

Combined Battery Calorimetry and Simulation for Prevention of Thermal Runaway and increased Safety

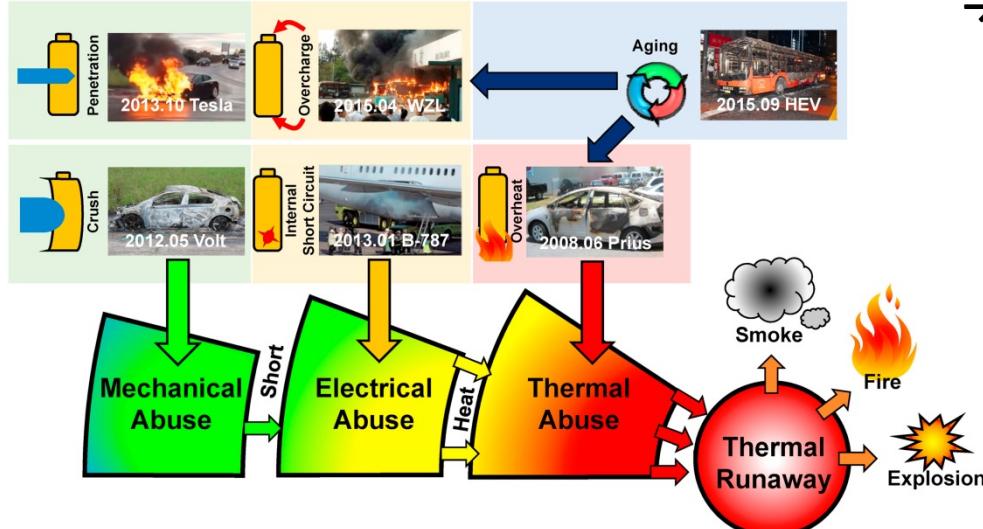
C. Ziebert, N. Uhlmann, S. Ouyang, W. Zhao, M. Rohde, H. J. Seifert

Institute for Applied Materials – Applied Materials Physics (IAM-AWP)

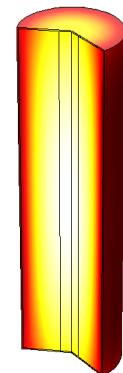


Motivation

Increase of safety and reliability of lithium-ion batteries for EV/HEV



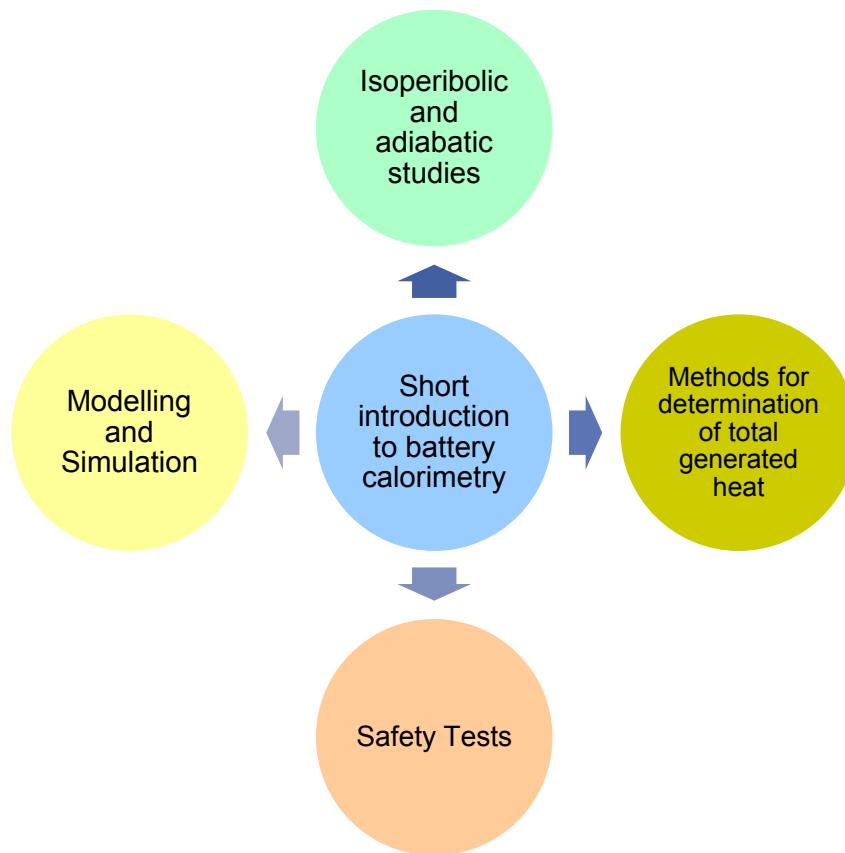
→ For improving battery management system (BMS) and thermal management system (TMS) electrochemical and thermal behavior of the cells have to be thoroughly studied



Feng et al., Energy Storage Materials 10 (2018) 246

Aim: Improvement of TMS and BMS by determination of quantitative data using battery calorimetry in combination with modelling and simulation

Outline



Short institute presentation

Karlsruhe Institute of Technology (KIT)

1/10/2009 - Foundation of KIT

Merger of the University of Karlsruhe (TH) and the Forschungszentrum Karlsruhe GmbH



Data 2016

Employees:	9.239
Students:	25.892
Professors:	365
Budget:	851 Mio Euro
Patents:	55
Spin-offs:	21



Campus South

Campus North

Research – Teaching – Innovation

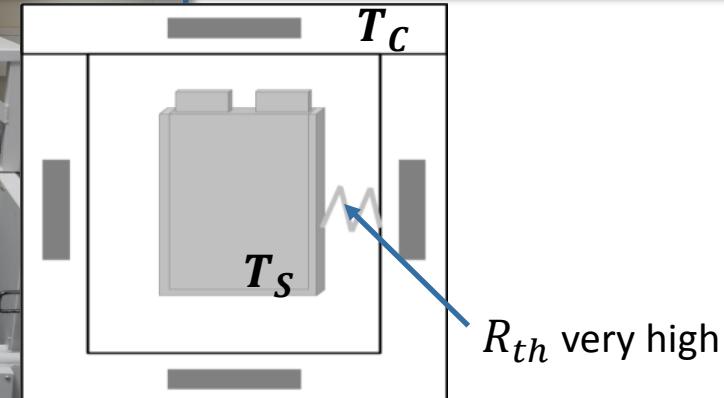
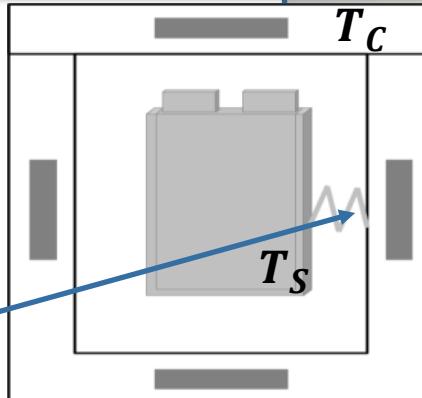
Short introduction to battery calorimetry

Possible conditions in an Accelerating Rate Calorimeter (ARC)

An ARC provides **isoperibolic** and **adiabatic** conditions

Under isoperibolic conditions the environmental temperature is kept constant.

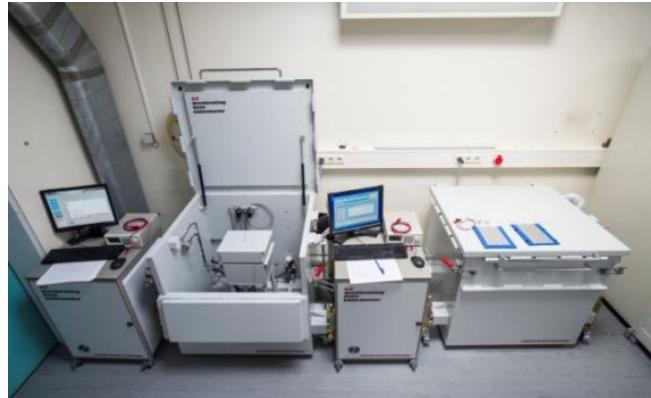
Under adiabatic conditions the heaters follow immediately any change of the bomb thermocouple thus preventing that the cell can transfer heat to the walls.



$$T_C \text{ constant}$$
$$T_S(t) = T_{S_0} + \alpha \cdot t$$

$$T_C = T_C(t)$$
$$= T_{C_0} + \alpha \cdot t$$

At IAM-AWP: Europe's Largest Battery Calorimetry Lab



Accelerating Rate Calorimeter(ARC)

Equipment: 6 ARC's (THT); 2 Tian-Calvet calorimeters (C80, Alexys1000: Setaram); DSC (Netzsch), TGA+STA (TAG, Setsys, Setaram); IR camera (FLIR); 12 Temperature chambers; 10 Cyclers; EIS (Ref3000, Gamry)



Adiabatic and Isoperibolic Measurements

Adiabatic Measurements

Worst Case Conditions

→ Cell in a pack surrounded by other cells

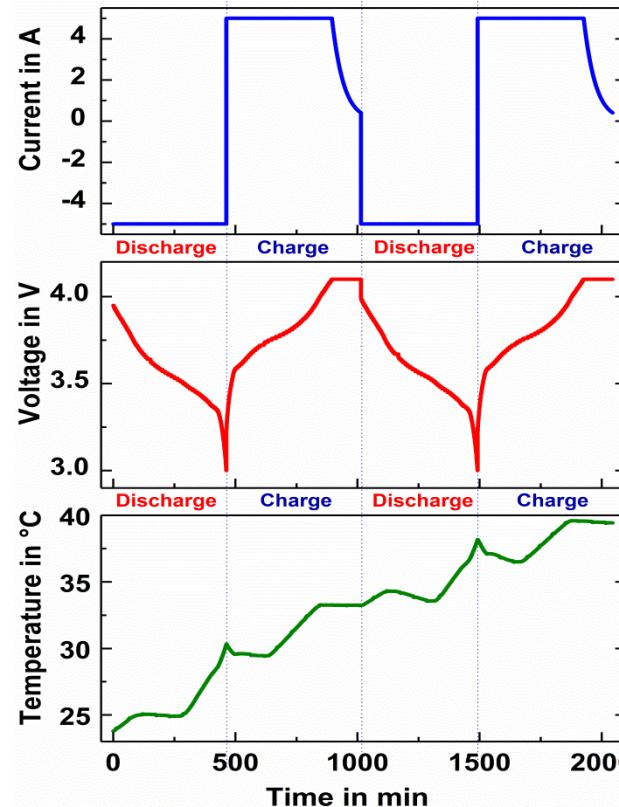
Discharge parameter:

- method: constant current (CC)
- $U_{\min} = 3.0V$
- $I = 5A \rightarrow C/8\text{-rate}$

Charge parameter:

- method: constant current,
constant voltage (CCCV)
- $U_{\max} = 4.1V$
- $I = 5A \rightarrow C/8\text{-rate}$
- $I_{\min} = 0.5A$

→ after each electrochemical cycle the cell
temperature increases further



$$T_{st} = 23^\circ\text{C (RT)}$$

Isoperibolic Measurements

Ideal conditions

→ Single cell

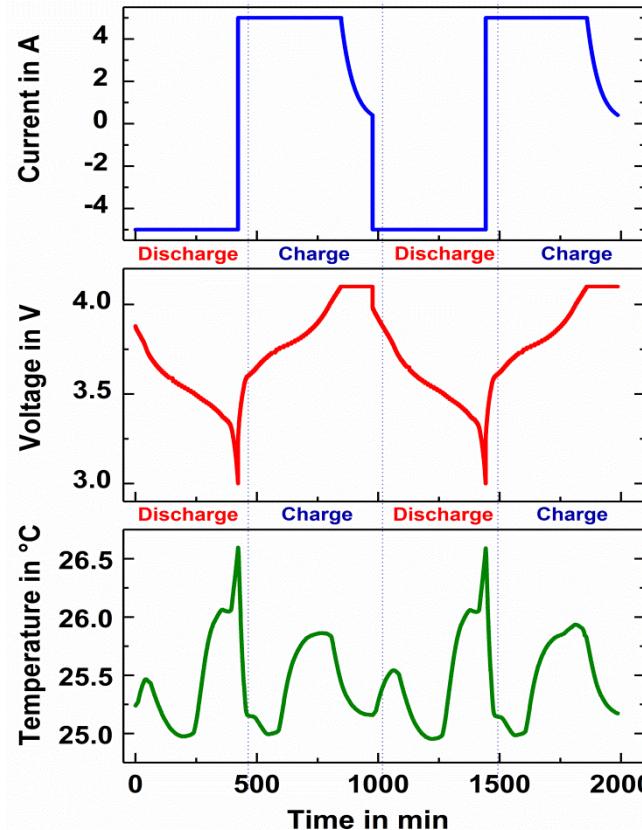
Discharge parameter:

- method: constant current (CC)
- $U_{\min} = 3.0V$
- $I = 5A \rightarrow C/8\text{-rate}$

Charge parameter:

- method: constant current,
constant voltage (CCCV)
- $U_{\max} = 4.1V$
- $I = 5A \rightarrow C/8\text{-rate}$
- $I_{\min} = 0.5A$

→ after one electrochemical cycle the cell
temperature reaches its initial value again



$$\left(\frac{\delta E}{\delta T} \right) < 0$$

temperature coefficient
negative!

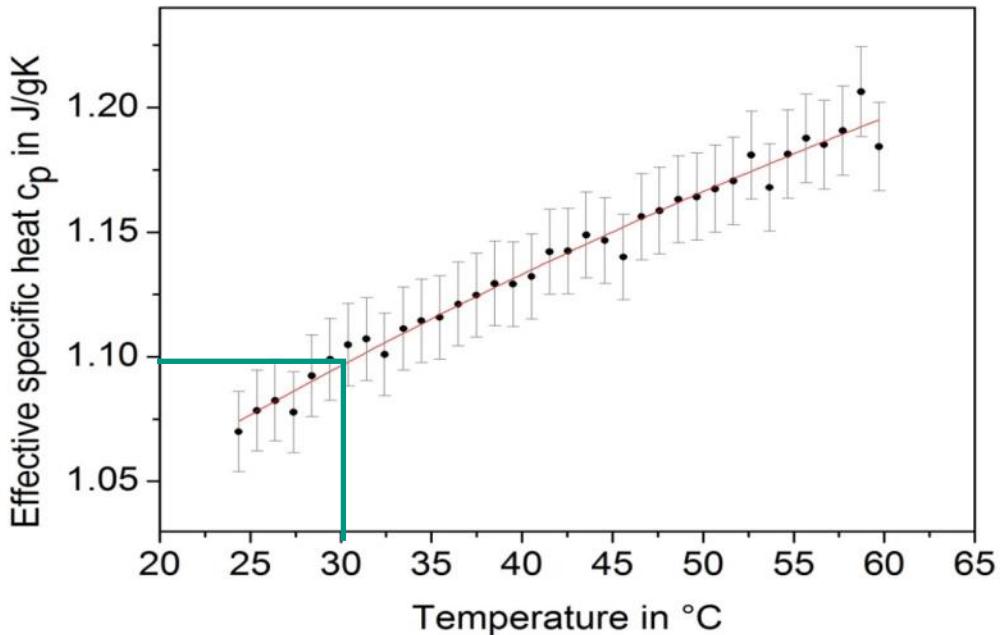
Heat generation of the cell during charging and discharging – Key data for thermal management and safety

Conversion of thermal data (temperature, temperature rate) to heat (Joule) and power (Watt) with the aim of understanding of heat release to determine heat removal requirements for thermal management.

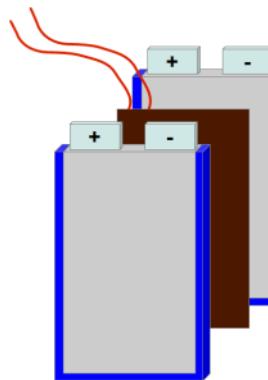
To be measured:

- **Cell effective specific heat capacity**
- **Heat transfer coefficient**
- **Reversible heat rate**
- **Irreversible heat rate**

Measurement of effective specific heat capacity c_p



e.g. at 30 °C $c_p = 1.095 \text{ J/g} \cdot \text{K}$



Sandwich setup
for pouch cells

Control of the current applied to the heater mat to ensure a constant heating rate

$$c_p = \frac{\Delta Q}{m \cdot \Delta T_{ad}} = \frac{\int U \cdot I \, dt}{m \cdot \Delta T_{ad}}$$

m: Mass of the cell

ΔT_{ad} : Temperature difference under adiabatic conditions

Measurement of heat transfer coefficient h with heat flux sensors



*gSKIN®-XP [1]
(10mm x 10mm)*

Working principle of heat flux sensor

Tiny, serially connected semiconductor piles inside the sensor generate a voltage, which is proportional to the heat passing through the surface. The voltage is read out and depending on the sensor's sensitivity the results are converted into the heat flux [2].

Sensitivity:

$$S_0 = 10.04 \frac{mV \cdot m^2}{W}$$

$$S(T) = S_0 + (T - 22.5 \text{ } ^\circ\text{C}) \cdot S_C$$

$$S_C = 0.0049 \cdot \frac{mV \cdot m^2}{W \cdot ^\circ\text{C}}$$

Room temperature sensitivity

$$\Rightarrow h = \frac{\int \frac{U_{\text{sensor}}}{S(T)} dt}{\int_0^t (T - T_c) dt}$$

Temperature correction factor

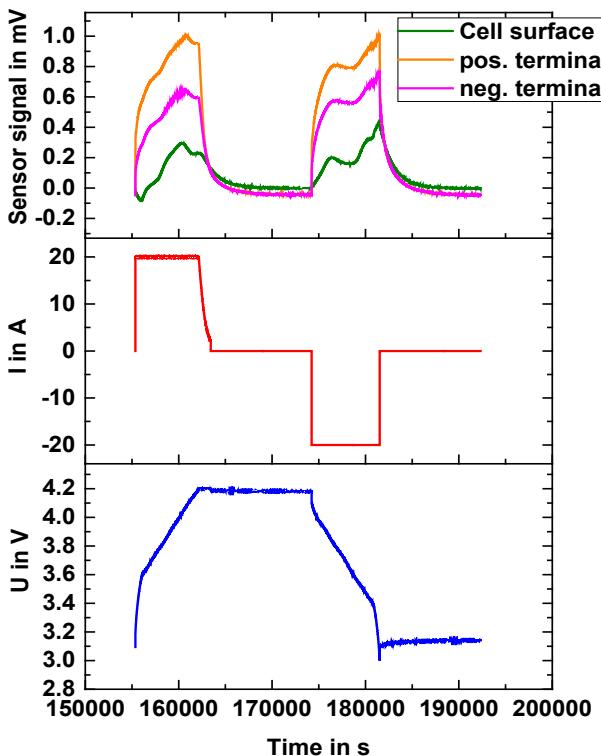
[1]

<http://shop.greenteq.com/shop/products-rd/gskin-xp/>

[2]

<https://www.greenteq.com/faq-heat-flux-sensing/>

Full cycle at 20A and 30°C



Comparison of the values for the generated heat determined by three different methods

1) Adiabatic Measurement

$$\dot{Q}_g = mc_p \frac{dT}{dt}$$

2) Isoperibolic Measurement

$$\dot{Q}_g = mc_p \frac{dT}{dt} + Ah \cdot (T_S - T_C)$$

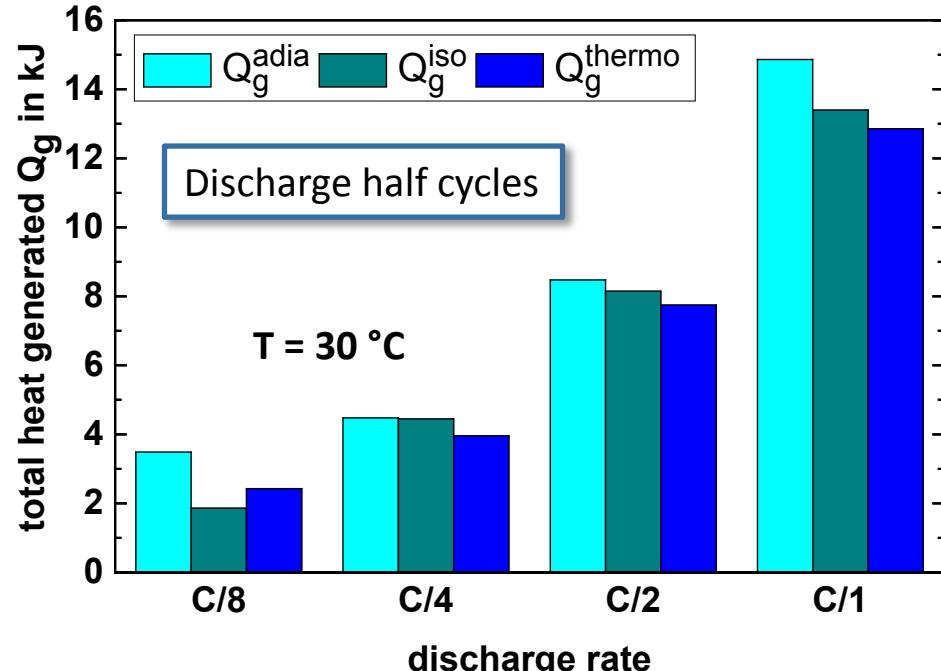
3) Measurement of irreversible and reversible heat using potentiometric and CIT method

$$\dot{Q}_g = -I(E_0 - E) - IT \frac{dE_0}{dT}$$

E_0 : Open circuit voltage (OCV), E : cell potential

Conclusion: good agreement between the values determined by the different methods

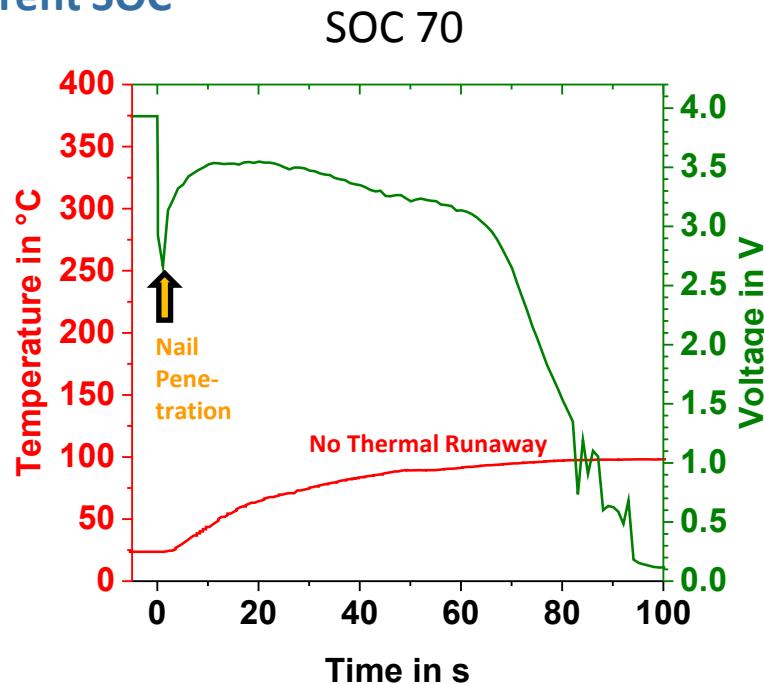
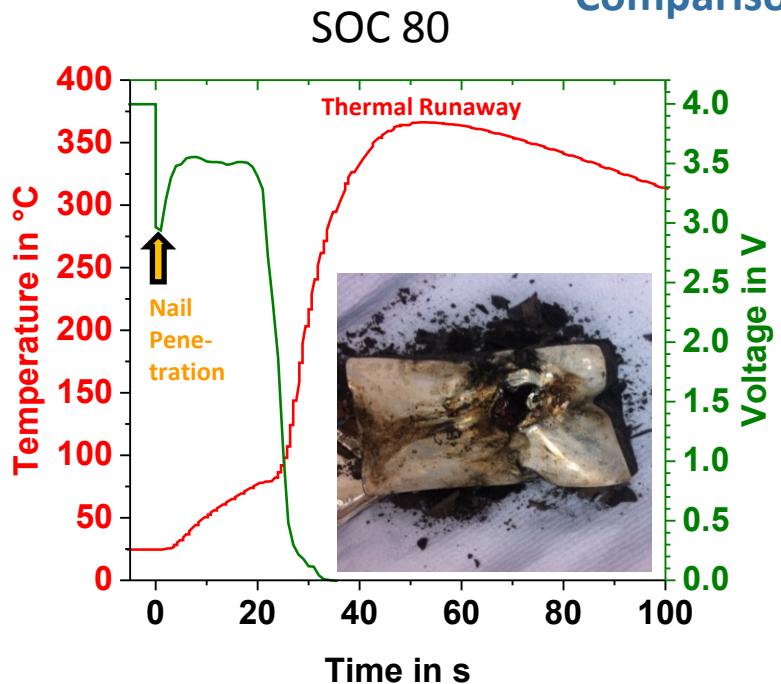
Source: E. Schuster, C. Ziebert, A. Melcher, M. Rohde, H.J. Seifert, J. Power Sources 268 (2015) 580-589



Safety tests

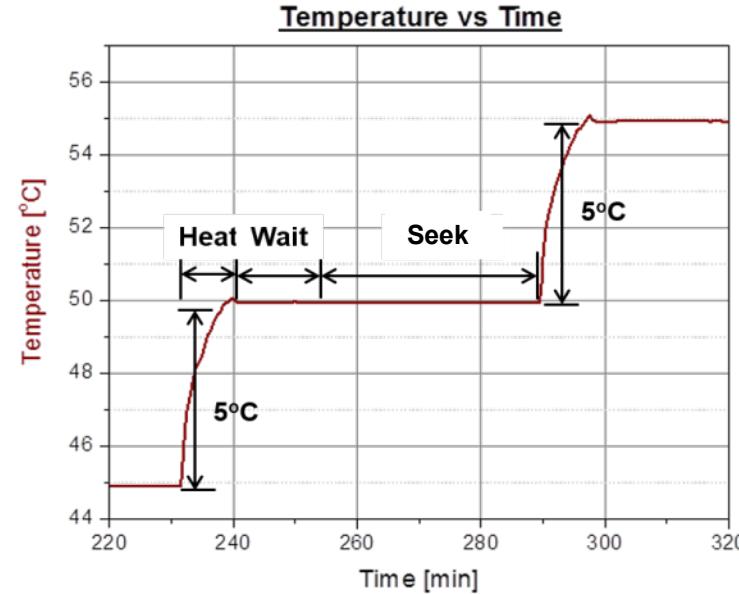
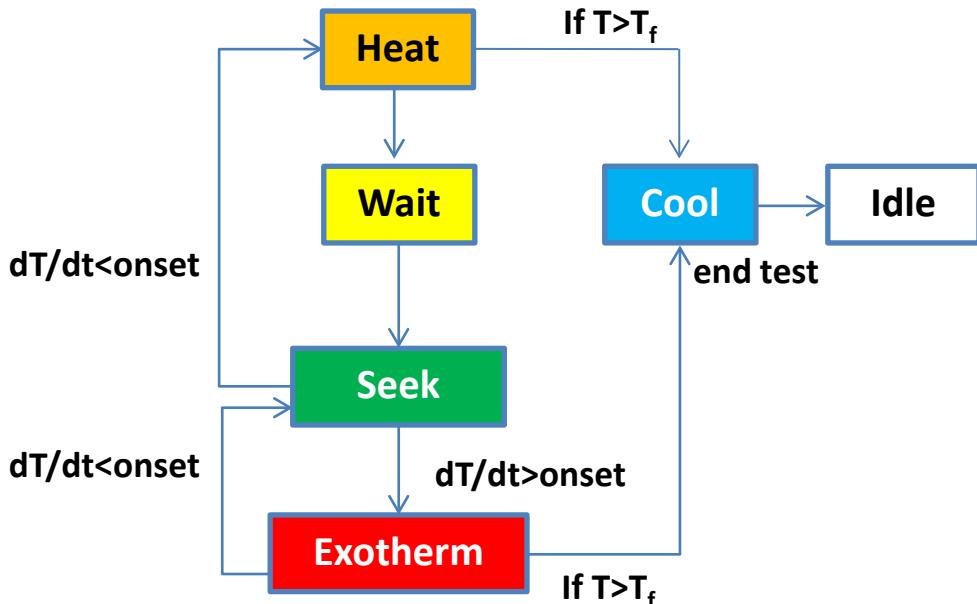
a) Mechanical abuse: Nail test

Comparison of different SOC



Nail penetration test in the ARC on a 2.5 Ah pouch cell

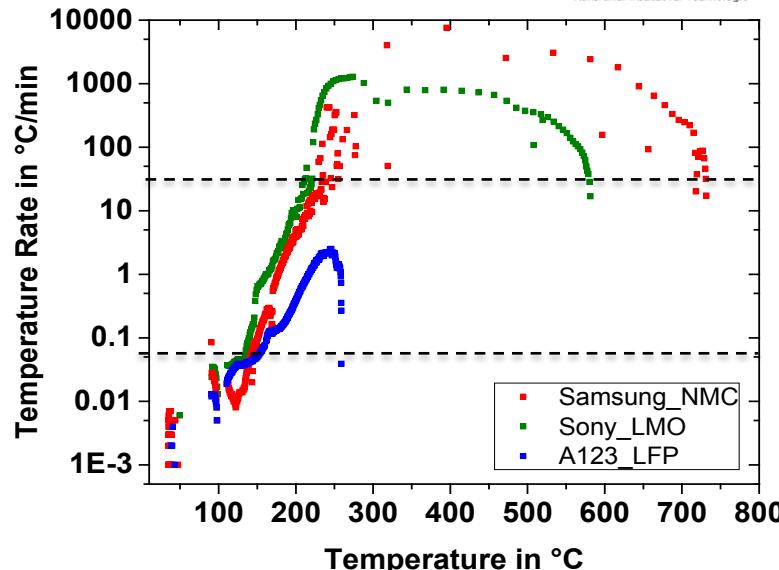
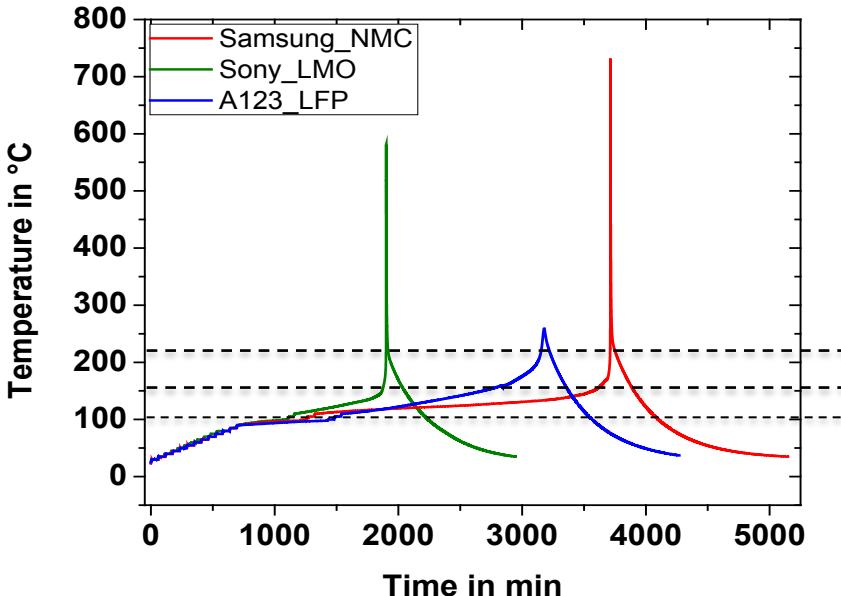
b) Thermal Abuse: Heat-Wait-Seek(HWS) Method



Example of a Heat-Wait-Seek step

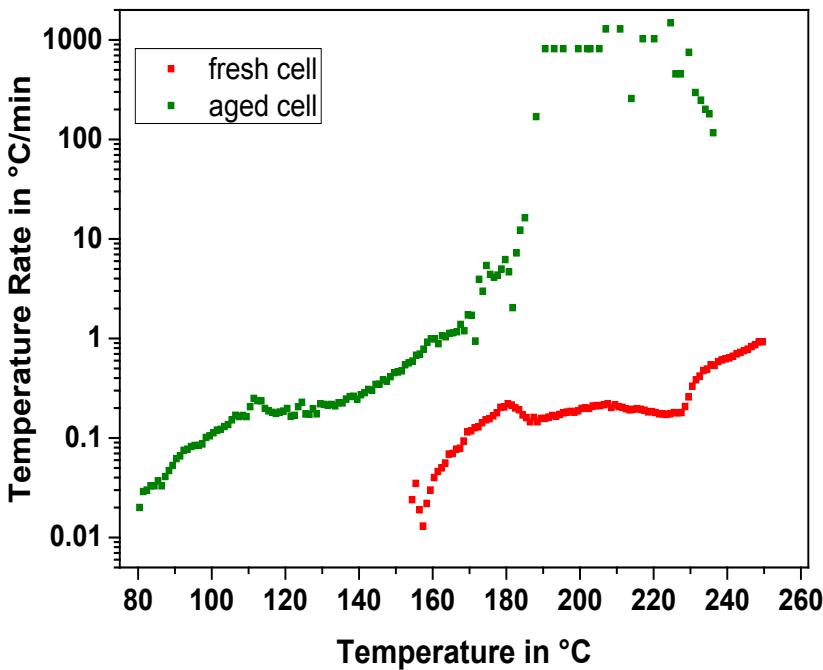
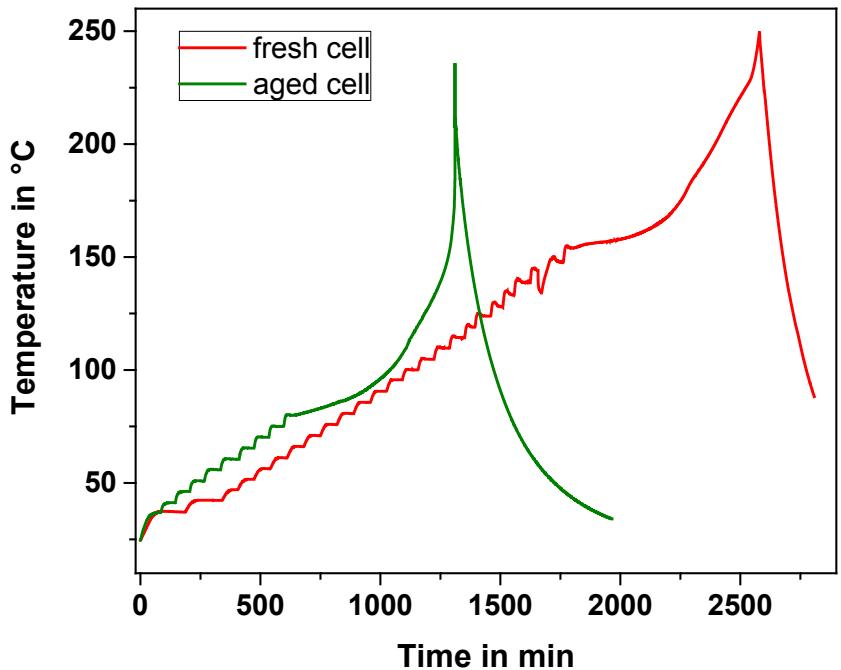
C. Ziebert, A. Melcher, B. Lei, W.J. Zhao, M. Rohde, H.J. Seifert, *Electrochemical-thermal characterization and thermal modeling for batteries*, in: L.M. Rodriguez, N. Omar, Eds., *EMERGING NANOTECHNOLOGIES IN RECHARGEABLE ENERGY STORAGE SYSTEMS*, Elsevier Inc. 2017, ISBN 978032342977.

Thermal Runaway: 18650 cells with different cathode materials



- 80<T<130°C: low rate reaction, 0.02 - 0.05 °C/min: exothermic decomposition of the SEI
- 130<T<200°C: medium rate reaction, 0.05 - 25 °C/min: solvent reaction, exothermic reaction between embedded Li ions and electrolyte => reduction of electrolyte at negative electrode
- T > 200°C: high rate reaction, higher than 25 °C/min: Exothermic reaction between active positive material and electrolyte at positive electrode => rapid generation of oxygen

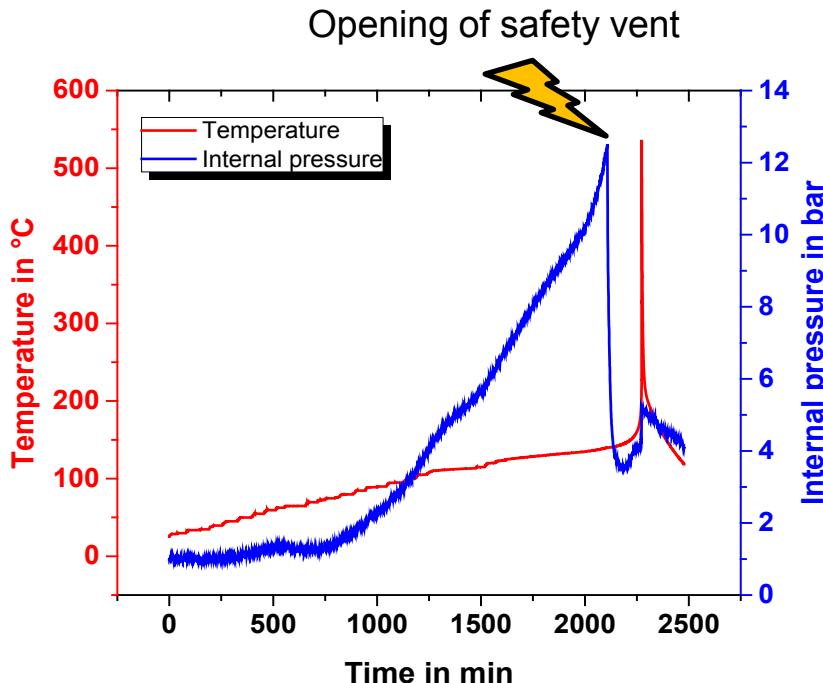
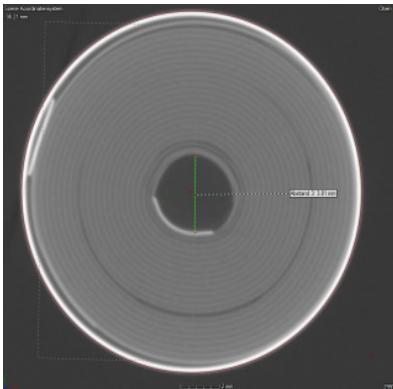
Study of ageing effects of PHEV1 cells by thermal runaway tests



Development of internal pressure measurement methods for 18650 cells



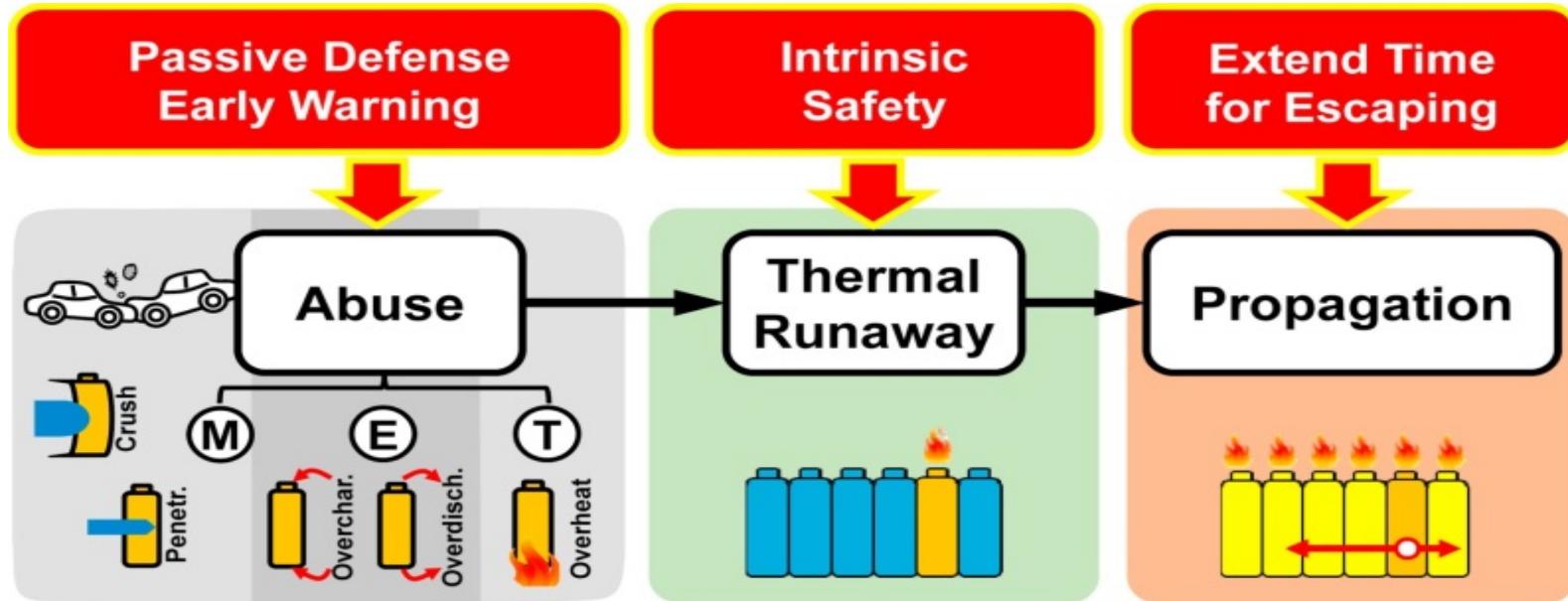
Pressure line (\varnothing 1.5 mm)



Internal pressure could be used in BMS for early prediction of processes leading to thermal runaway

B. Lei, W. Zhao, C. Ziebert, A. Melcher, M. Rohde, H.J. Seifert, *Batteries* 2017, 3, 14, [doi:10.3390/batteries3020014](https://doi.org/10.3390/batteries3020014).

The three-level strategy of reducing the hazard of thermal runaway



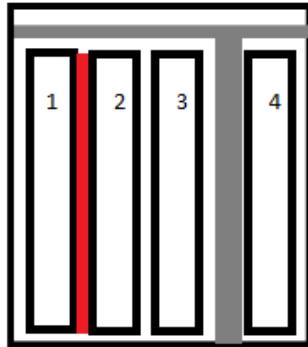
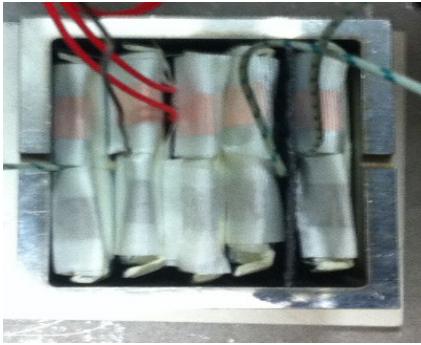
Step 1 - BMS

Detection of mechanical, thermal, electrical abuse

Step 2 – Cell : Venting, CID, PTC

Step 3 – Pack Passive propagation prevention

Thermal Runaway propagation testing

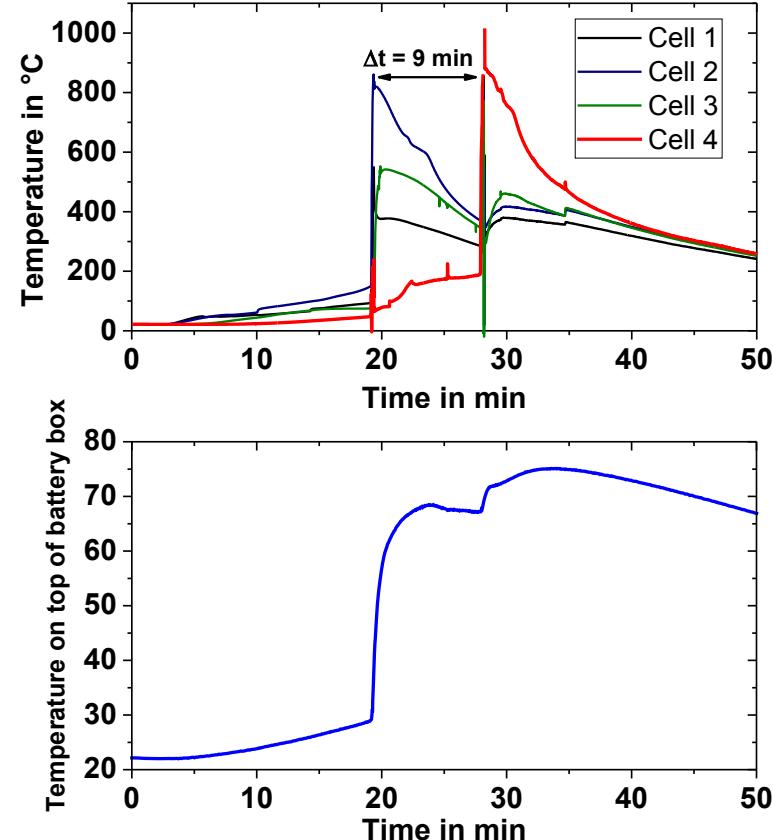


Protective Material evaluation in battery calorimeters:

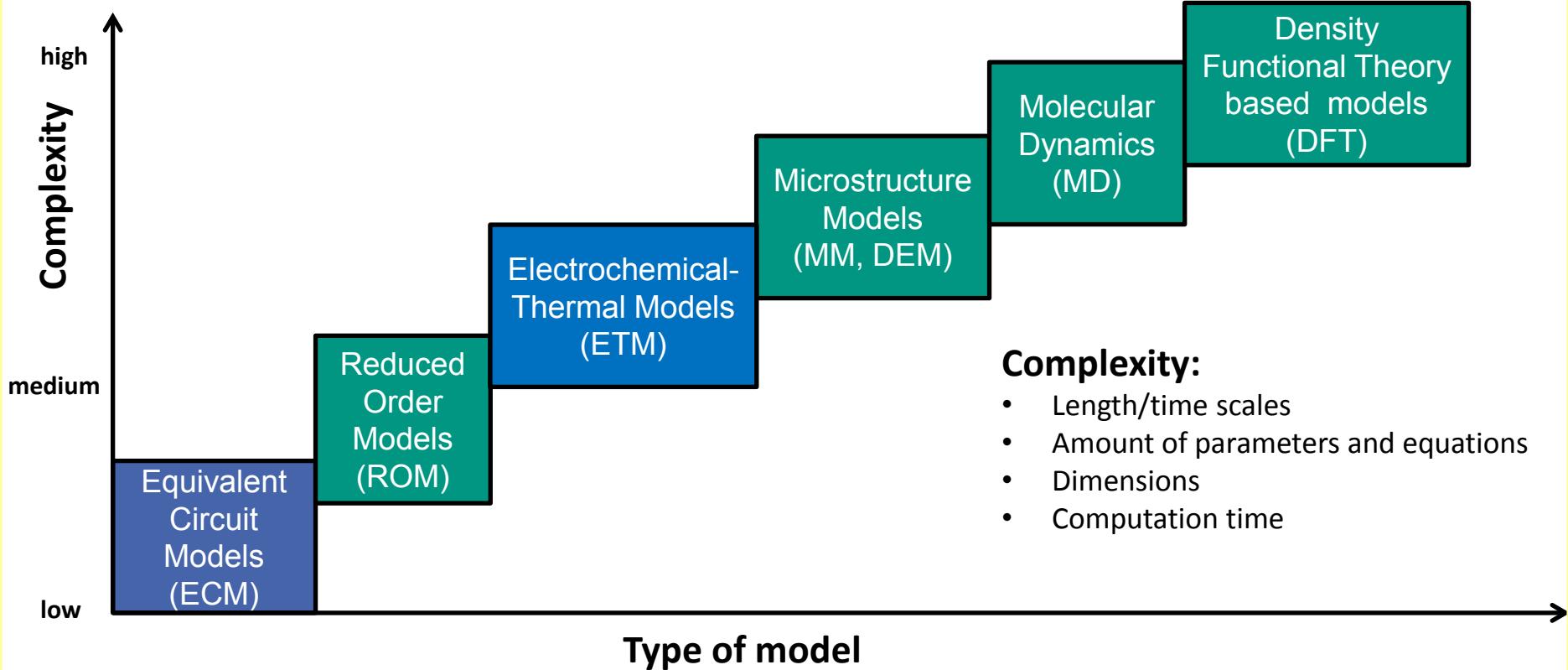
Red: heater mat for thermal runaway initiation

*Gray: protective material for cell 4 and lid of
battery box*

- **Extended time for thermal runaway propagation:
9 min**
- **Improved thermal protection: temperature
outside of battery box < 80 °C during thermal
runaway**

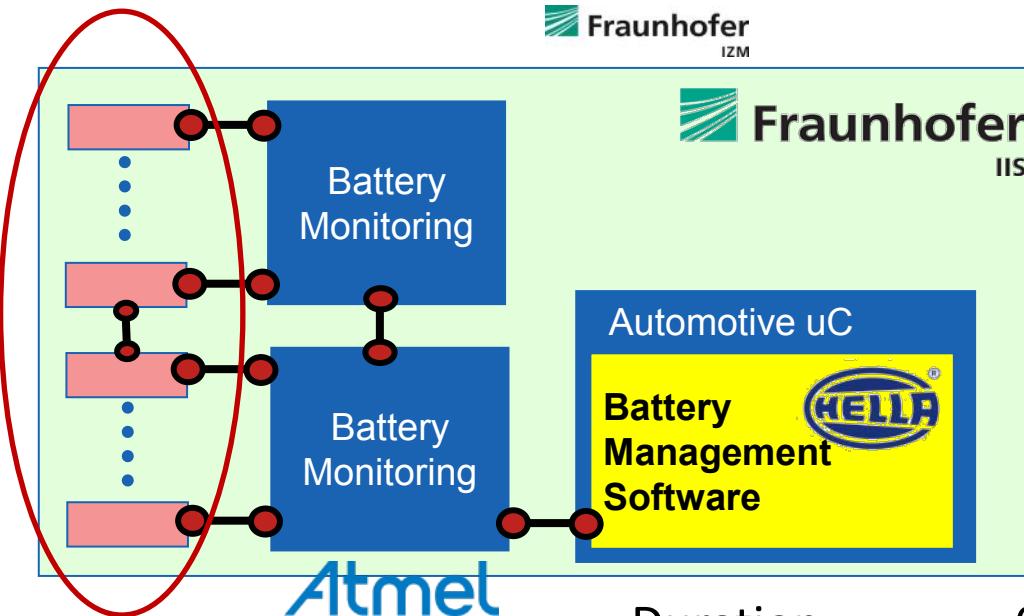


Modelling and Simulation



Integrated Components and Integrated Design of Energy Efficient Battery Systems

**ECM Cell
Modelling**



Automotive uC

Battery
Management
Software

Duration:

05/2013-07/2016

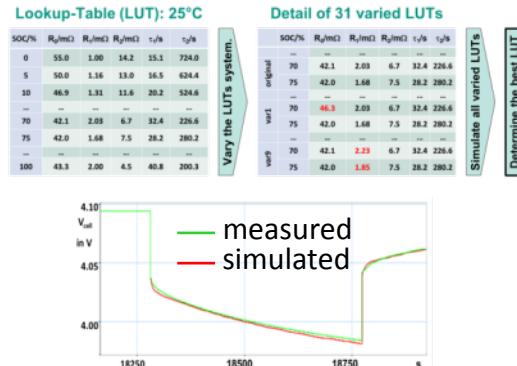
Budget:

7 Million Euro

Modelling Workflow

Measurements in battery calorimeters on cell and pack

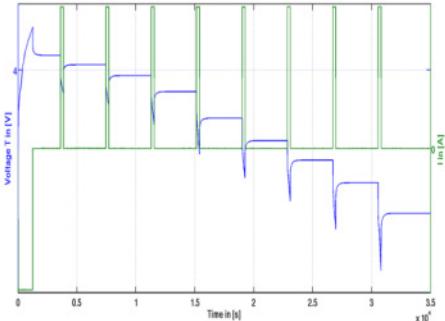
Cell Model Optimization



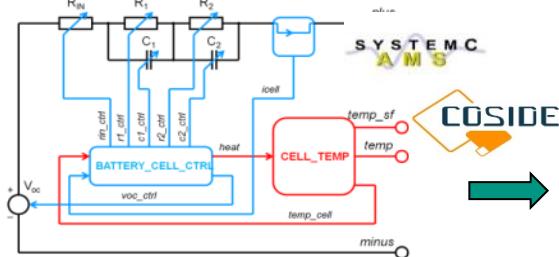
Cell Model Parametrization



6s1p
Pack



Cell Model Implementation



Battery model in BMS design platform

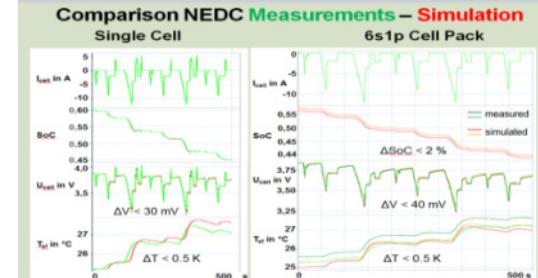
Cell Model Validation



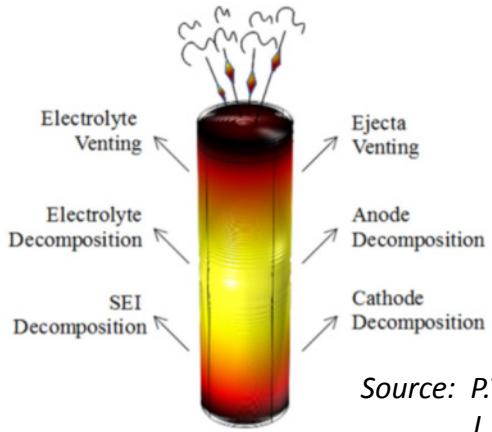
BMS Demonstrator



Atmel



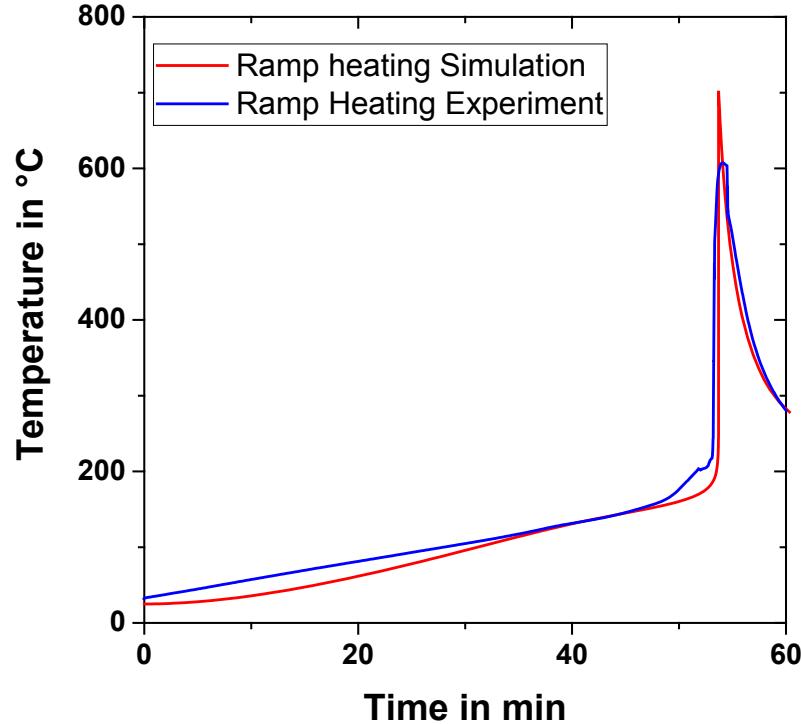
Electrochemical-Thermal Model: Lumped Matlab ODE model for ramp heating with venting



Source: P.T. Coman, S. Rayman, R. E. White,
J. of Power Sources **307** (2016) 56.

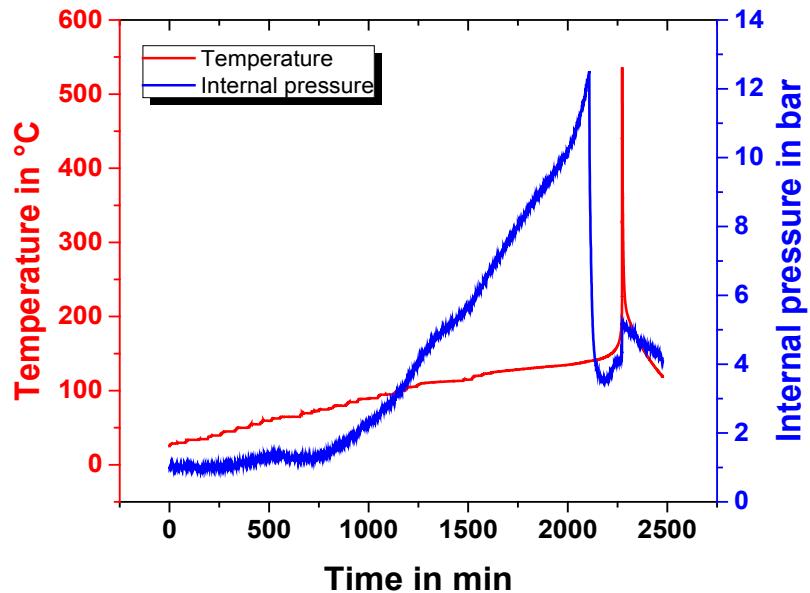
a model for ramp heating with ODEs representing:

- the decomposition rates
- the energy balance
- the ideal gas flow equations
- the burst condition for the trigger pressure
- the partial ejection of the jelly roll

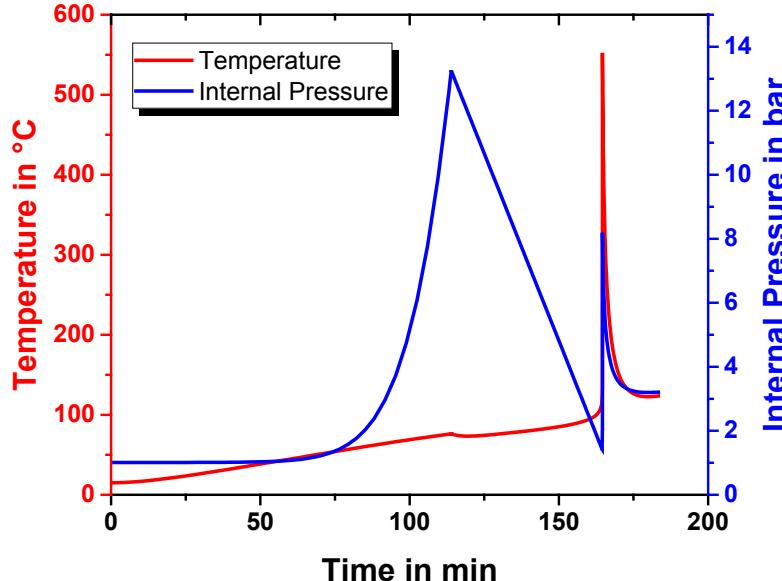


Thermal runaway including internal pressure evolution

Experiment (HWS)



Simulation (Ramp Heating)



Normal conditions of use

- Isoperibolic or adiabatic measurement

- Measurement of temperature curve and temperature distribution during cycling (full cycles,

For each: or application-specific load profiles), ageing studies

- Determination of the generated heat, Separation of heat in reversible and irreversible parts

Abuse conditions

- Thermal abuse: Heat-wait-seek test, ramp heating test, thermal propagation test
- External short circuit, nail penetration test
- Overcharge, deep discharge

- Temperature measurement

For each: ➢ External or internal pressure measurement

- Gas collection, Post Mortem Analysis, Ageing studies



Contact:

Phone: ++49/721608-22919

E-Mail: Carlos.Ziebert@kit.edu



Important data for BMS, TMS and safety

Thank You For Your Kind Attention

SPONSORED BY THE



This work has been partially funded by the Federal Ministry for Education and Research (BMBF) within the framework “IKT 2020 Research for Innovations” under the grant 16N12515 and is supervised by the Project Management Agency VDI|VDE|IT.

Additional funding by the German Research Foundation priority programme SPP1473 WeNDeLIB is gratefully acknowledged.



The authors would also like to thank Dr. Lukas Durrer from greenTEG AG for providing heat flux sensors and for helpful discussions.

