

Comparative effects of climate change and tidal stream energy extraction in a shelf sea

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Key Points:

- Numerical simulations of the present and future hydrodynamics of the NW European continental shelf are presented
- Tidal energy extraction and climate change both affect tidal elevation, currents and ocean stratification
- Climate change effects on ocean stratification are ten times larger than energy extraction effects

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14 **Abstract**

15 The environmental implications of tidal stream energy extraction need to be evaluated
16 against the potential climate change impacts on the marine environment. Here, we study
17 how hypothetical very large tidal stream arrays and a “business as usual” future climate
18 scenario can change the hydrodynamics of a seasonally stratified shelf sea. The Scottish
19 Shelf Model, an unstructured grid three-dimensional ocean model, has been used to re-
20 produce the present and the future state of the NW European continental shelf. Four
21 scenarios have been modelled: present conditions and projected future climate in 2050,
22 each with and without very large scale tidal stream arrays in Scottish Waters (UK). It
23 is found that where tidal range is reduced a few cm by tidal stream energy extraction,
24 it can help to counter extreme water levels associated with future sea level rise. Tidal
25 velocities, and consequently tidal mixing, are also reduced overall by the action of the
26 tidal turbine arrays. A key finding is that climate change and tidal energy extraction both
27 act in the same direction, in terms of increasing stratification due to warming and re-
28 duced mixing, however the effect of climate change is an order of magnitude larger.

29 **1 Introduction**

30 It is now widely recognised that there is a pressing need to mitigate the effects of
31 anthropogenically induced climate change and other environmental impacts of worldwide
32 reliance on fossil fuels. The actions to be taken to achieve a reduction of greenhouse gas
33 (GHG) emissions, and consequently the global mean temperature, include reducing emis-
34 sions from the power sector and encouraging investment in low-carbon technologies by
35 reforming the electricity market. The IPCC AR4 [Intergovernmental Panel on Climate
36 Change Fourth Assessment Report, *Solomon et al.*, 2007] was a key piece of evidence in
37 setting the EU’s 2050 target to cut GHG emissions to 80% - 95% below 1990 levels by
38 2050 [*European Commission*, 2011]. The more recent IPCC AR5 [Fifth Assessment Re-
39 port, *Stocker et al.*, 2013] brought even more certainty in these conclusions and “well be-
40 low 2°C above pre-industrial levels” is the global temperature warming limit to which
41 over 160 governments around the world have signed up with the Paris Agreement in 2015.

42 This widespread concern has led to a growing interest in alternative energy sources.
43 The first generation of renewable energy technologies, such as solar and wind, are now
44 available worldwide at commercially competitive prices. However, there is a pressing need
45 to further diversify the low-carbon generation capacity and more attention is being fo-

46 cused on the untapped source of energy from the marine environment. Ocean energy tech-
47 nologies (including tidal, wave and thermal) can be the next generation of renewable en-
48 ergy, which will be needed if we are to meet the 2050's objective of reducing GHG emis-
49 sions. Tidal stream energy extraction technology is currently more mature than wave
50 or thermal technologies, and there are more developers at full-scale demonstration stage.
51 The tidal energy sector has made significant progress towards commercialisation in the
52 UK, with the installation of the first tidal energy arrays in the Shetland Islands and the
53 Pentland Firth. A number of smaller tidal projects have also gone live in the EU and
54 in Canada [*Ocean Energy Systems*, 2016]. Those developments will lead the way for a
55 group of coastal states, including China, Japan, South Korea, Australia, New Zealand
56 and Chile, that potentially could harness the power of their local tides.

57 Many of the environmental problems the world faces today, including climate change,
58 air pollution, oil spills, and acid rain, result from worldwide reliance on fossil fuels, how-
59 ever since we need energy and there is an impact no matter how we generate it, the ob-
60 jective is to minimise it both locally and globally. Extracting energy from the ocean leaves
61 less energy in the ocean system, which will also have environmental impacts. The eco-
62 logical implications of marine renewable energy extraction need to be considered and eval-
63 uated against the possibly greater and global ecological threat of anthropogenically in-
64 duced climate change and other environmental impacts of the dependence on fossil fu-
65 els. In this context, the EcoWatt2050 project has been specifically designed to determine
66 ways in which marine spatial planning and policy development, can enable the maximum
67 level of marine energy extraction, while minimising environmental impacts. The present
68 paper is focused on tidal stream energy extraction and addresses the following questions:
69 (i) how can marine energy developments affect ocean hydrodynamic processes that can
70 be relevant for ecosystem habitats and animals' behaviour? (ii) how can we differenti-
71 ate the effects of climate change from energy extraction? (iii) are there ways in which
72 the deployment of marine renewables may ameliorate or exacerbate the predicted effects
73 of climate change? The results presented in this paper are now being used by further stud-
74 ies to understand how the physical changes will translate into impacts on ecosystem habi-
75 tats and animals' behaviour.

76 Observations of the effects of energy removal by large-scale tidal stream arrays are
77 not going to be possible until commercial-scale arrays have been deployed and operated
78 for several years. Hydrodynamic models are therefore the best tool to estimate how tidal

79 stream turbines may influence flow conditions. Evaluating the possible impacts might
80 help facilitate the exploitation of tidal energy by scaling and locating planned tidal en-
81 ergy farms to minimise harm to the marine environment. Furthermore, putting those
82 impacts in the context of the effects due to future climate change can help in better shap-
83 ing marine policies related to tidal energy developments. To date, only a few studies [*Karsten*
84 *et al.*, 2008; *Hasegawa et al.*, 2011; *van der Molen et al.*, 2016; *De Dominicis et al.*, 2017]
85 have focused on very far-field (>100 km) environmental effects of energy removal by tidal
86 stream turbines in different world locations. Among those only *van der Molen et al.* [2016]
87 and *De Dominicis et al.* [2017] have included atmospheric, oceanic and riverine forcing
88 in the model setup, which permits the study of impacts not only on the tidal dynam-
89 ics, but also on temperature, salinity, stratification and residual ocean circulation. This
90 is crucial, since these are the variables that affect the ocean ecosystems and habitat [*Scott*
91 *et al.*, 2010; *Holt et al.*, 2012; *Scott et al.*, 2013; *Wakelin et al.*, 2015; *Sadykova et al.*, 2017]
92 and are also going to be modified by future climate conditions in the NW European con-
93 tinental shelf. Coherent findings in the climate change literature for the region include
94 overall increases in sea level and ocean temperature, and a freshening of the North Sea,
95 which lead to changes in stratification and residual circulation [*Ådlandsvik*, 2008; *Holt*
96 *et al.*, 2010; *Mathis and Pohlmann*, 2014; *Schrum et al.*, 2016; *Tinker et al.*, 2016; *Mathis*
97 *et al.*, 2017].

98 The above mentioned studies looked at the effects of both climate change and tidal
99 energy extraction, however none of those aimed to examine to the combined effects of
100 climate change and energy extraction and to compare and differentiate their impacts.
101 Therefore, the aim of this work is to examine the ocean response to both very large tidal
102 stream turbine arrays in Scottish Waters and worst case future climate change condi-
103 tions. A typical annual cycle of the present NW European continental shelf hydrodynam-
104 ics was modelled, and compared with output for the same period of time perturbed by
105 very large-scale tidal stream energy extraction developments. In order to determine if
106 the latter may ameliorate or exacerbate the effects of future climate change on the ma-
107 rine system, the hydrodynamic conditions representative of the projected future climate
108 in 2050 were modelled, including two scenarios, one without tidal energy extraction de-
109 vices and a second with plausible very large scale tidal stream array layouts. This al-
110 lows us to evaluate the potential effect of climate change on the hydrodynamics and com-
111 pare it with the future state of the seas modified by large scale energy extraction.

112 The paper is organised as follows: Section 2 presents the methodology to design
113 (i) the tidal turbine arrays and (ii) the present and future climate model runs; Section
114 3 presents the results, in terms of estimate of (i) power available from Scottish Waters
115 and (ii) impacts on marine hydrodynamics of both tidal energy extraction and climate
116 change; Section 4 discusses the major outcomes, but also limitations and future expected
117 work and Section 5 highlights our conclusions.

118 2 Methodology

119 An unstructured grid coastal ocean model, FVCOM [Finite-Volume Community
120 Ocean Model, *Chen et al.*, 2003], was used to describe the hydrography and circulation
121 of the Scottish continental shelf waters, using an implementation known as the Scottish
122 Shelf Model [SSM, *Wolf et al.*, 2016]. The model domain includes the NW European con-
123 tinental shelf and extends beyond the shelf to include some of the adjacent north-east
124 Atlantic deep waters (see supporting information for the model bathymetry and full do-
125 main). It has a variable horizontal resolution, with horizontal node to node spacing rang-
126 ing from 10 - 20 km offshore down to 500 m - 1 km near the coast. The horizontal grid
127 is mainly refined in the water less than 200 m deep, i.e on the continental shelf (see sup-
128 porting information for the spatial distribution of the mesh size). The model mesh has
129 been built starting from the Global Self-consistent, Hierarchical, High-resolution Shore-
130 line [*GSHHS*] data for the coastline. For the vertical discretisation FVCOM uses a σ co-
131 ordinate system (terrain following coordinates), and the SSM implementation has 20 uni-
132 form layers. The SSM model bathymetry was supplied by the European Marine Obser-
133 vation and Data Network [*EMODnet*] and by the Northwest shelf Operational Oceanog-
134 raphic System [*NOOS*], the latter for the North Sea east of 0°E. The time step is 3 s
135 for the external mode (barotropic) and 18 s for the internal mode (baroclinic), as the gov-
136 erning equations can be solved in FVCOM using a split-mode method. The SSM uses
137 the ability of FVCOM of solving the equations directly in spherical coordinates, which
138 is important for basin or larger scale ocean application.

139 The SSM has been used (i) to design the large theoretical arrays of tidal stream
140 turbines, following a methodology described in Sec. 2.1; (ii) to reproduce present and
141 future ocean conditions in the NW European continental shelf, as described in Sec. 2.2
142 and 2.3; (iii) to estimate the maximum available power for electricity generation from

143 Scottish Waters, presented in Sec. 3.1; (iv) to evaluate the tidal energy extraction far-
 144 field effects during different seasonal and climatic conditions, shown in Sec. 3.2.

145 2.1 Very Large Scale Tidal Turbine Arrays Design

146 Areas where tidal stream energy developments should be deployed to minimise the
 147 impact to the environment and to be sustainable and economically viable to Scotland
 148 were identified by the Scottish Government [*The Scottish Government*, 2015] from an
 149 analysis of different users of the sea (fishing, oil and gas, marine protected areas, recre-
 150 ation etc.). The 10 “tidal plan option” sites are delimited by green lines in Fig. 1 and
 151 are the locations of the tidal stream arrays designed in this work. They can be classi-
 152 fied into three main regions: (1) the Pentland Firth and Orkney Waters (PFOW), that
 153 include the Pentland Firth, Westray, Eday and Sanday, (2) the Shetland Islands, to which
 154 Sumburgh, Yell Sound and Muckle Flugga belong and (3) the west coast of Scotland,
 155 that comprises South West Islay, Solway Firth and Mull of Kintyre.

156 The average power density (APD) in Scottish Waters is also shown in Fig. 1. APD
 157 is the power density in a vertical plane perpendicular to the tidal current direction, de-
 158 fined as

$$APD(i) = \left\langle \frac{1}{2} \rho \overline{|\mathbf{u}(i, t)|^3} \right\rangle_t \quad (1)$$

159 where ρ is the water density, $\overline{|\mathbf{u}(i, t)|}$ is the depth-averaged tidal current speed, $\langle \rangle_t$ stands
 160 for time-averaging over 30 days. APD has been estimated from a 30 days tide-only run
 161 of SSM forced by 8 tidal constituents (M_2 , S_2 , N_2 , K_2 , K_1 , O_1 , P_1 , Q_1), obtained from
 162 the TPXO7.2 model, the Oregon State University tidal inversion model of TOPEX/POSEIDON
 163 altimeter data [*Egbert and Erofeeva*, 2002]. Highest average power density areas are lo-
 164 cated in the PFOW, the Shetland Islands and the west coast of Scotland regions and are
 165 indeed in agreement with the areas identified for tidal energy developments.

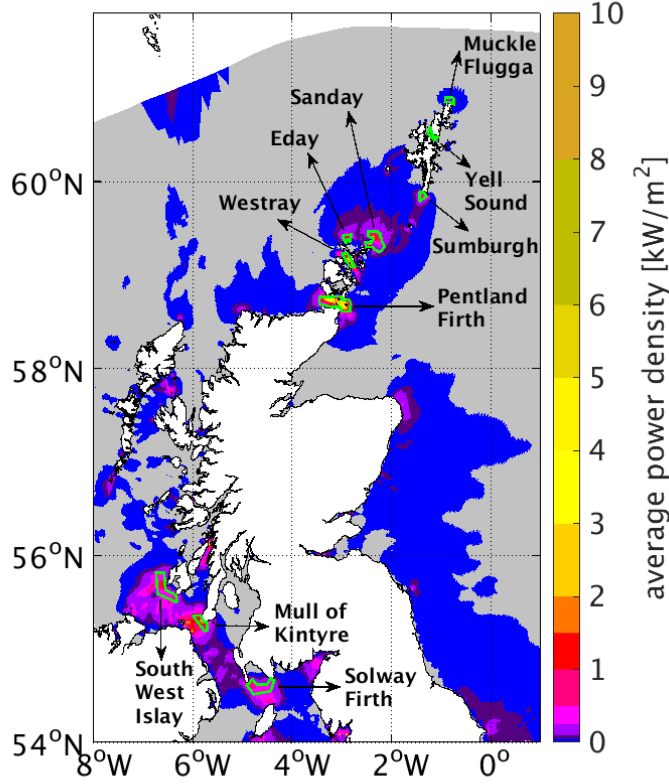
166 Starting from the 10 “tidal plan option” sites, large theoretical arrays of tidal stream
 167 turbines have been designed, which means identifying where and how many turbines should
 168 be deployed within those wider areas. The very large scale EcoWatt2050 tidal stream
 169 energy arrays for Scottish waters have been designed following a general method that
 170 considers three simple limitations: (i) a minimum water depth, 27.5 m; (ii) a turbine spac-
 171 ing limitation of 3 x 15 device widths; (iii) a capacity factor limit of 35%, following *De Do-*
 172 *minicis et al.* [2017]. The water depth limitation is driven by the choice of bottom-mounted

173 horizontal axis turbines, not a particular design, but a generic one, as described in *Bas-*
 174 *ton et al.* [2015], with 20 m diameter blades, which “weathervanes” into the tidal flow.
 175 The hub height has been set to be 15 m above the bed, giving a total height of 25 m.
 176 The turbine spacing is required to eliminate wake effects [*Myers and Bahaj*, 2010], giv-
 177 ing a minimum lateral spacing of 3 device widths and a minimum downstream spacing
 178 of 15 device widths. The capacity factor [*Polagye and Thomson*, 2013; *Robins et al.*, 2015]
 179 is defined as the ratio of the APD to the power density at the turbine rated speed, $|\mathbf{u}_R(i)|$:

$$CF(i) = \frac{\langle \frac{1}{2} \rho |\overline{\mathbf{u}(i, t)}|^3 \rangle_t}{\frac{1}{2} \rho |\mathbf{u}_R(i)|^3} 100 \quad (2)$$

180 In other words, the capacity factor is the ratio between the average instantaneous power
 181 and the maximum power (rated capacity) that can be generated by a turbine. Feasibil-
 182 ity studies suggest a capacity factor in the range 30%-40% for the lowest cost of tidal
 183 stream energy [*Bedard et al.*, 2006]. The rated speed is the current speed at which the
 184 turbine reaches its maximum efficiency; when it is exceeded, the power output reaches
 185 the limit that the electrical generator is capable of. The rated speed (and turbine de-
 186 sign) should be tuned (chosen) on the basis of the tidal regime in a particular site and
 187 within the limitations imposed by the turbine design (its electrical generator and struc-
 188 ture). In this work, we assumed the tidal turbines could have a rated capacity of between
 189 0.3 MW and 1 MW, i.e. with a rated speed in the range 1.25-2 m/s. For less energetic
 190 locations, such as Shetland Islands, we assumed turbines with a minimum rated capac-
 191 ity of 0.3 MW (rated speed 1.25 m/s), while for Solway Firth and South West Islay we
 192 hypothesised to use turbines with a rated capacity which can reach at lowest 0.5 MW
 193 (rated speed 1.5 m/s); for more energetic locations, such as the Mull of Kintyre and Orkney
 194 Waters, we assumed 0.7 MW (rated speed 1.75 m/s). For the Pentland Firth, the lim-
 195 its imposed were the same as those used by *De Dominicis et al.* [2017]. They are a more
 196 stringent constraint than for the other areas, assuming that the turbine has a rated speed
 197 of 2.5 m/s, i.e. rated capacity of 2 MW, and with a capacity factor limit increased to
 198 40%. The Pentland Firth area of search has been limited to the three main channels and
 199 to the PFOW Round One Development Sites, that are the sites for commercial renew-
 200 able energy development with lease agreement granted by The Crown Estate in 2010 [*The*
 201 *Crown Estate*, 2013].

205 The large scale arrays have been implemented in the SSM using the momentum
 206 sink approach, in which a momentum sink term represents the loss of momentum due



202 **Figure 1.** Average power density [kW/m^2] in Scottish Waters estimated from a 30 days SSM
 203 model run forced by 8 tidal constituents (M2, S2, N2, K2, K1, O1, P1, Q1), without including
 204 any feedbacks of tidal arrays on the flow. Green lines indicate areas identified for exploitation.

207 to tidal energy extraction. The effect of energy extraction on the fluid is simulated by
 208 implementing an additional retarding force equal and opposite to the thrust in the mo-
 209 mentum equations. According to Newton's third law of motion, the retarding, or drag,
 210 force exerted on the flow by a turbine is equal and opposite to the thrust, \mathbf{F}_T , exerted
 211 by the flow on the turbine.

$$\mathbf{F}_T = \frac{1}{2} \rho A C_T(i, t) |\mathbf{u}| \mathbf{u} \quad (3)$$

212 where C_T is the thrust coefficient, A is the area swept by the turbine and \mathbf{u} is the flow
 213 velocity. When the drag force is included in the 3D momentum equations, we consider
 214 the number of turbines in each model element and the vertical discretization of a tur-
 215 bine between multiple model layers. A full description of the momentum sink approach
 216 in FVCOM can be found in *Yang et al. [2013]* and *O'Hara Murray and Gallego [2017]*.

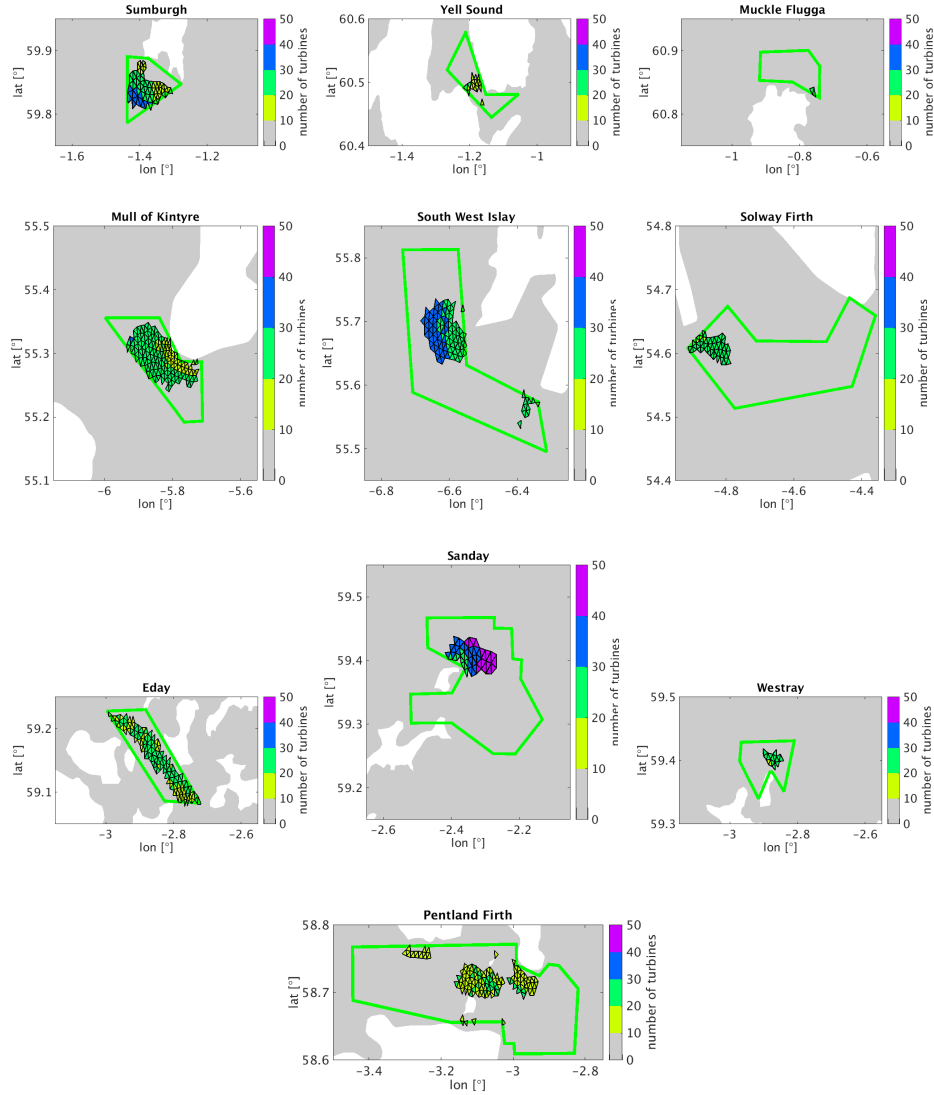
217 The turbine thrust coefficient can either be considered constant or more realistically var-
218 ied as a function of the flow speed in order to reproduce the turbine operation, which
219 is characterised by cut-in, cut-out and rated speed. In the present study, following *De Do-*
220 *minicis et al.* [2017], a variable thrust coefficient has been calculated using the generic
221 (i.e. not for a specific turbine design) thrust coefficient curve constructed in *Baston et al.*
222 [2015].

223 Since the turbines are sub-grid scale objects, a number of turbines is then allocated
224 to all model elements that are within the areas of search, with a capacity factor $> 35\%$
225 and a depth > 27.5 m. The number of turbines assigned to each model element is then
226 the maximum number of turbines that can be allocated, considering the size of the el-
227 ement and the spacing limits between turbines. As shown in Fig. 2 the number of tur-
228 bines assigned to each model element is usually in the range 10-40. The total number
229 allocated in Scottish Waters is ≈ 19000 : the number of turbines assigned to each loca-
230 tion is presented in Table 1.

235 **2.2 Present Climate Runs**

236 For the present day, the SSM was forced with climatologically averaged conditions
237 for the period 1990-2014, including atmospheric forcing, temperature and salinity at the
238 open boundary and fresh water input from rivers along the coastline. This choice allows
239 us to study the seasonal variability, but to ignore the inter-annual variability. The choice
240 of a time-slice of 25 years as the averaging period was determined by the need to sam-
241 ple sufficient natural variability to be able to average out the inter-annual variability, whilst
242 keeping the statistics within the time slice approximately stationary.

243 The climatological atmospheric forcing was built from a monthly 1990-2014 dataset
244 derived from ERA-Interim data [*ERA-Interim; Dee et al.*, 2011] data comprising mean
245 sea level pressure, precipitation, evaporation, relative humidity, temperature, thermal/solar
246 radiations and wind (for wind, 6 hourly/daily data were used to construct a monthly-
247 mean wind-stress which was then converted back into an equivalent wind field). Ocean
248 boundaries have been constructed using the monthly 1990-2014 data of temperature, salin-
249 ity, currents and sea elevation provided by the Atlantic Margin Model 7 km (AMM7, *O'Dea*
250 *et al.* [2012]; *Edwards et al.* [2012]) simulation. AMM7 is a NEMO model [*Madec and*
251 *the NEMO team*, 2016] implementation for the NW European continental shelf. The spe-



231 **Figure 2.** Number of turbines allocated in Orkney Waters (Pentland Firth, Eday, Sanday,
 232 Westray), west coast of Scotland (Mull of Kintyre, South West Islay, Solway Firth) and Shet-
 233 land Islands (Sumburgh, Yell Sound, Muckle Flugga) arrays. Black contoured elements are those
 234 occupied by tidal turbines. Green lines indicate the entire areas identified for exploitation

252 cific run used for SSM ocean boundaries was forced by the ERA-Interim reanalysis, thus
 253 being consistent with the atmospheric forcing chosen for the SSM model run. Hourly wa-
 254 ter elevation and tidal currents were added to the climatological currents and water el-
 255 evation (a representative average tidal year was selected as a climatological average for
 256 tides). Tidal currents and water elevations along the open boundary were obtained from

257 TPXO7.2, a global model of ocean tides based on the Oregon State University tidal in-
258 version of TOPEX/POSEIDON and Jason altimeter data [Egbert and Erofeeva, 2002].
259 Current velocities (residual and tidal), temperature, salinity and water elevation, after
260 being spatially interpolated, were prescribed at all the nodes and elements of the FV-
261 COM model boundary with a temporal resolution of 1 hour. The river runoff volume flux
262 climatology were obtained from the Centre for Ecology and Hydrology (CEH) Grid-to-
263 Grid (G2G) model [Bell *et al.*, 2007, 2009; Cole and Moore, 2009], covering the period
264 from 1962-2011 and including 577 rivers in Scottish Waters.

265 A full set of observed water level and current meter tidal analyses over the NW Eu-
266 ropean Shelf and into deep water just off the shelf were used to validate the model: for
267 tidal elevation amplitude the root mean square error is 0.3 m and the bias is -0.07 m,
268 while for tidal currents the root mean square error is 0.1 m/s and bias is 0.02 m/s. The
269 present climatological conditions for sea surface temperature and salinity reproduced by
270 the SSM have been compared with the World Ocean Atlas [Boyer *et al.*, 2013] regional
271 climatology (see supporting information). Furthermore, the model has been also run for
272 a specific period of time to further validate water levels, currents and temperature and
273 salinity against observed data (full model validation is presented in Wolf *et al.* [2016]).

274 **2.3 Future Climate Runs**

275 Future climate is partly determined by the magnitude of anthropogenic emission
276 of GHGs, aerosols and other natural and man-made forcings. The climate system is shaped
277 by the Earth’s response to those external forcings, along with internal variability inher-
278 ent in the climate system. The Representative Concentration Pathways (RCPs) describe
279 four different 21st century pathways of GHG emissions and atmospheric concentrations,
280 air pollutant emissions and land use [Stocker *et al.*, 2013] and are the basis for climate
281 model projections. The RCPs include a stringent mitigation scenario (RCP2.6), two in-
282 termediate scenarios (RCP4.5 and RCP6.0) and one scenario with very high GHG emis-
283 sions (RCP8.5) [Stocker *et al.*, 2013], termed the “business as usual” or “worst case” sce-
284 nario. Different climate models provide alternative representations of the Earth’s response
285 to those forcings, and of natural climate variability. For the last IPCC report, a stan-
286 dard set of coordinated climate model experiments were inter-compared in the frame-
287 work of the Coupled Model Intercomparison Project [CMIP5; Taylor *et al.*, 2012]. There
288 is then a range of plausible projections for future climate that arise from the future emis-

289 sions uncertainty and from the model uncertainty. One single projection (one single model
 290 and one future emission scenario) was chosen to force the SSM model: the HadGEM2-
 291 ES forced by the RCP8.5 scenario. HadGEM2-ES [*The HadGEM2 Development Team*
 292 *et al.*, 2011] is a coupled Earth System Model that has been used by the Met Office Hadley
 293 Centre for the CMIP5 simulations. HadGEM2 is a configuration of the Met Office Uni-
 294 fied Model (UM) developed from UM version 6.6. HadGEM2-ES was the first Met Of-
 295 fice Hadley Centre model to include Earth system components as standard. The HadGEM2-
 296 ES climate model includes an atmospheric model at N96 and L38 horizontal and ver-
 297 tical resolution, and an ocean model with a 1-degree horizontal resolution (increasing to
 298 1/3 degree at the equator) and 40 vertical levels. Earth system components included are
 299 the terrestrial and ocean carbon cycle and tropospheric chemistry. This model is one of
 300 the top-performing climate models for the North Atlantic, having small biases in winter-
 301 time position and median latitude of storms, consistent with reanalysis data [*Zappa et al.*,
 302 2013].

303 For a given choice of forcing data, a straight-forward approach is the direct use of
 304 the climate model data as ocean boundary and atmospheric forcing data for the present
 305 day run and the future climate change scenario. The climate change signal is then the
 306 difference between both model run realisations. The problem with this approach is that
 307 the climate model output shows regional- and parameter-dependent biases, for both at-
 308 mospheric and ocean components. Such biases will have a significant impact on processes
 309 such as stratification and upwelling. Where these are non-linearly dependent on the forc-
 310 ing variables, the biases will not cancel when the climate change signal is calculated. An
 311 alternative climate impact assessment method is the “delta-change” approach. In this
 312 method, the present day climate forcing is provided by a present day reference forcing,
 313 derived from the atmospheric ERA-Interim reanalysis alongside appropriate oceanic con-
 314 ditions (AMM7-NEMO run also forced with ERA-Interim reanalysis). This approach re-
 315 moves the influence of biases from the climate model forcings and preserves the mean
 316 climate change signal, that is the most robust part of the signal from climate models.
 317 The climate change forcing is then derived by perturbing the reference forcing with a mul-
 318 tiplicative (Eqs. 4-5) or an additive spatially varying correction (Eqs. 6-7), that is a func-
 319 tion of the future climate change forcing in relation to its present day control:

$$\phi_f = \phi_{REF} F_M \quad (4)$$

$$F_M = \phi_{RCP8.5} / \phi_{CNTRL} \quad (5)$$

320

$$\phi_f = \phi_{REF} + F_A \quad (6)$$

321

$$F_A = \phi_{RCP8.5} - \phi_{CNTRL} \quad (7)$$

322 where ϕ_f is any atmospheric or oceanic model variable and F_M and F_A are the multi-
 323 plication and additive corrections, respectively, f indicates the perturbed variable; *REF*
 324 is the reanalysis reference: 1990-2014 ERA-Interim (atmospheric forcing) and 1990-2014
 325 AMM7-NEMO forced by ERA-Interim (ocean boundaries); *CNTRL* is the climate model
 326 control period: 1990-2014 HadGEM2-ES (atmospheric forcing and ocean boundaries);
 327 *RCP8.5* is the climate model future scenario period: 2038-2062 (i.e. centred on 2050)
 328 HadGEM2-ES (atmospheric forcing and ocean boundaries). The river freshwater discharges
 329 were not perturbed, due to lack of information about future precipitation over Scottish
 330 catchments.

331 An additive correction was used for atmosphere and ocean temperature, wind and
 332 ocean current velocity component and sea surface height (SSH). It was disregarded for
 333 the rest of the variables owing to problems with negative values of variables which are
 334 always defined positive. Since the inter-annual variability of the future and control sim-
 335 ulations are not related (in time), the fields must be appropriately time-averaged before
 336 calculating the perturbation to the reference simulation. We used the climatological monthly
 337 values, so preserving the seasonal cycle. HadGEM2-ES and ERA-Interim are on differ-
 338 ent grids, and thus required a further interpolation step (only using sea points) before
 339 applying the “delta-change” approach. Additionally, the SSH correction required an ad-
 340 hoc procedure. In state-of-the-art global ocean models, such as HadGEM2-ES, SSH is
 341 an anomaly with respect to the globally averaged SSH, which can have an unphysical
 342 trend in time. Global ocean models typically use the Boussinesq approximation, and so
 343 conserve volume but not mass [*Griffies and Greatbatch, 2012*] and steric effects are cal-
 344 culated as a diagnostic. Thus, the additive correction for SSH has been corrected to elim-
 345 inate the globally average mean sea level trend and to add the globally averaged steric
 346 sea level change [*Jackson and Jevrejeva, 2016*]. This procedure allows the sea level rise,
 347 as predicted by the RCP8.5 scenario, to be imposed along the model domain boundary
 348 .

3 Results

3.1 Available Tidal Power Resource in Scottish Waters

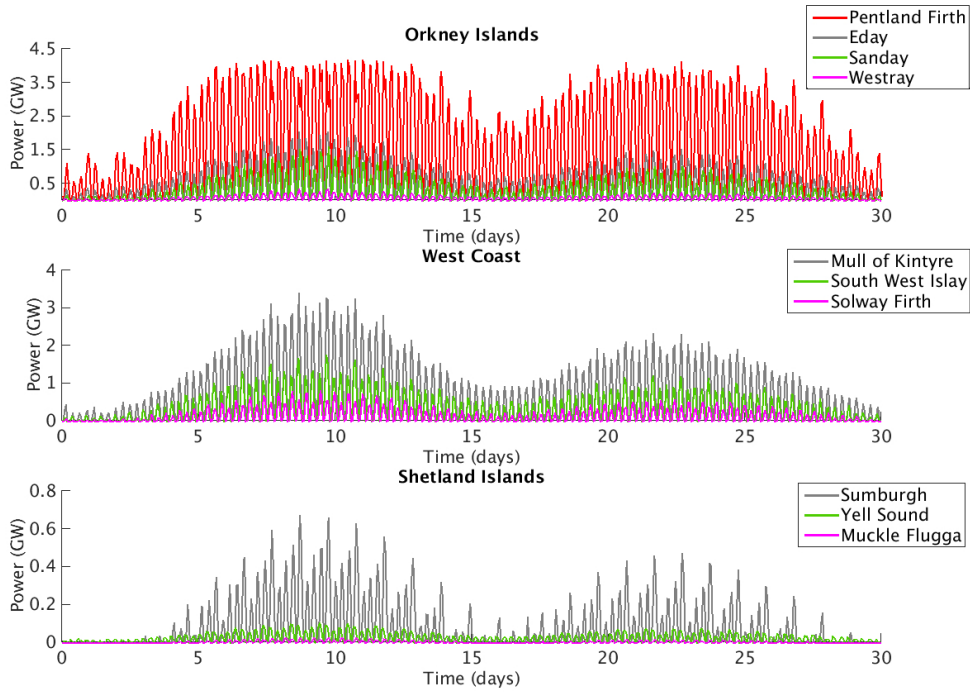
The power that can be generated is dependent on the vertical cross-sectional area occupied by tidal stream turbines and is the work done by the thrust force per unit of time:

$$P(i, t) = \frac{1}{2} \rho AN(i) C_T(i, t) \overline{|\mathbf{u}(i, t)|}_T^3 \quad (8)$$

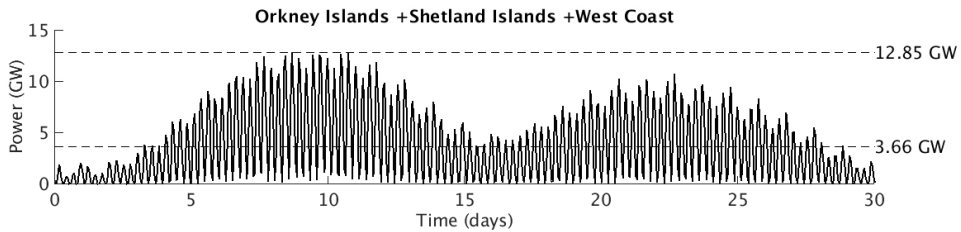
where $\overline{|\mathbf{u}(i, t)|}_T = \sum_{k=1}^{k=n} K_\sigma(i, k) |\mathbf{u}(i, k, t)|$ is the weighted average of the current speed over the diameter of the tidal turbine. It can therefore be considered to be the maximum available power for electricity generation at any instant in time.

Fig. 3 shows the power provided by each location calculated from a 30-day SSM run forced by 8 tidal constituents. The power calculation included the feedbacks of tidal energy extraction on the flow and assumed a variable thrust coefficient, giving us an estimate of the so-called practical resource. The specific geometry of the North Sea basin implies a tidal amplification in the semi-diurnal spectral range [*Sündermann and Pohlmann, 2011*]. As a tidal energy device will generate electricity during the flood and ebb phases of the tidal cycle, peak power is available every 6 hours. The superposition of the semidiurnal principal lunar and solar tides ($M_2 + S_2$), which are in phase every ≈ 14.75 days, causes a significant spring (in-phase) and neap (out-of-phase) rhythm in the power availability. Fig. 3 (top panel) shows the practical resource available from the arrays located in Orkney Waters. The temporal average power available from the Pentland Firth is 1.64 GW, in agreement with what was obtained when running the model with only the Pentland Firth array included (1.63 GW, *De Dominicis et al. [2017]*). However, there is an increase of 0.01 GW, which is due to the combined operation of the other tidal arrays.

All the other Orkney Islands sites (Eday, Sanday, Westray, Fig. 1) can potentially provide similar power to each other. Indeed, the average per turbine are similar in the three locations, with Westray being slightly more energetic, showing a maximum power per turbine of 1 MW (see Table 1). The difference in the total amount of power provided is mainly due to the number of turbines virtually deployed in the model (Fig. 2), that were constrained by depth and capacity factor limits. The Eday array scenario can produce the most power, with an average of 0.45 GW and a maximum of 2.04 GW. How-



371 **Figure 3.** Power resource from a SSM run forced by 8 tidal constituents (M_2 , S_2 , N_2 , K_2 , K_1 ,
 372 O_1 , P_1 , Q_1) including the feedbacks of tidal stream energy extraction on the flow and using a
 373 variable thrust coefficient: PFOW (top panel); west coast of Scotland (central panel); Shetland
 374 Islands (bottom panel).



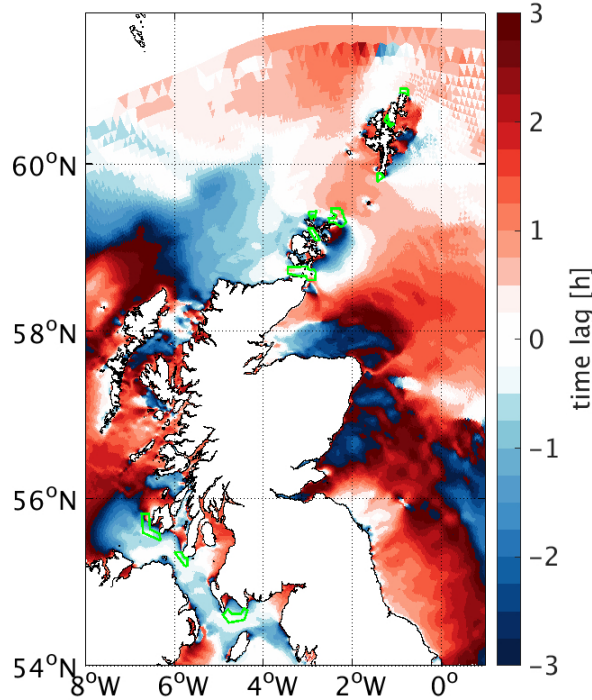
375 **Figure 4.** Aggregated power resource from all tidal arrays in Scottish Waters from a SSM run
 376 forced by 8 tidal constituents (M_2 , S_2 , N_2 , K_2 , K_1 , O_1 , P_1 , Q_1) including the feedbacks of tidal
 377 stream energy extraction on the flow and using a variable thrust coefficient, with the temporal
 378 mean average and maximum values shown.

386 ever, it must be noted that to achieve $\approx 30\%$ of the average practical resource available
 387 from the Pentland Firth (and half of the maximum) requires roughly the same number
 388 of turbines as deployed in the Pentand Firth (see Table 1).

389 Looking to the west coast of Scotland, South West Islay and the Solway Firth (Fig.
390 1) show equal average power per turbine (see Table 1), with the South West Islay array
391 providing more power than the Solway Firth (Fig. 3 - central panel), due to the larger
392 number of turbines deployed (see Table 1). The Mull of Kintyre site is as energetic as
393 the Orkney Waters locations (Eday, Sanday, Westray), in terms of average and maxi-
394 mum power per turbine (see Table 1). However, given the wider area considered avail-
395 able for exploitation (Fig. 2), a larger number of turbines were included, leading to a to-
396 tal average practical resource of 0.67 GW and a maximum of 3.40 GW. This appears to
397 be the second most energetic location in Scottish Waters. It must be noted, as for Eday,
398 that to achieve just $\approx 40\%$ of the practical resource available from the Pentland Firth
399 it is necessary to increase by $\approx 55\%$ the number of turbines used in the Pentland Firth.
400 However, the Pentland Firth would require turbines with a rated power on average of
401 1.5 MW (see Table 1), while turbines rated at 1 MW on average would be suitable for
402 the rest of the Orkney Waters and west coast of Scotland locations.

403 The Shetland Islands locations (Sumburgh, Yell Sound, Muckle Flugga, Fig. 1) are
404 less energetic, with the lowest average (Sumburgh) and maximum power (Yell Sound)
405 per turbine (see Table 1) and a smaller area to be exploited (Fig. 2). Despite the smaller
406 number of turbines and lower extractable power, the amount of energy available could
407 satisfy the present Shetland Islands electricity demand (11-50 MW, Scottish Hydro Elec-
408 tric Power Distribution, <https://www.ssepd.co.uk/ShetlandEnergy/>). However, as Fig.
409 3 (bottom panel) shows, the Muckle Flugga array cannot extract any power during neap
410 tides, despite being the most energetic one during spring tides (in Shetland Waters, see
411 maximum power per turbine in Table 1). This is due to the generic turbine design that
412 has been considered in this work, with a cut-in speed of 1 m/s, thus not allowing any
413 power to be generated if the flow speed is lower. For the Shetland Islands locations it
414 would be better to deploy turbines with a lower cut-in speed, which are likely to be de-
415 veloped in future generations of tidal energy devices [Neill *et al.*, 2014].

418 From the estimate of the practical resource available from all locations we get an
419 average instantaneous power of 3.66 GW. The maximum power available from all loca-
420 tion is 12.85 GW (Fig. 4), which is only slightly less than summing up the maximum
421 power from each location (14.83 GW, see Table 1). This tells us that the peak power oc-
422 curs almost at the same time in all locations, indicating minimal phase diversity among
423 these high tidal energy sites, as also found by Neill *et al.* [2016]. This will provide an in-



416 **Figure 5.** Time lag indicates the time of peak currents relative to the timing of peak currents
 417 in the Pentland Firth, green lines indicate areas identified for tidal energy exploitation.

424 intermittent availability of power. If we assume that a tidal energy device will generate
 425 electricity equally during the flood and ebb phases of the tidal cycle, then an optimal
 426 complementary time lag between two sites would be 3.1 h, i.e. a quarter of the tidal cy-
 427 cle [Neill *et al.*, 2016]. The time lag, shown in Fig. 5, indicates the time of peak currents
 428 relative to the time of peak currents in the Pentland Firth and it is calculated as the dif-
 429 ference in the M_2 phase. It is shown that the time lags for peak currents between all the
 430 tidal arrays locations and the Pentland Firth are always within ± 1 h, as reported in Ta-
 431 ble 1.

437 The practical resource available for electricity generation from each of the 10 tidal
 438 plan options has been further calculated from a 1 year fully forced SSM run with present
 439 and future climate conditions, as it is suggested by Robins *et al.* [2015] that even pre-
 440 liminary resource assessments should be based on annual average power density. We found
 441 that including the wind and buoyancy driven currents adds 0.01-0.03 GW to the tem-

432 **Table 1.** For each of the 10 tidal plan options: total number of turbines, N_T , average and
 433 maximum instantaneous available power, P_{AVG} and P_{MAX} , average power per turbine and max-
 434 imum power per turbine, P_{AVG-T} and P_{MAX-T} and peak power time lag. Estimates are from
 435 a 30-day SSM model run forced by tides only with tidal stream energy extraction feedbacks
 436 included.

Location	N_T	P_{AVG} [GW]	P_{MAX} [GW]	P_{AVG-T} [MW]	P_{MAX-T} [MW]	Time lag [h]
Pentland Firth	2784	1.64	4.16	0.59	1.49	
Eday	2853	0.45	2.04	0.16	0.71	-0.2
Sanday	1935	0.29	1.58	0.15	0.82	+0.3
Westray	325	0.06	0.32	0.18	1.00	-0.9
Mull of Kintyre	4290	0.67	3.40	0.16	0.79	-0.6
South West Islay	3651	0.32	1.74	0.09	0.48	-0.6
Solway Firth	1379	0.13	0.79	0.09	0.57	-0.3
Sumburgh	1758	0.08	0.67	0.04	0.38	+0.3
Yell Sound	292	0.02	0.10	0.08	0.35	-0.9
Muckle Flugga	43	0.003	0.03	0.06	0.60	0

442 poral average instantaneous power available in the Pentland Firth, Sanday, Mull of Kin-
 443 tyre, South West Islay and Solway Firth. The average instantaneous power available at
 444 the other locations does not increase (see Table 2). The total average power available
 445 for electricity generation is 3.78 GW. The maximum power resource is usually 0.20-0.25
 446 GW larger than the tide-only estimation in Eday, Sanday, South West Islay, Solway Firth
 447 (see Table 2). The maximum power does not change for the Pentland Firth, while the
 448 Mull of Kintyre location shows a peak 0.76 GW larger than the tide-only estimation (see
 449 Table 2), which might be connected to strong wind events during the year. As expected
 450 tides are thus confirmed to be the most important available contribution to the energy
 451 available from currents in these highly energetic tidal locations, with spring peak power
 452 resources that can be further enhanced if in conjunction with strong wind events.

453 **Table 2.** Average power per turbine and maximum power for the 10 tidal plan options from
 454 1 year fully forced run with present, P_{AVG}^{PRE} and P_{MAX}^{PRE} , and future, P_{AVG}^{FUT} and P_{MAX}^{FUT} , climatic
 455 conditions. Tidal stream energy extraction feedbacks on the flow were included.

Location	P_{AVG}^{PRE} [GW]	P_{MAX}^{PRE} [GW]	P_{AVG}^{FUT} [GW]	P_{MAX}^{FUT} [GW]
Pentland Firth	1.67	4.19	1.68	4.19
Eday	0.45	2.25	0.46	2.30
Sanday	0.31	1.78	0.32	1.80
Westray	0.06	0.37	0.06	0.37
Mull of Kintyre	0.70	4.16	0.70	4.17
South West Islay	0.34	2.01	0.34	2.00
Solway Firth	0.14	1.00	0.14	1.02
Sumburgh	0.08	0.71	0.09	0.75
Yell Sound	0.02	0.11	0.03	0.12
Muckle Flugga	0.003	0.03	0.003	0.03

456 For future climate conditions we observed that the average instantaneous practi-
 457 cal resource either stays the same as the present day or increases by up to 0.01 GW, with
 458 peak power showing about the same values as the present climate conditions (see Ta-
 459 ble 2). Climate change will not then alter the resource estimate, which will show min-
 460 imal increases in some locations and a future total average practical resource of 3.82 GW.

461 **3.2 Impacts of Climate Change and Tidal Energy Extraction on Hydro-** 462 **dynamics**

463 **3.2.1 Tidal Dynamics**

464 The ocean response to tidal stream energy extraction was first analysed at the tem-
 465 poral scale of a spring-neap tidal cycle, examining changes in tidal dynamics. The main
 466 Atlantic semidiurnal M_2 Kelvin wave travels from south to north. Energy is transmit-
 467 ted across the shelf edge into the Celtic Sea between France and southern Ireland [*Robin-*
 468 *son, 1979*]. The tidal wave then progresses northwards, taking 5 hours to travel from the

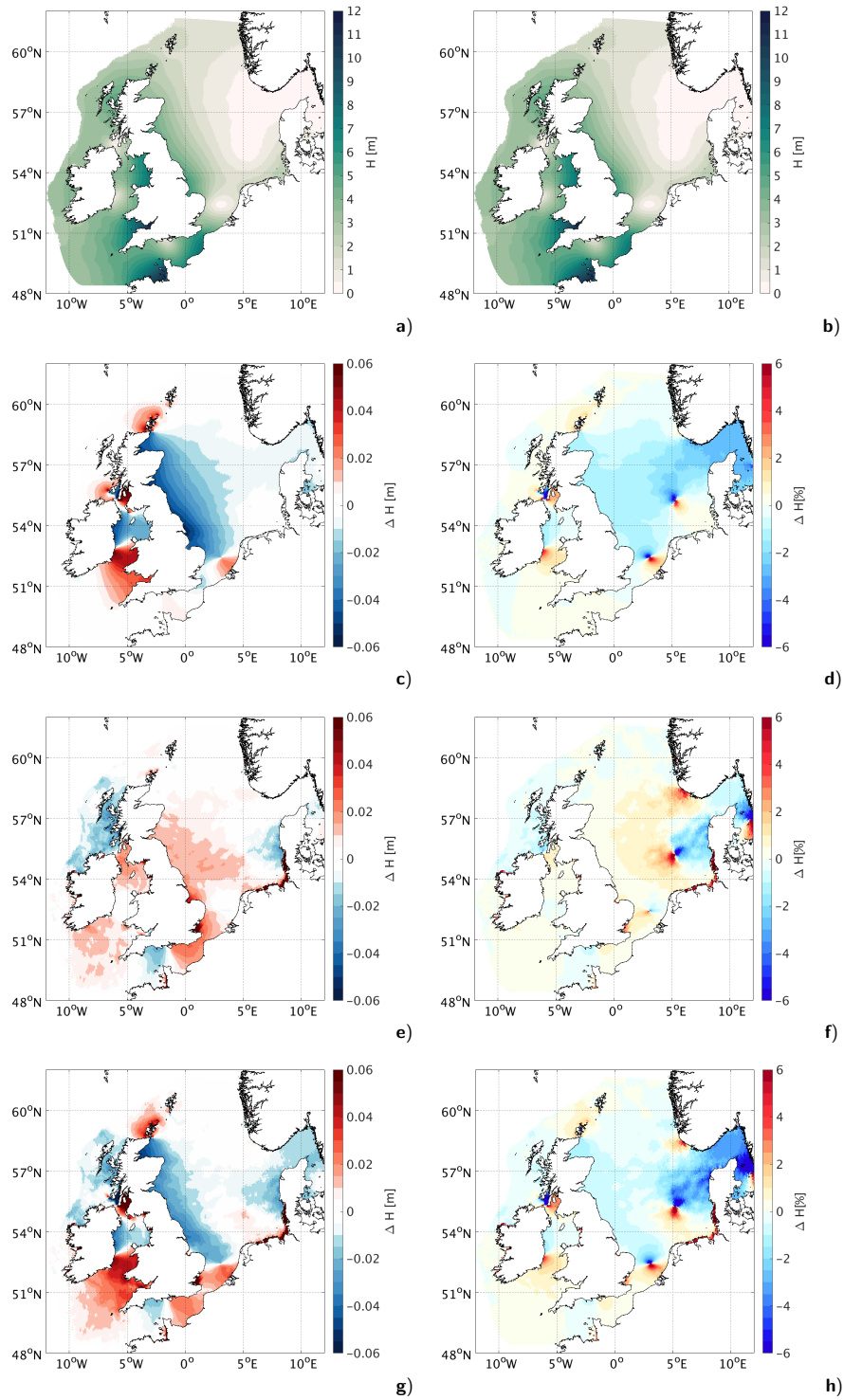
469 Celtic Sea to the north of Scotland and it is partly diffracted around the north of Scot-
470 land, where it turns east, travels southward along the east coast of Scotland into the North
471 Sea [Pugh, 1996] and moves anti-clockwise as a Kelvin wave through the entire basin.
472 Far-field effects on tidal elevation show increases upstream of the tidal farms locations
473 (considering the direction of propagation of the tidal wave), while a decrease is observed
474 downstream, along the UK east coast and also in the Irish Sea. A meaningful measure
475 of change, when thinking about coastal management, is the change in the mean spring
476 tidal range, indicating the mean tidal range during spring high and low water and thus
477 taking into account also the influence of the S_2 tidal constituent (mean spring tidal range
478 is defined as twice the sum of the M_2 and S_2 amplitudes). The decrease in mean spring
479 tidal range is up to 6 cm (Fig. 6c) along the whole east coast of the UK and it is caused
480 by the energy dissipation of the incoming Atlantic wave travelling through the tidal stream
481 turbines in the Pentland Firth. There are also far-field changes in the tidal elevation of
482 this magnitude upstream of the Pentland Firth, but covering a much smaller area (Fig.
483 6c).

484 In the Irish Sea, the extra energy dissipation along the west coast of Scotland in-
485 teracts with two Kelvin-type waves, one that progresses from the southwest through St.
486 George's Channel and a second one that is transmitted south through the North Chan-
487 nel [Robinson, 1979]. This generates one area of tidal range decrease in the middle of
488 the Irish Sea and two areas of increase upstream of the north and south entrances, lead-
489 ing up to 6 cm increase in tidal range in the St. George's Channel (Fig. 6c). As shown
490 in Fig. 6d) the above mentioned changes are within $\pm 1-2\%$, unless close to the amphidromes,
491 where a small change in the amphidrome locations results in a large percentage change
492 in tidal elevation. These changes to tidal elevation due to tidal turbines were found to
493 be broadly the same under the future climate hydrodynamic conditions (future baseline
494 is in Fig. 6b, differences are not shown).

495 Many modelling studies [Pickering *et al.*, 2012; Ward *et al.*, 2012; Pelling *et al.*,
496 2013; Idier *et al.*, 2017] have investigated the effect of sea level rise (SLR) on tides, and
497 it has been suggested that even moderate SLR can have impact on the tides on the Eu-
498 ropean Shelf. However, there are discrepancies between the predicted changes, mainly
499 due to the different scenarios analysed, spatially uniform or non-uniform SLR ranging
500 from 0.5 m to 10 m and with no inundation (fixed coastline) or change in coastal geo-
501 morphology (allowing coastline recession) conditions. The latter has been found to be

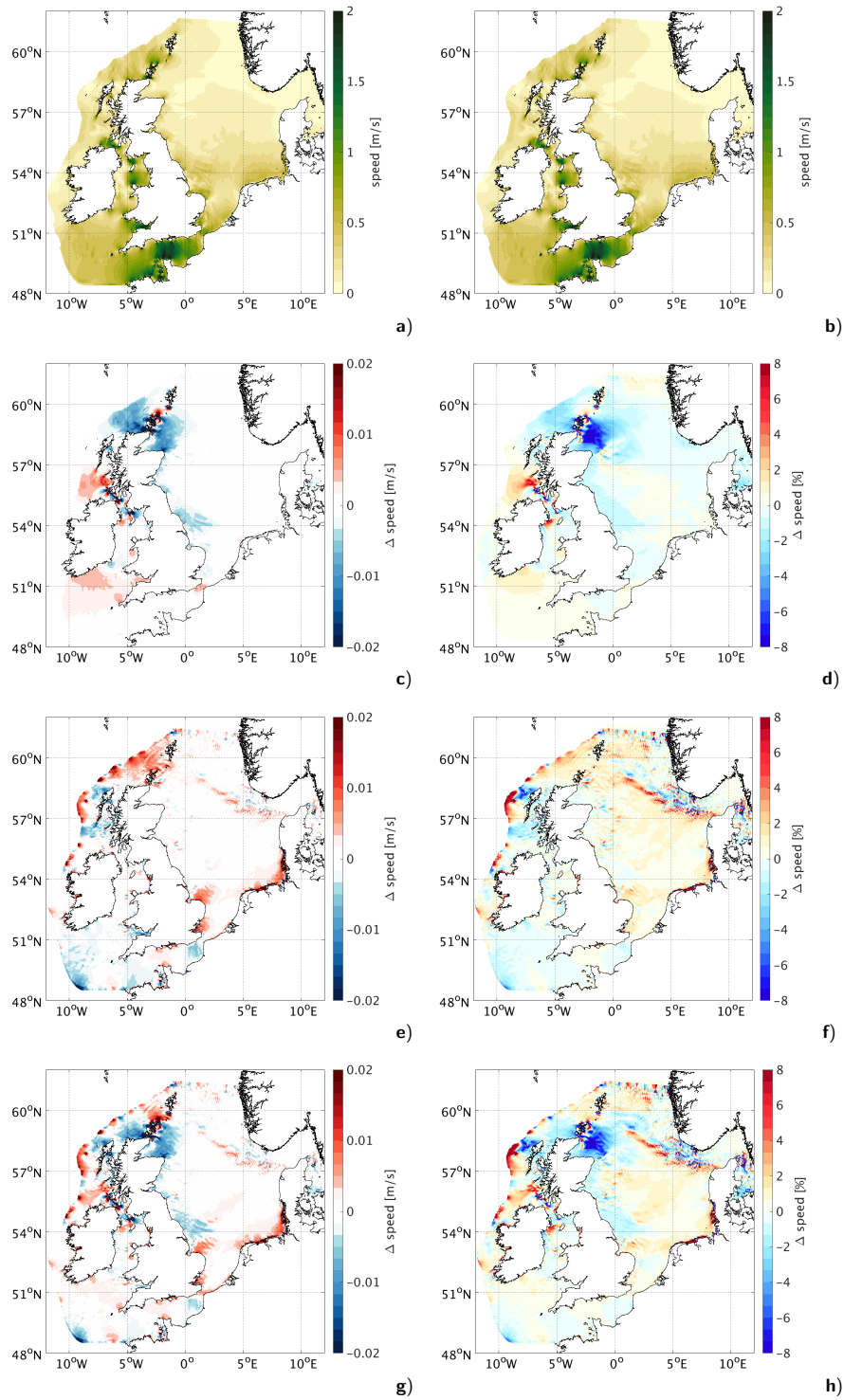
502 relevant only for sea level increase > 1 m [Pickering et al., 2017]. Our results account
503 for a spatially non-uniform SLR, as we imposed the globally averaged steric change in
504 sea level, as predicted by the RCP8.5 scenario, only along the model domain boundary,
505 leading to a ≈ 15 -30 cm non-uniform SLR by 2050 in the interior of the model domain.
506 Fig. 6e shows the change in mean spring tidal range due to climate change. There is a
507 spatial mixture of increases and decreases in mean tidal range. There are decreases in
508 the northwest of Scotland, the western English Channel, the Shetland Islands and north
509 of the Southern Bight (decrease is < 1 cm and $< 1\%$ for the SLR scenario analysed in this
510 paper, very light blue in Figs. 6e and 6f). The increases mainly occur in the North Sea,
511 the eastern English Channel, the central and the southernmost Irish Sea up to the French
512 Atlantic coast. Fig. 6f shows percentage changes that exceed 5% only in the vicinity of
513 the North Sea amphidromic points. *Idier et al.* [2017] analysed a similar scenario (non
514 uniform, ≈ 50 cm by 2100) and found the same high-tide level pattern of changes (ab-
515 solute changes are different due to different scenarios and here we are showing mean spring
516 tidal range differences rather than high-tide level).

517 Comparing tidal stream energy extraction and climate change, we found that both
518 can have an impact on tidal elevation of the order of a few centimetres. These changes
519 broadly occur in similar geographic areas, and can have the opposite effect on sea level
520 height. Indeed, summing up the effects of tidal energy extraction and climate change (Fig.
521 6g and Fig. 6h), the far-field decrease in the mean spring tidal range along the whole
522 east coast of the UK, generated by the turbines' action, can possibly counteract the in-
523 crease due to climate change along the same coastline. The same can be said for the Cen-
524 tral Irish Sea. However, it should be noted that in the near-field of the tidal farms (not
525 shown in this paper) the increase in tidal range can be the dominant effect [*De Domini-*
526 *cis et al.*, 2017]. The increase in tidal range on the western Scottish coast due to tidal
527 stream energy extraction can be eventually offset by the decrease due to climate change
528 (Fig. 6g and Fig. 6h). On the other hand, the southernmost part of the Irish Sea and
529 the Dutch coast are exposed to an increase in tidal range by both tidal stream energy
530 extraction and climate change (Fig. 6g and Fig. 6h).



531 **Figure 6.** Spring peak tidal range during present (a) and future (b) climate conditions;
 532 change due to tidal stream energy extraction during present conditions, absolute (c) and per-
 533 centage (d) difference; change due to future climate conditions, absolute (e) and percentage (f)
 534 difference; change due to tidal stream energy extraction and future climate conditions, absolute
 535 (g) and percentage (h) difference

536 Tidal currents may reach a speed of the order of several m/s (Fig. 7a and domi-
537 nate any other flow, especially as they move the entire water column. Tidal currents give
538 rise to strong mixing of water masses, preventing thermohaline stratification in the shal-
539 low southern North Sea [Sündermann and Pohlmann, 2011]. Extracting tidal stream en-
540 ergy from the ocean changes marine current patterns, which can be slowed down by the
541 turbines' action or intensified due to flow diversion processes. Reduction of the mean spring
542 currents (defined as the sum of the M_2 and S_2 semi-major axis amplitudes) is of the or-
543 der of few cm/s in the far-field (Fig. 7c). The pattern is generated by the interaction of
544 different processes acting on different temporal scales: changes in ebb/flood tides, changes
545 in tidal elevation, flow blockage and diversion processes. The dipole velocity changes that
546 are evident in the vicinity of the tidal arrays is due to the reduction of the ebb and flood
547 tidal currents generated by the sink of energy in the tidal arrays. This effect is very ev-
548 ident both upstream and downstream of the Pentland Firth. In terms of percentage changes
549 (Fig. 7d) the decrease in velocity is larger downstream of the Pentland Firth reaching
550 up to 8%. The same dipole ebb/flood effect is also visible in the vicinity of the tidal ar-
551 rays along the west coast of Scotland: the turbines' action generates a reduction of tidal
552 currents of the same order of magnitude as the reduction observed in the Pentland Firth,
553 but affecting a much smaller area (Figs. 7c and 7d). An increase in mean spring currents
554 is observed in the northern Orkney Waters due the blockage of the flow into the Pent-
555 land Firth and consequent diversion (Fig. 7c). Similarly in the Irish Sea, there is an in-
556 crease in mean spring currents in the vicinity of the tidal arrays that could be explained
557 as blockage effect of the tidal arrays up to 0.02 m/s (8%) increase (Figs. 7c and 7d). The
558 increase in tidal elevation previously observed lead to changes in tidal currents too. A
559 small reduction in current is visible along the east coast, better seen as a percentage change
560 (Fig. 7d), generated by the decrease in tidal range (Fig. 6d) and a consequent water depth
561 reduction and a friction increase. Of opposite sign is the change in tidal range at the north-
562 ern and southern entrance of the Irish Sea (Fig. 6d), with a consequent increase of wa-
563 ter depth, and a reduction of friction, that lead to a slight increase in tidal currents (Fig.
564 7d). These changes to tidal currents due to tidal turbines were found to be broadly the
565 same under the future climate hydrodynamic conditions (future baseline is in Fig. 7b,
566 difference are not shown).



567 **Figure 7.** Spring peak tidal currents during present (a) and future (b) climate conditions;
 568 change due to tidal stream energy extraction during present conditions, absolute (c) and per-
 569 centage (d) difference; change due to future climate conditions, absolute (e) and percentage (f)
 570 difference; change due to tidal stream energy extraction and future climate conditions, absolute
 571 (g) and percentage (h) difference

572 There are no studies available about the change to tidal currents in the North Sea
 573 due to SLR. We found that changes in SLR together with consequent changes in tidal
 574 amplitudes act to change the tidal currents as well. The general effect is that slightly
 575 stronger tidal currents occur with SLR: increased water depth, and consequent reduced
 576 friction, lead to an increase in tidal currents. Fig. 7f shows an overall increase of the or-
 577 der of 1% across the whole domain, this is modulated by bathymetry features, showing
 578 scattered larger increases or decreases. Areas where a small decrease in tidal currents
 579 is observed are deeper areas. On top of the SLR, we have the changes in tidal amplitude
 580 due to the SLR itself. This is relevant for Germany, the south-east coast of Denmark and
 581 south-east English coast, that show an increase in mean spring tidal currents (Fig. 7e),
 582 that is where the increase in mean spring tidal range was also observed (Fig. 6e). For
 583 tidal currents, the effect of providing 3.8 GW of instantaneous power is greater than cli-
 584 mate change: the reduction in current speed is stronger (exceeding 8%, see Fig. 7d) than
 585 the changes in tidal currents due to climate change (increase of 1%, Fig. 7f). Indeed, sum-
 586 ming up the effects of tidal energy extraction and climate change, they do not overlap
 587 and interact, thus showing their combined effects as the same of their stand-alone effects
 588 (see Fig. 7g and Fig. 7h).

589 **3.2.2 Stratification**

590 Over longer term seasonal timescales, the ocean response to tidal stream energy
 591 extraction is affected by the different present and future climate of the NW shelf hydro-
 592 dynamics. As tidal stream energy extraction can reduce tidal velocities overall, and as
 593 a consequence can decrease the energy of tidal mixing, the balance between stratifica-
 594 tion and vertical mixing processes in a tidally active and seasonally stratified sea, such
 595 as the NW European continental shelf, can be perturbed. In seasonally stratified seas,
 596 the seasonal and spatial distribution of stratification can be measured through the Po-
 597 tential Energy Anomaly (PEA), defined as the amount of energy required to bring about
 598 complete vertical mixing per unit of volume [*Simpson and Bowers, 1981*]. PEA is the
 599 potential energy (per unit of depth) required to fully mix the water column: where PEA
 600 is equal to zero there is a fully mixed water column and, for convenience, it is defined
 601 to be positive for stable stratification. Shelf waters are well mixed during winter, while
 602 during spring-summer the water column stratification onset is caused by decreased wind
 603 stress and freshwater inputs and increased summer-time heat-flux [*Holt and Umlauf, 2008*].

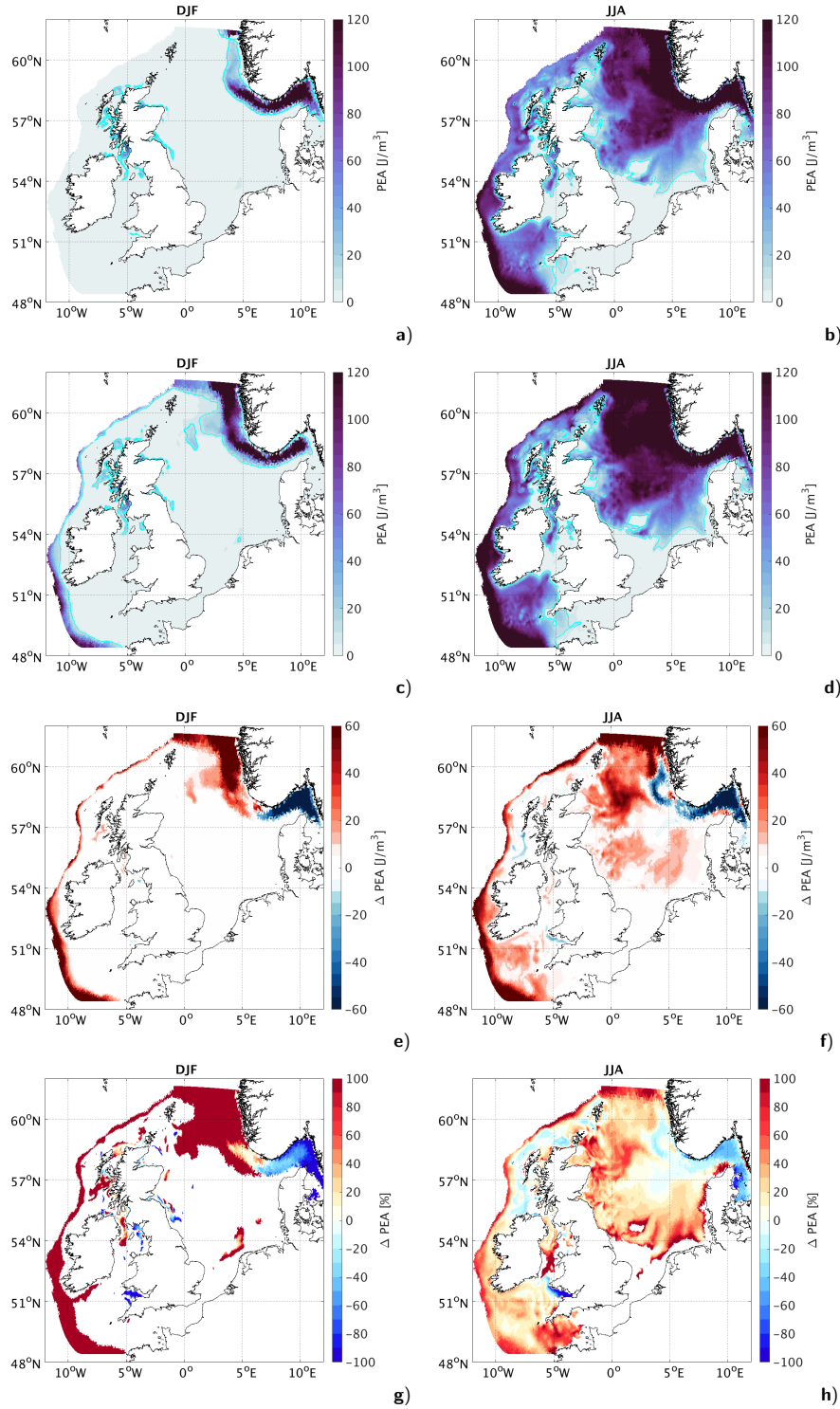
604 The present and future climatological year model runs have been analysed in term of win-
605 ter and summer means separately to account for the strong seasonality, characteristic
606 for the NW European continental shelf. Throughout the article, winter and summer means
607 refer to time averages over the three months of DJF (December, January, February) and
608 JJA (June, July, August), respectively.

609 During present climate winter conditions (Fig. 8a), the water is well-mixed over
610 the entire shelf, apart from a localised area along Norway and the Kattegat, where the
611 fresh water discharge from the Baltic Sea establishes a year round salinity stratification,
612 which is greater than the seasonal summer thermal stratification [*Tinker et al.*, 2016].
613 Winter stratified areas are also present along the west coast of Scotland (Firth of Clyde),
614 due to riverine discharges [*Simpson and Rippeth*, 1993]. In summer the extent of mixed
615 waters decreases, with the 10 J/m^2 contour (Fig. 8b), separating stratified from mixed
616 waters, in agreement with the position of tidal mixing fronts identified by *Pingree and*
617 *Griffiths* [1978] and with the summer distribution of observed thermal fronts found by
618 *Miller and Christodoulou* [2014].

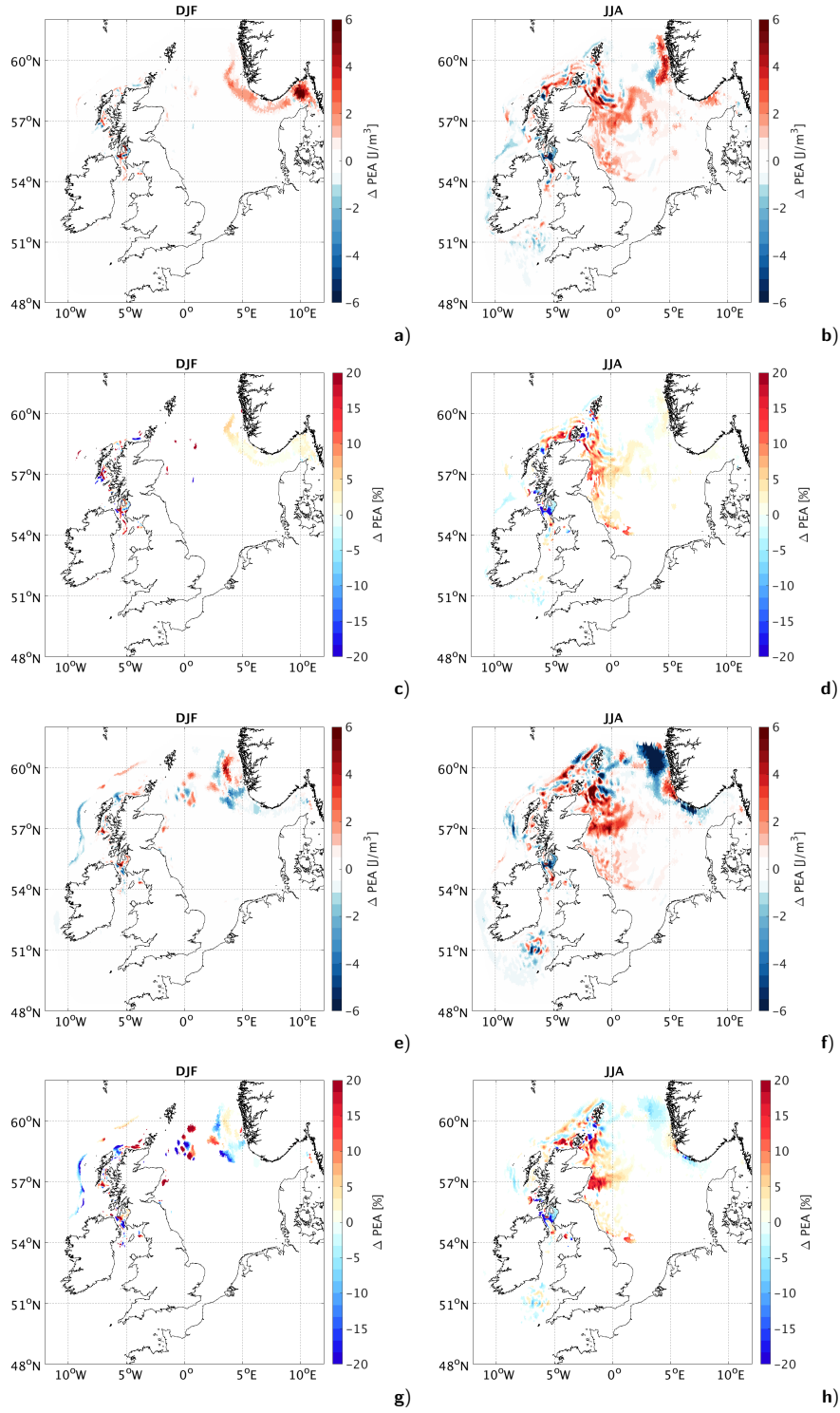
619 The projected future climate in 2050, under the RCP8.5 future scenario, shows an
620 increase in PEA on the NW European continental shelf during both winter (Fig. 8c) and
621 summer (Fig. 8d). During winter the shelf waters are fully mixed with little change due
622 to the future climate projections. However, the shelf-edge and the northern Norwegian
623 Trench show a future increase in winter stratification (Figs. 8e and 8g). Those regions
624 are influenced by the open-ocean dynamics, where stratification is mainly controlled by
625 salinity [*Holt et al.*, 2010; *Tinker et al.*, 2016]. Our model results predict salinity to de-
626 crease in the future both on- and off-shelf, but the freshening of the bottom layer is weaker
627 than at the surface, leading to an increase in water column stability. This is stronger along
628 the northern Norwegian Trench and the shelf-edge (not shown, see supporting informa-
629 tion), which are areas more influenced by the freshening of the north Atlantic. The lat-
630 ter is due to the future atmospheric forcing, marked by an intensifying hydrological cy-
631 cle and changes in the atmospheric moisture transport [*Mikolajewicz et al.*, 2007], that
632 lead to an evaporation reduction over the North Atlantic predicted by the HadGEM2-
633 ES. During summer stratification shows instead an increase $> 20\%$ (Fig. 8h) for most
634 of the shelf. It is larger in the area from the northeast of Scotland towards Norway and
635 where fronts are located in the southern North Sea and Irish Sea, where the increase can
636 exceed 60 J/m^3 (Fig. 8f). These increases are mainly dominated by the future temper-

637 ature rise [Holt *et al.*, 2010; Tinker *et al.*, 2016; Mathis *et al.*, 2017], as in most regions
638 on the shelf, the temperature dominates the seasonal stratification. The SSM future pro-
639 jections of sea surface and bottom temperatures showed an increase during both win-
640 ter and summer, with a larger surface than bottom increase during summer (not shown,
641 see supporting information). Off the shelf, the PEA significantly increases, as already
642 observed for future winter conditions. Changes are, instead, negligible or negative in the
643 area of the Norwegian Trench (Figs. 8f and 8h), as already found by Holt *et al.* [2010]
644 and Tinker *et al.* [2016].

645 The interaction between tidal stream energy extraction and the seasonal hydrody-
646 namic conditions for the present and future ocean state showed region-wide impacts on
647 PEA. For present climate conditions, *extracting energy to provide 3.8 GW* of instantane-
648 ous power does not have any detectable influence on the predominantly well-mixed wa-
649 ters during winter. Indeed changes due to tidal stream arrays operations are observable
650 only along the west coast of Scotland and the Norwegian Trench, areas where salinity
651 is the main driver of the winter stratification (Fig. 9a). The Norwegian Trench PEA in-
652 crease is negligible in terms of percentage change (Fig. 9c). On the other hand, on-shelf
653 summer stratified waters are affected by tidal stream energy extraction. Indeed, the re-
654 duction in vertical mixing due to the turbines' operations increases the strength of wa-
655 ter stratification, mostly along the UK east coast and in the area from the northeast of
656 Scotland towards Norway (Fig. 9b). Those changes can reach an increase of 6 J/m^3 , in
657 some limited areas (Fig. 9b), corresponding to a maximum PEA increase of 20% (Fig.
658 9d). However, the overall extent of the stratified region does not greatly change, as shown
659 in De Dominicis *et al.* [2017]. Thus, the enhanced biological and pelagic biodiversity hotspots,
660 such as tidal mixing front locations, are not shifted. These are areas of enhanced con-
661 centration of nutrients and plankton, due to cross-frontal exchange processes, and sep-
662 arate the seasonally stratified water from the permanently well-mixed waters. On the
663 west coast, a small detected decrease in PEA (Fig. 9b) can be linked to the increase in
664 mean spring currents previously observed (Fig. 7c).



665 **Figure 8.** Potential Energy Anomaly (PEA) during present climate winter - DJF (Dec-Jan-
 666 Feb) (a) and summer - JJA (Jun-Jul-Aug) (b) and during future climate winter (c) and summer
 667 (e), white line is the 10 J/m^2 contour line separating the stratified from mixed waters. Difference
 668 between the present and future climate baseline during winter (e - absolute difference, g - per-
 669 centage change) and during summer (f - absolute difference, h - percentage change), masked out
 670 for clarity percentage differences associated to absolute differences less than 1 J/m^2 .



671 **Figure 9.** Change in PEA due to tidal stream energy extraction during: present winter cli-
 672 mate (**a** - absolute difference, **c** - percentage change); present summer climate (**b** - absolute
 673 difference, **d** - percentage change), future winter climate (**e** - absolute difference, **g** - percentage
 674 change) and future summer climate (**f** - absolute difference, **h** - percentage change), masked out
 675 for clarity percentage differences associated to absolute differences less than 1 J/m^2 .

676 Tidal stream energy extraction effects on PEA are slightly amplified by future cli-
677 matic conditions. As stated before, tidal stream energy extraction noticeably affects strat-
678 ified waters and since climate change stratifies waters that were mixed during present
679 winter climate conditions, those can be then affected by turbines' action. Indeed, as shown
680 in Figs. 9e and 9g, in the future there is a detectable increase in winter PEA, generated
681 by tidal stream energy extraction. Future summer increase in on-shelf stratification leads
682 to an exacerbation of the impacts of the large turbine arrays in some limited areas (Fig.
683 9f), where changes go in the same direction of those due to climate change. Those changes
684 do not exceed 6 J/m^3 (Fig. 9f) or a 20% PEA increase (Fig. 9h), as was also found for
685 present climate conditions. The summer water column stratification generated by tidal
686 stream energy extraction during present or future climatic conditions is thus one order
687 of magnitude lower than climate change effect, and over a much smaller area, driven by
688 the temperature increase of future hydrodynamic conditions in 2050. The combined ef-
689 fects of climate change and tidal energy extraction on PEA show the same pattern (not
690 shown) as those driven by climate change only. Indeed, being ten times larger those ef-
691 fects overcome the PEA modifications due to tidal stream energy extraction.

692 *3.2.3 Circulation*

693 The wind-driven circulation is the dominant permanent residual current regime that
694 characterises the mean current system of the North Sea. While tidal currents might be
695 stronger, they are almost periodic with small net transport [*Sündermann and Pohlmann,*
696 2011]. The thermohaline circulation is superimposed on the wind-driven one and is de-
697 termined mainly by the strong seasonal variation in sea-surface temperature, by the in-
698 flow of water from the Atlantic Ocean and by the freshwater supply from the continent
699 and the Baltic Sea. The present-day climatological-mean circulation reproduced by the
700 SSM (Figs. 10a and 10b) captures well the main features of the general circulation of
701 the NW European continental shelf, a detailed description of those can be found in e.g.
702 *Turrell et al.* [1992], *OSPAR Commission* [2000], *Holt and Proctor* [2008], *Sündermann*
703 *and Pohlmann* [2011], *Mathis et al.* [2015] and *Quante et al.* [2016]. The North Sea mean
704 current system, as shown in Figs. 10a and 10b, forms a cyclonic circulation pattern, which
705 is mainly driven by the prevailing southwesterly winds over the NW European continen-
706 tal shelf [*Sündermann and Pohlmann, 2011*]. The wind-induced circulation is particu-
707 larly strong in winter when wind speeds are higher, as shown in Fig. 10a compared to

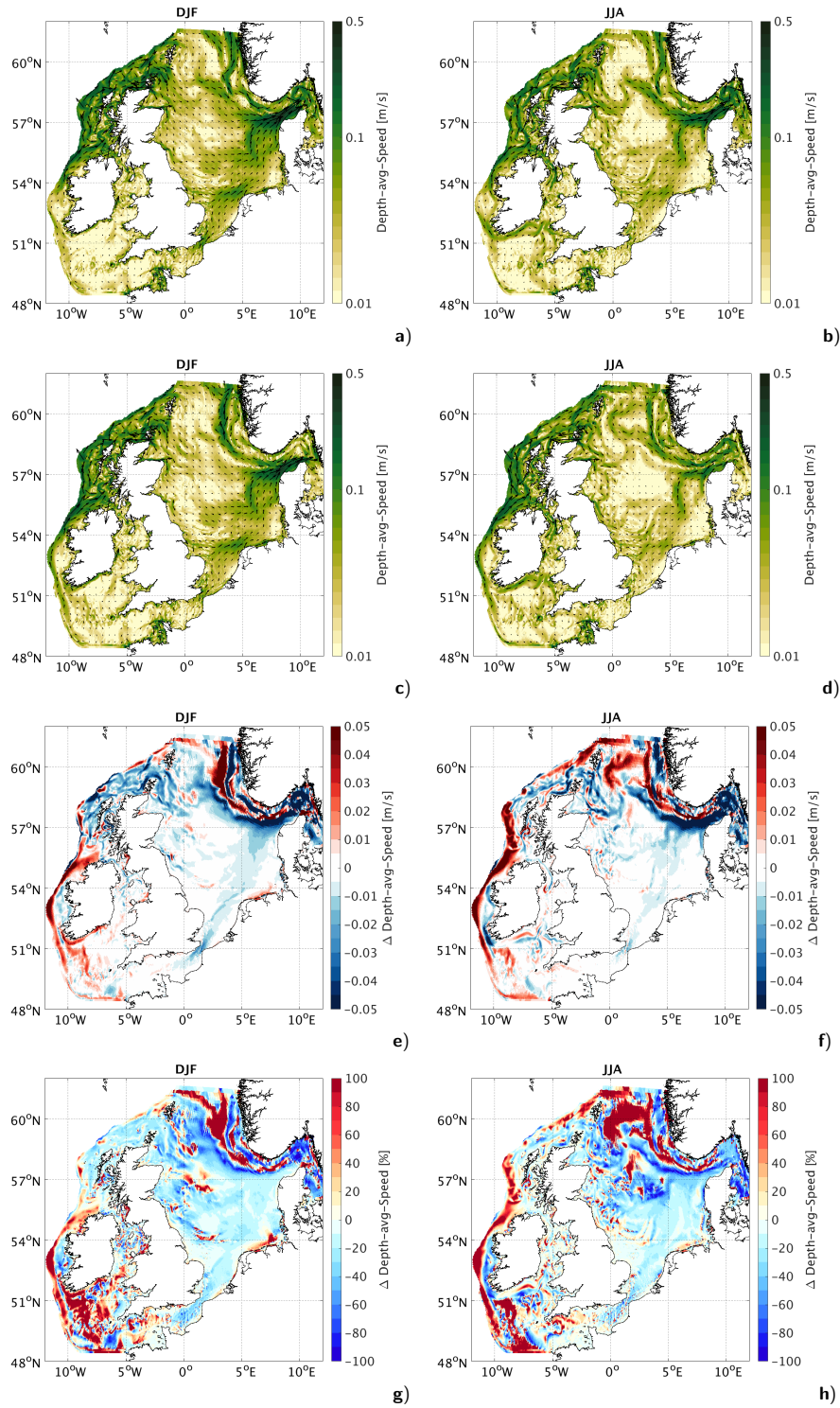
708 Fig. 10b. On the western side of the model domain, the density-driven currents provide
709 a continuous route from the French coastal region via the Celtic shelf and west of Ire-
710 land to the Scottish Shelf [*Hill et al.*, 2008; *Holt and Proctor*, 2008] and are stronger dur-
711 ing summer (Fig. 10b). To ease the analysis of the results, the modelled three-dimensional
712 current fields have been condensed to two-dimensional horizontal fields by depth-averaging,
713 thus including the signals of deeper layers. Depth-averaged rather than depth-integrated
714 values help to highlight the shelf areas.

715 The comparison between present (Figs. 10a and 10b) and future (Figs. 10c and 10d)
716 general circulation shows a weaker future cyclonic circulation in the North Sea, both in
717 summer (Figs. 10f and 10h) and winter (Figs. 10e and 10g). This can be caused by changes
718 in the wind patterns and less water exchange with the Atlantic. This change would have
719 negative consequences for the North Sea's ecosystem, which has become adapted to a
720 major cyclonic drift of water masses [*Sündermann and Pohlmann*, 2011]. A reduction
721 of the inflow of Atlantic water through the Fair-Isle Passage (between Orkney and Shet-
722 land Islands) and the Dover Strait is also visible, more pronounced during winter. A weaker
723 Dooley Current, the northernmost recirculation cell, is caused by the reduced Fair-Isle
724 inflow. Similar findings are described by *Mathis and Pohlmann* [2014] and *Tinker et al.*
725 [2016]. The Scottish coastal water, the Central and South North Sea water and the Con-
726 tinental coastal water currents are also slightly reduced, in particular during winter (Figs.
727 10e and 10g). A reduction of the Skagerrak recirculation is also observed.

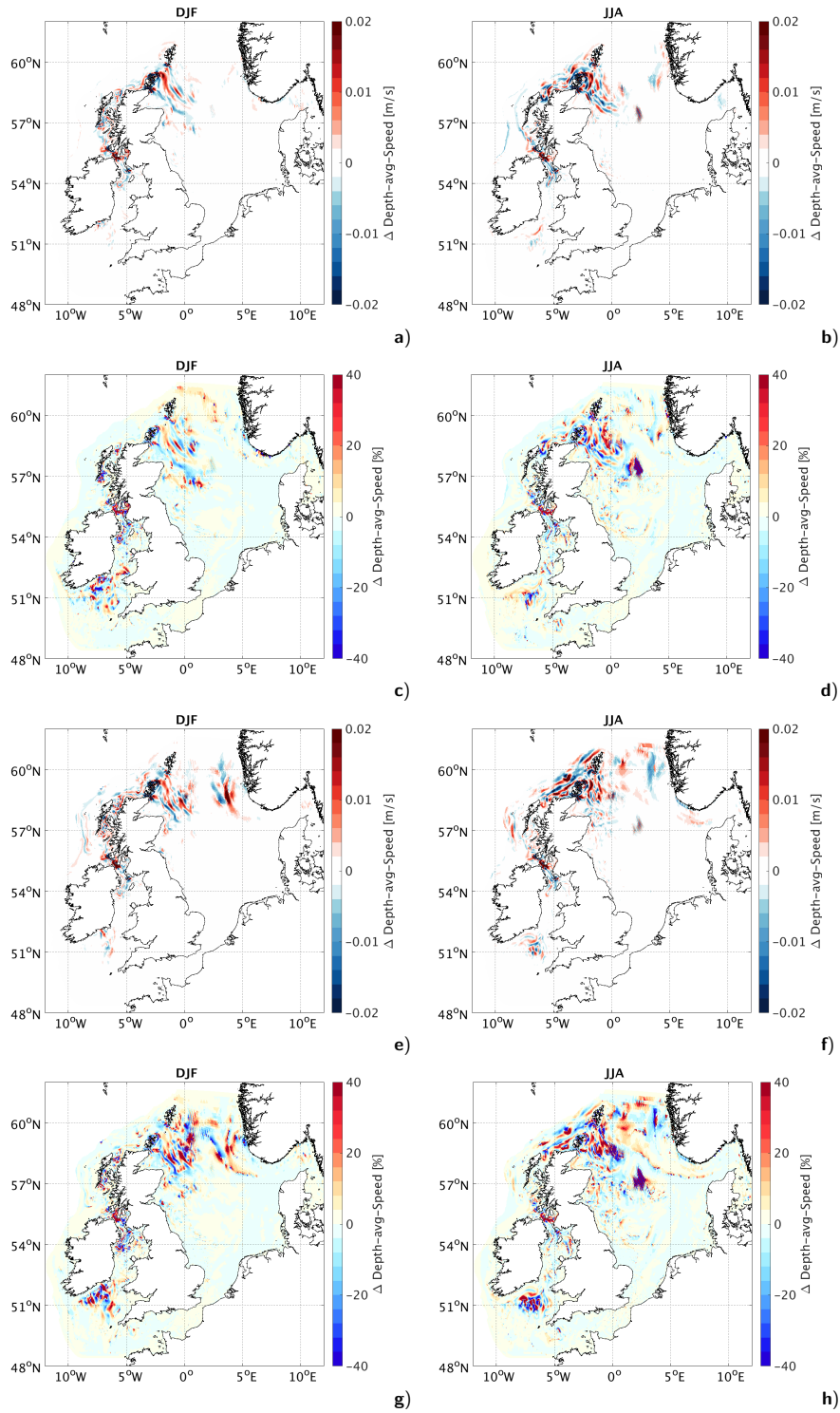
728 A strengthening of the European slope current is visible on the western side, par-
729 ticularly during summer (Figs. 10f and 10h), while during winter, an enhancement of
730 the Irish coastal current is detected (Figs. 10e and 10g). A slight increase of the north-
731 ern inflow is also indicated through the increasing current speed north-east of the Shet-
732 land Islands. However, during both seasons, a reduction of the inflow of Atlantic water
733 along the Norwegian trench is observed (Figs. 10e, 10f, 10g and 10h), as found also by
734 *Mathis and Pohlmann* [2014]. The large increase in current speed shown at the north-
735 east corner of Figs. 10e, 10f, 10g and 10h is due to a shift in position, and detaching from
736 the coast, of the Norwegian Coastal Current, that brings freshwater into the North Sea
737 and is the only net outflow of the North Sea water into the Atlantic. Additionally, the
738 SSM shows an increase in a northward flow east of Shetland Islands (at $\sim 2^\circ\text{E}$ in sum-
739 mer, Fig. 10b) and the appearance of a southward inflow close to the Norwegian coast
740 (winter and summer, Figs. 10c and 10d, respectively). Similar patterns have been shown

741 by *Mathis and Pohlmann* [2014] and *Tinker et al.* [2016], who observed that the weak-
742 ening of the Dooley current might lead to a substantial proportion of the northern in-
743 flow to reverse shortly after entering the northern North Sea, leading to an increase in
744 the Norwegian Coastal Current or to a north-westward flow parallel to the Norwegian
745 Coastal Current.

746 As shown in Figs. 11a and 11b, with present climate conditions, the effects of tidal
747 energy extraction on residual currents are observed mainly in the vicinity of the tidal
748 turbine arrays, in the Pentland Firth, between Orkney and Shetland, and in the Irish
749 Sea. Changes further propagate during winter in the Fair-Isle inflow region and up to
750 the Dooley Current region during summer. Changes can lead to a decrease/increase up
751 to 0.02 m/s, which are more intense and over a wider area during summer than in win-
752 ter (Figs. 11a and 11b). Those changes account for 40% of the residual water velocity
753 in the affected region (Figs. 11c and 11d). However, it must be noticed that changes in
754 the area are both positive/negative, they can thus be explained by currents being shifted,
755 rather than an enhancement/reduction of the Fair-Isle inflow. The climate change sce-
756 nario previously analysed was showing a coherent reduction of currents speed in the Fair-
757 Isle inflow, that could reach 0.05 m/s (Figs. 10e and 10f). In the Irish Sea, a decrease/increase
758 in residual currents is also observed, although confined to the vicinity of the tidal tur-
759 bine arrays.



760 **Figure 10.** Depth-averaged currents during present climate winter - DJF (Dec-Jan-Feb) (a)
 761 and summer - JJA (Jun-Jul-Aug) (b) and during future climate winter (c) and summer (d). Dif-
 762 ference between the present and future climate baseline during winter (e - absolute difference, g -
 763 percentage change) and during summer (f - absolute difference, h - percentage change).



764 **Figure 11.** Change in depth-averaged currents due to tidal stream energy extraction during:
 765 present winter climate (a - absolute difference, c - percentage change); present summer climate
 766 (b - absolute difference, d - percentage change), future winter climate (e - absolute difference, g -
 767 percentage change) and future summer climate (f - absolute difference, h - percentage change).

768 Future climate conditions show a pattern similar to the one observed for present
769 climate. Currents look to be shifted, given the alternation of decrease/increase of cur-
770 rent speed. Changes are of the same magnitude of the ones observed during present con-
771 ditions. However, an exacerbation of changes given future climate conditions is observed
772 only in the extent of the perturbed areas, being wider, in particular during summer, ex-
773 tending up to the Norwegian Trench and on western side up to the shelf break (Figs. 11e
774 and 11f). Although percentage changes can exceed 40% (Figs. 11g and 11h), showing
775 pattern of propagation of the changes up to the southern entrance of the Irish Sea, ab-
776 solute changes do not exceed 0.02 m/s. The impacts of extracting energy to provide 3.8
777 GW of instantaneous power appear to be smaller, over a restricted area and less con-
778 sistent that the impacts on residual currents generated by the future climate projection
779 considered in this work. Indeed, the effects of climate change on the residual circulation
780 largely overcome the modifications due to tidal stream energy extraction. The combined
781 effects of climate change and tidal energy extraction show the same pattern (not shown)
782 as those driven by climate change only.

783 4 Discussion

784 Renewable energy is a strategy to lower CO₂ emissions and to mitigate climate change
785 [*Edenhofer et al.*, 2011]. The global use of fossil fuels has increased, since the Industrial
786 Revolution, to meet the energy requirements of basic human needs and productive pro-
787 cesses. However, we have learned, while already experiencing their effect, that fossil fu-
788 els contribute significantly to the CO₂ emissions, among other environmental problems.
789 Energy conservation and efficiency, renewable energy, nuclear energy and carbon cap-
790 ture and storage are available strategies for satisfying the energy needs, while lowering
791 GHG emissions. However, an open question is whether all of these energy options are
792 free of any side effects. It is better to learn this before making our energy system reliant
793 on them. The aim of this work was therefore to analyse the potential impacts of tidal
794 energy extraction on the marine environment, as they should be considered when plan-
795 ning future tidal energy exploitation. We wanted to put them in the broader context of
796 the possibly greater and global ecological threat of climate change. Extracting energy
797 is not without its own consequences, but negative effects of climate change can be worse,
798 as demonstrated in this work. Moreover, while marine renewable energy alleviates the
799 climate change impacts, by reducing emissions, with a positive effect on a global scale,

800 its side effects will be mostly on a local scale. A key result of this study is that those lo-
801 cal effects are not only negative ones. For example, we found that tidal stream energy
802 extraction could ameliorate the undesirable effects of rising mean sea level in some lo-
803 cations. This is relevant from the perspective of the development of marine renewable
804 energy industry, that can be seen, in some occasions, as a mitigation measure for climate
805 change, not only on a global scale, but also on a local one (e.g. coastal defence).

806 3.8 GW is a realistic estimate of the average instantaneous power that can be pro-
807 vided from Scottish Waters. However, such large-scale tidal stream energy extraction is
808 unlikely to occur in the near future, since very large numbers of devices are required. It
809 must be noted that some power will be lost during the electricity generation process and,
810 whilst the generic tidal turbine parameters used are acceptable to stakeholders [*Baston*
811 *et al.*, 2015], more or less energy could be potentially generated by using other types of
812 devices and/or different array layouts. With the strongest currents in Scottish Waters,
813 the Pentland Firth gives almost half of the total power (1.67 GW) and it requires fewer
814 turbines at the same power output, but with a larger rated capacity (2 MW). The other
815 areas would not need such large devices. Turbine design is important, for example, tur-
816 bines not working below 1 m/s would not be optimal in some Shetland Islands locations.
817 As we found in this work, they would not produce any power during neap tides and a
818 lower cut-in speed should be developed in future generations of tidal energy devices [*Neill*
819 *et al.*, 2014]. The turbines used in this study approximate to the current best technol-
820 ogy, however, in the future the development of devices that are able to exploit deeper
821 locations or floating turbine platforms [*Zhou et al.*, 2017] may yield a different resource
822 estimate. Turbines suitable for exploiting lower energy sites can also lead to an increase
823 of the resource available [*Lewis et al.*, 2015; *Neill et al.*, 2017]. Furthermore, less ener-
824 getic tidal sites should be considered for future developments, as they offer less challeng-
825 ing environments in which to operate and more tidal energy phase diversity among the
826 different sites [*Lewis et al.*, 2015; *Neill et al.*, 2017]. The latter is an important factor
827 to consider when planning tidal array locations. Given the inherent intermittency of tidal
828 power (undesirable from a grid integration perspective), it would be advisable to com-
829 pensate this with tidal arrays that are lagged in phase. The arrays considered in this work
830 have shown instead a phase lag never exceeding 1 hour, while the optimal one would be
831 a quarter of the tidal cycle or about 3 hours [*Neill et al.*, 2016].

832 The action of very large scale tidal arrays on a seasonally stratified shelf sea was
833 evaluated by comparing a set of ocean physical parameters describing the hydrodynamic
834 conditions representative of present and projected future climate in 2050, provided by
835 the SSM model simulations. This work considered only the RCP8.5 scenario, the “worst
836 case” with very high GHG emissions, which gives a plausible pathway, upon which the
837 HadGEM2-ES climate model projection (the forcing of our future climate run) is based.
838 Although all models are built on the same physical principles, some choices and approx-
839 imations are needed, which include unrefined representation of known processes and in-
840 clusion or not of some processes in the models. These choices produce differences in cli-
841 mate projections from different models. There is then a range in plausible projections
842 for future climate that arise from the future emissions uncertainty and from the model
843 uncertainty. Although HadGEM2-ES is one of the top-performing climate models of the
844 North Atlantic, we presented only a single realisation of future conditions and, also, only
845 one possible tidal stream array layout, thus, our results should be seen as physically plau-
846 sible projections, rather than a prediction. Exact numbers are not the object of this work,
847 since we were looking for relative changes induced by two anthropogenic factors that could
848 shape the future NW European shelf dynamics. Besides model structural uncertainties,
849 both of the forcing of the model and of the shelf seas model, it is reassuring that our find-
850 ings are broadly in agreement with previous climate change impact studies, that include
851 SLR prediction and extreme water levels changes [*Pickering et al.*, 2012; *Ward et al.*, 2012;
852 *Pelling et al.*, 2013; *Idier et al.*, 2017], a warming and freshening of the North Sea and
853 consequent stratification increase and general circulation changes [*Ådlandsvik*, 2008; *Holt*
854 *et al.*, 2010; *Mathis and Pohlmann*, 2014; *Schrum et al.*, 2016; *Tinker et al.*, 2016; *Mathis*
855 *et al.*, 2017]. However, the amplitude and exact spatial pattern of the projected changes
856 still remain uncertain due to the difference in reference periods and emissions scenarios
857 from the existing literature.

858 The inter-annual variability (natural and of the induced anthropogenic changes)
859 cannot be assessed in this study. The “delta-change” method has the main advantage
860 that it only requires one additional simulation for estimating the climate change impact,
861 that can be estimated as the difference between the present day SSM run forced with
862 the reference reanalysis data and the model run with the perturbed future forcings. One
863 of the general disadvantages of the “delta-change” approach is the loss of information
864 about inter-annual variability. However, in our specific case, the SSM model for the present

865 day climate was forced with climatological averages and the inter-annual variability was
866 already neglected. This choice came from computational resource limitations, which make
867 a multi-year FVCOM simulation impractical. Essentially we asked: how would average
868 conditions in 2038-2062 differ from those in 1990-2014, assuming the inter-annual vari-
869 ability remains the same?

870 The SSM model has been proven to be a very useful tool, since it allows us to study
871 the effects over the entire NW European Shelf with a minimum spatial resolution (500
872 m - 1 km) that permits the resolution of the tidal-stream energy sites [Lewis *et al.*, 2015].
873 However, higher resolution might allow further improvements in the representation of
874 tidal stream turbines in the model, leading to both more accurate estimate of power and
875 environmental effects, those include: (i) small scale (< 1 km) interactions between tur-
876 bine wakes to be reproduced; (ii) optimisation techniques to be applied for the position-
877 ing and individual tuning of turbines, that could potentially increase the extracted en-
878 ergy [Funke *et al.*, 2014]; (iii) changes in turbulence due to turbines' action for a correct
879 reproduction of mixing behind turbines [Li *et al.*, 2017]. Additionally, a momentum sink
880 term due to the drag of the physical structures of turbine blades, supporting poles and
881 foundations [Yang *et al.*, 2013] can also be considered.

882 It has been shown that both climate change and the very large tidal stream arrays
883 can introduce detectable changes to the tidal elevation, marine (tidal and residual) cur-
884 rents and ocean stratification patterns. How do those changes in the physical ocean con-
885 ditions translate into impacts on ecosystem habitats and animals' behaviour? This is be-
886 ing answered by further studies looking at the possible consequences on the marine ecosys-
887 tem of the effects of climate change with those of tidal stream energy extraction. The
888 NW European continental shelf is a biologically rich region, inhabited by diverse species
889 of all trophic levels. A complex network of interactions between biota and the physical
890 environment characterises the marine shelf ecosystem, where patterns in habitat use can
891 coincide with particular oceanographic conditions: temperature, currents, frontal activ-
892 ity, the strength of the tidal currents which also affect primary productivity [Cox *et al.*,
893 2016; Sadykova *et al.*, 2017]. On going studies are evaluating whether the predicted phys-
894 ical changes due to tidal stream energy extraction and climate change will affect the avail-
895 ability and location of critical habitats for marine species, and as a consequence changes
896 in animal behaviours. This can be done by means of statistical models that uses as in-
897 put the results of the present work and explore the distributions of mobile predator and

988 prey species, such as pelagic fish and seabird and marine mammal species, to calculate
989 the degree of overlap in these species now and in future predictions.

900 On going studies are also assessing if the reduction in tidal currents presented in
901 this work and the consequent reduction in bed shear stress could lead to significant changes
902 in water turbidity, as already suggested by *Heath et al.* [2016]. On the other hand, the
903 localised areas where an increase in currents has been detected need further investiga-
904 tion, in particular where sediments could be mobilised, as done on a smaller scale by *Fair-*
905 *ley et al.* [2015] and *Martin-Short et al.* [2015]. Moreover, impacts on benthic commu-
906 nities is also an ongoing topic of research. However, the effect of tidal energy extraction
907 on benthos might be negligible, since their composition is stable over an approximate
908 1 m/s range of velocities in high velocity flow environments [*Kregting et al.*, 2016], which
909 is above the range of changes we found, an overall habitat loss might instead be predicted
910 to occur in response to climate change.

911 Modifications in the extent of the stratified areas mean shifting the position of tidal
912 mixing fronts, thus of enhanced biological and pelagic biodiversity hotspots, as well as
913 changes in PEA that can trigger phytoplankton blooms. If a decrease in water turbid-
914 ity is detected, it can in turn increase sunlight penetration and consequently lead to higher
915 primary productivity, possibly affecting the ecosystem habitats. Since stratification and
916 turbidity changes can have consequences on the ecosystem biogeochemistry, future work
917 should involve the use of a biogeochemical model to properly evaluate the impacts of changes
918 of physical factors on marine primary productivity and nutrients distribution. This would
919 be beneficial to better link the physical changes with ecological impacts. In addition, changes
920 in residual circulation are usually an overlooked stressor acting on marine ecosystems,
921 but consequences are beginning to emerge [*van Gennip et al.*, 2017]. Future studies are
922 needed to properly assess if the detected changes in residual currents, both due to cli-
923 mate change and tidal energy extraction, can lead to changes in transport pathways of
924 passive tracers, affecting larval transport and dispersal, and possibly population connec-
925 tivity.

926 5 Conclusions

927 This study provides a plausible projection of how the hydrodynamic conditions on
928 the NW European continental shelf might respond to climate change and to tidal stream

929 energy extraction. It responds to a substantial increase in the demand for evidence-based
930 policy advice for marine climate change and offshore renewable energy. We numerically
931 simulated changes in the physical marine environment of a shelf sea, induced by both
932 the “business as usual” future climate scenario (RCP8.5) and by hypothetical very large
933 tidal stream arrays in Scottish Waters (UK), able to provide 3.8 GW for electricity gen-
934 eration. This is about 10% of the UK present average instantaneous electricity consump-
935 tion [*Department for Business, Energy & Industrial Strategy, 2016*]. Tides have been con-
936 firmed to be the most important contribution to energy available from the currents. Cli-
937 mate change will not alter the energy resource estimate, which will show minimal increases
938 in some locations due to increases in tidal currents driven by SLR. Such large-scale tidal
939 stream energy extraction is realistic, but unlikely to occur in the near future. It is an
940 extreme best (worst in terms of impacts) case scenario to explore the environmental ef-
941 fects.

942 The potential effect of climate change on the ocean system have been evaluated and
943 compared with the present and the future state of the seas modified by large scale en-
944 ergy extraction. It has been shown that the very large scale tidal stream energy extrac-
945 tion can introduce detectable changes to the tidal range, that mainly increases upstream
946 of the tidal farm locations (considering the direction of propagation of the tidal wave),
947 while a decrease in the mean spring tidal range is observed downstream, along the UK
948 east coast and also in the Irish Sea. Those effects are found not to be exacerbated by
949 future climate conditions. Although changes are small, of the order of a few cm, the tidal
950 range reduction in some cases may act to counter the predicted rise in sea level due to
951 climate change by reducing extreme water levels.

952 Currents (both tidal and residual) are slowed down due to the sink of energy in the
953 tidal arrays or speeded up due to flow diversion and blocking. While the “business as
954 usual” future climate scenario can induce larger impacts in the residual current circu-
955 lation than the tidal stream arrays, tidal velocities show greater changes due to tidal en-
956 ergy extraction. The strongest signal in tidal velocities is an overall reduction, that can
957 have consequences on a seasonal temporal scale. Indeed, the strength of summer strat-
958 ification on the NW European continental shelf is found to slightly increase, due to the
959 tidal velocities decrease and, as a consequence, tidal mixing. A key finding is that cli-
960 mate change effects and tidal energy extraction both act in the same way in terms of in-
961 creasing stratification due to warming and reduced mixing. However, the future increase

962 in summer water column stratification driven by the temperature increase is ten times
963 larger and over a much wider area than the one generated by tidal stream energy extrac-
964 tion during present or future climate conditions.

965 The results presented in this work are the basis for other ongoing studies that eval-
966 uate the impacts of the above mentioned physical changes on animal behaviours, in par-
967 ticular the distributions of mobile predator and prey species, on sediment dynamics with
968 special attention to water turbidity, and on benthic communities.

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