



# PN code acquisition using smart antennas and adaptive thresholding for spread spectrum communications

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**Abstract** In this paper, we consider a pseudo-noise (PN) code acquisition for direct sequence spread spectrum communication in a Rayleigh fading multipath channel environment using smart antenna and adaptive thresholding automatic trimmed-mean constant false alarm rate (ATM-CFAR) processing. A smart antenna is an array of antenna elements that can modify the array pattern adaptively to minimize the effect of multiple access interference (MAI) from other users and multipath. PN code acquisition using a fixed threshold may lead to an excessive number of false alarms, and thus, adaptive thresholding ATM-CFAR processing is considered. In addition, since the interference (MAI and multipath) can be considered as outliers, an outlier determiner is embedded to the proposed system based on the interquartile range. This novel approach of combining smart antennas and adaptive thresholding ATM-CFAR detection with an outlier determiner proved to be very robust since it resulted in a serious enhancement of the probability of detection.

**Keywords** Automatic TM-CFAR · Interquartile range · LMS smart antenna · Outliers · PN code acquisition

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## 1 Introduction

Pseudo-noise (PN) code synchronization is an important stage in direct sequence spread spectrum (DS-SS) communication. There are two phases of code synchronization: code acquisition and code tracking. Code acquisition is the coarse alignment between the incoming PN code signal and the local despreading code at the receiver. When the codes are aligned then this process yields a correlation value. Obtaining a high correlation value leads to a better detection for acquisition. The receiver multiplies both codes and the result is integrated over some observation interval. The multiplication and integration are performed one by one for each code phase to be examined. The code tracking is a finer alignment for synchronization between the transmitter and the receiver.

In code division multiple access (CDMA) communication systems, the presence of multiple access interference (MAI) is a major challenge that significantly affects the performance. Smart antenna applications are deployed more and more in mobile communication systems because of their benefits in providing more promising results such as combating MAI and reducing multipath fading [1]. Smart antennas can solve the limited bandwidth problems, follow many beams to track several mobiles, and improve the received signal power gain and thus increase the detection probability. Therefore, a combination of smart antenna and PN code acquisition technique is considered in mobile communication. There are many well-known adaptive algorithms to adjust the required weighting in a smart antenna such as least mean square (LMS), sample matrix inversion (SMI), and recursive least square (RLS) [2]. Smart antennas for PN code acquisition have also been considered. In [3], Bing and Kwon proposed a system utilizing the LMS algorithm with smart antennas and a

fixed threshold for wireless communication while in [4] they consider smart antennas for PN code acquisition in direct sequence (DS) CDMA.

As mentioned previously, in order to decide to whether tracking or phase updating, the system uses a threshold value. If the threshold value is too high the probability of miss is increased, on the other hand, if the threshold is too low this may lead to a serious increase in the false alarm probability. Therefore, due to variations in the received signal power caused by the environmental influence and mobility, adaptive thresholding techniques based on maintaining the constant false alarm rate (CFAR), where the threshold value is set in accordance with the magnitude of background noise level, are preferred. Adaptive thresholding CFAR detection is well developed in automatic radar signal detection applications [5] and have also been applied in some CDMA communication applications.

In communication systems, the received signal contains noise and interfering signals that may be considered as outliers. The system must be able detect and trim the outliers to avoid unnecessary false alarms. In this paper, we identify the outlier by using the boxplot technique. The boxplot can give some information about the data set such as dispersion and identify outliers. The technique defines a resistant rule which is multiplication of a multiplier value  $\rho$  and dispersion for constructing fences. The data values exceeding the fences are defined as outliers.

In this paper, we consider PN code acquisition using smart antennas and adaptive thresholding ATM-CFAR processing with an outlier determiner for spread spectrum communication systems. The proposed PN code acquisition system uses smart antennas which would yield an increase in the signal to noise ratio (SNR) level and a serious interference reduction. We explore appropriate multiplier values of resistant rules to define demarcation points of outliers in the system. This novel combination of smart antenna and adaptive thresholding ATM-CFAR processing with an outlier determiner proved to be robust since it resulted in a significant enhancement of the detection probability as will be shown in the next sections.

The structure of this paper is as follows. In Sect. 2, we exhibit the related works on this area that have been conducted. In Sect. 3, we describe the proposed communication system model under consideration and present the problem formulation. We also obtain the conditional probability density functions under both hypotheses  $H_1$  and  $H_0$ . In addition, we apply the first and the third quartiles to obtain a multiplier value  $\rho$  in order to identify the fences as demarcation points for the outliers. In Sect. 4, we compare the performance of the proposed system using adaptive cell averaging (CA)-CFAR processing to the system given in [3] which, recall, does not consider multipath. However, in the problem under consideration in this paper we do

consider the presence of multipath and MAI, and also suggest the use of ATM-CFAR processing, which is based on rank order statistics in order to censor the cells containing interfering signals. Part of this paper was presented in [6], which considered the trimmed mean CFAR processing only instead of automatic censoring scheme using the outlier determiner. We investigate performance of the proposed system while reducing the effect of MAI and multipath. We also explore the multiplier value  $\rho$  to determine the fences for censoring the outlier cells in the reference cells. Furthermore, we derive an exact expression for the probability of detection and show the robustness of the system performance in terms of the theoretical probability of detection. The conclusion is given in Sect. 5.

## 2 Related work

In PN code acquisition techniques, several schemes have been proposed in the literatures, such as serial search acquisition [7, 8], parallel acquisition [9, 10], and hybrid acquisition [11, 12]. Antenna diversity has been proposed to further improve PN code acquisition such as decreasing the acquisition time and providing robustness in fading environments [13, 14]. The presence of MAI substantially affects the performance of CDMA communication systems. Various schemes have been proposed in the literature to suppress MAI [15–18]. In [15], multiuser interference cancellation in CDMA communication systems with diversity gain was introduced. Dodd et al. [16] proposed an iterative joint detection for MAI using DS-CDMA. In [17], a parallel interference cancellation using a combination of different linear equalization and a rake receiver was proposed for downlink CDMA systems. In Zhang et al. [18] proposed a multiuser detection system using smart antennas in a CDMA system to combat MAI in a multipath fading channel. Employing smart antenna to combat MAI in wireless communication systems was also considered in [19]. Smart antenna applications are continuously deployed in mobile communication systems because of their benefits. Recently, an implementation of the LMS and RLS algorithms with smart antennas to optimize the performance of advanced communication system was presented in [20].

Adaptive thresholding CFAR detection is well developed in automatic radar signal detection applications [5]. From the rich literature on CFAR detection, we cite some references from radar applications based on CA-CFAR in [21, 22] and robust order statistics (OS) CFAR processing in [23–25]. Adaptive thresholding techniques have also been applied in some CDMA communication applications. Several PN code acquisition schemes using adaptive thresholding CFAR processing have been addressed in [26–29] which show the enhancement of the detection

probability. Just very recently, Berbra et al. [30] proposed an adaptive array acquisition system, which integrates an adaptive thresholding technique based on ordered data variability index constant false alarm rate (ODV-CFAR) and LMS algorithm for CDMA communication.

We cite literatures in detecting the outliers. In [31], forward methods were proposed in CA-CFAR processing for locating the outlier. Tuckey [32] developed the boxplot technique to determine possible outliers. Moreover, several techniques exploring data based on the boxplot resistant rules are given in [33–35].

### 3 System description and problem formulation

The communication system model considered assumes  $D$  users from simultaneous transmitters while the first user is considered as the initial synchronization whose performance is to be investigated. Figure 1 shows the block diagram of the proposed communication system model. The transmitted signal of the  $i$ -th user is given by

$$s_i(t) = \sqrt{2P_{T_i}} b_i(t) c_i(t) \cos(\omega_c t + \xi_i) \tag{1}$$

where  $P_{T_i}$  is the transmitted power of the  $i$ -th signal,  $b_i$  is the data waveform,  $c_i$  is the spreading sequence,  $\omega_c$  is the angular carrier frequency, and  $\xi_i$  is the phase of the  $i$ -th modulator from the transmitter. At the beginning of each transmission, the transmitter sends a phase coded carrier without data modulation to help the initial synchronization [7, 8]. Hence, we assume for simplicity that there is no data modulation on the initial synchronization signals.

The user signals are transmitted through a communication channel assumed to be a Rayleigh fading multipath channel. The transmitted signals are received by an antenna array of  $M$  elements and go through an LMS processor. The output from the LMS processor undergoes ATM-CFAR processing in order to make a final decision about acquisition or not.

### 3.1 The received signal model

The communication channel model considered consists of  $L$  tapped delay lines with a tap spacing of one chip [36] that correspond to the number of resolvable multipath with amplitudes  $\alpha_{il}$  and phases  $\zeta_{il}$ ,  $i = 1, \dots, D$ ,  $l = 0, \dots, L - 1$ , where  $\alpha_{il}$  is Rayleigh random variable and  $\zeta_{il}$  is uniform random variable over  $[0, 2\pi]$ . We assume that the fading amplitude is constant during an observation interval but changes from one to another. Moreover, we normalize the total fading power in all resolvable paths to unity. The average fading power in each path is defined as [37]

$$E[\alpha_{il}^2] = \frac{1 - \exp(-\mu)}{1 - \exp(-\mu L)} \exp(-l\mu), \tag{2}$$

$$l = 0, 1, 2, \dots, L - 1; \mu \neq 0$$

where  $E[\cdot]$  is the statistical expectation and  $\mu$  is the exponential decay rate of the diffuse power in each path. The probability density function (pdf) of the distributed Rayleigh random variables  $\alpha_{il}$  is given by [5]

$$f_{\alpha_{il}}(x) = 2x/\psi_{il} \exp(-x^2/\psi_{il}), \quad x \geq 0 \tag{3}$$

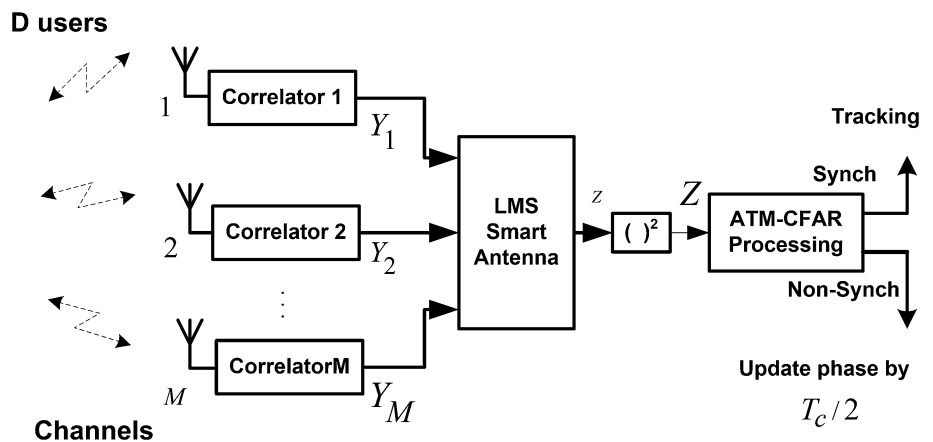
where  $\psi_{il} = E[\alpha_{il}^2]$ ,  $i = 1, \dots, D$ , and  $l = 0, \dots, L - 1$ .

The receiving antenna is a linear array of  $M$  identical elements spaced  $d$  apart with  $d = 0.5\lambda_c$  and  $\lambda_c$  is the wavelength of the carrier transmitted signal. Hence, the response vector of the antenna array is expressed as

$$\mathbf{a}(\theta) = \left[ 1 \ e^{-j\pi \sin\theta} \ \dots \ e^{-j\pi(M-1)\sin\theta} \right]^T \tag{4}$$

where  $\theta$  is the direction of arrival (DOA) angle of the signal and  $T$  denotes transpose. LMS is an adaptive array antenna algorithm which would adapt iteratively its weight vector to any array response vector. The received signal consists of the signal from the first user, MAIs from the others, and an additive white Gaussian noise (AWGN)  $n(t)$ . Thus, the received signal at the  $m$ -th antenna element of the array is [38]

**Fig. 1** Block diagram of the proposed communication system model



$$\begin{aligned}
 r_m(t) = & \sqrt{2P_s} \left\{ \sum_{l=0}^{L-1} \alpha_{1l} b_1(t - \tau_1 - lT_c) c_1(t - \tau_1 - lT_c) \right. \\
 & \left. \times \cos(\omega_c t + \varphi_{1l}) \exp(-j\pi(m-1)\sin\theta_s) \right\} \\
 & + \left\{ \sum_{i=2}^D \sqrt{2P_{i-1}} \sum_{l=0}^{L-1} \alpha_{il} b_i(t - \tau_i - lT_c) c_i(t - \tau_i - lT_c) \right. \\
 & \left. \times \cos(\omega_c t + \varphi_{il}) \exp(-j\pi(m-1)\sin\theta_{i-1}) \right\} + n_m(t); \\
 & m = 1, 2, \dots, M
 \end{aligned} \tag{5}$$

where  $P_s$  is the received signal power of the first user during initial synchronization,  $P_{i-1}$  is the received signal power of the interfering user  $i - 1$ ,  $\tau_i$  is the relative time delay associated with the asynchronous communication channel model;  $\varphi_{il} = \xi_i - \zeta_{il} - \omega_c(\tau_i + lT_c)$  is the phase in the demodulator of the receiver which  $i = 2, 3, \dots, D$ ,  $l = 0, 1, \dots, L - 1$ ,  $T_c$  is the chip duration,  $\theta_s$  is the DOA angle of the first user signal,  $\theta_{i-1}$  is the DOA angle of the interfering user. In this paper we consider the pilot channel instead of pilot symbols and thus we set  $b_i(t) = 1$ .

### 3.2 Correlator

The correlator that follows the  $m$ -th antenna element is shown in Fig. 2. The equivalent baseband signal  $r'_m(t)$  at the correlator can be written as follows

$$\begin{aligned}
 r'_m(t) = & 2\sqrt{P_s} \left\{ \sum_{l=0}^{L-1} \alpha_{1l} c_1(t - \tau_1 - lT_c) \cos(\omega_c t + \varphi_{1l}) \right. \\
 & \left. \times \cos(\omega_c t) \exp(-j\pi(m-1)\sin\theta_s) \right\} \\
 & + 2 \left\{ \sum_{i=2}^D \sqrt{P_{i-1}} \sum_{l=0}^{L-1} \alpha_{il} c_i(t - \tau_i - lT_c) \right. \\
 & \left. \times \cos(\omega_c t + \varphi_{il}) \cos(\omega_c t) \exp(-j\pi(m-1)\sin\theta_{i-1}) \right\} \\
 & + n_m(t);
 \end{aligned} \tag{6}$$

The in-phase and quadrature phase ( $I$ - $Q$ ) components of the correlator are multiplied by the locally generated PN code  $c(t - j_c T_c/2)$ ,  $j_c = 0, 1, \dots, N_c$  ( $N_c$  represents the reference window size of the CFAR processor), and integrated over a dwell time interval  $\tau_D = RT_c$  s, where  $R$  is the correlation length integer to yield respectively the  $I$  and  $Q$  branch components  $Y_m^I$  and  $Y_m^Q$ .

Then the output  $Y_m$  from each branch of the correlator gives the first user signal component, the MAI, and the AWGN, which can be expressed as

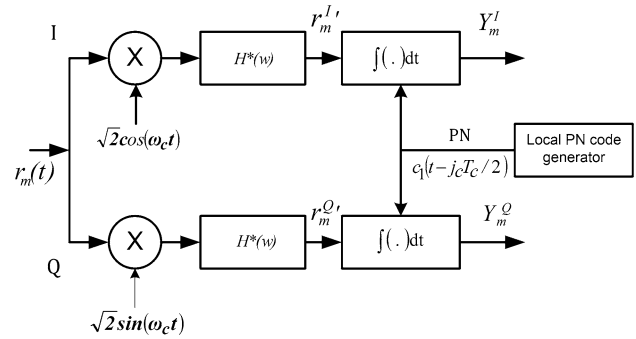


Fig. 2 Correlator consists of in-phase (I) and quadrature-phase (Q) components

$$\begin{aligned}
 Y_m = & \left\{ \sum_{l=0}^{L-1} (Y_{S1}^I + jY_{S1}^Q) \exp(-j\pi(m-1)\sin\theta_s) \right\} \\
 & + \left\{ \sum_{i=2}^D \sum_{l=0}^{L-1} (Y_{MAIil}^I + jY_{MAIil}^Q) \right. \\
 & \left. \times \exp(-j\pi(m-1)\sin\theta_{i-1}) \right\} + n_m
 \end{aligned} \tag{7}$$

where  $Y_{S1}^I + jY_{S1}^Q$  denotes  $I$ - $Q$  component of the first user,  $Y_{MAIil}^I + jY_{MAIil}^Q$  denotes  $I$ - $Q$  component of the MAI, and  $n_m(t) = N_m^I(t) + jN_m^Q(t)$  denotes the thermal noise. The in-phase signal component in (7) due to the first user is given by [8],

$$\begin{aligned}
 Y_{S1}^I = & \sqrt{P_s} \alpha_{1l} \cos(\varphi_{1l}) [\Delta_1 R_p(j_c, N + 1) + (T_c - \Delta_1) R_p(j_c, N)] \\
 = & \sqrt{P_s} R_{S1}^I
 \end{aligned} \tag{8}$$

where

$$R_{S1}^I = \alpha_{1l} \cos(\varphi_{1l}) [\Delta_1 R_p(j_c, N + 1) + (T_c - \Delta_1) R_p(j_c, N)] \tag{9}$$

where  $\Delta_1$  is a random variable uniformly distributed in  $[0, T_c]$  and  $R_p(j_c, N)$  is the code partial autocorrelation function of the first user. The quadrature phase signal component of the first user can be obtained by replacing  $\cos(\varphi_{il})$  with  $-\sin(\varphi_{il})$  in (8). The in-phase MAI term can be defined as

$$\begin{aligned}
 Y_{MAIil}^I = & \sqrt{P_{i-1}} \alpha_{il} \cos(\varphi_{il}) [\Delta_i R_p^{(i)}(j_c, N + 1) \\
 & + (T_c - \Delta_i) R_p^{(i)}(j_c, N)] \\
 = & \sqrt{P_{i-1}} R_{MAIil}^I
 \end{aligned} \tag{10}$$

where

$$R_{MAIil}^I = \alpha_{il} \cos(\varphi_{il}) [\Delta_i R_p^{(i)}(j_c, N + 1) + (T_c - \Delta_i) R_p^{(i)}(j_c, N)] \tag{11}$$

where  $R_p^{(i)}(j_c, N)$  is the code partial cross-correlation between the received sequence of the  $i - 1$ -th user and the

locally generated sequence. The  $R_{MAIl}^l$  decreases the power of the interfering signal that comes out the correlator, which is affected by factor of  $R_p^{(i)}(j_c, N)$ . The quadrature phase signal term of MAIs can be obtained by replacing  $\cos(\varphi_{il})$  with  $-\sin(\varphi_{il})$  in (10); and the noise term is determined by

$$N_m^l = \int_0^{RT_c} n_m^l c_1(t - jT_c/2) \sqrt{2} \cos(\omega_c t) dt \quad (12)$$

The quadrature phase of the noise term is defined by replacing  $\cos(\varphi_{il})$  by  $\sin(\varphi_{il})$ .

### 3.3 Smart antenna

Smart antenna in the proposed system performs adaptive beamforming by using the LMS algorithm by directing the main array pattern towards the preferred source signal and creating nulls in the directions of the interfering signals. The LMS algorithm computes iteratively the optimum beamforming weight vector with minimum square errors (MSE) between the desired signal value and the LMS processor output. We select the LMS algorithm because of its benefits such as simple, ease of implementation, good accuracy, and good convergence properties. The LMS algorithm has fewer of computational and easier for implementation compared to several algorithms; i.e., RLS and SMI. It also has accuracy as good as RLS algorithm. The input of the LMS processor comes from the output  $Y_m$  of  $M$  branches of the correlator which can be defined as follows

$$Y = [Y_1 \ Y_2 \ \dots \ Y_M]^T \quad (13)$$

The inputs of the LMS processor in (7) and (13) can be expressed as follows

$$\begin{aligned} Y &= Y_S^{lQ} + Y_{MAI}^{lQ} + n^{lQ} \\ &= \sum_{l=0}^{L-1} a_{sl}(\theta_{sl}) Y_S^{lQ} + \sum_{i=2}^D \sum_{l=0}^{L-1} a_{i-1l}(\theta_{i-1l}) Y_{MAI}^{lQ} + n^{lQ} \end{aligned} \quad (14)$$

where  $a_{sl}(\cdot)$  is the array steering vector of antenna to the first user or its replicates,  $a_{i-1l}(\cdot)$  is the array steering vector of antenna to the interfering user or the replicates,  $Y_S^{lQ} = (Y_{SI}^l + jY_{SI}^Q)$ ,  $Y_{MAI}^{lQ} = (Y_{MAIi-1l}^l + jY_{MAIi-1l}^Q)$ , and  $n^{lQ} = [n_1^{lQ} \ n_2^{lQ} \ \dots \ n_M^{lQ}]^T$ . The LMS processor incorporates an iterative procedure that makes successive corrections to the weight vector

$$w(n_c) = [w_1(n_c) \ w_2(n_c) \ \dots \ w_M(n_c)]^T \quad (15)$$

where  $n_c$  is a number of iterations until convergence is reached. Once the minimum MSE is attained we claim that

the weight vector in (15) is optimum, which should increase the first user signal to the interference signal ratio (SIR). In other words, it keeps the signal power of the first user as the desired signal and reduces the MAI signal effect. Furthermore, this optimum weight vector is used to generate a spatial correlation output given by

$$z = w_{opt}^H Y \quad (16)$$

Substituting the input of the LMS processor in (14) into (16), we obtain  $z$  as follows

$$z = w_{opt}^H \left\{ \sum_{l=0}^{L-1} a_{sl}(\theta_{sl}) Y_S^{lQ} + \sum_{i=2}^D \sum_{l=0}^{L-1} a_{i-1l}(\theta_{i-1l}) Y_{MAI}^{lQ} + n^{lQ} \right\} \quad (17)$$

The output  $z$  in (17) shows the iterative procedure of the LMS processor weights of the first user signal, the MAI signals, and the AWGN. The weight affects the ratio of the signal power of interfering user  $i - 1$  to the first user signal after the LMS processor, which is  $\beta_{i-1}$ ,  $i = 2, \dots, D$ , while  $\beta_{i-1}$  is defined as

$$\beta_{i-1l} = \left\{ w_{opt}^H a_{i-1l}(\theta_{i-1l}) Y_{i-1l}^{lQ} \right\} / \left\{ w_{opt}^H a_{s0}(\theta_{s0}) Y_{s0}^{lQ} \right\} \quad (18)$$

$a_{s0}(\theta_{s0})$  is the array steering vector of antenna to the first user,  $i = 2, \dots, D$ , and  $l = 1, 2, \dots, L - 1$ . Recall that the weighting of the LMS processor increases the signals to interference ratio (SIR) while the value of  $\beta_{i-1l}$  is decreased, which means the LMS decreases the interfering signal effect. Given the Gaussian nature of  $z^I$  and  $z^Q$ , the variable  $Z = |z|^2$  follows a noncentral Chi square distribution law with two degrees of freedom [5]. Statistically, the pdf of  $Z$  given the amplitude of first user path  $\alpha_{1l}$  corresponding to the  $l$ -th resolvable path can be written as

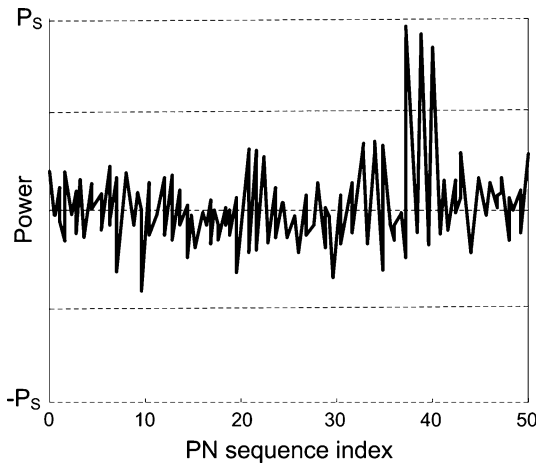
$$\begin{aligned} f_{Z|\alpha_{1l}}(z|\alpha_{1l}, H_1^l) &= \frac{1}{2\sigma_0^2 M_w} \exp\left(-\frac{\lambda^2 M_w^2 + z}{2\sigma_0^2 M_w}\right) I_0\left(\frac{\sqrt{\lambda^2 z}}{\sigma_0^2}\right), \\ z &\geq 0 \end{aligned} \quad (19)$$

$\lambda^2$  is the normalized noncentral parameter given by  $\lambda^2 = 9/16\alpha_{1l}^2$  [39].  $M_w = w^H a_{s0}(\theta_{s0}) M$  is the LMS element weighting factor,  $\sigma_0^2$  is the variance, and  $I_0(\cdot)$  is the zeroth order modified Bessel function of the first kind.  $\sigma_0^2$  is a representation of the background noise resulting from three signals, which are the self-interference from the nonaligned paths  $\sigma_S^2$ , the MAI caused by the interfering users  $\sigma_M^2$ , and thermal noises generated by the antenna array  $\sigma_N^2$  as defined in [8] and given by

$$\sigma_S^2 = \psi_{1l}/(3R) \quad (20)$$

$$\sigma_M^2 = \beta_{i-1lave} \psi_{i-1lave}/(3R) \quad (21)$$

$$\sigma_N^2 = 1/(2RS_c) \quad (22)$$



**Fig. 3** Energy profile of the ATM-CFAR samples

$\beta_{i-1lave}$  denotes the average value of  $\beta_{i-1l}$  s,  $\psi_{i-1lave}$  denotes the average value of  $\psi_{i-1l}$  s, and  $S_c$  denotes SNR/chip given by

$$S_c = T_c P_s / N_0 \tag{23}$$

The pdf of the decision variable  $Z$  under the aligned hypothesis corresponding to the  $l$ -th resolvable path is then obtained, after using Bayes theorem and doing some mathematical manipulations, to be

$$f_Z(z|H_1^l) = \frac{1}{2\sigma_0^2(M_w + M_w^2 v)} \exp\left(-\frac{z}{2\sigma_0^2(M_w + M_w^2 v)}\right), \quad z \geq 0 \tag{24}$$

where  $v = 9\psi_{il}/(32\sigma_0^2)$ . The pdf of decision variable  $Z$  under the nonaligned hypothesis is obtained from (24) to be

$$f_Z(z|H_0) = \frac{1}{2\sigma_0^2 M_w} \exp\left(-\frac{z}{2\sigma_0^2 M_w}\right), \quad z \geq 0 \tag{25}$$

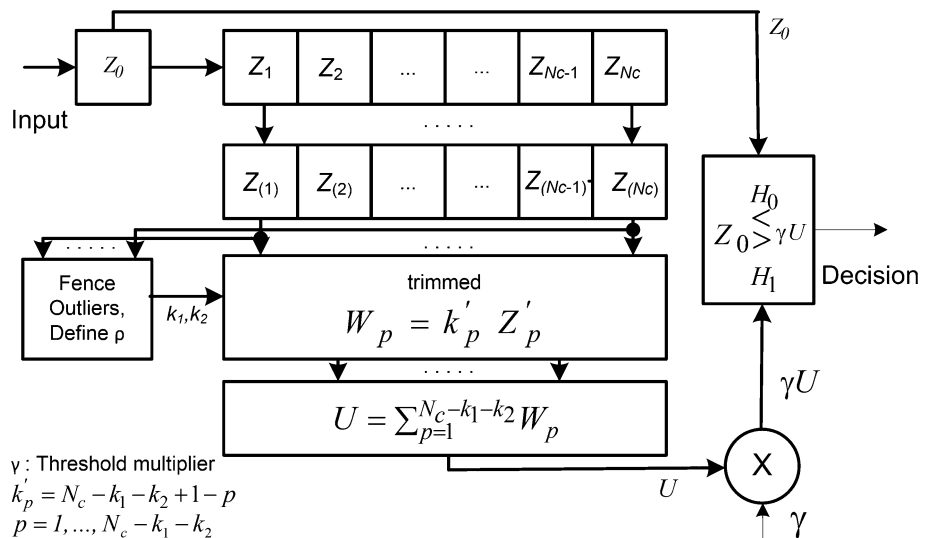
### 3.4 Automatic trimmed mean (ATM) CFAR

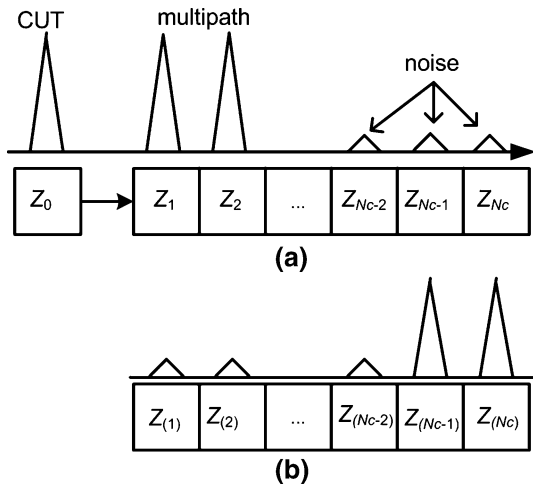
In a multipath fading environment, the transmitted signal is usually reflected by a variety of buildings or terrains. The signals of the first user and other user signals are with a time delay. The multipath delay introduces a high partial autocorrelation between the sequence of the first user and the locally generated PN code sequence. In addition, there are partial cross-correlations between the locally generated sequence and the other users (MAIs). Hence, the output from the LMS processor consists of the multipath signals of the first user with high correlation value and noises with correlation values not significant. The environment and the process which the signal undergoes are:

1. The fading effect on each path as described in (2),
2. The autocorrelation value through the correlator as defined in (8), and
3. The weighting process by the LMS processor as described in (17) affects the value of multipath signals.

We consider the three parameters above as one value  $\kappa$ . The situation described above of the first user can be represented by Fig. 3 [40]. These signals are the samples at the output of the LMS processor and the square operator. The distance between the multipath and noise samples is within thirty-two chips according to the PN code sequence index. The adaptive thresholding scheme used for maintaining the probability of false alarm constant during the code acquisition step in the spread spectrum communication considered is based on ATM-CFAR processing as shown in

**Fig. 4** ATM-CFAR processor with fence outliers for defining multiplier values





**Fig. 5** Interference and noise in reference cell of ATM-CFAR processor

Fig. 4. It consists of three main parts which are the reference cells, the fences for the outliers, and the decision threshold. The output samples from the LMS processor are sent serially into a shift register of length  $N_c$  called reference window and containing the outputs of the previous  $N_c$  phases  $Z_c, c = 1, 2, \dots, N_c$ . The contents of the reference cells are used according to some rule, which is adaptive trimmed mean in our case, as a statistic to represent the estimate of the background noise power level. The cell  $Z_0$  represents the cell under test (CUT) of the current examined phase.

Due to the presence of multipath signals of the first user and noises, we assume  $r$  samples of interfering signals and  $N_c - r$  samples with noise. The  $r$  interfering samples consist of multipath signals of the first user with high correlation values as shown in Fig. 5(a). These samples of the reference cells representing interfering signals plus noise are then arranged in ascending order according to their magnitudes  $Z_{(1)}, Z_{(2)}, \dots, Z_{(N_c)}$  as shown in Fig. 5(b). The ATM-CFAR processor censors  $k_1$  cells from the lower end and  $k_2$  cells from the upper end to eliminate the effect of the interfering signals. Hence, the fences as demarcation points of the outlier determiner are located at  $k_1$  and  $N_c - k_2$ , which are obtained using the Boxplot technique. The interquartile range (IQR) measures a statistical dispersion which is equal to the difference between the third ( $Q_3$ ) and the first ( $Q_1$ ) quartiles. An outlier is the random variable that resides in the outlier region which are below of lower fence (LF) or above of upper fence (UF) given by

$$\begin{aligned} LF &= Q_1 - \rho(IQR) \\ UF &= Q_3 + \rho(IQR) \end{aligned} \tag{26}$$

where  $\rho$  is a multiplier value to determine the outlier fence. The process is summarized as follows:

- Step 1 Define observation of sorted data  $Z_{(1)}, Z_{(2)}, \dots, Z_{(N_c)}$  from the reference cells. Then calculate the value of LF and UF.
- Step 2 Define initial value of  $k = 1$  as a cell index for data exploration of the reference cells.
- Step 3 Determine a value of  $k_1$ , evaluate  $LF \leq Z_{(k)}$  and increase the value of  $k$ . If the conditional upon  $LF \leq Z_{(k)}$  is true, then repeat this step, otherwise set  $k_1 = k$ .
- Step 4 To obtain a value of  $k_2$ , we evaluate  $UF \geq Z_{(k)}$  and increase the value of  $k$ . If the conditional upon  $UF \geq Z_{(k)}$  is true, then set  $k_2 = N_c - k$ , otherwise repeat the evaluation in this step.

Once we obtain  $k_1$  and  $k_2$  from the algorithm above, we censor  $k_1$  cells from the lower end and  $k_2$  from the upper end as in [41]. We perform a transformation of random variable on the remaining cells to obtain  $W_p = k'_p Z'_p$ , where  $k'_p = N_c - k_1 - k_2 + 1 - p, p = 1, \dots, N_c - k_1 - k_2$ . The estimated noise level value  $U$  is obtained by calculating the arithmetic mean of the remaining non-censored cells ( $N_c - k_1 - k_2$ ) to yield

$$U = \sum_{p=1}^{N_c - k_1 - k_2} W_p \tag{27}$$

The estimated noise level value  $U$  is scaled by a threshold multiplier  $\gamma$  in order to achieve the designed false alarm probability. The probability of detection for the  $l$ -th resolvable path can be determined by

$$P_{dl} = \prod_{p=1}^{N_c - k_1 - k_2} \Omega_{W_p} \left( \frac{\gamma}{\eta(1 + M_w \nu)} \right) \tag{28}$$

where  $\Omega_{W_p}$  is the moment generating function (mgf) of the random variables  $W_p$ 's,  $\eta = 2\sigma_0^2 M_w$ . The individual mgf of  $W_p$ 's are given by:

$$\begin{aligned} \Omega_{w_1} \left( \frac{\gamma}{\eta(1 + M_w \nu)} \right) &= q_1 \binom{N_c}{k_1} \sum_{b=0}^{k_1} (-1)^b \\ &\times \binom{k_1}{b} \frac{1}{\gamma/(1 + M_w \nu) + q_1 + q_1 b/(N_c - k_1)} \end{aligned} \tag{29}$$

$$\Omega_{w_p} \left( \frac{\gamma}{\eta(1 + M_w v)} \right) \begin{cases} = \frac{q_p}{\gamma/(1 + M_w v) + q_p}, & p = 2, \dots, N_c - r - k_1 \\ = \frac{q_p}{\gamma(1 + M_w I)/(1 + M_w v) + q_p}, & p = N_c - r - k_1 + 1, \dots, N_c - k_1 - k_2 \end{cases} \quad (30)$$

where  $q_p = (N_c - k_1 + 1 - p)/(N_c - k_1 - k_2 + 1 - p)$ ,  $q_1$  is  $q_p$  with  $p = 1$ , and  $I = l\sigma_S^2/\sigma_N^2$ .

The overall probability of detection  $P_d$  of the ATM CFAR processor is the expected value of the probability of detection for the  $l$ -th resolvable path  $P_{dl}$  with respect to the priori distribution. The probability of false alarm can be calculated theoretically by replacing  $\gamma/(1 + M_w v)$  with  $\gamma$  in (28) to obtain

$$P_f = \prod_{p=1}^{N_c - k_1 - k_2} \Omega_{w_p} \left( \frac{\gamma}{\eta} \right) \quad (31)$$

The CUT  $Z_0$  is then compared to the adaptive threshold  $\gamma U$  to decide  $H_1^l$  or  $H_0$ .  $H_1^l$  means the sample  $Z$  exceeds the detection threshold  $\gamma U$  and then tracking is performed. Otherwise, decide  $H_0$  which means there is no acquisition.

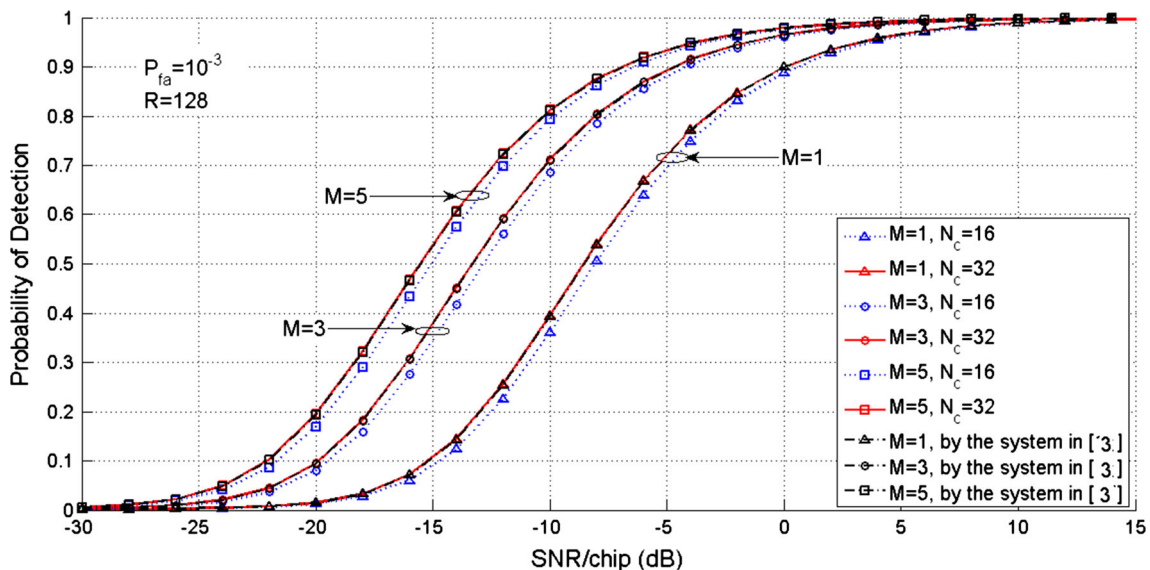
### 4 Results and discussions

In this section, we investigate the detection performance and the multiplier value  $\rho$  to determine the demarcation points at the lower and upper trimming of the proposed communication system for various parameters. The design

probability of false alarm is  $P_{fa} = 10^{-3}$ . Figure 6 shows a comparison of  $P_d$  between the proposed system and the system in [3] [using Eq. (31)]. The received signal comes from the first user signal without multipath of the first user. The lower trim  $k_1$  and upper trim  $k_2$  are equal to zero. The correlation length integer of the dwell time interval is  $R = 128$ , and the number of reference cells are  $N_c = 16$  and 32. The proposed system with a number of reference cells  $N_c = 16$  (dotted lines), lower trim  $k_1 = 0$ , and upper trim  $k_2 = 0$ , has slightly lower performance than the one in [3], but the same performance when  $N_c = 32$ . We note that the detection probability increases as the number of reference cells  $N_c$  increases as expected. We observe, however, that the proposed system with smart antennas can detect signals with lower SNRs.

With  $N_c = 16$  and  $M = 1$  we have a probability of detection  $P_d = 0.9$  at an  $SNR/chip = 0$  dB, whereas with  $N_c = 16$  and  $M = 5$  we get the same  $P_d$  at a much lower  $SNR/chip = -6$  dB. In other words,  $P_d$  increases as the number of antenna elements increases.

Figure 7 shows the simulated values of  $\rho$  using (26) against  $SNR/chip$  for several cell index values  $k$ 's when the number of reference cells  $N_c = 32$ , the number of multipath  $L = 3$ , and the number of users  $D = 3$ .  $\rho_{max}$  denotes



**Fig. 6** Comparison of probabilities of detection between the proposed system and system in [3] with  $N_c$  and  $M$  as parameters;  $P_{fa} = 10^{-3}$ ,  $R = 128$



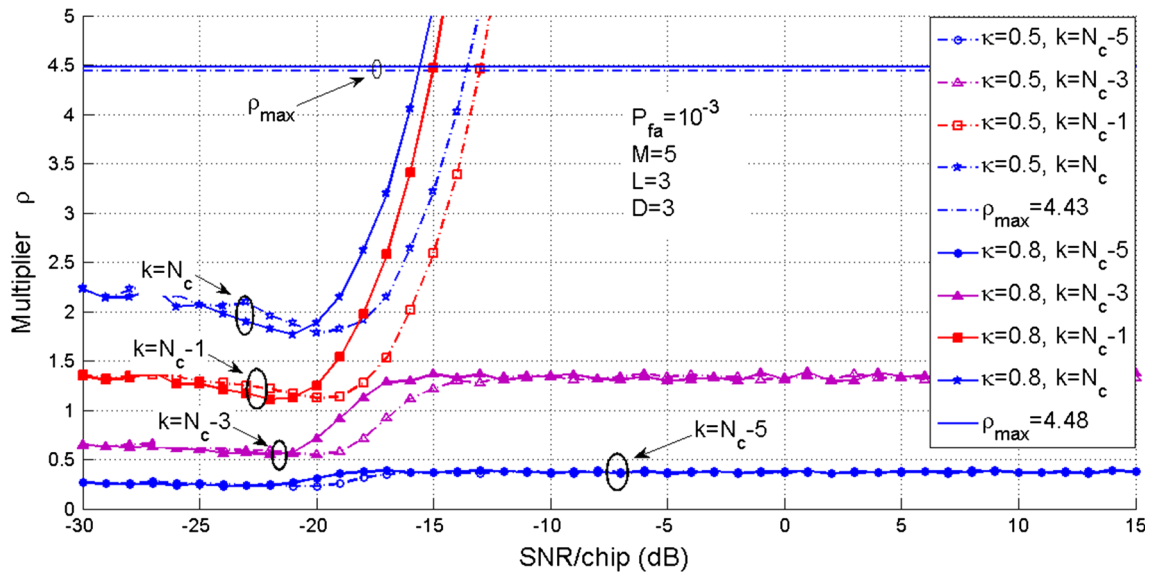


Fig. 7 Multiplier ( $\rho$ ) values of the proposed system for varying  $\kappa$  and  $k$ ; with  $P_{fa} = 10^{-3}$ ,  $M = 5$ ,  $L = 3$ , and  $D = 3$

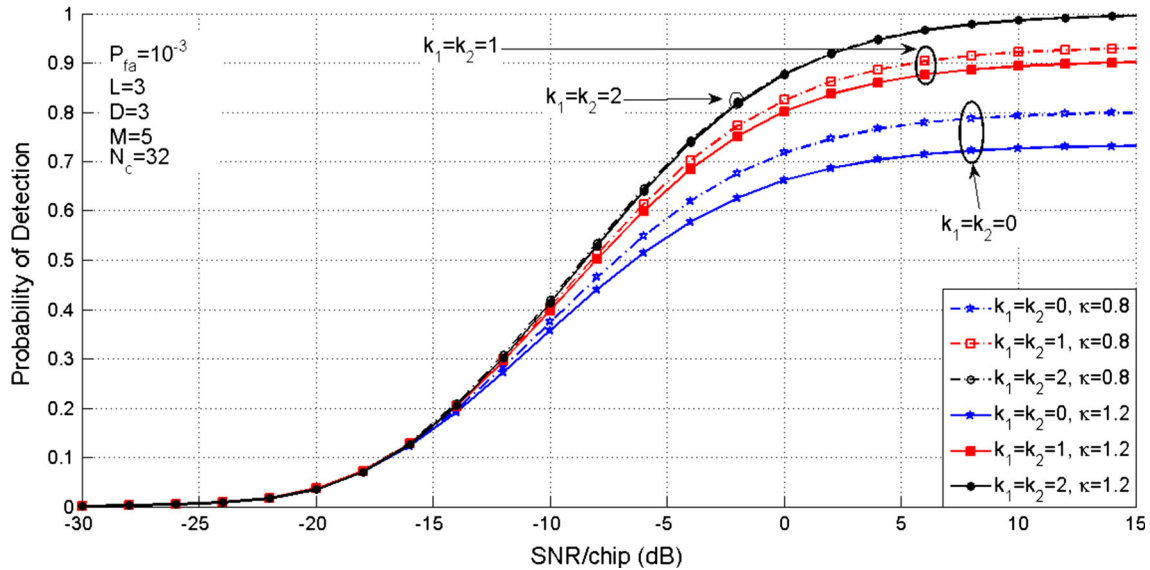


Fig. 8 Probabilities of detection of the system for varying  $\kappa$ ,  $k_1$  and  $k_2$ ; with  $P_{fa} = 10^{-3}$ ,  $M = 5$ ,  $L = 3$ ,  $D = 3$ , and  $N_c = 32$

the maximum value which limits the fence at cell index value less than the number of the reference cells  $N_c$ . The value of  $\rho$  for a reference cell that does not contain interference will never reach  $\rho_{max}$ , e.g.,  $\rho_{k=N_c-3}$ . Based on the simulated results, we can obtain the appropriate  $\rho$  to determine the fences at  $k_1$  and  $N_c - k_2$  using the algorithm as explained above at Sect. 2. In [34], it is suggested that a  $\rho$  with values of 1.5 and 3.0 would not be appropriate for our system. We observe that the proposed system will censor cells that contain interference appropriately by using  $\rho$  less than the suggested values in [34].

In Fig. 8, we give the probability of detection  $P_d$  for  $M = 5$  while varying  $\kappa$ ,  $k_1$  and  $k_2$ . We observe that the

performance of the system decreases as  $\kappa$  increases but once apply the ATM CFAR processing as suggested  $P_d$  is seriously improved which emphasizes the robustness of the algorithm proposed. In Fig. 9 we observe that for  $\kappa = 0.8$  while varying  $R$ , the performance of the system is significantly degraded by the presence of the interferences, that is there is no censoring ( $k_1 = k_2 = 0$ ). At low  $SNR/chip$  the probability of detection increases as the correlation length integer  $R$  increases; e.g., with  $k_1 = k_2 = 0$  and  $SNR/chip = -10$  dB, the  $P_d$  of the system for  $R = 128$  and  $R = 256$  are 0.38 and 0.51, respectively.

In Fig. 10, we plot the probability of detection  $P_d$  for  $\kappa = 1$ , antenna elements  $M = 1$  and  $M = 5$  while varying

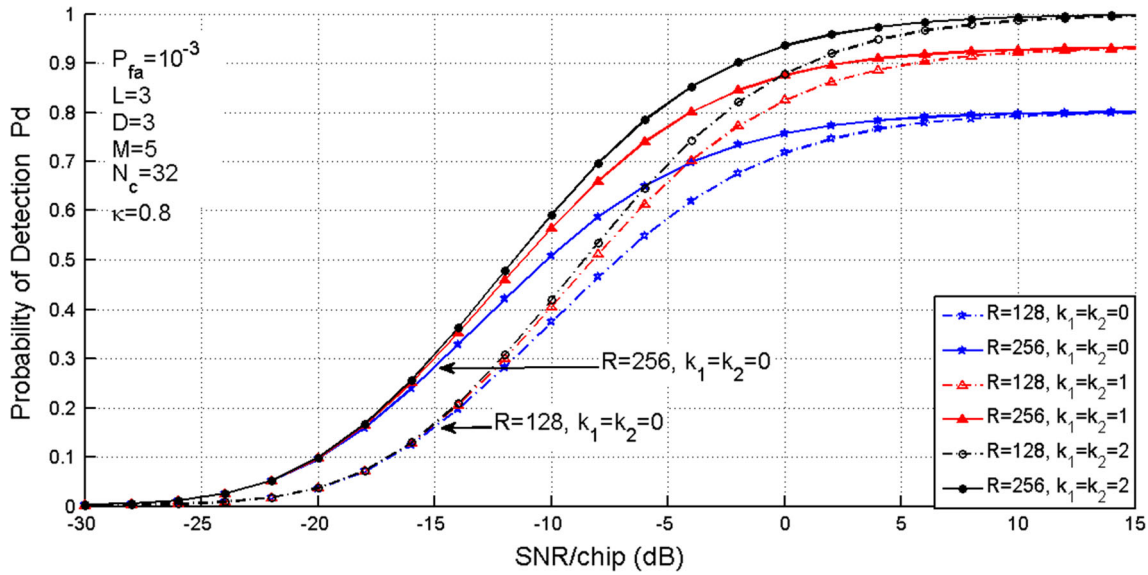


Fig. 9 Probabilities of detection of the system for varying  $R, k_1$ , and  $k_2$ ; with  $P_{fa} = 10^{-3}$ ,  $M = 5$ ,  $L = 3$ ,  $D = 3$ ,  $N_c = 32$  and  $\kappa = 0.8$

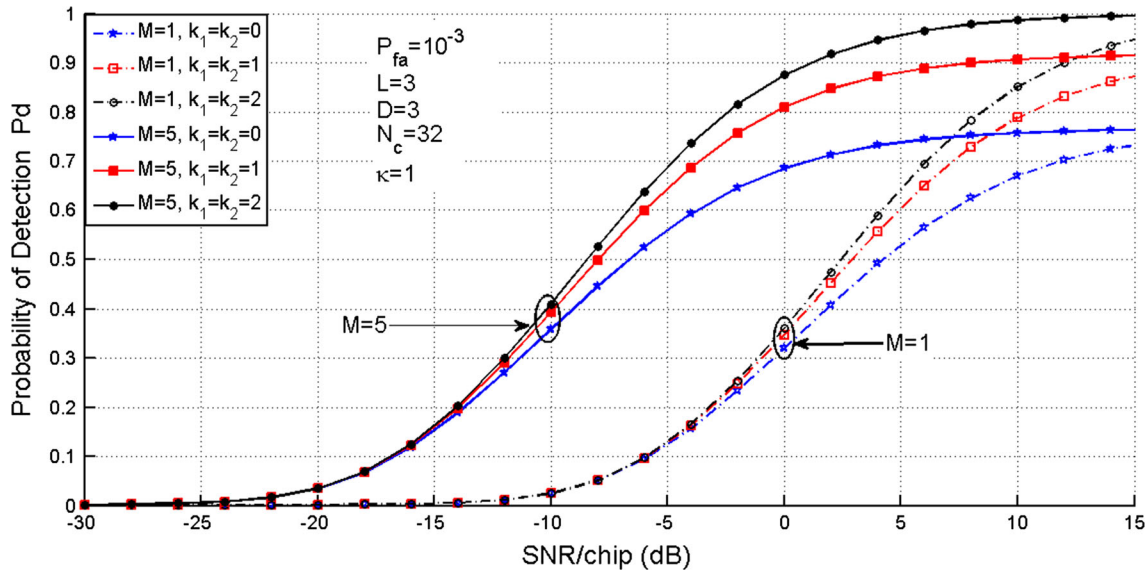


Fig. 10 Probabilities of detection of the system for varying  $M, k_1$ , and  $k_2$ ; with  $P_{fa} = 10^{-3}$ ,  $M = 5$ ,  $L = 3$ ,  $D = 3$ ,  $N_c = 32$  and  $\kappa = 1$

the censoring points  $k_1$ , and  $k_2$ . The performance of the system increases as the number of antenna elements increases as expected.

We also observe that even without censoring the interferences, the detection performance of the system with  $M = 5$  is better than that of the system with  $M = 1$ ; e.g., with  $k_1 = k_2 = 0$  and for  $SNR/chip = 0$  dB,  $P_d$  of the proposed system with  $M = 5$  and  $M = 1$  are 0.69 and 0.32, respectively. The smart antenna allows an enhancement of 0.37 (115 %). With censoring and if  $k_1 = k_2 = 2$ , which is equal to the number of multipath considered, for an  $SNR/chip = 0$  dB,  $P_d$  of the system for  $M = 5$  and  $M = 1$  are 0.88 and 0.36, respectively, which shows a significant

enhancement of 0.52 (144 %). Hence, the proposed system shows robustness as the probability of detection is significantly improved.

### 5 Conclusion

In this paper, we have proposed a spread spectrum communication system using smart antennas and adaptive ATM-CFAR processing with fence outliers determiner, a robust algorithm based on rank order statistics, for direct sequence PN code acquisition. We developed expressions for the conditional probability density functions of the

aligned and the nonaligned hypotheses using the LMS algorithm. The performance of the proposed system was studied in terms of simulated curves of the probability detection for several parameters. As expected, increasing number of reference cells in ATM-CFAR processing and the number of antenna elements enhanced the detection performance. In addition, by appropriately censoring the cells containing interferences, the performance of the systems is more robust compared to the system proposed in [3]. Recall that the performance of the system in [3] was only comparable to the proposed system with the conventional CA-CFAR processing. We also investigated values of  $\rho$  to determine the fences for proper identification of outliers. This approach of using a smart antenna with adaptive thresholding ATM-CFAR processing with an outlier determiner proved to be robust in combating MAI and multipath since the probability of detection improved significantly.

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