

MARINE RISER VORTEX INDUCED VIBRATION (VIV) SUPPRESSION DEVICE

NURSAHLIZA BINTI MUHAMAT YAIN

A project report submitted in fulfilment of the
requirements for the award of the degree of
Master of Science (Ship and Offshore Engineering)
Faculty of Mechanical Engineering

Universiti Teknologi Malaysia

JANUARY 2017

ACKNOWLEDGEMENT

First of all, In the name of Allah s.w.t, The Most Gracious and The Most Merciful, Alhamdulillah and thanks for His blessing and mercy, I am able to complete this Master Project. During preparing this thesis, I was accompanying with many people who continuously contributed towards my understanding and thoughts.

I would like to express my gratitude and appreciation to all those who gave me strength and guidance to complete this project. I would like to express my gratefulness to my supervisors, Prof. Dr. Adi Maimun bin Abdul Malik and Dr Yasser Mohamed Ahmed Abdel Razak for their valuable guidance, advice, support and lesson throughout this study. Not to forget, my colleague Mobassher Tofa for his guidance and help during the research. In this opportunity, I would like to give my greatest appreciation to my beloved parents, Muhamat Yain bin Bakar and Hasnah Binti Johar for their encouragement, moral support, and motivation during this period of time.

Special thanks and deepest appreciation dedicated to all my friends for their support and guidance, as well as sharing the knowledge and the idea. I would like to extend my special thanks to my course mates Ship and Offshore Engineering Batch 2014/2016. And also thanks to everyone who was directly and indirectly involved in this project.

Last but not least, my sincere gratitude towards Kementerian Pengajian Tinggi for the financial support and towards Netherlands Maritime Institute of Technology (NMIT) for the moral support and give me flexible hours during my study.

ABSTRACT

Vortex-Induced Vibration (VIV) is a common phenomenon that occurred in the oil and gas industry and become one of the main concerns for the engineers while designing the riser system. Thus, this research represents the analysis of the vortex-induced motion of the circular cylindrical by using the Computational Fluid Dynamics (CFD) ANSYS CFX. The simulation was carried out in two-dimensional with the stationary condition. The bare cylinder was used as the reference for this research while the graph Strouhal number versus Reynolds number as the validation. The validation by using the Strouhal number is the common practice for the stationary circular cylinder simulation and Strouhal frequency obtained from this research was $St \approx 0.2$. The simulation process was executed by using the ANSYS CFX Solver to simulate the cylinder and to identify the vortex shedding and also its magnitudes. The turbulent model used in this simulation is Detached Eddy Simulation and the vortices created at the back of the cylinder as well as the flow separation can be monitored through post-processor. Generally, when the fluid flow passed through the bluff body, it will excite by the forces and caused the vortices shed. These vortices will separate periodically asymmetrically from either side of the body caused the time varying non-uniform pressure distribution around it. This non-uniform pressure will create in both inline and transverse to the flow. By having the idea of parallel plates attached to the cylinder, it will help the flow separation become streamline as well as reduce the VIV on the marine riser. In addition, the Reynolds number is believed will give some significant effect on the behavior of VIV.

ABSTRAK

Getaran vortex yang disebabkan daripada silinder adalah fenomena biasa yang terjadi di dalam industri cari gali minyak dan gas dan ia menjadi salah satu kebimbangan utama kepada para jurutera semasa mereka bentuk system riser. Sehubungan dengan itu, kajian ini menyatakan analisis tentang getaran yang disebabkan oleh silinder bulat dengan menggunakan pengkomputeran bendalir dinamik (CFD) ANSYS CFX. Simulasi ini telah dijalankan di dalam dua-dimensi dengan keadaan yang statik atau pegun. Silinder yang terdedah telah digunakan sebagai rujukan untuk kajian ini manakala graf nombor Strouhal lawan nombor Reynolds digunakan sebagai pengesahan. Pengesahan menggunakan nombor Strouhal adalah amalan biasa yang sering dilakukan untuk simulasi silinder bulat yang pegun dan kekerapan Strouhal yang diperolehi untuk kajian ini adalah $St \approx 0.2$. Proses simulasi telah dilaksanakan menggunakan penyelesaian ANSYS CFX untuk mensimulasikan silinder and untuk mengenal pasti penumpahan vortex dan magnitudnya. Model bergelora yang digunnakan dalam simulasi ini adalah 'Detached Eddy Simulation' dan vorteks yang terhasil di belakang silinder termasuklah aliran pemisah boleh dipantau melalui catatan pemproses. Secara umumnya, apabila cecair mengalir melalui badan 'bluff', ia akan dibangkitkan oleh daya-daya dan akan mengakibatkan vorteks tersisih. Vorteks-vorteks ini akan terpisah secara simetri berkala daripada kedua-dua belah badan disebabkan oleh masa-masa yang berubah dan tekanan yang tidak seragam disekitarnya. Tekanan yang tidak seragam ini akan menghasilkan kedua-dua sebaris dan melintang kepada aliran. Denagn adanya idea menggunakan dua plat secara selari yang dilekatkan dibelakang silinder, ia akan membantu aliran pemisah menjadi selaras dan sekaligus dapat mengurangkan VIV terhadap riser marin. Tambahan pula, nombor Reynolds dipercayai akan memberi efek yang ketara terhadap tingkah laku VIV.

TABLE OF CONTENTS

CHAPTER	TITLE	PAGE
	DECLARATION	iv
	ACKNOWLEDGMENT	v
	ABSTRACT	vi
	ABSTRAK	vii
	TABLE OF CONTENTS	viii
	LIST OF TABLES	xi
	LIST OF FIGURES	xii
1	INTRODUCTION	1
	1.1 Introduction	1
	1.2 Problem Statement	3
	1.3 Purpose Statement	3
	1.4 Objective	4
	1.5 Scope of Research	4
2	LITERATURE REVIEW	5
	2.1 Introduction	5
	2.2 Vortex-induced Vibration (VIV)	5
	2.3 Suppression Device	8
	2.3.1 Helical Strakes	10
	2.3.2 Fairings	10
	2.4 Technical Comparison	11

3	METHODOLOGY	17
	3.1 Introduction	17
	3.2 Methodology Steps	19
4	THEORY	22
	4.1 Introduction	22
	4.2 Bluff Bodies, Vortex Shedding and Vortex-Induced Vibration (VIV)	22
	4.3 Vortex Lock-in	23
	4.4 Model for VIV and related equation	23
	4.5 Lift and Drag Force	25
5	SIMULATION SETUP AND VALIDATION	27
	5.1 Introduction	27
	5.2 Model Specification	27
	5.3 Computational Fluid Dynamic (CFD)	28
	5.4 CFD Simulation	29
	5.4.1 Pre-Processor Stage	30
	5.4.2 Manager Solver Stage	33
	5.4.3 Post-Processor Stage	33
	5.5 Validation	33
6	RESULT AND DISCUSSION	36
	6.1 Introduction	36
	6.2 Numerical Simulations of the Flow	36
	6.3 Constant in Gap (G)	37
	6.4 Constant in Length (L)	42
	6.5 L/G Ratio	47

7	CONCLUSION AND RECOMMENDATION	53
	7.1 Conclusion	53
	7.2 Recommendation	54
	REFERENCES	55

LIST OF TABLES

TABLE NO.	TITLE	PAGE
5.1	Parameter and Model Specification	28

LIST OF FIGURES

FIGURE NO.	TITLE	PAGE
1.1	Example of riser: (a) drilling riser during the installation, (b) rigid riser, (c) flexible riser, and (d) hybrid riser configuration called Self-Standing Hybrid Riser. (Murai M. & Yamamoto M. 2010)	2
2.1	Vortex shedding behind a 2D fixed cylinder in the famous Von Karman Street for a subcritical Reynolds number=140. (Mukundan H. 2008)	6
2.2	Vortex shedding pattern for different Reynolds number. (Robert D. B, 2001)	7
2.3	Strouhal Number versus Reynolds number for Circular Cylinder	8
2.4	Various devices for VIV suppression: (a) Single steel plate; (b) Ribbons/hair cables; (c) Guide vanes; (d) Hoops/spaces spoiler; (e) Helical strakes; (f) Perforated cylindrical shroud; (g) Axial rod shroud; (h) Fairing	9
2.5	Helical strakes installed on the marine riser. (VIV Solutions, 2012)	10
2.6	Fairings for marine riser (VIV Solutions, 2012)	11
2.7	Free motion response (1-DOF) for a straked cylinder	12
2.8	Drag Coefficient Ratio: Effect of strake and roughness	13
2.9	a) A/D vs Ur plots of the bare riser and riser	15

	with a fairing. b) Cd vs Ur plot of the abnormal stuck fairing. (Ng, 2008)	
2.10	Cross-flow (y^*/D) and streamwise (x^*/D) amplitude of vibration versus reduced velocity for a plain cylinder compared to cylinders fitted with oblique plates of various angles. (Assi, 2014)	16
3.1	Methodology of research	18
3.2	Mesh generated and set the boundary condition in Ansys Workbench 2016	20
3.3	Domain interface in CFX Pre-	20
4.1	Cylinder and coordinate system. (Blevin, R. D., 1990)	24
5.1	Cylinder attached with parallel plates	27
5.2	Basic concept of Ansys CFX simulation methodology	29
5.3	A rectangular box solution domain (LxD)	30
5.4	Unstructured meshing for cylinder with parallel plates in 2D	31
5.5	Boundary condition for the geometry	32
5.6	Strouhal number-Reynolds number relationship for circular cylinders (Lienhard, 1966; Achenbach and Heinecke, 1981). $S \approx 0.21(1 - 21/Re)$ for $40 < Re < 200$ (Roshko, 1955)	34
6.1	Velocity contour for bare cylinder	36
6.2	Velocity contour with parallel plates attached behind it	37
6.3	Graphs lift force ratio versus Reynolds number for constant gap (a-c)	38
6.4	Graphs of reduction percentage of lift force ratio versus Reynolds number for constant gap (a-c)	39
6.5	Graphs drag force ratio versus Reynolds	40

	number for constant gap (a-c)	
6.6	Graphs of reduction percentage of drag force ratio versus Reynolds number for constant gap (a-c)	41
6.7	Graphs lift force ratio versus Reynolds number for constant length (a-c).	43
6.8	Graphs of reduction percentage of lift force ratio versus Reynolds number for constant length (a-c).	44
6.9	Graphs drag force ratio versus Reynolds number for constant length (a-c).	45
6.10	Graphs of reduction percentage of drag force ratio versus Reynolds number for constant length (a-c).	46
6.11	Graph of lift force versus L/G for Reynolds number = 5×10^4 .	47
6.12	Graph of drag force ratio versus L/G for Reynolds number = 5×10^4	48
6.13	Graphs of lift force reduction percentage versus L/G for Reynolds number = 5×10^4	48
6.14	Graph of drag force reduction percentage versus L/G for Reynolds number = 5×10^4	49
6.15	Graph of lift force versus L/G for Reynolds number = 1×10^5 .	49
6.16	Graph of drag force ratio versus L/G for Reynolds number = 1×10^5	50
6.17	Graph of lift force reduction percentage versus L/G for Reynolds number = 1×10^5	50
6.18	Graphs of drag force reduction percentage versus L/G for Reynolds number = 1×10^5	51

CHAPTER 1

INTRODUCTION

1.1. Introduction

Nowadays, oil and gas exploration has been growing tremendously; the oil production companies and its facilities are moving forward to untapped the oil and gas reserve. Marine risers are one of the marine facilities that attached to the platform or floating vessels which have been used as transportation means for hydrocarbons resources as well as for drilling operation as shown in Figure 1.1. The conditions of sea states, the currents, and waves, the weather together with the hurricanes, are the big challenges harshly decrease a drill rig's operation magnificently. Based on research by Taggart et al. (2008), in the Gulf of Mexico (GoM), drilling and completion operation and resulting cost to operate can be very high due to the high loop currents and series of hurricanes. This statement has been supported by Grealish et.al which mentioned that GoM is one of the regions that has this high current profile, known as loop currents and cold core eddies.

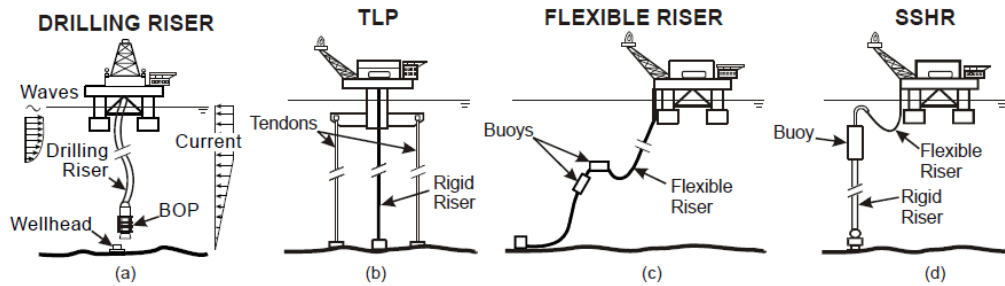


Figure 1.1: Example of riser: (a) drilling riser during the installation, (b) rigid riser, (c) flexible riser, and (d) hybrid riser configuration called Self-Standing Hybrid Riser. (Murai M. & Yamamoto M. 2010)

One of the critical part concerning in offshore industry is the riser, which connects the platform to the wellhead at the seabed. Risers are long and flexible structure and caused the critical ratio L/D tends to be very large. This problem always occurred especially in the deep ocean areas compared to the shallower water. Typically, more than 50% of the riser is covered, with the recent riser installation employing up to 100% with suppression device

The applications of riser for drilling and production activities are subjected to large forces, due to the waves and currents of the sea state. Generally, a slender structure like marine risers is susceptible to the vortex induced vibration (VIV), which can cause severe oscillation and lead to the fatigue as well as total damage to the structure. The resonance will occur when the frequency of excitation of vortices is at or close to the natural frequency of the structure. Thus, the large amplitude of oscillation may have induced between the flow and structure's motion which can cause the lock-in phenomenon.

The VIV phenomenon was found to be a problem in the offshore industry, formerly there are two approaches to address this problem, namely: modify the design of riser to eliminate the VIV or employ the usage of VIV suppression devices. In order to change the natural frequency of the structures are largely impossible and impractical, thus the VIV suppression devices can be deployed to disrupt the formation of vortices. There are many types of suppression devices in the market including helical strakes, fairings, vane and shroud. Helical strakes and fairings are

known as most effective and preferable commonly used by operators and company. Although the VIV can be suppressed by the strakes or fairings, the cost related to the hardware and installation is high. Hence, the research on the riser VIV has been rising in the oil and gas industry to achieve the safe and economical design.

1.2. Problem Statement

The current will cause vortexes to shed from the sides of the riser. Donald et al. (1998) mentioned in their research that these vibrations will lead to fatigue failure of the riser. Under steady current flow, cross flow vibrations of risers have two immediate consequences which are increased in fatigue damage and increased in line drag. Deepwater riser will fail to meet the fatigue design criteria due to VIV. To counteract the fatigue impact, VIV needs to be suppressed. There is two option whether redesign the riser which relatively expensive or by adding VIV suppression devices to reduce the vibration.

A lot of work or research has been carried out for suppressed the marine riser VIV. Many types of suppression devices have been introduced to overcome this problem. However, there is not much detailed study in numerical or experiment being done using the flat plate as a suppression device. This research will investigate this problem.

1.3. Purpose Statement

The purpose of this research is to validate the effectiveness of parallel plates as suppression device in order to minimize the Vortex Induced Vibration (VIV).

1.4. Objective

The objectives of this research are:

1. To study the efficiency of parallel plates as VIV suppression device that able to reduce VIV on the marine riser.
2. To evaluate the effect of plate lengths and gaps on different Reynolds number.

1.5. Scope of Research

This research is focusing on minimizing the occurrence of VIV in the marine riser by designing suppression device with parallel plates. The literature review of the art of VIV for marine riser has been carried out throughout this research. CFD software ANSYS CFX is used to study the ability of the different plate lengths and gaps for reducing VIV. The stationary bare riser is used as a reference and to validate this research we will use the graph and calculate the Strouhal number.

REFERENCES

- Allen, D. W., Henning, D. L. & Lee, L. (2004). Performance Comparisons of Helical Strakes for VIV Suppression of Risers and Tendons. *Conference on Offshore Technology Conference*
- Assi, G. R. S., Bearman, P. W., & Kitney, N. (2009). *Low Drag Solutions for Suppressing Vortex-Induced Vibration of Circular Cylinders*. *Journal of Fluids and Structures*. 25, 666-675.
- Assi, G. R. S., Bearman, P. W., Kitney, N. & Tognarelli, M. A. (2010). *Suppression of Wake-Induced Vibration of Tandem Cylinders with Free-to-Rotate Control Plates*. *Journal of Fluids and Structures*. 26, 1045-1057.
- Assi, G. R. S., Beaman, P.W., Rodrigues, J. R. H., Tognarelli, M. 2011 The effect of rotational friction on the stability of short-tailed fairings suppressing vortex-induced vibrations. *In the proceedings of OMAE2011, 30th International Conference on Ocean, Offshore and Arctic Engineering*, Rotterdam, The Netherlands.
- Assi, G. R. S., Franco, G. S. & Vestri, M. S. (2014). *Investigation on the Stability of Parallel and Oblique Plates as Suppressors of Vortex-Induced Vibration of a Circular Cylinder*. *Journal of Offshore Mechanics and Arctic Engineering*.
- Balmoral Offshore Engineering. (2014). *A Technical Guide to VIV Suppression*. Aberdeen, Scotland.
- Blevins, R. D. (2001). *Flow-Induced Vibration*. (2nd ed). Malabar, Florida. Krieger Publishing Company.

Boubenider, R., Fourchy, P., & De Wilde, J. J. (2008). Effectiveness of Polyethylene Helical Strakes in Suppressing VIV Response After Sustaining High Roller Deformation During S-Lay Installation. *Conference on Offshore Technology Conference*.

Constantinides, Y. & Oakley Jr., O. H. (2006). Numerical Prediction of Bare and Straked Cylinder VIV. *In the Proceeding from OMAE 2006. The 25th International Conference on Offshore Mechanics and Arctic Engineering*. Hamburg, Germany.

Cunff, C. Le., Biolley, F., Fontaine, E., Étienne, S., & Facchinetti, M. L. (2002). *Vortex-Induced Vibrations of Risers: Theoretical, Numerical and Experimental Investigation*. *Oil & Gas Science and Technology*, 57(1), 59–69.

Drilling Engineering Association (1998). *Deep Water Drilling Riser Technology VIV & Fatigue Management*. Paris, Howells H.

Fang, S. M., & Niedzwecki, J. M. (2014). *Comparison of Airfoil and Ribbon Fairings for Suppression of Flow-Induced Vibrations*, 2(1), 30–45.

Grealish, F. & Delahunt, S. *Vortex Induced Vibration – Key Issues*.

Gustafsson, A. (2012). *Analysis of Vortex-Induced Vibrations of Risers*. (Master Dissertation, Chalmers University of Technology, 2012).

Holmes, S., Oakley Jr, O. H. & Constantinides, Y. (2006). Simulation of Riser VIV Using Fully Three-Dimensional CFD Simulations. *Proceeding from OMAE 2006. The 25th International Conference on Offshore Mechanics and Arctic Engineering*. Hamburg, Germany.

Iizuka, M. R. C. (2014). *Prediction Method of the Vortex-Induced Vibration of one Degree of Freedom Spring Mass System*. (Master Dissertation, University of Rhode Island, 2014).

Jamei, S., Maimun, A., Ghazanfari, S. A., Ahmed, Y. M. (2014). Two degrees of freedom CFD Simulation of Vortex-Induced Vibration of Two Circular Cylinder in Tandem Arrangements. Proceeding from OTC '14. *Conference on Offshore Technology Conference*.

Khalak, A., Williamson, C.K.H., (1997). *Investigation of relative effects of mass and damping in the vortex-induced vibration of a circular cylinder*. Journal of Wind Engineering and Industrial Aerodynamics 69–71, 341–350.

Lee, L. (2013). A New VIV Design Procedure for Marine Tubular. *Proceedings of ASME 2013. The 3rd ASME/USCG Workshop on Marine Technology and Standards*. Arlington VA, USA.

Lienhard, J. H. (1966) “*Synopsis of Lift, Drag and Vortex Frequency Data for Rigid Circular Cylinders*,” Washington State University, College of Engineering, Research Division Bulletin 300.

Lim, F. & Howells, H. (2000). Deepwater Riser VIV, Fatigue and Monitoring. *Conference on Deepwater Pipeline & Riser Technology*. Houston, Texas.

Maritime Research Institute Netherlands (MARIN) (2005). *Laboratory Investigation of Long Riser VIV Response*. Wageningen, Netherland. Wilde, J. J. De, & Huijsmans, R. H. M

Mohammad Reza Gharib (1999). *Vortex-Induced Vibration, Absence of Lock-In and Fluid Force Deduction*. Doctoral Dissertation, California Institute of Technology, 1999.

Mukundan H. (2008). *Vortex-induced vibration of marine risers: motion and force reconstruction from the field and experimental data*. Doctoral dissertation, Massachusetts Institute of Technology, Cambridge, Ma, USA.

Murai, M., & Yamamoto, M. (2010). An Experimental Analysis of the Internal Flow Effects on Marine Risers. *Proceeding from MARTEC 2010. The International Conference on Marine Technology*. Dhaka, Bangladesh.

Ng, D. J. T., Teng, Y. J., Magee, A. R., AhmadZukni, N. B., AbdulMalik, A. M., AbdKader, A. S., et al (2014). Riser VIV Suppression Device Test. *Conference on Offshore Technology Conference*.

Norwegian Marine Technology Research Institute. (2005). *Deep-Water Riser Technology*.

Schaudt, K. J., Wajnikonis, C., Spencer, D., Xu, J., leverrete, S., Masters, R. 2008 Benchmarking of VIV Suppression System. *In the proceeding of OMAE2008, 27th International Conference on Offshore Mechanics and Arctic Engineering, Estoril, Portugal*.

Taggart, S. & Tognarelli, M. A. (2008). Offshore Drilling Riser VIV Suppression Devices – What’s Available to Operators? *Proceeding from OMAE 2008. The 27th International Conference on Offshore Mechanics and Arctic Engineering*. Estoril, Portugal.

Taggart, S., & Campbell, M. (2008). Actual VIV Fatigue Response of Full Scale Drilling Riser: With and Without Suppression Devices. *Proceeding from OMAE 2008. The 27th Conference on Offshore Mechanics & Arctic Engineering*. Estoril, Portugal.

Tofa, M.M., Maimun, A., Ahmed, Y. M., Jamei S. (2013). *Two Degree of Freedom Vortex Induced Vibration Tests of a Riser Model Using Spring Bars*.

Tofa, M.M., Maimun, A., Ahmed, Y. M., Jamei S. (2014). Numerical Studies of Vortex-Induced Vibration of a Circular Cylinder at High Reynolds Number. *Proceeding from OTC '14. Conference on Offshore Technology Conference*.

Tofa, M.M., Maimun, A., Ahmed, Y. M., Jamei S. (2014). *Experimental and Numerical Studies of Vortex Induced Vibration on Cylinder*. Journal of Technology. 66 (2), 169-175.

Vandiver, J. K. (1998). Research Challenges in the Vortex-Induced Vibration Prediction of Marine Risers. *Conference on Offshore Technology Conference*. Houston, Texas.

Vikestad, K., Larsen, C. M., & Vandiver, J. K. (2000). Norwegian Deepwater Program: Damping of Vortex-Induced Vibrations. *Conference on Offshore Technology Conference*. Houston, Texas.

Williamson, C. H. K. & Govardhan, R. (2004). *Vortex -Induced Vibrations*. [Annual Review of the Fluid Mechanic]. 36, 413-455.

Zhang, H., & Lim, F. (2010). VIV Suppression Device Effectiveness for Steel Catenary Risers. Proceeding from ISOPE 2010. *The 20th Conference on International Offshore and Polar Engineering Conference*. Beijing, China.