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## Enhanced refrigerant capacity in Gd-Al-Co microwires with a biphasic nanocrystalline/amorphous structure

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A class of biphasic nanocrystalline/amorphous  $\text{Gd}_{(50+5x)}\text{Al}_{(30-5x)}\text{Co}_{20}$  ( $x=0, 1, 2$ ) microwires fabricated directly by melt-extraction is reported. High resolution transmission electron microscopy and Fourier function transform based analysis indicate the presence of a volume fraction ( $\sim 20\%$ ) of  $\sim 10$  nm sized nanocrystallinities uniformly embedded in an amorphous matrix. The microwires possess excellent magnetocaloric properties, with large values of the isothermal entropy change ( $-\Delta S_M \sim 9.7 \text{ J kg}^{-1} \text{ K}^{-1}$ ), the adiabatic temperature change ( $\Delta T_{\text{ad}} \sim 5.2 \text{ K}$ ), and the refrigerant capacity ( $RC \sim 654 \text{ J kg}^{-1}$ ) for a field change of 5 T. The addition of Gd significantly alters  $T_C$  while preserving large values of the  $\Delta S_M$  and  $RC$ . The nanocrystallinities allow for enhanced  $RC$  as well as a broader operating temperature span of a magnetic bed for energy-efficient magnetic refrigeration.

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Magnetic refrigeration based on the magnetocaloric effect (MCE) of a magnetic solid material is a very promising technology due to its high cooling efficiency, lower energy costs, and environmental affability as compared to conventional gas compression-based refrigeration technology.<sup>1-4</sup> Currently, there is a large amount of research focusing on exploiting magnetic materials with large isothermal magnetic entropy change ( $\Delta S_M$ ) over a broad temperature range, namely, those exhibiting a large refrigerant capacity ( $RC$ ).<sup>3,4</sup>  $RC$  measures the amount of heat that can be transferred between the hot and cold sinks by the magnetic refrigerant in an ideal thermodynamic cycle. The working temperature span of a magnetic refrigerant is given by the temperature difference between  $T_{\text{hot}}$  and  $T_{\text{cold}}$  that defines the full-width at half-maximum (FWHM) of the  $\Delta S_M(T)$  curve, i.e.,  $\delta T_{\text{FWHM}} = T_{\text{hot}} - T_{\text{cold}}$ . A variety of approaches for achieving an increase in  $RC$ , such as successive magnetic transitions,<sup>5,6</sup> magnetic field sensitive magnetic phase transitions,<sup>7</sup> and multiple magnetic phase composites,<sup>8,9</sup> have been proposed.

Recently, there has been a growing interest in wire-shaped magnetocaloric materials.<sup>10-17</sup> As compared with their bulk counterparts, the wires with increased surface-to-volume areas allow for a higher heat transfer between the magnetic refrigerant and surrounding liquid. Theoretical studies have revealed that a magnetic bed composed of magnetocaloric wires will yield an optimal device performance.<sup>18,19</sup> In particular, Kuz'min has shown that shaping magnetic refrigerants in the form of spherical or irregular

particles is inefficient because of their high energy losses on viscous resistance and demagnetization.<sup>18</sup> Mechanical instability of the refrigerant can result in a significant loss of throughput due to maldistribution of flow. In a detailed analysis, Vuarnoz and Kawanami have theoretically shown that as compared to a magnetic bed made of Gd particles, a bed consisting of Gd wires yields a greater temperature span between its ends, which, in effect, results in a higher cooling efficiency.<sup>19</sup> In this context, our experimental efforts in the development of amorphous melt-extracted Gd-alloy microwires with enhanced  $RC$  represent an important task.<sup>11,13,14,16,20</sup> As compared to bulk metallic glass (BMG) and ribbon counterparts, the microwires exhibit larger values of  $\Delta S_M$  and  $RC$  along with their improved mechanical strength. This is due to their shape and inter-wire interaction effects.<sup>11,13</sup> We have shown that the presence of structural disorder significantly broadens the paramagnetic to ferromagnetic (PM-FM) transition and  $\Delta S_M(T)$  without significantly altering the nature of the second-order magnetic transition (SOMT) and long-range ferromagnetic order.<sup>20</sup> It is the large magnetic moment of Gd and the presence of the long-range ferromagnetic order that result in the large  $\Delta S_M$  along with the broadening of the PM-FM transition that contributes to the large  $RC$  in the amorphous melt-extracted Gd-alloy microwires. It has recently been reported that the partial nanocrystallizing of an amorphous magnetic material via an appropriate heat treatment will create a biphasic nanocrystalline/amorphous structure which significantly improves the  $RC$  relative to its amorphous counterpart.<sup>21</sup> This finding has motivated us to exploit Gd-alloy microwires with a biphasic nanocrystalline/amorphous structure in order to improve  $RC$ .

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In this letter, we report upon an enhanced  $RC$  in biphase nanocrystalline/amorphous microwires of  $\text{Gd}_{(50+5x)}\text{Al}_{(30-5x)}\text{Co}_{20}$  ( $x = 0, 1, 2$ ), which have been directly fabricated by the melt-extraction technique. The  $RC$  values of the microwires are greater than those of their BMGs and Gd-Al-Co-based ribbons.<sup>22–28</sup> Using these wires, we have proposed a design of a magnetic bed with enhanced  $RC$  and  $\delta T_{\text{FWHM}}$ . Our study paves a pathway for the development of biphase microwires with desirable magnetocaloric properties for active magnetic refrigeration in Micro Electro Mechanical Systems (MEMS) and Nano Electro Mechanical Systems (NEMS).

$\text{Gd}_{(50+5x)}\text{Al}_{(30-5x)}\text{Co}_{20}$  ( $x = 0, 1, 2$ ) microwires with a biphase nanocrystalline/amorphous structure were created directly by adjusting the melt-extraction parameters, details of which have been reported elsewhere.<sup>13</sup> A field-emission scanning electron microscope (SEM-Helios Nanolab600i) at 20 kV was used to observe the micromorphology. X-ray diffraction (XRD, D/max-rb with Cu K $\alpha$  radiation) was used to examine the phase structure of the microwires. A transmission electron microscope (TEM, Tecnai G2 F30) and a high resolution TEM (HRTEM) were used to take images of the microwires. Selected area electron diffraction (SAED) was also used to analyze the wires. Magnetic measurements were performed using a Magnetic Property Measurement System (MPMS) from Quantum Design. The wire specimens were prepared in the form of a bundle of wires (60 wires) with an average length of  $\sim 3$  mm. We placed the pre-weighed wires one by one in a sample holder with an inner diameter of 1 mm. Magnetic fields of up to 5 T were applied along the axial direction of the wires. The thermal relaxation method using the heat capacity option of a Physical Property Measurement System (PPMS) Evercool-1 platform from Quantum Design was employed to precisely measure  $C_p(T, \mu_0 H)$  as a function of temperature (2–160 K) in different fields of  $\mu_0 H = 0, 2, \text{ and } 5$  T.

Figure 1(a) shows an SEM image of the fabricated Gd-Al-Co wires, which possess smooth surfaces with an average diameter of  $\sim 30$   $\mu\text{m}$ . All the wires display the halo patterns without visible crystalline peaks within the XRD instrument limitation (Fig. 1(b)). However, the TEM and SAED for the  $x = 2$  sample show evidence of the presence of a volume fraction ( $\sim 20\%$ ) of nanocrystallinities of  $\sim 10$  nm size embedded in an amorphous matrix. The nanocrystalline area (blue square) and the amorphous matrix (red square) were analyzed by Fourier Function Transform (FFT) and Inverse Fourier Function Transform (IFFT) method (Figs. 1(d) and 1(e)), showing slight variation in the chemical elements. The volume fractions of nanocrystallinities for the other wires were also determined to be  $\sim 20\%$  as a result of the small compositional variations and the same preparation procedure.

Figure 2 shows the temperature dependence of magnetization ( $M$ - $T$ ) for the wires measured under a field ( $\mu_0 H$ ) of 20 mT. As shown in Fig. 2(a), the  $M$ - $T$  curves exhibit a broad FM-PM transition around the Curie temperatures ( $T_C$ ). The values of  $T_C$  are determined as the minima of the  $dM/dT$  vs.  $T$  curves, as displayed in the inset of Fig. 2(a).  $T_C$  increases with Gd addition;  $T_C = 86$  K, 100 K, and 109 K for  $\text{Gd}_{50}\text{Al}_{30}\text{Co}_{20}$ ,  $\text{Gd}_{55}\text{Al}_{25}\text{Co}_{20}$ , and  $\text{Gd}_{60}\text{Al}_{20}\text{Co}_{20}$ , respectively. Hysteresis loops ( $M$ - $\mu_0 H$ ) were measured at 20 K for all the wires and indicate a soft magnetic characteristic (due to the nature of

SOMT). This is a desirable quality for active magnetic refrigeration. The saturation magnetization ( $M_S \sim 200$  A m<sup>2</sup> kg<sup>-1</sup>) is large for all the wires and increases with increasing the Gd content as expected (see Fig. 2(b)).

Isothermal magnetization ( $M$ - $\mu_0 H$ ) curves were measured in fields of up to 5 T over a wide temperature range of 20–200 K and have been used to evaluate  $\Delta S_M$  of the wire samples through the Maxwell's relationship<sup>1</sup>

$$\Delta S_M(T, \mu_0 H) = \mu_0 \int_0^{H_{\text{max}}} \left( \frac{\partial M}{\partial T} \right)_H dH, \quad (1)$$

where  $M$  is the magnetization under a magnetic field  $\mu_0 H$ , and  $S$  is the magnetic entropy at a given temperature  $T$ . Figure 3(a) shows the temperature dependence of  $\Delta S_M$  for all the wire samples for  $\mu_0 \Delta H = 2$  and 5 T. It is clear that the wires exhibit broad  $\Delta S_M(T)$  curves ( $\delta T_{\text{FWHM}}$  of  $\sim 90$  K for  $\mu_0 \Delta H = 5$  T), with the largest values of  $\Delta S_M$  obtained at their  $T_C$  temperatures. The maximum value of  $\Delta S_M$ , denoted as  $\Delta S_M^{\text{max}}$ , is almost unchanged with the addition of Gd (Fig. 3(b)). For  $\mu_0 \Delta H = 5$  T,  $-\Delta S_M^{\text{max}} \cong 10.1$  J kg<sup>-1</sup> K<sup>-1</sup> in the  $\text{Gd}_{50}\text{Al}_{30}\text{Co}_{20}$  wires, which is almost equal to that of pure Gd ( $\sim 10.2$  J kg<sup>-1</sup> K<sup>-1</sup>)<sup>4</sup> and is much larger than those of other candidates in the similar temperature range.<sup>22–28</sup>

The increased values of  $\Delta S_M^{\text{max}}$  and  $\delta T_{\text{FWHM}}$  (Fig. 3(a)) point to a large  $RC$  of the microwires. In order to confirm this, the  $RC$  of the fabricated samples has been determined using the following formula:<sup>29</sup>

$$RC = \int_{T_{\text{cold}}}^{T_{\text{hot}}} -\Delta S_M(T) dT, \quad (2)$$

where  $T_{\text{cold}}$  and  $T_{\text{hot}}$  are the onset and offset temperatures of  $\delta T_{\text{FWHM}}$ . Enlarged values of  $RC$  are obtained for all the samples (Fig. 3(b)). For  $\text{Gd}_{50}\text{Al}_{30}\text{Co}_{20}$  wires,  $RC$  has reached a large value of  $\sim 672$  J kg<sup>-1</sup> for  $\mu_0 \Delta H = 5$  T. For comparison, the  $RC$  values of the present microwires and of BMGs and Gd-Al-Co-based amorphous ribbons are plotted in Fig. 3(c).<sup>22–28</sup> The larger values of  $RC$  in addition to their desirable geometries make the microwires more attractive for applications in magnetic refrigeration. A theoretical study of Franco *et al.* has shown an enhancement of  $RC$  in biphase magnetic systems as a result of magnetic interactions between the phases.<sup>30</sup> In case of our biphase microwires, magnetic coupling between the nanocrystalline and amorphous phases could result in the broadened SOMTs (Fig. 2(a)) and hence the enhanced  $RC$  values (Fig. 3(b)).

Due to the lack of specific heat  $C_p(T, \mu_0 H)$  measurements on wire-shaped samples, no information on the adiabatic temperature change ( $\Delta T_{\text{ad}}$ ) of Gd-based microwires has been reported in previous reports.<sup>11,13,14,16,20</sup> The inset of Fig. 3(d) shows the  $C_p(T, \mu_0 H)$  curves of  $\text{Gd}_{55}\text{Al}_{25}\text{Co}_{20}$  wires for  $\mu_0 H = 0$  and 5 T. The  $C_p(T, \mu_0 H)$  curves exhibit the peaks around the  $T_C$ , and their  $\lambda$ -like shape is in accordance with the  $M$ - $H$  data, both of which reveal the SOMT nature of the wires. The  $\Delta T_{\text{ad}}$  of the wires has been calculated by<sup>31</sup>

$$\Delta T_{\text{ad}}(\Delta H, T) = [T(S)_{H_1} - T(S)_{H_0}]_S. \quad (3)$$

For  $\text{Gd}_{55}\text{Al}_{25}\text{Co}_{20}$  wires,  $\Delta T_{\text{ad}} \sim 5.2$  K at  $\mu_0 \Delta H = 5$  T at its  $T_C$  of 100 K. This value of  $\Delta T_{\text{ad}}$  is about half of pure Gd

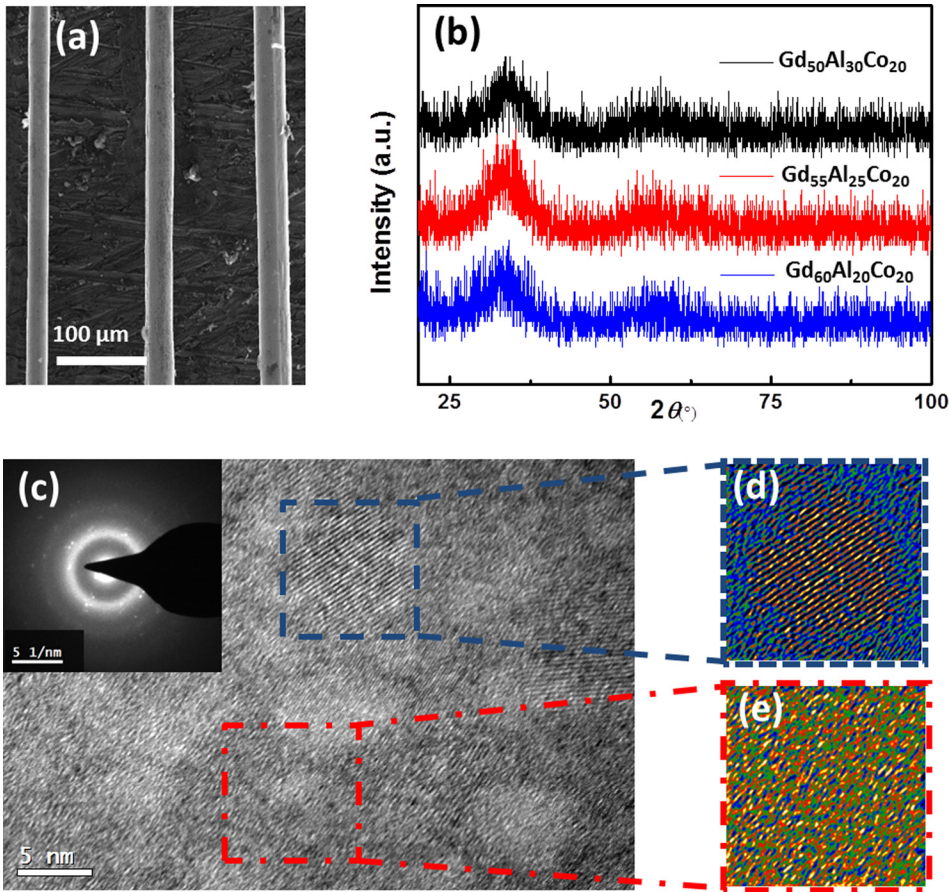


FIG. 1. (a) SEM and (b) XRD patterns of  $\text{Gd}_{(50+5x)}\text{Al}_{(30-5x)}\text{Co}_{20}$  ( $x=0, 1, 2$ ) microwires. (c) TEM and SAED (inset of c) images of the  $x=2$  sample. In (d) and (e), the corresponding Fourier transforms of the nanocrystalline regions and the amorphous matrix are shown.

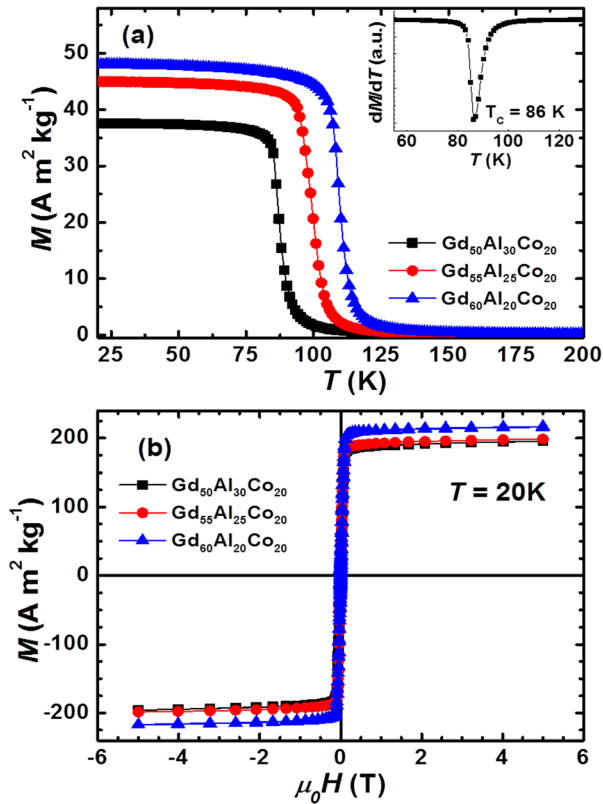


FIG. 2. (a)  $M$  vs.  $T$  curves under a field of 20 mT of  $\text{Gd}_{(50+5x)}\text{Al}_{(30-5x)}\text{Co}_{20}$  ( $x=0, 1, 2$ ) microwires. Inset of Fig. 2(a) shows the  $dM/dT$  vs.  $T$  curve of the  $x=0$  sample. (b) The hysteresis loops ( $M$ - $\mu_0H$ ) of the wires measured at 20 K.

( $\sim 11$  K at  $\mu_0\Delta H = 5$  T at  $T_C = 294$  K).<sup>32</sup> However, the  $\Delta T_{\text{ad}} \cong 1.8$  obtained at  $\mu_0\Delta H = 2$  T for  $\text{Gd}_{55}\text{Al}_{25}\text{Co}_{20}$  wires is about 8 times larger than that reported for NiMnGa glass-coated microwires ( $\Delta T_{\text{ad}} \cong 0.22$  K at  $\mu_0\Delta H = 1.8$  T at  $T_C = 320$  K). This would provide the impetus needed to develop Gd-based microwires for active magnetic refrigeration.

From an engineering perspective, a magnetic bed containing a stack of magnetocaloric wires will yield a better device performance as compared to that made of magnetocaloric particles.<sup>18,19</sup> The bundle of closely packed cylindrical wires, as illustrated in Fig. 4(a) (denoted as Specimen-1), is desirable for use in active magnetic refrigerators. This is because of their high mechanical stability and low porosity.<sup>18</sup> Considering two wires that possess similar values of  $\Delta S_M$  but different values of  $T_C$  (namely,  $\text{Gd}_{50}\text{Al}_{30}\text{Co}_{20}$  wires with  $-\Delta S_M = 10.09$  J  $\text{kg}^{-1}$   $\text{K}^{-1}$  and  $T_C = 86$  K;  $\text{Gd}_{60}\text{Al}_{20}\text{Co}_{20}$  with  $-\Delta S_M = 10.11$  J  $\text{kg}^{-1}$   $\text{K}^{-1}$  and  $T_C = 109$  K), we design an alternative magnetic bed (denoted as Specimen-2) composed of these wires that are arranged in a one-by-one fashion as illustrated in Fig. 4(b). Using the experimental MCE data of  $\text{Gd}_{50}\text{Al}_{30}\text{Co}_{20}$  and  $\text{Gd}_{60}\text{Al}_{20}\text{Co}_{20}$  (denoted as Wire A and Wire B, respectively) and considering their equal weight fractions, we have calculated the temperature dependence of  $-\Delta S_M$  for Specimen-2 following the relation:  $-\Delta S_{M(S-2)} = \alpha\Delta S_{M(A)} + \beta\Delta S_{M(B)}$ , where  $\alpha$  and  $\beta$  are the relative weight fractions of the two wires (here  $\alpha = \beta = 50\%$ ).<sup>33</sup> We have plotted in Fig. 4(c) the  $-\Delta S_M(T)$  curves for Wire A, Wire B, and Specimen-2 for  $\mu_0\Delta H = 5$  T. It can be observed that although the  $-\Delta S_M^{\text{max}}$  of Specimen-2 ( $\sim 9$  J  $\text{kg}^{-1}$   $\text{K}^{-1}$  for  $\mu_0\Delta H = 5$  T) is slightly smaller than those of both Wire A and Wire B ( $\sim 10.09$  and

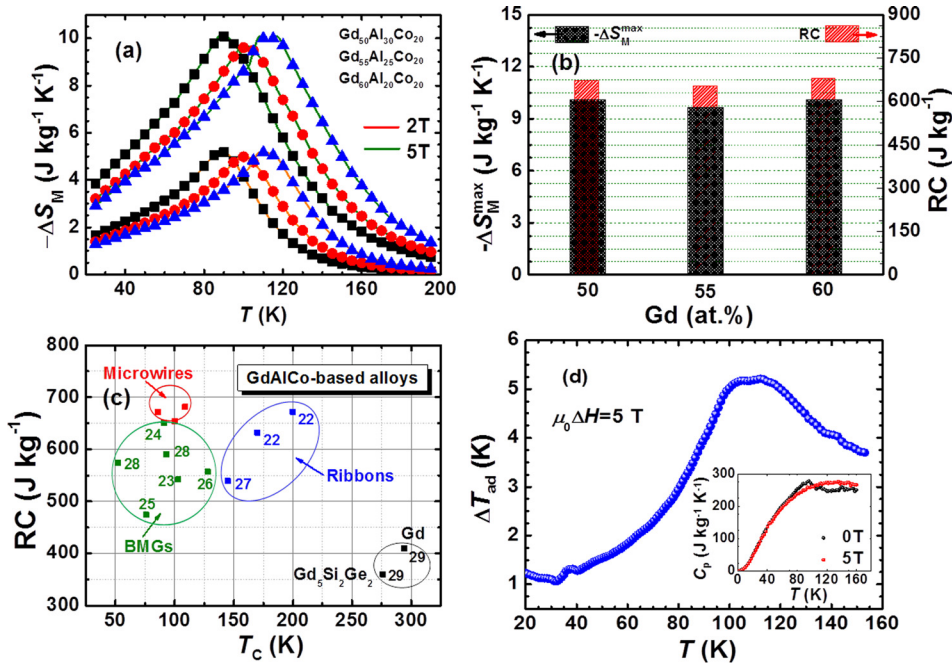


FIG. 3. (a)  $-\Delta S_M(T)$  curves of  $Gd_{(50+5x)}Al_{(30-5x)}Co_{20}$  ( $x=0, 1, 2$ ) wires for  $\mu_0\Delta H=2$  and 5 T; (b) the  $-\Delta S_M^{\max}$  values and RC values of these wires at  $\mu_0\Delta H=5$  T. (c) RC with respect to  $T_C$  of the present wires in comparison with Gd-Al-Co-based BMGs and amorphous ribbons reported in the literature. (d) Temperature dependence of the adiabatic temperature change ( $\Delta T_{ad}$ ) at  $\mu_0\Delta H=5$  T for  $Gd_{55}Al_{25}Co_{20}$  wires; the inset of (d) shows the temperature-dependent heat capacity  $C_p(T)$  measured at  $\mu_0H=0$  and 5 T.

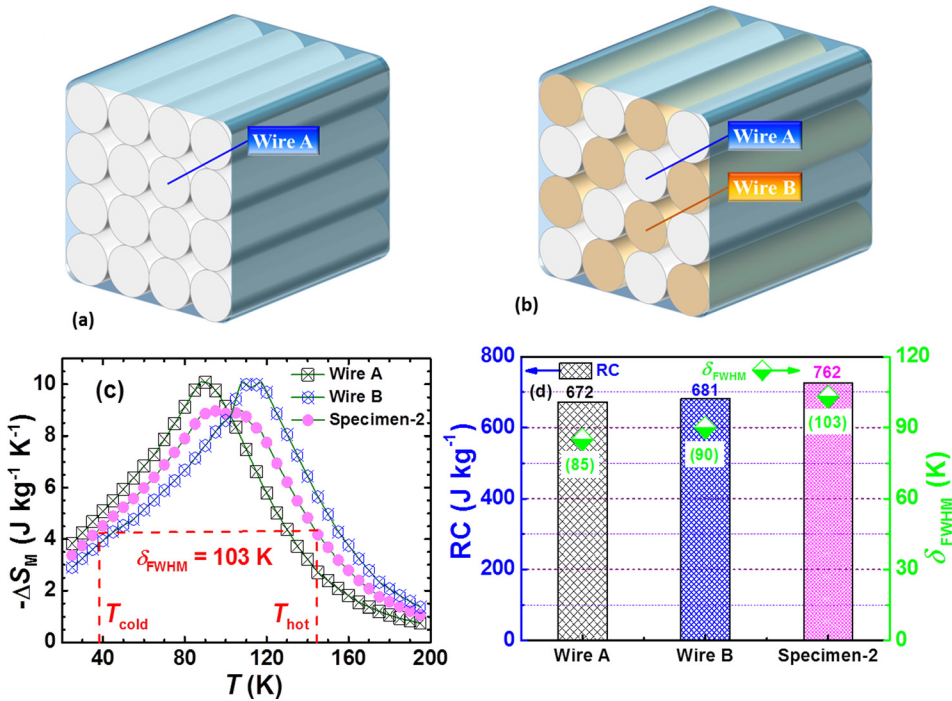


FIG. 4. (a) A magnetic regenerator bed made of closely packed cylindrical wires that have the same  $\Delta S_M$  and  $T_C$ ; (b) a magnetic regenerator bed made of closely packed cylindrical wires that have similar values of  $\Delta S_M$  but different values of  $T_C$ ; (c)  $-\Delta S_M(T)$  plots for Wire A, Wire B, and Specimen-2 for  $\mu_0\Delta H=5$  T; (d) the corresponding values of RC and  $\delta T_{FWHM}$  for the samples at  $\mu_0H=5$  T.

10.11 J kg<sup>-1</sup> K<sup>-1</sup> for  $\mu_0\Delta H=5$  T, respectively), the  $-\Delta S_M(T)$  curve is much broader for Specimen-2. The  $\delta T_{FWHM}$  of the  $-\Delta S_M(T)$  curve for Specimen-2 is  $\sim 103$  K, which is about 20% and 14% larger than those for Wire A ( $\sim 86$  K) and for Wire B ( $\sim 90$  K), respectively. As a result of this, the RC value of Specimen-2 ( $\sim 726$  J kg<sup>-1</sup>) is greater than those of Wire A ( $\sim 672$  J kg<sup>-1</sup>) and Wire B ( $\sim 681$  J kg<sup>-1</sup>). The table-like MCE shape (i.e., the relatively constant  $\Delta S_M$  with temperature) is also observed for Specimen-2, which is beneficial for Ericsson-cycle based magnetic refrigerators.<sup>1,4</sup>

In summary, we have shown the excellent magnetocaloric properties in  $Gd_{(50+5x)}Al_{(30-5x)}Co_{20}$  ( $x=0, 1, 2$ ) microwires

with a biphasic nanocrystalline/amorphous structure. We have also demonstrated an effective approach for enhancing both the RC and the operating temperature span of a magnetic bed by using wires that have similar values of the magnetic entropy change but different Curie temperatures. The present microwires are attractive candidates for their use in active magnetic refrigerators operating in the liquid nitrogen temperature range.

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