

A physically sound model for prediction of the pressure drop in small channel Taylor flow

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unit cell

 $J_{\rm G} = \frac{\dot{Q}_{\rm G}}{A} \prod_{\ell=1}^{M} \prod_{\ell=1}^{M} J_{\rm L} = \frac{\dot{Q}_{\rm L}}{A}$

U

 \sum_{a} \sum_{j} $J_a + J_a$

uc L_{uc} L_{uc}

B

*L*bubble

*L*slug *L*

1. Introduction

- \triangleright Monolithic reactors offer potential benefits for **heterogeneously catalyzed multiphase reactions** (e.g. Fischer-Tropsch synthesis)
- **Taylor flow** has advantageous mass transfer characteristics due to large specific interfacial area, thin liquid films, and good mixing in the liquid slug by recirculation
- Here a new model for the dynamic **pressure drop** (PD) along a Taylor flow unit cell is developed from DNS results

3. Pressure profiles from DNS > Pressure drop along the bubble / liquid film

 \geq Co-current downward Taylor flow in a square mini-channel [3]

4. New pressure drop model

- \triangleright Dynamic pressure drop consists of 2 parts: $\frac{\Delta P_{\text{uc}}^{\text{BW}}}{\Delta E_{\text{bulge}}} = \frac{\Delta P_{\text{slug}}^{\text{BW}}}{1 + \frac{\Delta P_{\text{bulbble}}^{\text{BW}}}{\Delta E_{\text{bulge}}}$ $P_{\rm nc}^{\rm BW}$ $\Delta P_{\rm slug}^{\rm BW}$ $\Delta P_{\rm l}$ $\frac{\Delta P_{\rm uc}^{\rm BW}}{L_{\rm uc}} = \frac{\Delta P_{\rm slug}^{\rm BW}}{L_{\rm uc}} + \frac{\Delta P_{\rm b}}{L}$
- \triangleright Pressure drop in the liquid slug

2. Pressure drop models in literature

 \triangleright Lockhart-Martinelli-Chisholm (LMC) model (does not account for σ)

$$
\frac{\Delta P_{\text{uc}}^{\text{LMC}}}{L_{\text{uc}}} = \underbrace{\frac{C_{\text{f}}}{2} \frac{\mu_{\text{L}} J_{\text{L}}}{D_{\text{h}}^2}}_{=\left(\frac{dP}{\Phi}\right)_{\text{L}}} \underbrace{\left(1 + 5\sqrt{\frac{\mu_{\text{G}}}{\mu_{\text{L}}} \frac{\beta}{1-\beta} + \frac{\mu_{\text{G}}}{\mu_{\text{L}}} \frac{\beta}{1-\beta} \right)}_{=\varphi_{\text{L}}^2 = 1 + \frac{C_{\text{Ciblabm}}}{\chi} + \frac{1}{\chi^2}}_{\frac{1}{\chi}^2} \qquad \qquad \chi^2 \equiv \underbrace{\left(\frac{dP}{\text{d}y}\right)_{\text{L}}}_{\left(\frac{dP}{\text{d}y}\right)_{\text{G}}} = \frac{\mu_{\text{L}}}{\mu_{\text{G}}} \frac{J_{\text{L}}}{J_{\text{G}}}
$$

► Kreutzer [1]: $a_{\text{exp}}=0.17$, $a_{\text{num}}=0.07$, $\delta=0$; Warnier [2]: $a_{\text{exp}}=0.1$, $\delta=D_{\text{B}}/3$

$$
\frac{\Delta P_{\text{uc}}^{\text{K/W}}}{L_{\text{uc}}} = \frac{C_{\text{f}}}{2} \frac{\mu_{\text{L}} J_{\text{total}}}{D_{\text{h}}^2} \left(\frac{L_{\text{slug}} + \delta}{L_{\text{uc}}} \right) \left(1 + a \frac{D_{h}}{L_{\text{slug}} + \delta} L a^{0.33} \right) \quad La \equiv \frac{Re_{\text{B}}}{Ca_{\text{B}}} = \frac{\sigma \rho_{\text{L}} D_{\text{h}}}{\mu_{\text{L}}^2}
$$

 \triangleright Relating the unknown bubble velocity to the given total superficial velocity

5. Conclusions \sim \triangleright The new model is in very good [Pa/m] agreement with the DNS data \triangleright It allows to estimate the unit cell pressure drop from the following six parameters: ρ_L , μ_L , σ , J_L , J_G , D_h \geq Outlook: comparison with $2x10$ $3x10$ experimental pressure drop data $(\Delta p_{\text{dw}}/L_{\text{uc}})_{\text{DNS}}$ [Pa/m]

References

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