

The effects of material formulation and manufacturing process on mechanical and thermal properties of epoxy/clay nanocomposites

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Abstract

A holistic study was conducted to investigate the combined effect of three different pre-mixing processes, namely mechanical mixing, ultrasonication and centrifugation, on mechanical and thermal properties of epoxy/clay nanocomposites reinforced with different platelet-like montmorillonite (MMT) clays (Cloisite Na⁺, Cloisite 10A, Cloisite 15 or Cloisite 93A) at clay contents of 3-10 wt%. Furthermore, the effect of combined pre-mixing processes and material formulation on clay dispersion and corresponding material properties of resulting composites was investigated using X-ray diffraction (XRD), transmission electron microscopy (TEM), scanning electron microscopy (SEM), flexural and Charpy impact tests, Rockwell hardness tests and

differential scanning calorimetry (DSC). A high level of clay agglomeration and partially intercalated/exfoliated clay structures were observed regardless of clay type and content. Epoxy/clay nanocomposites demonstrate an overall noticeable improvement of up to 10% in the glass transition temperature (T_g) compared to that of neat epoxy, which is interpreted by the inclusion of MMT clays acting as rigid fillers to restrict the chain mobility of epoxy matrices. The impact strength of epoxy/clay nanocomposites was also found to increase by up to 24% with the addition of 3 wt% Cloisite Na⁺ clays. However, their flexural strength and hardness diminished when compared to those of neat epoxy, arising from several effects including clay agglomeration, widely distributed microvoids and microcracks as well as weak interfacial bonding between clay particles and epoxy matrices, as confirmed from TEM and SEM results. Overall, it is suggested that an improved technique should be used for the combination of pre-mixing processes in order to achieve the optimal manufacturing condition of uniform clay dispersion and minimal void contents.

Keywords Mechanical mixing· Ultrasonication· Centrifugation· Montmorillonite (MMT) clays· Nanocomposites

1 Introduction

Excellent mechanical and adhesive properties of epoxy resin have played an important role in the development of epoxy/clay nanocomposites [1]. A wide range of applications in epoxy systems has attracted significant interests from researchers to develop epoxy/clay nanocomposites for automotive and aerospace applications, shipbuilding and electronic devices [2]. Such materials can also work as casting resins, adhesives and high-performance coatings for tribological applications such as

slide bearings and calendaring roller covers [3]. Notwithstanding that highly cross-linked epoxy matrices are known to exhibit high stiffness and strength, their lack of plastic deformation (*i.e.* brittle behavior) is a major drawback for many applications [4, 5].

In recent years, epoxy nanocomposites reinforced with montmorillonite (MMT) clays have drawn significant attention within the research community, especially in the aspect of the development of manufacturing techniques for polymer/clay nanocomposites [3, 6-10]. Furthermore, mechanical and thermal properties of polymer/clay nanocomposites may be significantly influenced by the material formulation associated with the wettability of clay particles and interfacial bonding between clay fillers and polymer matrices [3, 11-12]. For example, Alexandre and Dubois [3] stated that clays have been frequently used as nanofillers due to their ability to improve material performances, such as to increase strength and modulus, improve heat resistance, decrease gas permeability and exhibit excellent flame retardancy at very low clay contents with cost-competitiveness. On the other hand, Chen and Yang [6] reported that the modification of interlayer spacing of natural clays with onium ions could enhance interlayer spacing, and thus increasing the glass transition temperature of resulting nanocomposites. In addition, widespread investigations have been made to evaluate the effect of clay inclusions on tensile strength [13-16], Young's modulus [17-18], tensile creep behavior [19], flexural properties [20-22], heat resistance [23-24], barrier performance [25] and flame retardancy [26] of nanocomposites.

In epoxy/clay nanocomposite systems, physical and thermal properties are known to be influenced not only by the wettability of clay structures in term of their exfoliation but also the type of curing agent and curing temperature [27-31]. Kornmann et al. [32] studied the influence of curing agent's reactivity on resulting structures of epoxy/clay nanocomposites. It was found that curing agents with low reactivity such as aliphatic

tended to produce an exfoliated structure with better clay dispersion and higher flexural modulus of composites. Consistently, Azeez et al. [27] also noted that curing agent's reactivity affected the exfoliation structure in epoxy/clay nanocomposite systems. In contrast, Kong and Park [33] and Wang et al. [34] demonstrated that epoxy/clay nanocomposites based on a diglycidyl ether of bisphenol-A (DGEBA)/ 1, 3-phenylenediamine (PDA) system tended to produce an intercalated clay structure owing to the high reactivity of aromatic diamine curing agent. As a consequence, the synthesis of well-dispersed clay structures in epoxy nanocomposites can be prepared by controlling the curing speed of interlayer areas to be faster than that of external layer counterparts.

More critically, non-homogeneous clay dispersion and existence of voids due to air entrapment are formidable issues required to be tackled in order to successfully manufacture epoxy nanocomposites as such issues can adversely affect their resulting mechanical properties [10-11, 35]. The pre-mixing becomes an importance step to disperse clay fillers into polymer matrices. Shear mixing and ultrasonication processes are currently the common techniques that widely used on particle/filler dispersion process [6-7, 10-11, 13-14, 15, 27-29, 30, 36-37, 38]. In the shear mixing process, fluid shear force and impacts among clay-clay particles as well as impeller-clay particles owing to agitation of impeller break up clay aggregates into fine particles [39]. The illustration of fluid flow in shear mixing can be seen in Fig. 1.a. This physical process can suspend and disperse clay particles to make a slurry. According to Atiemo-Obeng et al. [39], there are six key points to achieve good wettability of solid-liquid mixing, which are operation methods, phases, properties of solid and liquid phases, unit operation, vessel geometry and mixing parameters. Shear mixing technique have been employed to obtain homogenous clay dispersion or clay wettability [13, 28, 37] and good interfacial bonding between clay nanofillers and

polymer matrices [40]. Moreover, Gupta et al. [38] reported that exfoliated structures resulted in increased tensile modulus, which was achieved by both mechanical mixing and shear mixing techniques. However, the presence of weak interfacial bonding appeared to decrease both tensile and compressive strengths. Additionally, Park et al. [41] found that the use of high shear forces during mixing could break up clay agglomerates and separate layered clay platelets into exfoliated structures, which, however, was at the expense of reduced tensile strength and modulus due to air entrapment. Yasmin et al. [42] showed that much higher shear mixing speeds could simultaneously produce foam mixtures with the increased viscosity. Both aspects were detrimental to mechanical properties of nanocomposites. Accordingly, it is evident that both shear mixing and mechanical mixing can potentially be used as an alternative technique to break up clay aggregates in order to achieve homogenous clay dispersion.

On the other hand, the effect of ultrasonication technique is also clearly demonstrated on clay dispersion in polymer matrices, which has been proven to be highly effective for the dispersion of fine fillers within polymer matrices [21, 42]. In the sonication process, when sound waves propagate into the liquid, ultrasound cavities like bubbles take place (Fig. 1b) [43, 44]. The bubbles motion can produce high pressure in the solution that is inserted between particles and separate or increase layer interplanar distances. Ultrasonic parameters impacting ultrasonics cavities are frequency, intensity, temperature, solvent viscosity, vapour pressure, surface tension, bubble gases and external pressure [43]. In line with this, current results [45] indicated that sonication time and energy played an important role in reducing the size of clay clusters. Moreover, it was highlighted that high-quality clay dispersion could be obtained through the combination of highest power intensity (i.e. 100%) and shorter sonication time (i.e. less than 20 minutes) [46-48]. On the other hand, Dean et

al. [49] investigated the effect of ultrasonication technique on mechanical and thermal properties of epoxy/clay nanocomposites. It was found that clay wettability was improved in the sonicated samples compared to shear mixed counterparts. Moreover, flexural strength of both sonicated nanocomposite samples at the clay content of 1 wt% was increased to over 100% and 27% as opposed to those of neat epoxy and shear mixed nanocomposite counterparts, respectively. Meanwhile, glass transition and thermal degradation characteristics of resulting nanocomposite materials via ultrasonication appeared to be quite similar to those of neat epoxy and shear-mixed nanocomposites with increasing the clay content.

Alternatively, centrifugal technique can be used to disperse clay particles into polymer matrices [8, 50-52]. Generally, centrifugal process is employed to separate mixtures. Rotational movement with a high speed of the centrifugal tube produces a centrifugal force leading to the particle movement (Fig. 1.c). Processing parameters such as rotor speed, duration of rotation and temperature process can highly influence the centrifugal process [53]. As mentioned by Saber-Samandari et al. [50], rotor speed is regarded as a quite influential parameter for resulting material properties of epoxy/clay nanocomposites. According to their results, the highest elastic modulus of epoxy/clay nanocomposites was found at the lowest rotor speed of 3000 rpm with a mix of intercalated/exfoliated clay structures. Using the centrifugal mixing, Kabakov et al. [51] revealed that only intercalated clay structures occurred in size of 500-1000 nm according to the SEM observation. High shear force has also been mentioned to be effective in separating multi-layers of clay platelets. Further investigation was undertaken by Agubra et al. [52] to manufacture epoxy/E-glass fibre/clay nanocomposites, using combined magnetic and centrifugal mixing, and subsequent roll milling. Such a combined mixing approach gave rise to exfoliated clay structures within epoxy matrices as evidenced by TEM results. Moreover, Ianchis et al. [8] used

centrifugal vacuum mixing to reduce the amount of air entrapment, arising from roll mill mixing. A higher storage modulus and stiffness were obtained for prepared nanocomposites, along with an increase of up to 40% for T_g when compared to those of neat epoxy. Such improvements could be ascribed to the removal of air bubbles.

In light of the results mentioned so far, current study aims to examine the effect of material formulation and combined pre-mixing methods (i.e. mechanical mixing, ultrasonication and centrifugation) on mechanical and thermal properties of epoxy/clay nanocomposites using a solution casting method. Two different types of MMT clay fillers based on pristine and organomodified clays with different organic modifiers, various interlayer spacing values and clay contents were selected to evaluate the morphological structure and mechanical and thermal properties of epoxy/clay nanocomposites. It is anticipated to eventually provide useful guidance on the further optimisation of material formulation and manufacturing process for epoxy/clay nanocomposites.

2 Experiment procedures

2.1 Materials

Diglycidyl ether of bisphenol-A (DGEBA) resin and isophronediamine (IPDA) curing agent (L13 kit) were supplied by Adhesive Engineering Pty, NSW Australia with a recommended mix ratio of 100:22.87. Two different types of MMT clay fillers, denoted as unmodified clays (Cloisite Na⁺) and organomodified clays (Cloisite 10A, Cloisite 15 and Cloisite 93A) were purchased from BYK-Chemie GmbH, Germany with organic modifiers, interlayer spacings (d_{001}) and cation exchange capacities (CEC) listed in Table 1.

2.2 Manufacture of epoxy/clay nanocomposites

Manufacture of epoxy/clay nanocomposites was started by pre-heating DGEBA resin (100 gram) at 80 °C in order to reduce the epoxy viscosity. Desired amounts of clay particles in range from 3 to 10 wt% were poured slowly and hand mixed into epoxy with a glass rod until all clay immersed. Clay fillers were pre-dried under vacuum at 80 °C for 24 h. Following this, DGEBA/clay mixture underwent shear mixing with a rotor speed of 510 rpm for 1 h using IKA RW20 mixer attached to a high shear impeller to reduce clay agglomeration. Further, the mixture was poured into a polyethylene sealed bag. This was followed by the ultrasonication (Model ELMA Ti-H-5) at 25 kHz with a sweep mode and 100% power intensity at 50 °C for 45 min for finer clay dispersion. After poured into a centrifugal tube, the mixture was then placed in a centrifugal machine (Eppendorf centrifuge 5810R) with a rotor speed of 4000 rpm for 30 min at 40 °C to remove entrapped air bubbles. IPDA curing agent was added to epoxy/clay mixture (previously allowed to cool down to ambient temperature) using thorough hand mixing for 5 min. It was followed by the ultrasonication that was performed at 25 kHz with a degas mode and 100% power intensity for 15 min at ambient temperature. The mixed slurry was subsequently poured into mold cavities for the preparation of mechanical testing samples. Finally, all prepared nanocomposite samples were cured at ambient temperature for 3 days. The entire preparation procedure is illustrated in Fig. 2.

2.3 Material testing and characterisation

To investigate the effect of manufacturing process and clay types on mechanical properties, flexural tests were carried out based on a three-point bending rig on a universal testing machine (Lloyds EZ50) according to ASTM D790. The samples in

size of $127 \times 12.7 \times 3.2$ mm were supported using a span of 51 mm and loaded with a crosshead speed of 31.37 mm/min. Charpy impact tests (V notch) were carried out based on ASTM D6110 with a pendulum arm of 225 mm, pendulum energy of 0.5 J and a span of 101.6 mm using a Zwick D-7900 impact tester. In addition, Rockwell hardness scale E (HRE) tests were conducted in accordance with ASTM D765 with an indenter of 3.175 mm and load of 980.7 N on an Avery 6470 Rockwell hardness-testing machine.

X-ray diffraction (XRD) patterns were obtained to investigate intercalated clay structures within epoxy/clay nanocomposites at a diffraction angle 2θ from 2 to 10° on a PANalytical EMPYREAN/PIXcel^{3D} X-ray diffractometer using $\text{CuK}\alpha$ radiation (wave length $\lambda = 0.1541$ nm) at 40 kV and 40 mA (scanning step time of 296 second/step and step size at 0.02°). A JEOL 2100 transmission electron microscope (TEM) was used to study clay morphological structures within epoxy matrices at an accelerating voltage of 120 kV. The TEM samples (average thickness ~ 100 nm) were cut with a glass knife using a Leica EM UC6 ultramicrotome with sliced samples collected on 300 mesh copper grids.

Fracture surfaces of flexural testing samples (coated with a 5 nm layer of platinum to avoid charging effects) were investigated by scanning electron microscopy (SEM) using a Zeiss Neon 40EsB at an accelerating voltage of 15 kV. Differential scanning calorimetry (DSC) was performed on a Perkin-Elmer DSC6000 thermal analyser. 10-15 mg samples were heated from -80 to 100 $^\circ\text{C}$ at a heating/cooling rate of 10 $^\circ\text{C}/\text{min}$ under a nitrogen flow of 20 mL/min.

3 Result and discussion

3.1 XRD analysis

XRD patterns of platelet-like clays and their corresponding nanocomposites are presented in Fig. 3. Calculated *d*-spacing values of as-received organoclays and epoxy nanocomposites with different clay types and contents are shown in Table 2. Overall, the addition of organoclays into epoxy matrices was found to increase *d*-spacing values for three types of clays, namely Cloisite Na⁺, Cloisite 10A and Cloisite 93A. However, the *d*-spacing value of epoxy/Cloisite 15 clay nanocomposites remained at a similar level to that of as-received Cloisite 15. It has been shown that epoxy nanocomposites reinforced with Cloisite Na⁺, Cloisite 10A, Cloisite 15 and Cloisite 93A exhibit increases in interlayer spacing values of approximately 33, 44, 6 and 40%, respectively. This implies that clay intercalation at different levels took place during the manufacture of epoxy/clay nanocomposites owing to the effect of cation exchange capacity (CEC) for different clay types and curing agents [32, 33, 55]. More interestingly, the *d*-spacing values of epoxy nanocomposites reinforced with organomodified clays (i.e. Cloisite 15, Cloisite 10A and Cloisite 93A) have similar values close to 3.5 nm. It is worth noting that DGEBA molecules can only be swollen into clay interlayer areas in order to increase the *d*-spacing values.

Based on XRD results depicted in Fig 3, XRD peaks of epoxy/clay nanocomposites are shifted to lower diffraction angles with a clear sign of intercalated clay structures. From the manufacturing point of view in the combination of three different pre-mixing method, this phenomenon might occur at the processing stage of mechanical mixing, during which large clay aggregates are broken up into fine particles and DGEBA molecules are diffused into interlayer areas of clay platelets. In the secondary ultrasonication with the presence of DGEBA infusion, ultrasound waves

could propagate epoxy liquids to cause their high-pressure movement into multilayers of clay platelets, thus further enhancing the separation of platelet layers. The results of intercalated clay structures can arise from the influence of non-optimum processing parameters, namely mechanical mixing parameters (i.e. mixing speed, time and temperature) and ultrasonic parameters (i.e. frequency, power intensity, temperature and time). The selection of those parameters may not be appropriate to substantially break up clay platelets and facilitate the penetration into clay interlayers. The other point worth mentioning is that molecular structure and chemical properties of epoxy resin also plays an essential part in final morphological structures of resulting nanocomposites, as previously stated by Becker et al. [55]. The length of epoxy molecules and number of molecular chains are limited, which makes exfoliated structures difficult to achieve when epoxy molecules are penetrated into interlayer areas of clay platelets. Moreover, the mobility of epoxy molecules into clay galleries, as well as the inter- and extra-gallery reaction of epoxy should also be taken into consideration. According to Akbari and Bagheri [56], alkylammonium modified clay chains are able to occupy the gaps in interlayer areas, which decreases the diffusion of epoxy molecules, thus resulting in a limited increase of d -spacing values. On the other hand, hydrophilic properties of pristine MMT clays (i.e. Cloisite Na⁺) may have contributed to a relatively small increase in d -spacing value up to only 1.4 nm for nanocomposites. Conversely, organoclays modified by organophilic and alkylammonium cations tend to possess essentially hydrophobic clay surfaces with expanded interlayer areas, which can facilitate the diffusion of epoxy molecules [6, 24, 57].

3.2 TEM morphological characterisation

As a supplementary technique to XRD analysis for the investigation of clay dispersion, TEM was carried out on epoxy/Cloisite 93A nanocomposites with various clay contents, as illustrated in Fig. 4. It is evident from these TEM micrographs that combining three different pre-mixing processes tend to produce non-uniform clay dispersion, as evidenced by the presence of clay aggregates with skewed nanoclay layers. The addition of 3 wt% clays resulted in a mix of morphological structures, comprising agglomerated and partially intercalated/exfoliated clay structures (Fig. 4(a)). Increasing the clay content demonstrated a high tendency for the provision of intercalated structures rather than exfoliated structures as depicted in high magnification TEM results, Figs. 4(b), (d), (f) and (h). It clearly shows the presence of intercalated structures with an interlayer spacing shifted from 2.55 nm to approximately 3.6 nm, Table 2. Moreover, exfoliated clay structures with single clay platelets can only be evidently seen in Figs. 4(b), (d) and (f). On the other hand, increasing the clay content from 3 to 10 wt% caused silicate layers to be clumped together, as indicated by the presence of clay aggregates with typical sizes ranging from 1 to 3 μm .

The above-mentioned fact implies that the combination of three different pre-mixing with those processing parameters could not produce desirable epoxy/clay nanocomposites with better clay wettability. The processing parameters of mechanical mixing and ultrasonication selected in this study may lack the effective manufacturing of nanocomposites to break up clay aggregates and disperse fine clay particles uniformly in epoxy matrices. The other plausible reason for clay agglomeration can be attributed to applied centrifugal forces in the third stage of pre-mixing process, which allows the silicate layers of clay particles to stick together, thus leading to the reduced functionality of clays as effective nanofillers. Such a phenomenon is in good

accordance with previous results obtained from Saber-Samandari et al. [50] by investigating the effect of centrifugal mixing at high rotor speeds on clay agglomeration. Consequently, optimum processing condition at different clay types and contents, as well as compatibility of physical and chemical properties of used coupling agents are the key to successfully manufacturing epoxy/clay nanocomposites with better clay wettability and excellent mechanical properties.

3.3 SEM analysis

The fracture surfaces of neat epoxy and epoxy/clay nanocomposites investigated by SEM are presented in SEM micrographs in Fig. 5 and Fig. 6. Neat epoxy samples exhibits typical smooth surfaces after brittle fracture with so-called “stream” marks adjacent to initial cracks (Fig. 5(a)). On the other hand, epoxy/clay nanocomposites possess significantly different morphology compared to those of neat epoxy with a clear sign of rougher fracture surfaces (Figs. 5(b)-(i)). Moreover, it can also be seen that increasing the clay content in nanocomposites further promotes the surface roughness level, signifying more brittle feature with embedded rigid clays.

On the other hand, the presence of clay aggregates with the size of approximately 2 to 5 μm , as seen in Figs. 5(b)-(i), indicates the pull-out of clay particles in fracture mechanism owing to the weak interfacial bonding between clay aggregates and epoxy matrices. Such observation is believed to further deteriorate mechanical properties of epoxy/clay nanocomposites. Moreover, increasing the clay content to 10 wt% induces serious clay clumps and agglomeration according to previous TEM results in Fig. 4. In general, nanofiller content above 5 wt% may offer less success in producing highly dispersed nanofillers within nanocomposite systems. The other possible reason for clay agglomeration can be due to inappropriate selection of processing parameters to produce sufficient dissipation energy for particle separation. In order to achieve good

clay wettability, it is essential to use high shear forces to overcome Van der Waals interactions among clay layers so that epoxy molecules can be easily diffused into clay interlayer areas and achieve the expansion of interlayer spacing, further resulting in well dispersed clay fillers within polymer matrices [38].

On the other hand, Figs. 6(a)-(h) demonstrate a large number of microvoids and microcracks for epoxy nanocomposites reinforced with organomodified and pristine clay types, namely Cloisite 10A, Cloisite 15, Cloisite 93A and Cloisite Na⁺. The crack propagation was initiated close to microvoids and clay aggregates due to weak epoxy network junctions around void edges. Therefore, the existence of microvoids can be attributed to several effects that may have taken place in aforementioned three different pre-mixing processes. During the shear mixing process, foamy and viscous mixed materials can be produced, which are hard to reduce in subsequent ultrasonication and centrifugal processes. Inappropriate mixing with a fast rotor speed can yield air entrapment or foamy mixture, built-up heat and poor clay dispersion, as illustrated from SEM results in Figs. 5 and 6. Despite the positive effect of centrifugal technique on bubble reduction [50], it may also break down large bubbles into microsized bubbles [58] as confirmed in Fig. 6 in this study. The use of inappropriate rotor speed makes it less effective to separate fillers/particles and reduce air bubbles in epoxy/clay mixtures. When the combination of three different pre-mixing processes, consisting of mechanical mixing, ultrasonication and centrifugal mixing, are directly employed in this study, it is manifested that clay wettability into polymer matrices fails to be substantially enhanced without the optimisation of material formulation and processing conditions according to obtained morphological structures in TEM and SEM results.

3.4 Mechanical properties

3.4.1 Flexural properties

Flexural testing results for epoxy/clay nanocomposites with different clay types and contents are demonstrated in Fig. 7. It is noted that epoxy/clay nanocomposites possess lower flexural strength than neat epoxy. Flexural strengths of epoxy nanocomposites reinforced with organomodified clays (i.e. Cloisite 10A, Cloisite 15 and Cloisite 93A) decreased with increasing the clay content. Quite differently, epoxy/ Cloisite Na⁺ nanocomposites have an almost constant flexural strength at approximately 62 MPa at the clay contents of 3-10 wt% (Fig. 7(b)). Overall, epoxy/Cloisite 15 nanocomposites have achieved the maximum flexural strength with 3 wt% clay inclusions, which, however, is still 12 % lower than that of neat epoxy.

On the other hand, the addition of pristine and organomodified clays into epoxy matrices could enhance flexural moduli as well. Flexural moduli of nanocomposites with the addition of 3 wt% Cloisite 15 and Cloisite Na⁺ were significantly improved by 21 and 17%, respectively, as opposed to that of neat epoxy, Fig. 7(a). Nevertheless, further increase in the clay content up to 10 wt% induces the retention of flexural moduli for epoxy/ Cloisite Na⁺ nanocomposites at approximately 3.2 GPa. Conversely, flexural moduli of epoxy/Cloisite 15 nanocomposites demonstrate a declining trend above the clay content of 3 wt%. Meanwhile, epoxy nanocomposites reinforced with Cloisite 10A and Cloisite 93A have a moderate increase of flexural moduli up to 3 wt% clay inclusions, which is followed by a slight reduction from 3 to 8 wt% in the clay content when compared with that of neat epoxy. Thus, it can be inferred that the addition of 3 wt% clays is the optimum level of filler contents for both pristine and organomodified clays.

The reduction in flexural strength and flexural moduli for all nanocomposites can be associated with many factors in material processing and morphology including clay

agglomeration and poor clay wettability [28], as well as weak interfacial bonding between clay particles and epoxy matrices. In particular, a high level of clay agglomeration can hinder epoxy network junction, which adversely influences the rigidity of nanocomposites. Low clay dispersibility and poor interfacial interaction inevitably lead to the less enhancement of flexural moduli and diminished flexural strengths for epoxy/clay nanocomposites. Furthermore, the presence of microvoids detected from TEM and SEM results also means typical defects to initiate the crack propagation around void edges, further worsening flexural properties of epoxy/clay nanocomposites.

3.4.2 Impact properties

The effect of clay type and content on impact strengths of epoxy nanocomposites is presented in Fig. 8. The impact strength of nanocomposites reinforced with 3 wt% Cloisite Na⁺ is approximately 24% higher (as highest strength level) than that of neat epoxy when compared to 12% and 14% increases in corresponding epoxy/Cloisite 10A nanocomposites and epoxy/Cloisite 93A nanocomposites, respectively. Afterwards, the mild decrease of impact strengths of all nanocomposites is revealed with increasing the clay content beyond 3 wt% except epoxy/Cloisite 10A nanocomposites with a significant decreasing trend up to 10 wt%. Overall, epoxy/Cloisite 15 nanocomposites possess the least decreasing level of impact strengths in range from 3 to 10 wt% in clay contents.

The improvement of impact strengths of nanocomposites, especially at a low clay content of 3 wt%, benefit from relatively good clay dispersion with exfoliated/intercalated structures to hinder the cracks. More well dispersed rigid clay platelets, to a certain extent, constrain the internal deformation (i.e. straining effect) of epoxy matrices prone to crack initiation, resulting in higher reinforcement efficiency.

On the other hand, the presence of clay aggregates and microvoids acting as stress concentration sites for the crack growth eventually causes earlier impact failure of epoxy/clay nanocomposites mainly at high clay contents.

3.4.3 Rockwell hardness

The influence of clay type and content on Rockwell hardness of epoxy/clay nanocomposites is depicted in Fig. 9. Evidently, a consistently modest decrease in hardness values of nanocomposites is manifested with increasing the clay content irrespective of clay types when compared to that of neat epoxy. When varying the clay content from 3 to 10%, hardness values of nanocomposites are reduced from approximately 76 to 72 HRE (decreasing level of 4%). The maximum hardness appears to be achieved at about 76 HRE for epoxy nanocomposites reinforced with 3 wt% Cloisite 15, which is still slightly below that of neat epoxy. Exceptionally, epoxy/Cloisite Na⁺ nanocomposites undergo initial hardness retention when the clay content increases with comparable hardness values to that of neat epoxy. The decreasing trend of hardness for epoxy/clay nanocomposites may be ascribed to poor clay wettability leading to agglomerated structures rather than high levels of exfoliated/intercalated counterparts, as well as the coexistence of microvoids and pores [58].

3.5 DSC thermal analysis

The DSC thermograms and T_g values for epoxy/clay nanocomposites under investigation are depicted in Fig. 10 and 11, respectively. Overall, T_g values of epoxy/clay nanocomposites were found to be higher than that of neat epoxy, which suggests that rigid clay particles can restrict the mobility of epoxy molecules so that a higher T_g is generally required to overcome the phase change of epoxy/clay nanocomposites. The addition of 3 wt% clay for epoxy nanocomposites reinforced

with Cloisite 10A, Cloisite Na⁺, Cloisite 93A and Cloisite 15 was found to consistently increase T_g by approximately 11, 13, 16 and 23%, respectively. Even though T_g decreases slightly at the clay content from 3 to 5 wt% for epoxy nanocomposites reinforced with Cloisite Na⁺, Cloisite 93A and Cloisite 15, associated values were still higher than that of neat epoxy. More remarkably, epoxy/Cloisite 15 nanocomposites exhibit a maximum increase of 28% in T_g (relative to neat epoxy) with 10 wt% clay inclusions.

These results for the enhancement of T_g can also be associated with interaction hindrance of epoxy network with embedded rigid clay particles into epoxy matrices, high clay dispersibility at the low content levels, degree of crosslinking, chain flexibility and molecular weight of used epoxy resin [3, 59]. The slight decrease in T_g at clay contents of 3-8 wt% for Cloisite Na⁺, Cloisite 93A and Cloisite 15 inclusions and 5-8 wt% for Cloisite 10A inclusions may arise from the reduction of the degree of crosslinking density in epoxy molecules.

4 Conclusions

This study has investigated the effect of material formulation of synthesised epoxy/clay nanocomposites on their resulting mechanical and thermal properties using three combined pre-mixing processes, namely shear mixing, ultrasonication and centrifugation. A mix of intercalated, exfoliated and predominantly agglomerated clay structures was observed by XRD, TEM and SEM. Based on the combination of three different pre-mixing processes, epoxy/clay nanocomposites possess decreased flexural strengths (up to 53%) and smaller Rockwell hardness values (up to the decreasing level of 7%) when compared to those of neat epoxy. These findings are due to weak interfacial bonding between clay fillers and epoxy matrices, as well as the presence of clay aggregates and microvoids acting as stress concentration sites and typical defects, respectively for crack initiation. Moreover, lower maximum

flexural modulus and impact strength of nanocomposites are affected by poor clay wettability and clay agglomeration according to SEM and TEM results. Finally, T_g of nanocomposites increases regardless of clay type as compared with that of neat epoxy. The mobility of epoxy molecules is believed to be obstructed with the inclusion of rigid clays. Further optimisation of material formulation and processing condition is required to achieve more desirable clay dispersibility and excellent mechanical and thermal properties of epoxy/clay nanocomposites.

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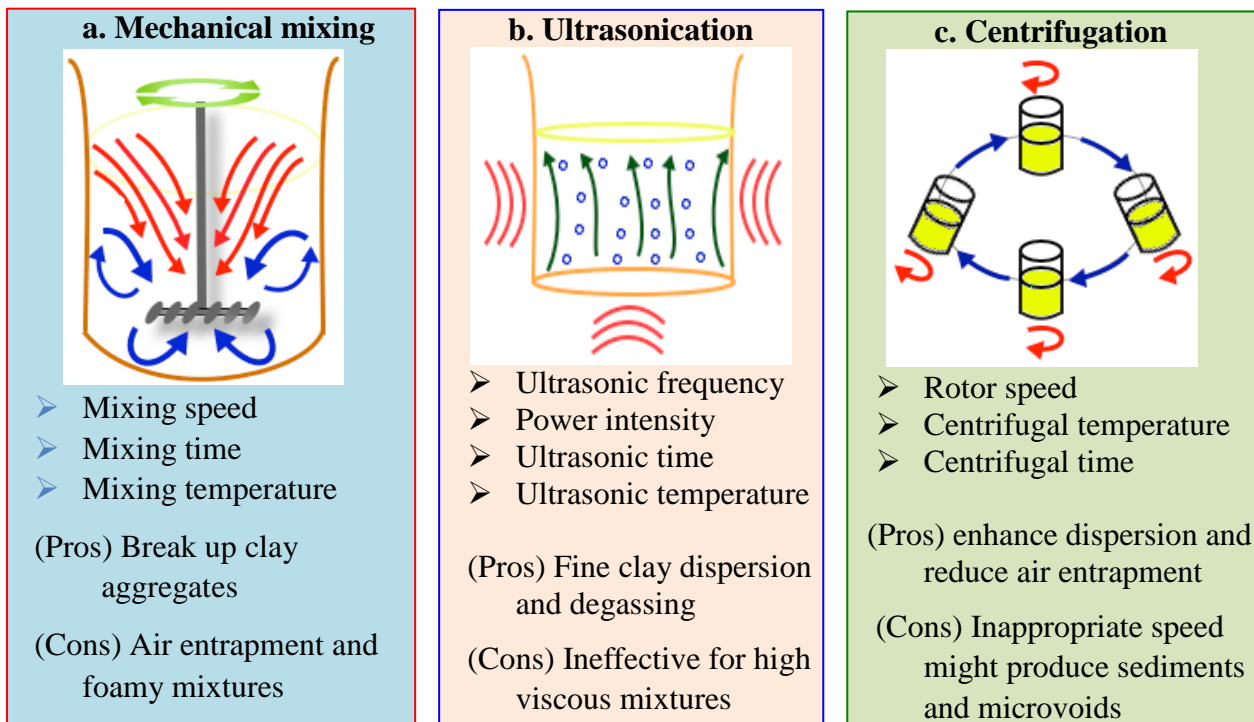


Fig. 1

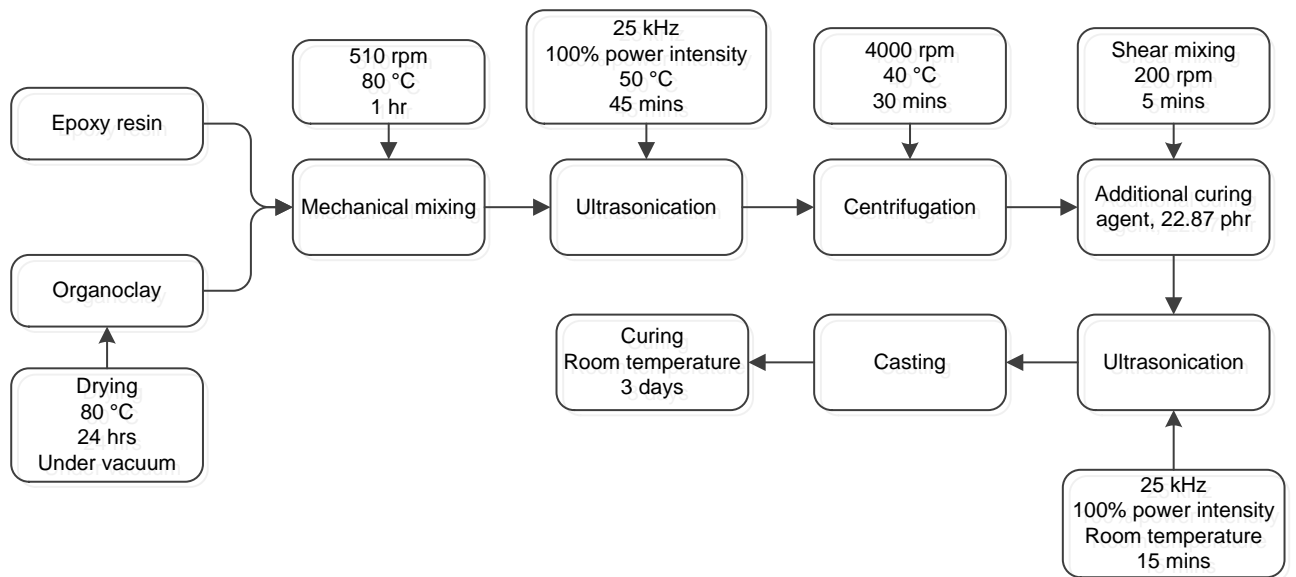


Fig. 2

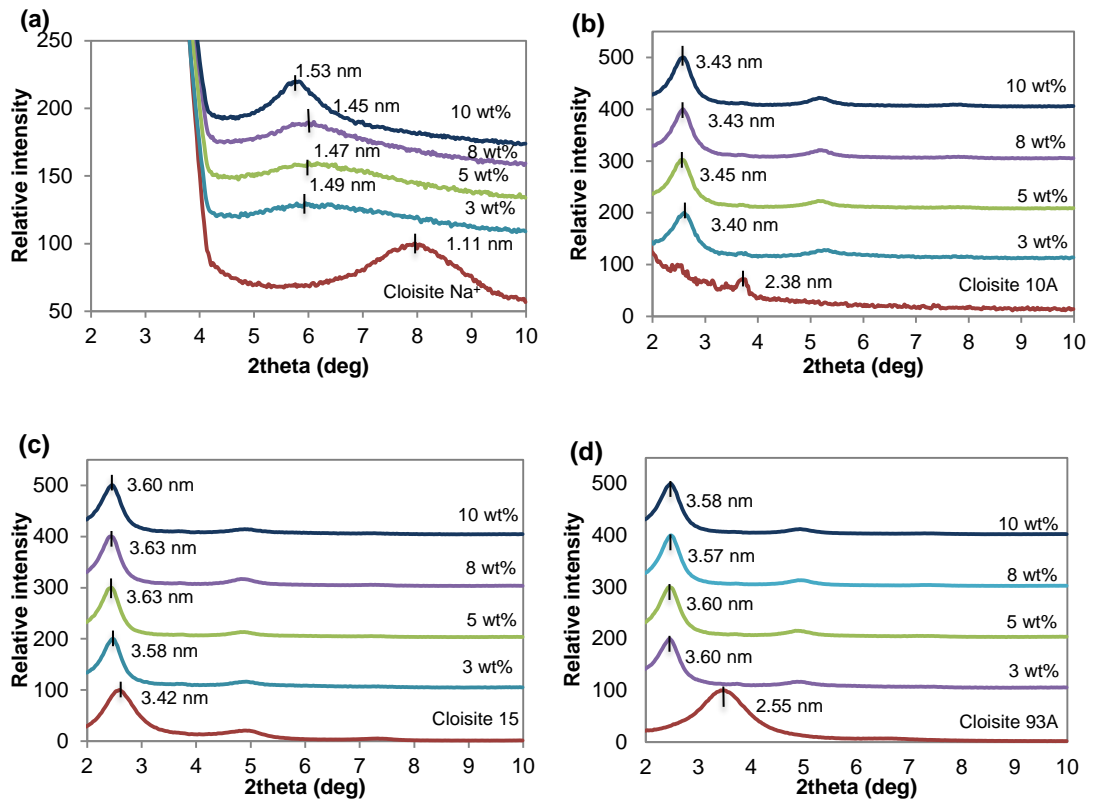


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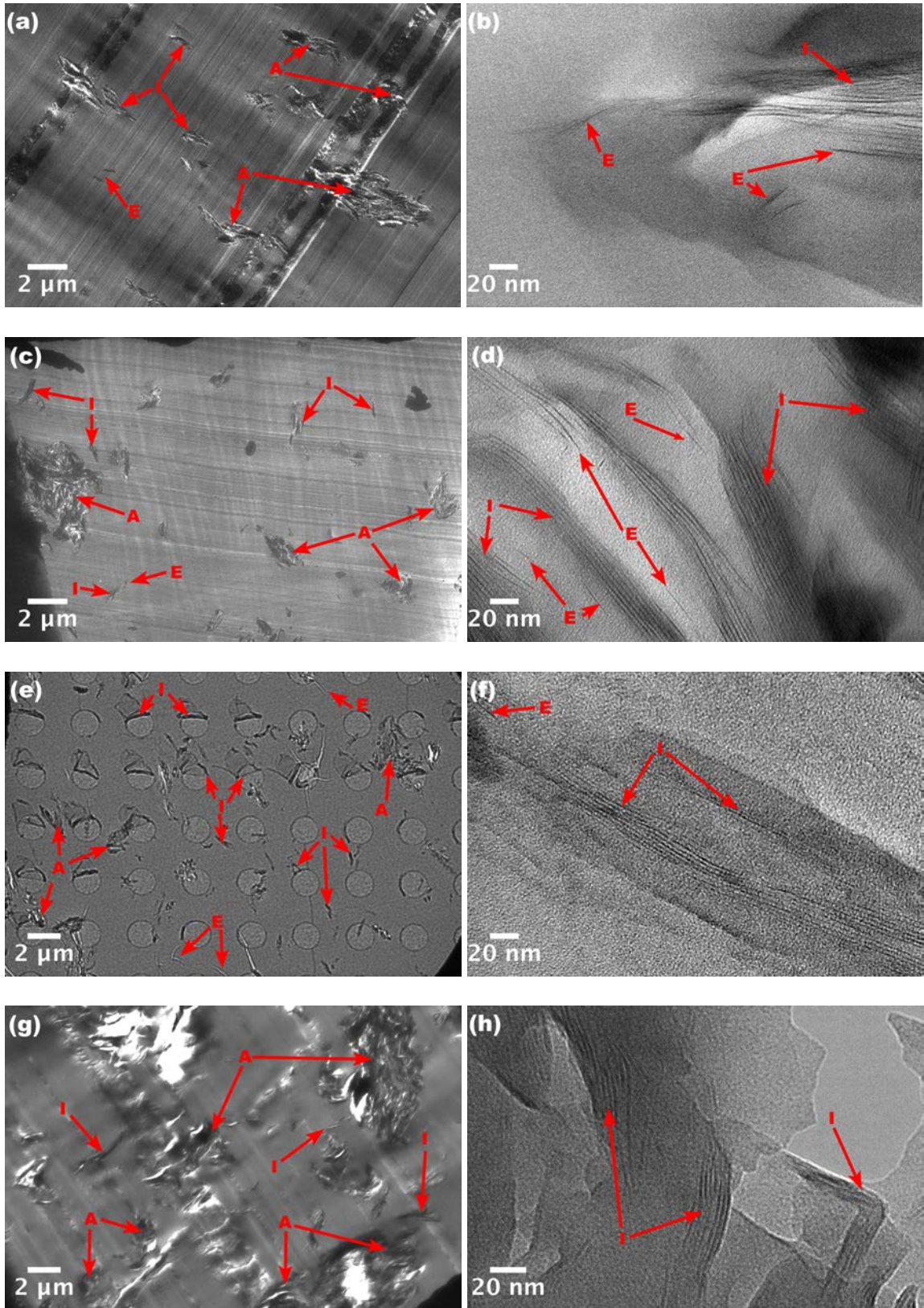


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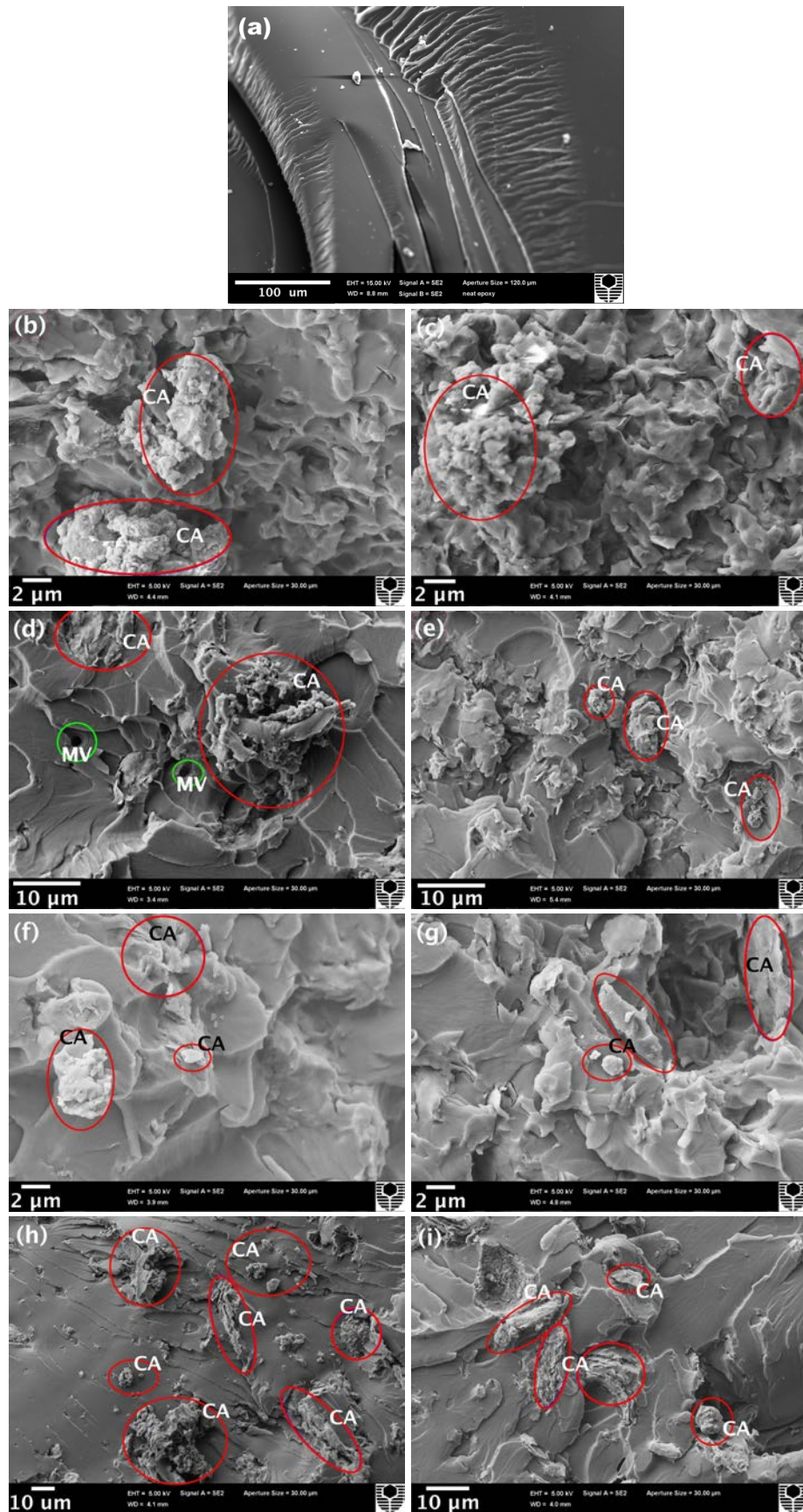


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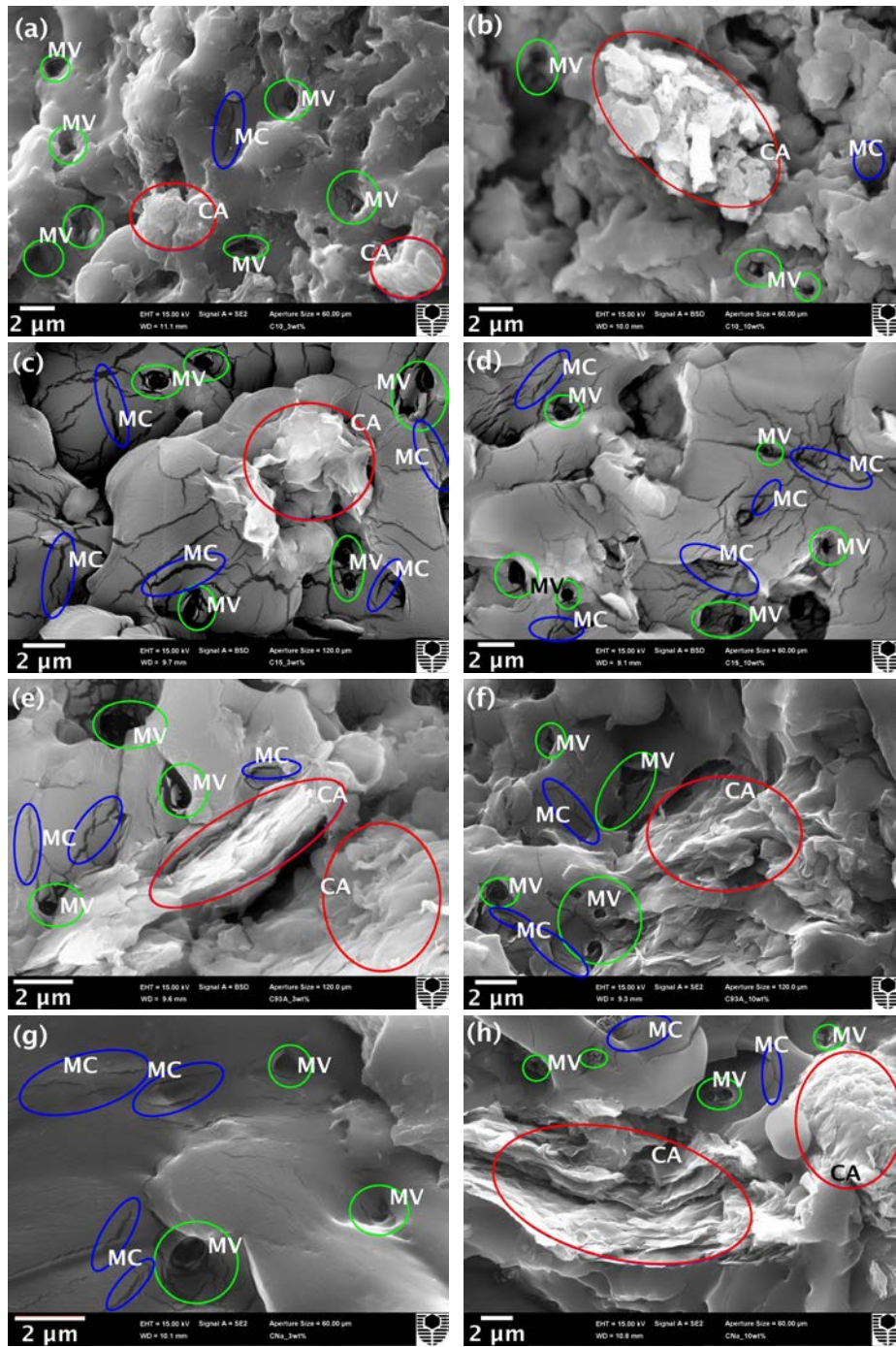


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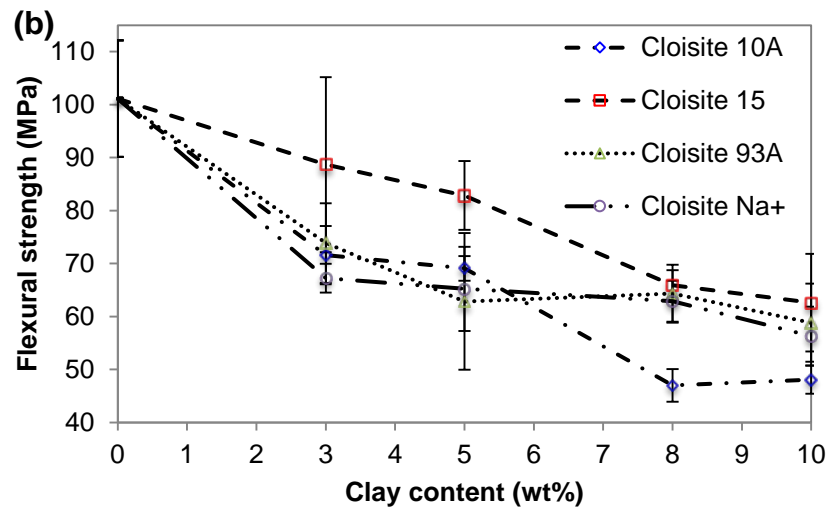
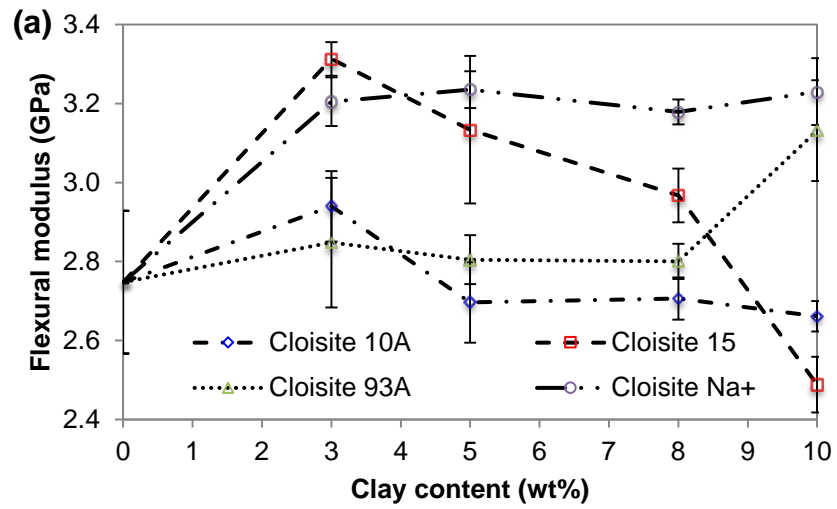


Fig. 7

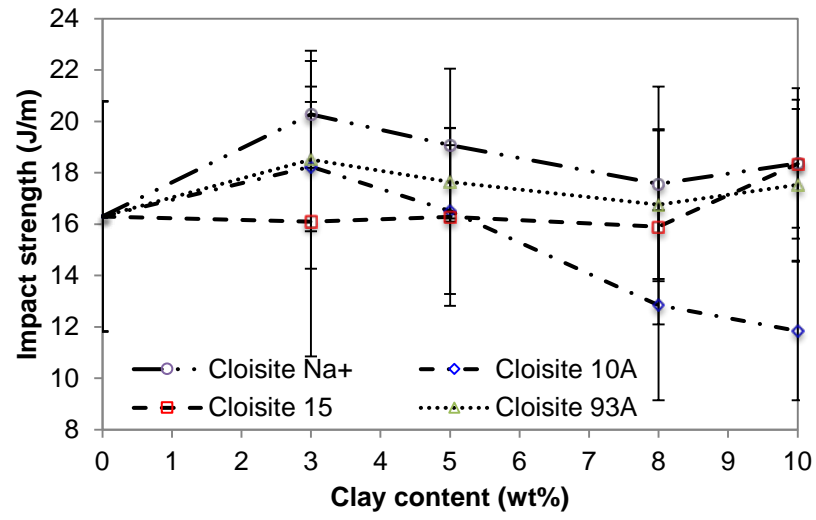


Fig. 8

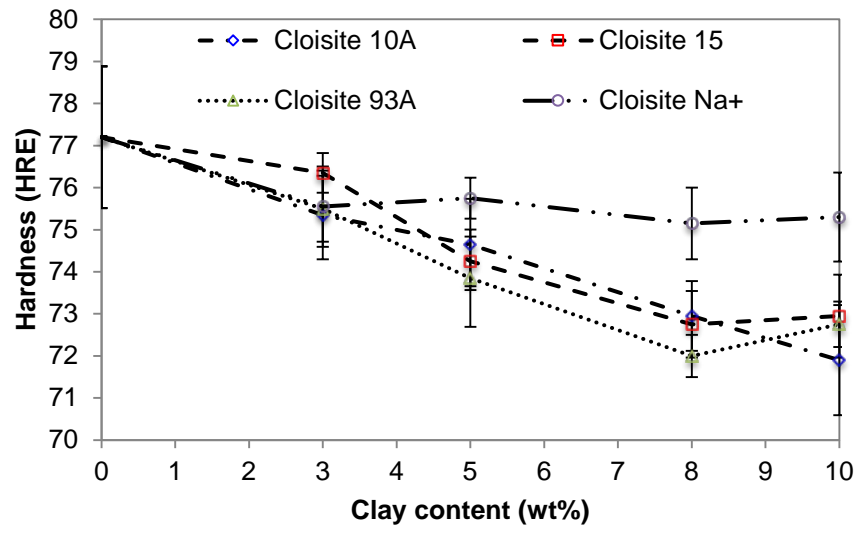


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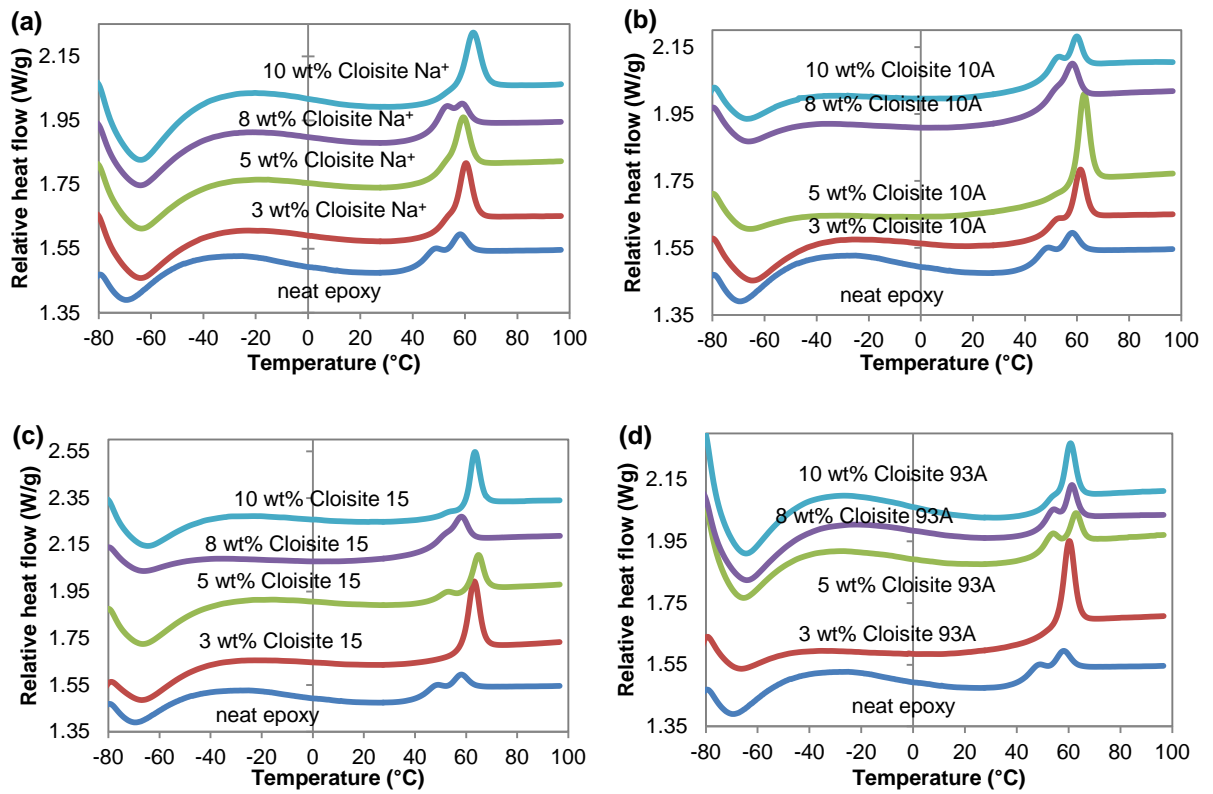


Fig. 10

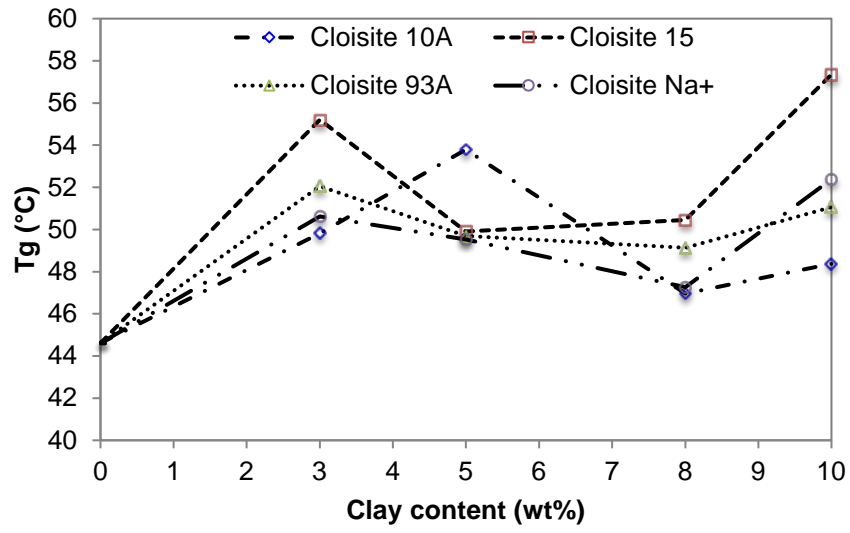


Fig. 11

Table 1. Specifications of Cloisite® clays [12, 54]

clay types	Organocation salt	Interlayer spacing d_{001} (nm)	Cation exchange capacity (meq/100g)
Cloisite Na ⁺		1.17	92.6
Cloisite 10A	Benzyl(hydrogenated tallow alkyl)dimethyl, salt	1.9	125
Cloisite 15	Bis(hydrogenated tallow alkyl)dimethyl, salt	3.63	125
Cloisite 93A	Trialkyl ammonium, salt	2.36	90

Table 2. Summary of interlayer spacing values for as-received clays and epoxy/clay nanocomposites

No	Material sample	XRD Peak		
		2 θ	Interlayer spacing d_{001} (nm)	% increase of d_{001}
1	Cloisite Na ⁺ (CNa ⁺)	7.94	1.11	
2	CNa ⁺ -3wt%	5.94	1.49	33.54
3	CNa ⁺ -5wt%	5.99	1.47	32.37
4	CNa ⁺ -8wt%	6.10	1.45	30.09
5	CNa ⁺ -10wt%	5.76	1.53	37.80
6	Cloisite 10A (C10A)	3.71	2.38	
7	C10A-3wt%	2.60	3.40	42.60
8	C10A-5wt%	2.56	3.45	44.69
9	C10A-8wt%	2.57	3.43	44.10
10	C10A-10wt%	2.57	3.43	44.15
11	Cloisite 15 (C15)	2.58	3.42	
12	C15-3wt%	2.47	3.58	4.70
13	C15-5wt%	2.43	3.63	6.19
14	C15-8wt%	2.44	3.63	6.04
15	C15-10wt%	2.45	3.60	5.31
16	Cloisite 93A (C93A)	3.47	2.55	
17	C93A-3wt%	2.45	3.60	41.31
18	C93A-5wt%	2.46	3.60	41.06
19	C93A-8wt%	2.48	3.57	39.89
20	C93A-10wt%	2.47	3.58	40.51