

OPTIMAL TUNING OF PROPORTIONAL INTEGRAL DERIVATIVE  
CONTROLLER FOR SIMPLIFIED HEATING VENTILATION AND AIR  
CONDITIONING SYSTEM

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*Special thanks to my beloved Mother, Father,  
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## ABSTRACT

A Heating Ventilation and Air Conditioning system (HVAC) is an equipment that is designed to adapt and adjust the humidity as well as temperature in various places. To control the temperature and humidity of the HVAC system, various tuning methods such as Ziegler–Nichols (Z-N), Chien-Hrones-Reswick (CHR), trial and error, robust response time, particle swarm optimization (PSO) and radial basis function neural network (RBF-NN) were used. PID is the most commonly used controller due to its competitive pricing and ease of tuning and operation. However, to effectively control the HVAC system using the PID controller, the PID control parameters must be optimized. In this work, the epsilon constraint via radial basis function neural network method is proposed to optimize the PID controller parameters. The advantages of using this method include fast and accurate response and follow the target values compared to other tuning methods. This work also involves the estimation of the dynamic model of the HVAC system. The non-linear decoupling method is used to modify the model of HVAC system. The benefits of using the proposed simplification technique rather than other techniques such as the relative gain array techniques (RGA) is because of its simplification, accuracy, and reduced non-linear components and interconnection effect of the HVAC system. It is observed that the amount of integral absolute error (IAE) for temperature and humidity based on the simplified model are decreased by 18% and 20% respectively. Moreover, it is revealed that optimization of PID controller through multi objective epsilon constraint method via RBF NN of the simplified HVAC system based on non-linear decoupling method shows better transient response and reaches better dynamic performance with high precision than other PID control tuning techniques. The proposed optimum PID controller and estimation of dynamical model of the HVAC system are compared with the different tuning techniques such as RBF and Z-N based on original system. It is observed that the energy cost function due to temperature ( $J_T$ ) and humidity ( $J_{RH}$ ) are lowered by 15.7% and 4.8% respectively; whereas the energy cost functions reflect the energy consumptions of temperature and humidity which are produced by the humidifier and heating coil. Therefore, based on the new optimization method the energy efficiency of the system is increased. The unique combination of epsilon constraint method and RBF NN has shown that this optimization method is promising method for the tuning of PID controller for non-linear systems.

## ABSTRAK

Sistem Pemanasan, Pengalihudaraan dan Penyaman Udara atau dikenali sebagai (HVAC) adalah satu sistem yang telah direka untuk mengekalkan dan melaraskan kelembapan dan juga suhu di beberapa kawasan. Untuk mengawal kadar kelembapan dan juga suhu dengan menggunakan sistem HVAC terdapat beberapa kaedah yang telah diperkenalkan antaranya Ziegler-Nichols (Z-N), Chien-Hrones-Reswick (CHR), kaedah cubaan, masa tindak balas teguh, kaedah pengoptimuman ia ini dikenali sebagai pengoptimuman kerumunan zarah (PSO) dan juga kaedah rangkaian neural (RBF-NN). Berkadaran kamiran terbitan (PID) adalah salah satu jenis alat kawalan yang sering digunakan kerana mempunyai kelebihan dari segi persaingan harga pasaran dan juga kemudahan melaraskan dan pengoperasian alat kawalan. Walau bagaimanapun, untuk mengawal sistem HVAC secara efektif dengan menggunakan alat kawalan jenis PID, pemboleh ubah untuk mengawal PID ini perlu dioptimumkan. Di dalam hasil kerja ini, pemalar epsilon dengan menggunakan kaedah rangkaian neural (RBF-NN) telah digunakan bagi mendapatkan nilai pemboleh ubah yang optimum bagi alat kawalan jenis PID. Kelebihan menggunakan kaedah ini ialah ia mempunyai kadar tindak balas yang cepat dan tepat dengan nilai yang ingin dicapai berbanding dengan kaedah yang lain. Hasil kajian ini juga melibatkan penganggaran model dinamik bagi sistem HVAC. Kaedah pengasingan secara tidak linear digunakan bagi mengubah model sistem HVAC. Kelebihan dengan menggunakan kaedah tatasusunan gandaan relatif (RGA) yang dicadangkan mempunyai ciri-ciri yang mudah, tepat dan juga meminimumkan kesan nilai yang tidak linear dan sistem penghubung di dalam model HVAC. Berdasarkan pemerhatian, nilai yang dihasilkan bagi ralat kamiran mutlak (IAE) suhu dan kelembapan bagi model yang telah dicadangkan menurun kepada 18% dan 20%. Selain daripada itu, dengan mengoptimumkan alat kawalan jenis PID menggunakan kaedah RBF-NN sistem HVAC pengasingan secara tidak linear menunjukkan hasil tindak balas seimbang yang lebih baik dan mencapai prestasi dinamik dengan kadar ketepatan yang lebih baik daripada kaedah lain. Kaedah yang dicadangkan telah dibandingkan hasil keputusannya dengan kaedah penalaan yang lain. Hasil dari keputusan menunjukkan kos fungsi yang dihasilkan bagi suhu ( $J_T$ ) dan kelembapan ( $J_{RH}$ ) adalah lebih rendah sebanyak 15.7% dan 4.8%; manakala fungsi kos tenaga mencerminkan penggunaan tenaga disebabkan suhu dan kelembapan yang dihasilkan oleh pelembap dan pemanasan gegelung. Oleh itu, berdasarkan kaedah pengoptimuman baru kecekapan tenaga sistem ini meningkat. Gabungan unik kekangan epsilon dan RBF NN telah menunjukkan bahawa kaedah pengoptimuman ini adalah kaedah yang berpotensi untuk penalaan pengawal PID sistem tidak linear.

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**LIST OF ABBREVIATIONS**

|        |   |   |
|--------|---|---|
| AC     | - | Air conditioner   |
| ANF    | - | Adaptive neuro-fuzzy  |
| ANN    | - | Artificial neural network   |
| AR     | - | Auto regressive   |
| ARIMA  | - | Autoregressive integrated moving average                                  |
| ARMAX  | - | Auto regressive moving average exogenous                                  |
| ASHRAE | - | American society of heating, refrigerating and air-conditioning engineers |
| CAS    | - | Central air supply  |
| C-H-R  | - | Chein-Hrones-Reswick  |
| CN     | - | Condition number  |
| COP    | - | Coefficient of Performance  |
| DAS    | - | Discharge air system  |
| DFL    | - | Direct feedback linear  |
| DNAC   | - | Decentralized non-linear adaptive controller                              |
| EC-RBF | - | Epsilon constraint-RBF  |
| EDE    | - | Energy delivery efficiency  |
| FS     | - | Fuzzy system  |
| FLC    | - | Fuzzy logic controller  |
| GFS    | - | Genetic fuzzy system  |
| GL     | - | Genetic learning  |



|         |   |   |
|---------|---|---|
| HVAC    | - | Heating ventilation air conditioning              |
| HVAC&R  | - | Heating ventilation air conditioning and research |
| IAE     | - | Integral absolute error                           |
| IEEMS   | - | Indoor environment energy management system       |
| LD      | - | Lie derivative                                    |
| LR      | - | Lagrangian relaxation                             |
| LS      | - | Least square                                      |
| MF      | - | Membership function                               |
| MLP     | - | Multi layered Perceptron                          |
| NFS     | - | Neuro-fuzzy system                                |
| NFC     | - | Neuro-fuzzy controller                            |
| NI      | - | Niederlinski index                                |
| NN      | - | Neural network                                    |
| NTU     | - | Number of transfer unit                           |
| P       | - | proportional                                      |
| PI      | - | proportional integral                             |
| PID     | - | Proportional integral derivative                  |
| PMV     | - | Predictive mean vote                              |
| RB      | - | Rule base   |
| RGA     | - | Relative gain array                               |
| RIA     | - | Relative interaction array                        |
| RIW-PSO | - | Random inertia weight particle swarm optimization |
| RLS     | - | Recursive least square                            |
| SFLC    | - | Self-fuzzy logic controller                       |
| SISO    | - | Single input single output                        |
| STFPIC  | - | Self -tuning fuzzy pi controller                  |
| THC     | - | Temperature-humidity control                      |

|       |   |                                      |
|-------|---|--------------------------------------|
| THC1  | - | Heater and thermostat-controlled fan |
| THC2  | - | Fan and thermostat-controlled heater |
| $T_s$ | - | Settling time                        |
| VAV   | - | Variable air volume                  |
| Z-N   | - | Ziegler-Nichols                      |

## LIST OF SYMBOLS

|                  |   |  |
|------------------|---|--|
| $\rho$           | - | Air mass density   |
| $T_{ao}$         | - | Air outlet temperature                                   |
| $T_2(t)$         | - | Air temperature immediately following the heat exchanger |
| $T_1(t)$         | - | Air temperature prior                                    |
| $T_{a_1}$        | - | Ambient temperature                                      |
| $T_a$            | - | Ambient temperature of outside air                       |
| $\overline{T_a}$ | - | Average ambient temperature of inside and outside air    |
| $\overline{T_c}$ | - | Average conduit temperature                              |
| $\overline{T_w}$ | - | Average temperature of chiller                           |
| $\overline{T_t}$ | - | Average temperature of inside and outside air            |
| $K$              | - | Constant gain  |
| $C_p$            | - | Constant pressure specific heat of air                   |
| $c_{pc}$         | - | Constant pressure specific heat of coil                  |
| $K_c$            | - | Controller integral gain                                 |
| $q_{sj}$         | - | Cooling loads  |
| $q_{lj}$         | - | Cooling loads  |
| $\Delta k_p$     | - | Corrections of the $k_p$                                 |
| $\Delta k_i$     | - | Corrections of the $k_i$                                 |
| $\Delta k_d$     | - | Corrections of the $k_d$                                 |
| $\Delta b_j$     | - | Corrections of the baseband parameters                   |
| $\Delta c_j$     | - | Corrections of the hidden node center                    |
| $C_w$            | - | $c_{pc} * m_{cw}$  |

|               |   |  |
|---------------|---|--|
| $\tau$        | - | Delay  |
| $\tau_v$      | - | Delay  |
| L             | - | Delay  |
| $\rho_w$      | - | Density of water                                   |
| $\rho_{zj}$   | - | Density of zone                                    |
| $T_d$         | - | Duct surface temperature                           |
| $M_{cw}$      | - | Effective mass of coil to outlet water temperature |
| $M_w$         | - | Effective mass of coil to outlet water temperature |
| $V_z$         | - | Effective of thermal space volume                  |
| $V_h$         | - | Effective volume air exchanger                     |
| $\eta_{s,ov}$ | - | Efficiency of fin tube                             |
| $\eta_{c,ov}$ | - | Efficiency of fin tube                             |
| $U_9$         | - | Energy input to the chiller                        |
| $t_{a,1}$     | - | Entering air temperature                           |
| $t_{w,2}$     | - | Entering water temperature                         |
| $h_w$         | - | Enthalpy of liquid water                           |
| $h_{sj}$      | - | Enthalpy of supply air                             |
| $h_w$         | - | Enthalpy of water                                  |
| $h_{fg}$      | - | Enthalpy of water vapor                            |
| $h_{zj}$      | - | Enthalpy of zone                                   |
| $\varepsilon$ | - | Epsilon boundary                                   |
| $\eta_m$      | - | Fan efficiency                                     |
| N             | - | Fan speed  |
| $u_3$         | - | Fan speed control                                  |
| D             | - | Fan wheel diameter                                 |
| $f_a$         | - | Flow rate  |
| gpm           | - | Flow rate of chilled water                         |

|              |   |   |
|--------------|---|---|
| $C_f$        | - | Function of the Reynolds number and coil configuration  |
| $K_p$        | - | Gain  |
| $h_{i,c}$    | - | Heat coefficient between tube and chiller               |
| $h_{i,d}$    | - | Heat coefficient between air and duct                   |
| $h_{m,c}$    | - | Heat coefficient between air and fin coil               |
| $h_{mi,d}$   | - | Heat coefficient between air and inside surface of duct |
| $h_{it}$     | - | Heat coefficient between tube surface and chilled water |
| $q_h(t)$     | - | Heat input to the heat exchanger                        |
| $h_{me,d}$   | - | Heat loss in side duct                                  |
| $h_{e,d}$    | - | Heat loss inside duct                                   |
| $w_{t,o,st}$ | - | Heat of fin coil  |
| $h$          | - | Heat transfer coefficient                               |
| $h_o$        | - | Heat transfer coefficient in the ambient                |
| $h_i$        | - | Heat transfer coefficient inside duct                   |
| $Q(t)$       | - | Heat transfer rate                                      |
| $w_a$        | - | Humidity ratio of air                                   |
| $w_s$        | - | Humidity ratio of air supply                            |
| $W_o$        | - | Humidity ratio of outdoor air                           |
| $w_{co}$     | - | Humidity ratio of the air out from the coil             |
| $w_m$        | - | Humidity ratio of the air out the mixing box            |
| $w_{si}$     | - | Humidity ratio of the supply air to the humidifier      |
| $W_3$        | - | Humidity ratio of thermal space                         |
| $w_{si}$     | - | Humidity ration of supply air                           |
| $w_{zj}$     | - | Humidity ration of zone                                 |
| $x_r$        | - | Indoor absolute humidity                                |
| $L_a$        | - | Inductance of armature                                  |
| $h_{a,2}$    | - | Inlet air enthalpy                                      |

|               |   |   |
|---------------|---|---|
| $T_{a,in}$    | - | Inlet air temperature                                   |
| $T_{in}$      | - | Inlet temperature of the fluid element                  |
| $h_{w,1}$     | - | Inlet water enthalpy                                    |
| $T_{wr}$      | - | Inlet water temperature                                 |
| $\eta$        | - | Learning rate   |
| $t_{a,2}$     | - | Leaving air temperature                                 |
| $t_{a,2,0}$   | - | Leaving air temperature offset                          |
| $t_{w,3}$     | - | Leaving water temperature                               |
| $L_c$         | - | Lewis number  |
| $m_a$         | - | Mass flow rate of air                                   |
| $U_8$         | - | Mass flow rate of chilled water                         |
| $m_a$         | - | Mass flow rate of the air stream                        |
| $M_a$         | - | Mass flow rate of the air stream                        |
| $m_w$         | - | Mass flow rate of water                                 |
| $m_{wj}$      | - | Mass flow rate of zone                                  |
| $M_c$         | - | Mass of conduit   |
| $m_t$         | - | Mass per unit for coil                                  |
| $m_d$         | - | Mass per unit for duct                                  |
| $m_{fin}$     | - | Mass per unit for tube of coil                          |
| $U_{9max}$    | - | Maximum energy input of the chiller                     |
| $U_{8max}$    | - | Maximum mass flow rate of chilled water                 |
| $\theta_{si}$ | - | Mixed air temperature at the inlet of air handling unit |
| $w_\infty$    | - | Moisture inside duct                                    |
| $w_{d,st}$    | - | Moisture inside of surface duct                         |
| $M_o$         | - | Moisture load   |
| $B_{eq}$      | - | Moment of inertia of the fan wheel                      |
| $j_{eq}$      | - | Moment of inertia of the motor wheel                    |

|              |   |   |
|--------------|---|---|
| $\eta_f$     | - | Motor efficiency  |
| $X_o$        | - | Outdoor absolute humidity                                     |
| $f_o$        | - | Outdoor air flow rate   |
| $\theta_o$   | - | Outdoor air temperature                                       |
| $h_{a,3}$    | - | Outlet air enthalpies   |
| $T_{a,out}$  | - | Outlet air temperature  |
| $T_{ws}$     | - | Outlet supply water temperature                               |
| $T_{out}$    | - | Outlet temperature of the fluid element                       |
| $h_{w,2}$    | - | Outlet water enthalpies                                       |
| $U_c$        | - | Overall heat transfer coefficient based on enthalpy potential |
| $a_{ch}$     | - | Overall thermal capacitance of chiller                        |
| $c_d$        | - | Overall thermal capacitance of humidifier                     |
| $C_a$        | - | Overall thermal capacitance of the air                        |
| $c_{ah}$     | - | Overall thermal capacitance of the air handling unit          |
| $c_h$        | - | Overall thermal capacitance of the humidifier                 |
| $(UA)_{ah}$  | - | Overall transmittance area factor of the air handling unit    |
| $\alpha_h$   | - | Overall transmittance area factor of the humidifier           |
| $\alpha_d$   | - | Overall transmittance- area factor outside humidifier         |
| $\Delta q_i$ | - | Perturbation of input variable from the operating point       |
| $\Delta q_o$ | - | Perturbation of output variable from the operating point      |
| $\Delta p_f$ | - | Pressure rise across the fan                                  |
| $W$          | - | Product of air flow rate and specific heat of air             |
| $w_r$        | - | Product of return specific heat of air                        |
| $h(t)$       | - | Rate of humid air that humidifier can produce                 |
| $R_a$        | - | Resistance  |
| $x_{si}$     | - | Return air absolute humidity                                  |
| $f_r$        | - | Return air flow rate  |

|               |   |   |
|---------------|---|---|
| $\theta_r$    | - | Return air temperature                            |
| $T_{wo}$      | - | Return water temperature                          |
| $\theta_{co}$ | - | Return water temperature to storage tank          |
| $Q_o$         | - | Sensible heat load                                |
| $c_t$         | - | Specific heat capacity of coil                    |
| $c_f$         | - | Specific heat capacity of coil                    |
| $c_{pd}$      | - | Specific heat capacity of duct                    |
| $c_{pa}$      | - | Specific heat of air                              |
| $c_p$         | - | Specific heat of air                              |
| $c_c$         | - | Specific heat of conduit material                 |
| $c_{pw}$      | - | Specific heat of water                            |
| $p$           | - | Static pressure                                   |
| $T_{aoSS}$    | - | Steady state air outlet temperature               |
| $T_{ss}$      | - | Steady state fluid outlet temperature             |
| $x_s$         | - | Supply air absolute humidity in air handling unit |
| $x_d$         | - | Supply air absolute humidity in humidifier        |
| $f_s$         | - | Supply air flow rate                              |
| $\theta_s$    | - | Supply air temperature in air handling unit       |
| $\theta_d$    | - | Supply air temperature in humidifier              |
| $T_h$         | - | Supply air temperature in humidifier              |
| $T_{wi}$      | - | Supply water temperature                          |
| $\theta_{ci}$ | - | Supply water temperature to cooling coil          |
| $A$           | - | Surface area of pipe or duct                      |
| $A_o$         | - | Surface of coil                                   |
| $K_s$         | - | System gain                                       |
| $T_c$         | - | System time constant                              |
| $T_{de}$      | - | System time delay                                 |



|                |   |  |
|----------------|---|--|
| $T_{\infty}$   | - | Temperature inside duct                      |
| $T(x_1)$       | - | Temperature of thermal space                 |
| $T_{\infty,t}$ | - | Temperature of chiller                       |
| $T_o$          | - | Temperature of outdoor air                   |
| $T_2$          | - | Temperature of supply air                    |
| $T(x_3)$       | - | Temperature of supply air                    |
| $T_{si}$       | - | Temperature of supply air to the humidifier  |
| $T_{co}$       | - | Temperature of the air out from the coil     |
| $T_m$          | - | Temperature of the air out of the mixing box |
| $T_m$          | - | Temperature of the air out of the mixing box |
| $T_3$          | - | Temperature of thermal space                 |
| $T_3(t)$       | - | Temperature of thermal zone                  |
| $T_{t,o}$      | - | Temperature of tube                          |
| $\lambda$      | - | Thermal conductivity                         |
| $q_z(t)$       | - | Thermal load                                 |
| $A_d$          | - | Thickness of the wall in duct                |
| $A_{it}$       | - | Thickness of tube in chilled water           |
| $T$            | - | Time constant                                |
| $K_r$          | - | Total control system gain                    |
| $\phi_c$       | - | Varies in space and time                     |
| $f_d$          | - | Varies in space and time                     |
| $v_a$          | - | Velocity of air                              |
| $e_a$          | - | Voltage                                      |
| $f_{sa}$       | - | Volume flow rate of the supply air           |
| $v_{he}$       | - | Volume of heat exchanger                     |
| $V_d$          | - | Volume of humidifier                         |
| $v_{ah}$       | - | Volume of the air handling unit              |

|           |   |                                      |
|-----------|---|--------------------------------------|
| $v_s$     | - | Volume of thermal space              |
| $v_{zj}$  | - | Volume of zone                       |
| $f(t)$    | - | Volumetric air flow rate             |
| $f$       | - | Volumetric flow rate of air          |
| $f_{sw}$  | - | Water flow rate                      |
| $\bullet$ | - | Water flow rate offset               |
| $m_{w,0}$ | - | Water flow rate offset               |
| $\bullet$ | - | Water flow rate offset               |
| $m_w$     | - | Water flow rate through cooling coil |
| $f_c$     | - | Water flow rate through cooling coil |

**LIST OF APPENDICES**

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## **CHAPTER 1**

### **INTRODUCTION**

#### **1.1 Heating Ventilation and Air conditioner (HVAC)**

At present, heating ventilation and air conditioners (HVAC) are common in our lives, especially in the tropical and subtropical regions of the world. HVAC is equipment that is designed to adapt and adjust the humidity as well as temperature in various places. One of the functions of HVAC is to capture heat and channel it outside. However, changing the temperature is not the only function of an air conditioner; the other feature is to function as a dehumidifier. Thus, HVAC can make people feel comfortable (Olesen and Brager, 2004). Two main objectives in the control of HVAC systems are control of both humidity and temperature (Arguello-Serrano and Velez-Reyes, 1999).

Moreover, HVAC mechanisms are also used for setting some environmental variables including temperature, moisture, and pressure (Khooban *et al.*, 2014). Achieving these purposes requires a suitable control system design. A survey by Kelman *et al.* (2012) reported that HVAC operations account for approximately 40% of the domestic energy consumption in the USA. Therefore, it is necessary to design HVAC control system that will deliver a high comfort level and more energy efficient. So far, various types of control systems have been proposed since the advent of HVAC systems (Wemhoff and Frank, 2010).

### 1.1.1 Concepts & Definitions

Air conditioning can be used to control certain environmental conditions including air temperature, air motion, moisture level and radiant heat energy level. Air conditioning involves the cooling of indoor air for thermal comfort, treatment of air for temperature, cleanliness and humidity, and efficient distribution of air to meet the requirements of a particular space. The fundamental targets of any HVAC systems are to provide and set interior thermal conditions that the number of residents will find suitable and sufficient. Sometimes this may need and require that air be changed at an ordinary speed to raise evaporation and transferring heat from the skin. It is mentioned that for providing occupant comfort well it needs to add or remove heat to or from spaces of building. Moreover, it is often a requirement that humidity be removed from spaces during the summer and humidity added during the winter. The foundation key system components which are provided the control functions of HVAC systems are heat and humidity. Before proceeding further, to define the character of HVAC system it is needed to describe many concepts and terms. Each building has balance point temperature, known as exterior temperature which is be able to encourage thermal comfort.

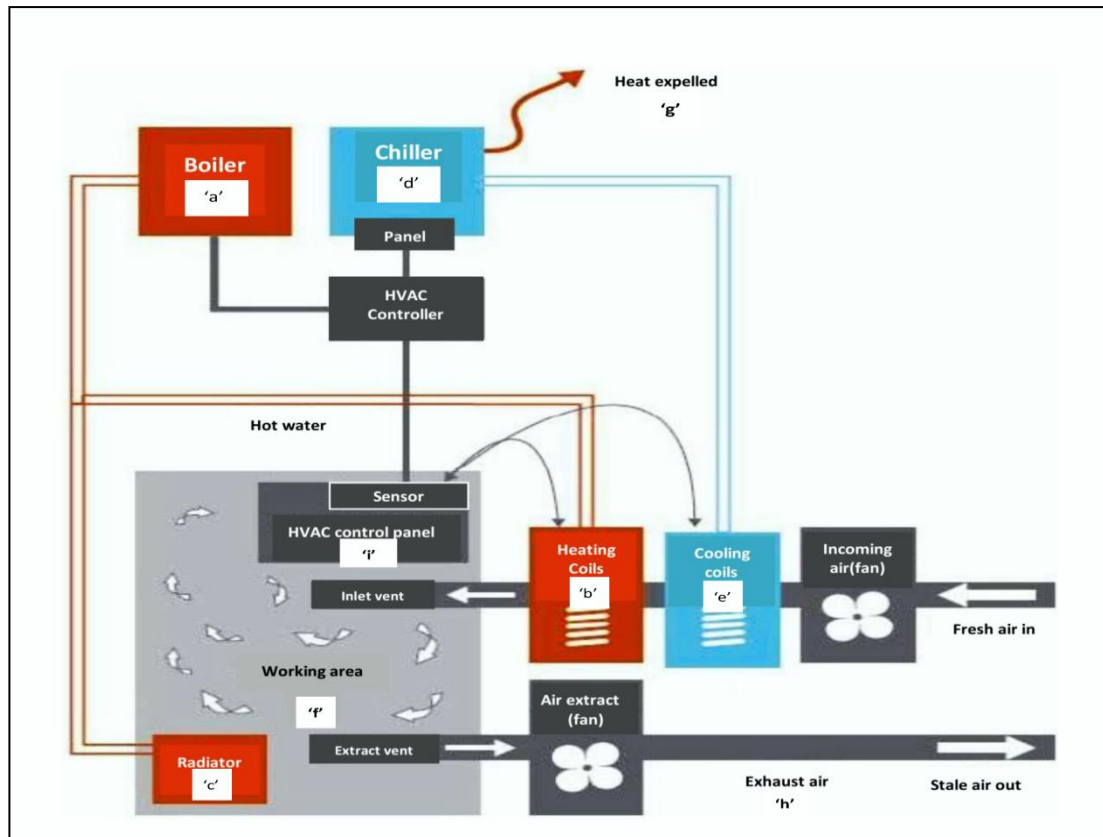
Losses and building heat gains are in equilibrium at the balance temperature. As a result, relevant interior temperature will be preserved naturally and without additionally involvement. When the air temperature of outside go downs below or exceeds, the heating system and cooling system are used, to drop or removes such excess heat, respectively to the balance point temperature (Grondzik and Furst, 2000).

Design of a sufficient controller depends on a good dynamic model of the system. An appropriate system model requires the selection of a suitable controller. The most important of this part is that modeling the components of the HVAC system makes easier to control the system. The model which is developed can be used for comparison validation, which is most important for in the design of a multivariable controller using control theory.

### 1.1.2 Components

Figure 1.1 shows the typical components in a HVAC system. The main HVAC system components are : boilers, cooling equipment, pump and controls (Trust, 2011).

- i) Boilers ('a') create hot water to deliver to the working space. This is done either by heating coils ('b') or through hot water pipes to radiators ('c').
- ii) Cooling tools ('d') cools water for pumping to cooling coils ('e'). Proceed air is then explode blown over the chilled water coils into the space to be cooled ('f') through the ventilation system. As part of the refrigeration cycle in the chiller, heat must also be rejected from the system via a cooling tower or condenser ('g').
- iii) Pumps are used throughout the system to circulate the chilled and hot water to the required areas throughout the building
- iv) Controls are used to make components work together efficiently. They turn tools on or off and tune boilers and chillers, air and water flow rates, temperature and pressure. A controller incorporating one or more temperature ('i') sensors inside the workspace sends a signal to the heating or cooling coils to activate.



**Figure 1.1:** Schematic diagram of typical HVAC system (Trust, 2011)

### 1.1.3 Categorize of HVAC Systems

There are different methods for categorizing the HVAC system; one category of HVAC system is known as the standard or commercial system and another category is the central or local system (Anderson *et al.*, 2007). The discussion to follow will focus on different types of classified HVAC systems.

#### 1.1.3.1 Standard HVAC System

In a standard HVAC system, shared water heaters (or water chillers) supply hot (or cold) water to multiple discharge air system (DAS) air handling units. In such systems, the supply water temperature is not locally controlled.

To each DAS controller, the water supply temperature must be regarded as constant, with any deviation a disturbance. This leaves the water flow rate and input air temperature as the only free parameters that can be locally varied (independent of the air flow rate) to achieve the desired discharge air temperature. Thus, the overall controller for the DASs typically consists of multiple, SISO control loops. For each loop controller, only one system parameter is regulated (Anderson *et al.*, 2007).

### 1.1.3.2 Commercial Systems

In a commercial HVAC system, a central air supply (CAS) typically provides air at a controlled temperature and flow rate for use in heating (or cooling) a space. A heating (or cooling) coil within the discharge air system (DAS) is used for heating (or cooling) the discharged air. The temperature of the discharged air is controlled by regulating the rate at which hot (or chilled) water flows through its heating (or cooling) coil(s). The flow rate of the discharged air is regulated to maintain a predetermined static air pressure within the temperature controlled space. The heat flow rate from a heating coil is a function of the flow rates of both the hot water and air, as well as the temperatures of the air and water flowing through the coil. In such a DAS, it is common to employ four separate single input single output (SISO) controllers to independently control these four parameters.

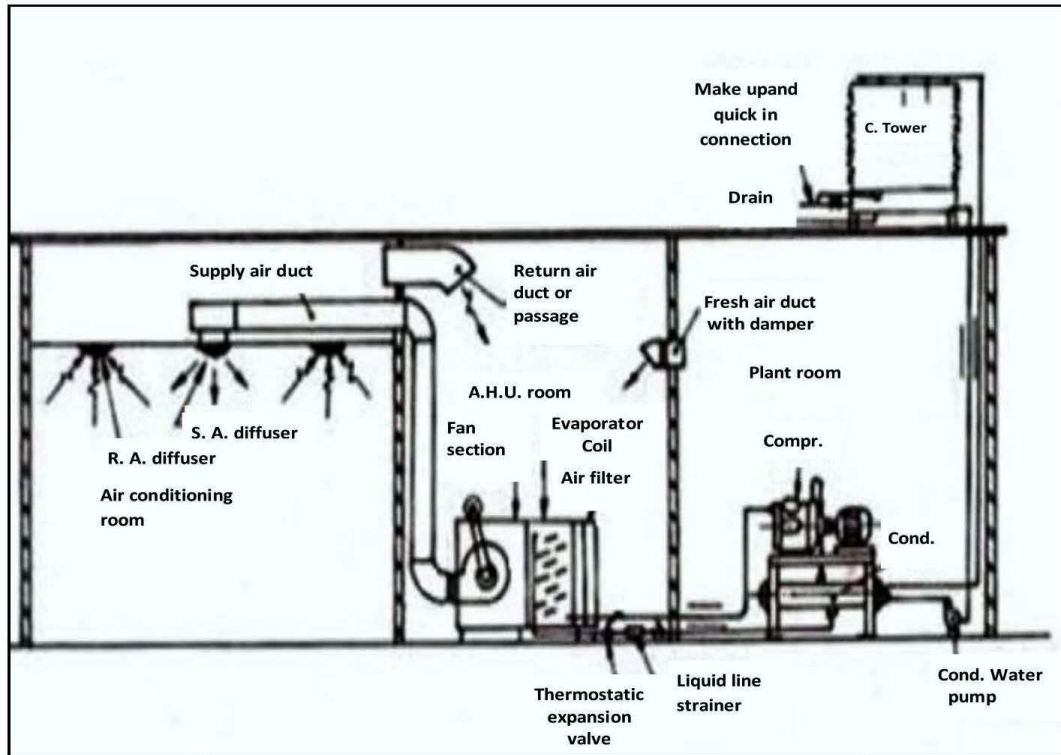
In a DAS, the temperature of the air leaving the mixing box, and subsequently going into the coil, is determined by the temperatures of the external and return air and the ratio at which they are mixed. Typically, the external and return air dampers are controlled in a coordinated manner so that the airflow rate is unaffected while the external-to-return air mix is varied to achieve a predetermined input air temperature (within the range limited by the return and external air temperatures). In general, the temperature of the water supplied to the heating coil is maintained at a constant temperature. The flow rate of the hot water through the coil is the primary parameter manipulated to control the heat flow rate and hence the discharge air temperature (Anderson *et al.*, 2007).



### 1.1.3.3 Central HVAC System

A central HVAC system has its major components which are located near building and may control and serve one or more thermal zones. The character of central HVAC system to transfer thermal energy is categorized in three types. In the first type system is termed an all-air system, which is conveyed only by means of cooled or heated air. In the second type system is called an all-water system, which is transferred only by means of cooled or hot water. Finally the system is phrased an air-water system which is moved by mixing of heated/cooled air or water.

By using of central HVAC systems there are a various benefits and advantages which are allowed and enabled important components to be separated in a mechanical room which is caused to take place limitation of interruption to building functions. In addition, it is caused to reduce noise and aesthetic impacts on building occupants. Other benefits of using central HVAC systems are economies of scale and reduction of building energy consumption. For the inner one larger system can achieve and improve system efficiencies in many climates by using of cooling towers. The later one in central system is also controlled to centralized energy management control schemes that, is made to reduce the energy consumption of building. Moreover, by using central HVAC system can be more suitable rather than climate control perspective which is active smoke control. Nevertheless, the disadvantages of central HVAC systems can be as a non-distributed system, which is affecting an entire building by failure of any components of equipments. Moreover, the repairing of system will be difficult if the system size and sophistication are increased (Grondzik and Furst, 2000). Figure 1.2 shows the diagram of the central HVAC system.



**Figure 1.2:** Diagram of central HVAC system (Jones, 2004)

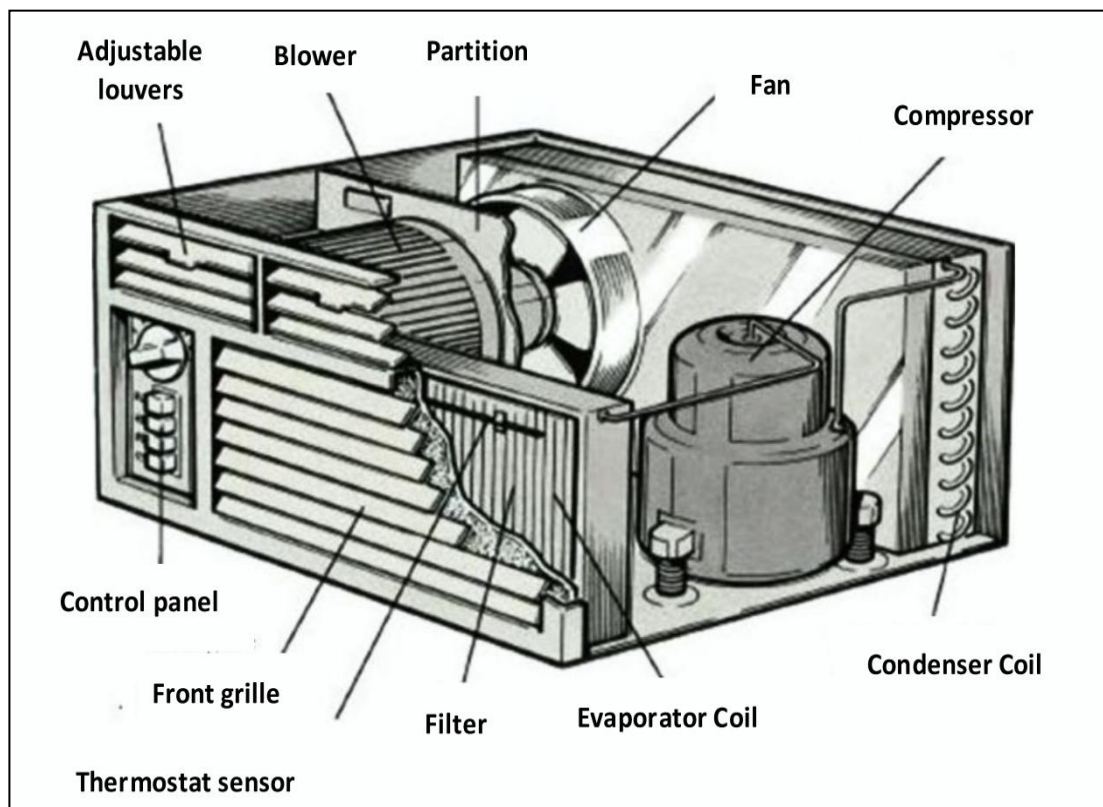
#### 1.1.3.4 Local HVAC System

A local HVAC system has important components which are located near the thermal zone itself, or on the boundary between the zone and exterior environment. This HVAC system controls a single thermal zone. Serving only as a single zone, local HVAC systems will have only one point of control; typically a thermostat for active systems. Each local system generally performs as a standalone system, without consider to the performance of other local systems. There are a many advantages of using local HVAC systems. Local systems tend to be distributed systems. Distributed systems prefer to provide greater collective reliability than do centralized systems.

Since local systems are likely to be of small capacity and are not complex and complicated by interconnections with other units. In addition, the maintenance of local systems tends to be routine and simple. Moreover, in a building which is

unoccupied and has unused space the local system can be turn off and makes energy saving.

Nonetheless, local systems have some disadvantages. For example local system units cannot be smoothly joined together to allow for management operations of centralized energy. Moreover, local systems can normally be centrally controlled with reference to on-off functions through electric circuit control, but it is not possible to use more sophisticated central control such as night-setback or economizer operation. In addition, local HVAC system has the low capacity coefficient of performance (COP). Therefore, they cannot benefit from economies of scale (Grondzik and Furst, 2000). Figure 1.3 shows the diagram of the local HVAC system.



**Figure 1.3:** Diagram of local HAVC system (Jones, 2004)

The comparison of different types of HVAC systems which consist of advantages and disadvantages are tabulated in Table 1.1.

**Table 1.1:** Categories of different types of HVAC system

| Type of system  | Advantage   | Disadvantage   |
|---|---|--|
| Local System  | <ul style="list-style-type: none"> <li>-Distributed systems maintenance tends to be simple, ordinary and available.</li> <li>-Produce suitable occupant comfort through individualized control options.</li> </ul>  | <ul style="list-style-type: none"> <li>-Cannot be easily connected together to let centralized energy management operations.</li> <li>-Be centrally controlled with respect to on-off functions through electric circuit control.</li> <li>-Low capacity.</li> <li>-Cannot suitable from economies of scale.</li> </ul>                                  |
| Central HVAC system <ul style="list-style-type: none"> <li>1. Air system</li> <li>2. water system</li> <li>3. Air-water system</li> </ul> | <ul style="list-style-type: none"> <li>-Major equipment components to be isolated in a mechanical room.</li> <li>-Reduce noise and aesthetic impacts.</li> <li>-Offer opportunities for economies.</li> <li>-Improve system efficiencies in many climates.</li> <li>-Can reduce building energy consumption via energy management control.</li> </ul> | <ul style="list-style-type: none"> <li>-Failure of any key equipment component may affect an entire building as a non-distributed system.</li> <li>-Maintenance may become more difficult as system size and sophistication increase.</li> <li>-Transferring of conditions such as air or water imposes space and volume depends on building.</li> </ul> |
| Commercial HVAC system  | <ul style="list-style-type: none"> <li>-Important tools are separated in a mechanical room.</li> <li>-Reduce noise and aesthetic impacts.</li> </ul>  | <ul style="list-style-type: none"> <li>-Maintenance may become more difficult based on system size and sophistication increase.</li> </ul>   |
| Standard HVAC system  | <ul style="list-style-type: none"> <li>-Overall controller for the DASs Typically consists of multiple, SISO control loops.</li> </ul>  | <ul style="list-style-type: none"> <li>-Supply water temperature is not locally controlled.</li> </ul>   |

In this project, the central HVAC system, which consists of air water system, is considered as a result, of having more benefits and advantages than the other types of HVAC systems.

## 1.2 Problem Statements

HVAC systems are a permanent part of everyday life in our industrial society. In developing countries the use of energy is increased which influences the economy and way of life. One of the most important pieces of equipment which influences energy consumption is HVAC system. It is important to mention that the rate of energy consumption is high; therefore, optimizing and developing air conditioning systems have become more and more important (Piao *et al.*, 1998).

It is noticed that the HVAC system is a highly non-linear system which means the input signal and output signal have no proportional relation. However, the HVAC system has played a very important role in the modern world, so identification and simplification of the dynamic model and control of HVAC system have significant justification. However, the basic PID controller which is commonly used to control the parameters of HVAC system is not sufficient based on the structure and characteristics of HVAC system. Therefore, to effectively control the HVAC system using the PID controller, the PID control parameters must be optimized. The problems of this study can be divided in three sections as follows:

- i) HVAC construction
- ii) Difficulty in control design due to complete math model of the HVAC
- iii) Tuning of PID controller to improve performance of the HVAC system

## 1.3 Objectives of Research

The present study investigates the effect of optimization of PID controller on humidity and temperature of simplified model of HVAC system. Regarding to the structure, complexity and non-linearity of the HVAC system simplification and

optimization of HVAC system must be considered. The accomplishment obtained from this investigation will be use full in enhance the performance of HVAC system with improved energy efficiency and human comfort. The adjustment of humidity and temperature are aimed to reduce energy consumption and increase human comfort, respectively.

The specific objectives of this research are:

- i) To examine the effect of non-linear decoupling method on HVAC system
- ii) To carry out the effect of optimization PID controller regarding to new algorithm on parameters of simplified HVAC system
- iii) To study the effect of optimized PID controller regarding to new algorithm on energy efficiency and human comfort.

#### **1.4 Scopes of Research**

In this project, a non-linear decoupling method is used to investigate the structure of a mathematical model of, humidifier and heating coil which are describing relative humidity as well as temperature responses of full mathematic dynamic model of the HVAC system, respectively. It is noticed that in mathematical model of HVAC system the CO<sub>2</sub> and air velocity models are ignored.

Epsilon constraint radial basis function of neural network has been used to control and optimized the parameters of PID controller with reference to overcome the non-linearity and convexity problem of the system. To obtain the optimization tuning method, the epsilon constraint algorithm and radial basis function neural

network has been combined to produce the multi objective optimization method to control the parameters of HVAC system. In addition, following results are obtained:

- i) The performance, transient response and human comfort of system are determined by integral absolute error (IAE) formulation based on new optimization algorithm
- ii) The energy efficiency of system is described by using the cost function formulation based on new optimization algorithm

### **1.5 Significance of Study**

In this research, a novel optimization method based on epsilon constraint through the radial basis function is considered to optimize the PID controller to control the parameters of the HVAC system. It is important to mention that the combination of radial basis function and epsilon constraint is used because of handling the non-linearity of the system and overcome the convexity problems of weighted sum techniques normally used in multi objective optimization.

It is noticed that a study on optimization technique based on epsilon constraint algorithm through the radial basis function is not reported yet. Based on the new algorithm these goals are achieved:

- i) Transient response of the system is improved.
- ii) Energy consumption of the system is decreased.
- iii) Performance of the system is increased.

## 1.6 Thesis Outline

The thesis is divided into 5 chapters.

Chapter 1 presents background of the different types of HVAC system, problem statements, objectives and scope of the study, and outline of the thesis.

Chapter 2 focuses on the literature review. The literature review contains 2 main parts. In the first section the basic principles as well as different models of HVAC systems are introduced. In the second part the different types of tuning PID controller which had been used to control the parameters of HVAC system to achieve energy efficiency and target values are introduced.

In chapter 3, the methodology explains in detail. It consists of 2 main parts. First different types of decoupling method are described. Then different types of tuning method of PID controller are explained. Regarding to the tuning of PID controller based on the new algorithm, the parameters of humidity and temperature of HVAC system are controlled.

Chapter 4 reports the influence of simplified model and tuning of PID controller which are being used in full mathematical dynamic model of HVAC system. This chapter also discusses different decoupling techniques as well as comparison of simplified and original model. Moreover, different types of controllers which are used to control the parameters of the HVAC system are compared and the best result which is validated by MATLAB is displayed.

In chapter 5 the conclusion of the thesis and suggestions for future work are presented.



epsilon constraint method is considered because of ability to overcome the convexity problem of weight sum techniques which is normally used in multi objective optimization method and multi parameters that must be optimized to control the parameters of PID controller. Regarding to new optimization of PID controller based on EC-RBF neural network the performance of the system is increased. In addition, based on EC-RBF neural network the energy cost function, robustness as well as stability of the system for both humidity and temperature are improved. Improving the energy cost function and transient response of system it makes to increase the energy efficiency and improve the human comfort, respectively.

## **5.2 Future Recommendation**

In this study, whereas some assumptions such as CO<sub>2</sub> and air velocity that are influenced the humidity and temperature are ignored. A few suggestions for future work will be considered in two parts as mentioned below:

In modeling part:

Employing mathematical model of CO<sub>2</sub> and air velocity are suggested.

In controlling part:

Based on new structure that is found in modeling part optimization of PID controller regarding to the multi objective and neural network algorithm is suggested.

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