

Highlights in modeling the reactive magnetron sputtering process with RSD2013

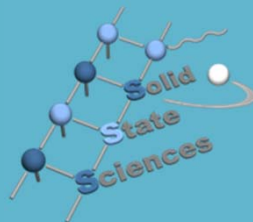
Koen Strijckmans,

Roeland Schelfhout, Florian Cougnon, Diederik Depla

MIATEC 2015

RSD2015

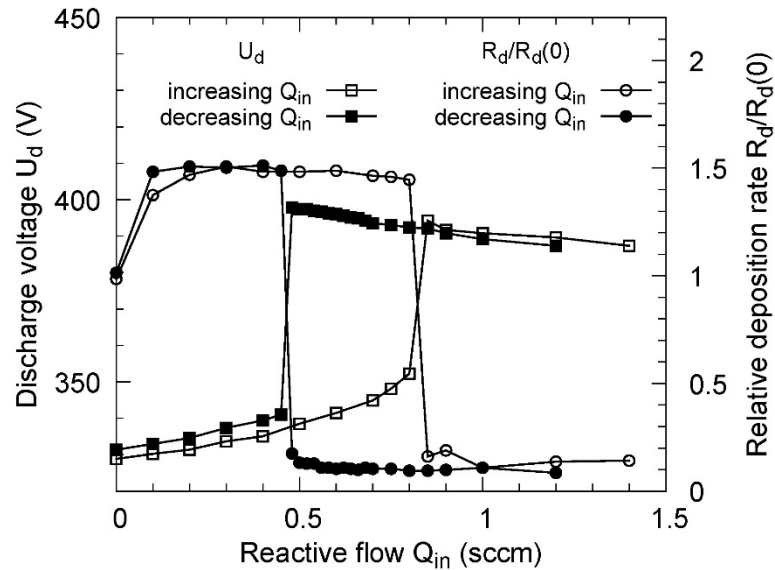
11th December 2015



Outline

- ① Introduction
- ② RSD2013 model
- ③ Finding parameters
- ④ Case studies
 - a) Redeposition
 - b) Dual target
 - c) Substrate rotation
- ⑤ Conclusion

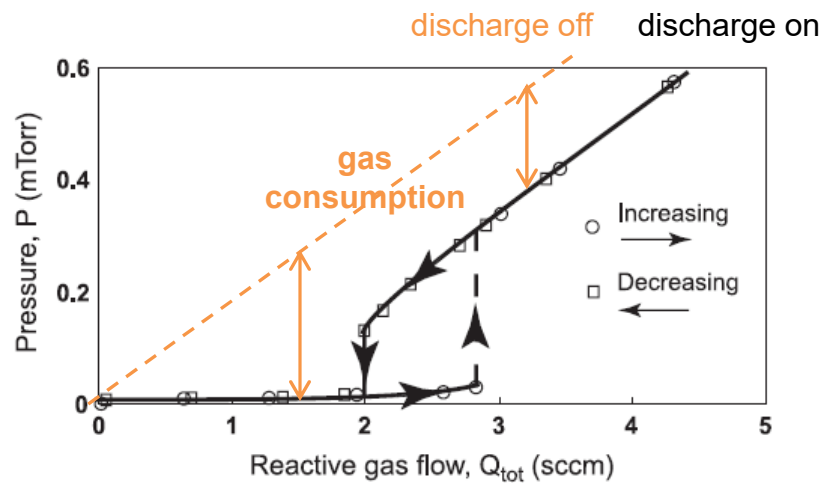
Hysteresis phenomena



Direct controlled hysteresis experiment = stepwise in/decrease of single **operation parameter** (e.g. reactive flow Q_{in})

Hysteresis in

- reactive gas pressure
- discharge voltage
- deposition rate



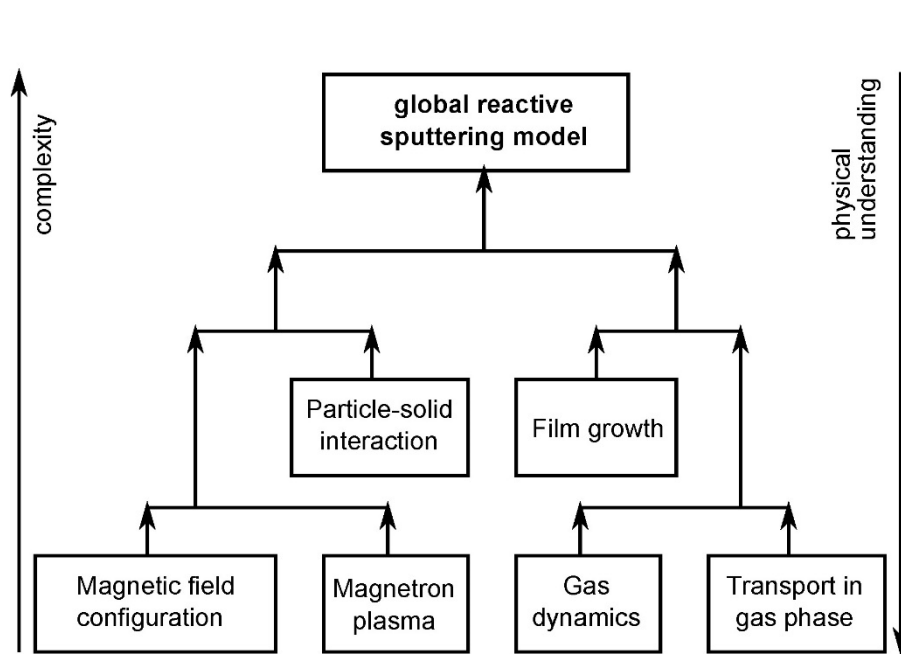
by **poisoning** (=compound formation target)

- vanishing getter pump
- changing Y_{SEE}
- decreasing sputter yield ($Y_c \ll Y_m$)

Two modeling approaches

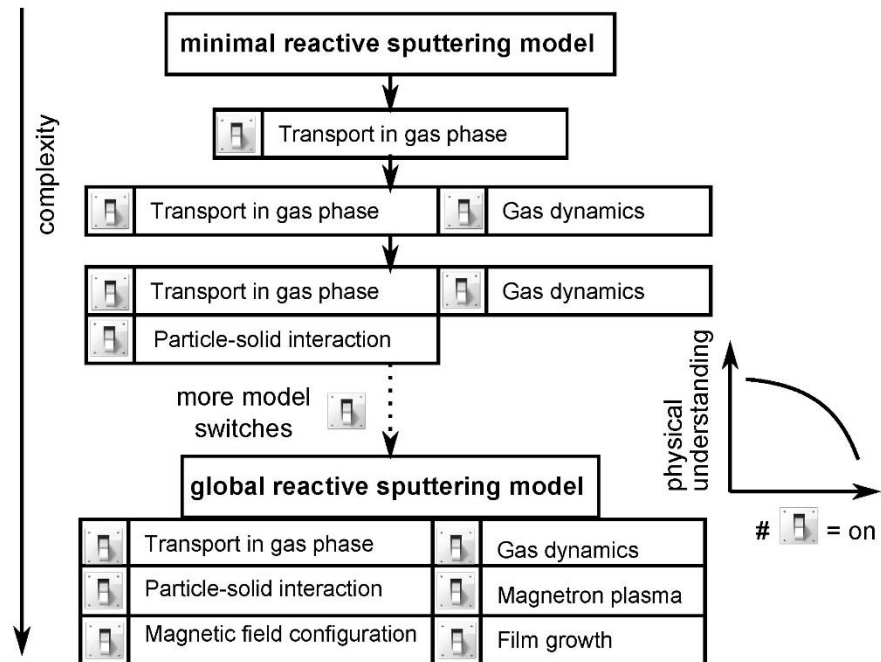
Atomistic approach =

combine complex but detailed models of the subprocesses into a even more complex global model



Holistic approach =

start from a minimal but global model that is gradually expanded with the ability of modularity to a complex global model



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Variables in RSD model

System part	Resolved variable	Model approach
Chamber	P Q_p	reactive partial pressure gas flow to pump one-cell
Target	Q_t	gas flow consumption uniform current one-cell
• Surface	θ_m θ_c	metallic fraction chemisorbed fraction multi-cell non-uniform current
• Subsurface	θ_r n_m(x) n_r(x)	reacted fraction metal concentration reactive gas concentration depth profile SRIM implantation
Substrate	θ_s Q_s	chemisorbed fraction gas flow consumption one-cell multi-cell SIMTRA profile

5 **BALANCE** equations ⇔ 5 **ODE's**

$$0 = f(y) \leftrightarrow \frac{dy}{dt} = f(y)$$

Steady state ⇔ **Time**

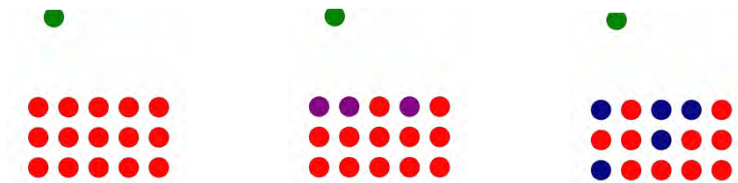
2 **ODE's** ⇔ 2 **PDE's**

$$0 = f\left(y, \frac{\partial y}{\partial x}\right) \leftrightarrow \frac{\partial y}{\partial t} = f\left(y, \frac{\partial y}{\partial x}\right)$$

Processes in RSD2013

Target

sputtering

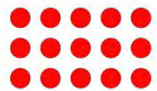
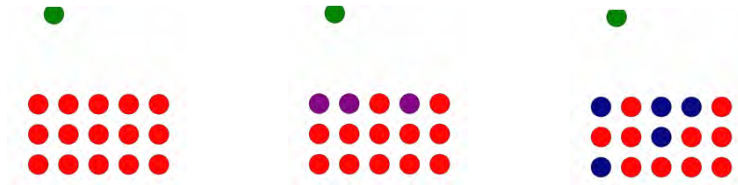


- metal M
- chemisorbed MR_z
- reacted MR_z
- reactive molecule R_2
- inert gas Ar
- reactive implanted atom R







Processes in RSD2013

Target

sputtering



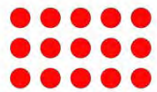
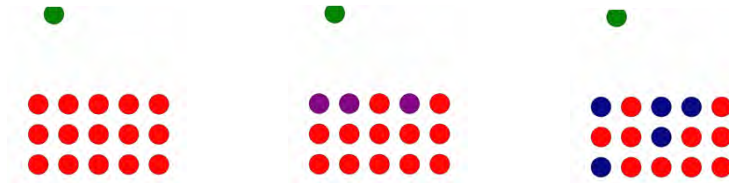
direct implantation

-  metal M
-  chemisorbed MR_z
-  reacted MR_z
-  reactive molecule R_2
-  inert gas Ar
-  reactive implanted atom R

Processes in RSD2013

Target







sputtering



direct implantation



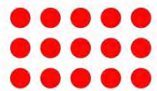
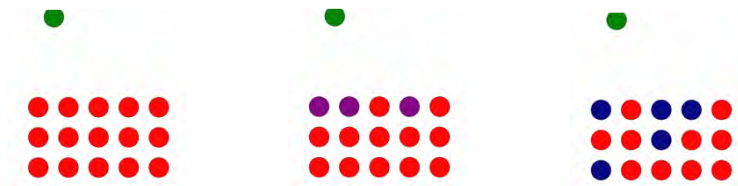
knock-on implantation

-  metal M
-  chemisorbed MR_z
-  reacted MR_z
-  reactive molecule R_2
-  inert gas Ar
-  reactive implanted atom R

Processes in RSD2013

Target

sputtering

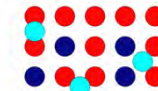








direct implantation



knock-on implantation

reaction

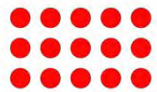
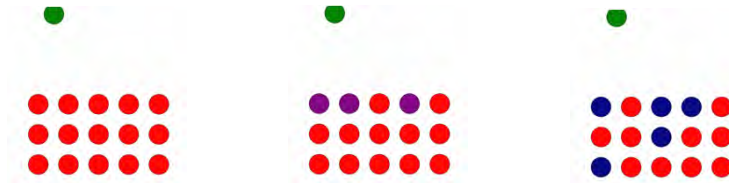


-  metal M
-  chemisorbed MR_z
-  reacted MR_z
-  reactive molecule R_2
-  inert gas Ar
-  reactive implanted atom R

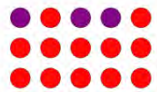
Processes in RSD2013

Target

sputtering

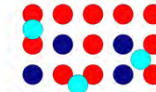


direct implantation



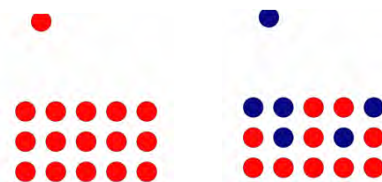
knock-on implantation







reaction



Target & substrate

deposition

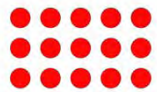
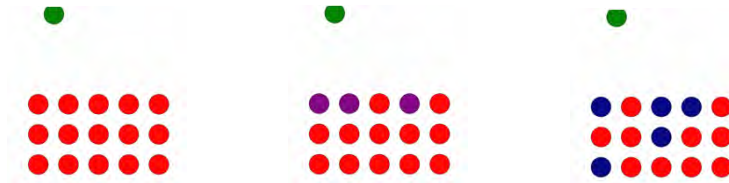


-  metal M
-  chemisorbed MR_z
-  reacted MR_z
-  reactive molecule R₂
-  inert gas Ar
-  reactive implanted atom R

Processes in RSD2013

Target

sputtering

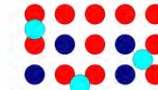


direct implantation



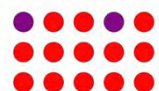
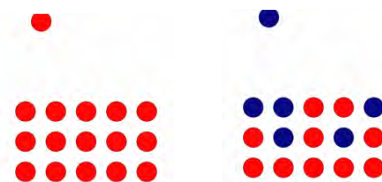
knock-on implantation

reaction









Target & substrate

deposition



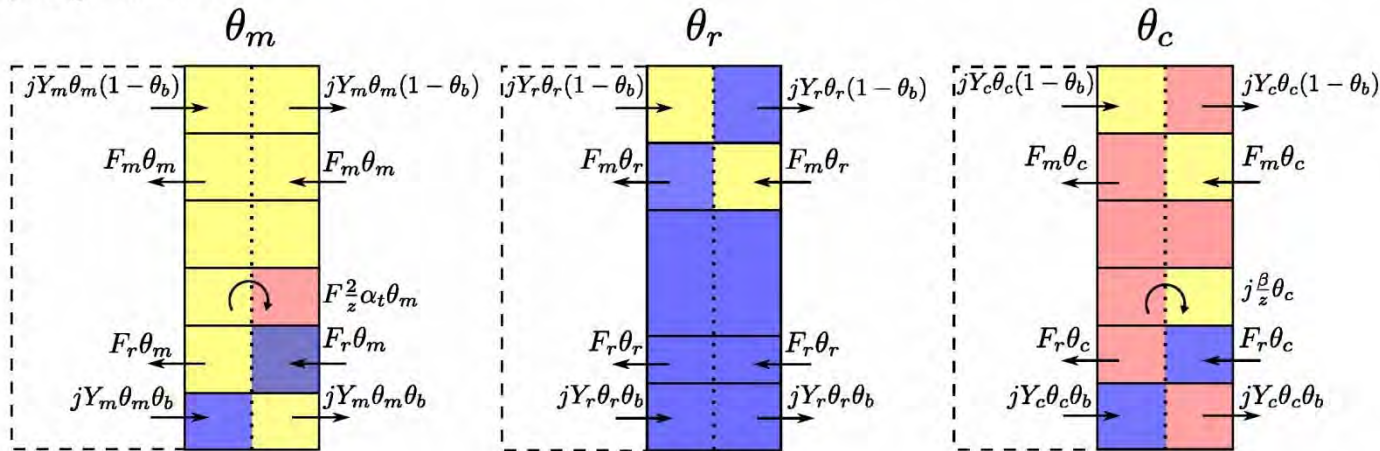
chemisorption

-  metal M
-  chemisorbed MR_z
-  reacted MR_z
-  reactive molecule R_2
-  inert gas Ar
-  reactive implanted atom R

From RSD2009 to RSD2013

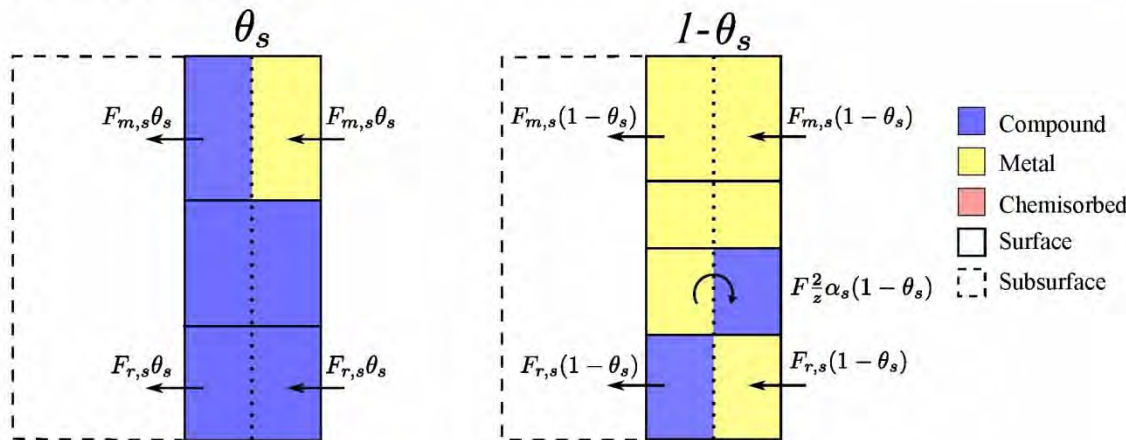
Derivation based on conservation of particles M and MR_z

(a) Target surface cell



multi-cell target
with deposition =
redeposition

(b) Substrate surface cell



RSD2013=
critical revision of RSD2009

- two discrete layer + subsurface
- saturation limit
- redefining surface equations

K. Strijckmans et al., *J. Phys. D: Appl. Phys.* 47 (2014) 235302

Connected with other software



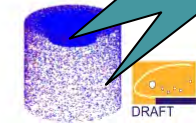
OR
SDTrimSP
TriDyn

nascent distribution



DRAFT Research Group
Ghent University
www.draft.ugent.be

Version 2.1.1-beta
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reactive implantation profile
knock-on yield
(sputter yields ?!)

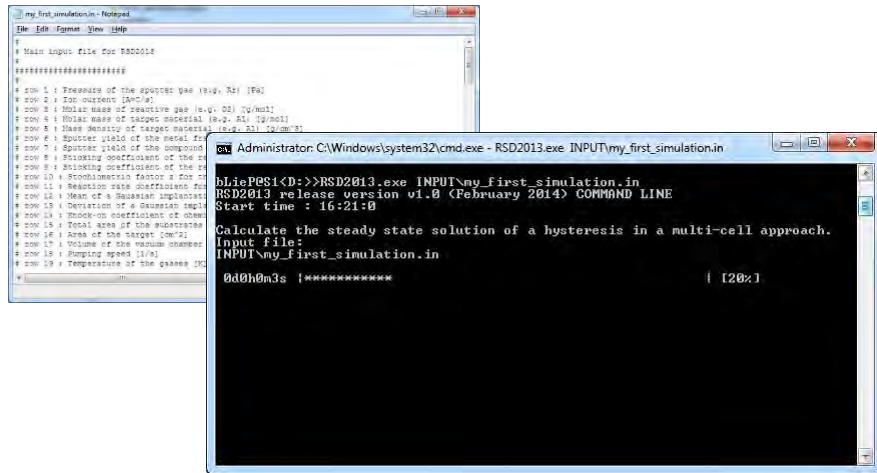
(re)deposition profile
redeposition fraction

D. Depla, et al.,
Thin Solid Films 520(20), 6337 (2012)

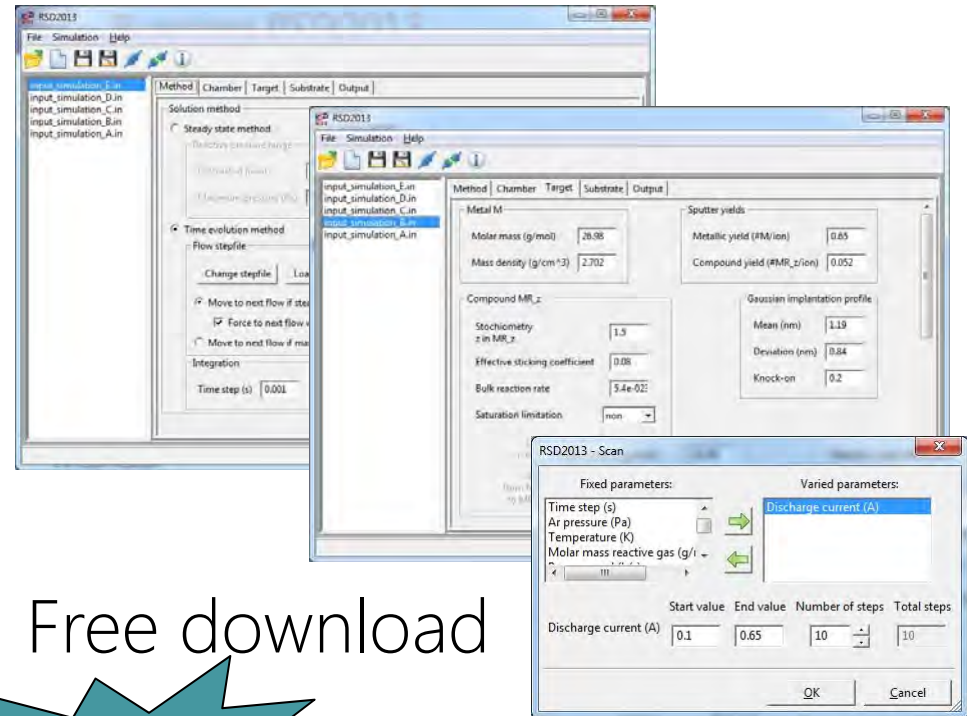


Running RSD2013 software

Command line



Graphical user interface (GUI)



Manual

Installation

The RSD2013 software is compiled to run on a Windows platform. It mainly consist out of two executables: `RSD2013.exe` and `RSD2013_GUI.exe`. The first executable is the graphical user interface (GUI) which makes the `RSD2013.exe` and can start up the RSD2013 simulation. The second executable is the effective simulation program. After downloading an install file with the GUI or manually, you can run `RSD2013_GUI.exe` on the `INSTALL` file to perform the installation.

Overview

The RSD2013 software is developed to simulate the reactive sputter process of a DC magnetron. Its focus is on the possible hysteresis curve of this process. To this end, it solves the equations of the RSD2013 model. By knowing the `START` and `STOP` values, you can run `RSD2013.exe` on the `INSTALL` file to perform the simulation.

The RSD model calculates following variables:

- the pressure P_i of the reactive gas in the system
- the compound O_x , dimensionless f_i , and metal f_m fractions of the target surface
- the compound O_x and metal fractions of the substrate surface
- the metal concentration n_m in the target substrate region
- the compound concentration in the target substrate region which is directly derived from n_m
- the non reacted implanted reactive gas concentration n_{rg} in the target substrate region
- the consumptions Q_i of reactive gas by the target
- the consumptions Q_s of reactive gas by the substrate
- the amount of reactive gas Q_p pumped away by the vacuum pump
- the amount of reactive gas Q_{in} introduced into the vacuum chamber

To the end the RSD model needs several input variables. These input variables are clarified throughout the following sections.

Quick start

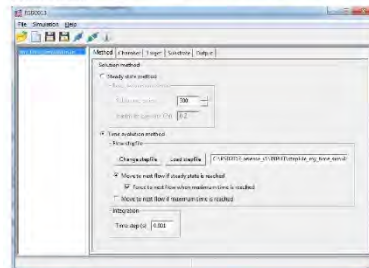
To run a first RSD simulation, you just double click the GUI executable `RSD2013_GUI.exe`. By default a complete input is specified in the window tabs `Method`, `Chamber`, `Target`, `Substrate` and `Output`.

All simulation options are visual within the window tabs. New used or relevant options or fields are grayed out and inaccessible. They become (un)accessible depending on which simulation choices you make. For example, when choosing the `Steady state method` in the window tab `Method` or `Time evolution method`, then the fields connected to the `Time evolution method` are irrelevant and as such grayed out.

Most fields have a restricted range of values that can set. This restriction only applies to the GUI and can be easily overruled by manually editing the `input.in` file.

Method

The window tab `Method` basically specifies from the RSD2013 model should be solved. Its solution method, two options are available: the `Steady state method` and `Time evolution method`. Primarily is the choice between the two methods exclusive.



Method window tabs

Steady state method

To solve the RSD2013 model in its steady state description, the reactive pressure P_i is stepwise increased up to the `START` pressure, and subsequently decreased. The total number of reactive pressure P_i values that are calculated are given by the field `Calculated points`.

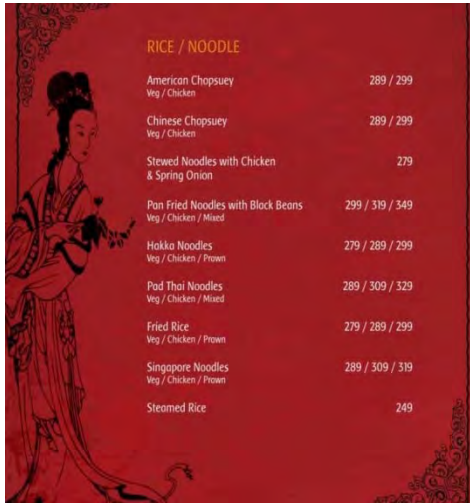
Calculated points

To define the total number N of reactive pressure P_i values that are calculated in the `START` and `STOP` values. So the $N/2$ reactive pressure P_i values are each calculated twice. The first time for an increasing reactive flow Q_{in} and the second time for a decreasing reactive flow Q_{in} .

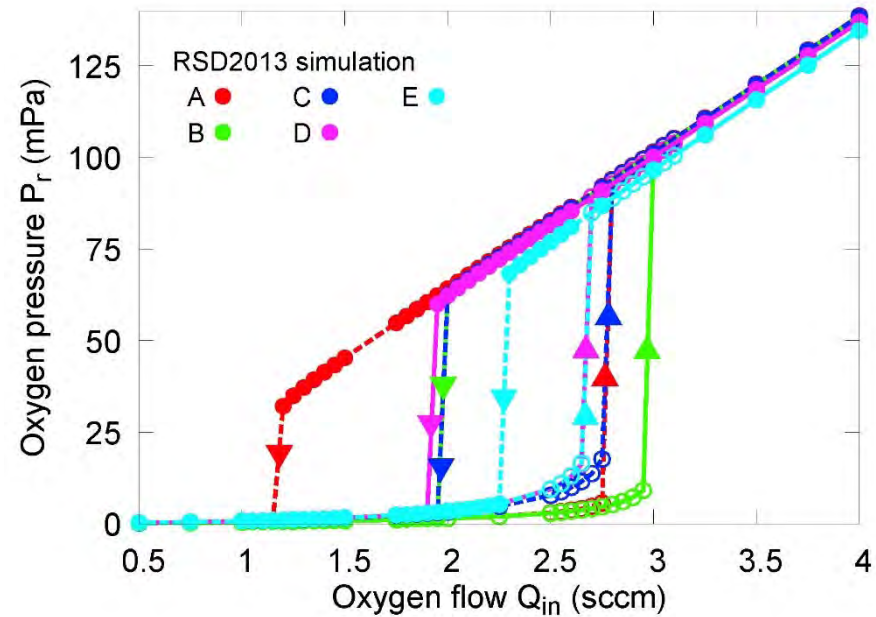
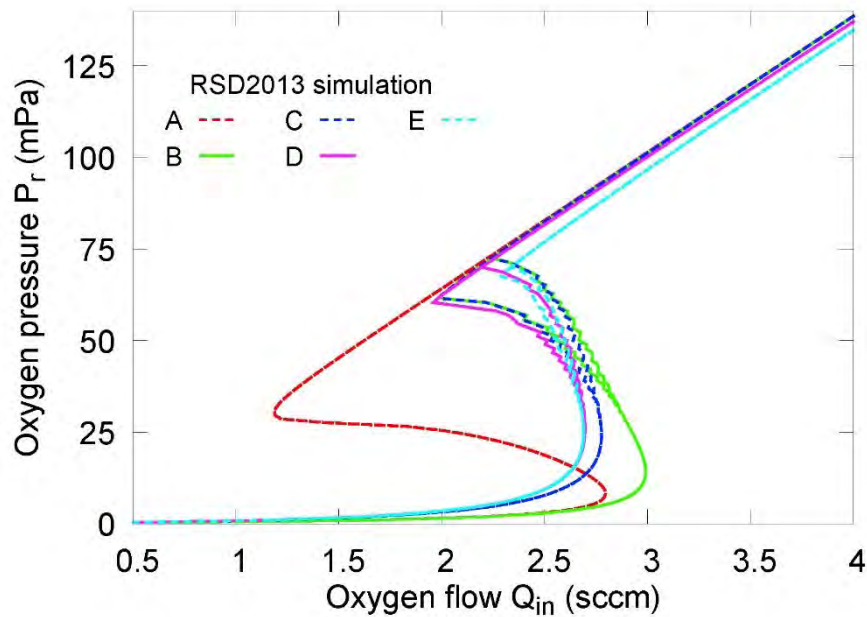
Free download



The "Chinese menu card" of RSD2013



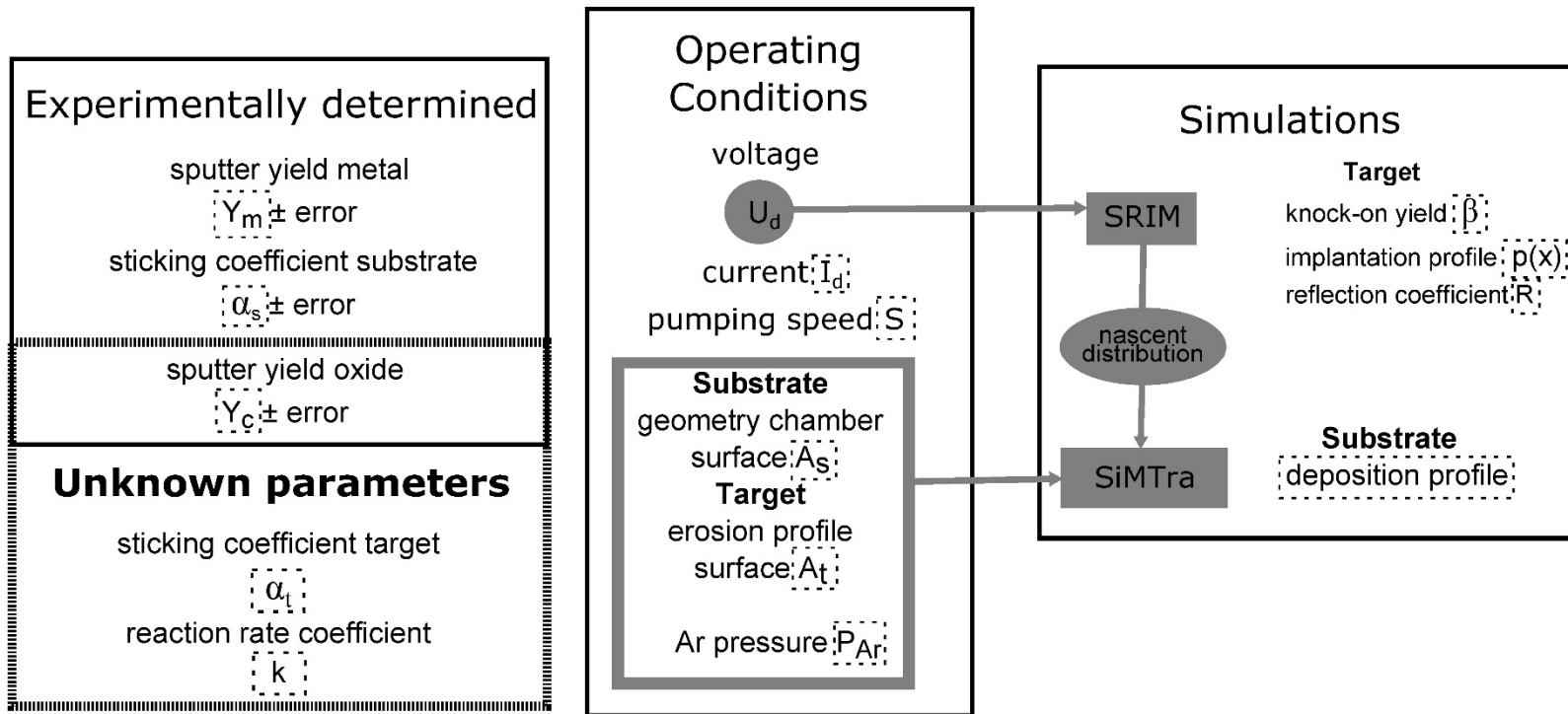
Solution:	Steady		Time			
Uniform deposition	C,D,E	A,B	Deposition profile	C,D,E	A,B	Uniform deposition
No redeposition	D,E	A,B,C	Redeposition	D,E	A,B,C	No redeposition
Uniform current	B,C,D, E	A	Non-uniform current	B,C,D, E	A	Uniform current
No saturation limit	E	A,B,C, D	Saturation limit	E	A,B,C, D	No saturation limit



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Input parameters : the quest



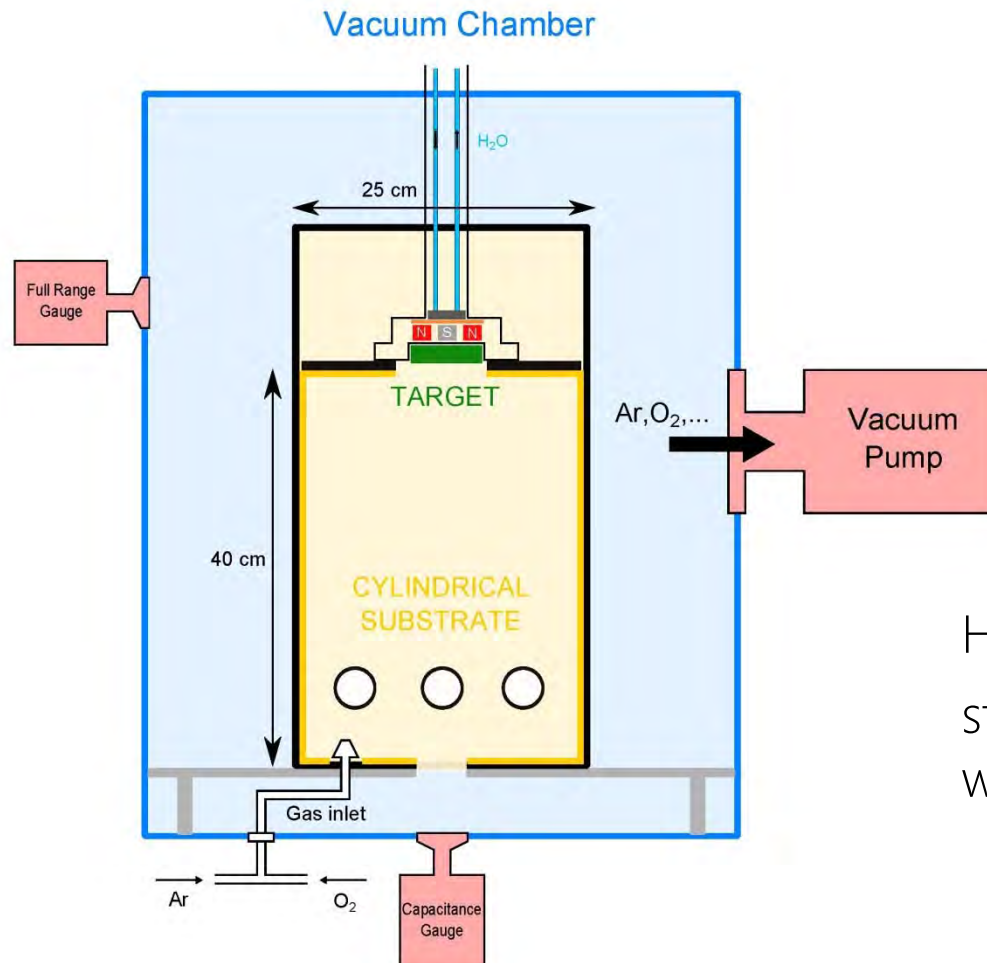
Problem: 2 unknown parameters (α_t , k)

Reason: experimentally or by simulation hard to retrieve (even for Y_c)

Goal: fit freedom and material dependency

Solution: fitting RSD model to experiments

Experimental setup



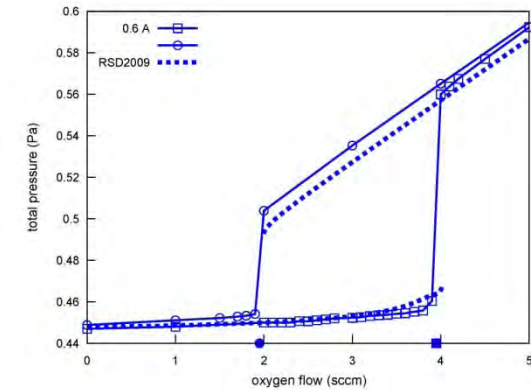
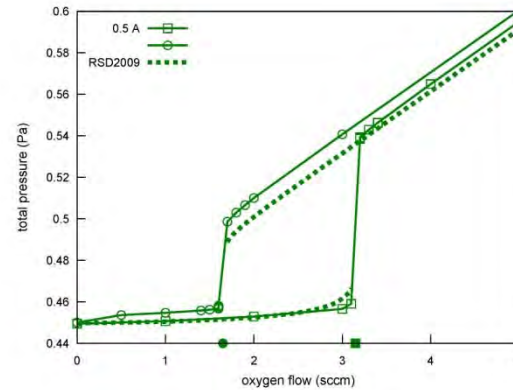
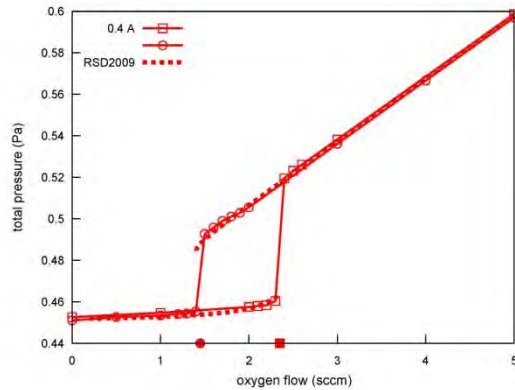
Sputter conditions:

- Target **Al** or **Y** ($D = 2''$)
- Process gas **Ar**
- Reactive gas **O₂**
- $S = 55 \text{ L/s}$ or 112 L/s
- $P_{\text{base}} = \sim 10^{-4} \text{ Pa}$
- $P_{\text{Ar}} = 0.45 \text{ Pa}$ or 0.37 Pa
- $I = 0.4 \text{ A}$, 0.5 A or 0.6 A

Hysteresis experiment =
stepwise in/decreasing the O₂ flow
while collecting

👉 steady state values 👈
 V , I and P_{tot}

Fitting procedure



Fit criteria = 6 critical O₂ flow values

- goodness of the fit = worst match out of 6
- fits are 'good' if critical points fall within acceptance tolerance f_a
(=experimental resolution)

Simulation includes

- ✓ measured V and I variation
- ✓ changing target oxidation

Y_m and I_{ion}
oxygen implantation profile
 I_{ion} (by Y_{SEE})

Scan algorithm

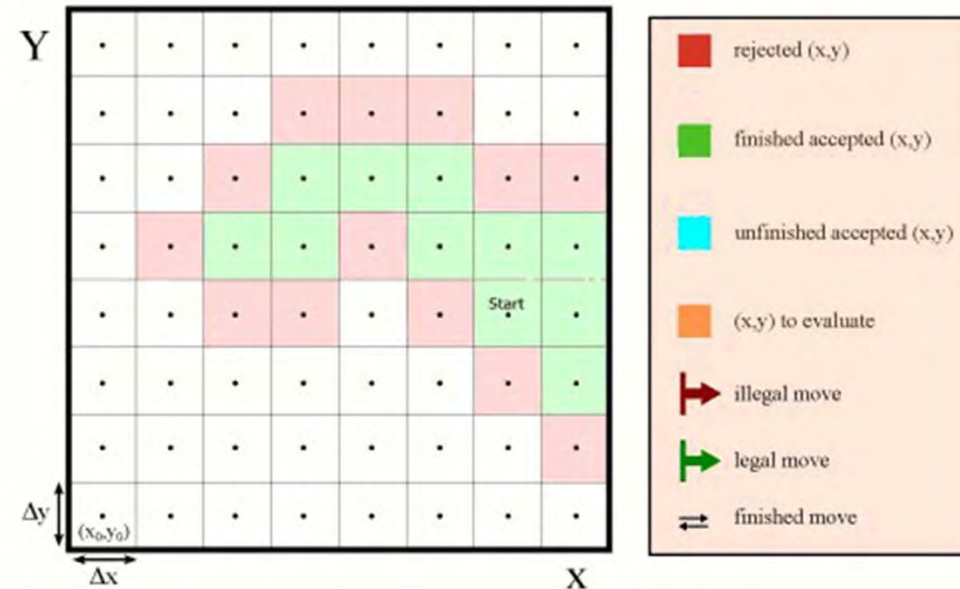
Serial implementation
illustrated for a 2-D
parameter space
(X,Y)

Goal finding all (x_i, y_i) combinations
that pass the fit criteria

Ingredients

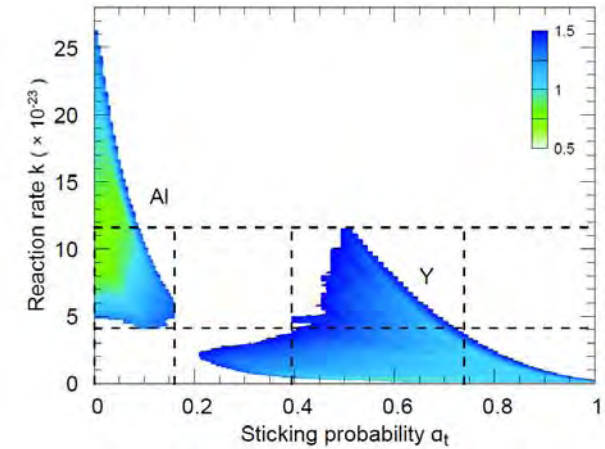
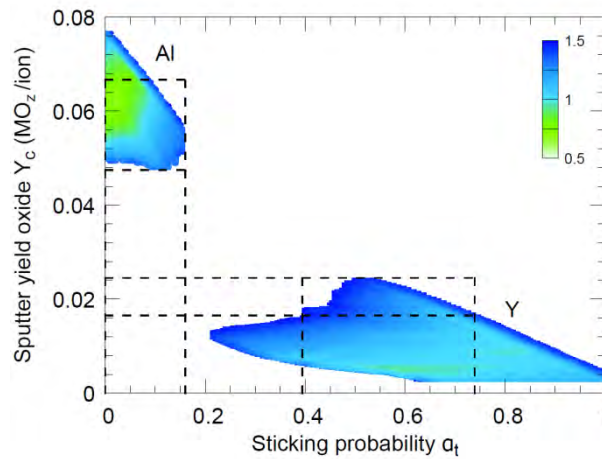
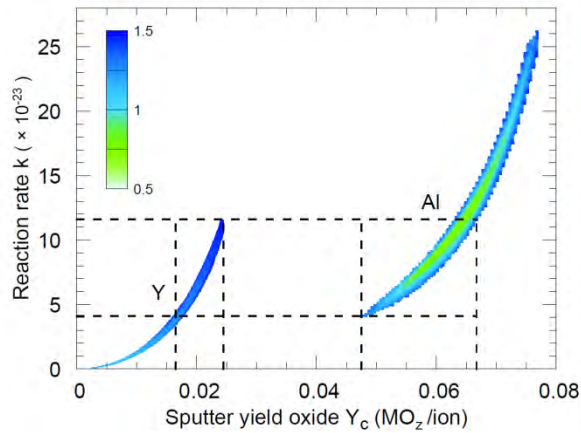
- starting point (**Start**) → found by (slightly) modified version
- step size (Δx , Δy)
- parameter boundaries
- fit procedure + acceptance tolerance f_a (>1)
- three lists: **rejected**, **accepted** and **unfinished**

Limitation only for a connected region



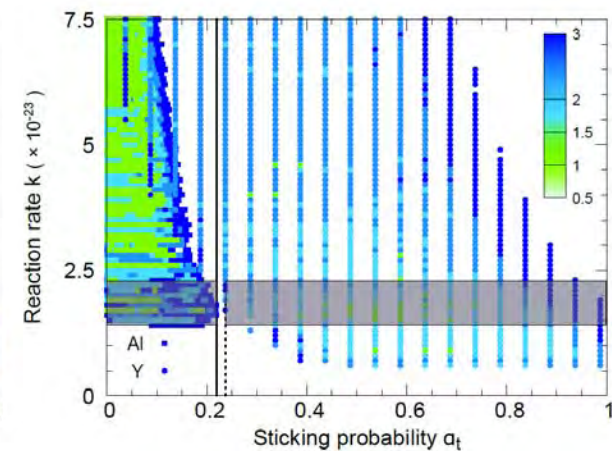
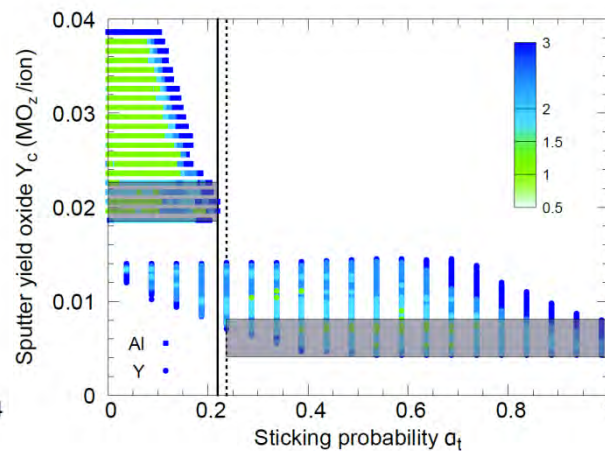
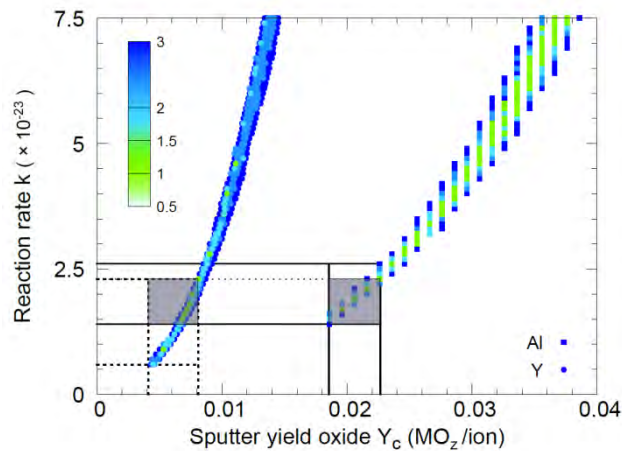
K. Strijckmans, et al., *Surf. Coat. Technol.* 206 (2012) 3666

Fitting results : correlations



↑ one-cell target
↓ multi-cell target

($f_a = 1.5$) ☹ experimental Y_c
($f_a = 3$) ☺ experimental Y_c

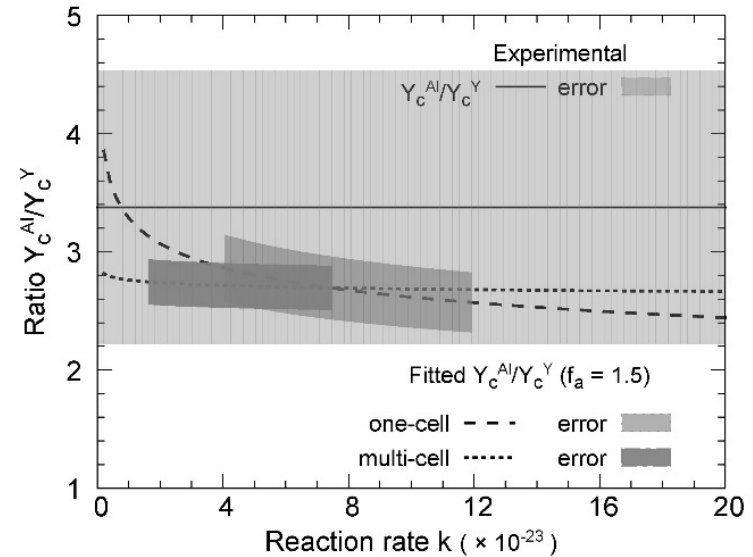
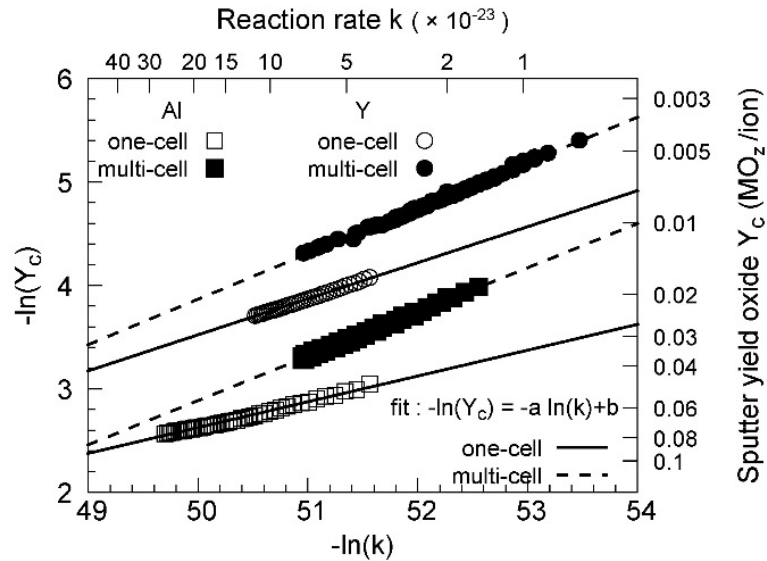


👉 ratio Y_c^{Al}/Y_c^Y is conserved

👉 $\alpha_t^{Al} < \alpha_t^Y$

under hypothesis $k^{Al} = k^Y$

Fitting results : analysis

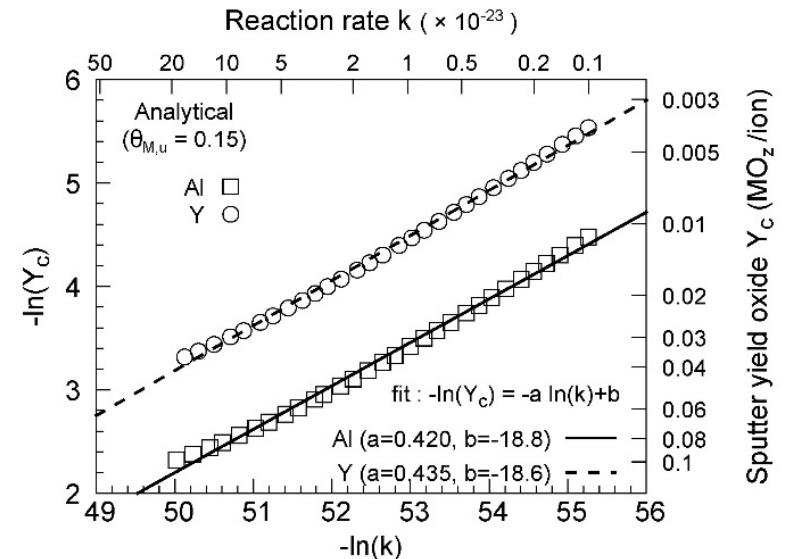


Reaction coefficient k and sputter yield oxide Y_c highly correlated

➔ Power law $Y_c = b' k^a$

👉 ratio Y_c^{Al}/Y_c^Y and correlation independent of

- reaction coefficient k
- one-cell or multi-cell target
- implantation profile



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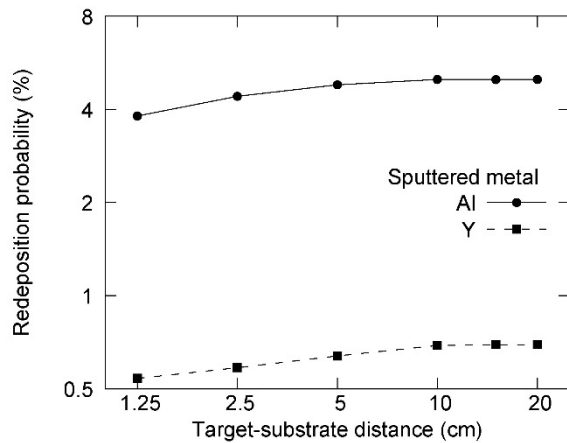
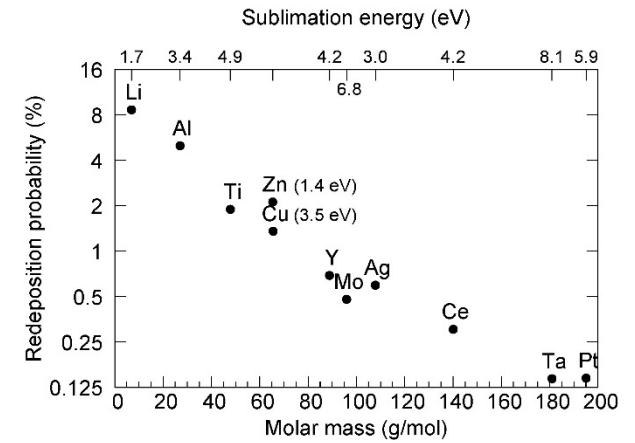
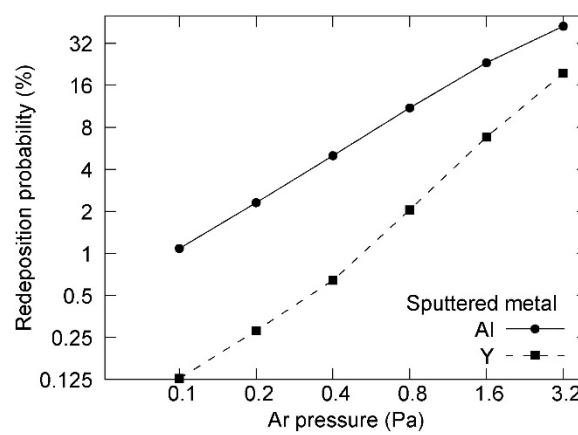
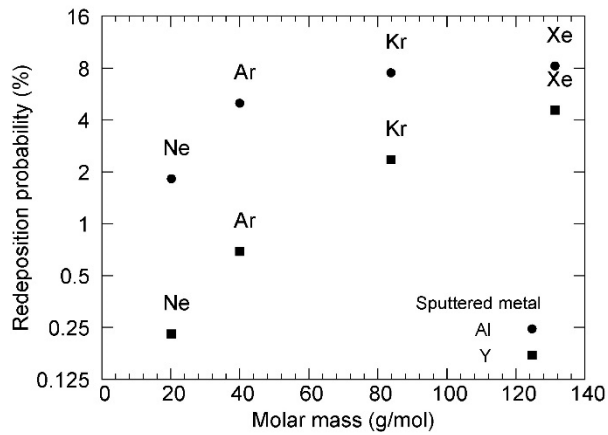
Case study : redeposition

Redeposition influenced by

1) sputter gas

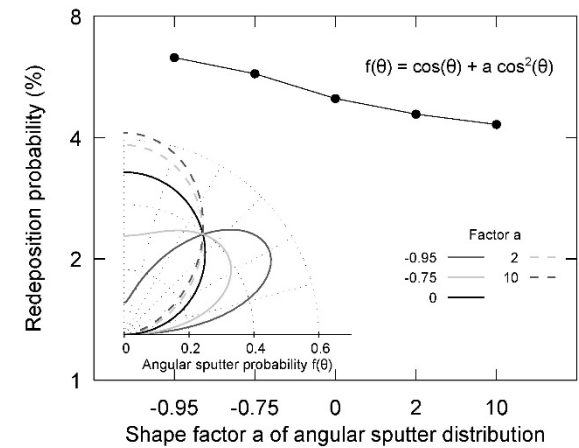
2) gas pressure

3) sputtered element

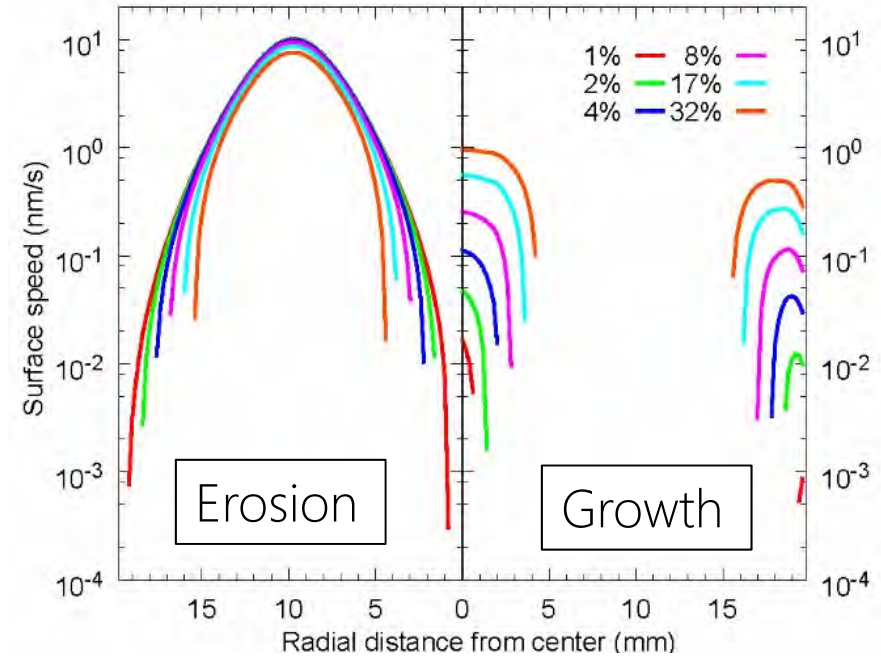
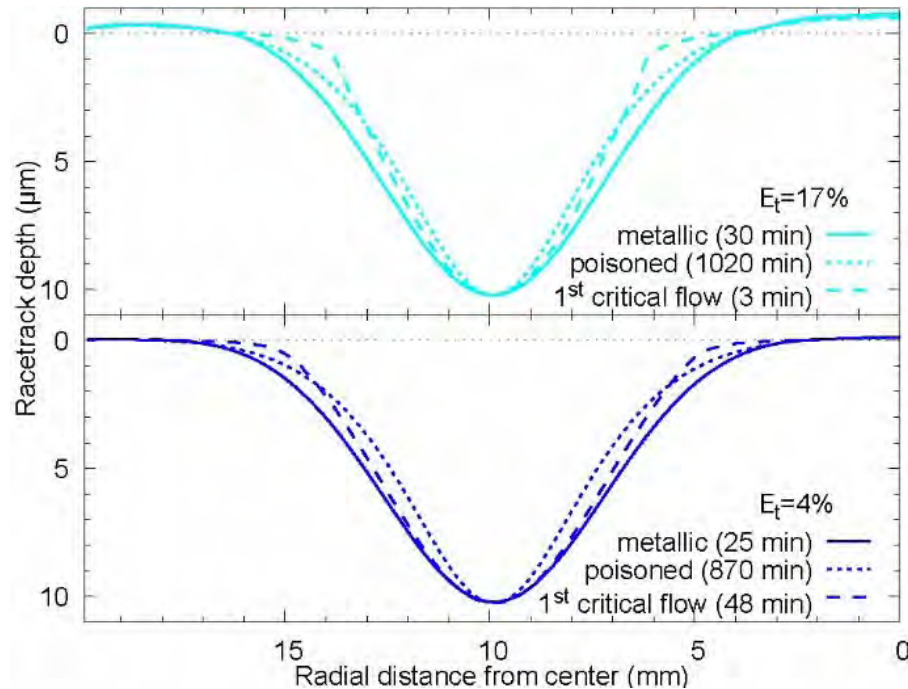


4) target-substrate distance

5) angular sputter distribution



Redeposition: Effect on racetrack profile



- Shape of racetrack depends
- redeposition fraction
 - operation point

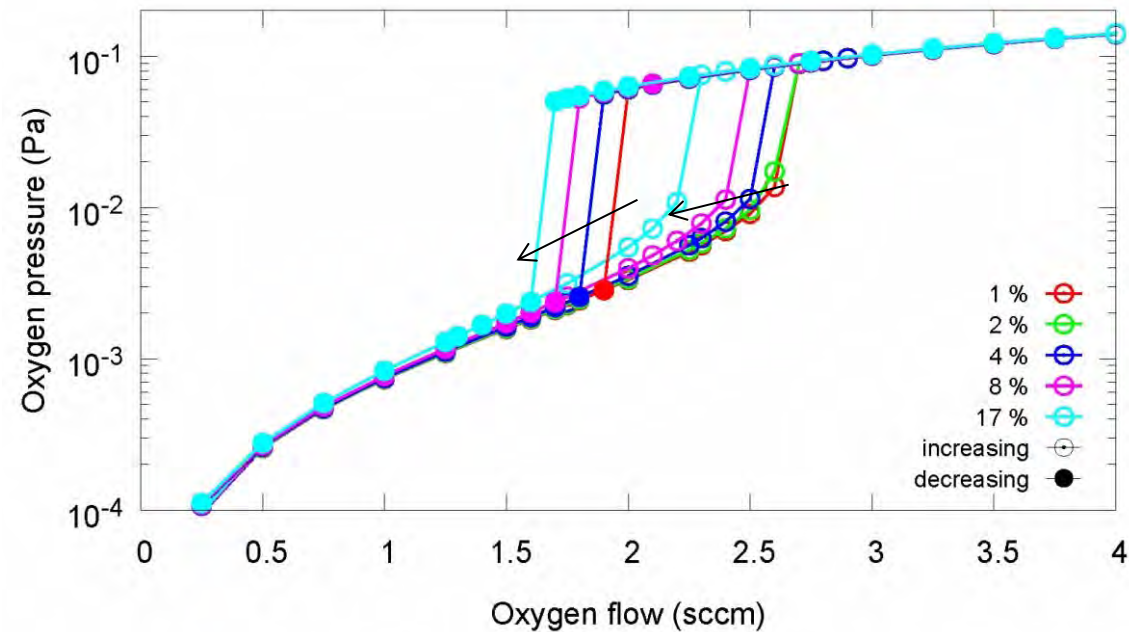
Increasing redeposition fraction decrease zone of effective erosion.

Surface speed v_s measure for racetrack depth

$$D = v_s \Delta t$$

K. Strijckmans, et al., *Appl. Surf. Sci.* 331, 185 (2015)

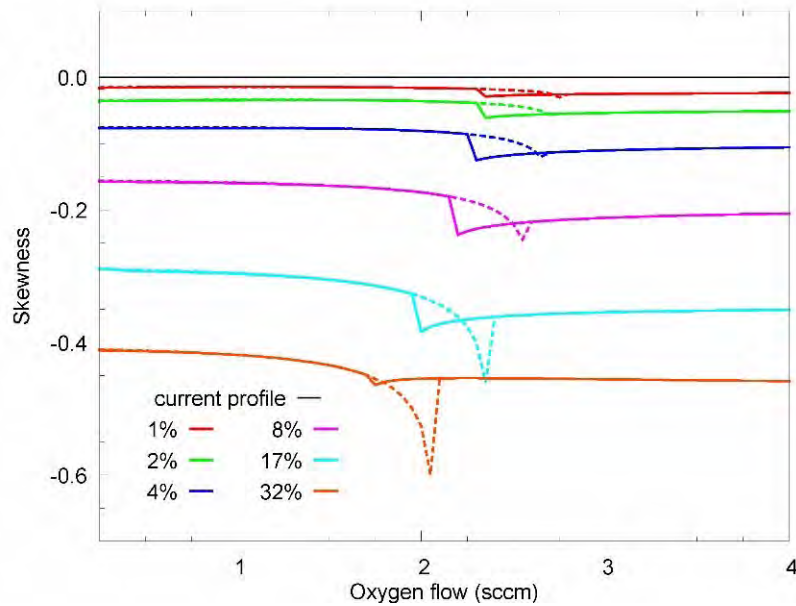
Redeposition: Effect on critical points



Shifting of both critical points to lower oxygen flows.

- 1st critical point:
the redeposition acts as a sink for sputtered metal
it reduces the metal flux towards substrate, which more easily gets oxidized
- 2nd critical point:
the redeposition slows down the erosion which give more time for reaction

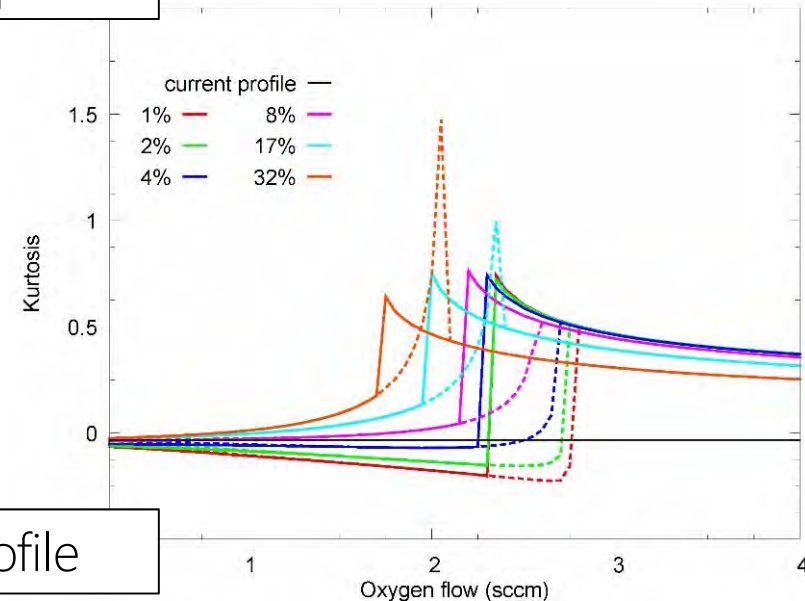
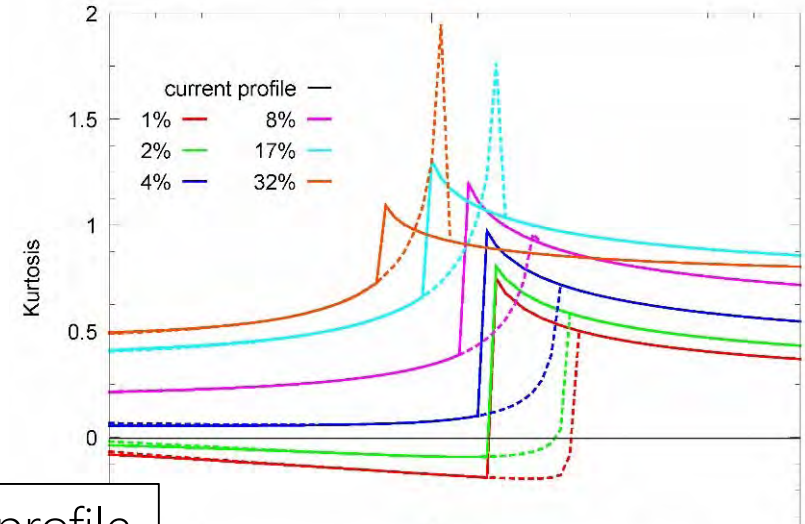
Redeposition : Shape modifications



Racetrack profile

Skewness = measure for asymmetry
 Kurtosis = measure for peakness and weight tails

racetrack profile \neq sputter profile

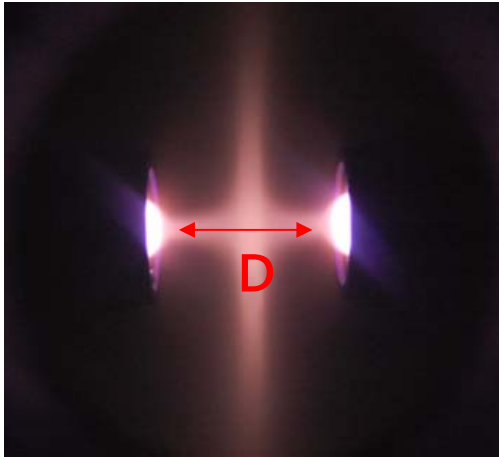


Sputter profile

Outline

- ① Introduction
- ② RSD2013 model
- ③ Finding parameters
- ④ Case studies
 - a) Redeposition
 - b) Dual target
 - c) Substrate rotation
- ⑤ Conclusion

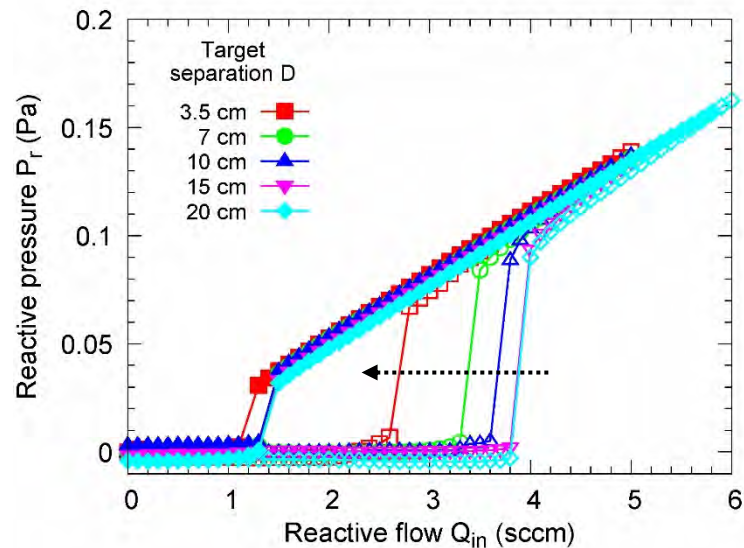
Dual target : hysteresis experiment



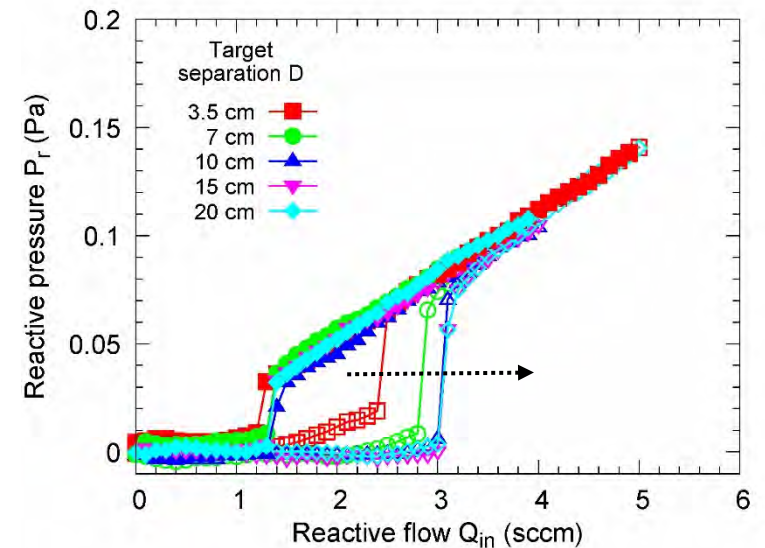
Conditions:

- cuboid chamber (50 x 50 x 50 cm)
- two facing 2" circular Al targets
- gasses Ar (0.4 Pa) / O₂
- target separation **D** 3.5 to 20 cm
- pumping 55 Ls⁻¹
- discharge current 0.3 A

decreasing **D**

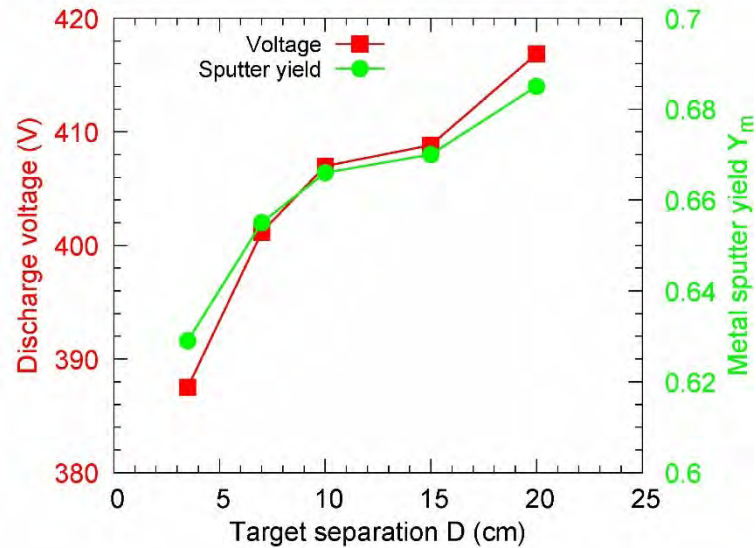


increasing **D**



Dual target : target erosion

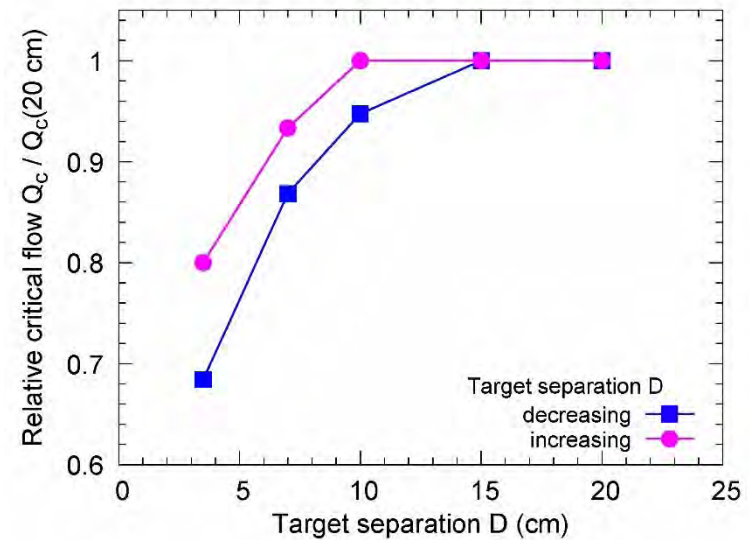
decreasing **D**



target erosion amplifies
shift 1st critical point

- target thickness ↘
- magnetic field ↗
- voltage ↘
- sputter yield ↘

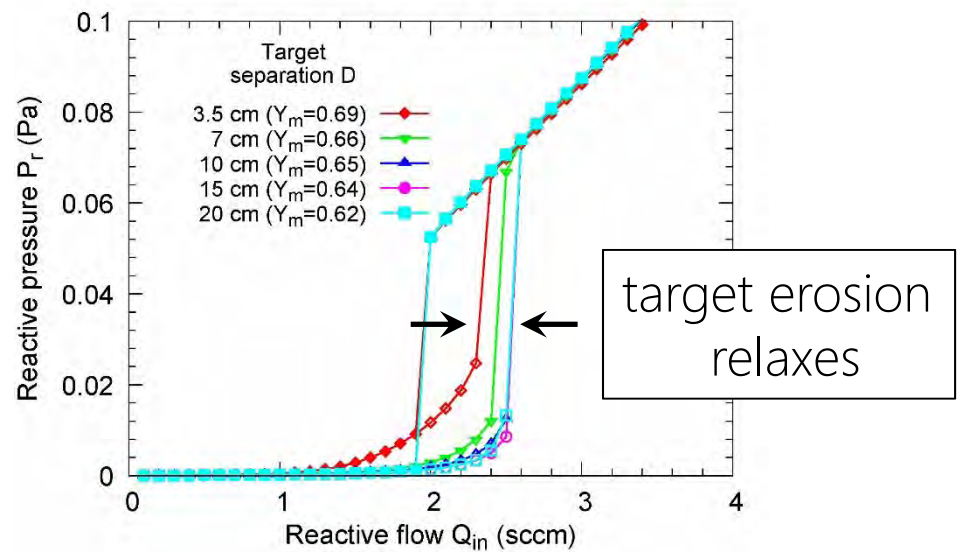
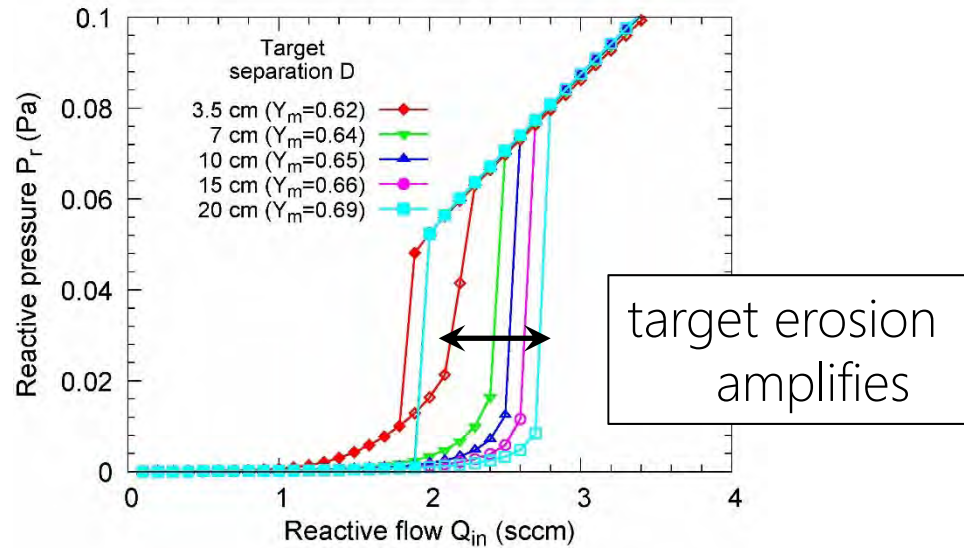
in/decreasing **D**



decreasing **D** ➤ erosion amplifies
increasing **D** ➤ erosion relaxes

1st critical point shifts ↘

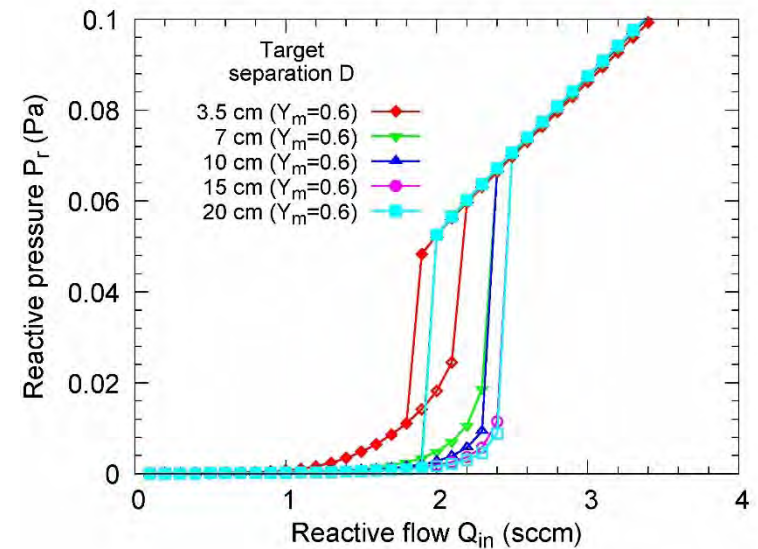
Dual target : RSD simulation



Conditions:

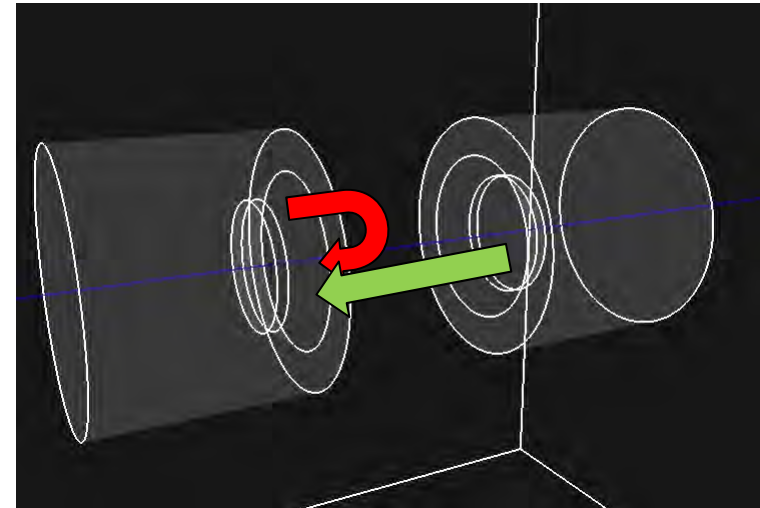
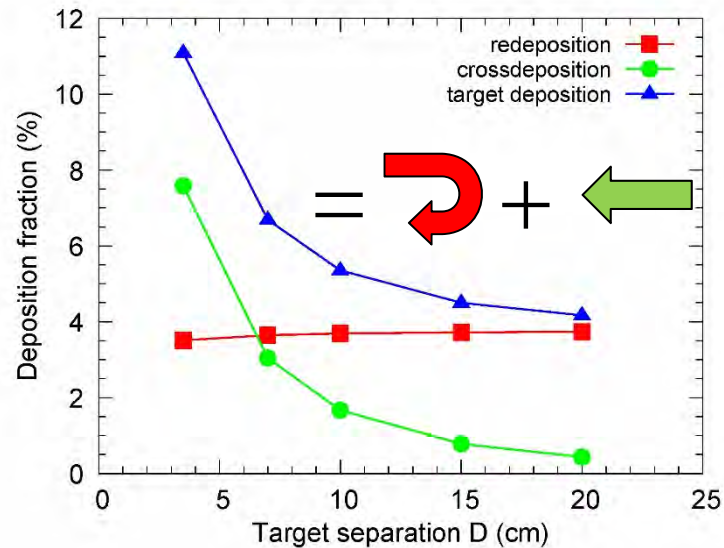
- RSD2013 time solution with redeposition
- Multicell target/substrate with varied SiMTra profiles

no
target erosion



Dual target : target deposition

SiMTra configuration of dual magnetron



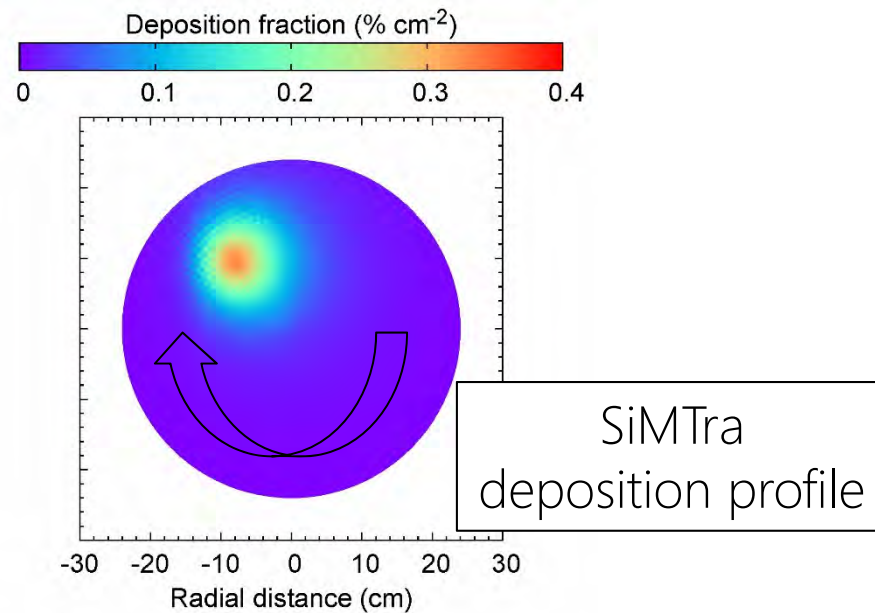
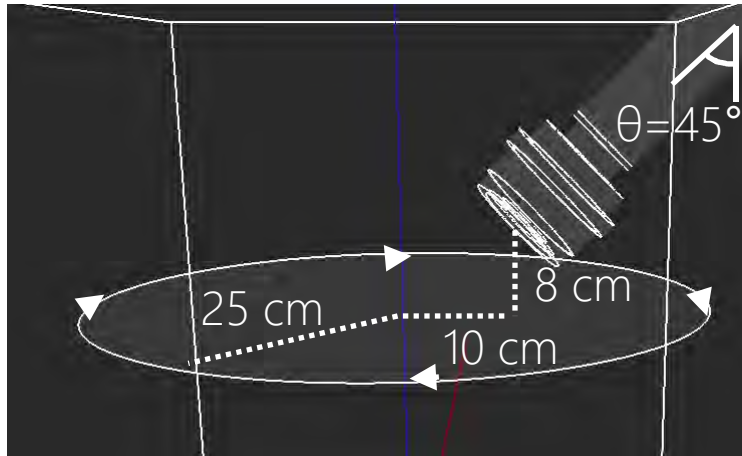
Decrease 1st critical point is substrate driven:

- Target deposition ↗ substrate deposition ↘
- Target separation ↘ effective substrate area ↘

Outline

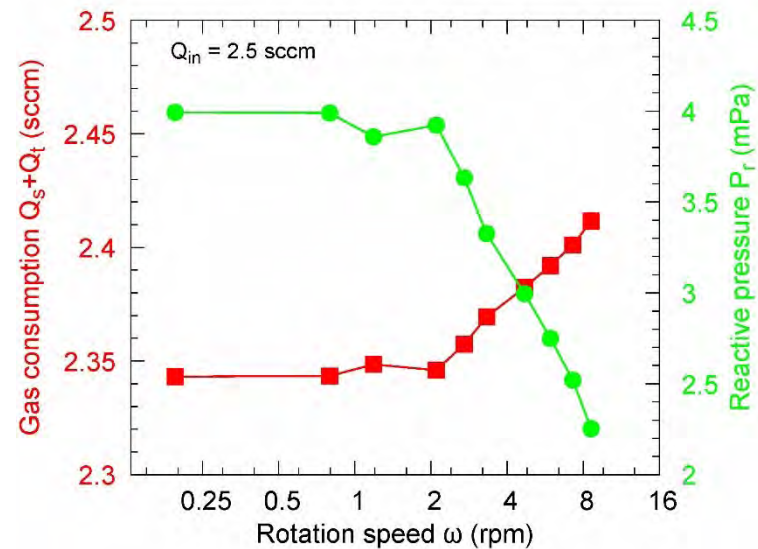
- ① Introduction
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Substrate rotation: experiment



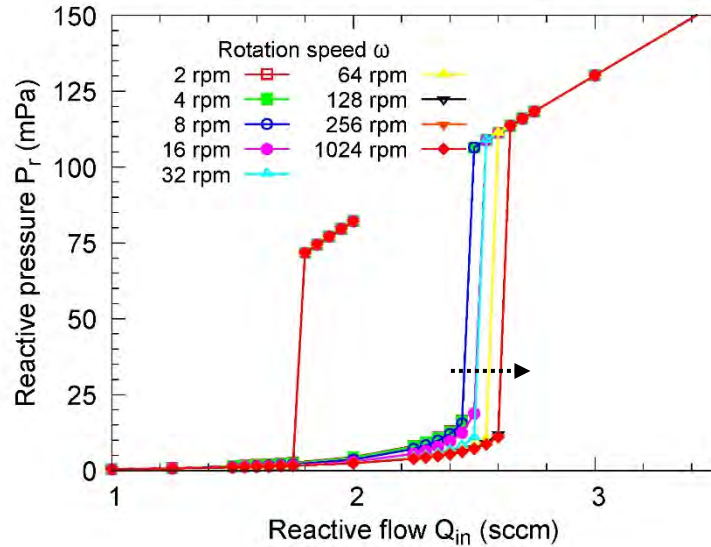
Conditions:

- cuboid chamber (50 x 50 x 50 cm)
- 2" circular Al target
- gasses Ar (0.4 Pa) / O₂ (2.5 sccm)
- rotating disk
- pumping 40 Ls⁻¹
- discharge current 0.5 A

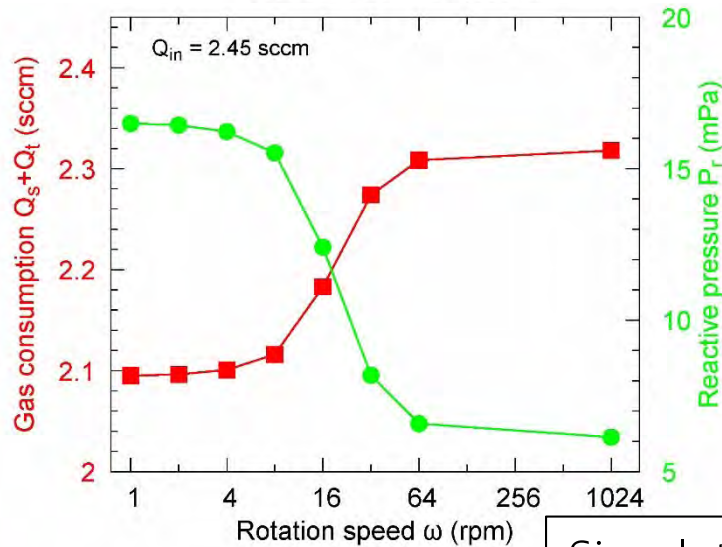


$$Q_s + Q_t = Q_{in} - P_r S$$

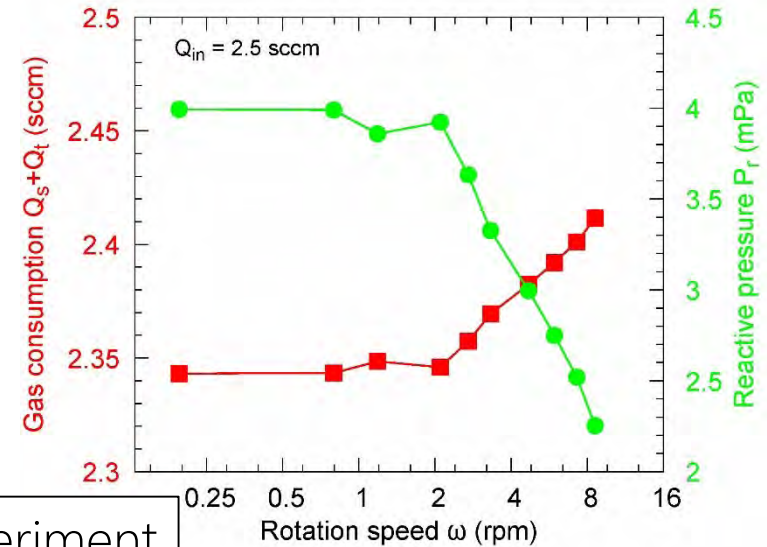
Substrate rotation: simulation



- Rotation speed on hysteresis:
- 1st critical point slightly increases
➤ experimental not resolvable
 - enhanced substrate gettering
➤ experimental resolvable
 - 2nd critical point unaffected

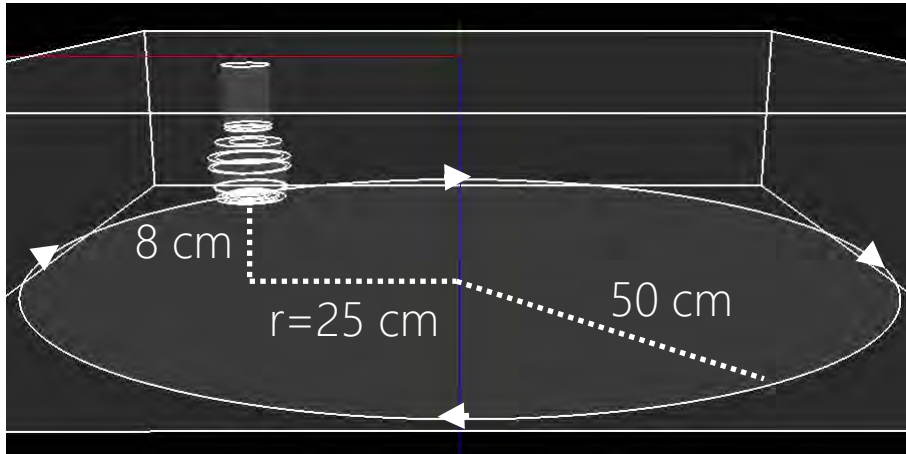


Simulation



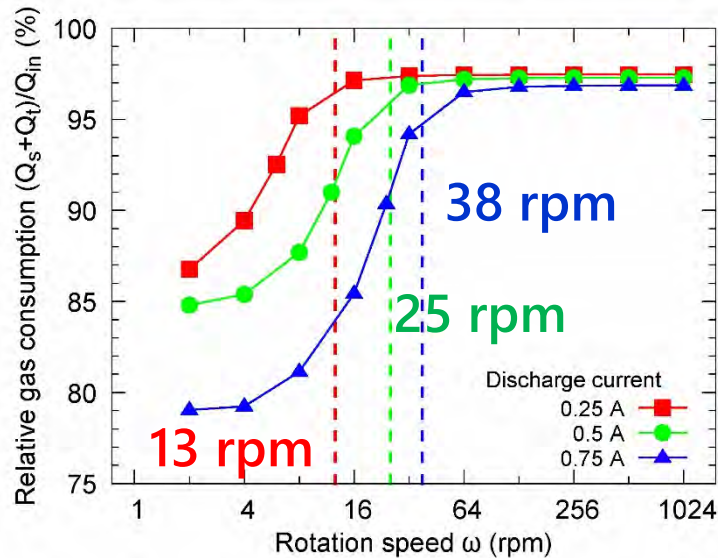
Experiment

Substrate rotation: simulation times two...

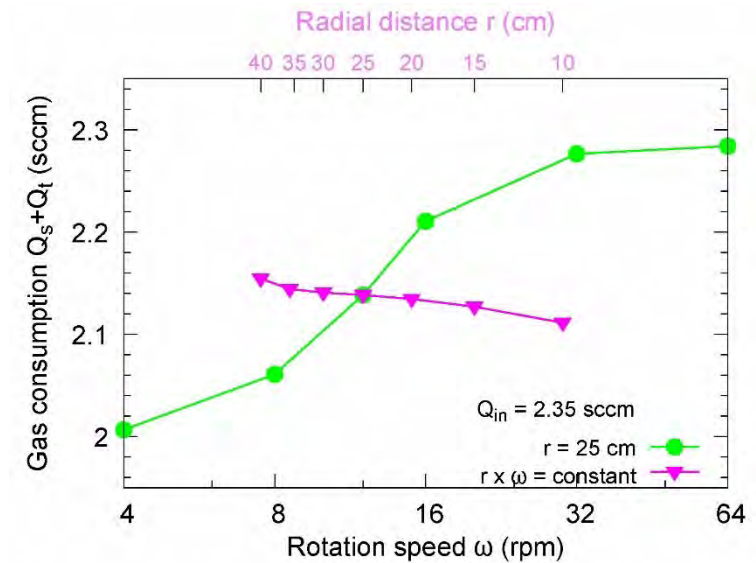


Conditions:

- chamber (100 x 100 x 25 cm)
- 2" circular Al target (0°)
- gasses Ar (0.4 Pa) / O₂
- rotating disk
- pumping 40 Ls⁻¹
- discharge current 0.5 A

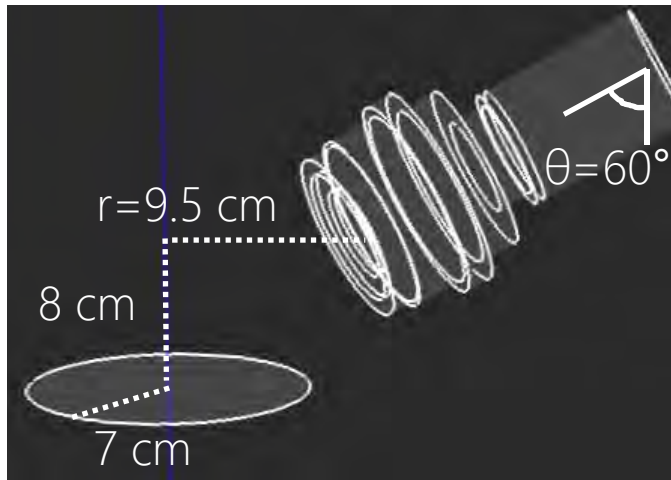


Maximum gas consumption around one monolayer per rotation



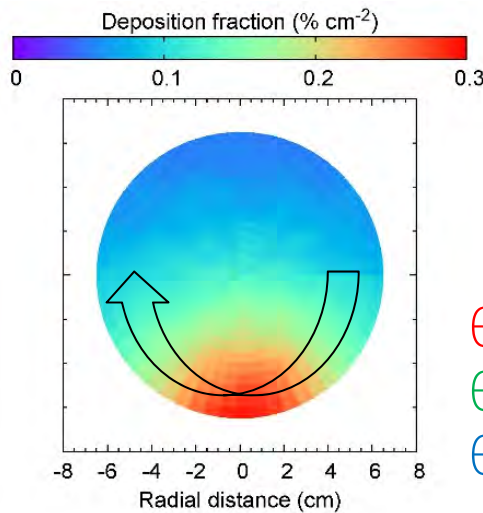
Gas consumption depends on surface speed $r \times \omega$

Substrate rotation: uniform thickness



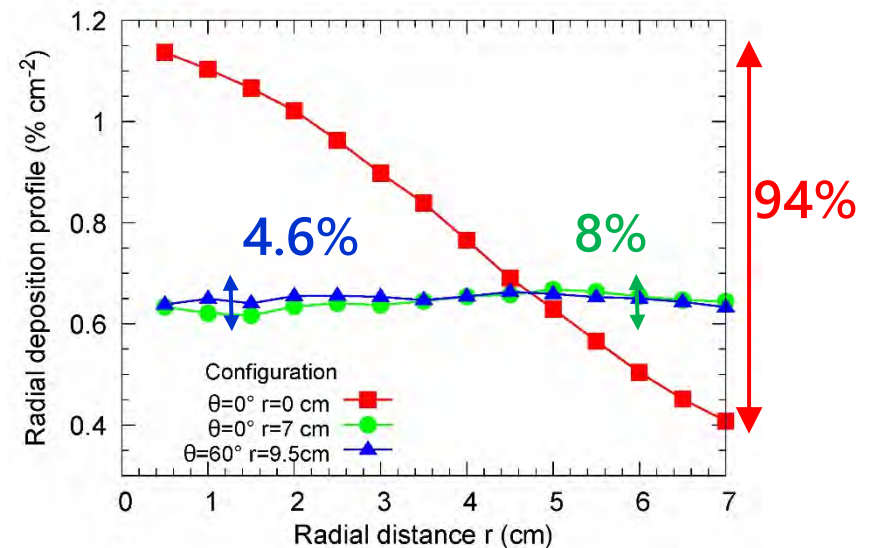
Conditions:

- cuboid chamber (50 x 50 x 50 cm)
- 2" circular Al target
- gasses Ar (0.4 Pa) / O₂
- rotating disk
- pumping 40 Ls⁻¹ and 80 Ls⁻¹
- discharge current 0.5 A and 1 A

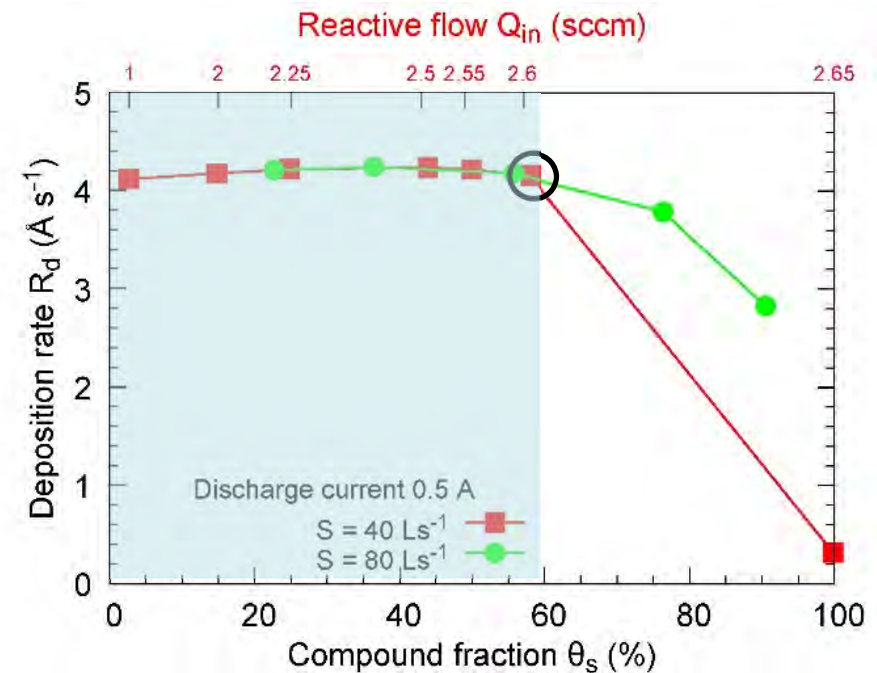
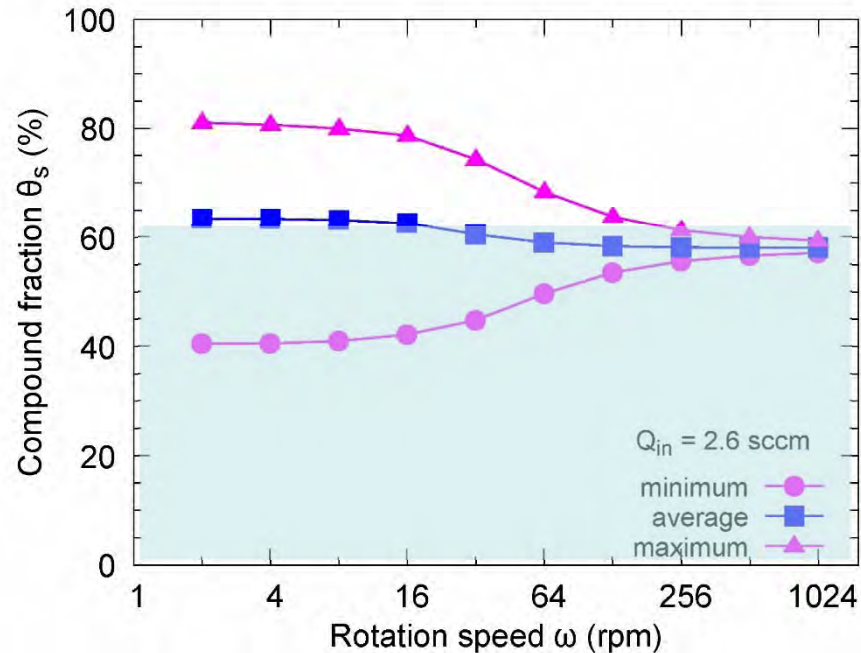


Rotation results in uniform deposition rate with efficiency

$\theta=0^\circ$	$r=0\text{cm}$	35%
$\theta=0^\circ$	$r=7\text{cm}$	21%
$\theta=60^\circ$	$r=9.5\text{cm}$	18%



Substrate rotation: tunable stoichiometry



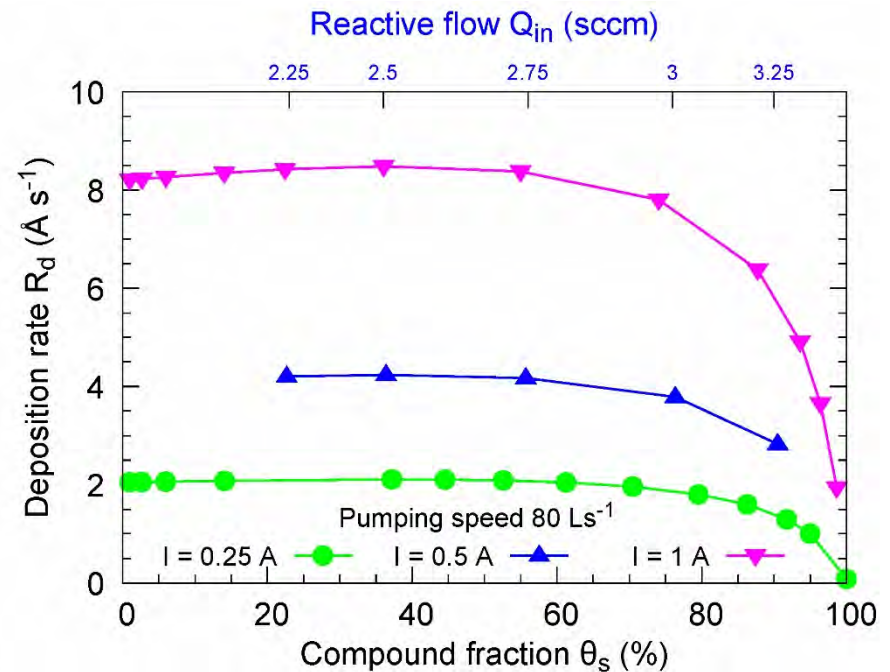
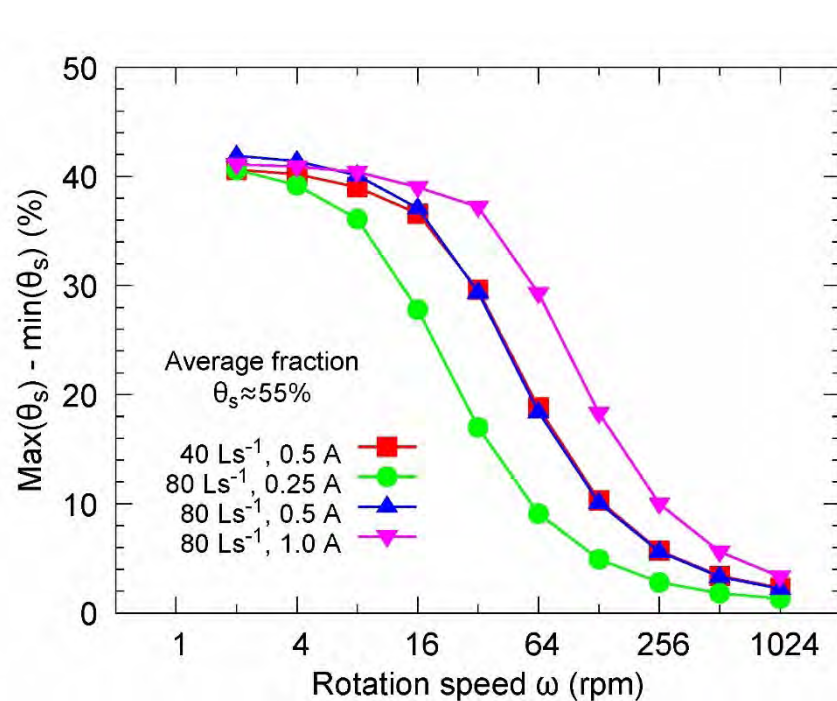
40 Ls^{-1}

- just before 1st critical point
- rotation speed ↗
- uniformity ↗
- limited fractions (< 60%)

80 Ls^{-1}

- metallic deposition rates
- pumping speed ↗
- range of fraction ↗ (< 95%)

Substrate rotation: tunable deposition rate



Spread in stoichiometry

- almost independent of pumping speed
- increases with discharge current

Deposition rate scales with discharge current

Efficiency = high pumping speed, high current and high rotation speed

Conclusion

- The RSD2013 software is a dynamic and **user-friendly** tool to simulate the **hysteresis** during reactive sputtering.
- **Ratio of oxide sputter yields** and **(k , Y_c) correlation** seems highly independent of exact RSD model choice.
- **Redeposition** influences the shape of the racetrack and the sputter profile on the target, which are no synonyms.
- The target separation in a **dual magnetron system** influences the hysteresis.
- A tunable, uniform stoichiometry and film thickness can be obtained by **substrate rotation**.

Acknowledgements

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Diederik Depla



Francis Boydens



*At DRAFT we want to become the recognized leader
in the understanding of thin film growth by
reactive magnetron sputtering
and
to enjoy research by experiments and simulations.*



Design, Research And Easibility of Ithin Films