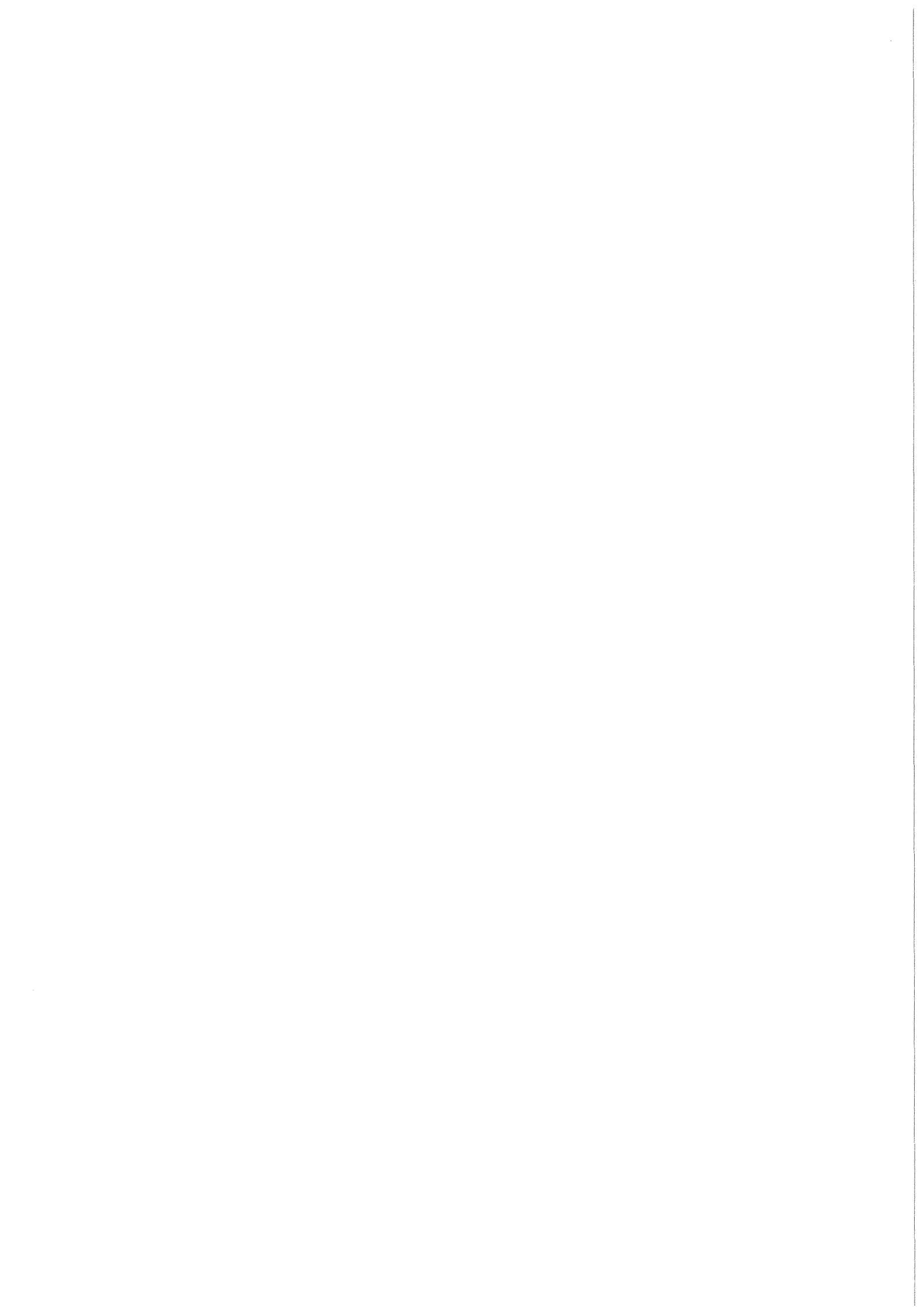


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# **HADA A FORTRAN-IV Program for the Thermohydraulic Design of an Advanced Pressurized Light Water Reactor with a Tight Fuel Rod Lattice**

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H A D A

A FORTRAN-IV Program for the Thermohydraulic Design of an  
Advanced Pressurized Light Water Reactor with a  
Tight Fuel Rod Lattice

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## Abstract

For the user of the program the input data are described in detail. Two sample runs demonstrate the usage of the program and the output. In addition to the description of the physical background given in KfK 3453, the provided and used solution algorithms are explained. In the last chapters the utility programs are described and an installation guide for the program system is listed.

H A D A

Ein FORTRAN-IV-Programm zur thermohydraulischen Auslegung von fortgeschrittenen Druckwasserreaktoren mit enger Stabteilung

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## Zusammenfassung

Es werden zunächst die Eingabedaten für die Anwendung des Programms ausführlich beschrieben. Zwei Beispiele, die mit der letzten Version gerechnet wurden, sollen die Anwendung des Programms demonstrieren und die Programmausgabe erläutern. Es folgt in Ergänzung zur Beschreibung der physikalischen Grundlagen in KfK 3453 eine kurze Erläuterung des mathematischen Lösungsverfahrens. Den Abschluß bilden eine Beschreibung der Hilfsprogramme und eine Anleitung zum Einrichten des Programmsystems.

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## 1. Introduction

HADA is a FORTRAN-IV program which computes the thermohydraulic parameters for Advanced Pressurized Light Water Reactors with tight fuel rod lattices based on the data of a Pressurized Light Water Reactor. It was developed and run on the IBM 3081/Siemens 7890 computer configuration in the Kernforschungszentrum Karlsruhe. It was translated under MVS/SP 1.3.2 using the Siemens Fortran 77 compiler with language level 66 and standard optimization. The program is written in FORTRAN-IV to grant the usage of earlier compiler versions, but it can also be translated with a Fortran 77 compiler. It doesn't contain computer specific statements or subroutine calls except DATUM. This routine provides two REAL\*8 arguments, first the current date, and second the actual time, both as text strings.

For the graphical representation of the results an independent program is available - written in FORTRAN-IV too and using Calcomp/Versatec plotter software. Probably some changes may be necessary to run this program with another plotter software.

In this report only the usage of the program is described, for a more detailed description of the physical background and the mathematical formulation of the problem the reader should refer to the three previous reports cited in literature list as number 1 to 3. The first report [1] describes the formulation and the results of an extended parametric study. In this report the reader will find also the explanation of all output parameters. In the second and third report [2],[3] the used modified correlations for the critical heat flux are described.

The program copy is delivered on a 9-track no-label-tape with a blocksize of 3120 bytes. The records are of fixed length of 80 bytes each. All source programs (main programs, subroutines, functions) are each written in their own file.

## 2. Input Data

The input parameters are divided into five groups

- problem identification  
(unit 47)
- control parameters for the input flow and programmable options  
(unit 05)
- common physical parameters  
(unit INP)
- special physical parameters  
(unit JNP)
- physical parameters for the computation of the critical heat flux  
(unit 05).

All data except character strings are read without format control

READ(...,\*,...) ...

This means, that, if there are required more then one input datum per line, successive data must be separated by at least one blank or a comma and may be entered in the same input line or, if necessary in continuation lines. It is not allowed to replace zeroes by blanks - as in formatted read - so, as many data must be present as required. The input data set should not be line numbered, to avoid misinterpreting in the case of continuation lines (the line numbers are treated as input data !).

### 2.1 Problem Identification (Unit 47)

A text of up to 55 characters can be entered as a problem identification. This text and the current date and time are used as header lines in all output data sets. If there are more characters then the allowed maximum, truncation occurs.



## 2.2 Control Parameters and Options (Unit 05)

The data of this group is read from the system input stream (unit 05) named SYSIN (IBM standards). The following values are required in particular:

1. line INP integer unit number associated to the data set containing the common physical parameters.

2. line IOP1 integer option controlling the computation of the pumping power in the primary circuit.  
=1 constant pumping power,  
=2 pumping power is computed using a given pump characteristic.

Other values are not allowed.

IOP2 integer option selecting the reactor type.  
=0 computation of the power fraction  $K$  for a given pressure drop  $\Delta p$ ,  
=1 computing the design parameters of a reactor with a homogeneous core,  
=2 computing the design parameters of a reactor with a heterogeneous core.

Other values are not allowed.

IOP3 integer option controlling the construction of the linear system.  
<0 the coefficient matrix is constructed in inverse order as the functional equations,  
≥0 the coefficient matrix is constructed in the same order as the functional equations (use this method only).

IOP4 integer option selecting the solution method.  
=1 Gauß algorithm without improvements (use this method),  
=2 Gauß algorithm with pivot search (rows),  
=3 Gauß algorithm with pivot search (rows and columns),  
=4 Gauß algorithm for a symmetrized coefficient matrix,  
=5 Gauß algorithm for a symmetrized coefficient matrix with reordering of the original matrix.

3. line IDR2 integer parameter controlling the output of the results. This parameter is divided into two subparameters

IDR2 and IMOD = IDR2/10

The subparameter IMOD denotes the number of iteration steps between successive dumps of the actual results. IDR2 controls the type and the extent of this output in correspondence to the following table :

IDR2	IMOD = 0
≤0	only the mean results are printed,
=1	the initial estimate is printed and after each iteration step the actual accuracy,
=2	as 1, and at the beginning of the iteration the coefficient matrix is printed before entering the elimination step,
=3	as 1,2, and at the beginning of the iteration the coefficient matrix is printed after leaving the elimination step,

IDR2	IMOD = IDR2/10
=10	as 1,2,3, and after solving the linear
=20	system the actual solutions are printed
=30	out every IMOD iteration step.
...	...

IDR3 integer parameter controlling the output of the heat flux calculations.

<1	Only the most important results are printed,
≥1	additionally local data as a function of the axial position is printed into a separate data set.

The following input line is only necessary for  $IOP2 > 0$ . If  $IOP2 = 0$  a special physical parameter must be present instead (s. 2.4.1).

4. line JNP integer unit number associated to the data set containing the special physical parameters
5. line GENAU real parameter denoting the required accuracy. The iteration is terminated, if the condition of eq. (6) comes true (the boundary  $\varepsilon$  corresponds to GENAU).
- DMAX real upper boundary for the increment of the solution vector. After each iteration step the condition of eq. (6) is tested against DMAX. If any of the increments is greater than DMAX, the solution is divided by two, until Eq. (6) is met. In most cases a value of 0.5 will result in good convergence of the iteration. But in some cases a smaller value may be needed to omit problems of divergency.
- ITMX integer maximum number of iteration steps. Non-convergent iterations are stopped after ITMX steps. Depending on the results, the computation may be repeated with a greater value of ITMX or with updated parameters.

### 2.3 Common Physical Parameters (Unit INP)

The data of this group is read from unit INP, which must be assigned to the data set containing the input.

- |         |      |      |                    |   |
|---------|------|------|--------------------|---|
| 1. line | Q0   | real | $Q_0$ [W]          | thermal power of the reference Pressurized Light Water Reactor. |
| 2. line | OP   | real | $O_p$ [-]          | power plant overpower factor.                                   |
|         | FDHO | real | $F_{\Delta H}$ [-] | hot channel factor for the enthalpy rise in the core.           |
|         | CDH  | real | $c_{\Delta H}$ [-] | parameter to force a DNB ratio of at least 1.3.                 |
|         | AKS  | real | $K'$ [-]           | part of the total mass flow rate cooling the core.              |
| 3. line | ALC  | real | $L_c$ [m]          | total length of the axial reflectors.                           |
| 4. line | DN   | real | $N$ [W]            | total pumping power for the primary circuit.                    |
|         | ETA  | real | $\eta$ [-]         | efficiency of the water pumps in the primary circuit.           |
| 5. line | P20  | real | $p_{20}$ [bar]     | water pressure at the outlet of the reference PWR.              |
| 6. line | T20  | real | $T_{20}$ [°C]      | average water temperature at the outlet of the reference PWR.   |

7. line	POS	real	$p_{0s}$ [bar] saturation pressure at the turbine of the reference PWR.
8. line	DMO	real	$M_0$ [kg/s] total mass flow rate in the primary circuit of the reference PWR.
9. line	DKO	real	KF [W/°C] heat transfer coefficient times the average total surface of the heat exchangers.
10. line	T10	real	$T_{10}$ [°C] average water temperature at the inlet of the reference PWR.
11. line	P10	real	$p_{10}$ [bar] water pressure at the inlet of the reference PWR.
12. line	HR	real	H [m] pressure head available for the rest of the primary circuit (besides the core) in the case of the reference PWR.
13. line	DNEL	real	$N_{e1}$ [W] total electrical power for internal use in the plant.
14. line	HTO	real	$H_{T0}$ [m] total pressure head of the water pumps in the primary circuit of the reference PWR.
15. line	QELO	real	$Q_{e10}$ [W] net electrical power of the reference PWR.

## 2.4 Special Physical Parameters (Unit 05, JNP)

For IOP2 > 0 the data of this group is read from unit JNP, which must be assigned to the data set containing the input. The number of the required parameters and their meaning depend on the value of IOP2. For IOP2 = 0 the data is read from unit 05 (system input stream).

### 2.4.1 Computation of the Power Ratio (IOP2=0, Unit 05)

In this case the power ratio K for an Advanced Pressurized Light Water Reactor is computed from the data of the reference Pressurized Water Reactor (common physical parameters) and a fixed value for the pressure drop over the core.

4. line	DPC	real	$\Delta p_c$ [bar]	
			required pressure drop over the core of the	
			Advanced Pressurized Water Reactor.	
5. line	GENAU	real		
	DMAX	real		
	ITMX	integer	as in chapter 2.2, 5. line.	

### 2.4.2 Reactor with a Homogeneous Core (Unit JNP)

For an Advanced Pressurized Water Reactor with a homogeneous core the geometry and special factors are read from unit JNP, which must be assigned to the corresponding data set.

- |         |       |      |   |
|---------|-------|------|---|
| 1. line | P     | real | $p$ [m]<br>fuel rod pitch.  |
| 2. line | D     | real | $d$ [m]<br>fuel rod diameter.   |
| 3. line | AK0   | real | $K_0$ [-]<br>aspect ratio for the spiral spacer ribs.   |
| 4. line | AK1   | real | $K_1$ [-]<br>ratio denoting the part of the total core cross section which is occupied by fuel rods and the subchannels between them.                 |
|         | AKL\$ | real | $K_{KL}$ [-]<br>correction factor for the relationship between average fuel rod linear rating and $p/d$ ratio.  |
| 5. line | AK2   | real | $K_2$ [-]<br>fraction of the "non-useful" cross section area (interface between fuel elements, control and structure rods) occupied by flowing water. |
| 6. line | DEQ   | real | $D_{eq}$ [m]<br>equivalent diameter, diameter of a circle with the same area as the cross section of the core.  |
| 7. line | HZUD  | real | $H/d$ [-]<br>pitch to diameter ratio for the spiral rib spacers.  |
| 8. line | AKI   | real | $K_I$ [-]<br>inlet pressure drop coefficient.   |

### 2.4.3 Reactor with a Heterogeneous Core (unit JNP)

For an Advanced Pressurized Water Reactor with a heterogeneous core the geometry and special factors are read from a data set assigned to unit JNP. In this case the reactor core is divided into two zones (seed and blanket).

- |         |        |      |                              |   |
|---------|--------|------|------------------------------|---|
| 1. line | RK1    | real | $K_1$ [-]                    | ratio of cross section area of seed to cross section area of blanket.   |
|         | AKLS\$ | real | $K_{KLS}$ [-]                | correction factor for the relationship between seed fuel rod linear rating and p/d ratio.                       |
|         | AKLB\$ | real | $K_{KLB}$ [-]                | correction factor for the relationship between blanket fuel rod linear rating and p/d ratio.                    |
| 2. line | RK2S   | real | $K_{2s}$ [-]                 | ratio denoting the part of the seed cross section which is occupied by fuel rods and relative cooling water.    |
| 3. line | RK2B   | real | $K_{2b}$ [-]                 | ratio denoting the part of the blanket cross section which is occupied by fuel rods and relative cooling water. |
| 4. line | RK3    | real | $K_3$ [-]                    | power ratio seed over blanket.  |
| 5. line | QVS    | real | $q_{Vs}$ [W/m <sup>3</sup> ] | average volume power density (seed).  |
| 6. line | DS     | real | $d_s$ [m]                    | fuel rod diameter (seed).   |
| 7. line | DEQ    | real | $D_{eq}$ [m]                 | equivalent diameter, diameter of a circle with the same area as the cross section of the core.                  |



8. line	ALSC	real	$L_{sC}$ [m] axial distance of spacer grids in the active core region (seed).
9. line	ALSR	real	$L_{sR}$ [m] axial distance of spacer grids in the fission gas plenum region (seed).
10. line	DKI	real	$K_I$ [-] inlet pressure drop coefficient.
11. line	CV	real	$C_v$ [-] modified drag coefficient of the spacer grid.
12. line	RK0	real	$K_0$ [-] aspect ratio for the spiral spacer ribs (blanket).
13. line	HZUDB	real	$[H/d]_b$ [-] pitch to diameter ratio for the spiral rib spacers (blanket).

## 2.5 Physical Parameters for the CHF Computations (Unit 05)

This group of data is read again from unit 05 (system input stream). The input stream contains options and parameters for the critical heat flux correlations. Four different correlations are available according to [2]. In an earlier version of the program the Shippingport relation was used [2], but in the present version an improved modified relation according to [3] is used. The subprogram which does the Shippingport calculations is still available and the input parameters must be present as dummy entries. The computation of the critical heat flux is done for a singular rod.

- |          |      |         |   |
|----------|------|---------|---|
| 6. line  | FIAX | real    | $\phi_{ax}$ [-]   |
|          |      |         | form factor accounting for the axial power distribution.  |
| 7. line  | AK   | real    | $K$ [W/m <sup>2</sup> ] $2.37 \cdot 10^6$   |
|          |      |         | constant used in the Shippingport relation. This parameter must be present as a dummy entry (its value has no importance), but it is not used in the latest version of the program. |
| 8. line  | H0   | real    | $H_0$ [J/kg] $1.588 \cdot 10^6$   |
|          |      |         | enthalpy base (depending on pressure) for the Shippingport relation. As the previous parameter this datum must be present as a dummy entry.   |
| 9. line  | FQ   | real    | $F_q$ [-]   |
|          |      |         | hot channel factor for the heat flux at the fuel rod surface.   |
| 10. line | AK4  | real    | $K_4$ [-]   |
|          |      |         | ratio between the shortening of the core active length due to insertion of the control rods and core active length without control rod insertion.                                   |
| 11. line | NC   | integer | $n_c$ [-]   |
|          |      |         | number of axial nodes for the computation of the local heat fluxes.   |

12.line	OP	real	$O_p$ [-]	overpower factor for the fuel rod under consideration.
13.line	Q1A	real	$Q_1$ 1.763	parameters used in the earlier version of our CHF correlation [2].
	Q2A	real	$Q_2$ 9.157	
	Q4A	real	$Q_4$ 6.507	
	Q1B	real	$Q_1$ 1.748	parameters used in the latter version of our CHF correlation [3].
	Q2B	real	$Q_2$ 7.540	
	Q4B	real	$Q_4$ 8.783	
14.line	FQN	real	$F_{qN}$ [-]	factor for the maximal heat flux accounting for the axial and radial power distribution.

### 3. Output

The program uses four output data sets associated to units 06,08,09, and 10. The first one, assigned to the system output data set (named SYSPRINT on IBM-systems), is used for the printing of system error messages. The second data set (unit 08) must be assigned to an existing file (named PROJECT.APWRS.DATA in the examples) with the following (or corresponding) DCB attributes

- record format RECFM=VBS
- record length LRECL=2996
- block size BLKSIZE=3000.

This data set is used as a result pool and contains the main results of consecutive runs. Data may be retrieved from this file by using one of the existing utility programs (s. chapter 6).

The input data, the main results, and, if required, the matrix, vector, and solution dumps are printed out to unit 09.

The local results of the critical heat flux calculation are printed out to unit 10.

The output in 09 and 10 is self-explaining, the same variable names are used as in chapter 2.5 for the input parameters. The variable names of the output parameters are explained in [1], so that no more detailed description is necessary here. In chapter 5 the output data of two sample runs are listed.

#### 4. Mathematical Background

The program HADA computes the solution of a nonlinear algebraic system by iteration. This system is given by a set of equations

$$(1) \quad F_j(x_i) = 0.$$

The elements of the solution vector  $x_i (i=1, \dots, n)$  are the zeroes of the  $(n)$  relations  $F_j$ . For solving this equations a simple Newton method is used as usually. In the first order Taylor approximation

$$(2) \quad F_j(x_i + \delta x_i) \approx F_j(x_i) + [\partial F_j(x_i) / \partial x_k] \delta x_k.$$

The condition  $F_j(x_i + \delta x_i) \rightarrow 0$  is forced by setting the left hand side of the equations system equal to zero

$$(3) \quad [\partial F_j(x_i) / \partial x_k] \delta x_k = -F_j(x_i).$$

Starting with an initial estimate  $x_i^0$  we obtain a series of approximations to the solution

$$(4) \quad [\partial F_j(x_i^v) / \partial x_k] \delta x_k^{v+1} = -F_j(x_i^v)$$

and

$$(5) \quad x_k^{v+1} = x_k^v + \delta x_k^{v+1},$$

which is considered as adequate if the related increment of all elements is less then a given positive number  $\varepsilon$ :

$$(6) \quad \max_k |\delta x_k^v / x_k^v| < \varepsilon.$$

The linear algebraic system (linear relative to  $\delta x$ ) is solved by using a Gauß algorithm (with or without pivot search). The matrix of coefficients is

$$(7.1) \quad a_j^k = \partial F(x_i^v) / \partial x_k$$

and the right hand sides are

$$(7.2) \quad b_j = -F_j(x_i^v).$$

Five different methods based on the Gauß algorithm are available in the program:

- straightforward algorithm without any computational improvements,
- pivot method (only rows are exchanged),
- pivot method (rows and columns are exchanged),
- Gauß algorithm for a system with symmetrical coefficient matrix,
- Gauß algorithm for a symmetrical system using a reordered coefficient matrix.

The two last methods don't solve the original equations (7), but a derived system which is obtained by multiplication from the left with the transposed coefficient matrix. From

$$(8) \quad a_j^k \delta x_k = b_j$$

we get the derived system

$$(9) \quad a_j^l a_l^k \delta x_k = a_j^l b_l.$$

The new matrix of coefficients is symmetrical:

$$(10.1) \quad s_j = a_j^l a_l^k.$$

The new right hand sides are

$$(10.2) \quad c_j = a_j^l b_l.$$

These two equations describe a new linear system replacing (8)

$$(11) \quad s_j^k \delta x_k = c_j.$$

To compute the elements of the coefficient matrix we need the partial derivatives of the functions. They are approximated numerically by a first order Taylor expansion.

For  $|x_k| \leq 10^{-6}$  we use:

$$f_1 = F_j(x_1, x_2, \dots, x_k^{-0.001}, \dots, x_n),$$

$$f_2 = F_j(x_1, x_2, \dots, x_k^{+0.001}, \dots, x_n),$$

$$\Delta x = 0.002,$$

and for  $|x_k| > 10^{-6}$ :

$$f_1 = F_j(x_1, x_2, \dots, 0.999 \cdot x_k, \dots, x_n),$$

$$f_2 = F_j(x_1, x_2, \dots, 1.001 \cdot x_k, \dots, x_n),$$

$$\Delta x = 0.002 \cdot x_k.$$

The derivatives are then calculated from

$$(12) \quad \partial F_j(x_i) / \partial x_k \approx (f_2 - f_1) / \Delta x.$$

In the testphase the increment  $\Delta x$  and the accuracy of the calculation have been varied, but the presented values and double precision arithmetic proved to be optimal.

## 5. Examples

To demonstrate the use of the program two sample runs are presented. The first sample is for a homogeneous reactor with computation of the water pumping power from a given characteristic. The input data and the control statements are shown at first. The used load module must be generated at first as described in chapter 7. For this sample the entire output is shown (units 09 and 10 in this order).

The second sample is for a heterogeneous reactor with computation of the water pumping power from a given characteristic too. In this case only the main results (unit 09) are shown.

### 5.1 Sample 1, Homogeneous Core, Constant Pump Characteristic

Control statements and input

```
Starting in column 1
↓
//PROJECT1 JOB (.....),.....,MSGCLASS=A
// EXEC PGM=HADA
//STEPLIB DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//*****
//**
//**          UNIT INP          COMMON PHYSICAL PARAMETERS
//**
//FT01F001 DD *
3.765E9          QO IN W
1.00,1.6,1.0266,0.94  OP,FDHO,CDH,K'
0.0             ALC FUER LR=1.1885*LC+0.02+ALC
1.7E7,0.774     N IN W,          ETA (NEU 8.9.83)
158.26          P20 IN BAR
326.12          T20 IN GRD C
64.5            POS IN BAR
1.8800E4        MO IN KG/S
1.55927E8       KFO IN W/GRD C
291.14          T10 IN GRD C
159.65          P10 IN BAR
70.6            HR IN M
5.4D7           NEL IN W
89.6            HTO IN M
1.3E9           NEL IN W
```





Main results (unit 09)

TITEL :

SAMPLE 1 HOMOGENEOUS REACTOR, CHARAKTERISTIC

18.01.85 11.36.25

EINGABEPARAMETER

Q0	=	3.7650D+09	W
POS	=	64.500	BAR
P20	=	158.26	BAR
T20	=	326.12	GRD C
KFO	=	1.5593D+08	WATT/GRD
N	=	1.7000D+07	WATT
P10	=	159.65	BAR
M0	=	18800.	KG/S
FDH0	=	1.6000	
CDH	=	1.0266	
OPF	=	1.0000	
T10	=	291.14	GRD C
HR	=	70.600	M
NEL	=	5.4000D+07	W
ALC	=	0.0	M

CONSTANT PUMP CHARACTERISTICS

P	=	1.1400D-02	M
D	=	9.5000D-03	M
DH	=	3.6908D-03	M
K0	=	0.33333	
K1	=	0.90640	
K2	=	0.50010	
DEQ	=	3.8594	M
H/D	=	20.000	
KI	=	1.2000	
P/D	=	1.2000	
B	=	6.3333D-04	M
KL	=	1.0000	-
QL	=	18000.	W/M
QV	=	1.5993D+08	W/CBM
AT	=	10.604	QM
NT	=	94212	
VM/VF	=	0.61890	
CELL	:	0.58783	

12.09.1983

HOMOGENEOUS REACTOR

EPS	=	1.0000D-03	%
DELTA	=	50.000	%

LOESUNGSVEKTOR UND ERREICHTE GENAUIGKEIT

NAME	NR	EINHEIT	WERT	ZUWACHS
*****	**	*****	*****	*****
K	1	-	1.0000	0.0
Q	2	W	2.9077D+09	0.0
T1	3	GRD C	291.14	0.0
RO1	4	KG/CBM	745.55	0.0
P1	5	BAR	159.65	0.0
H1	6	J/KG	1.2891D+06	0.0
T2	7	GRD C	326.12	0.0
RO2	8	KG/CBM	664.73	0.0
H2	9	J/KG	1.4900D+06	0.0
TS	10	GRD C	280.40	0.0
PS	11	BAR	64.500	0.0
TQ	12	GRD C	308.63	0.0
ROQ	13	KG/CBM	709.37	0.0
PQ	14	BAR	158.95	0.0
M	15	KG/S	18736.	0.0
KF	16	W/GRD	1.5583D+08	0.0
HT	17	M	91.473	0.0
HC	18	M	21.351	0.0
DP	19	BAR	1.3900	0.0
Y	20	-	1.4412	0.0
TSU	21	GRD C	332.91	0.0
RO2U	22	KG/CBM	643.72	0.0
H2U	23	J/KG	1.5355D+06	0.0
TQU	24	GRD C	308.63	0.0
ROQU	25	KG/CBM	709.37	0.0
NY	26	QM/S	1.2605D-07	0.0
U	27	M/S	6.0073	0.0
RE	28	-	2.1532D+05	0.0
LAM	29	-	2.4470D-02	0.0
ITER =	0	ABS :	8.1101D+08	2 *** REL : 0.50000 19
ITER =	1	ABS :	1.1757D+07	2 *** REL : 9.4562D-02 19
ITER =	2	ABS :	5.0986D+05	2 *** REL : 2.9138D-03 18

LOESUNGSVEKTOR UND ERREICHTE GENAUIGKEIT

NAME	NR	EINHEIT	WERT	ZUWACHS
****	**	*****	*****	*****
K	1	-	0.99068	-4.0402D-07
Q	2	W	3.7299D+09	-1521.1
T1	3	GRD C	290.33	-4.0844D-05
RO1	4	KG/CBM	747.22	7.4016D-05
P1	5	BAR	160.54	-2.6688D-06
H1	6	J/KG	1.2848D+06	-0.21171
T2	7	GRD C	326.09	-1.4125D-05
RO2	8	KG/CBM	664.80	4.0203D-05
H2	9	J/KG	1.4899D+06	-9.0553D-02
TS	10	GRD C	279.78	-2.7524D-05
PS	11	BAR	63.899	-2.6059D-05
TQ	12	GRD C	308.21	-2.7484D-05
ROQ	13	KG/CBM	710.41	5.9667D-05
PQ	14	BAR	159.40	-1.3344D-06
M	15	KG/S	18189.	-1.6975D-02
KF	16	W/GRD	1.5499D+08	-27.442
HT	17	M	96.968	1.5329D-04
HC	18	M	31.125	2.8047D-04
DP	19	BAR	2.2808	-2.6688D-06
Y	20	-	1.4790	1.5023D-06
TSU	21	GRD C	333.02	-9.9624D-06
RO2U	22	KG/CBM	643.35	3.2284D-05
H2U	23	J/KG	1.5363D+06	-6.8821D-02
TQU	24	GRD C	311.67	-2.5403D-05
ROQU	25	KG/CBM	702.48	5.9507D-05
NY	26	QM/S	1.2606D-07	-3.4434D-16
U	27	M/S	5.8890	-5.9456D-06
RE	28	-	2.1107D+05	-1.3620
LAM	29	-	2.4553D-02	2.7604D-08

ERGEBNISSE

Q = 3.7299D+09 W  
 K = 0.99068  
 PS = 63.899 BAR  
 TS = 279.78 GRD C  
 P1 = 160.54 BAR  
 T1 = 290.33 GRD C  
 T2 = 326.09 GRD C  
 M = 18189. KG/S  
 NP = 1.7800D+07 W  
 QNT = 1.2854D+09 W  
 QNT/QELO = 0.98879

\*\*\*\*\* ZUSATZ 08.09.1983 \*\*\*\*\*

KS = 0.94000 -  
 ETA = 0.77400 -  
 MS = 17098. KG/S  
 NPEL = 2.2998D+07 W

HOMOGENEOUS REACTOR

LC = 2.1995 M  
 LR = 2.6341 M  
 T2U = 333.02 GRD C  
 U = 5.8890 M/S  
 RE = 2.1107D+05  
 LAMBDA = 2.4553D-02  
 DP = 2.2808 BAR  
 DPTOT = 2.4992 BAR

\*\*\*\*\* ZUSATZ 08.09.1983 \*\*\*\*\*

DPP = 7.1056 BAR

CHF-CALCULATIONS

LC = 2.1995 M  
 T1 = 290.33 GRD C  
 RO1 = 747.22 KG/CBM  
 P1 = 160.54 BAR  
 H1 = 1.2848D+06 J/KG  
 T2 = 333.02 GRD  
 P2 = 158.26 BAR  
 ROQ = 702.48 KG/CBM  
 U = 5.8890 M/S  
 QL = 18000. W/M  
 D = 9.5000D-03 M  
 DH = 3.6908D-03 M  
 PZUD = 1.2000

EINGABEDATEN

FIAX = 1.4800  
 AK = 2.3700D+06  
 HO = 1.5880D+06 J/KG  
 FQ = 2.1000  
 K4 = 0.10000  
 NC = 40  
 OP = 1.1200  
 Q10 = 1.7630

Q20 = 9.1570  
Q40 = 6.5070  
Q1N = 1.7480  
Q2N = 7.5400  
Q4N = 8.7830  
FQN = 1.7760

ERGEBNISSE

X = 1.4729  
PI/2X = 1.0665  
LC<sup>1</sup> = 2.3456  
RLCR = 1.980  
RLCR<sup>1</sup> = 2.126  
V1 = 0.70000D+00 WSC-2  
V2 = 0.46105D+00 EIGENE,ALT  
V2 = 0.27023D+00 EIGENE,NEU



OVERPOWER FACTOR : 1.0000

POS X	T(X)	TW	EIGENE,ALT			EDLUND			WSC-2			EIGENE,NEU		
			CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR
0	0.0	324.48	2.656D+06	2.10	2.04	1.831D+06	1.45	1.31	1.979D+06	1.56	1.48	2.964D+06	2.34	2.28
1	0.05	327.00	2.515D+06	1.99	1.93	1.756D+06	1.39	1.25	1.907D+06	1.51	1.43	2.798D+06	2.22	2.15
2	0.11	329.51	2.379D+06	1.90	1.83	1.683D+06	1.34	1.21	1.834D+06	1.46	1.38	2.639D+06	2.11	2.04
3	0.16	332.00	2.246D+06	1.82	1.75	1.613D+06	1.31	1.17	1.760D+06	1.42	1.35	2.484D+06	2.01	1.94
4	0.22	334.44	2.116D+06	1.75	1.68	1.545D+06	1.27	1.14	1.686D+06	1.39	1.32	2.334D+06	1.93	1.86
5	0.27	336.83	1.989D+06	1.68	1.62	1.478D+06	1.25	1.12	1.611D+06	1.36	1.29	2.188D+06	1.85	1.78
6	0.33	339.15	1.864D+06	1.63	1.56	1.412D+06	1.23	1.11	1.534D+06	1.34	1.27	2.046D+06	1.79	1.72
7	0.38	341.39	1.741D+06	1.58	1.52	1.347D+06	1.22	1.10	1.457D+06	1.32	1.26	1.906D+06	1.73	1.67
8	0.44	343.54	1.620D+06	1.54	1.48	1.283D+06	1.22	1.10	1.377D+06	1.31	1.25	1.769D+06	1.68	1.62
9	0.49	345.59	1.501D+06	1.50	1.45	1.218D+06	1.22	1.11	1.296D+06	1.30	1.25	1.634D+06	1.64	1.58
10	0.55	347.52	1.382D+06	1.47	1.42	1.153D+06	1.23	1.13	1.213D+06	1.29	1.25	1.501D+06	1.60	1.55
11	0.60	349.33	1.263D+06	1.45	1.40	1.088D+06	1.25	1.16	1.127D+06	1.29	1.25	1.369D+06	1.57	1.52
12	0.66	351.01	1.145D+06	1.43	1.39	1.022D+06	1.27	1.19	1.039D+06	1.29	1.26	1.239D+06	1.54	1.50
13	0.71	352.53	1.027D+06	1.41	1.38	9.537D+05	1.31	1.25	9.477D+05	1.30	1.28	1.108D+06	1.52	1.48
14	0.77	353.91	9.089D+05	1.40	1.37	8.835D+05	1.36	1.32	8.528D+05	1.31	1.30	9.783D+05	1.50	1.47
15	0.82	355.13	7.899D+05	1.39	1.37	8.103D+05	1.42	1.43	7.541D+05	1.32	1.32	8.482D+05	1.49	1.47
16	0.88	356.18	6.699D+05	1.38	1.37	7.331D+05	1.51	1.58	6.509D+05	1.34	1.36	7.177D+05	1.48	1.47
17	0.93	357.06	5.487D+05	1.38	1.38	6.503D+05	1.64	1.84	5.428D+05	1.37	1.40	5.864D+05	1.48	1.47
18	0.99	357.76	4.258D+05	1.39	1.39	5.597D+05	1.82	2.34	4.292D+05	1.40	1.44	4.540D+05	1.48	1.48
19	1.04	358.29	3.009D+05	1.39	0.0	4.571D+05	2.11	0.0	3.091D+05	1.43	0.0	3.201D+05	1.48	0.0
20	1.10	358.63	1.736D+05	1.40	0.0	3.333D+05	2.69	0.0	1.819D+05	1.47	0.0	1.842D+05	1.49	0.0

MINIMALWERTE

CORRELATION	SMMIN	X	POS			
EIGENE,ALT	1.3821	0.93477	17	1.3684	0.82480	15
EDLUND	1.2180	0.43989	8	1.1036	0.38491	7
WSC-2	1.2912	0.60485	11	1.2456	0.49488	9
EIGENE,NEU	1.4768	0.98976	18	1.4662	0.87979	16

OVERPOWER FACTOR : 1.1200

POS X	T(X)	TW	EIGENE, ALT			EDLUND			WSC-2			EIGENE, NEU			
			CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	
0	0.0	328.58	341.65	2.656D+06	1.87	1.82	1.831D+06	1.29	1.17	1.979D+06	1.40	1.32	2.964D+06	2.09	2.04
1	0.05	331.40	343.63	2.515D+06	1.78	1.72	1.756D+06	1.24	1.12	1.907D+06	1.35	1.27	2.798D+06	1.98	1.92
2	0.11	334.22	345.47	2.379D+06	1.70	1.63	1.683D+06	1.20	1.08	1.834D+06	1.31	1.23	2.639D+06	1.88	1.82
3	0.16	337.00	347.17	2.246D+06	1.62	1.56	1.613D+06	1.17	1.05	1.760D+06	1.27	1.20	2.484D+06	1.79	1.73
4	0.22	339.73	348.70	2.116D+06	1.56	1.50	1.545D+06	1.14	1.02	1.686D+06	1.24	1.17	2.334D+06	1.72	1.66
5	0.27	342.41	348.89	1.989D+06	1.50	1.44	1.478D+06	1.12	1.00	1.611D+06	1.22	1.15	2.188D+06	1.65	1.59
6	0.33	345.01	348.85	1.864D+06	1.45	1.40	1.412D+06	1.10	0.99	1.534D+06	1.20	1.14	2.046D+06	1.60	1.54
7	0.38	347.52	348.80	1.741D+06	1.41	1.36	1.347D+06	1.09	0.99	1.457D+06	1.18	1.12	1.906D+06	1.54	1.49
8	0.44	349.93	348.75	1.620D+06	1.37	1.32	1.283D+06	1.09	0.99	1.377D+06	1.17	1.12	1.769D+06	1.50	1.45
9	0.49	352.22	348.69	1.501D+06	1.34	1.29	1.218D+06	1.09	0.99	1.296D+06	1.16	1.11	1.634D+06	1.46	1.41
10	0.55	354.39	348.63	1.382D+06	1.31	1.27	1.153D+06	1.10	1.01	1.213D+06	1.15	1.11	1.501D+06	1.43	1.38
11	0.60	356.41	348.57	1.263D+06	1.29	1.25	1.088D+06	1.11	1.03	1.127D+06	1.15	1.12	1.369D+06	1.40	1.36
12	0.66	358.29	348.50	1.145D+06	1.27	1.24	1.022D+06	1.14	1.07	1.039D+06	1.15	1.13	1.239D+06	1.38	1.34
13	0.71	360.00	348.43	1.027D+06	1.26	1.23	9.537D+05	1.17	1.11	9.477D+05	1.16	1.14	1.108D+06	1.36	1.32
14	0.77	361.54	348.35	9.089D+05	1.25	1.22	8.835D+05	1.21	1.18	8.528D+05	1.17	1.16	9.783D+05	1.34	1.31
15	0.82	362.91	348.27	7.899D+05	1.24	1.22	8.103D+05	1.27	1.27	7.541D+05	1.18	1.18	8.482D+05	1.33	1.31
16	0.88	364.08	348.17	6.699D+05	1.23	1.22	7.331D+05	1.35	1.41	6.509D+05	1.20	1.21	7.177D+05	1.32	1.31
17	0.93	365.07	348.06	5.487D+05	1.23	1.23	6.503D+05	1.46	1.64	5.428D+05	1.22	1.25	5.864D+05	1.32	1.31
18	0.99	365.86	347.94	4.258D+05	1.24	1.24	5.597D+05	1.63	2.09	4.292D+05	1.25	1.29	4.540D+05	1.32	1.32
19	1.04	366.44	347.86	3.009D+05	1.24	0.0	4.571D+05	1.89	0.0	3.091D+05	1.28	0.0	3.201D+05	1.32	0.0
20	1.10	366.82	347.66	1.736D+05	1.25	0.0	3.333D+05	2.40	0.0	1.819D+05	1.31	0.0	1.842D+05	1.33	0.0

MINIMALWERTE

CORRELATION	SMMIN	X	POS			
*****	*****	*****	***			
EIGENE, ALT	: 1.2340	0.93477	17	1.2218	0.82480	15
EDLUND	: 1.0875	0.43989	8	0.98535	0.38491	7
WSC-2	: 1.1528	0.60485	11	1.1121	0.49488	9
EIGENE, NEU	: 1.3186	0.98976	18	1.3091	0.87979	16

Local results from CHF calculations (unit 10)

TITEL :  
SAMPLE 1 HOMOGENEOUS REACTOR, CHARAKTERISTIC

18.01.85 11.36.25

OVERPOWER FACTOR : 1.0000

POS	X	T(X)	P(X)	HCHF(X)	HG(X)	HFG(X)	PR(X)	ALFA(X)	RE(X)	PHIN(X)	TW(X)	TW1	TW2
		CORRELATION		PHICHF(X)	PHIHS(X)	PHIHS(X)	PHIHS(X)	SM(X)	SMCR(X)				
NKD =		82	FAKT =	1.000									
0	0.0	324.48	159.40	1.5D+06	2.6D+06	9.3D+05	9.8D-01	4.7D+04	1.7D+05	1.1D+06	338.68	338.68	349.08
		EIGENE,ALT	:	2.6562D+06		1.2665D+06	1.3991D+06	2.10		2.04			
		EDLUND	:	1.8310D+06				1.45		1.31			
		WSC-2	:	1.9790D+06				1.56		1.48			
		EIGENE,NEU	:	2.9641D+06				2.34		2.28			
1	0.05	327.00	159.34	1.5D+06	2.6D+06	9.4D+05	1.0D+00	4.7D+04	1.8D+05	1.1D+06	340.45	340.45	349.05
		EIGENE,ALT	:	2.5153D+06		1.2631D+06	1.3944D+06	1.99		1.93			
		EDLUND	:	1.7557D+06				1.39		1.25			
		WSC-2	:	1.9065D+06				1.51		1.43			
		EIGENE,NEU	:	2.7983D+06				2.22		2.15			
2	0.11	329.51	159.29	1.5D+06	2.6D+06	9.4D+05	1.0D+00	4.7D+04	1.8D+05	1.1D+06	342.08	342.08	349.01
		EIGENE,ALT	:	2.3786D+06		1.2528D+06	1.3806D+06	1.90		1.83			
		EDLUND	:	1.6832D+06				1.34		1.21			
		WSC-2	:	1.8337D+06				1.46		1.38			
		EIGENE,NEU	:	2.6385D+06				2.11		2.04			
3	0.16	332.00	159.23	1.5D+06	2.6D+06	9.4D+05	1.0D+00	4.8D+04	1.8D+05	1.0D+06	343.57	343.57	348.98
		EIGENE,ALT	:	2.2456D+06		1.2358D+06	1.3577D+06	1.82		1.75			
		EDLUND	:	1.6129D+06				1.31		1.17			
		WSC-2	:	1.7602D+06				1.42		1.35			
		EIGENE,NEU	:	2.4840D+06				2.01		1.94			
4	0.22	334.44	159.17	1.6D+06	2.6D+06	9.4D+05	1.1D+00	4.8D+04	1.8D+05	1.0D+06	344.91	344.91	348.94
		EIGENE,ALT	:	2.1158D+06		1.2120D+06	1.3258D+06	1.75		1.68			
		EDLUND	:	1.5446D+06				1.27		1.14			
		WSC-2	:	1.6860D+06				1.39		1.32			
		EIGENE,NEU	:	2.3340D+06				1.93		1.86			
5	0.27	336.83	159.12	1.6D+06	2.6D+06	9.4D+05	1.1D+00	4.8D+04	1.8D+05	1.0D+06	346.09	346.09	348.89
		EIGENE,ALT	:	1.9888D+06		1.1816D+06	1.2851D+06	1.68		1.62			
		EDLUND	:	1.4777D+06				1.25		1.12			
		WSC-2	:	1.6108D+06				1.36		1.29			
		EIGENE,NEU	:	2.1881D+06				1.85		1.78			
6	0.33	339.15	159.06	1.6D+06	2.6D+06	9.4D+05	1.1D+00	4.8D+04	1.8D+05	9.7D+05	347.11	347.11	348.85
		EIGENE,ALT	:	1.8641D+06		1.1449D+06	1.2360D+06	1.63		1.56			
		EDLUND	:	1.4120D+06				1.23		1.11			
		WSC-2	:	1.5344D+06				1.34		1.27			
		EIGENE,NEU	:	2.0456D+06				1.79		1.72			
7	0.38	341.39	159.00	1.6D+06	2.6D+06	9.4D+05	1.1D+00	4.8D+04	1.8D+05	9.3D+05	347.96	347.96	348.80
		EIGENE,ALT	:	1.7415D+06		1.1019D+06	1.1787D+06	1.58		1.52			
		EDLUND	:	1.3471D+06				1.22		1.10			
		WSC-2	:	1.4567D+06				1.32		1.26			
		EIGENE,NEU	:	1.9061D+06				1.73		1.67			
8	0.44	343.54	158.94	1.6D+06	2.6D+06	9.4D+05	1.1D+00	4.8D+04	1.8D+05	8.9D+05	348.64	348.64	348.75
		EIGENE,ALT	:	1.6204D+06		1.0530D+06	1.1137D+06	1.54		1.48			
		EDLUND	:	1.2826D+06				1.22		1.10			
		WSC-2	:	1.3774D+06				1.31		1.25			
		EIGENE,NEU	:	1.7692D+06				1.68		1.62			
LOKALES SIEDEN :		0.495	M,	TB =	348.69								
9	0.49	345.59	158.89	1.7D+06	2.6D+06	9.4D+05	1.2D+00	4.9D+04	1.8D+05	8.4D+05	348.69	349.15	348.69
		EIGENE,ALT	:	1.5005D+06		9.9837D+05	1.0412D+06	1.50		1.45			
		EDLUND	:	1.2181D+06				1.22		1.11			
		WSC-2	:	1.2963D+06				1.30		1.25			
		EIGENE,NEU	:	1.6343D+06				1.64		1.58			
LOKALES SIEDEN :		0.550	M,	TB =	348.63								
10	0.55	347.52	158.83	1.7D+06	2.6D+06	9.4D+05	1.2D+00	4.9D+04	1.8D+05	7.9D+05	348.63	349.48	348.63
		EIGENE,ALT	:	1.3816D+06		9.3832D+05	9.6195D+05	1.47		1.42			
		EDLUND	:	1.1535D+06				1.23		1.13			
		WSC-2	:	1.2131D+06				1.29		1.25			

		EIGENE, NEU	:	1.5012D+06				1.60		1.55				
LOKALES SIEDEN	:	0.605 M,	TB =	348.57										
11	0.60	349.33 158.77		1.7D+06	2.6D+06	9.4D+05	1.2D+00	4.9D+04	1.9D+05	7.4D+05	348.57	349.64	348.57	
		EIGENE, ALT	:	1.2633D+06		8.7319D+05	8.7631D+05	1.45		1.40				
		EDLUND	:	1.0881D+06				1.25		1.16				
		WSC-2	:	1.1274D+06				1.29		1.25				
		EIGENE, NEU	:	1.3694D+06				1.57		1.52				
LOKALES SIEDEN	:	0.660 M,	TB =	348.50										
12	0.66	351.01 158.72		1.7D+06	2.6D+06	9.4D+05	1.2D+00	4.9D+04	1.9D+05	6.8D+05	348.50	349.63	348.50	
		EIGENE, ALT	:	1.1453D+06		8.0332D+05	7.8489D+05	1.43		1.39				
		EDLUND	:	1.0217D+06				1.27		1.19				
		WSC-2	:	1.0391D+06				1.29		1.26				
		EIGENE, NEU	:	1.2385D+06				1.54		1.50				
LOKALES SIEDEN	:	0.715 M,	TB =	348.43										
13	0.71	352.53 158.66		1.7D+06	2.6D+06	9.4D+05	1.3D+00	4.9D+04	1.9D+05	6.2D+05	348.43	349.44	348.43	
		EIGENE, ALT	:	1.0273D+06		7.2909D+05	6.8828D+05	1.41		1.38				
		EDLUND	:	9.5370D+05				1.31		1.25				
		WSC-2	:	9.4769D+05				1.30		1.28				
		EIGENE, NEU	:	1.1083D+06				1.52		1.48				
LOKALES SIEDEN	:	0.770 M,	TB =	348.35										
14	0.77	353.91 158.60		2.7D+06	2.6D+06	9.4D+05	1.3D+00	5.0D+04	1.9D+05	5.5D+05	348.35	349.09	348.35	
		EIGENE, ALT	:	9.0891D+05		6.5091D+05	5.8713D+05	1.40		1.37				
		EDLUND	:	8.8348D+05				1.36		1.32				
		WSC-2	:	8.5283D+05				1.31		1.30				
		EIGENE, NEU	:	9.7831D+05				1.50		1.47				
LOKALES SIEDEN	:	0.825 M,	TB =	348.27										
15	0.82	355.13 158.55		2.7D+06	2.6D+06	9.4D+05	1.3D+00	5.0D+04	1.9D+05	4.8D+05	348.27	348.57	348.27	
		EIGENE, ALT	:	7.8991D+05		5.6920D+05	4.8211D+05	1.39		1.37				
		EDLUND	:	8.1028D+05				1.42		1.43				
		WSC-2	:	7.5407D+05				1.32		1.32				
		EIGENE, NEU	:	8.4824D+05				1.49		1.47				
16	0.88	356.18 158.49		2.7D+06	2.6D+06	9.4D+05	1.3D+00	5.0D+04	1.9D+05	4.1D+05	347.89	347.89	348.17	
		EIGENE, ALT	:	6.6994D+05		4.8441D+05	3.7390D+05	1.38		1.37				
		EDLUND	:	7.3305D+05				1.51		1.58				
		WSC-2	:	6.5093D+05				1.34		1.36				
		EIGENE, NEU	:	7.1773D+05				1.48		1.47				
17	0.93	357.06 158.43		2.7D+06	2.6D+06	9.4D+05	1.4D+00	5.0D+04	1.9D+05	3.4D+05	347.05	347.05	348.06	
		EIGENE, ALT	:	5.4868D+05		3.9699D+05	2.6323D+05	1.38		1.38				
		EDLUND	:	6.5031D+05				1.64		1.84				
		WSC-2	:	5.4284D+05				1.37		1.40				
		EIGENE, NEU	:	5.8644D+05				1.48		1.47				
18	0.99	357.76 158.37		2.7D+06	2.6D+06	9.4D+05	1.4D+00	5.0D+04	1.9D+05	2.6D+05	346.06	346.06	347.94	
		EIGENE, ALT	:	4.2578D+05		3.0742D+05	1.5082D+05	1.39		1.39				
		EDLUND	:	5.5972D+05				1.82		2.34				
		WSC-2	:	4.2915D+05				1.40		1.44				
		EIGENE, NEU	:	4.5400D+05				1.48		1.48				
19	1.04	358.29 158.32		2.7D+06	2.6D+06	9.4D+05	1.4D+00	5.1D+04	1.9D+05	1.8D+05	344.91	344.91	347.86	
		EIGENE, ALT	:	3.0088D+05		2.1618D+05	1.5082D+05	1.39		0.0				
		EDLUND	:	4.5712D+05				2.11		0.0				
		WSC-2	:	3.0913D+05				1.43		0.0				
		EIGENE, NEU	:	3.2005D+05				1.48		0.0				
20	1.10	358.63 158.26		2.7D+06	2.6D+06	9.4D+05	1.4D+00	5.1D+04	1.9D+05	1.0D+05	343.62	343.62	347.66	
		EIGENE, ALT	:	1.7359D+05		1.2377D+05	1.5082D+05	1.40		0.0				
		EDLUND	:	3.3330D+05				2.69		0.0				
		WSC-2	:	1.8193D+05				1.47		0.0				
		EIGENE, NEU	:	1.8420D+05				1.49		0.0				

NKD = 107

OVERPOWER FACTOR : 1.1200

POS	X	T(X)	P(X)	HCHF(X)	HG(X)	HFG(X)	PR(X)	ALFA(X)	RE(X)	PHIN(X)	TW(X)	TW1	TW2
		CORRELATION		PHICHF(X)		PHIHS(X)		SM(X)		SMCR(X)			
*****													
NKD =		108	FAKT =	1.120									
0	0.0	328.58	159.40	1.5D+06	2.6D+06	9.3D+05	1.0D+00	4.7D+04	1.8D+05	1.1D+06	341.65	341.65	349.08
		EIGENE,ALT	:	2.6562D+06		1.4185D+06	1.5669D+06	1.87		1.82			
		EDLUND	:	1.8310D+06				1.29		1.17			
		WSC-2	:	1.9790D+06				1.40		1.32			
		EIGENE,NEU	:	2.9641D+06				2.09		2.04			
1	0.05	331.40	159.34	1.5D+06	2.6D+06	9.4D+05	1.0D+00	4.7D+04	1.8D+05	1.1D+06	343.63	343.63	349.05
		EIGENE,ALT	:	2.5153D+06		1.4147D+06	1.5618D+06	1.78		1.72			
		EDLUND	:	1.7557D+06				1.24		1.12			
		WSC-2	:	1.9065D+06				1.35		1.27			
		EIGENE,NEU	:	2.7983D+06				1.98		1.92			
2	0.11	334.22	159.29	1.5D+06	2.6D+06	9.4D+05	1.0D+00	4.8D+04	1.8D+05	1.1D+06	345.47	345.47	349.01
		EIGENE,ALT	:	2.3786D+06		1.4032D+06	1.5463D+06	1.70		1.63			
		EDLUND	:	1.6832D+06				1.20		1.08			
		WSC-2	:	1.8337D+06				1.31		1.23			
		EIGENE,NEU	:	2.6385D+06				1.88		1.82			
3	0.16	337.00	159.23	1.6D+06	2.6D+06	9.4D+05	1.1D+00	4.8D+04	1.8D+05	1.0D+06	347.17	347.17	348.98
		EIGENE,ALT	:	2.2456D+06		1.3841D+06	1.5206D+06	1.62		1.56			
		EDLUND	:	1.6129D+06				1.17		1.05			
		WSC-2	:	1.7602D+06				1.27		1.20			
		EIGENE,NEU	:	2.4840D+06				1.79		1.73			
4	0.22	339.73	159.17	1.6D+06	2.6D+06	9.4D+05	1.1D+00	4.8D+04	1.8D+05	1.0D+06	348.70	348.70	348.94
		EIGENE,ALT	:	2.1158D+06		1.3574D+06	1.4849D+06	1.56		1.50			
		EDLUND	:	1.5446D+06				1.14		1.02			
		WSC-2	:	1.6860D+06				1.24		1.17			
		EIGENE,NEU	:	2.3340D+06				1.72		1.66			
LOKALES SIEDEN :		0.275	M,	TB =		348.89							
5	0.27	342.41	159.12	1.6D+06	2.6D+06	9.4D+05	1.1D+00	4.8D+04	1.8D+05	1.0D+06	348.89	350.08	348.89
		EIGENE,ALT	:	1.9888D+06		1.3234D+06	1.4394D+06	1.50		1.44			
		EDLUND	:	1.4777D+06				1.12		1.00			
		WSC-2	:	1.6108D+06				1.22		1.15			
		EIGENE,NEU	:	2.1881D+06				1.65		1.59			
LOKALES SIEDEN :		0.330	M,	TB =		348.85							
6	0.33	345.01	159.06	1.6D+06	2.6D+06	9.4D+05	1.2D+00	4.9D+04	1.8D+05	9.7D+05	348.85	351.28	348.85
		EIGENE,ALT	:	1.8641D+06		1.2823D+06	1.3843D+06	1.45		1.40			
		EDLUND	:	1.4120D+06				1.10		0.991			
		WSC-2	:	1.5344D+06				1.20		1.14			
		EIGENE,NEU	:	2.0456D+06				1.60		1.54			
LOKALES SIEDEN :		0.385	M,	TB =		348.80							
7	0.38	347.52	159.00	1.7D+06	2.6D+06	9.4D+05	1.2D+00	4.9D+04	1.8D+05	9.3D+05	348.80	352.31	348.80
		EIGENE,ALT	:	1.7415D+06		1.2342D+06	1.3202D+06	1.41		1.36			
		EDLUND	:	1.3471D+06				1.09		0.985			
		WSC-2	:	1.4567D+06				1.18		1.12			
		EIGENE,NEU	:	1.9061D+06				1.54		1.49			
LOKALES SIEDEN :		0.440	M,	TB =		348.75							
8	0.44	349.93	158.94	1.7D+06	2.6D+06	9.4D+05	1.2D+00	4.9D+04	1.9D+05	8.9D+05	348.75	353.16	348.75
		EIGENE,ALT	:	1.6204D+06		1.1794D+06	1.2473D+06	1.37		1.32			
		EDLUND	:	1.2826D+06				1.09		0.986			
		WSC-2	:	1.3774D+06				1.17		1.12			
		EIGENE,NEU	:	1.7692D+06				1.50		1.45			
LOKALES SIEDEN :		0.495	M,	TB =		348.69							
9	0.49	352.22	158.89	1.7D+06	2.6D+06	9.4D+05	1.3D+00	4.9D+04	1.9D+05	8.4D+05	348.69	353.83	348.69
		EIGENE,ALT	:	1.5005D+06		1.1182D+06	1.1662D+06	1.34		1.29			
		EDLUND	:	1.2181D+06				1.09		0.993			
		WSC-2	:	1.2963D+06				1.16		1.11			
		EIGENE,NEU	:	1.6343D+06				1.46		1.41			
LOKALES SIEDEN :		0.550	M,	TB =		348.63							

10	0.55	354.39	158.83	2.7D+06	2.6D+06	9.4D+05	1.3D+00	5.0D+04	1.9D+05	7.9D+05	348.63	354.32	348.63
		EIGENE,ALT	:	1.3816D+06		1.0509D+06	1.0774D+06	1.31		1.27			
		EDLUND	:	1.1535D+06				1.10		1.01			
		WSC-2	:	1.2131D+06				1.15		1.11			
		EIGENE,NEU	:	1.5012D+06				1.43		1.38			
LOKALES SIEDEN	:	0.605 M,	TB =	348.57									
11	0.60	356.41	158.77	2.7D+06	2.6D+06	9.4D+05	1.4D+00	5.0D+04	1.9D+05	7.4D+05	348.57	354.62	348.57
		EIGENE,ALT	:	1.2633D+06		9.7797D+05	9.8147D+05	1.29		1.25			
		EDLUND	:	1.0881D+06				1.11		1.03			
		WSC-2	:	1.1274D+06				1.15		1.12			
		EIGENE,NEU	:	1.3694D+06				1.40		1.36			
LOKALES SIEDEN	:	0.660 M,	TB =	348.50									
12	0.66	358.29	158.72	2.7D+06	2.6D+06	9.4D+05	1.4D+00	5.1D+04	1.9D+05	6.8D+05	348.50	354.74	348.50
		EIGENE,ALT	:	1.1453D+06		8.9971D+05	8.7907D+05	1.27		1.24			
		EDLUND	:	1.0217D+06				1.14		1.07			
		WSC-2	:	1.0391D+06				1.15		1.13			
		EIGENE,NEU	:	1.2385D+06				1.38		1.34			
LOKALES SIEDEN	:	0.715 M,	TB =	348.43									
13	0.71	360.00	158.66	2.7D+06	2.6D+06	9.4D+05	1.4D+00	5.1D+04	1.9D+05	6.2D+05	348.43	354.68	348.43
		EIGENE,ALT	:	1.0273D+06		8.1658D+05	7.7087D+05	1.26		1.23			
		EDLUND	:	9.5370D+05				1.17		1.11			
		WSC-2	:	9.4769D+05				1.16		1.14			
		EIGENE,NEU	:	1.1083D+06				1.36		1.32			
LOKALES SIEDEN	:	0.770 M,	TB =	348.35									
14	0.77	361.54	158.60	2.8D+06	2.6D+06	9.4D+05	1.5D+00	5.1D+04	1.9D+05	5.5D+05	348.35	354.45	348.35
		EIGENE,ALT	:	9.0891D+05		7.2902D+05	6.5759D+05	1.25		1.22			
		EDLUND	:	8.8348D+05				1.21		1.18			
		WSC-2	:	8.5283D+05				1.17		1.16			
		EIGENE,NEU	:	9.7831D+05				1.34		1.31			
LOKALES SIEDEN	:	0.825 M,	TB =	348.27									
15	0.82	362.91	158.55	2.8D+06	2.6D+06	9.4D+05	1.5D+00	5.2D+04	1.9D+05	4.8D+05	348.27	354.05	348.27
		EIGENE,ALT	:	7.8991D+05		6.3751D+05	5.3996D+05	1.24		1.22			
		EDLUND	:	8.1028D+05				1.27		1.27			
		WSC-2	:	7.5407D+05				1.18		1.18			
		EIGENE,NEU	:	8.4824D+05				1.33		1.31			
LOKALES SIEDEN	:	0.880 M,	TB =	348.17									
16	0.88	364.08	158.49	2.8D+06	2.6D+06	9.4D+05	1.6D+00	5.2D+04	1.9D+05	4.1D+05	348.17	353.48	348.17
		EIGENE,ALT	:	6.6994D+05		5.4254D+05	4.1877D+05	1.23		1.22			
		EDLUND	:	7.3305D+05				1.35		1.41			
		WSC-2	:	6.5093D+05				1.20		1.21			
		EIGENE,NEU	:	7.1773D+05				1.32		1.31			
LOKALES SIEDEN	:	0.935 M,	TB =	348.06									
17	0.93	365.07	158.43	2.8D+06	2.6D+06	9.4D+05	1.6D+00	5.3D+04	1.9D+05	3.4D+05	348.06	352.76	348.06
		EIGENE,ALT	:	5.4868D+05		4.4463D+05	2.9481D+05	1.23		1.23			
		EDLUND	:	6.5031D+05				1.46		1.64			
		WSC-2	:	5.4284D+05				1.22		1.25			
		EIGENE,NEU	:	5.8644D+05				1.32		1.31			
LOKALES SIEDEN	:	0.990 M,	TB =	347.94									
18	0.99	365.86	158.37	2.8D+06	2.6D+06	9.4D+05	1.7D+00	5.3D+04	1.9D+05	2.6D+05	347.94	351.87	347.94
		EIGENE,ALT	:	4.2578D+05		3.4431D+05	1.6891D+05	1.24		1.24			
		EDLUND	:	5.5972D+05				1.63		2.09			
		WSC-2	:	4.2915D+05				1.25		1.29			
		EIGENE,NEU	:	4.5400D+05				1.32		1.32			
LOKALES SIEDEN	:	1.045 M,	TB =	347.86									
19	1.04	366.44	158.32	2.8D+06	2.6D+06	9.4D+05	1.7D+00	5.3D+04	1.9D+05	1.8D+05	347.86	350.84	347.86
		EIGENE,ALT	:	3.0088D+05		2.4212D+05	1.6891D+05	1.24		0.0			
		EDLUND	:	4.5712D+05				1.89		0.0			
		WSC-2	:	3.0913D+05				1.28		0.0			
		EIGENE,NEU	:	3.2005D+05				1.32		0.0			
LOKALES SIEDEN	:	1.100 M,	TB =	347.66									
20	1.10	366.82	158.26	2.8D+06	2.6D+06	9.4D+05	1.7D+00	5.4D+04	1.9D+05	1.0D+05	347.66	349.65	347.66
		EIGENE,ALT	:	1.7359D+05		1.3862D+05	1.6891D+05	1.25		0.0			



	EDLUND	:	3.3330D+05		2.40	0.0
	WSC-2	:	1.8193D+05		1.31	0.0
	EIGENE,NEU	:	1.8420D+05		1.33	0.0
	NKD =		133			
RC001	1 DATENSATZ					
	NA =		72 ZEICHEN TITELZEILE:			
			SAMPLE 1 HOMOGENEOUS REACTOR, CHARAKTERISTIC	18.01.85	11.36.25	
RC003	NR =		133 WOERTER REAL*4			
RC004	NI =		4 WOERTER INTEGER*4			
RC002	NEU GESCHRIEBEN					

## 5.2 Sample 2, Heterogeneous Core, Constant Pump Characteristic

Control statements and input

Starting in column 1

```
↓
//PROJECT2 JOB (.....,.....,.....),.....,MSGCLASS=A
// EXEC PGM=HADA
//STEPLIB DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//*****
//**
//**          UNIT INP          COMMON PHYSICAL PARAMETERS
//**
//FT01F001 DD *
3.765E9          QO IN W
1.00,1.6,1.0000,0.94  OP,FDHO,CDH,K'
0.0              ALC
1.7E7,0.774     N IN W
158.26          P20 IN BAR
326.12          T20 IN GRD C
64.5            POS IN BAR
18800.          MO IN KG/S
1.55927E8       KFO IN W/GRD C
291.14          T10 IN GRD C
159.65          P10 IN BAR
70.6            HR IN M
5.4D7           NEL IN W
89.6            HTO IN M
1.3E9           NEL IN W
//*****
//**
//**          UNIT JNP          SPECIAL PHYSICAL PARAMETERS
//**
//FT03F001 DD *
.302605,1.,1.   K1,KLS,KLB
.884686         K2S
.929184         K2B
.50824D0        K3
2.44652E8       QVS IN W/M**3
7.4000E-3       DS IN M
3.8469          DEQ IN M
.15             LSC IN M
.2              LSR IN M
1.2             KI
7.              CV
.3333333333333333 KO
20.             H/D
```

```
//*****
//**
//**          UNIT 05          SYSIN
//**
//FT05F001 DD *
1              INP
2,2,1,1      IOP1,IOP2,IOP3,IOP4 .,2,.. HETEROGEN <==
1,2          IDR1,IDR2
3            JNP              3      HETEROGEN <==
1.D-5,.5,20  EPS,DMAX,IMAX
1.54         PHIAX
2.37D6      K
1588.D3     HO
2.1         FQ
.1          K4
40          NC
1.12        OP
1.763,9.157,6.507,1.748,7.540,8.783 (Q1,Q2,Q4)ALT,(Q1,Q2,Q4)NEU
1.848       FQN
//FT06F001 DD SYSOUT=*,
//          DCB=(LRECL=133,BLKSIZE=3857,RECFM=FBA)
//FT08F001 DD DSN=PROJECT.APWRS.DATA,DISP=(MOD,PASS)
//FT09F001 DD SYSOUT=*,
//          DCB=(LRECL=133,BLKSIZE=3857,RECFM=FBA)
//FT10F001 DD SYSOUT=*,
//          DCB=(LRECL=133,BLKSIZE=3857,RECFM=FBA)
//*****
//:**
//**          UNIT 47          PROBLEM IDENTIFICATION
//**
//FT47F001 DD *
SAMPLE 2 HETEROGENEOUS CORE, CHARACTERISTIC
//
```

Main results (unit 09)

TITEL :  
SAMPLE 2 HETEROGENEOUS, CHARAKTERISTIC  
18.01.85 16.28.10

E I N G A B E P A R A M E T E R

Q0	=	3.7650D+09	W
POS	=	64.500	BAR
P20	=	158.26	BAR
T20	=	326.12	GRD C
KFO	=	1.5593D+08	WATT/GRD
N	=	1.7000D+07	WATT
P10	=	159.65	BAR
M0	=	18800.	KG/S
FDHO	=	1.6000	
CDH	=	1.0000	
OPF	=	1.0000	
T10	=	291.14	GRD C
HR	=	70.600	M
NEL	=	5.4000D+07	W
ALC	=	0.0	M

C O N S T A N T P U M P C H A R A C T E R I S T I C S

K1	=	0.30260	
K2S	=	0.88469	
K2B	=	0.92918	
K3	=	0.50824	
QVS	=	2.4465D+08	W/CBM
QVB	=	1.2434D+08	W/CBM
DEQ	=	3.8469	M
LSC	=	0.15000	M
LSR	=	0.20000	M
KI	=	1.2000	
CV	=	7.0000	
K0	=	0.33333	
H/DB	=	20.000	
QLS	=	19465.	W/M
DHS	=	6.2897D-03	M
HETEROGENEOUS REACTOR			
EPS	=	1.0000D-03	%
DELTA	=	50.000	%

LOESUNGSVEKTOR UND ERREICHTE GENAUIGKEIT

NAME	NR	EINHEIT	WERT	ZUWACHS
****	**	*****	*****	*****
K	1	-	1.0000	0.0
Q	2	W	3.7650D+09	0.0
T1	3	GRD C	291.14	0.0
RO1	4	KG/CBM	745.55	0.0
P1	5	BAR	159.65	0.0
H1	6	J/KG	1.2891D+06	0.0
T2	7	GRD C	326.12	0.0
RO2	8	KG/CBM	664.73	0.0
H2	9	J/KG	1.4900D+06	0.0
TS	10	GRD C	280.40	0.0
PS	11	BAR	64.500	0.0
TQ	12	GRD C	308.63	0.0
ROQ	13	KG/CBM	709.37	0.0
PQ	14	BAR	158.95	0.0
M	15	KG/S	18736.	0.0
KF	16	W/GRD	1.5583D+08	0.0
HT	17	M	91.473	0.0
HC	18	M	21.351	0.0
DP	19	BAR	1.4325	0.0
Y	20	-	1.4412	0.0
LR	21	M	2.6557	0.0
T2US	22	GRD C	326.12	0.0
RO2US	23	KG/CBM	664.73	0.0
H2US	24	J/KG	1.5307D+06	0.0
TQS	25	GRD C	308.63	0.0
ROQS	26	KG/CBM	709.37	0.0
NYS	27	QM/S	1.2605D-07	0.0
US	28	M/S	6.8892	0.0
RES	29	-	3.4375D+05	0.0
LAMS	30	-	1.4640D-02	0.0
NG	31	-	18.000	0.0
PB	32	M	1.3486D-02	0.0
BB	33	M	5.6908D-04	0.0
DB	34	M	1.1779D-02	0.0
AB	35	QM	2.2542D-05	0.0
DHB	36	M	3.8169D-03	0.0
T2UB	37	GRD C	326.12	0.0
RO2UB	38	KG/CBM	664.73	0.0
H2UB	39	J/KG	1.5192D+06	0.0
TQB	40	GRD C	308.63	0.0
ROQB	41	KG/CBM	709.37	0.0
NYB	42	QM/S	1.2605D-07	0.0
UB	43	M/S	6.6184	0.0
FB	44	-	0.77268	0.0
REB	45	-	1.7616D+05	0.0
CB	46	-	1.0000	0.0
LAMB	47	-	1.3055D-02	0.0
QLB	48	W/M	16958.	0.0
ITER =	0	ABS :	5.5611D+07	2 *** REL : 0.50000 44
ITER =	1	ABS :	8.4338D+06	2 *** REL : 0.49161 19
ITER =	2	ABS :	4.5661D+06	2 *** REL : 5.0263D-02 35
ITER =	3	ABS :	1.0100D+05	2 *** REL : 1.2077D-03 33

LOESUNGSVEKTOR UND ERREICHTE GENAUIGKEIT				
NAME	NR	EINHEIT	WERT	ZUWACHS
****	**	*****	*****	*****
K	1	-	0.98418	-1.0579D-08
Q	2	W	3.7054D+09	-39.831
T1	3	GRD C	289.58	-1.5078D-06
RO1	4	KG/CBM	748.79	-2.6675D-06
P1	5	BAR	161.48	-1.5542D-07
H1	6	J/KG	1.2808D+06	-6.0453D-03
T2	7	GRD C	326.68	-1.0092D-07
RO2	8	KG/CBM	663.09	2.8178D-06
H2	9	J/KG	1.4937D+06	-2.4937D-03
TS	10	GRD C	279.34	-7.3271D-07
PS	11	BAR	63.479	-6.8236D-07
TQ	12	GRD C	308.13	-8.0438D-07
ROQ	13	KG/CBM	710.70	2.0787D-06
PQ	14	BAR	159.87	-7.7708D-08
M	15	KG/S	17408.	-4.2005D-04
KF	16	W/GRD	1.5369D+08	-0.75269
HT	17	M	104.07	2.3310D-06
HC	18	M	43.914	4.8997D-06
DP	19	BAR	3.2246	-1.5542D-07
Y	20	-	1.5314	6.9107D-08
LR	21	M	2.6140	-2.7883D-08
T2US	22	GRD C	333.09	9.9135D-08
RO2US	23	KG/CBM	643.11	2.7610D-06
H2US	24	J/KG	1.5368D+06	-1.7745D-03
TQS	25	GRD C	311.33	-7.0435D-07
ROQS	26	KG/CBM	703.38	1.9329D-06
NYS	27	QM/S	1.2605D-07	-6.1046D-17
US	28	M/S	6.4552	-1.7280D-07
RES	29	-	3.2210D+05	-1.0604D-02
LAMS	30	-	1.5014D-02	1.0163D-10
NG	31	-	18.000	0.0
PB	32	M	1.2161D-02	1.4730D-10
BB	33	M	4.0000D-04	0.0
DB	34	M	1.1089D-02	-6.6198D-11
AB	35	QM	1.5101D-05	1.2931D-12
DHB	36	M	2.9276D-03	8.1619D-11
T2UB	37	GRD C	331.31	-3.8534D-07
RO2UB	38	KG/CBM	648.91	3.9597D-07
H2UB	39	J/KG	1.5245D+06	-1.9790D-03
TQB	40	GRD C	310.45	-9.4659D-07
ROQB	41	KG/CBM	705.44	2.5932D-07
NYB	42	QM/S	1.2605D-07	3.3804D-16
UB	43	M/S	6.6936	-8.8267D-08
FB	44	-	1.2721	6.4038D-08
REB	45	-	1.7534D+05	-1.8223D-02
CB	46	-	1.0000	0.0
LAMB	47	-	2.1509D-02	1.8287D-09
QLB	48	W/M	15924.	3.9807D-04



ERGEBNISSE

Q = 3.7054D+09 W  
 K = 0.98418  
 PS = 63.479 BAR  
 TS = 279.34 GRD C  
 P1 = 161.48 BAR  
 T1 = 289.58 GRD C  
 T2 = 326.68 GRD C  
 M = 17408. KG/S  
 NP = 1.8284D+07 W  
 QNT = 1.2750D+09 W  
 QNT/QELO = 0.98073

\*\*\*\*\* ZUSATZ 08.09.1983 \*\*\*\*\*

KS = 0.94000 -  
 ETA = 0.77400 -  
 MS = 16363. KG/S  
 NPEL = 2.3622D+07 W

HETEROGENEOUS REACTOR

LC = 2.1825 M  
 LR = 2.6140 M

SEED

KLS = 1.0000 - 12.09.1983  
 QLS = 19465. W/M  
 PS = 9.5850D-03 M  
 BS = 7.2833D-04 M  
 DS = 7.4000D-03 M  
 PS/DS = 1.2953  
 T2US = 333.09 GRD C  
 US = 6.4552 M/S  
 RES = 3.2210D+05  
 LAMS = 1.5014D-02

BLANKET

KLB = 1.00000 - 12.09.1983  
 QLB = 15924.3 W/M  
 PB = 1.21606D-02 M  
 BB = 4.00000D-04 M  
 DB = 1.10892D-02 M  
 PB/DB = 1.09662  
 T2UB = 331.314 GRD C  
 UB = 6.69356 M/S  
 REB = 175344.  
 LAMB = 2.15095D-02

GESAMT

DP = 3.2246 BAR  
 DPTOT = 3.4445 BAR

\*\*\*\*\* ZUSATZ 08.09.1983 \*\*\*\*\*

DPP = 7.6421 BAR

NG = 18  
 NS = 39107  
 NB = 58809  
 NT = 97916

VM/VF = 0.50771  
CELL : 0.48458

## SEED

## CHF-CALCULATIONS

LC	=	2.1825	M
T1	=	289.58	GRD C
RO1	=	748.79	KG/CBM
P1	=	161.48	BAR
H1	=	1.2808D+06	J/KG
T2	=	333.09	GRD
P2	=	158.26	BAR
ROQ	=	703.38	KG/CBM
U	=	6.4552	M/S
QL	=	19465.	W/M
D	=	7.4000D-03	M
DH	=	6.2897D-03	M
PZUD	=	1.2953	

## EINGABEDATEN

FIAX	=	1.5400	
AK	=	2.3700D+06	
HO	=	1.5880D+06	J/KG
FQ	=	2.1000	
K4	=	0.10000	
NC	=	40	
OP	=	1.1200	
Q10	=	1.7630	
Q20	=	9.1570	
Q40	=	6.5070	
Q1N	=	1.7480	
Q2N	=	7.5400	
Q4N	=	8.7830	
FQN	=	1.8480	

## ERGEBNISSE

X	=	1.5392	
P1/2X	=	1.0205	
LC'	=	2.2273	
RLCR	=	1.964	
RLCR'	=	2.009	
V1	=	0.7000D+00	WSC-2
V2	=	0.49357D+00	EIGENE,ALT
V2	=	0.62284D+00	EIGENE,NEU

OVERPOWER FACTOR : 1.0000

POS X	T(X)	TW	EIGENE,ALT			EDLUND			WSC-2			EIGENE,NEU			
			CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	
0	0.0	324.39	349.49	4.553D+06	2.59	2.52	2.718D+06	1.55	1.39	3.858D+06	2.19	2.08	4.036D+06	2.30	2.20
1	0.05	327.06	349.45	4.295D+06	2.45	2.37	2.602D+06	1.48	1.33	3.700D+06	2.11	2.00	3.839D+06	2.19	2.10
2	0.11	329.73	349.40	4.045D+06	2.33	2.25	2.489D+06	1.43	1.28	3.541D+06	2.04	1.93	3.645D+06	2.10	2.00
3	0.16	332.36	349.35	3.804D+06	2.22	2.14	2.381D+06	1.39	1.24	3.382D+06	1.98	1.87	3.454D+06	2.02	1.93
4	0.22	334.94	349.29	3.569D+06	2.13	2.05	2.275D+06	1.36	1.21	3.223D+06	1.92	1.82	3.265D+06	1.95	1.86
5	0.27	337.46	349.24	3.339D+06	2.05	1.97	2.172D+06	1.33	1.19	3.062D+06	1.88	1.78	3.078D+06	1.89	1.80
6	0.33	339.90	349.18	3.115D+06	1.98	1.90	2.070D+06	1.31	1.18	2.900D+06	1.84	1.75	2.892D+06	1.84	1.76
7	0.38	342.25	349.11	2.894D+06	1.92	1.84	1.969D+06	1.30	1.17	2.736D+06	1.81	1.73	2.707D+06	1.79	1.72
8	0.44	344.50	349.04	2.677D+06	1.87	1.79	1.869D+06	1.30	1.18	2.569D+06	1.79	1.71	2.522D+06	1.76	1.69
9	0.49	346.62	348.97	2.463D+06	1.82	1.76	1.769D+06	1.31	1.19	2.398D+06	1.77	1.70	2.336D+06	1.73	1.66
10	0.55	348.62	348.89	2.250D+06	1.78	1.72	1.668D+06	1.32	1.21	2.225D+06	1.76	1.70	2.150D+06	1.70	1.65
11	0.60	350.47	348.81	2.039D+06	1.75	1.70	1.566D+06	1.34	1.25	2.046D+06	1.76	1.71	1.962D+06	1.68	1.64
12	0.65	352.17	348.72	1.828D+06	1.72	1.68	1.461D+06	1.38	1.30	1.863D+06	1.76	1.72	1.772D+06	1.67	1.63
13	0.71	353.70	348.63	1.618D+06	1.70	1.67	1.354D+06	1.43	1.38	1.674D+06	1.76	1.74	1.579D+06	1.66	1.63
14	0.76	355.06	348.52	1.407D+06	1.69	1.66	1.242D+06	1.49	1.48	1.479D+06	1.78	1.77	1.383D+06	1.66	1.64
15	0.82	356.24	348.41	1.195D+06	1.68	1.66	1.124D+06	1.58	1.63	1.276D+06	1.79	1.80	1.183D+06	1.66	1.66
16	0.87	357.22	348.29	9.811D+05	1.68	1.67	9.982D+05	1.71	1.88	1.065D+06	1.82	1.85	9.783D+05	1.67	1.68
17	0.93	358.02	348.14	7.649D+05	1.68	1.68	8.610D+05	1.89	2.36	8.444D+05	1.85	1.90	7.684D+05	1.68	1.71
18	0.98	358.61	347.17	5.456D+05	1.68	0.0	7.063D+05	2.18	0.0	6.127D+05	1.89	0.0	5.522D+05	1.70	0.0
19	1.04	359.01	345.06	3.225D+05	1.69	0.0	5.213D+05	2.74	0.0	3.686D+05	1.94	0.0	3.290D+05	1.73	0.0
20	1.09	359.19	342.78	9.486D+04	1.71	0.0	2.603D+05	4.69	0.0	1.104D+05	1.99	0.0	9.753D+04	1.76	0.0

MINIMALWERTE

CORRELATION	SMMIN	X	POS			
EIGENE,ALT	1.6759	0.87302	16	1.6622	0.76389	14
EDLUND	1.3021	0.43651	8	1.1744	0.38195	7
WSC-2	1.7566	0.60020	11	1.7029	0.54564	10
EIGENE,NEU	1.6608	0.76389	14	1.6316	0.65476	12

OVERPOWER FACTOR : 1.1200

POS X	T(X)	TW	EIGENE,ALT			EDLUND			WSC-2			EIGENE,NEU			
			CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	
0	0.0	328.56	349.49	4.553D+06	2.31	2.25	2.718D+06	1.38	1.24	3.858D+06	1.96	1.86	4.036D+06	2.05	1.97
1	0.05	331.56	349.45	4.295D+06	2.19	2.12	2.602D+06	1.32	1.19	3.700D+06	1.88	1.79	3.839D+06	1.95	1.87
2	0.11	334.54	349.40	4.045D+06	2.08	2.01	2.489D+06	1.28	1.15	3.541D+06	1.82	1.72	3.645D+06	1.87	1.79
3	0.16	337.49	349.35	3.804D+06	1.98	1.91	2.381D+06	1.24	1.11	3.382D+06	1.76	1.67	3.454D+06	1.80	1.72
4	0.22	340.38	349.29	3.569D+06	1.90	1.83	2.275D+06	1.21	1.08	3.223D+06	1.72	1.63	3.265D+06	1.74	1.66
5	0.27	343.20	349.24	3.339D+06	1.83	1.76	2.172D+06	1.19	1.06	3.062D+06	1.68	1.59	3.078D+06	1.69	1.61
6	0.33	345.94	349.18	3.115D+06	1.77	1.70	2.070D+06	1.17	1.05	2.900D+06	1.64	1.56	2.892D+06	1.64	1.57
7	0.38	348.57	349.11	2.894D+06	1.71	1.65	1.969D+06	1.16	1.05	2.736D+06	1.62	1.54	2.707D+06	1.60	1.53
8	0.44	351.09	349.04	2.677D+06	1.67	1.60	1.869D+06	1.16	1.05	2.569D+06	1.60	1.53	2.522D+06	1.57	1.51
9	0.49	353.47	348.97	2.463D+06	1.63	1.57	1.769D+06	1.17	1.06	2.398D+06	1.58	1.52	2.336D+06	1.54	1.48
10	0.55	355.70	348.89	2.250D+06	1.59	1.54	1.668D+06	1.18	1.08	2.225D+06	1.57	1.52	2.150D+06	1.52	1.47
11	0.60	357.78	348.81	2.039D+06	1.56	1.52	1.566D+06	1.20	1.12	2.046D+06	1.57	1.53	1.962D+06	1.50	1.46
12	0.65	359.68	348.72	1.828D+06	1.54	1.50	1.461D+06	1.23	1.16	1.863D+06	1.57	1.54	1.772D+06	1.49	1.46
13	0.71	361.39	348.63	1.618D+06	1.52	1.49	1.354D+06	1.27	1.23	1.674D+06	1.57	1.55	1.579D+06	1.49	1.46
14	0.76	362.92	348.52	1.407D+06	1.51	1.48	1.242D+06	1.33	1.32	1.479D+06	1.59	1.58	1.383D+06	1.48	1.47
15	0.82	364.23	348.41	1.195D+06	1.50	1.48	1.124D+06	1.41	1.46	1.276D+06	1.60	1.61	1.183D+06	1.49	1.48
16	0.87	365.34	348.29	9.811D+05	1.50	1.49	9.982D+05	1.52	1.68	1.065D+06	1.62	1.65	9.783D+05	1.49	1.50
17	0.93	366.23	348.14	7.649D+05	1.50	1.50	8.610D+05	1.69	2.11	8.444D+05	1.65	1.70	7.684D+05	1.50	1.53
18	0.98	366.90	348.06	5.456D+05	1.50	0.0	7.063D+05	1.94	0.0	6.127D+05	1.69	0.0	5.522D+05	1.52	0.0
19	1.04	367.34	347.84	3.225D+05	1.51	0.0	5.213D+05	2.44	0.0	3.686D+05	1.73	0.0	3.290D+05	1.54	0.0
20	1.09	367.55	347.47	9.486D+04	1.53	0.0	2.603D+05	4.19	0.0	1.104D+05	1.78	0.0	9.753D+04	1.57	0.0

MINIMALWERTE

CORRELATION	SMMIN	X	POS			
EIGENE,ALT	1.4964	0.87302	16	1.4841	0.76389	14
EDLUND	1.1626	0.43651	8	1.0486	0.38195	7
WSC-2	1.5684	0.60020	11	1.5205	0.54564	10
EIGENE,NEU	1.4828	0.76389	14	1.4568	0.65476	12

BLANKET

CHF-CALCULATIONS

LC	=	2.1825	M
T1	=	289.58	GRD C
R01	=	748.79	KG/CBM
P1	=	161.48	BAR
H1	=	1.2808D+06	J/KG
T2	=	331.31	GRD
P2	=	158.26	BAR
ROQ	=	705.44	KG/CBM
U	=	6.6936	M/S
QL	=	15924.	W/M
D	=	1.1089D-02	M
DH	=	2.9276D-03	M
PZUD	=	1.0966	

EINGABEDATEN

FIAX	=	1.5400	
AK	=	2.3700D+06	
H0	=	1.5880D+06	J/KG
FQ	=	2.1000	
K4	=	0.10000	
NC	=	40	
OP	=	1.1200	
Q10	=	1.7630	
Q20	=	9.1570	
Q40	=	6.5070	
Q1N	=	1.7480	
Q2N	=	7.5400	
Q4N	=	8.7830	
FQN	=	1.8480	

ERGEBNISSE

X	=	1.5392	
P1/2X	=	1.0205	
LC'	=	2.2273	
RLCR	=	1.964	
RLCR'	=	2.009	
V1	=	0.7000D+00	WSC-2
V2	=	0.47975D+00	EIGENE,ALT
V2	=	0.57310D+00	EIGENE,NEU

OVERPOWER FACTOR : 1.0000

POS X	T(X)	TW	EIGENE,ALT			EDLUND			WSC-2			EIGENE,NEU			
			CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	
0	0.0	322.97	330.21	2.401D+06	2.50	2.41	1.794D+06	1.87	1.69	1.683D+06	1.75	1.65	2.077D+06	2.16	2.06
1	0.05	325.54	332.05	2.278D+06	2.38	2.29	1.717D+06	1.79	1.61	1.626D+06	1.70	1.59	1.987D+06	2.08	1.97
2	0.11	328.09	333.78	2.158D+06	2.28	2.18	1.643D+06	1.73	1.55	1.568D+06	1.65	1.55	1.898D+06	2.00	1.90
3	0.16	330.61	335.40	2.040D+06	2.18	2.09	1.572D+06	1.68	1.50	1.509D+06	1.62	1.52	1.808D+06	1.94	1.84
4	0.22	333.09	336.89	1.925D+06	2.10	2.01	1.502D+06	1.64	1.47	1.449D+06	1.58	1.49	1.719D+06	1.88	1.78
5	0.27	335.51	338.25	1.810D+06	2.03	1.95	1.434D+06	1.61	1.44	1.387D+06	1.56	1.47	1.630D+06	1.83	1.74
6	0.33	337.85	339.48	1.697D+06	1.98	1.89	1.368D+06	1.59	1.43	1.324D+06	1.54	1.46	1.540D+06	1.79	1.71
7	0.38	340.11	340.56	1.585D+06	1.92	1.84	1.301D+06	1.58	1.42	1.259D+06	1.53	1.45	1.450D+06	1.76	1.68
8	0.44	342.26	341.49	1.474D+06	1.88	1.81	1.235D+06	1.58	1.43	1.192D+06	1.52	1.45	1.358D+06	1.73	1.66
9	0.49	344.30	342.26	1.362D+06	1.84	1.78	1.169D+06	1.58	1.44	1.122D+06	1.52	1.46	1.265D+06	1.71	1.65
10	0.55	346.21	342.87	1.251D+06	1.81	1.75	1.103D+06	1.60	1.47	1.049D+06	1.52	1.47	1.171D+06	1.70	1.64
11	0.60	347.99	343.33	1.139D+06	1.79	1.74	1.036D+06	1.63	1.52	9.737D+05	1.53	1.49	1.074D+06	1.69	1.64
12	0.65	349.62	343.62	1.027D+06	1.77	1.73	9.668D+05	1.67	1.58	8.946D+05	1.55	1.52	9.758D+05	1.69	1.65
13	0.71	351.09	343.75	9.129D+05	1.76	1.73	8.959D+05	1.73	1.67	8.114D+05	1.57	1.55	8.748D+05	1.69	1.66
14	0.76	352.39	343.71	7.978D+05	1.76	1.73	8.221D+05	1.81	1.80	7.237D+05	1.59	1.60	7.708D+05	1.70	1.69
15	0.82	353.52	343.51	6.810D+05	1.75	1.74	7.445D+05	1.92	1.98	6.308D+05	1.62	1.65	6.634D+05	1.71	1.71
16	0.87	354.47	343.15	5.619D+05	1.76	1.76	6.616D+05	2.07	2.29	5.320D+05	1.66	1.72	5.521D+05	1.73	1.75
17	0.93	355.23	342.63	4.403D+05	1.77	1.79	5.710D+05	2.29	2.87	4.265D+05	1.71	1.79	4.364D+05	1.75	1.80
18	0.98	355.80	341.95	3.157D+05	1.78	0.0	4.688D+05	2.65	0.0	3.131D+05	1.77	0.0	3.158D+05	1.78	0.0
19	1.04	356.18	341.11	1.876D+05	1.80	0.0	3.465D+05	3.33	0.0	1.908D+05	1.83	0.0	1.894D+05	1.82	0.0
20	1.09	356.36	340.12	5.549D+04	1.83	0.0	1.736D+05	5.73	0.0	5.792D+04	1.91	0.0	5.656D+04	1.87	0.0

MINIMALWERTE

CORRELATION	SMMIN	X	POS			
EIGENE,ALT	1.7541	0.81845	15	1.7290	0.70933	13
EDLUND	1.5764	0.43651	8	1.4217	0.38195	7
WSC-2	1.5187	0.49107	9	1.4511	0.38195	7
EIGENE,NEU	1.6859	0.65476	12	1.6419	0.54564	10

OVERPOWER FACTOR : 1.1200

POS X	T(X)	TW	EIGENE, ALT			EDLUND			WSC-2			EIGENE, NEU			
			CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	CHF	SM	SMLWR	
0	0.0	326.97	333.15	2.401D+06	2.23	2.15	1.794D+06	1.67	1.50	1.683D+06	1.57	1.47	2.077D+06	1.93	1.84
1	0.05	329.85	335.21	2.278D+06	2.13	2.04	1.717D+06	1.60	1.44	1.626D+06	1.52	1.42	1.987D+06	1.85	1.76
2	0.11	332.71	337.16	2.158D+06	2.03	1.95	1.643D+06	1.55	1.39	1.568D+06	1.48	1.38	1.898D+06	1.79	1.70
3	0.16	335.54	338.99	2.040D+06	1.95	1.87	1.572D+06	1.50	1.34	1.509D+06	1.44	1.35	1.808D+06	1.73	1.64
4	0.22	338.31	340.70	1.925D+06	1.88	1.80	1.502D+06	1.47	1.31	1.449D+06	1.41	1.33	1.719D+06	1.68	1.59
5	0.27	341.02	342.26	1.810D+06	1.82	1.74	1.434D+06	1.44	1.29	1.387D+06	1.39	1.31	1.630D+06	1.64	1.55
6	0.33	343.64	343.69	1.697D+06	1.76	1.69	1.368D+06	1.42	1.27	1.324D+06	1.38	1.30	1.540D+06	1.60	1.52
7	0.38	346.17	344.96	1.585D+06	1.72	1.65	1.301D+06	1.41	1.27	1.259D+06	1.36	1.30	1.450D+06	1.57	1.50
8	0.44	348.58	346.06	1.474D+06	1.68	1.61	1.235D+06	1.41	1.27	1.192D+06	1.36	1.30	1.358D+06	1.55	1.48
9	0.49	350.87	347.01	1.362D+06	1.65	1.59	1.169D+06	1.41	1.29	1.122D+06	1.36	1.30	1.265D+06	1.53	1.47
10	0.55	353.01	347.78	1.251D+06	1.62	1.57	1.103D+06	1.43	1.31	1.049D+06	1.36	1.31	1.171D+06	1.52	1.47
11	0.60	355.00	348.39	1.139D+06	1.60	1.55	1.036D+06	1.45	1.35	9.737D+05	1.37	1.33	1.074D+06	1.51	1.47
12	0.65	356.82	348.46	1.027D+06	1.58	1.55	9.668D+05	1.49	1.41	8.946D+05	1.38	1.36	9.758D+05	1.51	1.47
13	0.71	358.47	348.37	9.129D+05	1.57	1.54	8.959D+05	1.54	1.49	8.114D+05	1.40	1.39	8.748D+05	1.51	1.49
14	0.76	359.93	348.27	7.978D+05	1.57	1.55	8.221D+05	1.61	1.60	7.237D+05	1.42	1.43	7.708D+05	1.51	1.50
15	0.82	361.19	348.17	6.810D+05	1.57	1.56	7.445D+05	1.71	1.77	6.308D+05	1.45	1.47	6.634D+05	1.53	1.53
16	0.87	362.25	348.06	5.619D+05	1.57	1.57	6.616D+05	1.85	2.04	5.320D+05	1.49	1.53	5.521D+05	1.54	1.56
17	0.93	363.11	347.93	4.403D+05	1.58	1.60	5.710D+05	2.05	2.57	4.265D+05	1.53	1.60	4.364D+05	1.56	1.60
18	0.98	363.75	347.80	3.157D+05	1.59	0.0	4.688D+05	2.36	0.0	3.131D+05	1.58	0.0	3.158D+05	1.59	0.0
19	1.04	364.17	347.04	1.876D+05	1.61	0.0	3.465D+05	2.98	0.0	1.908D+05	1.64	0.0	1.894D+05	1.63	0.0
20	1.09	364.37	346.11	5.549D+04	1.64	0.0	1.736D+05	5.12	0.0	5.792D+04	1.71	0.0	5.656D+04	1.67	0.0

MINIMALWERTE

CORRELATION	SMMIN	X	POS
EIGENE, ALT	1.5661	0.81845	15
EDLUND	1.4075	0.43651	8
WSC-2	1.3560	0.49107	9
EIGENE, NEU	1.5053	0.65476	12



## 6. Utility Programs

All main results of a run are appended to an existing data set, so that the results of many runs can be accumulated in this data pool. To retrieve and present these results some utility programs are necessary.

### 6.1 Creating the Data Pool

To create and initiate the data pool, the program INIT must be used as demonstrated in the following example:

```
//PROJECTL JOB (.....,.....,.....),.....,TIME=(,30),MSGCLASS=A
// EXEC PGM=IEFBR14
//DD1 DD DSN=PROJECT.APWRH.DATA,DISP=(OLD,DELETE)
// EXEC PGM=INIT
//STEPLIB DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//FT08F001 DD DSN=PROJECT.APWRH.DATA,UNIT=DISK,VOL=SER=BAT00D,
// DCB=(LRECL=2996,RECFM=VBS,BLKSIZE=3000),
// DISP=(NEW,CATLG),SPACE=(CYL,(10,10))
```

### 6.2 Listing the Results

With the program LIST accumulated results may be listed in a sorted manner as shown in [1]. This program requests as input first the unit number assigned to the data pool, and then one or more group indicators in successive lines as shown and described.

```
//PROJECTL JOB (.....,.....,.....),.....,TIME=(,30),MSGCLASS=A
//LIST EXEC PGM=LIST
//STEPLIB DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//FT05F001 DD *
8      EINGABEEINHEIT PROJECT.APWRS.DATA
2
3      DP-ITER.(1), HOMOGEN(2), HETEROGEN(3)
//FT06F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT08F001 DD DISP=SHR,DSN=PROJECT.APWRS.DATA
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
```

### 6.3 Deleting Entries

With the program DELT the results of certain runs may be deleted from the data pool. To do this the original data set is copied to a new one by excluding the specified entries. As first input line the unit numbers of the input and output data sets are required. Then in consecutive lines as many entry numbers as desired may be marked for exclusion. As the numbers of the entries (the record number in the data set) are changed during deletion, it is useful to start with the greatest number going down to the lowest one. In the following example deleting is demonstrated.

```
//PROJECTD JOB (.....,.....,.....),.....,TIME=(,30),MSGCLASS=A
//DELT EXEC PGM=DELT
//STEPLIB DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//FT05F001 DD *
8,18      EINGABEEINHEIT PROJECT.APWRD.DATA,AUSGABEEINHEIT
88
87
32
//FT06F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT08F001 DD DISP=SHR,DSN=PROJECT.APWRS.DATA
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT18F001 DD DISP=SHR,DSN=PROJECT.APWRH.DATA
```

### 6.4 Listing a Specified Entry

With the program OUT1 one or more entries may be listed as they are present in the data pool. The first input to this program is again the unit number. Then one or more entry numbers may be specified in consecutive lines. The following example demonstrates the usage of OUT1:

```
//PROJECTD JOB (.....,.....,.....),.....,TIME=(,30),MSGCLASS=A
//OUT1 EXEC PGM=OUT1
//STEPLIB DD DISP=SHR,DSN=TSO090.HADA.LOAD
//FT05F001 DD *
8          EINGABEEINHEIT PROJECT.APWRD.DATA,AUSGABEEINHEIT
31
75
//FT06F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT08F001 DD DISP=SHR,DSN=PROJECT.APWRD.DATA
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT18F001 DD DISP=SHR,DSN=PROJECT.APWRH.DATA
```

## 6.5 Compressing the Data Pool

The program COMP is used to omit entries with the same input data. As DELT this program uses two different data sets for input and output, so that the original data set remains unaffected. The program requires as input only the unit numbers assigned to the data pools.

```
//PROFECTC JOB (.....,.....,.....),.....,TIME=(,30),MSGCLASS=A
//COMP EXEC PGM=COMP
//STEPLIB DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//FT05F001 DD *
8,18      EINGABEEINHEIT PROJECT.APWRD.DATA,AUSGABEEINHEIT
//FT06F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT08F001 DD DISP=SHR,DSN=PROJECT.APWRS.DATA
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT18F001 DD DISP=SHR,DSN=PROJECT.APWRH.DATA
```

## 6.6 Plotting the Results

With the program PLOT specified entries or group of entries may be selected as input for the plot routines. This program needs Calcomp/Versatec plotter software and it is therefore restricted in usage. The following example shows the different commands and their meaning. The presented input stream was used to plot the figures in [1].

```
//PROJECTP JOB (.....,.....,.....),.....,TIME=(,30),MSGCLASS=A
//*MAIN LINES=50
//PLOT EXEC PGM=PLOT
//STEPLIB DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//PLOTWK01 DD UNIT=SYSSQ,SPACE=(CYL,(10,5))
//PLOTWK02 DD UNIT=SYSSQ,SPACE=(CYL,(10,5))
//VECTR1 DD UNIT=SYSSQ,SPACE=(CYL,(10,5)),DISP=(MOD,PASS),
//      DSN=&&VECTR1
//VECTR2 DD UNIT=SYSSQ,SPACE=(CYL,(10,5)),DISP=(MOD,PASS),
//      DSN=&&VECTR2
//PLOTLOG DD SYSOUT=*
//COMM DD SYSOUT=*
```

```
//FT01F001 DD *
KOM
KOM
KOM          BESCHREIBUNG DER EINGABEDATEN
KOM
KOM  INI PLOTTERNUMMER, XMAX, YMAX, PLOTFAKTOR
KOM      0,1,2,3,4,... 0 = DUMMY-PLOT
KOM                        1 = BILDSCHIRM GA
KOM                        2 = BILDSCHIRM T4015
KOM                        3 = SPEICHERBILDSCHIRM KSG
KOM                        4 = CALCOMP, STATOS, XYNETICS, VERSATEC
KOM                        >4 = PLOTAUSGABE ERFOLGT UEBER EINHEIT 9
KOM      XMAX          ZEICHNUNGSLAENGE IN CM (FUER FAKTOR 1)
KOM      YMAX          ZEICHNUNGSHOEHE IN CM (FUER FAKTOR 1)
KOM      PLOTFAKTOR   1  PLOTTEREINHEIT = 1CM
KOM                    <1  VERKLEINERUNG
KOM                    >1  VERGROESSERUNG
KOM
KOM
KOM  NPL
KOM
KOM
KOM  GRP INDEX, TEXT1, TEXT2
KOM      INDEX          GRUPPENINDEX
KOM                        1  HOMOGENE REAKTOREN
KOM                        2  HETEROGENE REAKTOREN
KOM                        3  1 UND 2
KOM
KOM
KOM  FIG NUMMER, TEXT1, TEXT2
KOM      NUMMER          ABBILDUNGSNUMMER
KOM
KOM
KOM  PAR NPAR, NAME=, EINHEIT, UMRECHNUNGSFAKTOR DARSTELLUNG/INTERN
KOM      NPAR          INDEX DES PARAMETERWERTS
KOM
KOM
KOM  XAX TEXT , EINHEIT, UMRECHNUNGSFAKTOR, STARTWERT, ENDWERT, ACHSENLAENGE
KOM      BEISPIEL      1.E2 CM/M WERT IN M WIRD IN CM DARGESTELLT.
KOM                        DIE ACHSE BEGINNT BEI 0.7 CM
KOM                        UND ENDET BEI 1.2 CM.
KOM                        DIE GEZEICHNETE ACHSENLAENGE IST 10 CM.
KOM
KOM
KOM  YAX TEXT , EINHEIT, UMRECHNUNGSFAKTOR, STARTWERT, ENDWERT, ACHSENLAENGE
KOM
KOM
KOM  TXT X-KOORD. , Y-KOORD. , HOEHE, TEXT, WINKEL
KOM
KOM
KOM  PLT TYP, OPTION, NX, NY
KOM      TYP :   DPI          DP-ITERATION
KOM                HOM        HOMOGENER KERN
KOM                HET        HETEROGENER KERN
KOM      OPTION : POW        KONSTANTE PUMPLEISUNG
KOM                CHR        KONSTANTE PUMPENCHARAKTERISTIK
KOM                NX         INDEX DES ABSZISSENWERTES
KOM                NY         INDEX DES ORDINATENWERTES
KOM
```

KOM  
KOM SYM TYP,OPTION,NX,NY,NSYM  
KOM  
KOM  
KOM ADI NN,NN WERTEPAARE IN INTERNEN EINHEITEN  
KOM  
KOM  
KOM ADD NN,NN WERTEPAARE IN DARSTELLUNGSEINHEITEN  
KOM  
KOM  
KOM ADZ NN,NN WERTEPAARE IN PLOTTEREINHEITEN  
KOM  
KOM  
KOM MIT FIG WIRD EIN EINZELPLOT EROEFFNET, DIESES KOMMANDO  
KOM MUSS DESHALB STETS ALS ERSTES ERSCHEINEN.  
KOM DIE KOMMANDOS PAR,XAX,YAX KOENNEN IN BELIEBIGER REIHEN-  
KOM FOLGE ANGESCHLOSSEN WERDEN, FEHLT DAS KOMMANDO PAR, SO  
KOM WERDEN ALLE DATEN FUER DIE AUSGEWAELTE DATENGRUPPE DAR-  
KOM GESTELLT (ALS EINE KURVE).  
KOM DIE GRUPPE PLT,ADI,ADD,ADZ,SYM SCHLIESST IN BELIEBIGER  
KOM REIHENFOLGE DIE KOMMANDOSEQUENZ AB. DAMIT EIN SINNVOLLER  
KOM PLOT ERSTELLT WERDEN KANN, MUSS MINDESTENS EINES DAVON  
KOM VORHANDEN SEIN.  
KOM  
KOM EIN NEUES EINZELBILD KANN DURCH FIG ODER DURCH INI  
KOM EROEFFNET WERDEN, WOBEI INI NUR DANN ANZUGEBEN IST, WENN  
KOM DIE GRUNDPARAMETER GEAENDERT WERDEN SOLLEN.  
KOM  
KOM DARSTELLUNG DER ERGEBNISSE  
KOM  
KOM  
KOM 1. BILD QELNET VS. D MIT P ALS PARAMETER  
KOM  
KOM  
PRT  
GRP 1,HOMOGENEOUS CORE,CONSTANT PUMP CHARACTERISTICS  
PAR 15, P=,CM,1.E2  
XAX ROD DIAMETER D,CM,1.E2,0.7,1.2,10.  
YAX NET PLANT ELECTRICAL POWER QELNET,MW,1.E-6,800.,1300.,10.  
PLT HOM,CHR,16,42  
NPL  
YAX DNB RATIO,-,1.,1.2,1.7,10.  
PLT HOM,CHR,16,101  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.  
ADD 4,0.7,1.301,1.2,1.301,1.2,1.299,0.7,1.299  
NPL  
YAX DNB RATIO WITH CONTROL ROD,-,1.,1.2,1.7,10.  
PLT HOM,CHR,16,104  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.  
ADD 4,0.7,1.301,1.2,1.301,1.2,1.299,0.7,1.299  
NPL  
YAX DNB RATIO,-,1.,1.1,1.6,10.  
PLT HOM,CHR,16,127  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.  
ADD 4,0.7,1.301,1.2,1.301,1.2,1.299,0.7,1.299

NPL  
YAX DNB RATIO WITH CONTROL ROD,-,1.,1.1,1.6,10.  
PLT HOM,CHR,16,130  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.  
ADD 4,0.7,1.301,1.2,1.301,1.2,1.299,0.7,1.299  
NPL  
YAX INLET TEMPERATURE T1,GRD C,1.,260.,310.,10.  
PLT HOM,CHR,16,38  
NPL  
YAX OUTLET TEMPERATURE T2,GRD C,1.,316.,326.,10.  
PLT HOM,CHR,16,39  
NPL  
YAX MASS FLOW RATE M,KG/S,1.,10000.,20000.,10.  
PLT HOM,CHR,16,40  
NPL  
YAX PUMPING POWER NP,MW,1.E-6,15.,20.,10.  
PLT HOM,CHR,16,41  
NPL  
YAX WATER TO FUEL ROD VOLUME RATIO VM/VF,-,1.,0.,1.,10.  
PLT HOM,CHR,16,29  
NPL  
YAX CORE FRICTION PRESSURE DROP DP,BAR,1.,0.,10.,10.  
PLT HOM,CHR,16,50  
NPL  
YAX ROD LINEAR POWER QL,W/CM,1.E-2,100.,200.,10.  
PLT HOM,CHR,16,26  
NPL  
YAX CORE POWER DENSITY QV,W/CM\*\*3,1.E-6,100.,300.,10.  
PLT HOM,CHR,16,27  
NPL  
YAX VELOCITY U,M/S,1.,5.,10.,10.  
PLT HOM,CHR,16,47  
NPL  
YAX POSITION OF INCIPIENT LOCAL BOILING,CM,1.E2,0.,200.,10.  
PLT HOM,CHR,16,107  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.  
NPL  
YAX POSITION OF INCIPIENT LOCAL BOILING,CM,1.E2,0.,100.,10.  
PLT HOM,CHR,16,133  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.  
NPL  
YAX CORE HEIGHT LC,CM,1.E2,120.,320.,10.  
PLT HOM,CHR,16,44  
GRP 2,HETEROGENEOUS CORE,CONSTANT PUMP CHARACTERISTICS  
PAR 48, DS=,CM,1.E2  
XAX SEED POWER DENSITY QVS,W/CM\*\*3,1.E-6,100.,300.,10.  
YAX NET PLANT ELECTRICAL POWER QELNET,MW,1.E-6,800.,1300.,10.  
PLT HET,CHR,19,41  
NPL  
YAX DNB RATIO SEED,-,1.,1.5,2.0,10.  
PLT HET,CHR,19,116  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.  
NPL  
YAX DNB RATIO SEED WITH CONTROL ROD,-,1.,1.5,2.0,10.  
PLT HET,CHR,19,119  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.

NPL  
YAX DNB RATIO SEED,-,1.,1.3,1.8,10.  
PLT HET,CHR,19,142  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.  
NPL  
YAX DNB RATIO SEED WITH CONTROL ROD,-,1.,1.3,1.8,10.  
PLT HET,CHR,19,145  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.  
NPL  
YAX DNB RATIO BLANKET,-,1.,1.3,1.8,10.  
PLT HET,CHR,19,198  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.  
NPL  
YAX DNB RATIO BLANKET WITH CONTROL ROD,-,1.,1.3,1.8,10.  
PLT HET,CHR,19,201  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.  
NPL  
YAX DNB RATIO BLANKET,-,1.,1.1,1.6,10.  
PLT HET,CHR,19,224  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.  
ADD 4,100.,1.301,300.,1.301,300.,1.299,100.,1.299  
NPL  
YAX DNB RATIO BLANKET WITH CONTROL ROD,-,1.,1.1,1.6,10.  
PLT HET,CHR,19,227  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.  
ADD 4,100.,1.301,300.,1.301,300.,1.299,100.,1.299  
NPL  
YAX INLET TEMPERATURE T1,GRD C,1.,260.,310.,10.  
PLT HET,CHR,19,37  
NPL  
YAX OUTLET TEMPERATURE T2,GRD C,1.,316.,326.,10.  
PLT HET,CHR,19,38  
NPL  
YAX MASS FLOW RATE M,KG/S,1.,10000.,20000.,10.  
PLT HET,CHR,19,39  
NPL  
YAX PUMPING POWER NP,MW,1.E-6,15.,20.,10.  
PLT HET,CHR,19,40  
NPL  
YAX WATER TO FUEL ROD VOLUME RATIO VM/VF,-,1.,0.,1.5,10.  
PLT HET,CHR,19,65  
NPL  
YAX CORE FRICTION PRESSURE DROP DP,BAR,1.,0.,10.,10.  
PLT HET,CHR,19,63  
NPL  
YAX POSITION OF INCIPIENT LOCAL BOILING SEED,CM,1.E2,0.,200.,10.  
PLT HET,CHR,19,122  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.  
NPL  
YAX POSITION OF INCIPIENT LOCAL BOILING SEED,CM,1.E2,0.,100.,10.  
PLT HET,CHR,19,148  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.  
NPL  
YAX POSITION OF INCIPIENT LOCAL BOILING BLANKET,CM,1.E2,0.,200.,10.  
PLT HET,CHR,19,204,10  
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1,0.

```
NPL
YAX POSITION OF INCIPIENT LOCAL BOILING BLANKET,CM,1.E2,0.,100.,10.
PLT HET,CHR,19,230
TXT 8.,-2.5,.21,OVERPOWER FACTOR 1.12,0.
NPL
YAX CORE HEIGHT LC,CM,1.E2,100.,500.,10.
PLT HET,CHR,19,43
NPL
YAX PITCH BLANKET PB,CM,1.E2,.8,1.8,10.
PLT HET,CHR,19,55
NPL
YAX PITCH SEED PS,CM,1.E2,.6,1.6,10.
PLT HET,CHR,19,46
NPL
YAX ROD DIAMETER BALNKET DB,CM,1.E2,.8,1.8,10.
PLT HET,CHR,19,57
NPL
YAX PITCH TO DIAMETER RATIO SEED PS/DS,-,1.,1.,1.5,10.
PLT HET,CHR,19,49
NPL
YAX PITCH TO DIAMETER RATIO BLANKET PB/DB,-,1.,.9,1.4,10.
PLT HET,CHR,19,58
NPL
YAX ROD LINEAR POWER SEED QLS,W/CM,1.E-2,150.,250.,10.
PLT HET,CHR,19,28
NPL
YAX ROD LINEAR POWER BLANKET QLB,W/CM,1.E-2,100.,200.,10.
PLT HET,CHR,19,54
NPL
YAX VELOCITY BLANKET UB,M/S,1.,5.,10.,10.
PLT HET,CHR,19,60
NPL
YAX VELOCITY SEED US,M/S,1.,6.,8.5,10.
PLT HET,CHR,19,51
GRP 3
PAR
XAX NET PLANT ELECTRICAL POWER QELNET,MW,1.E-6,800.,1300.,10.
YAX WATER TO FUEL ROD VOLUME RATIO VM/VF,-,1.,0.,1.,10.
PLS HOM,CHR,42,29,2
PLS HET,CHR,41,65,10
SYM 8.,2.,.21,2,0.
TXT 8.5,1.9,.21,HOM.,0.
SYM 8.,1.5,.21,10,0.
TXT 8.5,1.4,.21,HET.,0.
//FT05F001 DD *
8,1,0
//FT06F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT08F001 DD DISP=SHR,DSN=PROJECT.APWRS.DATA
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT20F001 DD DISP=(,DELETE),UNIT=SYSSQ,SPACE=(1,1),
//          DCB=(RECFM=FB,LRECL=80,BLKSIZE=3120)
//PLOT Parm DD *
&PLOT XMAX=300. &END
//VERS EXEC SVPLOT
```



## 6.7 Listing the Contents

With the program SHOW selected Variables of a specified entry may be listed. The following example demonstrates the usage:

```
//PROJECTS JOB (.....,.....,.....),.....,TIME=(,30),MSGCLASS=A
//SHOW EXEC PGM=SHOW
//STEPLIB DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//FT05F001 DD *
8      EINGABEEINHEIT PROJECT.APWRS.DATA
48     REAKTORNUMMER
XF 149,230
//FT06F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
//FT08F001 DD DISP=SHR,DSN=PROJECT.APWRS.DATA
//FT09F001 DD SYSOUT=*,DCB=(RECFM=FBA,LRECL=133,BLKSIZE=3857)
```

## 7. Installing the Programs

All programs, subroutines, and functions are copied to the tape each in a separate file. The following shows how the program library HADA.LOAD is to be generated.

```
//PROJECTG JOB (....,....,.....),....,TIME=1,MSGCLASS=N
//*MAIN LINES=20
//*****
//INPUTO EXEC F7CL,PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(INPUTO)
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(INPUT1)
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(INPUT2)
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
  ALIAS INPUT1,INPUT2
  NAME INPUTO(R)
//*****
//COMPRS EXEC F7CL,PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(COMPRS)
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
  NAME COMPRS(R)
//*****
//IVGL EXEC F7CL,PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(IVGL)
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
  NAME IVGL(R)
//*****
//OUTPUT EXEC F7CL,PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(OUTPUT)
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
  NAME OUTPUT(R)
```

```
//*****  
//DELETE EXEC F7CL,PARM.L='NCAL'  
//C.SYSPRINT DD SYSOUT=N  
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(DELETE)  
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD  
//L.SYSPRINT DD SYSOUT=H  
//L.SYSIN DD *  
NAME DELETE(R)  
//*****  
//OUTLST EXEC F7CL,PARM.L='NCAL'  
//C.SYSPRINT DD SYSOUT=N  
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(OUTLST)  
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD  
//L.SYSPRINT DD SYSOUT=H  
//L.SYSIN DD *  
NAME OUTLST(R)  
//*****  
//OUTHOM EXEC F7CL,PARM.L='NCAL'  
//C.SYSPRINT DD SYSOUT=N  
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(OUTHOM)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(OUTHET)  
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD  
//L.SYSPRINT DD SYSOUT=H  
//L.SYSIN DD *  
ALIAS OUTHET  
NAME OUTHOM(R)  
//*****  
//OUTLIN EXEC F7CL,PARM.L='NCAL'  
//C.SYSPRINT DD SYSOUT=N  
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(OUTLIN)  
//L.SYSPRINT DD SYSOUT=H  
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD  
//L.SYSIN DD *  
NAME OUTLIN(R)  
//*****  
//OUTPLT EXEC F7CL,PARM.L='NCAL'  
//C.SYSPRINT DD SYSOUT=N  
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(OUTPLT)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(BILDER)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(KOMGET)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(EXINT)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(EXTXT)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(EXREL)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(EXTRC)  
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD  
//L.SYSPRINT DD SYSOUT=H  
//L.SYSIN DD *  
ALIAS BILDER,STORE,STORP,ZEICHN,KOMGET,EXINT,EXTXT,EXREL,EXTRC  
NAME OUTPLT(R)
```

```

//*****
//XACHSE EXEC F7CL, PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR, DSN=PROJECT.HADA.DATA(XACHSE)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(ENCODE)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(IENT)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(PLTEXT)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(LAENGE)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(YACHSE)
//L.SYSMOD DD DISP=SHR, DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
  ALIAS YACHSE, ENCODE, IENT, PLTEXT, LAENGE
  NAME XACHSE(R)
//*****
//PLTIN EXEC F7CL, PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR, DSN=PROJECT.HADA.DATA(PLTIN)
//L.SYSMOD DD DISP=SHR, DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
  ALIAS PLTOF, NULLP
  NAME PLTIN(R)
//*****
//OUTSHW EXEC F7CL, PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR, DSN=PROJECT.HADA.DATA(OUTSHW)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(GETIND)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(IGET)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(GET2)
//L.SYSMOD DD DISP=SHR, DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
  ALIAS GETIND, IGET, GET2
  NAME OUTSHW(R)
//CHFCLC EXEC F7CL, PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR, DSN=PROJECT.HADA.DATA(CHFCLC)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SHIP)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(EDLD)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(WSC2)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(DDCR)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(VKNEW)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(VKOLD)
//L.SYSMOD DD DISP=SHR, DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
  ALIAS SHIP, EDLD, WSC2, DDCR, VKNEW, VKOLD
  NAME CHFCLC(R)

```

```
//GAUSS EXEC F7CL, PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR, DSN=PROJECT.HADA.DATA(GAUSS)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(ELIMS)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SOLVS)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(GAUSS0)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(GAUSS1)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(GAUSS2)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(ELIMN)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SOLVN)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SETLIN)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SETIT)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(DMPMAT)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(XNEU)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SETMAT)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SETVEK)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(MAT)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(VEK)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SORT)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(TAUS)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(EXCH)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SMAX)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(IMAX)
//L.SYSLMOD DD DISP=SHR, DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
ALIAS ELIMS, SOLVS, GAUSS0, GAUSS1, ELIMN, SOLVN, SETLIN, SETIT, DMPMAT, XNEU, *
      SETMAT, SETVEK, MAT, VEK, SORT, TAUS, EXCH, SMAX, IMAX
NAME GAUSS(R)
//*****
//EFPW EXEC F7CL, PARM.L='NCAL'
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR, DSN=PROJECT.HADA.DATA(EFPW)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(EFPD)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(EFS)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(PSIO)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(PSI)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(Q)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(B)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(FI)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(PR)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(HR)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(HS)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(PS)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(ARG1)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SUCHEN)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(PINV)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(RP)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(SUMME)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(FE)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(FL)
// DD DISP=SHR, DSN=PROJECT.HADA.DATA(FC)
//L.SYSLMOD DD DISP=SHR, DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *
ALIAS EFPD, EFS, PSIO, PSI, Q, B, FI, PR, HR, HS, PS, ARG1, SUCHEN, PINV, RP, SUMME, *
      FE, FL, FC
NAME EFPW(R)
```

```
//*****  
//DRUCK EXEC F7CL,PARM.L='NCAL'  
//C.SYSPOINT DD SYSOUT=N  
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(DRUCK)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(STOR8)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(OUTREC)  
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD  
//L.SYSPOINT DD SYSOUT=H  
//L.SYSIN DD *  
  ALIAS OUTREC,STOR8  
  NAME DRUCK(R)  
//F EXEC F7CL,PARM.L='NCAL'  
//C.SYSPOINT DD SYSOUT=N  
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(F)  
// DD DISP=SHR,DSN=PROJECT.HADA.DATA(DF)  
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD  
//L.SYSPOINT DD SYSOUT=H  
//L.SYSIN DD *  
  ALIAS DF  
  NAME F(R)
```

```
//*****
```

```
//**
```

```
//**
```

```
//**
```

```
//**
```

```
//**
```

```
//**
```

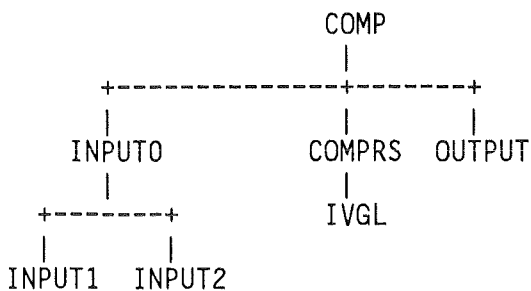
```
//**
```

```
//**
```

```
//**
```

```
//**
```

```
//**
```



```
//COMP EXEC F7CL
```

```
//C.SYSPOINT DD SYSOUT=N
```

```
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(COMP)
```

```
//L.SYSLIB DD
```

```
// DD DISP=SHR,DSN=PROJECT.HADA.LOAD
```

```
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
```

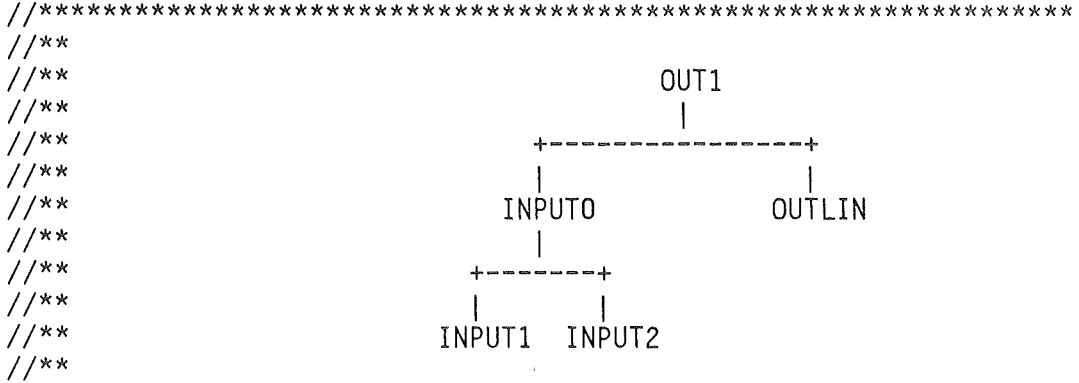
```
//L.SYSPOINT DD SYSOUT=H
```

```
//L.SYSIN DD *
```

```
  ENTRY MAIN
```

```
  NAME COMP(R)
```





```

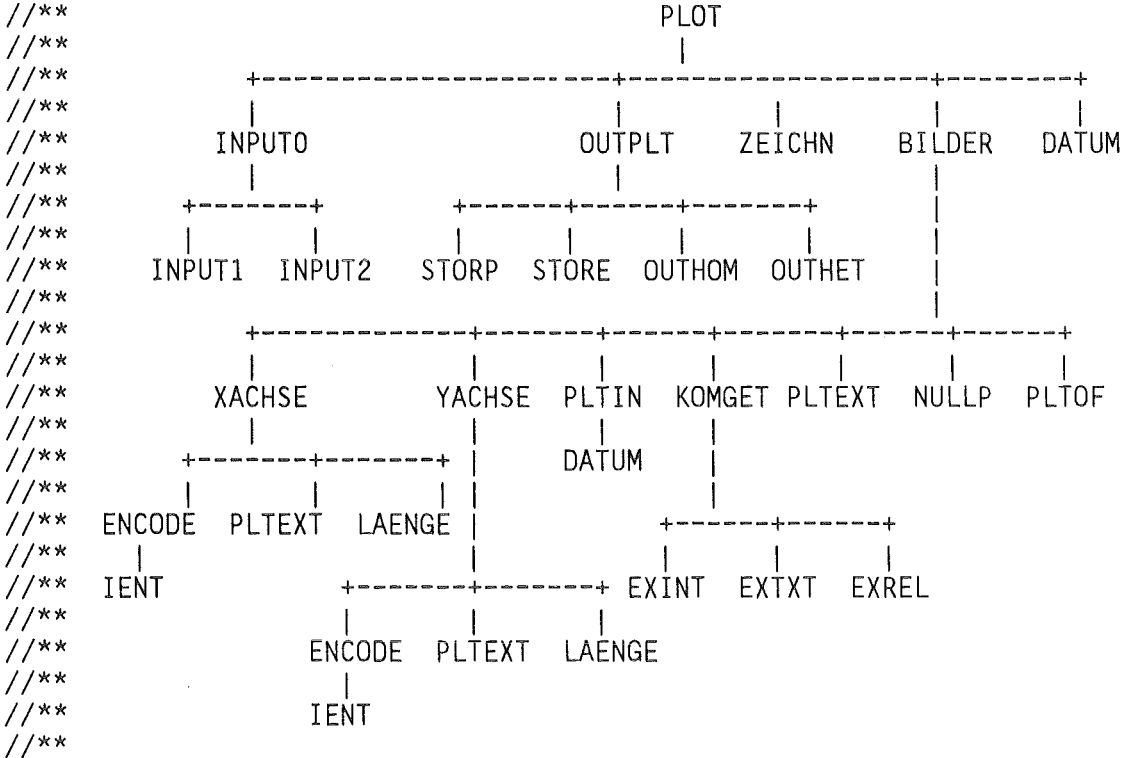
//OUT1 EXEC F7CL
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(OUT1)
//L.SYSLIB DD
// DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *

```

```

ENTRY MAIN
NAME OUT1(R)
//*****

```



```

//PLOT EXEC F7CL
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN DD DISP=SHR,DSN=PROJECT.HADA.DATA(PLOT)
//L.SYSLIB DD
// DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN DD *

```

```

ENTRY MAIN
NAME PLOT(R)

```



```

//*****
//**
//**
//**          SHOW
//**          |
//**          +-----+-----+
//**          |           |           |
//**        INPUTO      OUTSHW      DATUM
//**          |           |           |
//**          +-----+           +-----+
//**        INPUT1  INPUT2      GETIND  LAENGE
//**          |           |           |           |
//**          |           |           +-----+
//**          |           |           |     |
//**          |           |           GET2  IGET
//**
//SHOW EXEC F7CL
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN    DD DISP=SHR,DSN=PROJECT.HADA.DATA(SHOW)
//L.SYSLIB  DD
//          DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN   DD *
  ENTRY MAIN
  NAME SHOW(R)
//*****
//**
//HADA EXEC F7CL
//C.SYSPRINT DD SYSOUT=N
//C.SYSIN    DD DISP=SHR,DSN=PROJECT.HADA.DATA(HADA)
//L.SYSLIB  DD
//          DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSLMOD DD DISP=SHR,DSN=PROJECT.HADA.LOAD
//L.SYSPRINT DD SYSOUT=H
//L.SYSIN   DD *
  ENTRY MAIN
  NAME HADA(R)

```

8. Literature

1 M. Dalle Donne, W. Hame

"A Parametric Thermohydraulic Study of an Advanced Pressurized Light Water Reactor with a Tight Fuel Rod Lattice"

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2 M. Dalle Donne, W. Hame

"A Critical Heat Flux Correlation for Advanced Pressurized Light Water Reactor Application"

KfK 3279, EUR 7057e, Mai 1982

3 M. Dalle Donne, W. Hame

"A Critical Heat Flux Correlation for Triangular Array Rod Bundles with Tight Lattices, Including the Effect of Special Spacers"

to be published in Nuclear Technology