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Tortuosity and other vessel attributes for arterioles and venules of the human cerebral cortex

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A B S T R A C T

Despite its demonstrated potential in the diagnosis and/or staging of disease, especially in oncology, tortuosity has not received a formal and unambiguous clinical definition yet. Using idealized three-dimensional vessel models (wavy helices) with known characteristics, we first demonstrate that, among various possible tortuosity indices, the standard deviation of the curvature K_{sd} best satisfies i) scale invariance and ii) positive monotonic response with respect to the amplitude and frequency of vessel oscillations. K_{sd} can thus be considered as a robust measure of tortuosity. On the contrary, indices previously considered as tortuosity metrics, such as the distance factor metrics (DFM), are highly scale dependent and inappropriate for that purpose.

The tortuosity and other vessel attributes (curvature, length-to-diameter ratio (LDR),...) of more than 15,000 cortical vessels are subsequently studied, establishing their statistical properties as a function of the vessel nature (arterioles versus venules) or topological order (hierarchical position). In particular, arterioles have a higher LDR than venules, but the two kinds of vessels have the same mean curvature and tortuosity. Moreover, the lower the order of the vessels, i.e. the nearer to the capillary network, the more curved and tortuous they are. These results provide an essential reference both for diagnosis and for a future large reconstruction of the cerebral microvascular network.

Introduction

Vascular architecture, particularly of cerebral microvessels, has profound implications upon both health and disease. In fact, quoting Bullitt et al. (2005a), “almost every disease from cancer to the common cold affects blood vessel attributes (vessel number, radius, tortuosity and branching pattern)”. Vascular alterations associated with pathology are attracting attention (Lu et al., 2004) with pathological angiogenesis being a recognized hallmark of disease (Carmeliet, 2005; Carmeliet and Jain, 2000; Fukumura and Jain, 2008). Furthermore, cerebral microcirculation is linked to many other areas such as functional neuroimaging (Lorthois et al., 2011a,b; Uludağ et al., 2009; Weber et al., 2008), Alzheimer's disease (Meyer et al., 2008), vascular occlusions in cerebro-vascular disease (Nishimura et al., 2007), and blood vessel morphologic changes during growth and subsequent treatment of brain tumors (Baish and Jain, 2000; Baish et al., 1996; Bullitt et al.,

2005b, 2007b; Jain, 2005). Thus, providing accurate and comprehensive measurements of vascular morphology is essential in the analysis of vascular formation and structural adaptations under physiological (development, growth and exercise) or patho-physiological conditions (inflammation, hypertension, diabetes, obesity and metabolic syndrome, cancer) (Jonk et al., 2007; Levy et al., 2008; Murfee and Schmid-Schonbein, 2008; Patton et al., 2005; Pries and Secomb, 2008; Pries et al., 2005; Wiernsperger et al., 2007).

In this context, a wide variety of morphometric parameters, or vessel attributes, are potentially available for automated analyses. For example, a user-interactive software quantifying local vessel diameter, tortuosity, fractal dimension, and avascular spacing of two-dimensional (2D) digitized vascular trees is now commercially available (Vickerman et al., 2009). Among these parameters, vessel tortuosity has a demonstrable importance in the diagnosis of many diseases. For example, the clinical recognition of abnormal vascular tortuosity can lead to the diagnosis of tumors and retinopathies, among other conditions (Johnson and Dougherty, 2007).

Regarding tumors, malignancy induces characteristic vascular morphological changes, described as “...a profound sort of tortuosity, with many smaller bends upon each larger bend” (Baish and Jain, 2000). This abnormal tortuosity may be related to increases in nitrous oxide

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induced by VEGF (Folkman, 2000) and is found in a wide variety of malignant tumors including those of the breast (Huang et al., 2008; Lau et al., 1999), brain (Burger et al., 1991), colon (Siemann, 2002), lung (Helmlinger et al., 2002), and skin (Astner et al., 2008). The widespread view is that these microvascular shape abnormalities and severe abnormal network architecture increase the geometric resistance to blood flow – which in general is significantly higher in tumors than in normal tissues – and decrease overall perfusion (Baish et al., 1996; Jain, 1988). The resulting – heterogeneous and/or compromised – inadequate blood supply hinders the delivery of therapeutic agents to tumors and causes an abnormal microenvironment within them, a feature that selects out more aggressive and metastatic cancer cells and favors tumor growth. However, a recent study (Gaustad et al., 2009) suggested that differences in blood supply between individual tumors growing in a mouse dorsal window chamber mainly are a consequence of differences in the geometric resistance of the tumor-supplying arteries (i.e., differences in vessel tortuosity and diameter) rather than features of the tumor microvascular network.

Vessel shape abnormalities indeed extend far beyond tumor confines and involve initially healthy vessels coursing in the tumor vicinity (Li et al., 2000). It is possible to visualize these larger vessels using high-resolution non-invasive magnetic resonance angiography (MRA), as demonstrated by Bullitt et al. in a series of papers on the breast and brain tumors (Bullitt et al., 2003, 2005a,b, 2006a,b, 2007a,b). In these papers, a new “Malignancy Probability” equation, based on a quantitative, statistical measure of vessel tortuosity derived from two different tortuosity indexes, has been introduced. On this basis, all but one of 30 human brain tumors have been successfully classified as benign or malignant, by reference to histological evaluation. In a study on choroid plexus carcinoma in genetically engineered mice, these analyses of vessel tortuosity correctly identified emerging malignancy even in very small lesions (0.3 to 1 mm³ in size), which had posed problems for other diagnosis modalities (Bullitt et al., 2006b). Thus, vessel shape may predict tumor response several months in advance of traditional methods. Interestingly, abnormal vessel tortuosity appears to resolve rapidly with effective treatment (Baish et al., 1996; Jain, 2001; Li et al., 2000), making the approach potentially useful for therapeutic development and assessment in preclinical murine models and for rapid assessment of treatment in human subjects.

As such, analysis of vessel tortuosity may offer a complementary approach to magnetic resonance perfusion imaging: assessment of malignant tumors by analyzing their vascular tortuosity has already been performed on images acquired from 3D power Doppler ultrasound (e.g. ovarian mass, Sladkevicius et al., 2007) and in vivo fluorescence confocal microscopy (e.g. skin cancer, Astner et al., 2008; Lademann, 2008).

Regarding retinopathies, ophthalmologists use morphological features of the retinal vascular tree as signs suggesting their onset or prognosis. For example, morphological features of the retinal vascular tree are often the early symptoms indicating the onset of hypertensive retinopathy (Grisan et al., 2008). Tortuosity is also increased in diabetes, although it predominantly affects venules (Sutter and Helbig, 2003). Moreover, in plus disease, which is a major component of the international classification for retinopathy of prematurity (ROP) and is characterized by arteriolar tortuosity and venous dilation, computer-based image analysis systems have shown a higher diagnosis accuracy than ROP experts (Gelman et al., 2007; Kemper et al., 2008).

In addition, in the retinal microcirculation, the arteriolar length-to-diameter ratio (LDR) has been found to increase in hypertension (Wong et al., 2001, 2002, 2003) and, very recently, in Alzheimer’s disease (AD) (Frost et al., 2013). This increase was associated with increased stroke mortality (Witt et al., 2006), suggesting that evaluation of the retinal microvasculature may be a useful predictor of target organ damage and cardiovascular risk. An unexpected relationship between reduced tortuosity and death from ischemic heart disease (IHD), independent on blood pressure, has also been observed (Witt et al., 2006).

Reduction of venous tortuosity has also been demonstrated in AD (Frost et al., 2013).

Other clinical applications have been proposed in neurology, where a morphometric analysis of arteriolar tortuosity in human cerebral white matter demonstrated changes associated with clinical vascular dementia (Brown et al., 2009).

Despite its demonstrated potential in the diagnosis and/or staging of disease, tortuosity has not received a formal and unambiguous clinical definition yet. The clinical findings reviewed above indeed rely on diverse methodologies used for measuring the microvascular changes, either qualitatively or quantitatively: several possible indexes have been proposed, including the distance factor metric (Hart et al., 1999; Smedby et al., 1993), the number of inflection points (Bullitt et al., 2003), the angle change along segments (Bullitt et al., 2003; Gelman et al., 2007) and various line integrals of local curvature values (Hart et al., 1997, 1999), but none has gained universal acceptance or utility. Results derived from these different measures are sometimes contradictory or even directly opposite, as noted by Bullitt et al. (2005b). As they point out, “it might be desirable to formulate a single tortuosity metric capable of detecting both large and small scale tortuosity abnormalities at the same time, but we have not yet been able to do so.”

Thus, in spite of the promising results obtained by this group, the question of finding an index that adequately matches intuitive notions of tortuosity remains open. Adding to the difficulty is the fact that tortuosity does not have a formal clinical definition. For Hart et al. (1997, 1999) and Johnson and Dougherty (2007), several intuitive properties like reproducibility, invariance to affine transformations and compositionality need to be satisfied in order to yield a clinically meaningful tortuosity measure. In addition to these properties, a monotonic relationship with respect to amplitude and frequency of the vessel bends is needed (Grisan et al., 2008).

Hart et al. (1999) described seven measures of tortuosity and tested their ability to classify the data extracted from retinal images in tortuous or non-tortuous vessels. While no single tortuosity measure was clearly superior, they recommended a total squared curvature measure. However, as with most of the previous research until recently, their analysis was applied to 2D images and is therefore inadequate for analyzing 3D data (O’Flynn et al., 2007). Johnson and Dougherty (2007) also proposed a mean square curvature measure. Their approach was tested in 3D on model objects, by manipulating the parameters of simple noisy helices simulated by adding small random components to the helix radius. More recently, they applied their metrics to abdominal aortograms of low tortuosity and established their validity through a strong observed correlation with the ranking of an expert panel of three vascular surgeons (Dougherty and Johnson, 2008). O’Flynn et al. (2007) introduced a method for the three-dimensional geometric characterization of the arterial vasculature from MR angiograms, with possible applications in planning of endovascular interventional procedures and in improving endovascular device design and endograft sizing. However, in this work, the centerline data are smoothed by using a ninth-order polynomial approximation. If this is reliable in large and relatively straight arteries such as the aorta, it would probably become much less accurate when applied to the tortuous vessels of brain microcirculation.

Ultimately, despite the importance of abnormal vessel attributes in clinics, little is known about the statistical properties of vessel attributes or branching patterns, even in healthy conditions. In particular, it is unclear whether the statistical properties of various vessel attributes fit a Gaussian distribution, and how dependent upon anatomical location they might be (Bullitt et al., 2005a). These uncertainties impair our ability to reveal signatures of normal vascular trees (Cassot et al., 2010) and to design studies that compare patients with suspected disease to a database of healthy subjects (Bullitt et al., 2005a).

Therefore, the first objective of this paper is to propose a three-dimensional methodology yielding new and more robust indexes of tortuosity and curvature. For that purpose, idealized vessel models are considered. Using such idealized vessels, with known characteristics, the validity and geometrical significance of this new methodology can be checked and discussed by comparison with various indexes proposed in the literature. The second objective is to apply this methodology to a large microvascular database of the human cerebral cortex. This will allow the statistical data needed as reference or rationale for further assessment of vessel attributes under pathological conditions for the purpose of clinical diagnosis and disease staging to be obtained. For that purpose, a 3D quantitative anatomical data library on the architecture of the microcirculation of the human cerebral cortex, previously produced by our group (Cassot et al., 2006), is exploited.

This same data library has previously been used with success to assess the general morphometric and topological characteristics of the arteriolar, venular and capillary cortical networks (Cassot et al., 2006; Lauwers et al., 2008), their multi-scale properties (Cassot et al., 2009; Lorthois and Cassot, 2010) and the variations of microvascular density as a function of cortical depth (Lauwers et al., 2008). These data have fed a significant number of simulation studies. These studies include blood flow simulations by our group in the corresponding anatomical network, which enabled to study brain blood flow regulation in the context of functional neuroimaging (Lorthois et al., 2011a,b). They also include modeling approaches of blood flow and oxygen transfers based on the generation of synthetic vascular architecture (Su et al., 2012; Linninger et al., 2013). In these papers, however, straight vessels were considered, while the influence of tortuosity on oxygen transfers has been demonstrated (Goldman and Popel, 2000).

In the present paper, we consider the vessel attributes (curvature, tortuosity, length-to-diameter ratio) of cortical vascular trees, establishing their statistical properties as a function of the vessel nature (arterioles versus venules) or the segment topological order (hierarchy).

Materials and methods

Creation of a microvascular network database of the human cerebral cortex

The procedures used for image acquisition, mosaic construction and vessels segmentation have been described in detail elsewhere (Cassot et al., 2006) and are briefly outlined below.

Data acquisition

Digital three-dimensional images of the intra-cortical vascular network were obtained from thick sections (300 μm) of India ink-injected human brain (Duvernoy et al., 1981) by confocal laser microscopy. The specimen used in this study was a 60-year old female who died from an abdominal lymphoma with no evidence of vascular or cerebral disease. The secondary cortex next to the collateral sulcus in the right temporal lobe was the anatomical region chosen for this study owing to the outstanding quality of the injection in this area. While it is noteworthy that anatomical preparation is likely to induce shrinkage, generating an underestimation of morphometric data (length, diameter), the technique of injection, used to “mark” the vessels and give a complete and physiological-like perfusion of the whole vascular system of the brain, is likely to generate uniform shrinkage in the specimen.

The entire volume of the cortex on both sides of the sulcus (fusiform and parahippocampal gyri) was digitized on 3 adjacent coronal sections. Each elementary dataset contained 70 sections of 512×512 pixels, with a voxel size of $1.22 \times 1.22 \times 3 \mu\text{m}$.

These individual datasets covering a large zone were then summarized in a special data object called an image mosaic and realigned to ensure that the vessels in the overlapping area matched perfectly. Ten mosaics were so constructed to cover the entire cortex area chosen corresponding to a cortical volume of 28.6 mm^3 .

Each image mosaic contains a large quantity of data (typically several gigabytes) and is too large to be processed at once in the memory of a standard personal computer. Adapted methods were developed to adequately process such images (Cassot et al., 2006; Fouard et al., 2006). Their main feature and advantage are that they process data locally while preserving global properties. They allowed the extraction of vessel center lines and the computation of distance maps which measure the distance between any points within a vessel to the nearest vessel wall, providing for each center line point a good estimation of the vessel radius. Finally, a graph representation (skeleton) of the 3D microvascular network was obtained for each mosaic and a value of the vessel radius estimated from the distance map was attached to every vertex. For further processing of the morphometric data and analysis of the topology, the skeleton lineset was stored in an ASCII file. Each line of this file corresponds to a vertex (center line point) and contains its x, y, z coordinates and the radius of the vessel at this point. The vertices of a given segment, i.e. a blood vessel between two successive bifurcations, are listed successively, and vessel segments are separated.

Next, to account for the dual nature of the network architecture (Lorthois and Cassot, 2010), the tree-like arterioles and venules were separated from the whole skeleton, which also includes capillary vessels. To extract a vascular tree, its origin in the sulcus was identified and all the paths from this origin through vessel segments in which resistance to flow is lower than a prescribed value were detected (Cassot et al., 2006). Each tree was classified as arterial or venous according to its morphological features, following Duvernoy's classification (Duvernoy et al., 1981; Reina-De La Torre et al., 1998).

Vessel taxonomy

The topology of these vascular trees was analyzed according to the diameter-defined Strahler taxonomy (Kassab et al., 1993). This taxonomy produced a hierarchical ranking of vessel segments, assigning them an order from 0, for the “terminal” branches closest to the capillaries, to a maximal rank for the branches closest to the pial tree origin. In many instances, several vessel segments of the same order are connected in series: their combination is then called an element (Cassot et al., 2006).

Derivation of geometrical parameters

In order to remove any spurious local curvature discontinuity of the vessel which may arise from voxel-sized artefacts or from the segmentation process, centerline coordinate data of each vascular segment were smoothed prior to 3D geometrical analysis. For this purpose, a simple five-points weighted local smoothing, centered on each vertex, was applied to each coordinate of the centerline points (Abramovitz and Stegun, 1972).

Arc length s was then determined at each vertex. This smooth curve description was then resampled using cubic spline interpolation to yield vertices at constant intervals ($\Delta s = 0.5 \mu\text{m}$) along the curve length. First, second and third derivatives with respect to the arc length s were derived for each vertex of the resampled curves. This smoothing and interpolating process led to define parameterized centerline curves for each vascular segment in the form $\mathbf{r}(s) = (x(s), y(s), z(s))$ with their corresponding derivatives $\mathbf{r}'(s) = (x'(s), y'(s), z'(s))$, the unit tangent vector (Korn and Korn, 2000), $\mathbf{r}''(s)$ and $\mathbf{r}'''(s)$.

Vessel curvature and torsion

The Frenet frame (\mathbf{t} , \mathbf{b} , \mathbf{n}) at each vertex is straightforwardly defined using the following formulae (Korn and Korn, 2000):

$$\mathbf{t} = \mathbf{r}' \quad ; \quad \mathbf{b} = \mathbf{r}' \times \mathbf{r}'' / |\mathbf{r}''| \quad ; \quad \mathbf{n} = \mathbf{b} \times \mathbf{t},$$

where \times denotes the cross product.

Provided with the parametric representation of the curve defined above and using the Frenet–Serret theory of differential geometry, curvature κ and torsion τ can be derived using standard formulas (Korn and Korn, 2000):

$$\kappa = \left| \mathbf{r}''(s) \right| \quad \text{and} \quad \tau = \frac{[\mathbf{r}'(s), \mathbf{r}''(s), \mathbf{r}'''(s)]}{|\mathbf{r}''(s)|^2}$$

where $[\mathbf{r}'(s), \mathbf{r}''(s), \mathbf{r}'''(s)]$ denotes a scalar triple product.¹ These parameters are computed at all vertices of the interpolated centerline curves.

Assessment of vessel tortuosity

In order to quantify the tortuous nature of vessels, various line integrals of local curvature values have previously been used. In the present work, the curvature average value by unit length (κ_m) as well as its standard deviation (κ_{sd}) and root mean square (κ_{rms}) are computed for each segment according to:

$$\kappa_m = (\Delta s/L) \sum_{i=3}^{n-2} \kappa_i,$$

$$\kappa_{sd} = (\Delta s/L)^{1/2} \sqrt{\sum_{i=3}^{n-2} (\kappa_i - \kappa_m)^2}$$

and

$$\kappa_{rms} = (\Delta s/L)^{1/2} \sqrt{\sum_{i=3}^{n-2} \kappa_i^2},$$

where L is the total path length of the vascular segment.

Other indexes of tortuosity have been defined such as the “Distance Metric” (DM) defined as the total path length L of a vessel divided by the linear distance between its endpoints D_{ex} (Bullitt et al., 2003, 2005a), or the “Distance Factor Metric” (DFM) which measures the relative lengthening of a vessel and is simply defined as $DFM = DM - 1$ (O’Flynn et al., 2007). The “Inflection Count Metric” (ICM) multiplies the number of inflections (plus one) present in a 3D space curve by the DM (Bullitt et al., 2003, 2005a). The “Sum of Angles Metric” (SOAM) sums the unsigned angular variations between successive points along a sampled space curve and normalizes by path length² (Bullitt et al., 2003, 2005a).

Another widely used shape factor: the length-to-diameter ratio

A simple and robust way to characterize the vessel shape is to compute the length-to-diameter ratio for each segment and to analyze the statistical distributions of this ratio on the whole segments and on sub-groups defined as a function of their nature and taxonomy.

Validation using helical curves

Circular helices ($x = R \cos t$; $y = R \sin t$; $z = \lambda t$; $t \in [0, t_{max}]$) have uniform curvature and torsion given by $\kappa = \frac{R}{R^2 + \lambda^2}$ and $\tau = \frac{\lambda}{R^2 + \lambda^2}$.

¹ Note that these expressions are different from the expressions of curvature and torsion used by O’Flynn et al. (2007) (see Eqs. 3 and 5 in their paper). However, these equations can be simplified by taking into account that $|\mathbf{r}'(s)| = 1$.

² Note that, with an alternative definition using the signed angular variations instead of the unsigned ones, the SOAM would be very close to the mean curvature, as the signed angular variation between successive points $d\alpha$ can be approximated by $ds/r(s)$, $r(s)$ being the local radius of curvature.

Moreover, their path length ($t_{max} \sqrt{R^2 + \lambda^2}$) is proportional to the maximal range of the parameter t . For further analysis, we introduce the angular extension A of the helix in the Oxy plane as multiples of $\pi/4$ angles (i.e. $t_{max} = A \cdot \pi/4$).

To simulate “smaller bends over a larger bend” (Baish and Jain, 2000), we added a sinusoidal component to the constant radius R so that $R = R_0 + \alpha \sin 2kt$, where α is the amplitude of the oscillations and k is their angular frequency. Such wavy helices, some of which are displayed in Fig. 1, are fully defined by the following set of five parameters ($R_0, \lambda, \alpha, k, A$). In this particular case, and more generally when the coordinates of a segment can be described analytically, the curvature can be calculated semi-analytically, which can then be used to validate the various indexes and the numerical methods proposed above.

Finally, noisy vessels (see Fig. 1) were simulated by adding a random component $\beta = (0.5 - \rho)/2^\chi$ where ρ is a random number between 0 and 1 and $\chi = 1, 2$ or 3 for a signal-to-noise ratio of 6, 9 and 12 dB, respectively.

Statistical data analysis

A standard statistical analysis was applied to the vessel attributes populations. To determine statistical significance of differences, especially between the mean or median values of the vessel attributes as a

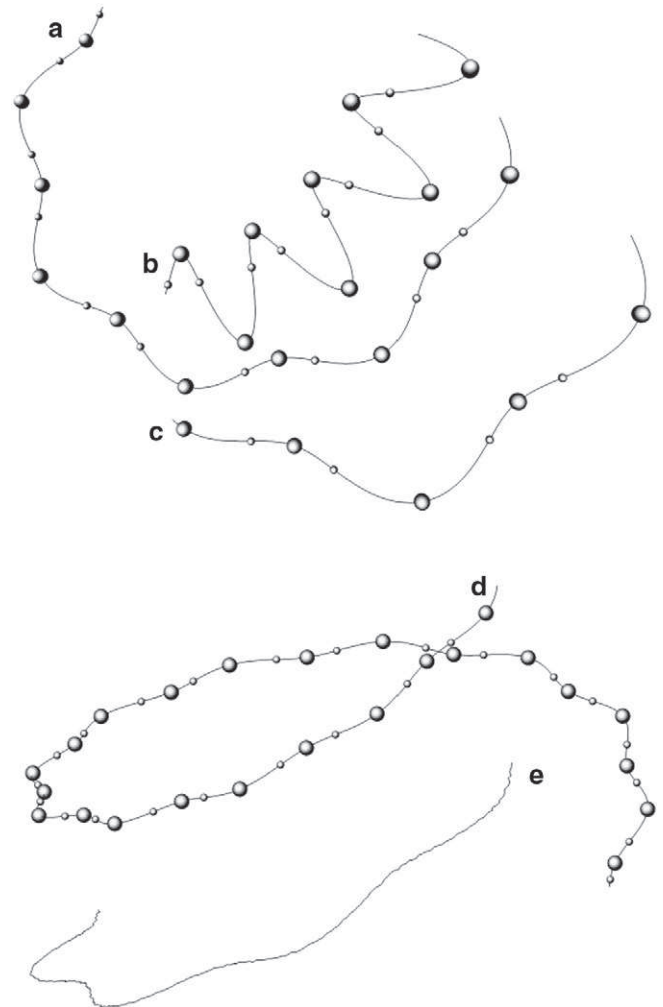


Fig. 1. Examples of wavy helices (a to d) and effect of noise (e). $R_0 = 30$; $\lambda = 6$. (a) $T = 5$, $k = 4$, $\alpha = 2$; (b) $T = 2$, $k = 8$, $\alpha = 6$; (c) $T = 3$, $k = 3$, $\alpha = 3$; (d) $T = 8$, $k = 6$, $\alpha = 1$; (e) $T = 4$, $k = 4$, $\alpha = 2$, $S/N = 6$ dB. Small spheres show inflection points and large spheres local maxima.

function of the nature and taxonomy, we carried out various statistical analyses, including paired or unpaired Student t tests, Kruskal–Wallis and Wilcoxon–Mann–Whitney non-parametric tests. From the histograms of local curvature for each segment, the probability densities (functions) of the curvature were derived for subgroups gathered according to their taxonomy, i.e. their order index.

Results

Adequacy of various indexes of tortuosity: assessment on model vessels

The accuracy of the numerical methods presented above has first been tested by comparing the computed values of the six potential indexes of tortuosity defined above (K_m , K_{sd} , K_{rms} , DFM, SOAM and ICM) for circular helices to their analytical values. Then, the significance of these six parameters as tortuosity indexes, and their robustness to noise, has been studied using wavy helices.

Such wavy helices are defined by five parameters (R_0 , λ , α , k , A) (see [Materials and methods](#)). In the whole following, the values of the mean helix radius R_0 and pitch $2\pi\lambda$ are fixed to 30 and 37.7 (arbitrary units), respectively. Sets of wavy helices have been generated by varying α , k and A by unit steps in the following ranges: $k \in [0-16]$; $\alpha \in [0-10]$; $A \in [1,8]$, with a constant sampling $\Delta t = \pi/256$. For each model vessel corresponding to a particular combination of k , α , and A , the same six parameters have been computed.

It is first noteworthy that neither DFM nor ICM are scale invariant: for a given amplitude and frequency of the oscillations superimposed to the circular helix, their value depends on the helix angular extension A (Figs. 2 and 3). The strong variations of DFM with the helix angular extension (Fig. 2) are consistent with the influence of segment recurrence, a known drawback of this widely-used tortuosity index. Some authors ([Bullitt et al., 2003](#)) proposed the ICM index to overcome this difficulty. However, while the ICM by unit length is almost independent on the oscillation amplitude, it is still highly dependent on the helix angular extension and on the oscillation frequency (Fig. 3): ICM thus remains highly scale dependent.

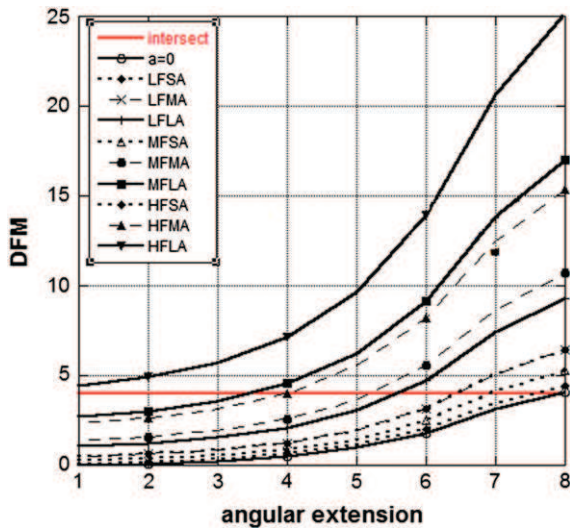


Fig. 2. DFM's variations as a function of the helix angular extension (A) for 10 different cases of tortuosities in wavy helices: completely smooth circular helices with no oscillations ($\alpha = 0$), with small (SA, $\alpha = 2$), medium (MA, $\alpha = 6$) and large (LA, $\alpha = 10$) amplitude, and with low (LF, $k = 4$), medium (MF, $k = 8$) and high (HF, $k = 12$) frequency oscillations superimposed. The non-constant and non-linear behavior of DFM with angular extension is noteworthy (note that the HFSA and LFMA curves are practically superimposed). The red horizontal line indicates a constant DFM value of 4. This line intersects nearly all the curves, indicating that this particular DFM value can be associated to nearly all tortuosity cases.

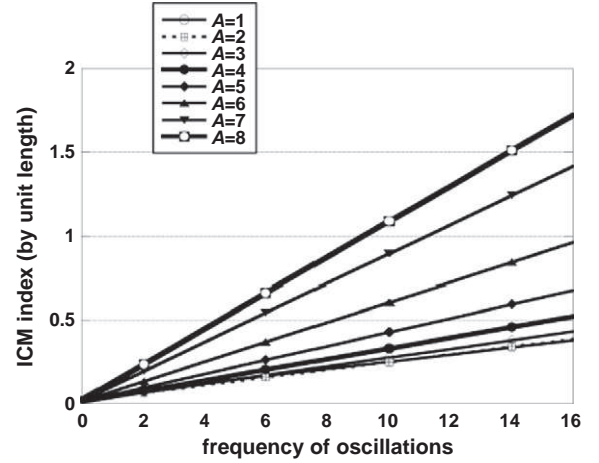


Fig. 3. ICM index normalized by path length as a function of the frequency of the superimposed oscillations (k) in wavy helices. The normalized ICM can be calculated ana-

lytically as $\frac{kA}{D_{ex}} + 1$, where D_{ex} denotes the linear distance between the wavy helix end-points. It is straightforward to demonstrate that D_{ex} is independent on the oscillation amplitude α for even values of k , when A is an integer. For other cases, the normalized ICM is almost independent on α .

By contrast, K_m , SOAM, K_{sd} and K_{rms} are scale invariant. As suggested by [Grisan et al. \(2008\)](#), a relevant index of tortuosity would behave monotonically as a function of the oscillation amplitude and frequency, i.e. it should increase i) with the frequency for a given amplitude and ii) with the amplitude for a given frequency. Condition i) is fulfilled by the four scale invariant indexes (K_m , SOAM, K_{sd} and K_{rms}), but not condition ii), see Fig. 4a–b, where the dashed lines correspond to the zeros of the partial derivatives of each index with respect to the amplitude. Each line delineates two areas: under the line, the corresponding shape parameter increases monotonically; above the line it decreases. Within the lower left area, the shape factor fulfills condition ii) whatever the amplitude and the frequency. Within the upper right area, this condition is not met. Excepting at very low frequencies ($k < 3$), the mean curvature (K_m) does not vary in a monotonic fashion with the amplitude. The mean curvature indeed decreases – even steeply – for nearly half the range of amplitudes and frequencies considered here, while the vessel is more tortuous. By contrast, the standard deviation of curvature K_{sd} increases monotonically with amplitude even for relatively high frequencies ($k \leq 10$). Only for a very small upper part of the amplitude–frequency domain, this index decreases very moderately while the vessel tortuosity actually increases. The root mean square curvature, which is the root of the sum of the squares of K_m and K_{sd} , behaves intermediately, with a monotonic increase at low to moderate frequencies ($k \leq 7$) and a moderate decrease at higher frequencies for amplitudes greater than a value which itself decreases with frequency (data not shown).

Of course, these indexes are sensitive to noise (Fig. 5): the superimposition of random, artificial noise on to model vessels induces estimation errors for both K_m and K_{sd} which naturally decrease as the S/N ratio increases but also as the oscillations amplitude (α) increases. However, the influence of the oscillation frequency (k) on the noise-induced estimation errors depends on the considered index. Regarding the mean curvature K_m , the estimation errors are always positive and decrease exponentially with k from a maximal value at zero frequency to very negligible values (< 0.004) at the highest frequencies. The maximal value of the error strongly decreases from 0.2 to 0.02 (i.e. a tenfold decrease) when the signal-to-noise ratio increases from 6 to 12 dB. Regarding the curvature standard deviation K_{sd} , the estimation errors also decrease with k at very low frequencies but become negative for low ($k = 2$) to moderate ($k = 6$) frequencies depending on the oscillation

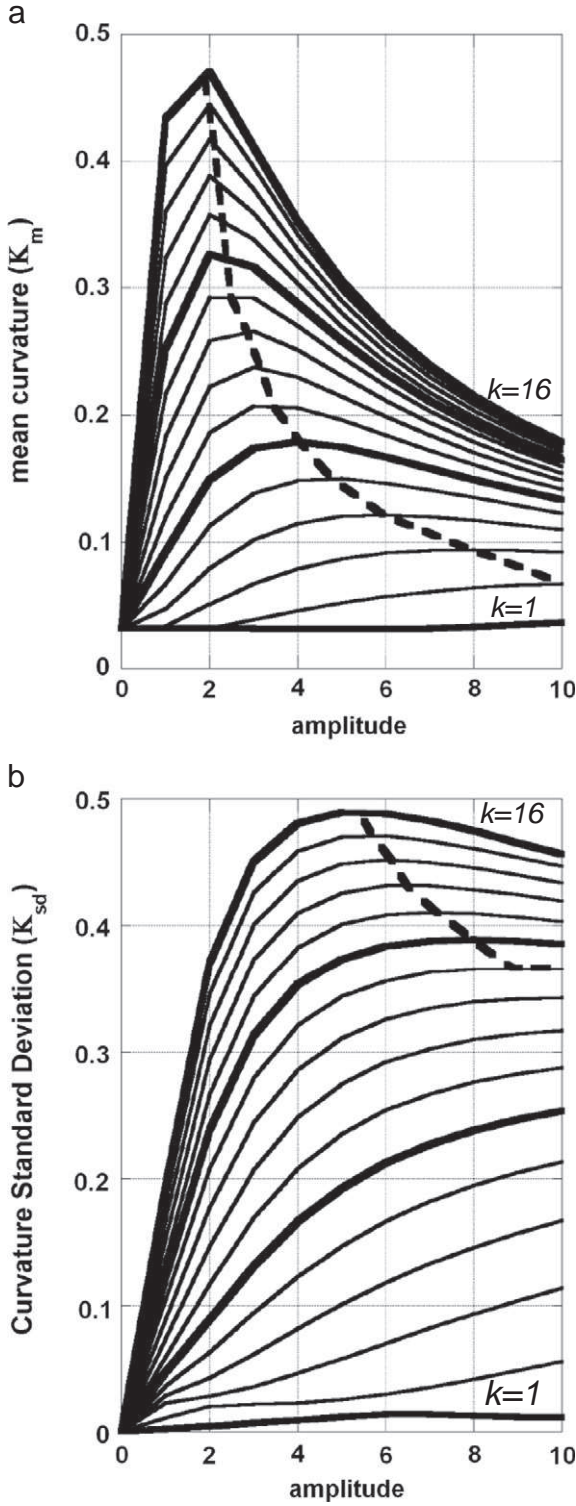


Fig. 4. Mean curvature (a) curvature standard deviation (b) in wavy helices as a function of the amplitude of superimposed oscillations, for $k \in [1-16]$.

amplitude. At higher frequencies, K_{sd} computed from the noisy vessels systematically underestimates the real value, but the absolute values of the estimation errors progressively decrease towards very negligible values (<0.005) for the highest frequencies. The relative errors vary in the same way decreasing to zero at high frequencies. Regarding K_{sd} , their absolute values typically remain smaller than 10% over a large range of parameters, except at very low frequencies, i.e. $k < 2$ for high

S/N ratios, and reaching $k < 6$ for low S/N ratios. By comparisons, the range of parameters for which the K_m relative errors remains smaller than 10% is reduced, i.e. $k < 4$ for high S/N ratios, and reaching $k < 9$ for low S/N ratios.

In the light of these tests, the standard deviation of curvature (K_{sd}) can be considered as a robust measure of tortuosity. Its mean (K_m) is much less robust for assessing vessel tortuosity. In particular, for model vessels of given amplitude, K_m increases with K_{sd} but at decreasing rate (Fig. 6a, plain lines). Moreover, for model vessels of given frequency, it exhibit a non-monotonic behavior, with an initial increase and a subsequent decrease over a large range of K_{sd} values (Fig. 6a, dashed lines). The mean curvature (K_m) is nevertheless scale invariant and is useful in order to assess the global curvature of a segment. As expected (see ²), the SOAM index is a close approximation of the mean curvature and is linearly related to the mean curvature (SOAM $\sim 0.92 K_m + 0.002$; $R^2 \sim 0.989$) (Fig. 6b). Finally, DFM and ICM, because they are not scale invariant, should not be used as curvature nor tortuosity indexes.³

General data on extracted vascular trees

228 vascular trees were extracted from 10 mosaics (covering a surface of approximately 1.5 cm^2 and encompassing a cerebral tissue volume of 28.6 mm^3). They were divided into 152 arterial and 76 venous trees according to their morphological features. These trees were segmented in 17,976 segments, i.e. vessel sections connecting two successive bifurcations, including 10,365 arterial and 7611 venous segments. The total number of orders between a postcapillary venule or a precapillary arteriole and its pial origin in the sulcus, according to the diameter-defined Strahler taxonomy, ranged from 3 to 5. The corresponding number of vessel elements was 13,196, including 7604 arterial and 5592 venous elements.

Statistical distributions of vessel attributes. Correlations

As demonstrated above by using wavy helices, the mean (K_m) and standard deviation (K_{sd}) of curvature can be considered as measures of global curvature and tortuosity, respectively. These parameters have been computed for the 17,976 vascular intra-cortical segments considered in the present study, as well as the root mean square curvature K_{rms} . In addition, the length-to-diameter ratio (LDR), the DFM, the sum of angles SOAM and the normalized ICM have also been computed. Since these vessel attributes are either scale invariant or are the ratios of lengths (as DFM) or of length to diameters, their values remain independent of shrinkage.

Their main statistical parameters are displayed in Table 1. The mean and median values of K_m and K_{sd} are close to $0.15 \mu\text{m}^{-1}$ and $0.09 \mu\text{m}^{-1}$, respectively, while DFM has a median of 1.135.

These values mirror the values taken by these parameters for a model vessel (wavy helix) with low amplitude ($\alpha = 2$) and moderate frequency ($k = 6$) of the superimposed oscillations. Clearly, the real vessels are much less regular and their shape variations have much more complex frequency contents, but nevertheless this is an interesting observation. In particular, while around these values, K_m increases with both α and k (and thus with K_{sd}), it rapidly saturates and decreases for moderate increases of the oscillation amplitude (Figs. 4a and 6a), i.e. in the physiologic range.

The mean and standard deviation of curvature can be considered as normally distributed (mean \sim median, small skewness and excess). Their histograms are well fitted ($R^2 = 0.979$ and 0.978 , respectively)

³ Note that, while other parameters have been considered, such as the mean length of subsegments between successive inflection points, it has not been possible, by combining these parameters, to derive other indexes with a dominant dependence on the helix angular extension A , the oscillation frequency k or amplitude α .

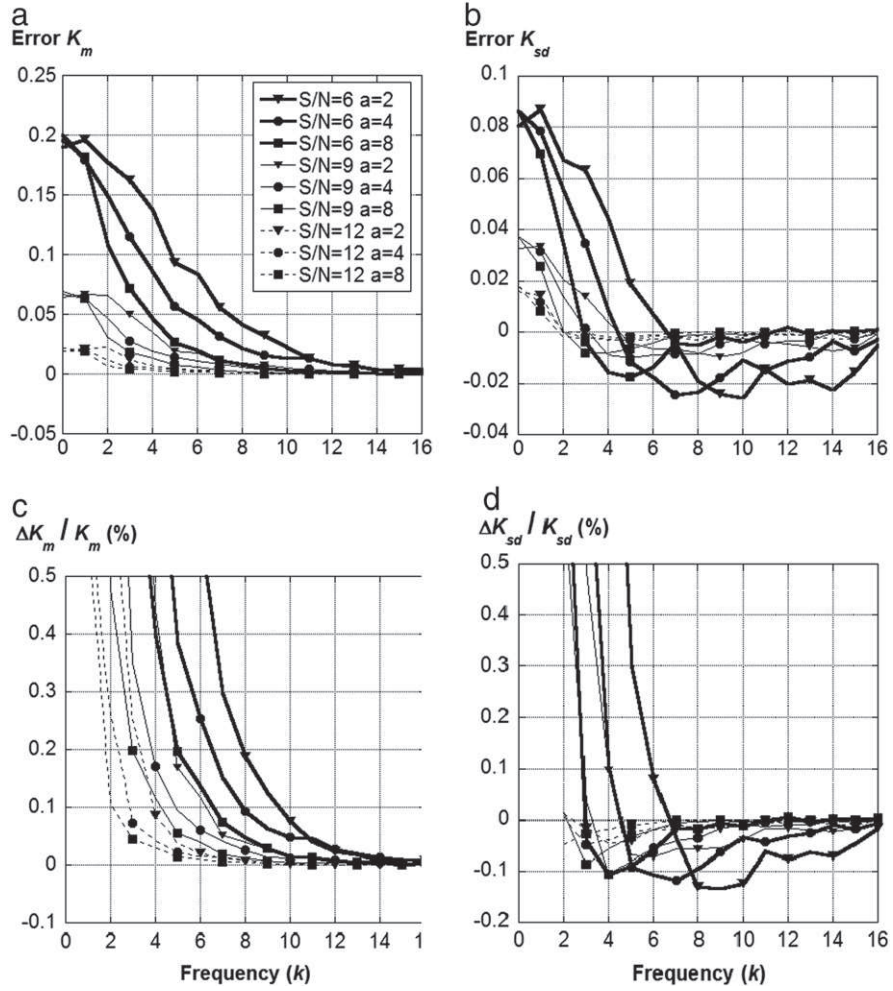


Fig. 5. Influence of noise on K_m and K_{sd} as a function of the frequency of superimposed oscillations in wavy helices.

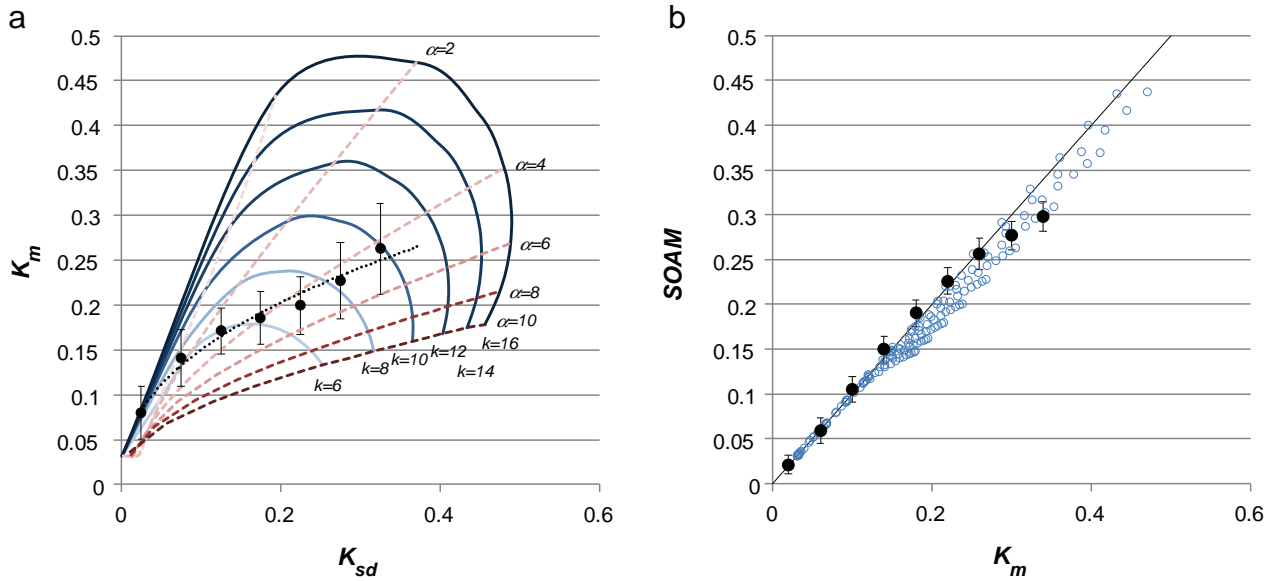


Fig. 6. Comparison of various possible tortuosity measures in wavy helices and in cortical vessels (filled circles) (a) Mean curvature as a function of curvature standard deviation. Plain lines: iso-frequency of the superimposed oscillation in wavy helices; Dashed lines: iso-amplitude of the superimposed oscillation; Black circles: Mean \pm SD of K_m values corresponding to cortical vessels with K_{sd} in $0.05 \mu\text{m}^{-1}$ intervals centered around the corresponding circles; Dashed line: best adjustment to a power law ($K_m = 0.41K_{sd}^{0.43}$, $R^2 = 0.98$). (b): Correlation between SOAM and mean curvature. Open symbols: wavy helices; Black circles: Mean \pm SD of SOAM values corresponding to cortical vessels with K_m in $0.05 \mu\text{m}^{-1}$ intervals centered around the corresponding circles. Plain line: Identity line.

Table 1

Main statistics (mean, median and standard deviation) of various vessel attributes (LDR, curvature (K_m , SOAM), tortuosity (K_{sd} , K_{rms} and DFM) in 17,976 cortical vessels (10,365 arterioles and 7611 venules).

Stats	LDR	K_m (μm^{-1})	SOAM (μm^{-1})	K_{sd} (μm^{-1})	K_{rms} (μm^{-1})	DFM
Mean	10.37	0.149	0.163	0.093	0.188	1.234
Median	7.46	0.153	0.168	0.094	0.191	1.135
SD	9.41	0.036	0.045	0.026	0.052	0.351

by Gaussian distributions with mean equal to 0.155 and 0.095 and variance equal to 0.0454^2 and 0.028^2 , respectively, with a small asymmetry towards the low values. By contrast, the histogram of the relative vessel lengthening (DFM) is best fitted ($R^2 = 0.988$) by a lognormal distribution with mean and variance equal to -2.65 and 1.12^2 , respectively. The histogram of the logarithm of the LDR is almost perfectly fitted ($R^2 > 0.99$) by a Gaussian curve centered on a value of 2.04 (corresponding to a LDR median value of 7.69) with a standard deviation of 1.31.

The standard deviation of curvature and its mean are not independent parameters. For the considered vessel population, $K_m = 0.41K_{sd}^{0.43}$ ($R^2 = 0.98$), see Fig. 6a (black circles and dotted line), i.e. a significant deviation to linearity, where K_m increases with K_{sd} but at decreasing rate. This highlights the loss of robustness of K_m as a tortuosity index for the most tortuous vessels, which correspond to wavy helices of low to medium amplitude ($\alpha \sim 4$) and medium to high frequency ($k \sim 10$) of the superimposed oscillations. In these vessels, SOAM, while remaining linearly related to K_m , also slightly begins to underestimate the mean curvature (Fig. 6b). By contrast, the DFM is very weakly correlated with either K_m or K_{sd} ($R^2 = 0.17$ and 0.25 , respectively). A particular value of DFM can be virtually associated with any value of K_m and K_{sd} , except for values of DFM very close to unity, which would yield very low values of mean and standard deviation of curvature, or for very high values of the DFM, which are generally associated with high values of K_m and K_{sd} . Overall, this confirms that DFM does neither provide an adequate estimation of the curvature nor the tortuosity.

As the standard deviation of curvature provides a simple and robust scalar index of tortuosity for each vascular segment, the statistical distribution of curvature along each vessel was further analyzed. Fig. 7 displays the mean histogram obtained for the 17,976 segments analyzed. The curvature at any point of a given vascular segment is distributed according to a lognormal law with mean and variance equal to -1.962 and 0.648 , respectively (75% of the vessels have a curvature $< 0.2 \mu\text{m}^{-1}$, 90% of the vessels have a curvature $< 0.3 \mu\text{m}^{-1}$, 5% of the vessels have a curvature $> 1/3 \mu\text{m}^{-1}$ (curvature radius $< 3 \mu\text{m}$)).

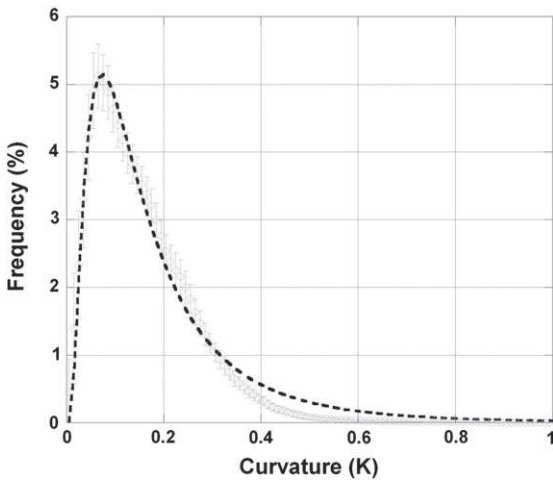


Fig. 7. Mean curvature histogram obtained for 17,976 cortical vessels. This histogram represents the mean \pm standard deviation of the frequencies corresponding to each curvature bins in the individual histograms of each segments.

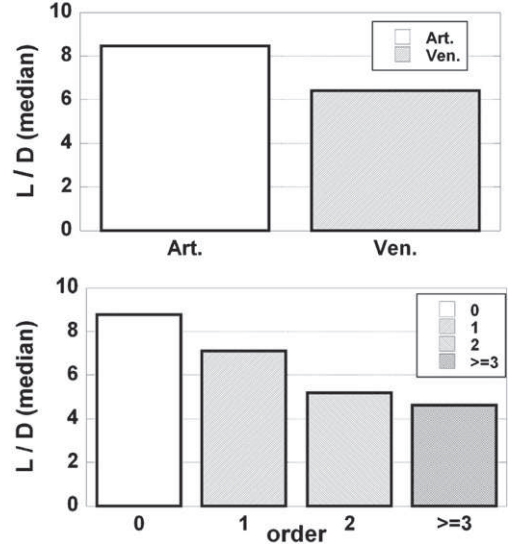


Fig. 8. Median of the length-to-diameter ratio as a function of type and hierarchical position for 17,976 cortical vessels.

Variations of vessel attributes with the nature and topological order of vascular segments

In the previous subsections we described the global statistics of 6 vessels attributes (LDR, K_m , SOAM, K_{sd} , K_{rms} , DFM). In the present section, we investigate how these attributes depend on the type – arteriole or venule – and on the hierarchical location of the vessel in the vascular tree, as defined by its order in the diameter-defined Strahler classification.

The simplest of these shape factors, the LDR, displays marked differences both according to the type and location of the segments (Fig. 8). The arterioles have a median LDR more than 30% higher, and very significantly so ($P < 0.001$), than that of the venules (i.e. 8.46 vs. 6.42). The differences between the LDR median values are even more marked as a function of the vessel order: the median LDR of the 0-order (terminal) segments (8.77) is almost twice that of higher order (≥ 3) segments (4.6). The logarithm of the LDR decreases linearly ($\log(\text{LDR}) = 0.9397 - 0.0971 N$; $R^2 = 0.98$), consistent with the fractal nature of these tree-like vessels (Cassot et al., 2006; Lorthois and Cassot, 2010). However, the slope of this linear decrease cannot be deduced from Horton's laws, which indeed relate the logarithm of the element lengths and diameters versus order (Cassot et al., 2006), while result presented here is for vessel segments. When considering vessel elements, the logarithm of the LDR increases linearly ($\log(\text{LDR}_{\text{elements}}) = 0.194 N + 0.911$; $R^2 = 0.864$). Slope and intercept are consistent with slope (0.208) and intercept (1.039) deduced from Horton's laws ($\log(L_{\text{elements}}) = 0.127 N + 0.936$ and $\log(D_{\text{elements}}) = 0.335 N + 1.975$, unpublished data for the same population). With regards to vessel elements, the difference between arteries and veins, while slightly smaller ($\sim 25\%$), is still highly significant ($P < 0.001$).

There is no significant difference between the mean values of K_m and K_{sd} for the arteriolar and venular groups (t probability = 0.053 and 0.13, respectively). However, the mean value of DFM for the arteriolar group (1.25) is slightly but significantly (t probability < 0.001) higher than for the venular group (1.22). Moreover, the considered vessel attributes decrease as the segment order increases (Fig. 9): the vessels get more curved and tortuous as they get closer to the capillary network. The distribution of probability of the curvature – $\Pr(\kappa < K)$ – along a given segment varies in the same way as its order (Fig. 10): for instance, the probability that a point has a curvature less than $0.1 \mu\text{m}^{-1}$ – $\Pr(\kappa < 0.1)$ – varies from 0.38 (segment of order 0 or 1) to more than 1/2 (0.57) (segment of order 4), with intermediate values of 0.41 and 0.48 for segments of order 2 and 3.

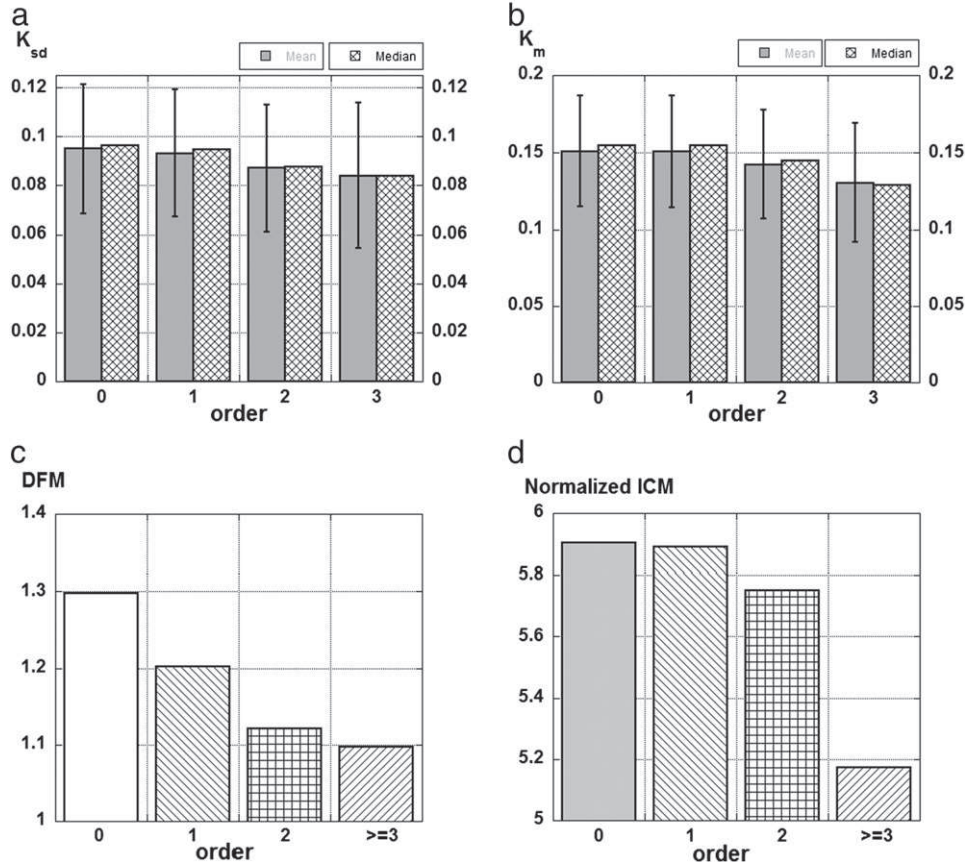


Fig. 9. Influence of hierarchical position of vessels on their vessel attributes for 17,976 cortical vessels. (a) K_{sd} mean \pm standard deviation and median; (b) K_m mean \pm standard deviation and median; (c) DFM median; and (d) normalized ICM median.

Discussion

Abnormal vessel attributes, especially vascular tortuosity, have demonstrable importance in the diagnosis of many diseases, such as cancer and retinopathies. Paradoxically, until now, tortuosity has not received a formal and unambiguous clinical definition. In this context, the objectives of the present study were:

- to propose a new and more robust definition and methodology for the estimation of vessel attributes, in particular tortuosity, and to test this methodology on model vessels,

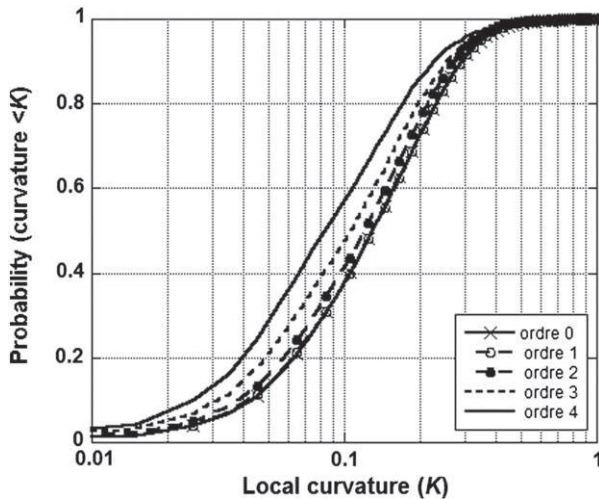


Fig. 10. Mean cumulative histogram of local curvature for vessels of given order.

- to apply this methodology to a large microvascular database of the human cerebral cortex in order to obtain the statistical data needed as reference or rationale for further assessment of vessel attributes under pathological conditions for the purpose of clinical diagnosis.

The methodology proposed was based on a two-step procedure, including:

- a smoothing/resampling step designed both to normalize the lineset obtained through the skeletonization process and to resample the data points at equally spaced curvilinear abscissa, using a cubic spline interpolation algorithm,
- the computation of the three-dimensional geometrical characteristics of a vessel, solidly grounded on the classical formulation of differential geometry and robust numerical derivation techniques.

With respect to some recent work with similar objectives, the methodology proposed here differs in significant ways:

- the resampled vessels go through the smoothed original data points, a condition which is not always fulfilled either by the polynomial curve-fitting method (O'Flynn et al., 2007) nor by the interpolation method (Johnson and Dougherty, 2007) used in previous works. This is a necessary condition to avoid uncontrolled, significant divergences from the real data,
- the methodology is based on the direct computation of the curvilinear abscissa, without any parameterization. This allows a straightforward derivation of the unit tangent vector components and, in consequence, a better accuracy of the numerical method based on simpler analytical formulas,
- in this study, we have not considered measurements of torsion as proposed by O'Flynn et al. (2007). The calculation of torsion would require the numerical computation of the third derivatives of the

vertex coordinates. This would certainly be much more sensitive to noise than the computation of lower order derivatives necessary to estimate the parameters considered here. While the impact of noise on the indexes proposed in this paper has been shown to be small even at low S/N ratio, this would not remain the case when estimating the torsion from currently available vascular imaging techniques.

However the most significant methodological advance in this study concerns the definition of a reliable tortuosity index satisfying: i) scale invariance and ii) positive monotonic response with respect to the amplitude and frequency of vessel oscillations (in other words, “the more bends that occur along the length of a vessel, and the greater their amplitudes, the larger the tortuosity index should be” (Johnson and Dougherty, 2007)). We performed numerous tests on a large body of vessel models, from those with regular but recurrent curves (low frequency and amplitudes, large value of total path length) to those which were more sinuous in nature, generated using simple analytical parameters. These tests allowed to assess method reliability and accuracy, and demonstrated that the standard deviation of the curvature best satisfied the above criteria over a broad range of vessel models. On the contrary, the measure of mean curvature, which is scale invariant, satisfies monotonic variation only at low amplitudes or low frequency (or both) and the measure of root mean square curvature displays paradoxical variations at moderate or high frequencies. The SOAM index is actually an approximation of the mean curvature and so does not satisfy the second criterion given here. The DFM and ICM indexes are highly scale dependent and this scale dependence still remains after normalization by the vessel length, which reduces their utility as tortuosity indexes.

We therefore propose the measure of the standard deviation of the curvature (K_{sd}) as a new and reliable index of tortuosity. Note that, using this new methodology and the index of tortuosity, the mean curvature (K_m) and the curvature root mean square (K_{rms}) can be obtained simultaneously without significant extra computational cost.

The computation of these vessel attributes on a large vascular database of the human cerebral cortex allowed the establishment of reference morphometric data and the characterization of their statistical distributions. To our knowledge, this has never been done before, and certainly not with regard to such a large database, for any organ, human or otherwise. The most important findings of this part of our study are:

- Mean, standard deviation and root mean square of the curvature are normally distributed around values which, by comparison with vessel models, would correspond to low amplitude ($\alpha \sim 2$) and moderate frequency oscillations ($k \sim 6$). They display relatively high coefficients of variation (from 25% to 40% approximately) highlighting a marked intervascular heterogeneity, with a twofold increase in both amplitude and frequency for the most tortuous vessels. This heterogeneity may be due to the multi-frequency components of the vessel curvature, and comparison with vessel models should be made with caution. The distributions of the length-to-diameter ratio (LDR) and of the relative lengthening (DFM) are lognormal. These findings are coherent with the lognormal distribution of vessel length (Lauwers et al., 2008).
- DFM is very weakly correlated with K_m and K_{sd} , indicating that a particular value of this index can be associated with nearly any value of mean curvature or tortuosity. This confirms that this simple measurement can reliably assess neither curvature nor tortuosity. Thus, the large body of literature where DFM is considered as a tortuosity index should be interpreted with caution.
- Arterioles have a higher median LDR than venules, but the two kinds of vessels have the same mean curvature and tortuosity.
- Length-to-diameter ratio decreases very significantly and markedly with vessel order, the LDR logarithm following a linear relationship with vessel order consistent with the fractal nature of the tree-like vessels of the cerebral cortex.

- While clinical papers based on the assessment of the LDR often consider separately arteriolar and venous vessels, the hierarchical position of the vessels in the vascular tree should also be considered in a perspective of diagnosis and/or staging,
- The lower the order of the vessels, i.e. the nearer to the capillary network, the more curved and tortuous the vessels are. The analysis of the probability distribution of the curvature along a given vessel confirms this finding, showing that the probability that the curvature at a given vessel point is less than a prescribed value increases with the order of the vessel. This is consistent with the predictions of a theoretical model of vascular morphogenesis highlighting the influence of mechanical forces induced by blood flow and tissue growth during development, which lead to straighter and longer proximal vessels (Nguyen et al., 2006). Thus, it is likely to be the consequence of ubiquitous physical constraints and to hold in other organs, especially in the retina, the vasculature of which is known to share similar anatomic, physiological, and embryological characteristics to the cerebral vessels (Baker et al., 2008; Patton et al., 2005).

Many recent researches have shown that changes of the vessel tortuosity, for instance, might be an early “marker” of tumor malignancy. Vessel “normalization” (Jain, 2005), in particular a marked reduction of their tortuosity might permit analysis of the efficacy of cancer therapy. In this context, the analysis of various vessel attributes performed on vessel models has highlighted the drawbacks of empirical methods currently used, especially for highly tortuous vessels, and has validated a new and robust tortuosity index. The superiority of this new index compared to previous ones must be confirmed in studies focused on tumor vessels, the tortuosity of which is likely to be greater than the one of the most tortuous healthy vessels in the present study, for which a loss of robustness of previous tortuosity indexes has been demonstrated.

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