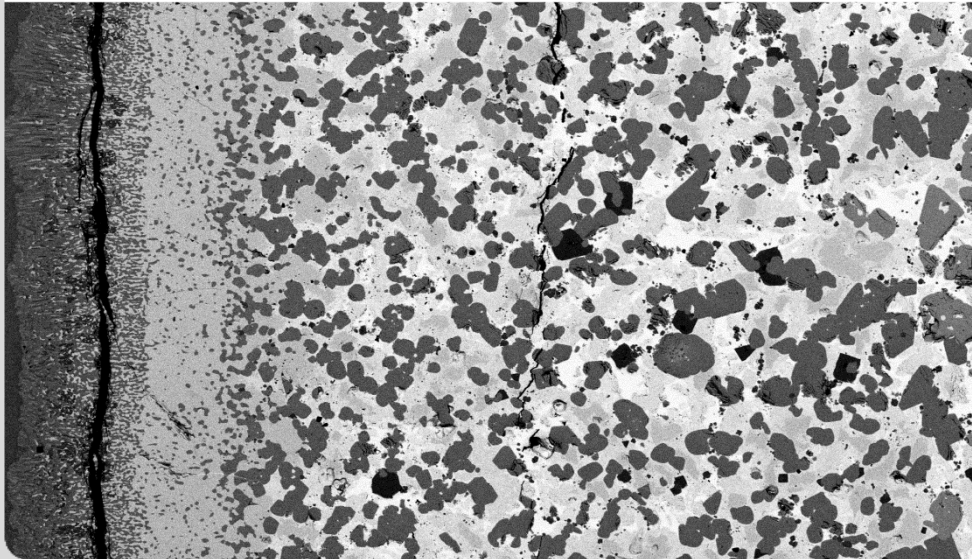


# Evaluation of liquid tin corrosion on austenitic steels as well as nickel-based alloys and first tests on possible protective surface layers at high temperature

Thomas Emmerich, Carsten Schroer

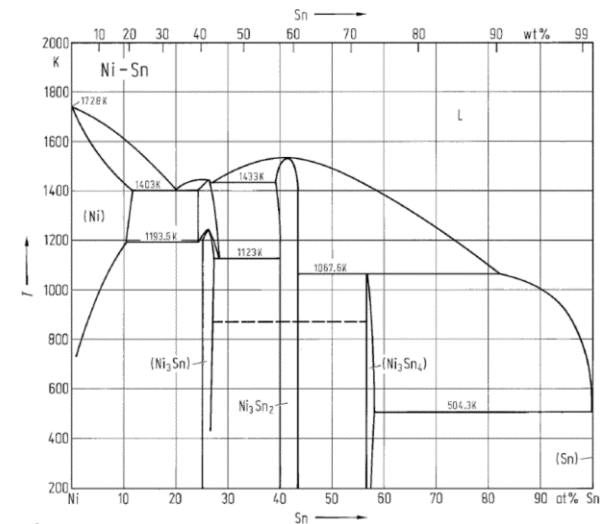
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- ❑ Introduction
  - ❑ Liquid tin
  - ❑ Motivation
- ❑ Evaluation of liquid tin corrosion
  - ❑ Tested materials
  - ❑ Setup and procedure of corrosion experiments
  - ❑ Analysis of liquid tin corrosion
- ❑ Development of protective surface layers
  - ❑ Properties and production of surface layers
  - ❑ Analysis of layer behaviour in liquid Sn

- ❑ Application of liquid Sn as heat transfer medium
  - ❑ Large liquid temperature range 232 – 2620 °C
  - ❑ Allows high heat flux
  - ❑ Not volatile or toxic
- ❑ Corrosion of metallic materials
  - ❑ Solution of alloying elements
  - ❑ Formation of intermetallic phases with Sn (stannides)
- ❑ Compatible materials
  - ❑ Rhenium, tungsten, quartz-glass, ceramics, graphite
- ❑ Alternative
  - ❑ Protective surface layers on steels or Ni-based alloys

J. Pacio et al., Sol. Energy 93 (2013) 11–22.



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R.N. Lyon, Liquid-metals Handbook, U.S. Government Printing Office, 1950.

E.L. Reed, J Am Ceram Soc 37 (1954), 146–153.

H. Shimotake et al., T Am Nucl Soc 10 (1965), 141–146.

# Evaluation of liquid tin corrosion

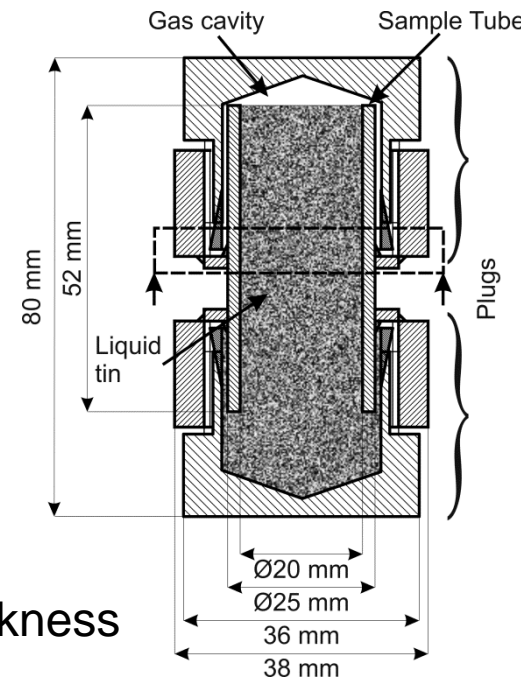
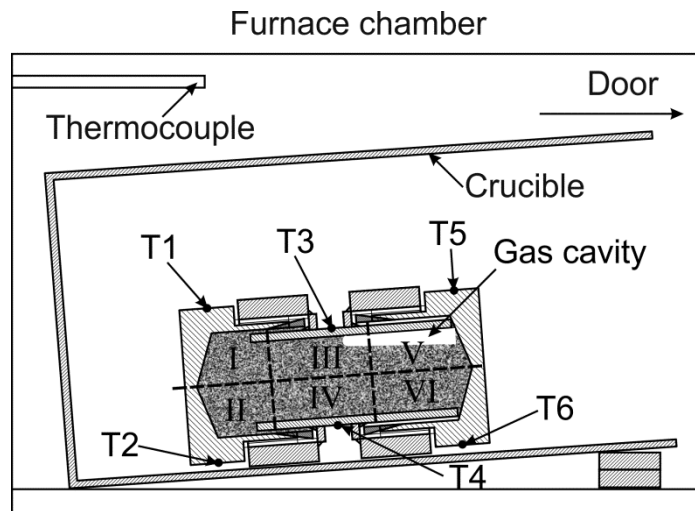
## Tested materials

- ❑ Austenitic steels (1.4301, 1.4571) at 500 and 700 °C
- ❑ Ni-based alloys (2.4650, 2.4663) at 700 and 1000 °C

Material	Al	C	Co	Cr	Fe	Mo	Si	Ti	Ni
1.4301	-	≤ 0.07	-	17.5-19.5	Bal.	-	-	-	8-10.5
1.4571	-	≤ 0.08	-	16.5-18.5	Bal.	2-2.5	-	5x C ≤ Ti ≤ 0.7	10.5-13.5
2.4650	0.45	0.05	19.8	20	0.44	5.9	0.09	2.1	Bal.
2.4663	0.99	0.06	11.7	21.97	1.09	8.53	0.13	0.41	Bal.

# Evaluation of liquid tin corrosion

## Setup and procedure of the corrosion experiments



### ❑ Preparation

- ❑ Determination of the average wall-thickness
- ❑ Filling in Ar-atmosphere

### ❑ Testing

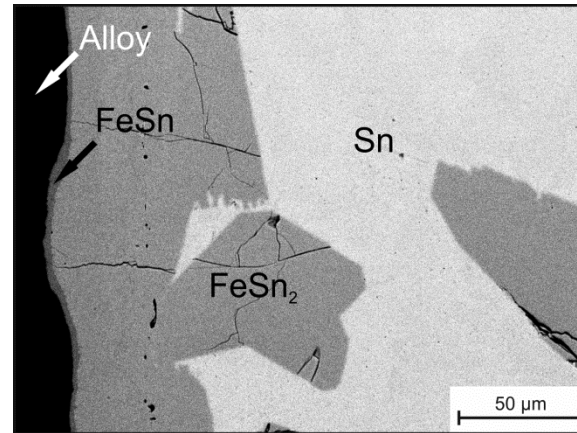
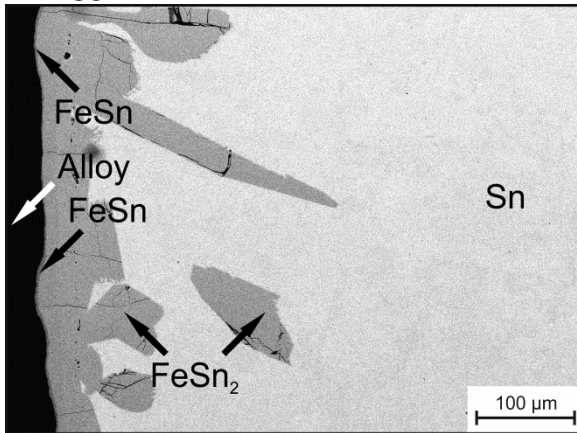
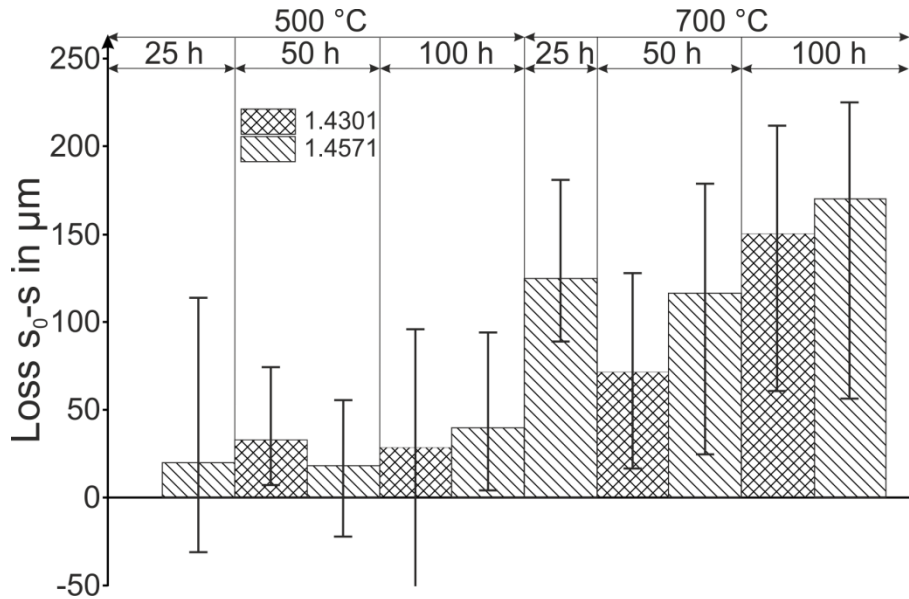
- ❑ Exposure at 500, 700 and 1000 °C for 25, 50 und 100 h
- ❑ Measurement of the temperature distribution

### ❑ Post-test analysis

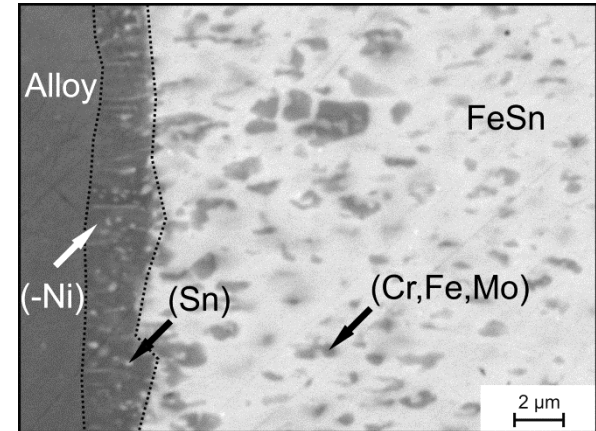
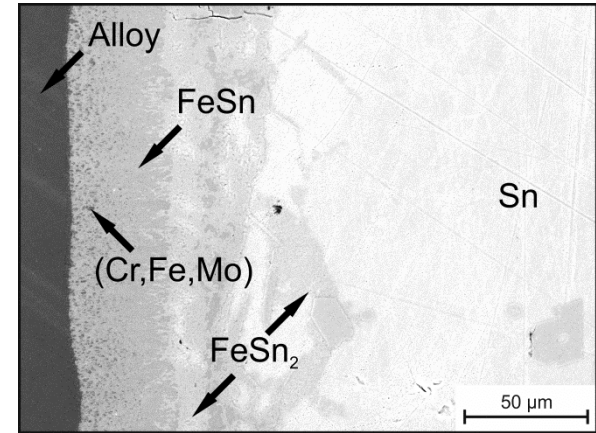
- ❑ OM, SEM, EDX

# Evaluation of liquid tin corrosion

## Steels after corrosion experiments



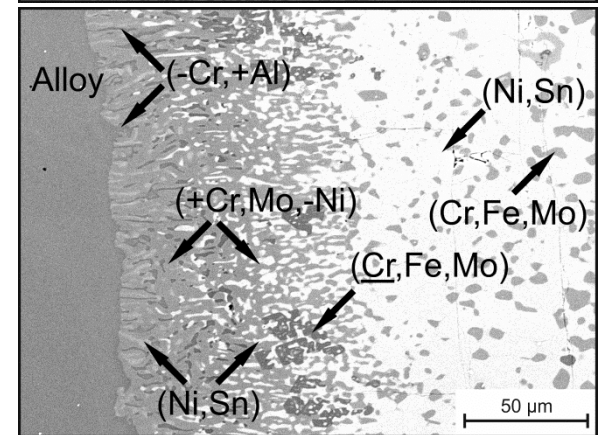
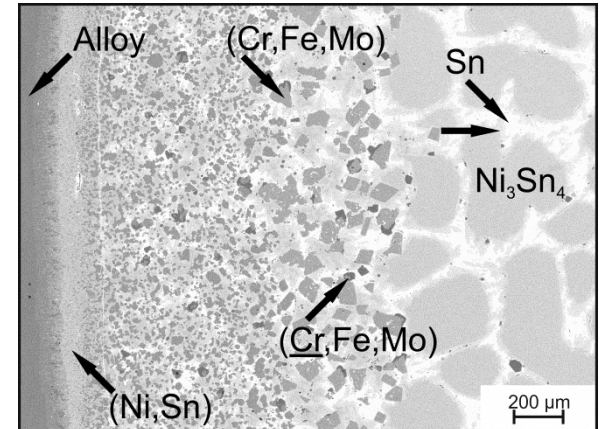
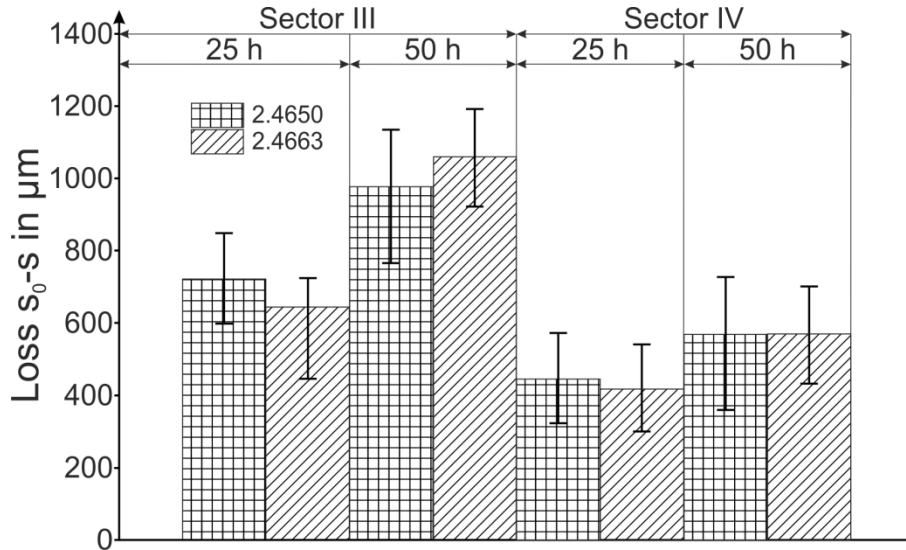
1.4301 at 500 °C for 100 h



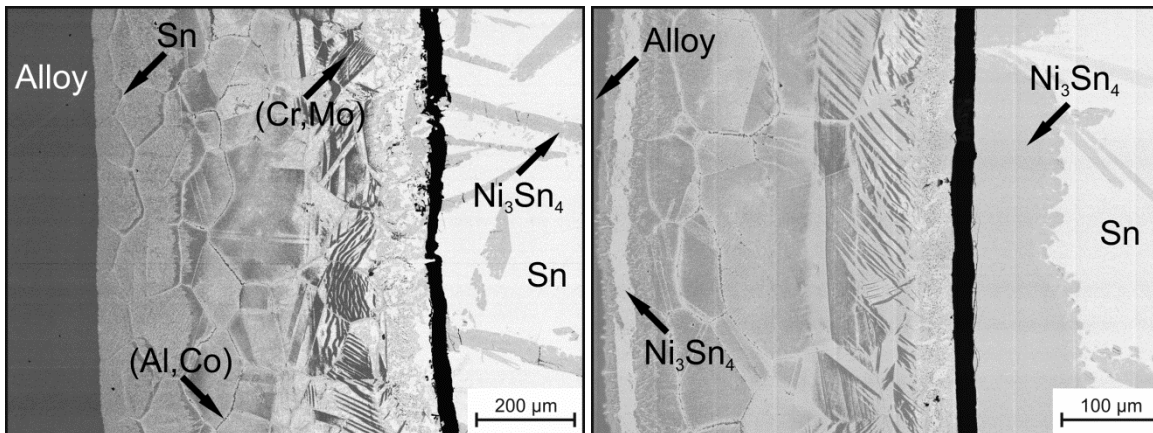
1.4571 at 700 °C for 25 h

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# Evaluation of liquid tin corrosion Ni-based alloys after corrosion experiments



2.4663 at 1000 °C for 25 h



2.4663 at 700 °C for 25 h

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# Evaluation of liquid tin corrosion

## Conclusions from corrosion experiments in liquid tin

### ❑ Solution based corrosion

- ❑ High solubility of Ni causes selective leaching of Ni and higher material losses of Ni-based alloys than of steels
- ❑ Less soluble Cr, Fe and Mo form  $\alpha$ -,  $\sigma$ - or similar phases

### ❑ Growth of stannides

- ❑ Precipitate from locally saturated melt
- ❑ Re-precipitation of solutes leads to further material consumption
- ❑ Solid state diffusion through layers allows corrosion to continue

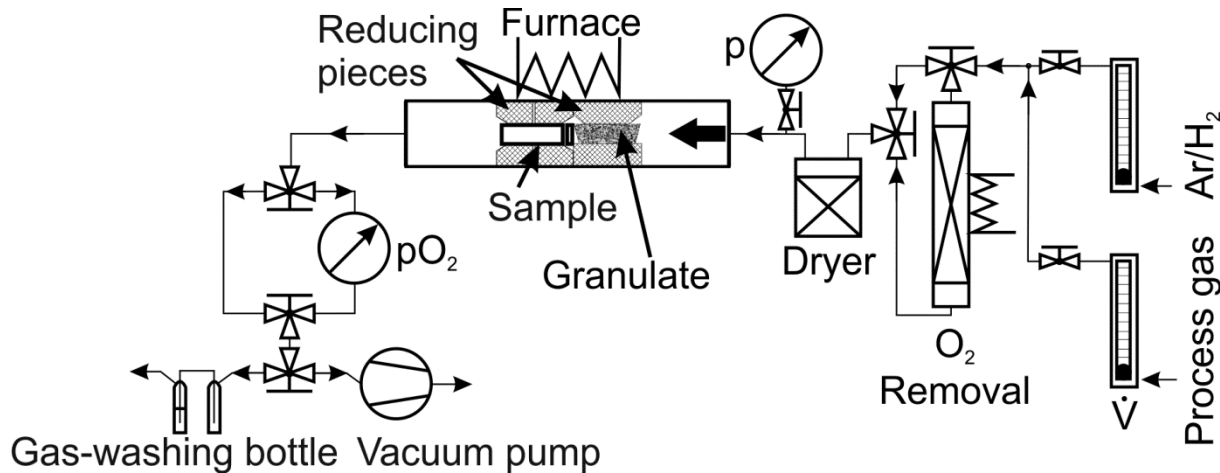
### ❑ Consequences

- ❑ Dense protective surface layers necessary
- ❑ Short grace periods especially at 1000 °C
- ❑ Precise corrosion monitoring necessary



# Development of protective surface layers

## Properties and production of surface layers



### Carbides

- C shows very low solubility in liquid tin

- Low pressure carburisation
- At 1000 °C in propane
- $p \leq 10$  mbar,  $t - 8$  h
- PVD: TiC

### Oxides

- O is soluble in liquid tin
- Short term protection

- High temperature gas oxidation
- At 800 °C in flowing Ar 6.0
- $t - 48$  h

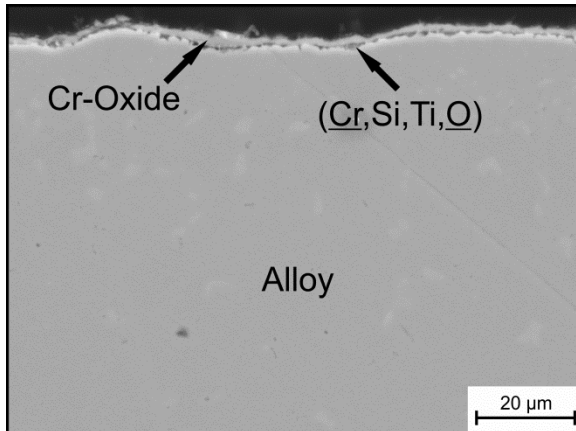
### Nitrides

- N shows very low solubility in liquid tin

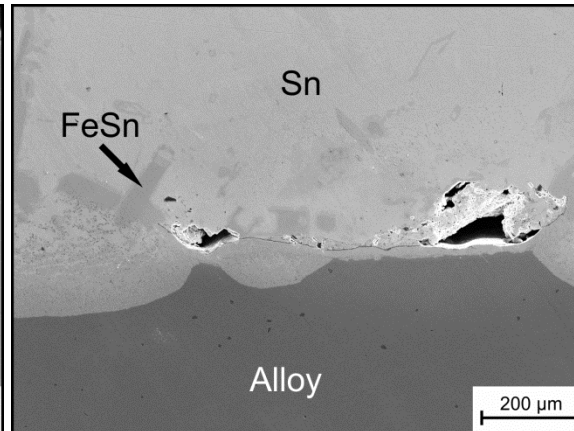
- High temperature gas nitration
- At 800 °C in flowing N<sub>2</sub> 6.0
- $t - 192$  h
- PVD: TiN

# Development of protective surface layers

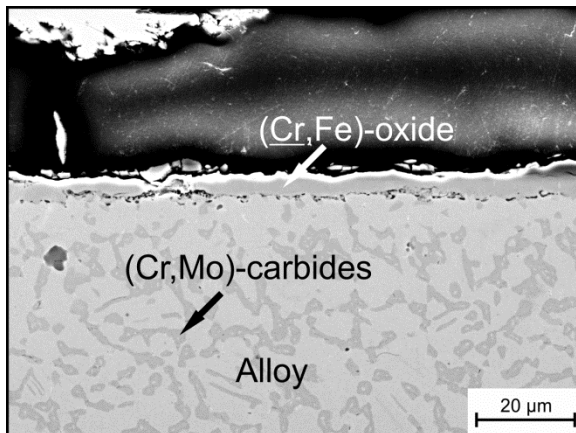
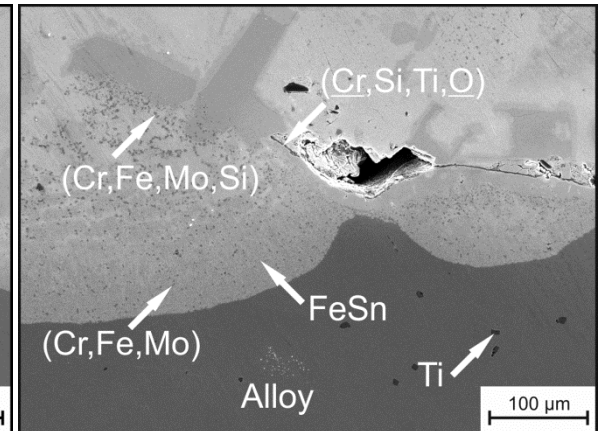
## Corrosion experiments on oxide layers



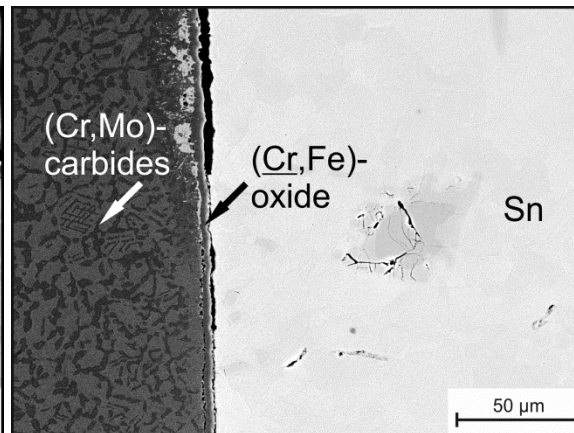
Oxidised



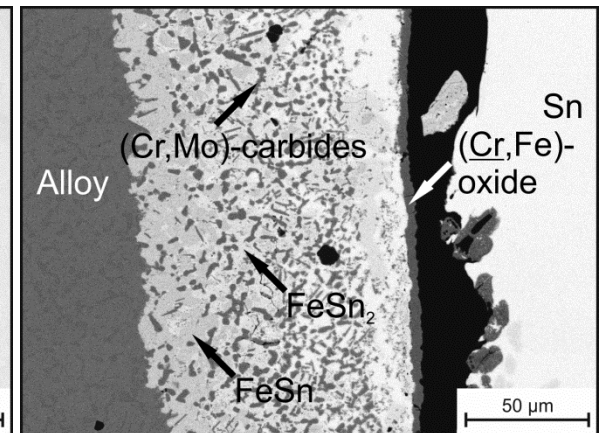
1.4571 at 700 °C for 100 h



Carburised



1.4571 at 700 °C for 100 h

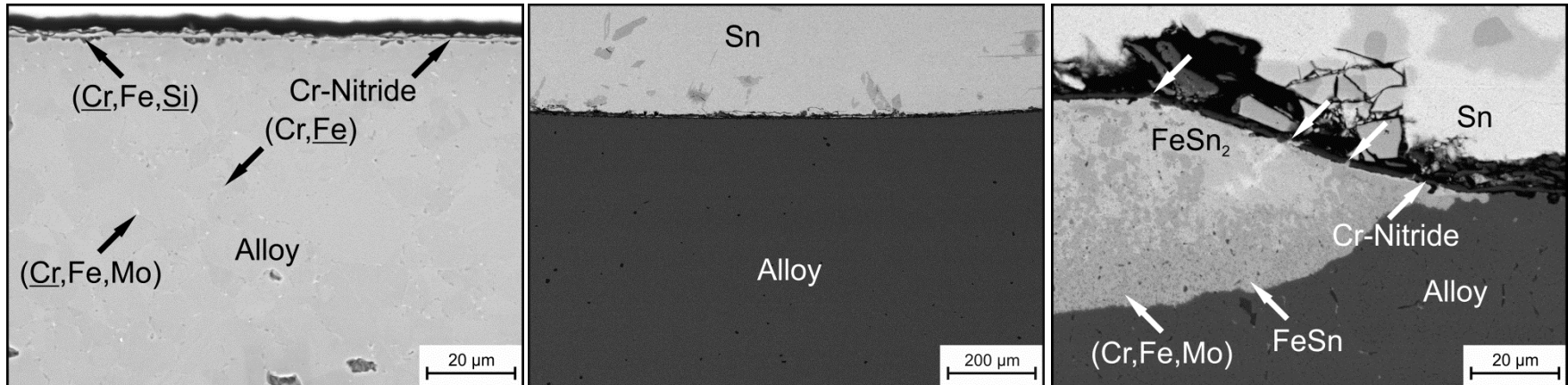


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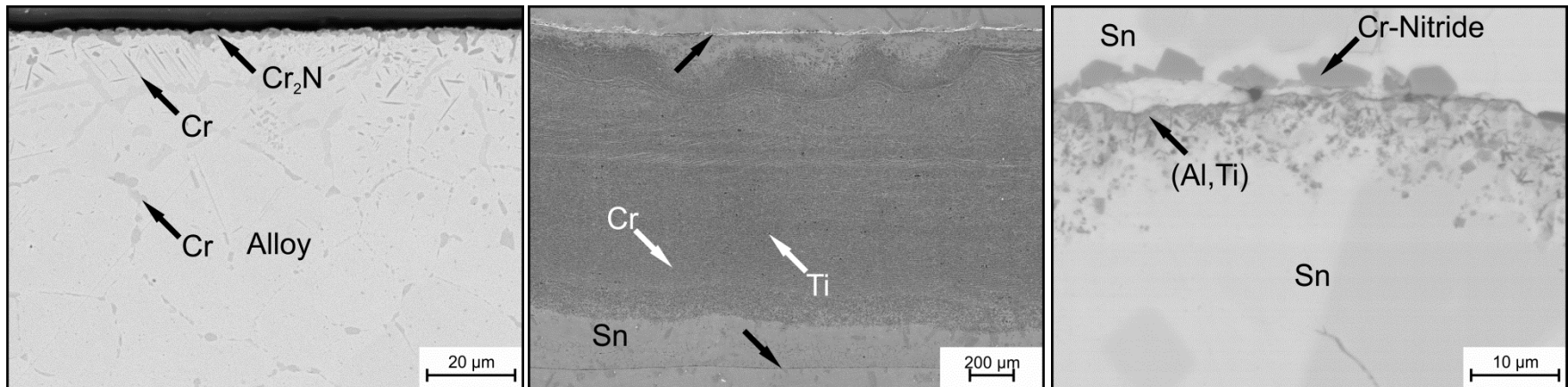
# Development of protective surface layers

## Corrosion experiments on nitride layers



Nitrided

1.4571 at 700 °C for 100 h



Nitrided

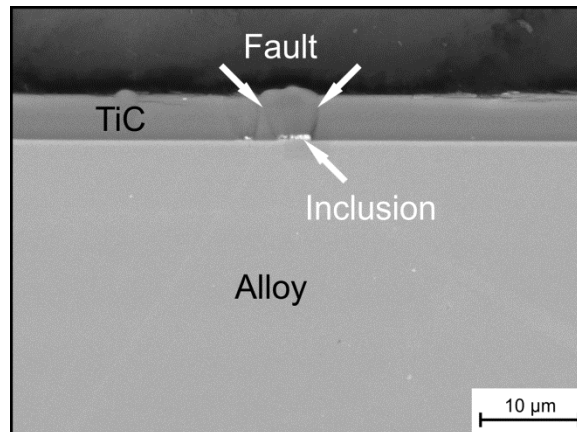
2.4642 at 700 °C for 50 h

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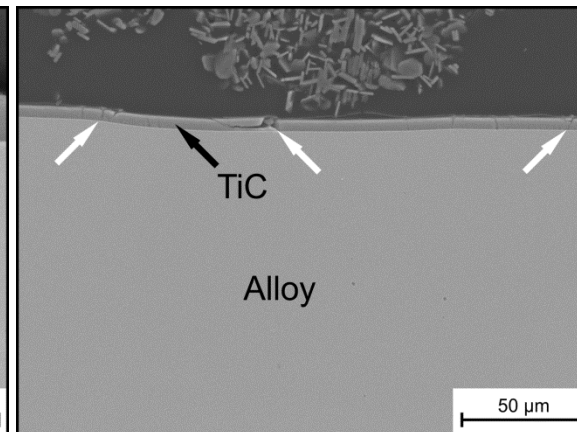
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# Development of protective surface layers

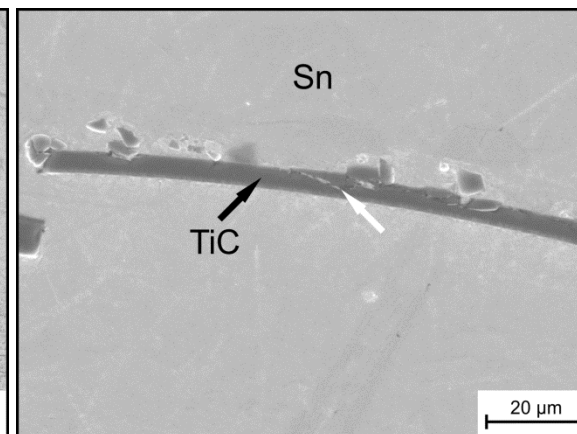
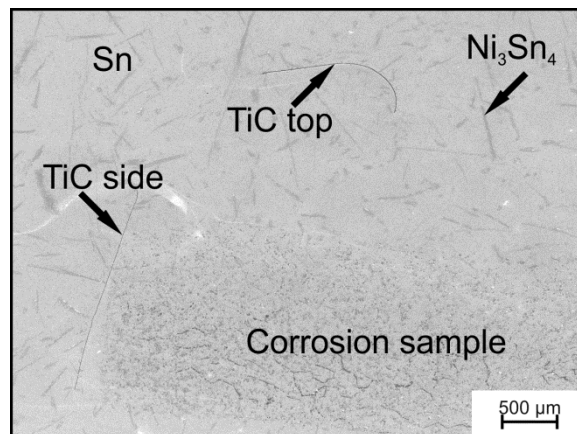
## Corrosion experiments on PVD layers



PVD



700 °C for 50 h in Ar



2.4642 at 700 °C for 50 h

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# Development of protective surface layers

## Conclusions from corrosion experiments on surface layers

- ❑ Oxides
  - ❑ Dissolution of thin Cr-oxide layers underline limited stability
  - ❑ Thicker layers necessary for protection against liquid tin
- ❑ Carbides
  - ❑ Carbides show stability against liquid tin
  - ❑ No reduction of corrosion as network
  - ❑ Deposition as complete carbide layers required
- ❑ Nitrides
  - ❑ Formed continuous layers and protected wide sample areas
  - ❑ Penetration of liquid tin only through cracks in the layer
  - ❑ Increase of chemical stability by higher alloying content of Al or Ti than Cr
- ❑ Most promising approach
  - ❑ Preferably nitrides for thermo-chemical layer formation
  - ❑ Compensation of different thermo-mechanical properties for deposited coatings by functionally graded layers
  - ❑ Layers of chemical stable compounds like Al- or Ti-nitrides to prevent transformation by alloying elements

# Thank you for your attention!

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