

## Physical properties of Mesozoic sedimentary rocks from the Perth Basin, Western Australia.

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Running title: Petrophysics of Perth basin sedimentary rocks

The Perth Basin (PB) hosts important aquifers within the Yarragadee [Formation](#) and adjacent geological formations with potential for economic exploitation by both geothermal energy and carbon capture and sequestration. ~~Yet p~~Published studies on the reservoir quality of the sedimentary units of the PB are very few. This study reports some petrophysical and lithological characteristics of the sedimentary units of interest for geothermal and geosequestration scenarios and help interpolation toward non-sampled intervals. A new fluvial dominated lithofacies scheme was developed for the Mesozoic stratigraphy from four wells drilled in the central Perth Basin (Pinjarra-1, Cockburn-1, Gingin-1 and Gingin-2) based on grain size, sorting, sedimentary structures and colour that relate to the environment of deposition. Systematic laboratory measurements of permeability, porosity, and thermal conductivity were conducted on core samples to investigate a variety of lithofacies and depths from these wells. Empirical correlations are established among the different physical properties, indicating ~~very~~encouraging relationships for full PB basin interpolation ~~by instancesuch as~~ between porosity and permeability, when the samples are grouped into 'hydraulic units' defined by a 'flow zone indicator' parameter.

The common principal controls on the PB thermal conductivity are the pore space arrangement and mineralogical content, which ~~is-are~~ strongly lithofacies specific. Therefore the lithofacies type could be a good first-order discriminator for describing spatial variations of thermal conductivity and then estimate their flow zone indicator.

Keywords: Perth Basin, petrophysics, porosity, permeability, thermal conductivity, lithofacies, hydraulic units.

## INTRODUCTION

The north to north-northwest trending Perth Basin (PB) extends about 1300 km along the southwestern margin of Australia and is part of the East Gondwana rift system. It contains a thick Permian to Cretaceous succession that incorporates an unconformity associated with the break-up of Australia and Greater India in the Early Cretaceous. The post-break-up succession is relatively thin onshore but thickens rapidly offshore and extends to the edge of the continent–ocean boundary.

Exploration for hydrocarbons in the PB began in the late 1940s; oil and gas has been produced from Jurassic sandstones strata within the Cattamarra Coal Measures, within and underlying the Kockatea Shale, from the Upper-upper Permian Dongara Sandstone and Wagina Sandstone, and from the Lower-lower Permian Irwin River Coal Measures.

Based on sparse data available from petroleum exploration wells, Bestow (1982) identified low temperature reservoirs (65–85°C) at depths of 2.0–3.5 km, with as having the best economic potential in the PB (Bestow 1982). More recently the PB has been the subject of studies evaluating its potential for direct use of geothermal energy (e.g. Ghori 2008; Reid *et al.* 2012; Ricard *et al.* 2012; Timms *et al.* 2012) and CO<sub>2</sub> geosequestration (Varma *et al.* 2009; Delle Piane *et al.* 2013; Stalker *et al.* 2013).

These studies are affected by the limited information available in the literature published data on the distribution of permeability and thermal properties within the sedimentary units. This information is critical for the successful evaluation and management of the geothermal energy and repository potential of the PB.

The aim of this study is to petrophysically characterise the sedimentary formations in four wells drilled along a north–south transect of the central, onshore part of the PB. Laboratory measurements of porosity, permeability and thermal conductivity on core plugs were used to build empirical relationships between different physical properties of the rocks, and correlated with lithofacies so that they can be applied to field studies for which where only wireline log measurements are available.

## REGIONAL GEOLOGY AND STRATIGRAPHY

The Perth Basin contains a Permian to Holocene sedimentary succession overlying Precambrian basement. The basin originated as a rift with significantly variable rifting rates along its axis that gave rise to temporal variations in the rate of deposition along the basin; variable formation thicknesses are reported reflecting local variations in subsidence (Crostella & Backhouse 2000).

The stratigraphy of the PB is dominated by fluvial to shallow marine siliciclastic facies; for this study we focussed on Triassic to Jurassic units, especially the Lesueur Sandstone, Cattamarra Coal Measures, Cadda Formation and the Yarragadee Formation. The Cretaceous and overlying units are too thin and shallow to be considered for geosequestration or geothermal energy and porosity–permeability degradation with depth considerably reduces the potential of underlying units. The stratigraphic boundaries for our wells are taken from Crostella & Backhouse (2000), while the sedimentology of the units follows the interpretation presented by Timms *et al.* (2012, 2013)

Among the stratigraphic units analysed in this study two are of particular interest for their potential commercial exploitation: i) the Lesueur Sandstone, a medium to very coarse grained sandstone representing the potential target for CO<sub>2</sub> geosequestration project in the southern PB (Varma *et al.*

2009; Stalker *et al.* 2013); and ii) the Yarragadee Formation, a fine to coarse grained, poorly sorted feldspathic sandstone succession representing the potential target for geothermal projects in the PB (Reid *et al.* 2012; Timms *et al.* 2012).

## CORE COLLECTION AND EXPERIMENTAL METHODS

This study is based on the analysis of solid plugs cut from cores from the only four exploration wells drilled in the PB with available cored sections. From south to north, these wells were Pinjarra-1, Cockburn-1, Gingin-1, and Gingin-2 (Figure 1). The cores are housed at the Western Australia Core Library facility of the Geological Survey of Western Australia. Samples were chosen to ensure a statistical representation of the measured physical properties, and to capture intra-formation variations. Table 1 summarises the total depth and the formation tops for the four studied wells.

The solid plugs were cut from homogeneous and coherent sections of whole- and half-slabbed core pieces without 'visible' faults and fractures that could influence physical measurements.

### Lithofacies classification scheme

Little core material was taken from each well as, at the time (in the mid to late 1960s), individual cores were typically 1 to 5 m long and spaced 100 to 150 m apart. Despite such an incomplete record, the regular length and spacing of the cored intervals provides a statistically unbiased snapshot of the formations. In Pinjarra-1 28 cores (totalling 60 m) were cut; in Cockburn-1 26 cores (65 m); in Gingin-1 28 cores (86 m); and in Gingin-2, 8 cores (97 m); the number of samples analysed from each well is shown in Table 1. Sedimentary logging at approximately 1:1000 on the cores from Pinjarra-1, Cockburn-1, Gingin-1 and Gingin-2 was used to develop a lithofacies scheme (see Timms *et al.* 2012, 2013 for details); each sample was assigned a lithofacies type according to sedimentary logging.

Each lithofacies was recognised based on the distinct physical characteristics of the cored sections including grain size, sorting, sedimentary structures and colour. The primary control on these characteristics is the environment of deposition therefore a lithofacies scheme is commonly interpreted in terms of sedimentary environment; a braided fluvial-dominated facies scheme developed by Miall (1996) was adapted in the interpretation of the sedimentary origin of the units from Cockburn-1, Gingin-1, Gingin-2 and Pinjarra-1.

Nine distinct lithofacies were identified:

1. Ai – Gravel to very coarse sandstone, commonly cross bedded, interpreted to represent high energy fluvial channel fill;
2. Aii – Medium to very coarse cross-bedded sandstone with significant grain size variation between beds, interpreted to be migratory barforms in high energy fluvial channels;
3. Aiii – Thickly bedded massive, coarse sandstone, interpreted to be fluidised fluvial barforms;
4. B – Massive, medium sandstone with flaser cross lamination, interpreted to represent moderate energy migrating fluvial barforms;
5. C – Fine to medium cross laminated sandstone, with common organic fragments and flaser-drapes, interpreted to be moderate to low energy stacked migrating ripples;
6. D – pale grey homogenised muddy sandstone with rootlets and thin coals, interpreted to be floodplain paleosols;

7. E – Muddy, bioturbated sandstone with slumps and dewatering structures, interpreted to be swampy/lagoonal deposits formed under waterlogged conditions;
8. F – Interbedded silty fine sandstone and siltstone with trough cross lamination, interpreted to be crevasse splays and overbank deposits;
9. G – Muddy laminated silt with plant fragments and thin laminated fine sandstone, interpreted to be swampy/ overbank deposits.

Grain sorting generally decreases from lithofacies A to G. Bioturbation in lithofacies E and G comprises simple sand-filled horizontal burrows and the occasional escape burrow. Lithofacies F is highly variable in grain size and can appear heterolithic in places. Rare synaeresis cracks in lithofacies G indicate subaqueous shrinkage, possibly due to fluctuations in salinity at the sediment–water interface, rather than desiccation.

#### Porosity and permeability

Porosity and permeability were measured in the CSIRO Petrophysics laboratory, Perth, on 38 mm diameter core plugs approximately 50 mm in length using an automated helium gas Permeameter–Porosimeter AP608 from Coretest Systems Inc. Porosity and permeability are routinely measured on dry samples with a precision of 0.1 and 0.9%, respectively. The technique is widely used in core evaluation and returns the equivalent liquid permeability (i.e. Klinkenberg corrected), which can then be readily used to estimate fluid flow behaviour under the assumption of no interaction between fluid phase and solid rock frame.

Porosity and permeability of each of the cores were measured at an arbitrary confining pressure of 13.8 MPa (i.e. equivalent to an overburden stress at 500 m deep sandstone).

#### Hydraulic units

Estimation of porosity and permeability is essential for the evaluation of fluid flow and recovery/injection rates in a reservoir. Whereas porosity can be estimated from downhole logging tools, permeability is usually estimated from indirect measurements via correlation with known parameters. Simple porosity–permeability correlation can lead to severe miss-estimation of the capacity for fluid transport of rocks; in this study we use an approach illustrated by Amaefule *et al.* (1993) based on a generalised version of the Kozeny-Carman relation:

$$\kappa = \frac{1}{F_s \tau^2 S_{vgr}^2} \frac{\phi^3}{(1-\phi)^2}$$

Where  $\kappa$  is permeability (in mD);  $\phi$  is the fractional porosity;  $F_s$  is the pore shape factor;  $\tau$  is tortuosity; and  $S_{vgr}$  is the specific surface area per unit grain volume. The last three variables are generally difficult to quantify limiting the applicability of the above relation, which can be simplified to:

$$\log RQI = \log FZI + \log \varepsilon$$

where  $\varepsilon$  is the void ratio,  $RQI$  is the reservoir quality index, and  $FZI$  is the flow zone indicator (Amaefule *et al.* 1993; Prasad 2003). Void ratio ( $\varepsilon$ ),  $RQI$  and  $FZI$  are defined as follows:

$$\varepsilon = \frac{\phi}{(1-\phi)};$$

$$RQ = 0.0314 \sqrt{\frac{\kappa}{\phi}};$$

$$FZI = \frac{1}{\sqrt{F_s \tau S_{Vgr}}};$$

In this way all the geometrical parameters related to pore space are grouped into one single variable (*FZI*) which can be estimated via laboratory measurements of porosity and permeability:

$$FZI = \frac{0.0314}{\varepsilon} \sqrt{\frac{\kappa}{\phi}};$$

The important outcome of this type of analysis is that rocks characterised by similar *FZI* also show similar flow properties, i.e. they belong to one hydraulic unit (Prasad 2003).

### Thermal properties

Thermal conductivity ( $\lambda$ ) was measured on the dry and water saturated core plugs using an Optical Thermal Scanner (OTS) (Popov *et al.* 1999) at The University of Melbourne, Australia. The measurements were collected by scanning the surface of a sample with a focused heat source in combination with an infrared temperature sensor (Popov *et al.* 1999). In the instrument, the heat source and temperature sensor are a fixed distance apart, and move in the same direction and same speed so that the sensor records the maximum temperature rise along the heating line behind the source. The comparative temperature differential before and after heating on the sample, and on a standard material (i.e. pure quartz), is used to compute thermal conductivity.

Thermal conductivity can be measured with the OTS to an accuracy of 1.5% within a range of 0.1 to 70 Wm<sup>-1</sup>K<sup>-1</sup>. The maximum depth of investigation using this instrument is about 0.5 to 1 cm (i.e. 0.5 to 1 cm<sup>3</sup>). Before the analysis each plug was painted in black to avoid heat reflection; thermal conductivity was then measured by scanning the surface parallel to the plug axis first on dry specimens and then after they had been saturated with tap water under vacuum for 24 hours.

## RESULTS

### Porosity and permeability

The values of porosity and permeability are plotted as a function of depth in Figures 2 and 3. A statistical summary of the measurements is provided in Table 2 with results grouped by formation. In the four wells analysed, the Yarragadee Formation has the highest porosity (up to 36%) as well as the highest mean porosity (16%). On the other hand the Cattamarra Coal Measures shows the lowest porosities, with mean values around 5%. Overall, the porosity values show a general trend of reduction with depth. However, within each core porosity varies by several percentile points.

Permeability also attains maximum values in the Yarragadee Formation (up to 1400 mD), as well as showing the highest mean value in the same formation (approximately 45 mD). A common result for

all the formations, however, is that permeability values show a weak trend of reduction with depth, and can change by several orders of magnitude within the same stratigraphic formation (Figure 2).

### Thermal conductivity

Thermal conductivity (TC) measured under dry and water saturated conditions on specimens from the four wells is presented as a function of depth in Figure 4 and summarised in Table 3.

TC ranges from 2.76 to 3.29  $\text{Wm}^{-1}\text{K}^{-1}$  under dry, and from 4.27 to 4.43  $\text{Wm}^{-1}\text{K}^{-1}$  under saturated conditions. Within each well and each sedimentary unit, some variations of thermal conductivity are observed (Figure 4). The Yarragadee Formation clearly records the lowest thermal conductivity across the wells under dry (2.6  $\text{Wm}^{-1}\text{K}^{-1}$ ) and saturated conditions (4.3  $\text{Wm}^{-1}\text{K}^{-1}$ ).

## DISCUSSION

Porosity–permeability relationships for different lithofacies have been derived for the complete data set and reported in Timms *et al.* (2012, 2013), who shows that exponential trend lines fit the data with good correlation in some lithofacies specific grouping, but the statistical correlation dramatically reduces for facies E, F and G. The lower statistical correlation could be explained by the small grain sizes, high initial clay content, and lithological variability inherent to these lithofacies.

Here we present an alternative attempt to derive correlations between different physical properties measured on the same rock samples.

### Porosity–permeability relationship: hydraulic units grouping

*In situ* rock permeability is an elusive parameter and difficult to determine using sub-surface logging technology. Nuclear magnetic resonance (NMR) is currently the technique of choice for permeability estimation using wireline logs, but this logging method post-dates the drilling of the studied wells. Therefore, *in situ* permeability has to be determined from other commonly acquired parameters, calibrated to the core data. Using the hydraulic units classification described [in section 3.3 above](#) it is possible to obtain a framework to relate porosity and permeability according to the *FZI* number determined for each tested specimen.

The histogram of the distribution of *FZI* values calculated from our dataset (Figure 5a) shows a multimodal distribution of *FZI* ranging from 0.028 to 223. Samples with similar values of *FZI* were grouped into four clusters: 0.01 to 1; 1 to 3; 3 to 10; and finally 10 to 250. This grouping yields very good regression values in terms of relationships between porosity and permeability, as can be seen in Figure 5b where a simple power law fitting shows regression coefficients between 0.66 and 1 (Table 4). It should be noted the regression coefficient of 1 for the *FZI* class 10–250 is a function of the small sample population size. Figure 5b also shows that samples with similar porosity record a positive correlation between their *FZI* class and their permeability, therefore a higher *FZI* indicates a comparatively higher permeability.

To check how the lithofacies scheme compares with the hydraulic units grouping, [of the same samples population](#) a comparison is made between what is essentially a classification of the depositional environment of the rock samples based on qualitative estimates of grain size and sorting, and characteristic sedimentary structures determined from sedimentary logging and a quantitative characterisation of their measured flow properties.

No general trend is found when sample assigned to the same lithofacies type are plotted in a depth–*FZI* space (Figure 6).

The samples assigned to each of the 9 lithofacies are plotted as box and whisker graphs against the lithofacies type (Figure 7) indicating that:

- Facies Ai is characterised by relatively compact spread of *FZI*, mostly between 3 and 10;
- Facies Aii, and B show very similar distributions and largely fall in the 1–3 *FZI* grouping, indicating a first order hydraulic likeness;
- Facies Aiii and C show very similar distributions and largely fall in the 0.01 to 1 *FZI* grouping, indicating a first order hydraulic likeness;
- Facies D is characterised by the lowest *FZI* values with the entire population falling within the 0.01 to 1 grouping;
- Facies E, F and G show a wide spread of *FZI* values and span two or three classes.

A first order correlation is therefore apparent between lithofacies types and *FZI* grouping with the former defining distinct subgroups that otherwise show similar hydraulic characteristics.

Permeability predictions for the uncored sections of the wells ~~could~~ can be performed based on the hydraulic unit profiling performed on each well, for example, by computing probabilities of distribution of each hydraulic unit with depth from the distribution observed on the cores.

Using the cored sections as control intervals for the creation of a reference matrix between different rock properties it would then be possible to establish the probability of having the same hydraulic unit in a given prediction window (Amaefule *et al.* 1993).

#### Thermal conductivity considerations

No satisfactory correlation was found between TC and the other rock physical properties measured in this study. Although *FZI* seems a good first order discriminator for porosity and permeability, it does not encompass enough information to be a valid discriminator for thermal conductivity. This could be a consequence of thermal conductivity being strongly dependent on mineralogy (Clauser & Huenges 1995; Clauser 2006; Tong *et al.* 2009). Several authors have used this dependency to calculate thermal conductivity from the proportions and thermal conductivity of the dominant mineral phases and neglect the influence of subordinate minerals (McKenna *et al.* 1996; Ozkahraman *et al.* 2005, 2004; Abdulagatova *et al.* 2009). Quartz is the dominant mineral phase in our samples and the proportion of secondary minerals is somewhat lithofacies dependant (Timms *et al.* 2012).

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Given that the depositional environment exerts primary control on the physical characteristics defining a lithofacies, the dependency of thermal conductivity on lithofacies type is mostly controlled by the depositional energy such that high-energy facies (i.e. quartz dominated) show the highest TC, and low energy facies (i.e. clay-clay-rich mudstones) have lower TC values (Figure 8). The presence of water in the pore volume seems to enhance this trend (Figure 8).

#### Petrophysical facies signature

A cross plot of thermal conductivity and *FZI* summarises the experimental measurements conducted on the PB sample grouped according to the lithofacies scheme of Timms *et al.* (2012) (Figure 9). The

plot highlights how different facies may show similar hydraulic properties (e.g. facies B and Aii; and C and Aiii) but can be distinguished based on their thermal conductivity. Therefore by knowing the facies type and the thermal conductivity one can associate a minimum and maximum bound of expected *FZI*. Such an observation may be extrapolated to areas of a basin with similar depositional settings if that the depositional setting is equivalent to the one studied here. Moreover, the relationships between facies type, thermal conductivity and *FZI* can potentially be used in areas where core material is not available but facies types can be identified; for example, using wireline logging tools and/or cuttings from drilling operations.

## CONCLUSIONS

This study presents a comprehensive set of petrophysical analysis on core samples from the central Perth Basin. The selected plugs are representative of sedimentary units of fluvial origin presently considered as possible targets for geothermal and CO<sub>2</sub> sequestration projects in Western Australia. Despite their important industrial implications, data on the petrophysical properties of such units are critically absent in the open literature, and therefore the new results should provide much needed support for the above-mentioned projects.

The experimental results are interpreted in light of the geology of the central Perth Basin and can be summarised as follows:

1. Measurements of petrophysical properties of samples from nine lithofacies can be grouped into four hydraulically meaningful categories. This analysis shows that stratigraphic boundaries do not account for the intra-formational variation of petrophysical properties in the Perth Basin, but there is a good to excellent relationship between porosity and permeability in samples grouped according to the *FZI*.
2. An appraisal of the qualitative (lithofacies scheme) and the quantitative (hydraulic units) sample classification indicate a first order correlation between lithofacies types and *FZI* groups.
3. Thermal conductivity does not follow the same trend and only seems to be related to facies type based on a qualitative description of the mineralogical content and grain arrangement within the rock.
4. In the absence of core or suitable wireline log, a combination of lithofacies type and thermal conductivity may be used to estimate *FZI*, thereby providing important information on hydraulic properties.

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#### FIGURE CAPTIONS

Figure 1 (A) Geological map of the central Perth Basin showing the location of the studied wells (modified after Timms *et al.* 2012); geological timescale, after Gradstein *et al.* (2012).

Figure 2 Experimentally measured porosity as a function of depth for core plugs extracted from four wells in the Perth Basin. Values of porosity reported in the Figure are those measured at a confining pressure of 13.8 MPa.

Figure 3 Experimentally measured gas permeability as a function of depth for core plugs extracted from four wells in the Perth Basin.

Figure 4 Experimentally measured thermal conductivity ( $\lambda$ ) as a function of depth for core plugs extracted from four wells in the Perth Basin.

Figure 5 a) Histogram of the flow zone indicator (*FZI*) values in the Perth Basin as estimated from a population of 158. Four families of samples have been discriminated based on the histogram distribution. b) porosity–permeability cross plot for samples grouped according to their *FZI* values. Thick lines are the power law fit to the data, regression coefficient of each fit line is reported as  $R^2$  value, dashed lines are the 95% confidence bands of each regression.

Figure 6 Relationships between depth, *FZI* and lithofacies type for the sample collection analysed in this study.

Figure 7 Comparison between *FZI* grouping and lithofacies scheme classification of the samples presented in this study. Horizontal dashed lines mark the limit of each *FZI* group; lower right corner of the figure indicates the statistical values of reported for each population box.

Figure 8 Experimentally measured thermal conductivity as a function of lithofacies typically encountered in the sedimentary units of the Perth Basin.

Figure 9 Comparison between values of *FZI* and experimentally measured thermal conductivity (saturated conditions) per facies.

#### TABLES

**Table 1** Formation tops (in m) of the wells used in this study (Crostella & Backhouse 2000). Ldv = Leederville Formation; SPS = South Perth shale; Jer = Jervoise Sandstone; Oto = Otorowiri Formation; Yarra = Yarragadee Formation; Cadda = Cadda Formation; CCM = Cattamarra Coal Measures; Ene = Eneabba Formation; Les = Lesueur Sandstone. T.D. = total depth.

**Table 2** Statistical values of porosity ( $\phi$ ) and permeability ( $\kappa$ ) as measured on core plugs. Values grouped by formation.

**Table 3** Descriptive statistics of thermal conductivity ( $\lambda$ ) as measured on core plugs.

**Table 4** Summary of empirical relationships between permeability, porosity, and compressional wave velocity for sample grouped in four *FZI* clusters.