wide applications of ZnO inspire extensive research working on ZnO doped with transition metal oxides. In last few years, quite a substantial number of researchers have investigated ZnO doped with transition metal ions, but most of them paid their attention to its microstructure and electrical properties, but little report on the effect of applied field stresses on the stability of ZnO varistor ceramics.

In spite of many investigations carried out on ZnO varistor, investigation concerning the stability of ZnO ceramic containing small amount of metal oxides has not been sufficiently elucidated. Hence in this research the effect of applied field stresses on the stability of ZnO ceramics with CaMnO_3 as additive for varistor application was studied.

1.9 Objectives

In this present research work, different mole percentages of the dopant (CMO) with the same sintering temperature and different sintering time were performed. The objectives of this project are;

1. To study the effect of CMO contents on nonlinearity coefficient (α) enhancement of ZnO based low voltage varistor derived through modified citrate gel solution coating,
2. To study the nonlinear stability of ZnO based varistor ceramic against DC electrical field and thermal stresses as a function of CMO contents.

1.10 Hypothesis

1. Using wet chemical method to synthesize CMO, the nonlinearity coefficient value is expected to have an optimum value with the increase in the CMO contents
2. A good stability is expected after subjecting the ZnO + CMO varistor to DC electrical and thermal stresses at certain CMO content

1.11 Scope of Research

This work focuses on these areas:

1. ZnO material doped only with CMO. The dopant is added to investigate its contribution on electrical properties of ZnO varistor.
2. Microstructure characteristics are analysed using X-ray diffraction (XRD), Scanning Electron Microscope (SEM), Energy Dispersive X-ray (EDX), and Thermogravimetric/Differential Thermal Analysis (TG/DTA).
3. Electrical characteristics are analysed through the current density-electric field (J-E) characteristics of the sintered samples. The variation of nonlinear coefficient (α), degradation of the samples with various formulation, leakage current and stability.

REFERENCES

- Alfaruq, D. S., Otal, E. H., Aguirre, M. H., Populoh, S., and Weidenkaff, A. (2012). Thermoelectric properties of CaMnO₃ films obtained by soft chemistry synthesis. *Journal of Materials Research* **27**, 985-990.
- Baek, S., Song, J., and Lim, S. (2007). Improvement of the optical properties of ZnO nanorods by Fe doping. *Physica B: Condensed Matter* **399**, 101-104.
- Bai, S.-N., Shieh, J.-S., and Tseng, T.-Y. (1995). Characteristic analysis of ZnO varistors made with spherical precipitation powders. *Materials Chemistry and Physics* **41**, 104-109.
- Bernik, S., and Daneu, N. (2007). Characteristics of ZnO-based varistor ceramics doped with Al₂O₃. *Journal of the European Ceramic Society* **27**, 3161-3170.
- Bernik, S., Maček, S., and Bui, A. (2004). The characteristics of ZnO–Bi₂O₃ -based varistor ceramics doped with Y₂O₃ and varying amounts of Sb₂O₃. *Journal of the European Ceramic Society* **24**, 1195-1198.
- Bui, A., Nguyen, H., and Loubiere, A. (1995). High-field ZnO-based varistors. *Journal of Physics D: Applied Physics* **28**, 774.
- Canikoğlu, N., Toplan, N., Yıldız, K., and Toplan, H. Ö. (2006). Densification and grain growth of SiO₂ -doped ZnO. *Ceramics International* **32**, 127-132.
- Chen, C.-S., Kuo, C.-T., Wu, T.-B., and Lin, I.-N. (1997). Microstructures and Electrical Properties of V₂O₅ -based Multicomponent ZnO Varistors Prepared by Microwave Sintering Process. *Japanese Journal of Applied Physics*. **36**, 1169-1175.
- Clarke, D. R. (1999). Varistor ceramics. *Journal of the American Ceramic Society* **82**, 485-502.
- Cutler, R. (1991). Engineered Materials Handbook, vol. 4, Ceramics and Glasses. *ASM International. The Materials Information Society, USA*.
- Das, J.C. (2010). Transients in Electrical Systems: Analysis, Recognition, and Mitigation. McGraw-Hill Companies.
- Dienel, H. (1956). Silicon Carbide Varistors: Properties and Construction. *Bell Lab. Record* **34**, 407-411.
- Duran, P., Capel, F., Tartaj, J., and Moure, C. (2001). Sintering Behavior and Electrical Properties of Nanosized Doped-ZnO Powders Produced by Metallorganic Polymeric Processing. *Journal of the American Ceramic Society* **84**, 1661-1668.

- Eda, K. (1978). Conduction mechanism of non-Ohmic zinc oxide ceramics. *Journal of Applied Physics* **49**, 2964-2972.
- Eda, K. (1989). Zinc oxide varistors. *Electrical Insulation Magazine, IEEE* **5**, 28-30.
- Eda, K., Iga, A., and Matsuoka, M. (1980). Degradation mechanism of non-Ohmic zinc oxide ceramics. *Journal of Applied Physics* **51**, 2678-2684.
- Falamaki, C., Afarani, M. S., and Aghaie, A. (2004). Initial sintering stage pore growth mechanism applied to the manufacture of ceramic membrane supports. *Journal of the European Ceramic Society* **24**, 2285-2292.
- Frosch, C. (1954). Improved silicon carbide varistors. *Bell Lab Rec* **32**, 336.
- Gupta, T. (1991). Varistors. *Ceramics and Glasses ASM International, 1991*, 1150-1155.
- Gupta, T. K. (1990). Application of zinc oxide varistors. *Journal of the American Ceramic Society* **73**, 1817-1840.
- Gupta, T. K., Carlson, W., and Hower, P. (1981). Current instability phenomena in ZnO varistors under a continuous ac stress. *Journal of Applied Physics* **52**, 4104-4111.
- Gupta, T. K., and Carlson, W. G. (1985). A grain-boundary defect model for instability/stability of a ZnO varistor. *Journal of Materials Science* **20**, 3487-3500.
- Hamdad, N., and Bouhafs, B. (2010). Theoretical analysis of the spin effect on the electronic and magnetic properties of the calcium manganese oxide CaMnO_3 : GGA+U calculation. *Physica B: Condensed Matter* **405**, 4595-4606.
- Han, J., Mantas, P., and Senos, A. (2000). Grain growth in Mn-doped ZnO. *Journal of the European Ceramic Society* **20**, 2753-2758.
- Han, J., Senos, A., and Mantas, P. (1999). Nonisothermal sintering of Mn doped ZnO. *Journal of the European Ceramic Society* **19**, 1003-1006.
- Han, J., Senos, A., and Mantas, P. (2002). Varistor behaviour of Mn-doped ZnO ceramics. *Journal of the European Ceramic Society* **22**, 1653-1660.
- Hng, H., and Tse, K. (2008). Effects of MgO doping in ZnO-0.5 mol% V_2O_5 varistors. *Ceramics International* **34**, 1153-1157.
- Horio, N., Hiramatsu, M., Nawata, M., Imaeda, K., and Torii, T. (1998). Preparation of zinc oxide/metal oxide multilayered thin films for low-voltage varistors. *Vacuum* **51**, 719-722.

- Huang, M. H., Mao, S., Feick, H., Yan, H., Wu, Y., Kind, H., Weber, E., Russo, R., and Yang, P. (2001). Room-temperature ultraviolet nanowire nanolasers. *science* **292**, 1897-1899.
- Ivanchenko, A., Tonkoshkur, A., and Makarov, V. (2004). Desorption thermal degradation model of zinc oxide ceramics. *Journal of the European Ceramic Society* **24**, 3709-3712.
- Jeong, Y. K., Nakahira, A., Morgan, P. E., and Niihara, K. (1997). Effect of milling conditions on the strength of alumina–silicon carbide nanocomposites. *Journal of the American Ceramic Society* **80**, 1307-1309.
- Kelleher, M., and Hashmi, M. (2008). The effect of vibratory milling on the powder properties of zinc oxide varistors. *Journal of Materials Processing Technology* **201**, 645-650.
- Kittel, C. (1996). Introduction to solid physics. *The Feynman Lectures on Physics* **2**.
- Kostić, P., Milosević, O., Uskoković, D., and Ristić, M. (1988). Potential barrier degradation at the grain boundary of ZnO-based nonlinear resistors. *Physica B+ C* **150**, 175-178.
- Kutty, T., and Ezhilvalavan, S. (1996). The role of silica in enhancing the nonlinearity coefficients by modifying the trap states of zinc oxide ceramic varistors. *Journal of Physics D: Applied Physics* **29**, 809.
- Kutty, T., and Ezhilvalavan, S. (1997). The effect of aluminosilicate on the delayed onset of upturn voltages of zinc oxide varistor ceramics. *Materials Science and Engineering: B* **47**, 101-109.
- Lao, Y., Kuo, S., and Tuan, W. (2009). Influence of ball milling on the sintering behaviour of ZnO powder. *Ceramics International* **35**, 1317-1320.
- Lee, S.-M., and Kang, S.-J. L. (1998). Theoretical analysis of liquid-phase sintering: Pore filling theory. *Acta materialia* **46**, 3191-3202.
- Levinson, M., and Phillip, R. H. (1986). *ZnO oxide Varistor—A Review*. *American Ceramic Society Bull* **4**, 639-646.
- Macchesney, J., Williams, H., Potter, J., and Sherwood, R. (1967). Magnetic Study of the Manganate Phases: CaMnO_3 , $\text{Ca}_4\text{Mn}_2\text{O}_{10}$, $\text{Ca}_3\text{Mn}_3\text{O}_7$, Ca_2MnO_4 . *Physical Review* **164**, 779-785.
- Mahan, G. (1983). Intrinsic defects in ZnO varistors. *Journal of applied physics* **54**, 3825-3832.
- Margionte, M., Simoes, A., Riccardi, C., Ries, A., Perazolli, L., and Varela, J. (2006). Nonlinear characteristics of Cr_2O_3 , WO_3 , ZnO and CoO doped SnO_2 varistors. *Materials Letters* **60**, 142-146.

- Masuyama, T., and Matsuoka, M. (1968). Current Dependence of Voltage Non-linearity in SiC Varistors. *Japanese Journal of Applied Physics* **7**, 1294-1294.
- Matsuoka, M. (1971). Nonohmic properties of zinc oxide ceramics. *Japanese Journal of Applied Physics*, **10(6)**, 736.
- Nahm, C.-W. (2003). Nonlinear electrical properties and DC accelerated aging characteristics of ZnO-Pr₆O₁₁-CoO-Cr₂O₃-Dy₂O₃-based varistors. *Solid State Communications* **127**, 389-393.
- Nahm, C.-W. (2004). Effect of cooling rate on degradation characteristics of ZnO-Pr₆O₁₁-CoO-Cr₂O₃-Y₂O₃-based varistors. *Solid State Communications* **132**, 213-218.
- Nahm, C.-W. (2007). The effect of sintering temperature on electrical properties and accelerated aging behavior of PCCL-doped ZnO varistors. *Materials Science and Engineering: B* **136**, 134-139.
- Nahm, C.-W. (2007). Electrical properties and aging characteristics of terbium-doped ZPCC-based varistors. *Materials Science and Engineering: B* **137**, 112-118.
- Nahm, C.-W. (2008). Influence of Mn doping on microstructure and DC-accelerated aging behaviors of ZnO-V₂O₅-based varistors. *Materials Science and Engineering: B* **150**, 32-37.
- Nahm, C.-W., and Park, C.-H. (2000). Microstructure, electrical properties, and degradation behavior of praseodymium oxides-based zinc oxide varistors doped with Y₂O₃. *Journal of Materials Science* **35**, 3037-3042.
- Nahm, C. (2003). Electrical properties and stability of praseodymium oxide-based ZnO varistor ceramics doped with Er₂O₃. *Journal of the European Ceramic Society* **23**, 1345-1353.
- Nahm, C. (2005). Influence of sintering time on electrical and dielectric behavior, and DC accelerated aging characteristics of Dy³⁺-doped ZnO-Pr₆O₁₁-based varistors. *Materials Chemistry and Physics* **94**, 275-282.
- Nies, C. W. (1989). Compatibility Studies of Zinc Oxide Varistor Materials with Integrated Ceramic Packaging Technology, Materials Research Laboratory, the Pennsylvania State University.
- Onreabroy, W., and Sirikulrat, N. (2006). Effects of cobalt doping on nonlinearity of zinc oxide. *Materials Science and Engineering: B* **130**, 108-113.
- Oshikiri, M., Imanaka, Y., Aryasetiawan, F., and Kido, G. (2001). Comparison of the electron effective mass of the n-type ZnO in the wurtzite structure measured by cyclotron resonance and calculated from first principle theory. *Physica B: Condensed Matter* **298**, 472-476.

- Park, J.-A. (2008). Effect of Al₂O₃ on the electrical properties of ZnO-Pr₆O₁₁-based varistor ceramics. *Physica. B, Condensed matter* **403**, 639-643.
- Pike, G.E. (1994). *Semiconducting polycrystalline ceramics*, *Journal of Material Science and Technology* **11**, 731-754
- Pierret, R.F. (1996). Semiconductor device fundamentals, First edition, *Addison-Wesley Publishing Company, Inc.*
- Poepelmeier, K., Leonowicz, M., Scanlon, J., Longo, J., and Yelon, W. (1982). Structure determination of CaMnO₃ and CaMnO_{2.5} by X-ray and neutron methods. *Journal of Solid State Chemistry France* **45**, 71-79.
- Ramírez, M., Bueno, P., Ribeiro, W., Varela, J., Bonett, D., Villa, J., Márquez, M., and Rojo, C. (2005). The failure analyses on ZnO varistors used in high tension devices. *Journal of Materials Science* **40**, 5591-5596.
- Ramírez, M., Simoes, A., Bueno, P., Márquez, M., Orlandi, M., and Varela, J. (2006). Importance of oxygen atmosphere to recover the ZnO-based varistors properties. *Journal of materials science* **41**, 6221-6227.
- Sato, K., Takada, Y., Takemura, T., and Ototake, M. (1982). A mechanism of degradation in leakage currents through ZnO varistors. *Journal of Applied Physics* **53**, 8819-8826.
- Schwing, U., and Hoffmann, B. (1981). New approach to the measurement of the single-contact varistor. *Grain Boundary Phenomena in Electronic Ceramics, American Ceramic Society, Columbus, OH*, 383-393.
- Sedky, A., Abu-Abdeen, M., and Almulhem, A. A. (2007). Nonlinear IV characteristics in doped ZnO based-ceramic varistor. *Physica B Condensed Matter* **388**, 266-273.
- Sedky, A., El-Brolossy, T., and Mohamed, S. (2012). Correlation between sintering temperature and properties of ZnO ceramic varistors. *Journal of Physics and Chemistry of Solids* **73**, 505-510.
- Selim, F., Gupta, T., Hower, P., and Carlson, W. (1980). Low voltage ZnO varistor: device process and defect model. *Journal of Applied Physics* **51**, 765-768.
- Senda, T., and Bradt, R. C. (1991). Grain growth of zinc oxide during the sintering of zinc oxide—antimony oxide ceramics. *Journal of the American Ceramic Society* **74**, 1296-1302.
- Shohata, N., Matsumura, T., Utsumi, K., and Ohno, T. (1981). Grain Boundary Phenomena in Electronic Ceramics. *Advances in Ceramics* **1**, 349.
- Simoes, A., Ries, A., Perazolli, L., Longo, E., and Varela, J. (2006). Nonlinear electrical behaviour of the Cr₂O₃, ZnO, CoO and Ta₂O₅-doped SnO₂ varistors. *Ceramics International* **32**, 283-289.

- Simões, A., Ries, A., Perazolli, L., Longo, E., and Varela, J. (2006). Nonlinear electrical behaviour of the Cr₂O₃, ZnO, CoO and Ta₂O₃-doped SnO₂ varistors. *Ceramics International* **32**, 283-289.
- Sinha, A., and Sharma, B. (1997). Novel route for preparation of high voltage varistor powder. *Materials Research Bulletin* **32**, 1571-1579.
- Smith, A., Gasgnier, G., and Abélard, P. (1990). Voltage-Current Characteristics of a Simple Zinc Oxide Varistor Containing Magnesia. *Journal of the American Ceramic Society* **73**, 1098-1099.
- Sonder, E., Austin, M., and Kinser, D. (1983). Effect of oxidizing and reducing atmospheres at elevated temperatures on the electrical properties of zinc oxide varistors. *Journal of Applied Physics* **54**, 3566-3572.
- Srinivasan, G., and Kumar, J. (2008). Effect of Mn doping on the microstructures and optical properties of sol-gel derived ZnO thin films. *Journal of Crystal Growth* **310**, 1841-1846.
- Stucki, F., and Greuter, F. (1990). Key role of oxygen at zinc oxide varistor grain boundaries. *Applied Physics Letters* **57**, 446-448.
- Subasri, R., Asha, M., Hembram, K., Rao, G., and Rao, T. (2009). Microwave sintering of doped nanocrystalline ZnO and characterization for varistor applications. *Materials Chemistry and Physics* **115**, 677-684.
- Tonkoshkur, A., Lyashkov, A. Y., Gomilko, I., and Ivanchenko, A. (2000). Effect of long-term electrical degradation on the distribution of donor impurities in ZnO varistor ceramics. *Inorganic Materials* **36**, 745-748.
- Trontelj, M., Kolar, D., and Kraševc, V. (1986). Influence of Chemical Composition on the Barrier Height in ZnO Varistors. In "Tailoring Multiphase and Composite Ceramics", pp. 509-515. Springer.
- Vijayanandhini, K., and Kutty, T. (2006). Low-voltage varistors from ZnO+CaMnO₃ ceramics. *Applied Physics Letters* **88**, 123513-123513-3.
- Wang, M.-h., Hu, K.-a., Zhao, B.-y., and Zhang, N.-f. (2007). Degradation phenomena due to humidity in low voltage ZnO varistors. *Ceramics International* **33**, 151-154.
- Wang, M.-h., Li, G., and Yao, C. (2011). Microstructure and electrical properties of Pr₆O₁₁-Co₃O₄-MnCO₃-Y₂O₃-doped ZnO varistors. *Ceramics International* **37**, 2901-2905.
- Wang, M.-h., Yao, C., and Zhang, N.-f. (2008). Degradation characteristics of low-voltage ZnO varistor manufactured by chemical coprecipitation processing. *Journal of Materials Processing Technology* **202**, 406-411.

- Wang, Q.B., Wang, Q.G., Wan C.X. (2010). Effect of sintering time on microstructure and properties of inorganic polyphosphate bioceramics. *Science of Sintering* **42**, 337-343
- Wiebe, C., Greedan, J., Gardner, J., Zeng, Z., and Greenblatt, M. (2001). Charge and magnetic ordering in the electron-doped magnetoresistive materials $\text{CaMnO}_{3-\delta}$ ($\delta=0.06, 0.11$). *Physical Review B* **64**, 064421.
- Wong, J. (1980). Sintering and varistor characteristics of $\text{ZnO-Bi}_2\text{O}_3$ ceramics. *Journal of Applied Physics* **51**, 4453-4459.
- Xu, D., Shi, L., Wu, Z., Zhong, Q., and Wu, X. (2009). Microstructure and electrical properties of $\text{ZnO-Bi}_2\text{O}_3$ -based varistor ceramics by different sintering processes. *Journal of the European Ceramic Society* **29**, 1789-1794.
- Yen, A. J., Lee, Y. S., and Tsen, T. Y. (1994). Electrical Properties of Multilayer-Chip ZnO Varistors in a Moist-Air Environment. *Journal of the American Ceramic Society* **77**, 3006-3011.
- Yoshikazu, S., Yasuhiro, O., Toshio, K., and Jun, M. (2002). Evaluation of Sb_2O_5 -doped ZnO varistors by photoacoustic spectroscopy. *Japanese Applied Physics* **41**, 3379-82.
- Zhang, C., Hu, Y., Lu, W., Cao, M., and Zhou, D. (2002). Influence of TiO_2O_3 ratio on ZnO varistor ceramics. *Journal of the European Ceramic Society* **22**, 61-65.
- Zhou, D., Zhang, C., and Gong, S. (2003). Degradation phenomena due to dc bias in low-voltage ZnO varistors. *Materials Science and Engineering: B* **99**, 412-415.
- Zhou, H., Guo, R., Chu, D., Chang, B., Qin, Y., and Fang, L. (2013). $\text{Bi}_4\text{Ti}_3\text{O}_{12}$ modified low voltage ZnO-based varistors: microstructure, electrical properties and aging characteristics. *Journal of Materials Science: Materials in Electronics* **24**, 4987-4992.

<http://v5.books.elsevier.com/bookscat/samples/9780750663854/4355-Kang-01.pdf>

http://www.webelements.com/compounds/zinc/zinc_oxide.html

LIST OF PUBLICATIONS

The following journal publications were achieved from the output of this research and during the period of candidature:

Accepted

- I. I. Iakin**, A. Zakaria, Y. Abdollahi, D. Umaru, (2014). Effect of Sintering Temperature on Microstructure and Electrical Properties of ZnO + CaMnO₃ Ceramics used in Low-Voltage Varistor. Digest Journal of Nanomaterials and Biostructures.

Submitted

- I. I. Iakin**, A. Zakaria, H. M. Kamari, R. S. Aziz and R. Wan Abdullah, (2014). Degradation Characteristics of Low Voltage Varistor from ZnO + CaMnO₃ Ceramics. Solid State Communications.



UNIVERSITI PUTRA MALAYSIA

STATUS CONFIRMATION FOR THESIS / PROJECT REPORT AND COPYRIGHT

ACADEMIC SESSION : 2014/2015

TITLE OF THESIS / PROJECT REPORT :

FABRICATION AND EFFECT OF APPLIED STRESSES
ON STABILITY OF ZnO CERAMICS WITH CaMnO_3
AS ADDITIVE FOR VARISTOR APPLICATION

NAME OF STUDENT : ISMAIL IBRAHIM LAKIN

I acknowledge that the copyright and other intellectual property in the thesis/project report belonged to Universiti Putra Malaysia and I agree to allow this thesis/project report to be placed at the library under the following terms:

1. This thesis/project report is the property of Universiti Putra Malaysia.
2. The library of Universiti Putra Malaysia has the right to make copies for educational purposes only.
3. The library of Universiti Putra Malaysia is allowed to make copies of this thesis for academic exchange.

I declare that this thesis is classified as :

*Please tick (✓)

CONFIDENTIAL

(Contain confidential information under Official Secret Act 1972).

RESTRICTED

(Contains restricted information as specified by the organization/institution where research was done).

OPEN ACCESS

I agree that my thesis/project report to be published as hard copy or online open access.

This thesis is submitted for :

PATENT

Embargo from _____ until _____
(date) (date)

Approved by:

ISMAIL Lakin

(Signature of Student)
New IC No/ Passport No.:

(Signature of Chairman of Supervisory Committee)
Name:

Date :

Date :

[Note : If the thesis is CONFIDENTIAL or RESTRICTED, please attach with the letter from the organization/institution with period and reasons for confidentially or restricted.]