Modeling, Control and Design of a Quadrotor Platform

for Indoor Environments

by

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ABSTRACT

Unmanned aerial vehicles (UAVs) are widely used in many applications because of their small size, great mobility and hover performance. This has been a consequence of the fast development of electronics, cheap lightweight flight controllers for accurate positioning and cameras. This thesis describes modeling, control and design of an oblique-cross-quadcopter platform for indoor-environments.

One contribution of the work was the design of a new printed-circuit-board (PCB) flight controller (called MARK3). Key features/capabilities are as follows:

(1) a Teensy 3.2 microcontroller with 168MHz overclock –used for communications, full-state estimation and inner-outer loop hierarchical rate-angle-speed-position control, (2) an on-board MEMS inertial-measurement-unit (IMU) which includes an LSM303D (3DOF-accelerometer and magnetometer), an L3GD20 (3DOF-gyroscope) and a BMP180 (barometer) for attitude estimation (barometer/magnetometer not used), (3) 6 pulse-width-modulator (PWM) output pins supports up to 6 rotors (4) 8 PWM input pins support up to 8-channel 2.4 GHz transmitter/receiver for manual control, (5) 2 5V servo extension outputs for other requirements (e.g. gimbals), (6) 2 universal-asynchronous-receiver-transmitter (UART) serial ports - used by flight controller to process data from Xbee; can be used for accepting outer-loop position commands from NVIDIA TX2 (future work), (7) 1 I2C-serial-protocol two-wire port for additional modules (used to read data from IMU at 400 Hz), (8) a 20-pin port for Xbee telemetry module connection; permits Xbee transceiver on desktop PC to send position/attitude commands to Xbee transceiver on quadcopter.

The quadcopter platform consists of the new *MARK3* PCB Flight Controller, an ATG-250 carbon-fiber frame (250 mm), a DJI Snail propulsion-system (brushlessthree-phase-motor, electronic-speed-controller (ESC) and propeller), an HTC VIVE Tracker and RadioLink R9DS 9-Channel 2.4GHz Receiver. This platform is completely compatible with the HTC VIVE Tracking System (HVTS) which has 7ms latency, submillimeter accuracy and a much lower price compared to other millimeterlevel tracking systems.

The thesis describes nonlinear and linear modeling of the quadcopter's 6DOF rigid-body dynamics and brushless-motor-actuator dynamics. These are used for hierarchical-classical-control-law development near hover. The HVTS was used to demonstrate precision hover-control and path-following. Simulation and measured flight-data are shown to be similar. This work provides a foundation for future precision multi-quadcopter formation-flight-control.

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Chapter 1

OVERVIEW

1.1 Introduction and Motivation

In the last few decades, quadrotors have been used for many industrial and agricultural applications. The need for UAV with greater maneuverability and hovering ability compared with fixed-wing aircraft has led to a rise in quadrotor research. Research continuously increases the abilities of quadcopters in stability, and maneuverability. Quadrotors are capable of advanced autonomous missions like formation flight and environment exploration. Also quadrotors exhibit a good degree of decoupling, which makes the flight controller design easier than helicopters.

The work of this thesis is the first step of achieving a quadrotor swarm mission. Potential applications can include: manufacturing, transportation, firework display and much more. A flight controller with a teensy 3.2 microcontroller and MEMS sensors is designed to develop a low-cost quadrotor platform that can be used for formation flight. With development of Virtual Reality Entertainment System, we can use low-cost indoor tracking devices (HTC VIVE Virtual Reality System) to do indoor tracking with millimeter-level accuracy instead of expensive motion capture system like VICON and Optitrack.

Plant model of this quadrotor platform within both rigid body dynamics and actuator dynamics is examined. In order to design full- state feedback cascade controllers for a quadrotor, the nonlinear model of rigid body dynamics need to be linearized under the small roll and pitch movement assumption (hovering mode). Additionally, the actuator also requires linearization before controllers designed for each separate system input.

Control design and implementation have high priority in the applications of quadrotors. Many control methods have been proposed for quadrotor control problem, such as PID, LQR, backstepping nonlinear control and sliding mode control. In practice, cascaded feedback control is the most widely used quadrotor control technique providing comparable or even better performance than more complex controllers.

1.2 Literature Survey

To introduce quadrotor modeling, hardware, design, and control, the following literature survey is offered. An approach is made below to indicate what papers or works are most relevant to this thesis. For short, the following works are most relevant for the developments within this thesis

- quadrotor linear control work within: [1] and [2]
- quadrotor modeling work within: [5] and [6]
- quadrotor parameters measurement work within: [7]
- design of quadrotor flight controller and ground station architecture within: [8] and [9]
- quadrotor state estimation within: [11], [14] and [23]

An attempt is made below to provide relevant leading technical details.

• Quadrotor Modeling Within this thesis, kinematics, rigid-body dynamics and acutator dynamics are represented as a central focus of the work. Here we assume quadrotor including frame, propulsion system and flight controller as a rigid body. And we assume 4 ESC-motor-propeller sets (propulsion system) are identical. The actuator inputs are voltages and PWM (Pulse Width Modulation) signals. Two motors are rotating in clockwise direction (CW mode) while other two are rotating in counterclockwise direction (CCW mode). The thrust generated by four propellers produces total thrust and torque in roll and pitch movement. The torque generated by four motors produces torque in yaw movement.

Kinematic Model: A kinematic model of quadrotor is presented [5]. Here we use Euler angle to represent roll, pitch and yaw angle on linearized model, modeling analysis and linear control. Quaternion is used to represent attitude on design of nonlinear state estimator for low cost of microcontroller calculation, avoidance of bad use of singular value and prevention of gimbal lock [15].

Dynamic Model: The dynamic model of quadrotor consists of two parts: rigid dynamics and actuator dynamics. For rigid dynamics, we assume the whole quadrotor is a rigid body and the center of frame matches the center of mass. Based on Newton's second law, we can get the rigid dynamics for positional movement and angular movement. For actuator dynamics, we assume all four sets of actuator are identical and the actuator model is an ideal ESC-motor system [2]. From actuator testing, we can get the mapping from PWM signal to desired rotation speed of motors in order to represent the actuator model with a first-order transfer function.

• Quadrotor Control The quadrotor control is split into a low-level part for attitude control and a high-level part for position control. The desired orientation and the desired thrust command are outputs of high-level position control. These desired values are inputs of the low-level attitude control and decoupled as the direct command for all four motors.

Low Level Control: The low-level controller is designed for tracking the desired orientation generated from the high-level controller. It is split into angular rate control as inner loop and attitude control as outer loop. The angular rate controller is based on PD control [3] law (Classical control design). It also corresponds to an LQR controller for a dynamical system containing the body rates and body torques as state [4].

High Level Control: The high-level controller consists of translational movement control and vertical movement (altitude control). Both can be split into position control as outer loop and velocity control as inner loop. The reference input of the outer loop is the desired position and the reference input of the inner loop is the desired velocity. The nonlinear constraint must be added to the output of the velocity control in the real flight controller. Here we use P-PD cascade control to perform high-level controller.

• Design of Quadrotor Flight Controller and Ground Station Architecture

Quadrotor Flight Controller Design: The flight controller consists of a Microcontroller Unit, an IMU Module, Power Modules and a Communication Module. It is also a hub offering enough design redundancy for many other important peripherals on the quadrotor like 4 ESCs (Electronic Speed controller), a 2.4Ghz Radio System Receiver, I2C/UART devices, etc. The firmware is programmed to achieve high-level/low-level control, communication process, state estimation and power/device management function. **Ground Station Architecture Design:** The ground station consists of motion capture system (HTC VIVE) and a desktop [10]. The desktop will process data from SteamVR API and send flight data pakage and command from mission planner to the flight controller on the quadrotor through the communication module. Besides, it is responsible for monitoring the flight status of the quadrotor using a GUI written in MATLAB.

• State Estimation

Sensor Calibration: The onboard MEMS sensors (accelerometer, gyroscope) have bias and they are sensitive with mechanical noise. Calibration based on sensor dynamics need to be designed to ensure that the collected sensor data is close to real value.

IIR Filtering: The MEMS sensors require low-pass filtering to reduce the influence of noise during flight. The classic infinite impulse response digital filter is applied to the output of accelerometer and gyroscope.

Full-State Estimation: A full-state nonlinear complementary filter augmented by the 6-DOF nonlinear model of quadrotor rigid body dynamics is designed as low-cost computing state estimator in the flight controller firmware. The attitude estimator is based on an explicit complimentary filter [12] obtained from accelerometer data which has MOCAP compensation and gyroscope data. The position & velocity estimator is based on a general complementary filter fusing MOCAP data and accelerometer data in world frame.

The literature survey of this thesis are of importance especially to those interested in quadrotor research.

1.3 Contribution of Work: Questions to be addressed

Within this thesis, the following fundamental questions are addressed. When taken collectively, the answers offered below, the details within the thesis, represent a useful contribution to researchers in the field. Moreover, it must be emphasized that answer to thes questions are critical in order to move substantively toward the research on formation flight.

What does a flight controller consist of? Referring to popular flight controllers on the market (Multiwii, CC3D, Pixhawk, etc), a flight controller consists of: (1) a Microcontroller Unit that offers enough computing power. (2) a MEMS (micro-electro-mechanical) IMU (Inertial Measurement Unit). (3) a Communication Module or at least a socket for it. (4) a Power Module that gives stable 3.3v ~ 5v voltage. The Mark3 Flight Controller is shown in figure (1) <u>MCU</u> Teensy 3.2 MCU which can be overclocked over 96Mhz (See Figure 1.1) offers enough computing capacity to execute high-level/low-level control and state estimation with low-cost computing work.



Figure 1.1: Teensy 3.2 Microcontroller Unit

(2) <u>IMU</u> GY-89 10DOF Sensor Module (See Figure 1.2) carrying L3GD20 (Gyroscope), LSM303D (Accelerometer and Magnetometer) and BMP180 (Barometer) is capable of measuring rotation states during flight and giving acceleration

data. The gyroscope gives angular rate and the accelerometer gives resultant force vector of the quadrotor. Currently we are not using the magnetometer and the barometer because of environmental impacts on these sensors and high RMSE (Root-Mean-Square Deviation).



Figure 1.2: GY-89 10DOF Sensor Module

(3) <u>Communication Module</u> XBee 3.0 (See Figure 1.3) is the communication module for all protocols including: ZigBee, 802.15.4, DigiMesh, BLE, etc with up to 250 Kbps RF bandwidth and up to 200 ft indoor working range.



Figure 1.3: Digi XBee3 Zigbee 3.0

(4) <u>Power Module</u> The working voltage of MCU, IMU and Communication Module is 3.3v. This step down voltage regulator (See Figure 1.4) gives stable 3.3v power supply.



Figure 1.4: 5V to 3.3V Step Down Voltage Regulator

2. How to choose other frame components? Here we choose 250mm size carbon fiber frame (See Figure 1.5)



Figure 1.5: 250mm quadrotor carbon fiber frame

which offers enough firmness for this platform. Typical actuator sets are designed for this kind of frame from different manufacturers (EMax, T-motor, DJI, etc). An actuator set consists of a propeller, a brushless motor and an ESC (Electronic Speed Controller). A quadrotor has four actuator sets.



Figure 1.6: Actuator Set (Propulsion System)

The most important criterion too choose actuator is the settling time of step response. The Snail Propulsion System shown in (See Figure 1.6) figure gives the shortest settling time compared with other actuator sets we have tested which is illustrated in Chapter 3.

3. What is the suitable indoor positioning system for a low-cost platform? Expensive motion capture systems from Optitrack or VICON that provides low latency data with millimeter-level accuracy are the premier solution for UAV and Robotic studies in the labs like UPENN Grasp Lab, Bristol Robotics Lab, etc. As development of the virtual reality entertainment system grows fast, we can use cheap devices to get similar performance to get low latency data with millimeter-level accuracy.



Figure 1.7: An idea to use HTC VIVE trackers to do robot localization

HTC VIVE Virtual Reality System offers a solution to achieve accurate indoor tracking with very low cost compared with other expensive motion capture systems based on cameras and markers. As shown in Figure 1.7, the HTC VIVE tracker placed on the gaming rifle can be also placed on a quadrotor.

- 4. What is a suitable low-level control structure? The low-level control consists of angular rate control and attitude control. For angular rate control, a simple PD control law suffices (In Chapter 5). It also corresponds to an LQR design considering actuator dynamics. For attitude control, a simple proportional control works based on the assumptions of the quadrotor model (In Chapter 2).
- 5. What is a suitable high-level control structure? The high-level control consists of altitude-vertical-velocity control and translational movement control. The altitude and vertical velocity control has the same structure as angular rate and attitude control. The quadrotor model is linearized at hovering state. So we can use P-PD structure for translational movement control (In Chapter 5).

While partial answers have been provided above, the thesis (when applicable) provedes more detailed answers. When taken collectively, the contributions of this thesis are significant - particularly to those interested in developing low-cost platforms for conducting quadrotor research.

1.4 Organization of Thesis

The remainder of the thesis is organized as follows.

- Chapter 2 (page 14) presents nonlinear model and linearization of quadrotor kinematrics, rigid body dynamics and actuator dynamics.
- Chapter 3 (page 33) describes the parameters of quadrotor rigid body dynamics and actuator dynamics measurement. This chapter also describes design of the *MARK3* flight controller and general frame structure of the hardware and software.

- Chapter 4 (page 47 presents analysis of the linearized model including angular movement and positional movement when quadrotor works near hovering mode.
- Chapter 5 (page 53) describes design of low-level control and high-level control of quadrotor hovering mode along with the simulation results.
- Chapter 6 (page 86) introduces full-state estimation based on sensor fusion of accelerometer, gyroscope and HTC VIVE Tracking System.
- Chapter 7 (page 99) presents hardware result of low-level control and high-level control along with the simulation plots.
- Chapter 8 (page 102) summarizes the thesis and presents direction for future robotics research. While much has been accomplished in this thesis, lots remain to be done.
- Appendix A (page 108) contains all MATLAB mfiles used to generate the simulation results for this thesis.
- Appendix B (page 136) contains MATLAB GUI code for UART communication between the quadrotor platform and the upper computer and UDP protocol for receiving data from SteamVR API.
- Appendix C (page 144) contains the firmware for the flight controller.
- Appendix D (page 199) contains hardware assembly instructions & software initialization for this indoor quadrotor platform to show simple indoor flight demo.

1.5 Summary and Conclusions

In this chapter, we provided an overview of the work presented in this thesis and the major contributions. A central contribution of the thesis is a low-cost quadrotor platform which is compatible with HTC VIVE tracking system that can be used for drone formation research. A simple formation demonstration was conducted with two quadrotors using the *MARK3* flight controller and HTC VIVE trackers. The thesis attempts to address most critical modeling, design, and control issues in detail - as needed.

Chapter 2

NONLINEAR MODEL & LINEARIZATION

2.1 Introduction and Overview

In this chapter, we describe the nonlinear model of the quadrotor kinematics, rigidbody dynamics, actuator dynamics, and model linearization. In order to design the control system at equilibrium point, we need to analyze and simplify quadrotor rigidbody dynamics relying on small angle assumptions for roll and pitch movement. For actuator dynamics, we can use a first-order transfer function to reproduce correlation between set-point rotor speed and actual rotor speed.

2.2 Quadrotor Nonlinear Model

2.2.1 Assumptions

The modeling of quadrotor is based on following assumptions.

- The whole quadrotor is a rigid body.
- The quadrotor frame is symmetrical.
- The center of frame matches the center of mass.
- The inertia of motor is small and neglected.
- The range of pitch movement and roll movement is small.

2.2.2 Kinematics

There are two types of quadrotor frame setup. They are 'x' configuration and '+' configuration shown in figure 2.1. While doing pitch or roll movement, the quadrotor with '+' configuration only uses 2 rotors to produce roll movement or pitch movement while the one with 'x' configuration uses all four rotors. We use 'x' configuration to fully use all four rotors for more available torque in roll and pitch movement.



Figure 2.1: Quadrotor Frame Setup

Here we let $\xi = [x, y, z]^T$ to represent position of the quadrotor in the inertial frame. Where x axis points east, y axis points north, and z axis points up. $\xi_b = [x_b, y_b, z_b]^T$ represents position of the quadrotor in the body frame. $\mathbf{V} = [v_x, v_y, v_z]^T$ represents velocity of the quadrotor in the inertial frame. $\Theta = [\phi, \theta, \psi]^T$ represents angular position of the quadrotor in the inertial frame. Yaw angle, denoted by ψ , represents rotation along z axis. Pitch angle, denoted by θ , represents rotation along y axis. Roll angle, denoted by ϕ , represents rotation along x axis. $\nu = [p, q, r]^T$ represents the angular rate of the quadrotor in body frame.



Figure 2.2: Quadrotor Coordinate Diagram

We use rotation matrix [17] based on Z-Y-X Eurler angles to present rigid-body vector that rotates from body frame to inertial frame shown in figure 2.2.

• Rotation about z axis is

$$R_{\psi} = \begin{bmatrix} \cos(\psi) & \sin(\psi) & 0\\ -\sin(\psi) & \cos(\psi) & 0\\ 0 & 0 & 1 \end{bmatrix}$$
(2.1)

• Rotation about y axis is

$$R_{\theta} = \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$
(2.2)

• Rotation about **x** axis is

$$R_{\phi} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\phi) & -\sin(\phi) \\ 0 & \sin(\phi) & \cos(\phi) \end{bmatrix}$$
(2.3)

Then we have the rotation matrix from body coordinate to inertial coordinate.

$$R_{E \to B} = R_{\phi} R_{\theta} R_{\psi} = \begin{bmatrix} \cos(\theta) \cos(\psi) & \cos(\theta) \sin(\psi) & \sin(\theta) \\ -\cos(\phi) \sin(\psi) + \cos(\psi) \sin(\phi) \sin(\theta) & \cos(\phi) \cos(\psi) + \sin(\phi) \sin(\theta) \sin(\psi) & -\cos(\theta) \sin(\phi) \\ -\cos(\phi) \cos(\psi) \sin(\theta) - \sin(\phi) \sin(\psi) & \cos(\psi) \sin(\phi) - \cos(\phi) \sin(\theta) \sin(\psi) & \cos(\phi) \cos(\theta) \end{bmatrix}$$

$$(2.4)$$

The above matrix is orthonormal. So we can have the rotation matrix from body coordinate to inertial coordinate by taking the transpose of $R_{E\to B}$.

$$R_{B\to E} = R_{E\to B}^T \tag{2.5}$$

And we have

$$R_{B \to E} = \begin{bmatrix} \cos(\psi)\cos(\theta) & -\cos(\phi)\sin(\psi) + \cos(\psi)\sin(\phi)\sin(\theta) & -\cos(\phi)\cos(\psi)\sin(\theta) - \sin(\phi)\sin(\psi) \\ \cos(\theta)\sin(\psi) & \cos(\phi)\cos(\psi) + \sin(\phi)\sin(\psi)\sin(\theta) & \cos(\psi)\sin(\phi) - \cos(\phi)\sin(\psi)\sin(\theta) \\ \sin(\theta) & -\cos(\theta)\sin(\phi) & \cos(\phi)\cos(\theta) \end{bmatrix}$$

$$(2.6)$$

Thus

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = R_{B \to E} \begin{bmatrix} x_b \\ y_b \\ z_b \end{bmatrix}$$
(2.7)

The Euler rates of the quadrotor is same as other aircrafts [18]. It can be used to determine the attitude of the quadrotor. The relation between the euler rates and the body angular rates is

$$\begin{bmatrix} p \\ q \\ r \end{bmatrix} = \begin{bmatrix} \dot{\phi} \\ 0 \\ 0 \end{bmatrix} + R_{\phi} \begin{bmatrix} 0 \\ \dot{\theta} \\ 0 \end{bmatrix} + R_{\phi} R_{\theta} \begin{bmatrix} 0 \\ 0 \\ \dot{\psi} \end{bmatrix} = \Omega_{E \to B} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$
(2.8)

Then

$$\Omega_{E \to B} = \begin{bmatrix} 1 & 0 & \sin(\theta) \\ 0 & \cos(\phi) & -\sin(\phi)\cos(\theta) \\ 0 & \sin(\phi) & \cos(\theta)\cos(\phi) \end{bmatrix}$$
(2.9)

And

$$\Omega_{B\to E} = \Omega_{E\to B}^{-1} = \begin{bmatrix} 1 & \sin(\phi)\tan(\theta) & -\cos(\phi)\tan(\theta) \\ 0 & \cos(\phi) & \sin(\phi) \\ 0 & -\frac{\sin(\phi)}{\cos(\theta)} & \frac{\cos(\phi)}{\cos(\theta)} \end{bmatrix}$$
(2.10)

Finally

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \begin{cases} p + \sin(\phi) \tan(\theta)q - \cos(\phi) \tan(\theta)r \\ \cos(\phi)q + \sin(\phi)r \\ -\frac{\sin(\phi)}{\cos(\theta)}q + \frac{\cos(\phi)}{\cos(\theta)}r \end{cases}$$
(2.11)

2.2.3 Dynamics

According to Newton's second law of motion, the mass center motion kinematics equation of quadrotor is:

$$\frac{d(m\vec{V})}{dt} = \vec{F} \tag{2.12}$$

Thrust generated by each motor is T_i (i = 1, 2, 3, 4). So the **total thrust** is

$$T = T_1 + T_2 + T_3 + T_4 \tag{2.13}$$

The inverse torque required to generate **yaw moment** is generated by each motor. Where m_i (i = 1, 2, 3, 4). The total inverse torque generated by four motors is

$$\tau_{\psi} = m_1 + m_2 - m_3 - m_4 \tag{2.14}$$

The differential thrust generated by 4 motors generates **pitch moment** and **roll moment**. l is the distance between each motor and the center of the frame.

• Pitch Movement

For moving in positive x direction, the rotation speed of motor 1 and 3 is decreased and that of motor 2 and 4 is increased as shown in Figure 2.3



Figure 2.3: Pitch Movement

• Roll Movement

For moving in positive y direction, the rotation speed of motor 2 and 3 is decreased and that of motor 1 and 4 is increased as shown in Figure 2.4



Figure 2.4: Roll Movement

• Yaw Movement

For making quadrotor rotate around z axis in body frame, the rotation speed of motor 3 and 4 is decreased and that of motor 1 and 2 is increased as shown in Figure 2.5



Figure 2.5: Yaw Movement

And we have

$$\tau_{\theta} = \frac{\sqrt{2}}{2} l(T_1 + T_3 - T_2 - T_4) \tag{2.15}$$

Similarly

$$\tau_{\phi} = \frac{\sqrt{2}}{2} l(T_2 + T_3 - T_1 - T_4) \tag{2.16}$$

The air drag[19] related to ground coordinate system is

$$\begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix} = \begin{bmatrix} K_1 \dot{x} \\ K_2 \dot{y} \\ K_3 \dot{z} \end{bmatrix}$$
(2.17)

Then the dynamics equations of force is:

$$m\begin{bmatrix}\dot{v_x}\\\dot{v_y}\\\dot{v_z}\end{bmatrix} = mg\begin{bmatrix}0\\0\\-1\end{bmatrix} + R_{B\to E}T\begin{bmatrix}0\\0\\1\end{bmatrix} - \begin{bmatrix}K_1v_x\\K_2v_y\\K_3v_z\end{bmatrix}$$
(2.18)

So position movement of quadrotor can be expressed as:

$$\begin{bmatrix} \ddot{x} \\ \ddot{y} \\ \ddot{z} \end{bmatrix} = \begin{bmatrix} \dot{v_x} \\ \dot{v_y} \\ \dot{v_z} \end{bmatrix} = \begin{bmatrix} \frac{T_m}{m} (-\cos(\psi)\sin(\theta)\cos(\phi) - \sin(\psi)\sin(\phi)) - K_1 \dot{x} \\ \frac{T_m}{m} (\cos(\psi)\sin(\phi) - \sin(\psi)\sin(\theta)\cos(\phi)) - K_2 \dot{y} \\ \frac{T_m}{m} \cos(\phi)\cos(\theta) - g - K_3 \dot{z} \end{bmatrix}$$
(2.19)

The rotation kinematics equation of quadrotor is:

$$\frac{d(J\nu)}{dt} = M \tag{2.20}$$

And $J = diag[J_x, J_y, J_z]$ is quadrotor moments of inertia related to 3 axes of body coordinate system. M is the resultant moment applied on the quadrotor. $(M = \dot{H} + \nu \times H \text{ and } H = J\nu)$ External moments mainly consist of body torque and aerodynamic drag torque. Body torque (2.14) generated by rotors is:

$$\begin{bmatrix} \tau_{\phi} \\ \tau_{\theta} \\ \tau_{\psi} \end{bmatrix} = \begin{bmatrix} \frac{\sqrt{2}}{2}l(T_2 + T_3 - T_1 - T_4) \\ \frac{\sqrt{2}}{2}l(T_1 + T_3 - T_2 - T_4) \\ m_1 + m_2 - m_3 - m_4 \end{bmatrix}$$
(2.21)

Aerodynamic drag torque is:

$$\tau_{af} = K_{af}\nu\tag{2.22}$$

Where $K_a f = diag[k_{afx}, k_{afy}, k_{afz}]$. So dynamics equations of torque is
$$M = \begin{bmatrix} M_x \\ M_y \\ M_z \end{bmatrix} = \begin{bmatrix} \dot{p}J_x + qr(J_z - J_y) \\ \dot{q}J_y + pr(J_x - J_z) \\ \dot{r}J_z + pq(J_y - J_x) \end{bmatrix} = \begin{bmatrix} \tau_\phi - \tau_{afx} \\ \tau_\theta - \tau_{afy} \\ \tau_\psi - \tau_{afz} \end{bmatrix}$$
(2.23)

Then we have the equations of angular movement of the quadrotor

$$\begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} \frac{J_y - J_z}{J_x} qr + \frac{\tau_{\phi}}{J_x} - \frac{\tau_{afx}}{J_x} \\ \frac{J_z - J_x}{J_y} pr + \frac{\tau_{\theta}}{J_y} - \frac{\tau_{afy}}{J_y} \\ \frac{J_x - J_y}{J_z} pq + \frac{\tau_{\psi}}{J_z} - \frac{\tau_{afz}}{J_z} \end{bmatrix}$$
(2.24)

Then we can get the whole nonlinear quadrotor rigid body dynamics

$$\dot{\mathbf{X}} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \dot{y} \\ \dot{z} \\ \dot{v}_x \\ \dot{v}_y \\ \dot{v}_z \\ \dot{\phi} \\ \dot{\phi$$

which is a non-linear system. We need to linearize the quadrotor kinematics and rigid body dynamics at a near-hover state where ϕ , θ and ψ are close to zero.

2.3 Actuator Model

The aerodynamic force and moment are obtained by combining the momentum theory of the blade element. The torque and the force generated by each rotorpropeller are proportional to the square of the propeller speed as

$$T_i = C_T \frac{4\rho_a R^4}{\pi^2} \Omega_i^2 \tag{2.26}$$

$$m_i = C_Q \frac{4\rho_a R^5}{\pi^3} \Omega_i^2 \tag{2.27}$$

Where ω_m is rotor rotation speed, ρ_a is the air density, R is the propeller radius, C_T is the thrust factor, and C_Q is the momentum factor. We simplify these equations as

$$T_i = b\Omega_i^2 \tag{2.28}$$

$$m_i = d\Omega_i^2 \tag{2.29}$$

Assume the voltage input is u, the current is I, and the rotational speed of rotor of each motor is Ω_i . According to Kirchhoff laws, we can get

$$L\frac{di}{dt} = u - RI - K_e \Omega_i \tag{2.30}$$

R is the equivalent resistance of the motor, L is equivalent inductance of the motor, and K_e is voltage coefficients.

torque equilibrium equation during rotation is

$$L\frac{d\Omega_i}{dt} = k_m i - d\Omega_i^2 \tag{2.31}$$

J is the equivalent moment of inertia of motor. τ_m is motor torque and τ_d is loading torque. L is negligible because we are using small brushless motor. Then we can get approximate motor dynamic model.

$$\dot{\Omega}_i = \frac{K_m K_e}{RJ} \Omega_i - \frac{d}{j} \Omega_i^2 + \frac{K_m}{RJ} u$$
(2.32)

Use taylor expansion, remove high-order terms, keep the first-order term. we can get the linearized equation.

$$\dot{\Omega}_i = -A\Omega_i + Bu + C \tag{2.33}$$

Then

$$\frac{\Omega(s)}{u} = \frac{z_{vol}}{s+a} \tag{2.34}$$

In practical use, we cannot directly read the voltage as the input of the brushless motor. The ESC of each actuator set only accept PWM signal as command. By curve fitting in Chapter 3, we can have the mapping from PWM signal to desired motor speed Ω^* which includes the mapping from PWM signal to input voltage u and that from input voltage u to desired motor speed Ω^* . The transfer function between desired motor speed Ω^* and actual motor speed Ω can be presented as a first-order low-pass filter.

$$\frac{\Omega(s)}{\Omega^*(s)} = \frac{a}{s+a} \tag{2.35}$$

2.4 Linearization

• Linearization of rigid-body dynamics

The non-linear rigid-body dynamics is represented as

$$\dot{\mathbf{X}}_{rig} = f(\mathbf{X}_{rig}, \mathbf{U}_{rig}) \tag{2.36}$$

Where

$$\mathbf{X}_{rig} = \begin{bmatrix} \boldsymbol{\xi} \\ \mathbf{V} \\ \boldsymbol{\Theta} \\ \boldsymbol{\nu} \end{bmatrix} = \begin{bmatrix} \boldsymbol{x} \\ \boldsymbol{y} \\ \boldsymbol{z} \\ \boldsymbol{v}_{x} \\ \boldsymbol{v}_{y} \\ \boldsymbol{v}_{z} \\ \boldsymbol{v}_{y} \\ \boldsymbol{v}_{z} \\ \boldsymbol{\phi} \\ \boldsymbol{\phi} \\ \boldsymbol{\theta} \\ \boldsymbol{\psi} \\ \boldsymbol{p} \\ \boldsymbol{q} \\ \boldsymbol{r} \end{bmatrix}$$
(2.37)

And

$$\mathbf{U}_{rig} = \begin{bmatrix} U_1 \\ U_2 \\ U_3 \\ U_4 \end{bmatrix} = \begin{bmatrix} T \\ \tau_{\phi} \\ \tau_{\theta} \\ \tau_{\psi} \end{bmatrix}$$
(2.38)

 \mathbf{X}_{rig} represents the state vector and \mathbf{U}_{rig} represents the input vector. Trim Points are $\mathbf{X}_0 = [0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0]$ and $\mathbf{U}_0 = [mg, 0, 0, 0]^T$. Then we have

$$f(\mathbf{X}_{equil}, \mathbf{U}_{equil}) = 0 \tag{2.39}$$

Based on [20], The linear equation can be represented as

$$\delta \dot{\mathbf{X}} = A \delta \mathbf{X} + B \delta \mathbf{U} \tag{2.40}$$

The characteristic matrix \boldsymbol{A} and the input matrix \boldsymbol{B} can be calculated from

$$A = \frac{\delta f}{\delta \mathbf{X}} |_{\mathbf{X} = \mathbf{X}_{equil}, \mathbf{U} = \mathbf{U}_{equil}}$$
(2.41)

$$B = \frac{\delta f}{\delta \mathbf{U}} |_{\mathbf{X} = \mathbf{X}_{equil}, \mathbf{U} = \mathbf{U}_{equil}}$$
(2.42)

Then we have

	0	0	0	1	0	0	0	0	0	0	0	0	
	0	0	0	0	1	0	0	0	0	0	0	0	
	0	0	0	0	0	1	0	0	0	0	0	0	
	0	0	0	$-K_1$	0	0	0	-g	0	0	0	0	
	0	0	0	0	$-K_2$	0	g	0	0	0	0	0	
4 —	0	0	0	0	0	$-K_3$	0	0	0	0	0	0	(2.13)
л —	0	0	0	0	0	0	0	0	0	1	0	0	(2.40)
	0	0	0	0	0	0	0	0	0	0	1	0	
	0	0	0	0	0	0	0	0	0	0	0	1	
	0	0	0	0	0	0	0	0	0	$-K_4$	0	0	
	0	0	0	0	0	0	0	0	0	0	$-K_5$	0	
	0	0	0	0	0	0	0	0	0	0	0	$-K_6$	

And

Then we have the linearized quadrotor rigid-body dynamics

$$\dot{\mathbf{X}}_{rig} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \dot{y} \\ \dot{z} \\ \dot{v}_x \\ \dot{v}_y \\ \dot{z} \\ \dot{v}_x \\ \dot{v}_y \\ \dot{v}_z \\ \dot{v}_y \\ \dot{v}_z \\ \dot{v}_y \\ \dot{v}_z \\ \dot{v}_y \\ \dot{v}_z \\ \dot{\phi} \\ \dot{$$

• Linearization of actuator dynamics

The full actuator model is shown in Figure 2.6. Obviously we have $\mathbf{U}_{act} = [T, \tau_{\phi}, \tau_{\theta}, \tau_{\psi}]^{T}$.



Figure 2.6: Full Actuator Dynamics

Here we use simulink toolbox shown in Figure 2.7 to linearized the nonlinear actuator dynamic model. The trim points are $U_0^* = [mg, 0, 0, 0]^T$, $U_0 = [mg, 0, 0, 0]^T$ and $\omega_1 = \omega_2 = \omega_3 = \omega_4 = 842.99 rad/s$ (Optimization Method: Gradient Descent with Elimination; Algorithm: Active-Set).



Figure 2.7: Using Simulink Toolbox

And we get the linearized actuator dynamic model in Figure 2.8



Figure 2.8: Linearized Actuator Dynamics

With $\mathbf{U}_{act}^* = [T^*, \tau_{\phi}^*, \tau_{\theta}^*, \tau_{\psi}^*]^T$, linearized actuator model (state space represented)

tation) can be written as:

$$\dot{\mathbf{U}}_{act} = -a\mathbf{I}_{4\times4}\mathbf{U}_{act} + a\mathbf{I}_{4\times4}\mathbf{U}_{act}^* \tag{2.46}$$

• Whole Quadrotor Linearized Model

Combining the linearized quadrotor rigid body dynamic model and the linearized acutator model. Assuming all drag coefficients are zero, the whole quadrotor linearized model (state space representation) is shown below:

$$\dot{\mathbf{X}} = \begin{bmatrix} \mathbf{I}_{3\times3} & \mathbf{0}_{3\times13} \\ \mathbf{0}_{1\times3} & -g & \mathbf{0}_{1\times12} \\ \mathbf{0}_{1\times4} & g & \mathbf{0}_{1\times11} \\ \mathbf{0}_{1\times12} & \frac{1}{m} & \mathbf{0}_{1\times3} \\ \mathbf{0}_{3\times6} & \mathbf{I}_{3\times3} & \mathbf{0}_{3\times7} \\ \mathbf{0}_{3\times9} & diag[\frac{1}{J_x}, \frac{1}{J_y}, \frac{1}{J_z}] & \mathbf{0}_{3\times4} \\ \mathbf{0}_{4\times12} & -a\mathbf{I}_{4\times4} \end{bmatrix} \mathbf{X} + \begin{bmatrix} \mathbf{0}_{12\times4} \\ a\mathbf{I}_{4\times4} \end{bmatrix} \mathbf{U}$$
(2.47)

Chapter 3

PARAMETERS MEASUREMENT AND HARDWARE IMPLEMENTATIONS

3.1 Introduction and Overview

This chapter is illustrates measurement of quadrotor rigid-body and actuator parameters with bifilar pendulum and propulsion system test. Also the design of the MARK3 flight controller and the general frame structure of hardware and software are presented.

3.2 Airframe Size, Mass and Moment Measurement

3.2.1 Airfame Size

Due to the limitation of volume of indoor test area, we choose 250mm quadrotor frame as the quadrotor airframe which is made of carbon fiber with good sturdiness and light weight. As shown in Figure 3.1, the distance from center of frame to the each motor l = 0.125m.



Figure 3.1: 250 quadrotor frame

Apparently, the declared size of the quadrotor on market represents the diagonal distance between the two motors on each arm of the frame which is equivalent to twice of l.

3.2.2 Mass and Moment Measurement

The moment of intertia of the quadrotor is obtained from bifilar pendulum experiment [21], where for each axis, the moment of inertia J, can be computed by measuring the period of twist oscillation with the experimental stand setup shown in figure 3.2



Figure 3.2: The bifilar pendulum experiment for three body axis

the equation used to compute the moment of inertia is

$$J = \frac{mgT^2L_1^2}{4\pi^2 L_2} \tag{3.1}$$

where T is the period of each oscillation. The free oscillation can be regard as simple harmonic motion because amplitude of the swing of the quadrotor rigid body is small. To improve the accuracy, the averaged period from 100 oscillations is obtained from the flight controller board by checking the plus-minus sign of the gyroscope output. And L_1 , L_2 is indicated in figure. The result obtained from the bifilar pendulum experiment mass measurement is shown in the Table 3.1.

Parameters	Definition	Nominal Values
J_x	Moment of Inertia in x axis	$0.0019005 \ kg * m^2$
J_y	Moment of Inertia in y axis	$0.0019536 \ kg * m^2$
J_z	Moment of Inertia in z axis	$0.0036894 \ kg * m^2$
m	Mass	$0.551 \ kg$

Table 3.1: Moment of inertia experiment results

Obviously, the moment of inertia in x axis has very small quantitative difference with that in y axis. But that in z axis are much bigger than the others. This will be discussed in Chapter 4.

3.3 Propulsion System Test

Based on Chapter 2, we must know torque coefficient, thrust coefficient and constant of actuator dynamics in the first-order transfer function. With the help of Dynamometer Series 1580 in Figure 3.3 from RCbenchmark, we can get all these numbers easily. Also, the mapping between the desired motor rotation speed and PWM signal is also needed for programming the firmware of MARK3 flight controller.



Figure 3.3: Dynamometer Series 1580

3.3.1 Thrust Coefficient and Torque Coefficient Measurement

The Dynamometer Series 1580 test stand is connected with an upper computer to transfer data and commands. By changing duty ratio of PWM on the Snail actuator Set, the test stand can adjust motor rotation speed automatically.



Figure 3.4: Actuator Test Equipment Structure and GUI

As shown in Figure 3.4, the structure of the whole test equipment and the software interface are presented. The test stand can identify real-time thrust and torque with three sets of piezoresistive pressure sensors. The rotation speed is read through the change of the voltage on one phase of the brushless motor. Then we can have the thrust coefficient b and the torque coefficient d.

From the curve fitting in Figure 3.5, we get $b = 1.91 \times 10^{-6} N s^2 / rad^2$.



Figure 3.5: Thrust vs Motor Rotation Speed Fitting Curve

From the curve fitting in Figure 3.6, we get $d = 2.47 \times 10^{-8} Nm s^2/rad^2$.



Figure 3.6: Torque vs Motor Rotation Speed Fitting Curve

Then we need to find the mapping between motor rotation speed and PWM signal. According to [16], since we use electronic speed controllers that control the percentage of input voltage, the resulting motor rotation speed for a given PWM command depends on the battery voltage. The voltage compensation is also needed for motor speed mapping. By performing motor speed and PWM mapping identifications with different voltaged wich are controlled by a power supply unit, we can find a linear function to represent the 3-D curve fitting.



Figure 3.7: PWM vs Motor Rotation Speed vs Battery Voltage

The mapping is presented in Figure 3.7 with the equation (ϵ is PWM signal, ω is motor rotation speed and u_{bat} is battery voltage):

$$\epsilon = \frac{\omega^2 + a_1 \omega + a_2}{a_3 u_{bat} + a_4} + a_5 \tag{3.2}$$

From the curve fitting, we have $a_1 = 5393$, $a_2 = 29960$, $a_3 = 1166$, $a_4 = 1544$ and $a_5 = 895$. This PWM-speed mapping with battery compensation ensures the PWM commands are calculated for motors when given the output of controllers in angular rate loop and vertical velocity loop.

To identify the pole of first-order linearized actuator dynamics, step response experiment is performed. The open-loop pole a is estimated using MATLAB Ident toolbox.



Figure 3.8: Actuator Pole Identification Curve

The identification result is shown in Figure 3.8 when a = 9.79 (the pole from the actuator dynamics mentioned in Chapter 2) with 92% fitness. This actuator model based system identification accurately reflects actual characteristic.

3.4 Design of the Flight Controller

The flight controller consists of a Microcontroller Unit, an MEMS sensor board, a Communication Module, and external IOs. The flight controller is responsible for executing communication protocol, state estimation, control and ESC command inputs. To simplify the software design, a microprocessor was needed with sufficient computational power for heavy load of floats computation.



Figure 3.9: Block Diagram of Mark3 Flight Controller

The design of the flight controller is shown in Figure 3.9. The Cortex-M4 MK20DX256 32 bit which can be overclocked to 168MHz offers large flash space, large RAM space, USB interface, low per unit cost and hardware simplicity. The GY-89 10DOF Sensor Board gives enough design redundancy of onboard sensing. The I2C port gives up to 1000Hz data transfer rate to ensure the rate of inner-loop control (angular rate). To ensure the normal power supply of all the on-board modules and peripheral devices, a 5v-3.3v regulator and an I2C logic converter are added. Additional headers are also reserved on this flight controller for more peripheral devices (High-level Embedded System, Other Sensor Boards, etc) in the future. The Schematic Print and the Composite Drawing of the *MARK3* flight controller are presented in Appendix B.



Figure 3.10: Mark3 Flight Controller Photo

The assembled design photo is shown in Figure 3.10

3.5 General Frame Structure of Hardware & Software

The Quadrotor Platform Electrical Architecture. The block diagram of the quadrotor platform electrical architecture is presented in Figure 3.11. Total 4 Electronic Speed Controllers are connected with the pin headers on the *MARK3* flight controller to receive the PWM command from the flight controller. The flight controller is powered by the 5v source on the Matex Power Distribution Board. The Distribution Board also powers all four ESCs with the voltage from the 3S Lipo Battery of which the safe voltage ranges from 10.2v to 12.6v. The flight controller reads battery voltage with a certain header while the $10.2v \sim 12.6v$ battery voltage is being converted to $2.04 \sim 2.52v$ which is suitable for an analog pin of Teensy 3.2 MCU.



Figure 3.11: The Quadrotor Platform Electrical Architecture

The remote receiver is connected via S.BUS Header to receive and send receiver (RX) and transmitter (TX) protocols. A reserved UART header is for connection between the high-level embedded system which will be used for research in the future.

The Flight Controller Softeware Architecture. The block diagram of the flight controller software architecture is presented in Figure 3.12. The software was implemented in two separate threads. The on-board sensor data collection, angular rate control, ESC output and loop checking are updated at 400 Hz. Communication process, state estimator, position & velocity control and attitude control are updated at 100 Hz where they are distributed in 4 loops of 400-Hz software main loop.



Figure 3.12: The MARK3 Flight Controller Software Architecture

The Experimental System Hardware Architecture. The block diagram of the experimental system hardware architecture is presented in Figure 3.12. The motion capture system consists of HTC VIVE Tracking System (Two Lighthouse 1.0 Basestaions and some HTC VIVE Trackers) and a high-performance desktop equipped



with a CPU not lower than Intel i5-4590 and a GPU not lower than Nvidia GTX970.

Figure 3.13: The Experimental System Hardware Architecture

The HTC VIVE tracker transmitt full-state data via a WIFI Dongle. Here a GUI Programmed in MATLAB gets data from SteamVR API and send the serial data packet to the host Xbee 3.0 module. Then the extension Xbee 3.0 module on the MARK3 will receive the serial packet. The transmitter is standby during flight for manual control in case that accident happens (communication loss with the upper computer, collision, etc).

Chapter 4

ANALYSIS OF LINEAR MODEL

4.1 Angular Movement Analysis

Based on Chapter 2, we get the linearized model of the whole quadrotor model including actuator dynamics. Given above, the associated transfer function matrix is given by

$$P = C(sI - A)^{-1}B + D (4.1)$$

Then

$$P_{rate} = \begin{bmatrix} \frac{p}{\tau_{\phi}^{*}} & 0 & 0\\ 0 & \frac{q}{\tau_{\theta}^{*}} & 0\\ 0 & 0 & \frac{r}{\tau_{\psi}^{*}} \end{bmatrix} = \begin{bmatrix} \frac{a}{J_{x}s(s+a)} & 0 & 0\\ 0 & \frac{a}{J_{y}s(s+a)} & 0\\ 0 & 0 & \frac{a}{J_{z}s(s+a)} \end{bmatrix}$$
(4.2)

Clearly the angular rate linearized model is decoupled. We can also get the block diagram of the angular rate model in Figure 4.1



Figure 4.1: Angular Rate Plant Diagram

From the measured parameter values in Chapter 3, we obtain the transfer functions with numerical values below. For these nominal parameter values, we obtain the following numeriacal SISO transfer functions including:

Roll Rate

$$P_p = \frac{p}{\tau_{\phi}^*} = \frac{5151.28}{s(s+9.79)} \tag{4.3}$$

Pitch Rate

$$P_q = \frac{q}{\tau_{\theta}^*} = \frac{5011.26}{s(s+9.79)} \tag{4.4}$$

Yaw Rate

$$P_r = \frac{r}{\tau_{\psi}^*} = \frac{2653.55}{s(s+9.79)} \tag{4.5}$$



Figure 4.2: Angular Rate Movement Bode Plot

Firstly bode frequency response plot for the angular rate plant is presented in Figure 4.2. Obviously dynamics of pitch angular movement and roll angular movement resemble. To generate same angular acceleration, yaw angular movement requires more torque than that of pitch angular movement and roll angular movement because the moment inertia in x and y body axis is smaller than that in z body axis.



Figure 4.3: Motor Speed vs Torque in Body Frame

Secondly in Figure 4.3, to get same value of body torque from all 4 motors when the quadrotor is near hovering mode (T = mg), torque for yaw angular movement requires much more maximum motor speed than that for pitch angular movement and roll angular movement. The reason is that the actuator torque coefficient $(d = 2.47 \times 10^{-8} Nm s^2/rad^2)$ is much smaller than the combined actuator thrust factor $(\frac{\sqrt{2}}{2}bl = 1.69 \times 10^{-7} Nm s^2/rad^2)$.

Based on the above two points, we know that the designed bandwidth for yaw angular movement should be smaller than that for pitch angular movement and roll angular movement. With an integral item, we can have attitude presented in the whole angular movement block diagram of the linearized model in Figure 4.4.



Figure 4.4: Angular Movement Plant Diagram

The control design of angular movement is presented in Chapter 4 with cascade structure. This model is applied in the flight controller firmware when quadrotor flying near hovering mode (ϕ and θ are not big).

4.2 Vertical Movement Analysis

The structure of vertical movement (vertical velocity and altitude) model is same as that of attitude movement shown in Figure 4.5

$$\xrightarrow{T^{*}} \overbrace{(s+a)}^{g} \xrightarrow{T} \overbrace{\frac{1}{m}}^{g} \xrightarrow{v_{z}} \overbrace{\frac{1}{s}}^{z} \xrightarrow{z} \xrightarrow{T} \overbrace{\frac{1}{s}}^{z}$$

Figure 4.5: Vertical Movement Plant Diagram

The linearized model is designed for simulation. Even though the quadrotor is near hovering mode, we still need to add nonlinear constraint to the vertical velocity controller output in the flight controller firmware [22] due to the nonlinearity in the real world:

$$T_{act}^* = \frac{T^*}{\cos(\phi)\cos(\theta)} \tag{4.6}$$

where T_{act} is the real input value of motor driver in the firmware.

4.3 Translational Movement Analysis

The structure of translational movement (translational velocity and position) model is presented in Figure 5.35



Figure 4.6: Translational Movement Plant Diagram

Similarly the linearized model is designed for simulation. We need to add nonlinear constraint to the translational velocity controller output in the flight controller firmware due to the nonlinearity in the real world. We have:

$$a = \cos(\psi) \tag{4.7}$$

$$b = \sin(\psi) \tag{4.8}$$

$$c_1 = mT\theta^* \tag{4.9}$$

$$c_2 = mT\phi^* \tag{4.10}$$

And finally we have:

$$\phi_{act}^* = asin(ac_2 - bc_1) \tag{4.11}$$

and

$$\theta_{act}^* = asin(-(ac_1 + bc_2)/cos(\theta^*)) \tag{4.12}$$

where θ_{act}^* and ϕ_{act}^* is the real input value of attitude controller in the firmware.

4.4 Summary and Conclusion

Based the model analysis above, attitude control and vertical movement control will have the similar structure. But the maximum available bandwidth is limited by the actuator output in different channels. In the next chapter, the full-state control design is illustrated based on this model analysis.

Chapter 5

CONTROL DESIGN METHODS AND SIMULATIONS

5.1 Introduction and Overview

In this chapter, we describe how to design controller with full-state feedback for this quadrotor platform equipped with the *MARK3* flight controller. The attitude/angularrate control has been designed with control parameter trader off. The altitude/verticalvelocity and translational position/velocity are presented and analyzed. The underlying theory for each controller is explained and justified.

5.2 Angular Movement Cascade Control

5.2.1 Angular Rate Control

In this section, we describe (p, q, r) angular rate control for this quadrotor platform equiped with the *MARK3* flight controller. The angular velocity of the quadrotor is from gyroscope. The frequency of angular rate control in the firmware is 400Hz.

Control Design: PD Controller. We focus on roll angular movement first. The block diagram of close loop angular rate control is shown in Figure 5.1.



Figure 5.1: Close Loop Diagram of Angular Rate Control

Based on the model obtained from the previous section

$$P_p = \frac{p}{\tau_{\phi}^*} = \frac{5151.28}{s(s+9.79)} \tag{5.1}$$

we design a PD controller

$$K_p = g(s+z) \tag{5.2}$$

This K_p will be used to generate input of motor driver in the firmware of the *MARK3* flight controller. This PD controller will place the dominant closed loop pole near

$$s = 9.79$$
 (5.3)

The open loop transfer function L_p is given by

$$L_p = P_p K_p = g(s+z) \frac{5151.28}{s(s+9.79)}$$
(5.4)

In this case $k_p = g$ and $k_d = gz$.

Open Loop *L* **Analysis.** Figure 5.2 and Figure 5.3 show the plots of $L_p = P_p K_p$ for specific (g, z) variations.



Figure 5.2: Open Loop Bode Plot When changing g



Figure 5.3: Open Loop Bode Plot When changing z

- increasing g increases magnitude of L and increasing z increase magnitude of L at low frequencies
- increasing g impacts the crossover proportionately and increasing z doesnn't impact the crossover much
- increasing g doesn't impact phase of L and increasing z impacts phase of L clearly at the frequencies near z

Sensitivity (T_{d_oy}) . The sensitivity bode plot is presented in Figure 5.4 and Figure 5.5



Figure 5.4: Sensitivity Bode Plot When changing g



Figure 5.5: Sensitivity Bode Plot When changing z

- increasing g results smaller magnitude of S at low frequencies
- increasing z results smaller magnitude of S at low frequencies but increases peak sensitivity
- peak sensitivities do not bring much change with increasing z

Complementary Sensitivity (T_{ry}) . The complementary sensitivity bode plot is presented in Figure 5.6 and Figure 5.7



Figure 5.6: Complementary Sensitivity Bode Plot When changing g



Figure 5.7: Complementary Sensitivity Bode Plot When changing z

- increasing g results larger bandwidth
- increasing z results larger peak complementary sensitivity

The z value in roll, pitch and yaw angular rate controller is same. As discussed in Chapter 4, the g value for yaw angular rate should be smaller than that of roll and pitch angular movement because of more needed motor speed to generate enough torque for yaw movement.

Input Disturbance to Output T_{d_iy} (PS). The input disturbance to output bode plot is presented in Figure 5.8 and Figure 5.9



Figure 5.8: Input Disturbance to Output Bode Plot When changing g



Figure 5.9: Input Disturbance to Output Bode Plot When changing z
- increasing g reduces magnitude at low frequencies
- increasing z reduces magnitude at low frequencies with a little peak

Reference to Control T_{ru} . The reference to control bode plot is presented in Figure 5.10 and Figure 5.11



Figure 5.10: Reference to Control Bode Plot When changing g



Figure 5.11: Reference to Control Bode Plot When changing z

Based on the Figures above:

- increasing g increases magnitude at high frequencies
- increasing z results larger peak in T_{ru}

Sensor Noise to Output T_{ny} (T_{d_iu}). The sensor noise to output bode plot is presented in Figure 5.12 and Figure 5.13



Figure 5.12: Sensor Noise to Output Bode Plot When changing g



Figure 5.13: Sensor Noise to Output Bode Plot When changing z

Based on the Figures above:

- increasing g increases magnitude at high frequencies
- increasing z results larger peak in T_{ny}

Sensor noise is the main issue limits the angular movement bandwidth. Increasing g brings not only higher bandwidth but also much more noise at higher frequencies. The value g = 0.0045 is obtained from actual experiment with the quadrotor fixed on the test stand based on trade-off of complementary sensitivity and sensor noise to output.

Output Disturbance to Control T_{d_ou} . The output disturbance to control bode plot is presented in Figure 5.14 and Figure 5.15



Figure 5.14: Output Disturbance to Control Bode Plot When changing g



Figure 5.15: Output Disturbance to Control Bode Plot When changing z

Based on the Figures above:

- increasing g increases magnitude at high frequencies in T_{d_ou}
- increasing z results larger peak in T_{d_ou}

Step Response. The step response is presented in Figure 5.16 and Figure 5.17



Figure 5.16: Step Response When changing g



Figure 5.17: Step Response When changing \boldsymbol{z}

Based on the Figures above:

- increasing g reduces settling time
- increasing z reduces rising time but brings more overshoot when z is bigger than the actuator constant a = 9.79

Roll-off Term. To reduce effect of high frequency noise in the feedback loop, roll-off term is needed to added with cut-off frequency at 10 times of control bandwidth. The roll-off term is

$$K_{rolloff1} = \frac{220^2}{(s+220)^2} \tag{5.5}$$

The angular rate controller provides good tracking and disturbance rejection. This design corresponds to a LQR controller considering the dynamics of the angular rates and torque in three-axis [4]. Considering a subsystem containing the body rates and body torques as state, it leads to the system like this $(\mathbf{J} = diag[1/J_x, 1/J_y, 1/J_z]^T,$ $\nu = [p, q, r]^T$ as angular rate, $\tau = [\tau_{\phi}, \tau_{\theta}, \tau_{\psi}]^T$ as torque in three-axis coordinate system and $\tau^* = [\tau_{\phi}^*, \tau_{\theta}^*, \tau_{\psi}^*]^T$ as desired torque)

$$R_{\psi} = \begin{bmatrix} \dot{\nu} \\ \dot{\tau} \end{bmatrix} = \begin{bmatrix} \mathbf{0} & \mathbf{J}^{-1} \\ \mathbf{0} & -a\mathbf{I}_3 \end{bmatrix} \begin{bmatrix} \nu \\ \tau \end{bmatrix} + \begin{bmatrix} \mathbf{0} \\ a\mathbf{I}_3 \end{bmatrix} \tau^*$$
(5.6)

where an infinite-horizon LQR control law $\mathbf{u} = -\mathbf{K}_{lqr}\mathbf{s}$ that minimizes the cost function

$$\int \mathbf{s}^T \mathbf{Q} \mathbf{s} + \mathbf{u}^T \mathbf{R} \mathbf{u}$$
(5.7)

Where **Q** is a diagonal weight matrix and **R** is the identity matrix. The solution to the formulated LQR problem is a gain matrix of the form (presented with (g, z) in the PD controller)

$$\mathbf{K}_{lqr} = \begin{bmatrix} g_p z_p & 0 & 0 & J_x g_p & 0 & 0 \\ 0 & g_q z_q & 0 & 0 & J_y g_q & 0 \\ 0 & 0 & g_r z_r & 0 & 0 & J_z g_r \end{bmatrix}$$
(5.8)

Finally, we choose $K_p = K_q = 0.0045(s + 12)$ as the p and q angular rate controller given that the closed loop poles are at [(-16.17, 3.02), (-16.17, -3.02)] and the only zero is at (-12, 0). The step response settling time is 0.12s (1.2% overshoot).

Based on the modeling analysis in Chapter 4, the bandwidth of yaw movement control should be much smaller than that for pitch and roll movement. Here I choose $K_r = 0.0012(s + 12)$ as the r angular rate controller. The open loop root locus for angular rate control is presented in Figure 5.18:



Figure 5.18: Angular Rate Control Open Loop Root Locus

The closed loop poles of yaw angular rate control are at [(-8.45, 0), (-4.52, 0)] and the only zero is at (-12, 0). The step response settling time is 0.93s (0% overshoot).

5.2.2 Attitude Cascade Control

In this section, we describe (ϕ, θ, ψ) attitude control for this quadrotor platform equiped with the *MARK3* flight controller. The attitude of the quadrotor is from attitude state estimation (fusion of gyroscope, accelerometer and MOCAP). The frequency of attitude control in the firmware is 100Hz.

Control Design: Proportional Controller. Pitch and roll control of quadrotor is almost same. The block diagram of close loop angular rate control is shown in Figure 5.19.



Figure 5.19: Close Loop Diagram of Attitude Control

Based on the close loop structure obtained from the previous section

$$T_{p^*\phi} = \frac{\phi}{p^*} = \frac{22.55s + 276}{s^3 + 32.34s^2 + 270.6s}$$
(5.9)

we design a P controller

$$K_{\phi} = k_p \tag{5.10}$$

This k_p will be used to generate input of angular rate control in the firmware of the MARK3 flight controller. The open loop transfer function L_p is given by

$$L_{\phi} = P_{\phi}K_{\phi} = K_{\phi}\frac{22.55s + 276}{s^3 + 32.34s^2 + 270.6s}$$
(5.11)

Then we have the open loop root locus of L = PK in Figure 5.20



Figure 5.20: Open Loop Root Locus of Attitude Control

The complimentary sensitivity of attitude control is presented in Figure 5.21



Figure 5.21: Complimentary Sensitivity of Attitude Control when k_p changes

The sensitivity of attitude control is presented in Figure 5.22



Figure 5.22: Sensitivity of Attitude Control when k_p changes

The sensor noise to output of attitude control is presented in Figure 5.23



Figure 5.23: Sensor Noise to Output of Attitude Control when k_p changes

The step response of attitude control is presented in Figure 5.24



Figure 5.24: Step Response of Attitude Control when k_p changes

From the above figures, we have seen that as the angular rate loop is well tuned, we just need find the largest value of K_{ϕ} to ensure the possible maximum attitude loop bandwidth. And finally I have $K_{\phi} = K_{\theta} = 9$. The step response settling time is 0.26s (0% overshoot). The closed loop poles are at [(-11.43, 11.23), (-11.43, -11.23), (-9.48, 0)] and the only zero is at (-12, 0). Similarly, I can have the yaw attitude controller $K_{\psi} =$ 2. And the closed loop poles of yaw control are at [(-8.95, 0), (-2.01, 2.12), (-2.01, -2, 12)] and the only zero is at (-12, 0) with that the settling time of step response is 1.58s (0% overshoot).

5.3 Vertical Movement Cascade Control

The vertical movement of quadrotor has the same structure with attitude movement. So we can use the same idea to design vertical movement cascade control. The block diagram is shown in Figure 5.25.



Figure 5.25: Close Loop Diagram of Vertical Movement Control

5.3.1 Vertical Velocity Control

We can use the same idea from design of angular rate control with pole placement to design a PD controller. The vertical velocity of the quadrotor is from state estimation (fusion of accelerometer and MOCAP). The frequency of vertical control in the firmware is 100Hz. The open loop transfer function L_{v_z} is given by

$$L_{v_z} = P_{v_z} K_{v_z} = g(s+z) \frac{15.18}{s(s+9.79)}$$
(5.12)

With z = 12, we have the complimentary sensitivity of vertical velocity control is presented in Figure 5.26



Figure 5.26: Complimentary Sensitivity of Vertical Velocity Control when g changes

It is clear to see the bandwidth of vertical velocity control increases as we increase g and the maximum bandwidth is limited by sensor noise. We can also the sensiticity plot presented in Figure 5.27



Figure 5.27: Sensitivity of Vertical Velocity Control when g changes

And we have sensor noise to output in Figure 5.28



Figure 5.28: Sensor Noise to Output of Vertical Velocity Control when g changes

The step response of attitude control is presented in Figure 5.29



Figure 5.29: Step Response of Vertical Velocity Control when g changes

Finally, we have $K_{v_z} = 0.525(s + 12)$ as the finalized vertical velocity controller. The closed loop poles are at [(-8.88, 4.10), (-8.88, -4.10)] and the only zero is at (-12, 0). The settling time of step response is 0.34s (0.34% overshoot).

5.3.2 Altitude Control

The altitude of the quadrotor is from state estimation (sensor fusion of accelerometer and MOCAP). The frequency of altitude control in the firmware is 100Hz. The altitude plant transfer function P_z is given by

$$P_z = \frac{7.969s + 95.62}{s^3 + 17.76s^2 + 95.62s} \tag{5.13}$$

Similar as attitude control, we can use proportional control as the altitude controller. We have the open loop root locus of L = PK in Figure 5.30



Figure 5.30: Open Loop Root Locus of Altitude Control

The complimentary sensitivity of altitude control is presented in Figure 5.31



Figure 5.31: Complimentary Sensitivity of Altitude Control when k_p changes

The sensitivity of altitude control is presented in Figure 5.32



Figure 5.32: Sensitivity of Altitude Control when k_p changes

The sensor noise to output of altitude control is presented in Figure 5.33



Figure 5.33: Sensor Noise to Output of Altitude Control when k_p changes

The step response of altitude control is presented in Figure 5.34



Figure 5.34: Step Response of Altitude Control when k_p changes

From the above figures, we have seen that as the angular rate loop is well tuned, we just need find the largest value of K_z to ensure the possible maximum attitude loop bandwidth. And finally we have $K_z = 4.2$. The closed loop poles are at (-7.82, 0), (-4.9708, 5.16) and (-4.9708, -5.16) and the only zero is at (-12, 0). Besides, the input command of vertical movement control is designed with saturation for flight safety. So design of altitude control law has more conservation than that of attitude control.

5.4 Translational Movement Cascade Control

After the design of attitude cascade control, we can achieve full-state control on translational movement with help of the HTC VIVE Tracking System. The block diagram of translational movement cascade control is shown in Figure 5.35.



Figure 5.35: Close Loop Diagram of Translational Movement Cascade Control

5.4.1 Translational Velocity Control

In this section, we describle (V_x, V_y) Translational control for this quadrotor platform equiped with the *MARK3* flight controller. The velocity of the quadrotor is from state estimation (sensor fusion of accelerometer and MOCAP). The frequency of translational control in the firmware is 100Hz.

Control Design: PD Controller. Based on the previous section we have the plant model including attitude control close loop, a $g_{gravity}$ factor and an integral item

$$P_{v_y} = \frac{1989s + 23874}{s^4 + 32.34s^3 + 473.6s^2 + 2435s}$$
(5.14)

We have the open loop root locus of L = PK in Figure 5.36 $(K_{vy} = 0.038(s + 20))$



Figure 5.36: Open Loop Root Locus of Translational Velocity Control

The CF of translational velocity control is presented in Figure 5.37



Figure 5.37: Complimentary Sensitivity of Translational Velocity Control when g changes

The sensitivity of translational velocity is presented in Figure 5.38



Figure 5.38: Sensitivity of Translational Velocity Control when g changes

The sensor noise to output of translational velocity is presented in Figure 5.39



Figure 5.39: Sensor Noise to Output of Translational Velocity Control when g changes

The step response of translational velocity is presented in Figure 5.41



Figure 5.40: Input to Control of Translational Velocity Control when g changes

The input to control of translational velocity is presented in Figure 5.40



Figure 5.41: Step Response of Translational Velocity Control when g changes

Finally, we pick $K_{v_y} = 0.038(s+20)$ as the finalized translational velocity controller as the translational velocity controller is designed for lower bandwidth compared with attitude control. The closed loop poles are at (-7.32, 12.05), (-7.32, -12.05), (-8.85, 3.56) and (-8.85, -3.56) and zeros are at (-20, 0) and (-12, 0) with settling time of step response is 0.45s (4% overshoot).

5.4.2 Translational Position Control

The translational position of the quadrotor is from state estimation (sensor fusion of accelerometer and MOCAP). The frequency of translational position control in the firmware is 100Hz. The translational position plant transfer function P_y is given by

$$P_y = \frac{151.2s^2 + 4837s + 36282}{s^5 + 32.34s^4 + 549.1s^3 + 5005s^2 + 36282s}$$
(5.15)

Similar as attitude control, we can use proportional control as the translational position controller. We have the open loop root locus of L = PK in Figure 5.42 when $K_y = 2.0$



Figure 5.42: Open Loop Root Locus of Translational Position Control

The complimentary sensitivity of position control is presented in Figure 5.43



Figure 5.43: CF of Translational Position Control when k_p changes

The sensitivity of position control is presented in Figure 5.43



Figure 5.44: Sensitivity of Translational Position Control when k_p changes





Figure 5.45: Step Response of Translational Position Control when k_p changes

Finally we have the finalized $K_y = 2.0$ with closed loop poles at $(-7.27, \pm 11.18)$, $(-7.41, \pm 3.66)$ and (-2.99, 0) and zeros at (-20, 0) and (-12, 0).

5.5 Summary and Conclusions

This Chapter provides a complimentary study for full-state classical control of quadrotor. All control law developments is mainly based on feedback control theory. The actuator and sensor performance limited the bandwidth of the quadrotor near hovering mode.

Chapter 6

FLIGHT STATE ESTIMATION

6.1 Onboard Sensor Calibration

Gyroscope Thermal Calibration

For silicon MEMS gyroscopes with high quality (Q) factors [23] and [24]. In engineering application, it is needed to remove as much of the offset as possible before processing. This is achieved by heating the sensor board to 65°C and cooling the board to 15°C. The curve fitting is done by MATLAB curve fitting toolbox. A 4th degree polynomial was used to describe the gyroscope bias with temperature ranges from 15°C to 65°C. The curve fitting of 3 axis is shown in Figure 6.1, Figure 6.2 and Figure 6.3.



Figure 6.1: gyroscope p temperature calibration



Figure 6.2: gyroscope q temperature calibration



Figure 6.3: gyroscope r temperature calibration

The thermal calibration stabilizes the gyroscope output and remove most of the gyroscope offset.

Accelerometer 6-point Tumble Calibration

Based on [25] and [26], an accelerometer requires calibration via 6-point Tumble calibration in Figure 6.4. This way is easy to use on every MCU.



Figure 6.4: Reference for Sensor Orientation While Performing 6-point Tumble Calibration (ST DT0053 Design tip)

The algorithm is described for the particular case of an accelerometer. But it can also be approached on a magnetometer. How true acceleration is related to measured acceleration:

$$\begin{bmatrix} a_{raw,x} \\ a_{raw,y} \\ a_{raw,z} \end{bmatrix} = \begin{bmatrix} g_x & g_{yx} & g_{zx} \\ g_{xy} & g_y & g_{zy} \\ g_{xz} & g_{yz} & g_z \end{bmatrix}_{A_{Cal}} \begin{bmatrix} a_{true,x} \\ a_{true,y} \\ a_{true,z} \end{bmatrix} + \begin{bmatrix} X_{offset} \\ Y_{offset} \\ Z_{offset} \end{bmatrix}$$
(6.1)

We need to measure raw accelerometer 3-axis output of 6 points: Equivalent gravity vector along +X axis, $a_{true,1} = [+g, 0, 0]^T$ Equivalent gravity vector along -X axis, $a_{true,2} = [-g, 0, 0]^T$ Equivalent gravity vector along +Y axis, $a_{true,3} = [0, +g, 0]^T$ Equivalent gravity vector along -Y axis, $a_{true,4} = [0, -g, 0]^T$ Equivalent gravity vector along +Z axis, $a_{true,5} = [0, 0, +g]^T$ Equivalent gravity vector along -Z axis, $a_{true,6} = [0, 0, -g]^T$

Based on the above measurements, we can calculate the offset in each axis:

Offset along X axis,
$$X_{offset} = \frac{1}{2}(a_{raw,x_1} + a_{raw,x_2})$$

Offset along Y axis,
$$Y_{offset} = \frac{1}{2}(a_{raw,y_3} + a_{raw,y_4})$$

Offset along Z axis,
$$Z_{offset} = \frac{1}{2}(a_{raw,z_5} + a_{raw,z_6})$$

The offsets are computed by summing two out of measures listed above. Then the gain matrix (9 numbers in A_{cal}) can be calculated by applying three point (one point from each axis).

After data in all 6 points have been recorded, the offset and the gain matrix will be stored in the flight controller EEPROM. After calibration, we will see that the plane static calibrated accelerometer output is much closer to $[0, 0, g]^T$ shown in Figure 6.5, Figure 6.6 and Figure 6.7



Figure 6.5: Calibrated ACC output vs. Raw output in x axis



Figure 6.6: Calibrated ACC output vs. Raw output in y axis



Figure 6.7: Calibrated ACC output vs. Raw output in z axis

The 6-point accelerometer calibration ensures that the resultant force vector of quadrotor in body frame is close to reality. Based on [4], it is not possible to estimate the attitude of a quadrotor in flight without drift by only using IMU measurements. So it is needed to use measurements from the motion capture system.

6.2 IIR Low-Pass Filtering

Based on [27], MEMS (micro-electro-mechanical system) based inertial sensors not only suffer from bias instability, but also noisy output. From Chapter 5, we have seen that noisy sensor feedback limits the quadrotor bandwidth. It is needed to reduce the mechanical noise caused by motors. Here the noise analysis experiment is performed to give the noise specturm.



Figure 6.8: Fast Fourier Transform of Gyroscope Output when Motors off

In Figure 6.8, it is clear to see that the zero output of gyroscope is close to white noise (we assume it is gaussian) when the quadrotor holds still on ground (the quadrotor is put on normal foam mats) and motors are off.



Figure 6.9: Fast Fourier Transform of Gyroscope Output when Motors on

As we turn on all four motors and increase the rotation speed (without propellers) towards T = mg for simulating quadrotor hovering mode. In Figure 6.9, it is clear to see that there are peaks on 35 Hz, 67 Hz and 90 Hz. Accelerometer has similar characteristics with gyroscope. So we need to design a low-pass filter cutting off at 30 Hz for onboard MEME sensors.

IIR (Infinite Impulse Response) filters are the most efficient type of filter to implement in DSP (digital signal processing). MATLAB IIR filter toolbox in Figure 6.10 offers multiple choices of IIR filters.



Figure 6.10: Different IIR Filters Spectrum Using MATLAB Toolbox

Here we are using Butterworth filter as the IIR filter to deal with MEMS sensor mechanical noise. We can represent it in laplacian form:

$$H = \frac{35532.45}{s^2 + 377.16s + 35532.45} \tag{6.2}$$

Where the cut-off frequency is $\frac{\sqrt{35532.45}}{2\pi} = 30$ Hz. This IIR filter is implemented in the

MARK3 flight controller. The filtered gyroscope zero output spectrum is presented in Figure 6.11. Compared with Figure 6.9, the noise generated from motors is well filtered.



Figure 6.11: Filtered Gyroscope Zero Output Spectrum with Motors on

In the flight controller firmware, the filtered gyroscope output is defined as the angular rate feedback and the filtered accelerometer output is defined as resultant force vector joining the full-state estimation.

6.3 Quaternion Based Attitude Estimation

Euler Angle representation are used to show rotation in the model. This chapter considers the Z - Y - X convention as the rotation order within a rotation around the yaw axis, a rotation around the new pitch axis and a rotation around the new roll axis. This method of rotation representation has two main disadvantages in the flight controller firmware.

Singularities Singularities exist in Euler Angle especially when yaw angle is at

 $\pm \pi$, pitch angle is at $\pm 0.5\pi$ and roll angle is at $\pm \pi$. These changes require massive use of conditional statements to attempt to correct when executing sensor fusion algorithm. Besides, high computational cost is needed for huge use of trigonometric function in the math.h library.

Gimbal Lock When the two axes of the quadrotor are driven into a parallel configuration, the rotation system will lose one degree of freedom. This would cause strange effects in the attitude estimation resulting accidents.

Quaternion is widely used in the UAV state estimation and it can be written in two forms [11]:

$$q = q_0 + q_1 i + q_2 j + q_3 k \tag{6.3}$$

and

$$q = [q_0, q_1, q_2, q_3]^T \tag{6.4}$$

The multiplication of quaternions can be represented as:

$$p \otimes q = \begin{bmatrix} p_0 & -p_1 & -p_2 & -p_3 \\ p_1 & p_0 & p_3 & -p_2 \\ p_2 & -p_3 & p_0 & p_1 \\ p_3 & p_2 & -p_1 & p_0 \end{bmatrix} q = p \begin{bmatrix} q_0 & -q_1 & -q_2 & -q_3 \\ q_1 & q_0 & -q_3 & q_2 \\ q_2 & q_3 & q_0 & -q_1 \\ q_3 & -q_2 & q_1 & q_0 \end{bmatrix}$$
(6.5)

The rotation matrix from body frame to earth frame can presented using quaternion $\mathbf{x}_E = R_{B\to E}(q)\mathbf{x}_B$. And we have

$$R_{B\to E} = \begin{bmatrix} q_0^2 + q_1^2 - q_2^2 - q_3^2 & 2(q_1q_2 + q_0q_3) & 2(q_1q_3 - q_0q_2) \\ 2(q_1q_2 - q_0q_3) & q_0^2 - q_1^2 + q_2^2 - q_3^2 & 2(q_2q_3 + q_0q_1) \\ 2(q_1q_3 + q_0q_2) & 2(q_2q_3 - q_0q_1) & q_0^2 - q_1^2 - q_2^2 + q_3^2 \end{bmatrix}$$
(6.6)
and the derivative $([r_x, r_y, r_z]^T$ is the angular rate data collected from gyroscope)

$$\begin{bmatrix} \dot{q_0} \\ \dot{q_1} \\ \dot{q_2} \\ \dot{q_3} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 0 & -r_x & -r_y & -r_z \\ r_x & 0 & r_z & -r_y \\ r_y & -r_z & 0 & -r_x \\ r_z & r_y & -r_x & 0 \end{bmatrix} \begin{bmatrix} q_0 \\ q_1 \\ q_2 \\ q_3 \end{bmatrix}$$
(6.7)

And we have the iteration step

$$q(k+1) = q(k) + \dot{q}(k)T$$
(6.8)



Figure 6.12: Complimentary Filter Pitch Angle Estimation

The Explicit Complimentary Filter is based on [11]. If the gyroscope has no bias on aircrafts, we can use integral term of gyroscope output as attitude feedback value. But even the gyroscope calibration is executed and most of the bias is removed, we still cannot use integral term of gyroscope. By using the explicit complimentary filter in Figure 6.13, we can add accelerometer and MOCAP as reference to make the estimated value is close to real value.



Figure 6.13: Explicit Complimentary Filter Diagram

And the complimentary filter estimation on pitch angle is shown in Figure 6.12. It is clear to see that the attitude estimation removes bias of integral gyroscope output and converges to noisy output accelerometer.

6.4 Position & Velocity Estimation

Even though we have an accurate MOCAP system, we still need to do state estimation to reduce influence of communication signal loss shown in Figure 6.12 and Figure 6.15. It is clear to see the estimated value is reliable when the length of signal loss is small. The velocity estimation iteration step is based on

$$v(k+1) = v(k) + a(k)T$$
(6.9)

And the position estimation iteration step is based on

$$x(k+1) = x(k) + v(k)T + \frac{1}{2}a(k)T^{2}$$
(6.10)



Figure 6.14: Complimentary Filter Velocity in x axis Estimation



Figure 6.15: Complimentary Filter Position in x axis Estimation

The output from the estimator is used as the feedback for all controllers.

Chapter 7

EXPERIMENTAL HARDWARE RESULTS AND COMPARISONS WITH SIMULATION RESULTS

The simulated data is compared with actual data from flight experiment. The simulated data is generated from Simulink.

7.1 Attitude Command-response Graph with Simulation Results

The step response of ϕ control is presented in Figure 7.1



Figure 7.1: ϕ Step Response with Simulated Data

The ramp response of ψ control is presented in Figure 7.2



Figure 7.2: ψ Ramp Response with Simulated Data

7.2 Altitude Command-response Graph with Simulation Results

The ramp response of altitude control is presented in Figure 7.3



Figure 7.3: Altitude Ramp Response with Simulated Data

7.3 Translational Position Command-response Graph with Simulation Results The ramp response of translational position control is presented in Figure 7.4



Figure 7.4: Position Ramp Response with Simulated Data

7.4 Summary and Conclusions

This chapter provided comparision of simulation and hardware results. With the HTC VIVE Tracking System and the upper computer GUI, the data is well collected. For inner loop (Attitude Control) we can get good actual response. But for outer loop(Altitude and Translational Position Control), the output is affected by turbulence generated from propeller when the quadrotor is flying near the ground as shown above. Because of the experiment site limitation, we currently can only do flight test small area with HTC VIVE of SteamVR 1.0. In the future, HTC VIVE based on SteamVR 2.0 offering larger tracking area will solve this problem.

Chapter 8

CONCLUSIONS AND DIRECTIONS FOR FUTURE RESEARCH

8.1 Summary of Work

This thesis addressed design, modeling and control of a quadrotor platform for indoor environments. This platform is capable of indoor formation flight. The following summarizes key themes within the thesis.

- Design and Implementation of Mark3 Flight Controller. In this thesis, the MARK3 flight controller is designed including a 120MHz Teensy 3.2 MCU, a GY-89 10DOF Sensor Board and Xbee 3.0 to offer enough design of redundancy for quadrotor research. The flight controller firmware contains communication processing, full-state estimation, full-state feedback control and system checking function. The MARK3 flight controller PCB design, code and instructions have been uploaded to https://github.com/ragewrath/Mark3-Copter-Pilot.
- Overall Indoor Flight Architecture. A 250mm low-cost platform is designed giving enough payload and agility. The HTC VIVE tracking system is introduced for indoor tracking with submillimeter accuracy. A MATLAB based GUI is designed for communication and receive tracking data from SteamVR API (see Appendix B).
- 3. Modeling. The rigid-body dynamic model and the actuator dynamics model were presented and analyzed. A linearized model with actuator dynamics near hovering model is designed which is useful for the full-state feedback control. The moment parameters are measured with a bifilar pendulum experiment.

The actuator parameters are measured using RCbenchmark 1580 test stand. All parameters are well measured and applied in the control simulation and the flight controller firmware.

- 4. Control. The full-state feedback control design is discussed including attitude cascade control, altitude cascade control and translational movement cascade control. Step response and ramp response experiment is also executed to compare the actual data and simulated data. The whole design shows strong robustness and limitations of the design caused by actuator performance limitation and sensor noise. This part is very useful to researchers pursuing quadrotor developments.
- 5. Estimation. Then onboard sensor calibration and low-pass filtering is presented to get high quality gyroscope output and accelerometer output. The full-estimation is illustrated in the flight controller firmware with sensor fusion of accelerometer, gyroscope and HTC VIVE tracking system. Attitude state value is from the quaternion based complimentary filter with a PI feedback loop. Position and velocity value is from complimentary filter to get rid of influence of possible signal loss.

8.2 Directions for Future Research

Future work will involve each of the following:

1. Formation Flight. With compatibility of HTC VIVE tracking system and Xbee 3.0, multi-quadrotor cooperation can performed and the upper computer collects all the data from quadrotors and HTC VIVE tracking system to determine what to do next.

- 2. **On-board Sensing.** The *MARK3* flight controller is designed with enough redundancy for on-board sensing. Multiple pin headers for I2C and UART communication ensure the flight controller can be connected additional devices (GPS, Rangefinders, LIDAR, High-level Embedded System, etc).
- 3. Human-Robot Interaction. The compatibility with HTC VIVE tracking system on this quadrotor platform offers possibility that human-robot interaction uses virtual reality devices to identify gestures and body movements.
- 4. Flight in Virtual Reality. Using the HTC VIVE tracking system offers possibility to fly drones in the most realistic simulation with Unity. In this way, the drone experiences real physics, gets real inertial measurements, but gets photorealistically simulated camera images. This allows researchers and developers to fly their drones in various simulated virtuals environments.

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APPENDIX A

MATLAB CODE

Angular Rate Control Simulation File

```
1 close all;
2 clc;
3 clear;
            ---Angular Rate Control------%
4 %----
5 %% Parameters
6 t=0:0.01:2;
7 J_y = 0.0019536;
s a = 9.79;
9 s=tf('s');
10 P=1 * a /((J_y*s)*(s+a));
11 %% Controller
12 K0=0.001 \star (s+12);
13 K1=0.002 \star (s+12);
14 K2=0.0045 \star (s+12);
15 K3=0.008*(s+12);
16 K4=0.015*(s+12);
17 K5=0.040*(s+12);
18 %% 1 Plot L = PK
19 LO=P*K0;
20 L1=P*K1;
21 L2=P*K2;
22 L3=P*K3;
23 L4=P*K4;
24 L5=P*K5;
25 figure(1);
26 bodemag(L0);
27 hold on;
28 bodemag(L1);
29 hold on;
30 bodemag(L2);
31 hold on;
32 bodemag(L3);
33 hold on;
34 bodemag(L4);
35 hold on;
36 bodemag(L5);
37 hold off;
38 legend("K_{p}=0.001*(s+12)",...
39
          "K_{p}=0.002*(s+12)",...
          "K<sub>-</sub>{p}=0.0045*(s+12)",...
40
          "K_{p}=0.008*(s+12)",...
41
          "K_{p}=0.015*(s+12)",...
42
          K_{-}(p)=0.040*(s+12)");
43
44 title('Open Loop bodemag L');
45 grid on;
46 grid minor;
47 plot_axis;
48 %% 2 Plot Try (T)
49 TO=minreal(LO/(1+LO));
50 T1=minreal(L1/(1+L1));
51 T2=minreal(L2/(1+L2));
52 T3=minreal(L3/(1+L3));
53 T4=minreal(L4/(1+L4));
54 T5=minreal(L5/(1+L5));
```

```
55 figure(2);
56 bodemag(T0);
57 hold on;
58 bodemaq(T1);
59 hold on;
60 bodemag(T2);
61 hold on;
62 bodemag(T3);
63 hold on;
64 bodemag(T4);
65 hold on;
66 bodemag(T5);
67
   hold off;
   legend("K_{p}=0.001*(s+12)",...
68
           "K_{p}=0.002*(s+12)",...
69
           "K_{p}=0.0045*(s+12)",...
70
           "K_{p}=0.008*(s+12)",...
71
           "K_{p}=0.015*(s+12)",...
72
           "K<sub>-</sub>{p}=0.040*(s+12)");
73
74 title('Complimentary Sensitivity, T_{ry}');
75 grid on;
76 grid minor;
77 plot_axis;
78 %% 3 Plot Tdoy (S)
79 SO=1/(1+L0);
80 S1=1/(1+L1);
81 S2=1/(1+L2);
82 S3=1/(1+L3);
83 S4=1/(1+L4);
84 S5=1/(1+L5);
85 figure(3);
s6 bodemag(S0);
87 hold on;
ss bodemag(S1);
89 hold on;
90 bodemag(S2);
91 hold on;
92 bodemag(S3);
93 hold on;
94 bodemag(S4);
95 hold on;
   bodemag(S5);
96
   hold off;
97
   legend("K_{p}=0.001*(s+12)",...
98
           "K_{p}=0.002*(s+12)",...
99
           "K_{p}=0.0045*(s+12)",...
100
           "K_{p}=0.008*(s+12)",...
101
           "K_{p}=0.015*(s+12)",...
102
           "K_{p}=0.040*(s+12)");
103
104 title('Sensitivity');
105 grid on;
106 grid minor;
107 plot_axis;
108 %% 4 Plot Tdiy (PS)
109 PSO=P/(1+LO);
110 PS1=P/(1+L1);
111 PS2=P/(1+L2);
```

```
112 PS3=P/(1+L3);
113 PS4=P/(1+L4);
114 PS5=P/(1+L5);
115 figure(4);
116 bodemag(PS0);
117 hold on;
118 bodemag(PS1);
119 hold on;
120 bodemag(PS2);
121 hold on;
122 bodemag(PS3);
123 hold on;
124 bodemag(PS4);
125 hold on;
126 bodemag(PS5);
127 hold off;
   legend("K_{p}=0.001*(s+12)",...
128
            "K<sub>-</sub>{p}=0.002*(s+12)",...
129
            "K_{p}=0.0045*(s+12)",...
130
            "K_{p}=0.008*(s+12)",...
131
            "K<sub>-</sub>{p}=0.015*(s+12)",...
132
            "K_{p}=0.040*(s+12)");
133
134 title('PS');
135 grid on;
136 grid minor;
137 plot_axis;
138 %% 5 Plot Tny Tdiu
139 \text{ Tny0} = -L0/(1+L0);
140 Tny1= -L1/(1+L1);
141 Tny2= -L2/(1+L2);
142 \text{ Tny3} = -L3/(1+L3);
143 Tny4= -L4/(1+L4);
144 Tny5= -L5/(1+L5);
145 figure(5);
146 bodemag(Tny0);
147 hold on;
148 bodemag(Tny1);
149 hold on;
150 bodemag(Tny2);
151 hold on;
152 bodemag(Tny3);
153 hold on;
154 bodemag(Tny4);
155 hold on;
156 bodemag(Tny5);
   hold off;
157
   legend("K_{p}=0.001*(s+12)",...
158
            "K_{p}=0.002*(s+12)",...
159
            "K_{p}=0.0045*(s+12)",...
160
            "K<sub>-</sub>{p}=0.008*(s+12)",...
161
            "K_{p}=0.015*(s+12)",...
162
            "K_{p}=0.040*(s+12)");
163
164 title('T_{n y}');
165 grid on;
166 grid minor;
167 plot_axis;
168 %% 6 Plot Tru (KS)
```

```
169 Tru0= K0/(1+L0);
170 Tru1= K1/(1+L1);
171 Tru2= K2/(1+L2);
172 Tru3= K3/(1+L3);
173 Tru4= K4/(1+L4);
   Tru5= K5/(1+L5);
174
175
   figure(6);
176
177 bodemag(Tru0);
178 hold on;
179 bodemag(Tru1);
180 hold on;
181 bodemag(Tru2);
182 hold on;
183 bodemag(Tru3);
184 hold on;
185 bodemag(Tru4);
186 hold on;
187 bodemag(Tru5);
188 hold off;
   legend("K_{p}=0.001*(s+12)",...
189
            "K_{p}=0.002*(s+12)",...
190
            "K_{p}=0.0045*(s+12)",...
191
            "K<sub>-</sub>{p}=0.008*(s+12)",...
192
            "K_{p}=0.015*(s+12)",...
193
            "K<sub>-</sub>{p}=0.040*(s+12)");
194
195 title('T_{r u} KS');
196 grid on;
197 grid minor;
198 plot_axis;
199 %% 7 Plot Tdou Tnu
200 \text{ Tdou0} = -K0/(1+L0);
201 \text{ Tdoul} = -K1/(1+L1);
202 \text{ Tdou2} = -K2/(1+L2);
203 Tdou3= -K3/(1+L3);
204 \text{ Tdou4} = -K4/(1+L4);
205 \text{ Tdou5} = -\text{K5}/(1+\text{L5});
206 figure(7);
207 bodemag(Tdou0);
208 hold on;
209 bodemag(Tdoul);
210 hold on;
211 bodemag(Tdou2);
212 hold on;
213 bodemag(Tdou3);
214 hold on;
215 bodemag(Tdou4);
216 hold on;
217 bodemag(Tdou5);
218 hold off;
   legend("K_{p}=0.001*(s+12)",...
219
            "K_{p}=0.002*(s+12)",...
220
            "K_{p}=0.0045*(s+12)",...
221
            "K<sub>-</sub>{p}=0.008*(s+12)",...
222
            "K_{p}=0.015*(s+12)",...
223
            "K_{p}=0.040*(s+12)");
224
225 title('T_{do u} T_{n u}');
```

```
226 grid on;
227 grid minor;
228 plot_axis;
229 %% Plot Step Response
230 figure(8);
231 st0=stepplot(T0,t);
232 hold on;
233 stl=stepplot(T1,t);
234 hold on;
235 st2=stepplot(T2,t);
236 hold on;
237 st3=stepplot(T3,t);
238 hold on;
239 st4=stepplot(T4,t);
240 hold on;
241 st5=stepplot(T5,t);
242 hold off;
243 legend("K_{p}=0.001*(s+12)",...
           "K_{p}=0.002*(s+12)",...
244
           "K_{p}=0.0045*(s+12)",...
245
           "K_{p}=0.008*(s+12)",...
246
           "K_{p}=0.015*(s+12)",...
247
           "K<sub>-</sub>{p}=0.040*(s+12)");
248
249 ylabel('Angular Rate q (rad/s)');
250 grid on;
251 grid minor;
252 plot_axis;
253 %% Open Loop Root Locus
254 figure(10);
255 rlocus(T0);
256 grid on;
257 grid minor;
258 legend("K0=0.001*(s+12)");
259 figure(11);
260 rlocus(L1);
261 grid on;
262 grid minor;
263 legend("K1=0.002*(s+12)");
264 figure(12);
265 rlocus(T2);
266 grid on;
267 grid minor;
268 legend("Kp=0.0045*(s+12)");
269 figure(13);
270 rlocus(L3);
271 grid on;
272 grid minor;
273 legend("K3=0.008*(s+12)");
274 figure(14);
275 rlocus(L4);
276 grid on;
277 grid minor;
278 legend("K4=0.015*(s+12)");
279 figure(15);
280 rlocus(L5);
281 grid on;
282 grid minor;
```

283 legend("K5=0.040*(s+12)");

Attitude Control Simulation File

```
1 close all;
2 clc;
3 clear;
4 %-----
           ---Attitude Control------%
5 %% Parameters
6 t=0:0.01:2;
7 J_y = 0.0019536;
s = 9.79;
9 s=tf('s');
10 P2=1 * a /((J_y*s)*(s+a));
11 K2=0.0045 \star (s+12);
12 P = minreal(P2*K2/(1+P2*K2)/s);
13 %% Controller
14 KO=3;
15 K1=6;
16 K2=9;
17 K3=12;
18 K4=15;
19 K5=20;
20 %% 1 Plot L = PK
21 LO=P*K0;
22 L1=P*K1;
23 L2=P*K2;
24 L3=P*K3;
25 L4=P*K4;
26 L5=P*K5;
27 figure(1);
28 bodemag(L0);
29 hold on;
30 bodemag(L1);
31 hold on;
32 bodemag(L2);
33 hold on;
34 bodemag(L3);
35 hold on;
36 bodemag(L4);
37 hold on;
38 bodemag(L5);
39 hold off;
40 legend("K\phi=3",...
          "K\phi=6",...
41
          "K\phi=9",...
42
          "K\phi=12",...
43
          "K\phi=15",...
44
          "K\phi=20");
45
46 title('Open Loop bodemag L');
47 grid on;
48 grid minor;
49 plot_axis;
50 %% 2 Plot Try (T)
51 TO=minreal(L0/(1+L0));
52 T1=minreal(L1/(1+L1));
```

```
53 T2=minreal(L2/(1+L2));
54 T3=minreal(L3/(1+L3));
55 T4=minreal(L4/(1+L4));
56 T5=minreal(L5/(1+L5));
57 figure(2);
58 bodemag(T0);
59 hold on;
60 bodemag(T1);
61 hold on;
62 bodemag(T2);
63 hold on;
64 bodemag(T3);
65 hold on;
66 bodemag(T4);
67 hold on;
68 bodemag(T5);
69 hold off;
70 legend("K\phi=3",...
           "K\phi=6",...
71
           "K\phi=9",...
72
           "K\phi=12",...
73
           "K\phi=15",...
74
           "K\phi=20");
75
76 title('Complimentary Sensitivity, T_{ry}');
77 grid on;
78 grid minor;
79 plot_axis;
80 %% 3 Plot Tdoy (S)
81 \quad SO=1/(1+LO);
82 S1=1/(1+L1);
S_{3} S2=1/(1+L2);
84 S3=1/(1+L3);
85 S4=1/(1+L4);
86 S5=1/(1+L5);
87 figure(3);
ss bodemag(S0);
89 hold on;
90 bodemag(S1);
91 hold on;
92 bodemag(S2);
93 hold on;
94 bodemag(S3);
95 hold on;
96 bodemag(S4);
97 hold on;
98 bodemag(S5);
99 hold off;
   legend("K\phi=3",...
100
           "K\phi=6",...
101
           "K\phi=9",...
102
           "K\phi=12",...
103
           "K\phi=15",...
104
           "K\phi=20");
105
106 title('Sensitivity, T_{do y}');
107 grid on;
108 grid minor;
109 plot_axis;
```

```
110 %% 4 Plot Tdiy (PS)
111 PSO=P/(1+L0);
112 PS1=P/(1+L1);
113 PS2=P/(1+L2);
114 PS3=P/(1+L3);
115 PS4=P/(1+L4);
116 PS5=P/(1+L5);
117 figure(4);
118 bodemag(PSO);
119 hold on;
120 bodemag(PS1);
121 hold on;
122 bodemag(PS2);
123 hold on;
124 bodemag(PS3);
125 hold on;
126 bodemag(PS4);
127 hold on;
128 bodemag(PS5);
129 hold off;
130 legend("K\phi=3",...
           "K\phi=6",...
131
           "K\phi=9",...
132
           "K\phi=12",...
133
           "K\phi=15",...
134
           "K\phi=20");
135
136 title('PS, T_{di y}');
137 grid on;
138 grid minor;
139 plot_axis;
140 %% 5 Plot Tny
141 Tny0= -L0/(1+L0);
142 Tny1= -L1/(1+L1);
143 Tny2= -L2/(1+L2);
144 Tny3= -L3/(1+L3);
145 Tny4= -L4/(1+L4);
146 Tny5= -L5/(1+L5);
147 figure(5);
148 bodemag(Tny0);
149 hold on;
150 bodemag(Tny1);
151 hold on;
152 bodemag(Tny2);
153 hold on;
154 bodemag(Tny3);
155 hold on;
156 bodemag(Tny4);
157 hold on;
158 bodemag(Tny5);
159 hold off;
160 legend("K\phi=3",...
           "K\phi=6",...
161
           "K\phi=9",...
162
           "K\phi=12",...
163
           "K\phi=15",...
164
           "K\phi=20");
165
166 title('T_{n y}');
```

```
167 grid on;
168 grid minor;
169 plot_axis;
170 %% 6 Plot Tru (KS)
171 Tru0= K0/(1+L0);
172 Tru1= K1/(1+L1);
173 Tru2= K2/(1+L2);
174 Tru3= K3/(1+L3);
175 Tru4= K4/(1+L4);
176 Tru5= K5/(1+L5);
177 figure(6);
178 bodemag(Tru0);
179 hold on;
180 bodemag(Tru1);
181 hold on;
182 bodemag(Tru2);
183 hold on;
184 bodemag(Tru3);
185 hold on;
186 bodemag(Tru4);
187 hold on;
188 bodemag(Tru5);
189 hold off;
190 legend("K\phi=3",...
           "K\phi=6",...
191
           "K\phi=9",...
192
           "K\phi=12",...
193
           "K\phi=15",...
194
            "K\phi=20");
195
196 title('T_{r u}');
197 grid on;
198 grid minor;
199 plot_axis;
200 %% 7 Plot Tdou Tnu
201 \text{ Tdou0} = -K0/(1+L0);
202 Tdou1= -K1/(1+L1);
203 \text{ Tdou2} = -K2/(1+L2);
204 Tdou3= -K3/(1+L3);
205 \text{ Tdou4} = -K4/(1+L4);
206 \text{ Tdou5} = -\text{K5}/(1+\text{L5});
207 figure(7);
208 bodemag(Tdou0);
209 hold on;
210 bodemag(Tdoul);
211 hold on;
212 bodemag(Tdou2);
213 hold on;
214 bodemag(Tdou3);
215 hold on;
216 bodemag(Tdou4);
217 hold on;
218 bodemag(Tdou5);
219 hold off;
220 legend("K\phi=3",...
            "K\phi=6",...
221
            "K\phi=9",...
222
            "K\phi=12",...
223
```

```
"K\phi=15",...
224
           "K\phi=20");
225
226 title('T_{do u} T_{n u}');
227 grid on;
228 grid minor;
229 plot_axis;
230 %% Plot Step Response
231 figure(8);
232 st0=stepplot(T0,t);
233 hold on;
234 st1=stepplot(T1,t);
235 hold on;
236 st2=stepplot(T2,t);
237 hold on;
238 st3=stepplot(T3,t);
239 hold on;
240 st4=stepplot(T4,t);
241 hold on;
242 st5=stepplot(T5,t);
243 hold off;
244 legend("K\phi=3",...
           "K\phi=6",...
245
           "K\phi=9",...
246
           "K\phi=12",...
247
           "K\phi=15",...
248
           "K\phi=20");
249
250 ylabel('Attitude \phi (rad)');
251 grid on;
252 grid minor;
253 plot_axis;
254 %% Close Loop Pole
255 figure(10);
256 rlocus(L0);
257 grid on;
258 grid minor;
259 legend("K\phi=3");
260 figure(11);
261 rlocus(L1);
262 grid on;
263 grid minor;
264 legend("K\phi=6");
265 figure(12);
266 rlocus(T2);
267 grid on;
268 grid minor;
269 legend("K\phi=9");
270 figure(13);
271 rlocus(L3);
272 grid on;
273 grid minor;
274 legend("K\phi=12");
275 figure(14);
276 rlocus(L4);
277 grid on;
278 grid minor;
_{279} legend("K\phi=15");
```

```
281 rlocus(L5);
282 grid on;
283 grid minor;
284 legend("K\phi=20");
```

Vertical Velocity Control Simulation File

```
1 close all;
2 clc;
3 clear;
4 %------
           -----Vertical Velocity Control----
                                           5 %% Parameters
6 t=0:0.01:2;
7 m = 0.645;
s = 9.79;
9 s=tf('s');
10 P=1 * a / ((m*s)*(s+a));
11 %% Controller
12 K0=0.050*(s+12);
13 K1=0.100 \star (s+12);
14 K2=0.2*(s+12);
15 K3=0.525*(s+12);
16 K4=1*(s+12);
17 K5=2*(s+12);
18 %% 1 Plot L = PK
19 LO=P*K0;
20 L1=P*K1;
21 L2=P*K2;
22 L3=P*K3;
23 L4=P*K4;
24 L5=P*K5;
25 figure(1);
26 bodemag(L0);
27 hold on;
28 bodemag(L1);
29 hold on;
30 bodemag(L2);
31 hold on;
32 bodemag(L3);
33 hold on;
34 bodemag(L4);
35 hold on;
36 bodemag(L5);
37 hold off;
38 legend("K0=7.000 + 0.050*s",...
          "K1=7.000 + 0.200*s",...
39
          "K2=7.000 + 0.525*s",...
40
          "K3=7.000 + 0.800*s",...
41
          "K4=7.000 + 1.000*s",...
42
          "K5=7.000 + 2.000 + s");
43
44 title('Open Loop bodemag L');
45 grid on;
46 grid minor;
47 plot_axis;
48 %% 2 Plot Try (T)
49 TO=LO/(1+LO);
```

```
50 T1=L1/(1+L1);
51 T2=L2/(1+L2);
52 T3=L3/(1+L3);
53 T4=L4/(1+L4);
54 T5=L5/(1+L5);
55 figure(2);
56 bodemag(TO);
57 hold on;
58 bodemag(T1);
59 hold on;
60 bodemag(T2);
61 hold on;
62 bodemag(T3);
63 hold on;
64 bodemag(T4);
65 hold on;
66 bodemag(T5);
67 hold off;
68 legend("K0=7.000 + 0.050*s",...
           "K1=7.000 + 0.200*s",...
69
           "K2=7.000 + 0.525*s",...
70
           "K3=7.000 + 0.800*s",...
71
           "K4=7.000 + 1.000*s",...
72
           "K5=7.000 + 2.000*s");
73
74 grid on;
75 title('Complimentary Sensitivity, T_{ry}');
76 grid minor;
77 plot_axis;
78 %% 3 Plot Tdoy (S)
79 SO=1/(1+LO);
80 S1=1/(1+L1);
81 S2=1/(1+L2);
82 S3=1/(1+L3);
83 S4=1/(1+L4);
84 S5=1/(1+L5);
85 figure(3);
s6 bodemag(S0);
87 hold on;
ss bodemag(S1);
89 hold on;
90 bodemag(S2);
91 hold on;
92 bodemag(S3);
93 hold on;
94 bodemag(S4);
95 hold on;
96 bodemag(S5);
97 hold off;
   legend("K0=7.000 + 0.050*s",...
98
           "K1=7.000 + 0.200*s",...
99
           "K2=7.000 + 0.525*s",...
100
          "K3=7.000 + 0.800*s",...
101
          "K4=7.000 + 1.000*s",...
102
           "K5=7.000 + 2.000*s");
103
104 title('Sensitivity, T_{do y}');
105 grid minor;
106 plot_axis;
```

```
107 %% 4 Plot Tdiy (PS)
108 PSO=P/(1+L0);
109 PS1=P/(1+L1);
110 PS2=P/(1+L2);
111 PS3=P/(1+L3);
112 PS4=P/(1+L4);
113 PS5=P/(1+L5);
114 figure(4);
115 bodemag(PSO);
116 hold on;
117 bodemag(PS1);
118 hold on;
119 bodemag(PS2);
120 hold on;
121 bodemag(PS3);
122 hold on;
123 bodemag(PS4);
124 hold on;
125 bodemag(PS5);
126 hold off;
127 legend("K0=7.000 + 0.050*s",...
           "K1=7.000 + 0.200*s",...
128
           "K2=7.000 + 0.525*s",...
129
           "K3=7.000 + 0.800*s",...
130
           "K4=7.000 + 1.000*s",...
131
           "K5=7.000 + 2.000*s");
132
133 title('PS, T_{di y}');
134 grid minor;
135 plot_axis;
136 %% 5 Plot Tny
137 \text{ Tny0} = -L0/(1+L0);
138 \text{ Tnyl} = -L1/(1+L1);
139 Tny2= -L2/(1+L2);
140 Tny3= -L3/(1+L3);
141 Tny4= -L4/(1+L4);
142 Tny5= -L5/(1+L5);
143 figure(5);
144 bodemag(Tny0);
145 hold on;
146 bodemag(Tny1);
147 hold on;
148 bodemag(Tny2);
149 hold on;
150 bodemag(Tny3);
151 hold on;
152 bodemag(Tny4);
153 hold on;
154 bodemag(Tny5);
155 hold off;
156 legend("K0=7.000 + 0.050*s",...
           "K1=7.000 + 0.200*s",...
157
           "K2=7.000 + 0.525*s",...
158
           "K3=7.000 + 0.800*s",...
159
           "K4=7.000 + 1.000*s",...
160
           "K5=7.000 + 2.000*s");
161
162 title('T_{n y}');
163 grid minor;
```

```
164 plot_axis;
165 %% 6 Plot Tru (KS)
166 Tru0= K0/(1+L0);
167 Tru1= K1/(1+L1);
168 \text{ Tru2} = \text{K2}/(1+\text{L2});
169 Tru3= K3/(1+L3);
170 Tru4= K4/(1+L4);
171 Tru5= K5/(1+L5);
172 figure(6);
173 bodemag(Tru0);
174 hold on;
175 bodemag(Tru1);
176 hold on;
177 bodemag(Tru2);
178 hold on;
179 bodemag(Tru3);
180 hold on;
181 bodemag(Tru4);
182 hold on;
183 bodemag(Tru5);
184 hold off;
185 legend("K0=7.000 + 0.050*s",...
            "K1=7.000 + 0.200*s",...
186
           "K2=7.000 + 0.525*s",...
187
           "K3=7.000 + 0.800*s",...
188
           "K4=7.000 + 1.000*s",...
189
           "K5=7.000 + 2.000 + s");
190
191 title('T_{r u}');
192 grid minor;
193 plot_axis;
194 %% 7 Plot Tdou Tnu
195 \text{ Tdou0} = -\text{K0}/(1+\text{L0});
196 Tdou1= -K1/(1+L1);
197 \text{ Tdou2} = -\text{K2}/(1+\text{L2});
198 Tdou3= -K3/(1+L3);
199 Tdou4= -K4/(1+L4);
200 \text{ Tdou5} = -K5/(1+L5);
201 figure(7);
202 bodemag(Tdou0);
203 hold on;
204 bodemag(Tdoul);
205 hold on;
206 bodemag(Tdou2);
207 hold on;
208 bodemag(Tdou3);
209 hold on;
210 bodemag(Tdou4);
211 hold on;
212 bodemag(Tdou5);
213 hold off;
214 legend("K0=7.000 + 0.050*s",...
            "K1=7.000 + 0.200*s",...
215
            "K2=7.000 + 0.525*s",...
216
            "K3=7.000 + 0.800*s",...
217
            "K4=7.000 + 1.000*s",...
218
            "K5=7.000 + 2.000*s");
219
220 title('T_{do u} T_{n u}');
```

```
221 grid minor;
222 plot_axis;
223 %% Plot Step Response
224 figure(8);
225 st0=stepplot(T0,t);
226 hold on;
227 stl=stepplot(T1,t);
228 hold on;
229 st2=stepplot(T2,t);
230 hold on;
231 st3=stepplot(T3,t);
232 hold on;
233 st4=stepplot(T4,t);
234 hold on;
235 st5=stepplot(T5,t);
236 hold off;
237 legend("K0=7.000 + 0.050*s",...
           "K1=7.000 + 0.200*s",...
238
           "K2=7.000 + 0.525*s",...
239
           "K3=7.000 + 0.800*s",...
240
           "K4=7.000 + 1.000*s",...
241
           "K5=7.000 + 2.000*s");
242
243 ylabel('Angular Rate q (rad/s)');
244 grid minor;
245 plot_axis;
246 %% Close Loop Pole
247 figure(10);
248 rlocus(TO);
249 grid on;
250 grid minor;
_{251} legend ("K0=7.000 + 0.050*s");
252 figure(11);
253 rlocus(T1);
254 grid on;
255 grid minor;
256 legend("K1=7.000 + 0.200*s");
257 figure(12);
258 rlocus(T2);
259 grid on;
260 grid minor;
261 legend("K2=7.000 + 0.525*s");
262 figure(13);
263 rlocus(T3);
264 grid on;
265 grid minor;
266 legend("K3=7.000 + 0.800*s");
267 figure(14);
268 rlocus(T4);
269 grid on;
270 grid minor;
271 legend("K4=7.000 + 1.000*s");
272 figure(15);
273 rlocus(T5);
274 grid on;
275 grid minor;
276 legend("K5=7.000 + 2.000*s");
```

Altitude Control Simulation File

```
1 close all;
2 clc;
3 clear;
4 %-----
         -----Altitude Control------%
5 %% Parameters
6 t=0:0.01:2;
7 m = 0.645;
s a = 9.79;
9 s=tf('s');
10 P_in=1 * a / ((m*s)*(s+a));
11 K_in=0.525 \star (s+12);
12 L_in=P_in*K_in;
13 P=minreal(L_in/(1+L_in)/s);
14 %% Controller
15 KO=0.500;
16 K1=1.000;
17 K2=2.000;
18 K3=4.200;
19 K4=10.000;
20 K5=20.000;
21 %% 1 Plot L = PK
22 LO=P*K0;
23 L1=P*K1;
24 L2=P*K2;
25 L3=P*K3;
26 L4=P*K4;
27 L5=P*K5;
28 figure(1);
29 bodemag(L0);
30 hold on;
31 bodemag(L1);
32 hold on;
33 bodemag(L2);
34 hold on;
35 bodemag(L3);
36 hold on;
37 bodemag(L4);
38 hold on;
39 bodemag(L5);
40 hold off;
41 legend("K0=0.5",...
           "K1=1",...
42
           "K2=3",...
43
           "K3=5",...
44
           "K4=10",...
45
           "K5=20");
46
47 title('Open Loop bodemag L');
48 grid on;
49 grid minor;
50 plot_axis;
51 %% 2 Plot Try (T)
52 TO=minreal(LO/(1+LO));
53 T1=minreal(L1/(1+L1));
54 T2=minreal(L2/(1+L2));
```

```
55 T3=minreal(L3/(1+L3));
56 T4=minreal(L4/(1+L4));
57 T5=minreal(L5/(1+L5));
58 figure(2);
59 bodemag(T0);
60 hold on;
61 bodemag(T1);
62 hold on;
63 bodemag(T2);
64 hold on;
65 bodemag(T3);
66 hold on;
67 bodemag(T4);
68 hold on;
69 bodemag(T5);
70 hold off;legend("K0=0.5",...
            "K1=1",...
71
            "K2=3",...
"K3=5",...
72
73
            "K4=10",...
74
            "K5=20");
75
76 title('Complimentary Sensitivity, T_{ry}');
77 grid minor;
78 plot_axis;
79 %% 3 Plot Tdoy (S)
80 SO=1/(1+L0);
81 S1=1/(1+L1);
82 S2=1/(1+L2);
83 S3=1/(1+L3);
84 S4=1/(1+L4);
85 S5=1/(1+L5);
s6 figure(3);
87 bodemaq(S0);
ss hold on;
89 bodemag(S1);
90 hold on;
91 bodemag(S2);
92 hold on;
93 bodemag(S3);
94 hold on;
95 bodemag(S4);
96 hold on;
97 bodemag(S5);
98 hold off;legend("K0=0.5",...
99
            "K1=1",...
100
            "K2=3",...
            "K3=5",...
101
            "K4=10",...
102
            "K5=20");
103
104 title('Sensitivity, T_{do y}');
105 grid minor;
106 plot_axis;
107 %% 4 Plot Tdiy (PS)
108 PSO=P/(1+LO);
109 PS1=P/(1+L1);
110 PS2=P/(1+L2);
111 PS3=P/(1+L3);
```

```
112 PS4=P/(1+L4);
113 PS5=P/(1+L5);
114 figure(4);
115 bodemag(PS0);
116 hold on;
117 bodemag(PS1);
118 hold on;
119 bodemag(PS2);
120 hold on;
121 bodemag(PS3);
122 hold on;
123 bodemag(PS4);
124 hold on;
125 bodemag(PS5);
126 hold off;legend("K0=0.5",...
             "K1=1",...
127
             "K2=3",...
128
             "K3=5",...
129
             "K4=10",...
130
             "K5=20");
131
132 title('PS, T_{di y}');
133 grid minor;
134 plot_axis;
135 %% 5 Plot Tny Tdiu
136 \text{ Tny0} = -L0/(1+L0);
137 \text{ Tnyl} = -L1/(1+L1);
138 \text{ Tny2} = -L2/(1+L2);
139 \text{ Tny3} = -L3/(1+L3);
140 Tny4= -L4/(1+L4);
141 Tny5= -L5/(1+L5);
142 figure(5);
143 bodemag(Tny0);
144 hold on;
145 bodemag(Tnyl);
146 hold on;
147 bodemag(Tny2);
148 hold on;
149 bodemag(Tny3);
150 hold on;
151 bodemag(Tny4);
152 hold on;
153 bodemag(Tny5);
154 hold off;
155 legend("K0=0.5",...
             "K1=1",...
156
             "K2=3",...
157
             "K3=5",...
158
             "K4=10",...
159
             "K5=20");
160
161 title('T_{n y} T_{di u}');
162 grid minor;
163 plot_axis;
164 %% 6 Plot Tru (KS)
165 \text{ Tru0} = \text{K0} / (1 + \text{L0});
166 Tru1= K1/(1+L1);
167 \text{ Tru2} = \frac{\text{K2}}{(1+\text{L2})};
168 Tru3= K3/(1+L3);
```

```
169 Tru4= K4/(1+L4);
170 Tru5= K5/(1+L5);
171 figure(6);
172 bodemag(Tru0);
173 hold on;
174 bodemag(Tru1);
175 hold on;
176 bodemag(Tru2);
177 hold on;
178 bodemag(Tru3);
179 hold on;
180 bodemag(Tru4);
181 hold on;
182 bodemag(Tru5);
183 hold off;
184 legend("K0=0.5",...
            "K1=1",...
185
            "K2=3",...
186
            "K3=5",...
187
            "K4=10",...
188
            "K5=20");
189
190 title('T_{r u}');
191 grid minor;
192 plot_axis;
193 %% 7 Plot Tdou Tnu
194 Tdou0= -K0/(1+L0);
195 Tdou1= -K1/(1+L1);
196 \text{ Tdou2} = -K2/(1+L2);
197 \text{ Tdou3} = -K3/(1+L3);
198 Tdou4= -K4/(1+L4);
199 Tdou5= -K5/(1+L5);
200 figure(7);
201 bodemag(Tdou0);
202 hold on;
203 bodemag(Tdoul);
204 hold on;
205 bodemag(Tdou2);
206 hold on;
207 bodemag(Tdou3);
208 hold on;
209 bodemag(Tdou4);
210 hold on;
211 bodemag(Tdou5);
212 hold off;
213 legend("K0=0.5",...
            "K1=1",...
214
            "K2=3",...
215
            "K3=5",...
216
            "K4=10",...
217
            "K5=20");
218
219 title('T_{do u} T_{n u}');
220 grid minor;
221 plot_axis;
222 %% Plot Step Response
223 figure(8);
224 st0=stepplot(T0,t);
225 hold on;
```

```
226 stl=stepplot(T1,t);
227 hold on;
228 st2=stepplot(T2,t);
229 hold on;
230 st3=stepplot(T3,t);
231 hold on;
232 st4=stepplot(T4,t);
233 hold on;
234 st5=stepplot(T5,t);
235 hold off;
236 legend("K0=0.5",...
            "K1=1",...
237
           "K2=3",...
238
           "K3=5",...
239
            "K4=10",...
240
            "K5=20");
241
242 ylabel('Altitude (m)');
243 grid minor;
244 plot_axis;
245 %% Close Loop Pole
246 figure(10);
247 rlocus(L0);
248 grid on;
249 grid minor;
250 legend("K0=0.5");
251 figure(11);
252 rlocus(L1);
253 grid on;
254 grid minor;
255 legend("K1=1");
256 figure(12);
257 rlocus(L2);
258 grid on;
259 grid minor;
260 legend("K2=3");
261 figure(13);
262 rlocus(L3);
263 grid on;
264 grid minor;
265 legend("Kz=4.2");
266 figure(14);
267 rlocus(L4);
268 grid on;
269 grid minor;
270 legend("K4=10");
271 figure(15);
272 rlocus(L5);
273 grid on;
274 grid minor;
275 legend("K5=20");
```

Translational Control Simulation File

1 close all; 2 clc; 3 clear;

```
4 %------Translational Velocity Conrol---
                                                      ___%
5 %% Parameters
6 t=0:0.01:2;
7 q = 9.8;
8 s=tf('s');
y = J_y = 0.0019536;
10 a = 9.79;
11 P_2=1 * a /((J_y*s)*(s+a));
12 K_2 = 0.0045 * (s+12);
13 P_3 = minreal(P_2 * K_2 / (1 + P_2 * K_2) / s);
14 K_3 = 9;
15 L_2 = P_3 * K_3;
16 T_2 = minreal(L_2/(1+L_2));
17 P = minreal(T_2 * q/s);
18 %% Controller
19 K0=0.02 \star (s+10);
_{20} K1=0.05*(s+10);
_{21} K2=0.075*(s+10);
22 K3=0.10*(s+10);
23 K4=0.15*(s+10);
24 K5=0.20*(s+10);
25 %% 1 Plot L = PK
26 LO=minreal(P*KO);
27 L1=minreal(P*K1);
28 L2=minreal(P*K2);
29 L3=minreal(P*K3);
30 L4=minreal(P*K4);
31 L5=minreal(P*K5);
32 figure(1);
33 bodemag(L0);
34 hold on;
35 bodemag(L1);
36 hold on;
37 bodemag(L2);
38 hold on;
39 bodemag(L3);
40 hold on;
41 bodemag(L4);
42 hold on;
43 bodemag(L5);
44 hold off;
45 legend("K0=1.3+0.02*s",...
          "K1=1.3+0.05*s",...
46
          "K2=1.3+0.08*s",...
47
          "K3=1.3+0.10*s",...
48
          "K4=1.3+0.15*s",...
49
          "K5=1.3+0.20*s");
50
51 title('Open Loop bodemag L');
52 grid on;
53 grid minor;
54 plot_axis;
55 %% 2 Plot Try (T)
56 T0=minreal(L0/(1+L0));
57 T1=minreal(L1/(1+L1));
58 T2=minreal(L2/(1+L2));
59 T3=minreal(L3/(1+L3));
60 T4=minreal(L4/(1+L4));
```

```
61 T5=minreal(L5/(1+L5));
62 figure(2);
63 bodemag(T0);
64 hold on;
65 bodemag(T1);
66 hold on;
67 bodemag(T2);
68 hold on;
69 bodemag(T3);
70 hold on;
71 bodemag(T4);
72 hold on;
73 bodemag(T5);
74 hold off;
75 legend("K0=1.3+0.02*s",...
           "K1=1.3+0.05*s",...
76
           "K2=1.3+0.08*s",...
77
           "K3=1.3+0.10*s",...
78
           "K4=1.3+0.15*s",...
79
           "K5=1.3+0.20*s");
80
81 title('Complimentary Sensitivity, T_{ry}');
82 grid on;
83 grid minor;
84 plot_axis;
85 %% 3 Plot Tdoy (S)
86 \quad SO=1/(1+LO);
87 S1=1/(1+L1);
88 S2=1/(1+L2);
89 S3=1/(1+L3);
90 S4=1/(1+L4);
91 S5=1/(1+L5);
92 figure(3);
93 bodemaq(S0);
94 hold on;
95 bodemag(S1);
96 hold on;
97 bodemag(S2);
98 hold on;
99 bodemag(S3);
100 hold on;
101 bodemag(S4);
102 hold on;
103 bodemag(S5);
104 hold off;
105 legend("K0=1.3+0.02*s",...
           "K1=1.3+0.05*s",...
106
           "K2=1.3+0.08*s",...
107
           "K3=1.3+0.10*s",...
108
           "K4=1.3+0.15*s",...
109
           "K5=1.3+0.20*s");
110
in title('Sensitivity, T_{do y}');
112 grid on;
113 grid minor;
114 plot_axis;
115 %% 4 Plot Tdiy (PS)
116 PSO=P/(1+LO);
117 PS1=P/(1+L1);
```

```
118 PS2=P/(1+L2);
119 PS3=P/(1+L3);
120 PS4=P/(1+L4);
121 PS5=P/(1+L5);
122 figure(4);
123 bodemag(PS0);
124 hold on;
125 bodemag(PS1);
126 hold on;
127 bodemag(PS2);
128 hold on;
129 bodemag(PS3);
130 hold on;
131 bodemag(PS4);
132 hold on;
133 bodemag(PS5);
134 hold off;
135 legend("K0=1.3+0.02*s",...
           `"K1=1.3+0.05*s",...
136
           "K2=1.3+0.08*s",...
137
           "K3=1.3+0.10*s",...
138
           "K4=1.3+0.15*s",...
139
           "K5=1.3+0.20*s");
140
141 title('PS, T_{di y}');
142 grid on;
143 grid minor;
144 plot_axis;
145 %% 5 Plot Tny
146 \text{ Tny0} = -L0/(1+L0);
147 \text{ Tnyl} = -\text{Ll}/(1+\text{Ll});
148 \text{ Tny2} = -L2/(1+L2);
149 Tny3= -L3/(1+L3);
150 Tny4= -L4/(1+L4);
151 Tny5= -L5/(1+L5);
152 figure(5);
153 bodemag(Tny0);
154 hold on;
155 bodemag(Tny1);
156 hold on;
157 bodemag(Tny2);
158 hold on;
159 bodemag(Tny3);
160 hold on;
161 bodemag(Tny4);
162 hold on;
163 bodemag(Tny5);
164 hold off;
165 legend("K0=1.3+0.02*s",...
           "K1=1.3+0.05*s",...
166
           "K2=1.3+0.08*s",...
167
           "K3=1.3+0.10*s",...
168
           "K4=1.3+0.15*s",...
169
           "K5=1.3+0.20*s");
170
171 title('T_{n y}');
172 grid on;
173 grid minor;
174 plot_axis;
```

```
175 %% 6 Plot Tru (KS)
176 Tru0= K0/(1+L0);
177 Tru1= K1/(1+L1);
178 Tru2= K2/(1+L2);
179 Tru3= K3/(1+L3);
180 Tru4= K4/(1+L4);
181 Tru5= K5/(1+L5);
182 figure(6);
183 bodemag(Tru0);
184 hold on;
185 bodemag(Tru1);
186 hold on;
187 bodemag(Tru2);
188 hold on;
189 bodemag(Tru3);
190 hold on;
191 bodemag(Tru4);
192 hold on;
193 bodemag(Tru5);
194 legend("K0=1.3+0.02*s",...
           "K1=1.3+0.05*s",...
195
           "K2=1.3+0.08*s",...
196
           "K3=1.3+0.10*s",...
197
           "K4=1.3+0.15*s",...
198
           "K5=1.3+0.20*s");
199
200 title('T_{r u}');
201 grid on;
202 grid minor;
203 plot_axis;
204 %% 7 Plot Tdou Tnu
_{205} Tdou0= -K0/(1+L0);
206 \text{ Tdou1} = -\text{K1}/(1+\text{L1});
_{207} Tdou2= -K2/(1+L2);
208 \text{ Tdou3} = -K3/(1+L3);
209 \text{ Tdou4} = -K4/(1+L4);
_{210} Tdou5= -K5/(1+L5);
211 figure(7);
212 bodemag(Tdou0);
213 hold on;
214 bodemag(Tdoul);
215 hold on;
216 bodemag(Tdou2);
217 hold on;
218 bodemag(Tdou3);
219 hold on;
220 bodemag(Tdou4);
221 hold on;
222 bodemag(Tdou5);
223 hold off;
224 legend("K0=1.3+0.02*s",...
           "K1=1.3+0.05*s",...
225
           "K2=1.3+0.08*s",...
226
           "K3=1.3+0.10*s",...
227
           "K4=1.3+0.15*s",...
228
           "K5=1.3+0.20*s");
229
230 title('T_{do u} T_{n u}');
231 grid on;
```
```
232 grid minor;
233 plot_axis;
234 %% Plot Step Response
235 figure(8);
236 st0=stepplot(T0,t);
237 hold on;
238 stl=stepplot(T1,t);
239 hold on;
240 st2=stepplot(T2,t);
241 hold on;
242 st3=stepplot(T3,t);
243 hold on;
244 st4=stepplot(T4,t);
245 hold on;
246 st5=stepplot(T5,t);
247 hold off;
248 legend("K0=1.3+0.02*s",...
           "K1=1.3+0.05*s",...
249
           "K2=1.3+0.08*s",...
250
           "K3=1.3+0.10*s",...
251
           "K4=1.3+0.15*s",...
252
           "K5=1.3+0.20*s");
253
254 ylabel('Translational Velocity Vy (m/s)');
255 grid on;
256 grid minor;
257 plot_axis;
258
259 %% Close Loop Pole
260 figure(10);
261 rlocus(TO);
262 grid on;
263 grid minor;
264 legend("K0=1.3+0.01*s");
265 figure(11);
266 rlocus(T1);
267 grid on;
268 grid minor;
269 legend("K1=1.3+0.02*s");
270 figure(12);
271 rlocus(L2);
272 grid on;
273 grid minor;
274 legend("Kvy=0.075*(s+10)s");
275 figure(13);
276 rlocus(T3);
277 grid on;
278 grid minor;
279 legend("K3=1.3+0.10*s");
280 figure(14);
281 rlocus(T4);
282 grid on;
283 grid minor;
284 legend("Kvy=1.3+0.20*s");
285 figure(15);
286 rlocus(T5);
287 grid on;
288 grid minor;
```

```
289 legend("Kvy=1.3+0.50*s");
```

Translational Position Simulation File

```
1 clc;
2 clear;
3 close all;
         ------Translational Position Control-----
                                                       ----8
4 %------
5 %% Parameters
6 t=0:0.01:10;
7 s=tf('s');
8 %% Parameters
9 T2_vy = (149.2 \times s^2 + 3282 \times s + 1.79e04)/...
           (s^4+32.34*s^3+...
10
            622.7*s<sup>2+5717*s+1.79e04</sup>);
11
12 P = minreal(T2_vy / s);
13 KO=0.2;
14 K1=0.4;
15 K2=0.8;
16 K3=1.0;
17 K4=2.0;
18 K5=4.0;
19 %% 1 Plot L = PK
20 LO=minreal(P*KO);
21 L1=minreal(P*K1);
22 L2=minreal(P*K2);
23 L3=minreal(P*K3);
24 L4=minreal(P*K4);
25 L5=minreal(P*K5);
26 figure(1);
27 bodemag(L0);
28 hold on;
29 bodemag(L1);
30 hold on;
31 bodemag(L2);
32 hold on;
33 bodemag(L3);
34 hold on;
35 bodemag(L4);
36 hold on;
37 bodemag(L5);
38 hold off;
39 legend("K0=0.2",...
          "K1=0.4",...
40
          "K2=0.8",...
41
          "K3=1.0",...
42
          "K4=2.0",...
43
          "K5=4.0");
44
45 title('Open Loop bodemag L');
46 grid on;
47 grid minor;
48 plot_axis;
49 %% 2 Plot Try (T)
50 TO=minreal(L0/(1+L0));
51 T1=minreal(L1/(1+L1));
52 T2=minreal(L2/(1+L2));
```

```
53 T3=minreal(L3/(1+L3));
54 T4=minreal(L4/(1+L4));
55 T5=minreal(L5/(1+L5));
56 figure(2);
57 bodemag(T0);
58 hold on;
59 bodemag(T1);
60 hold on;
61 bodemag(T2);
62 hold on;
63 bodemag(T3);
64 hold on;
65 bodemag(T4);
66 hold on;
67 bodemag(T5);
68 hold off;
69 title('Complimentary Sensitivity, T_{r y}');
70 legend("K0=0.2",...
           "K1=0.4",...
71
           "K2=0.8",...
72
           "K3=1.0",...
73
           "K4=2.0",...
74
           "K5=4.0");
75
76 grid on;
77 grid minor;
78 plot_axis;
79 %% Plot Step Response
80 figure(9);
81 st0=stepplot(T0,t);
82 hold on;
83 stl=stepplot(T1,t);
84 hold on;
85 st2=stepplot(T2,t);
s6 hold on;
87 st3=stepplot(T3,t);
ss hold on;
89 st4=stepplot(T4,t);
90 hold on;
91 st5=stepplot(T5,t);
92 hold off;
93 legend("K0=0.2",...
           "K1=0.4",...
94
           "K2=0.8",...
95
           "K3=1.0",...
96
97
           "K4=2.0",...
           "K5=4.0");
98
99 ylabel('Angular Rate q (rad/s)');
100 grid on;
101 grid minor;
102 plot_axis;
```

APPENDIX B

MATLAB BASED GUI

Mark3 Ground Station

```
1 function varargout = Mark3_GUI(varargin)
2 gui_Singleton = 1;
3 gui_State = struct('gui_Name', mfilename, ...
    'gui_Singleton', gui_Singleton, ...
4
   'gui_OpeningFcn', @Mark3_GUI_OpeningFcn, ...
\mathbf{5}
   'gui_OutputFcn', @Mark3_GUI_OutputFcn, ...
6
   'gui_LayoutFcn', [] , ...
7
   'gui_Callback',
                       []);
8
9 if nargin && ischar(varargin{1})
       gui_State.gui_Callback = str2func(varargin{1});
10
11 end
12
13 if nargout
       [varargout{1:nargout}] = gui_mainfcn(gui_State, varargin{:});
14
15 else
       gui_mainfcn(gui_State, varargin{:});
16
17 end
18
19 function Mark3_GUI_OpeningFcn(hObject, eventdata, handles, varargin)
20
21 %fclose(instrfindall);
22 global udp_timer;
23 global udp_timer_2;
24 global drone;
_{25} drone(1).command_count = 50;
_{26} drone(1).command = 1234;
27 \text{ drone}(1) \cdot \text{des}_{x} = 0;
_{28} drone(1).des_y = 0.75;
29 drone(1).des_z = 0.60;
30 drone(1).des_psi = 0;
31 drone(1).polar_psi = 0;
32
33 strRec = '';
34 setappdata(hObject, 'strRec', strRec);
_{35} udp_timer = 5;
_{36} udp_timer_2 = 10;
37
38 handles.fid = fopen('roll.txt', 'a');
39 handles.output = hObject;
40 % Update handles structure
41 guidata(hObject, handles);
42 % UIWAIT makes Mark3_GUI wait for user response (see UIRESUME)
43 % uiwait (handles.figure1);
44
45
46 % ---- Outputs from this function are returned to the command line.
47 function varargout = Mark3_GUI_OutputFcn(hObject, eventdata, handles)
48
49 varargout{1} = handles.output;
50
51 function Open_Serial_Callback(hObject, eventdata, handles)
52 handles.xbee_pack_drone1=serial('COM4');
ss set(handles.xbee_pack_drone1, 'BaudRate', 230400, 'Parity', 'none',...
       'DataBits',8,'StopBits',1,...
54
```

```
'Timeout', 0.01,...
55
       'InputBufferSize',2048,...
56
57
       'OutputBufferSize',10240,...
       'BytesAvailableFcnMode', 'byte', ...
58
       'BytesAvailableFcn', {@Xbee_bytes_drone1, handles});
59
60 fopen(handles.xbee_pack_drone1);
61 handles.timer = timer('Period', 0.01, 'ExecutionMode',...
62 'FixedRate', 'TimerFcn', {@xbee_pack_drone1_Send, handles});
63 start(handles.timer);
64 guidata(hObject, handles);
65
66 function Xbee_bytes_drone1(obj,eventdata,handles)
67 global udp_timer;
68 strRec = getappdata(handles.figure1, 'strRec');
69 check=get(obj,'BytesAvailable');
70 if check
       packet = fread(obj,check,'uchar');
71
       xbee_length = length(packet);
72
       if udp_timer == 5
73
     set(handles.xbee_pack_length_drone1, 'string', num2str(xbee_length));
74
       end
75
       pack_string = char(packet');
76
       if get(handles.Write_Data,'value')
77
     fprintf(handles.fid, '%s', pack_string);
78
79
       end
       if udp_timer == 5
80
     if get(handles.data_disp, 'value')
81
set(handles.Serial_Dis, 'string', pack_string);
83
     end
84
       end
       setappdata(handles.figure1, 'strRec', strRec);
85
86 end
87
88 function Close_Serial_Callback(hObject, eventdata, handles)
stop(handles.timer);
90 delete(handles.timer);
91 stopasync(handles.xbee_pack_drone1);
92 fclose(handles.xbee_pack_drone1);
93 delete(handles.xbee_pack_drone1);
94 %fclose(instrfindall)
95 % ---- Executes on button press in pushbutton1.
96 function Open_Udp_Callback (hObject, eventdata, handles)
97 % 184 is the buffer size
98 BUFSIZE = 184;
99 % 5400 is the port number
100 PORT = 5400;
101 handles.udpReceive=udp('127.0.0.1','LocalPort',PORT,...
       'InputBufferSize', BUFSIZE, 'Timeout', Inf);
102
103 fopen(handles.udpReceive);
104 handles.udpReceive.ReadAsyncMode = 'continuous';
105 set(handles.udpReceive, 'DatagramTerminateMode', 'on');
106 handles.udpReceive.DatagramReceivedFcn={@UDPdataProtocol,handles};
107 guidata(hObject, handles);
108
109
110 % ---- Executes on button press in pushbutton2.
111 function Close_Udp_Callback (hObject, eventdata, handles)
```

```
112 stopasync(handles.udpReceive);
113 fclose(handles.udpReceive);
114 delete(handles.udpReceive);
115 %close();
116
117 function DataSend_Callback(hObject, eventdata, handles)
118 global drone;
119 str = get(hObject, 'string');
120 if length(str)==4
       drone(1).command = str2num(str);
121
122 end
123
124 function DataSend_CreateFcn(hObject, ~, handles)
   if ispc && isequal(get(hObject, 'BackgroundColor'),...
125
        get(0, 'defaultUicontrolBackgroundColor'))
126
127
        set(hObject, 'BackgroundColor', 'white');
128
   end
129
130
       -- Executes on button press in Write_Data.
131 % ---
132 function Write_Data_Callback(hObject, eventdata, handles)
133 % ---- Executes on button press in send_otus.
134 function Send_Otus_Callback (hObject, eventdata, handles)
135
136 function xbee_pack_drone1_Send(obj,event,handles)
137
138 global drone
139
   drone(1).data_command = int16(drone(1).command);
140
141
142 if get(handles.checkbox_plan, 'value')
       drone(1).polar_psi = drone(1).polar_psi + 0.4;
143
        if drone(1).polar_psi >= 180
144
     drone(1).polar_psi = -180;
145
       end
146
       drone(1).des_x = 0.75 * sin(drone(1).polar_psi*pi/180);
147
       drone(1).des_y = 0.75 * cos(drone(1).polar_psi*pi/180);
148
       drone(1).des_z = 0.6;
149
        drone(1).des_psi = -drone(1).polar_psi;
150
151
   end
152
153 data_start = [uint8(111), uint8(121), uint8(131)];
154 data_x_check = [uint8(21), uint8(101)];
155 data_y_check = [uint8(22), uint8(102)];
156 data_z_check = [uint8(23),uint8(103)];
157 data_vx_check = [uint8(24), uint8(104)];
158 data_vy_check = [uint8(25), uint8(105)];
159 data_vz_check = [uint8(26), uint8(106)];
160 data_yaw_check = [uint8(27), uint8(107)];
161 data_pitch_check = [uint8(28), uint8(108)];
162 data_roll_check = [uint8(29), uint8(109)];
163
164 data_q0_check = [uint8(31), uint8(111)];
165 \text{ data_q1_check} = [uint8(32), uint8(112)];
166 \text{ data_q2_check} = [uint8(33), uint8(113)];
   data_q3_check = [uint8(34), uint8(114)];
167
168
```

```
169 data_des_x_check = [uint8(35), uint8(115)];
170 data_des_y_check = [uint8(36), uint8(116)];
171 data_des_z_check = [uint8(37), uint8(117)];
172 data_des_psi_check = [uint8(38),uint8(118)];
173
   data_command_check = [uint8(30), uint8(110)];
174
175
   data_end = [uint8(50), uint8(75), uint8(100)];
176
177
178 drone(1).array_x=typecast(drone(1).data_x, 'uint8');
   drone(1).array_y=typecast(drone(1).data_y, 'uint8');
179
   drone(1).array_z=typecast(drone(1).data_z,'uint8');
180
181
   drone(1).array_vx=typecast(drone(1).data_vx, 'uint8');
182
   drone(1).array_vy=typecast(drone(1).data_vy, 'uint8');
183
   drone(1).array_vz=typecast(drone(1).data_vz, 'uint8');
184
185
186 drone(1).array_roll=typecast(drone(1).data_roll,'uint8');
187 drone(1).array_pitch=typecast(drone(1).data_pitch,'uint8');
188 drone(1).array_yaw=typecast(drone(1).data_yaw, 'uint8');
189
190 drone(1).array_q0=typecast(drone(1).data_q0,'uint8');
191 drone(1).array_q1=typecast(drone(1).data_q1, 'uint8');
upper drone(1).array_q2=typecast(drone(1).data_q2,'uint8');
193 drone(1).array_q3=typecast(drone(1).data_q3, 'uint8');
194
195 data_des_x = single(drone(1).des_x);
196 data_des_y = single(drone(1).des_y);
197 data_des_z = single(drone(1).des_z);
198 data_des_psi = single(drone(1).des_psi);
199
200 drone(1).array_des_x=typecast(data_des_x,'uint8');
201 drone(1).array_des_y=typecast(data_des_y,'uint8');
202 drone(1).array_des_z=typecast(data_des_z,'uint8');
203 drone(1).array_des_psi=typecast(data_des_psi,'uint8');
204
205 drone(1).array_command=typecast(drone(1).data_command,'uint8');
   %clc;
206
207
208
   packet = [data_start ...
       data_x_check drone(1).array_x ...
209
       data_y_check drone(1).array_y ...
210
       data_z_check drone(1).array_z ...
211
       data_vx_check drone(1).array_vx ...
212
       data_vy_check drone(1).array_vy ...
213
       data_vz_check drone(1).array_vz ...
214
       data_yaw_check drone(1).array_yaw ...
215
       data_pitch_check drone(1).array_pitch ...
216
       data_roll_check drone(1).array_roll ...
217
       data_q0_check drone(1).array_q0 ...
218
219
       data_q1_check drone(1).array_q1 ...
220
       data_q2_check drone(1).array_q2 ...
221
       data_q3_check drone(1).array_q3 ...
       data_des_x_check drone(1).array_des_x ...
222
223
       data_des_y_check drone(1).array_des_y ...
       data_des_z_check drone(1).array_des_z ...
224
       data_des_psi_check drone(1).array_des_psi ...
225
```

```
226
       data_command_check drone(1).array_command ...
       data_end];
227
228
   if get(handles.send_otus, 'value')
229
       fwrite(handles.xbee_pack_drone1, packet, 'uchar');
230
231 end
232
233
234 % ---- Executes on button press in pushbutton6.
235 function Exit_Callback(hObject, eventdata, handles)
236 fclose(handles.fid);
237 close();
238
239
240
241
   function xbee_pack_drone1_Callback(hObject, eventdata, handles)
242
243 function xbee_pack_dronel_CreateFcn(hObject, eventdata, handles)
244
245 if ispc && isequal(get(hObject, 'BackgroundColor'),...
       get(0, 'defaultUicontrolBackgroundColor'))
246
       set(hObject, 'BackgroundColor', 'white');
247
248 end
249
250
251 % ---- Executes on button press in checkbox_plan.
252 function checkbox_plan_Callback(hObject, eventdata, handles)
```

UDP Protocol

```
1 function UDPdataProtocol(obj,event,handles)
2 byte_vector = fread(handles.udpReceive,1);
3 if mod(length(uint8(byte_vector)),8) == 0
4 double_vector = typecast(uint8(byte_vector), 'double');
5 end
6 controller_id = strcat(native2unicode(byte_vector(1)),...
                           native2unicode(byte_vector(2)),...
\overline{7}
                           native2unicode(byte_vector(3)),...
8
9
                           native2unicode(byte_vector(4)),...
                           native2unicode(byte_vector(5)),...
10
                           native2unicode(byte_vector(6)),...
11
                           native2unicode(byte_vector(7)),...
12
                           native2unicode(byte_vector(8)));
13
14
15 timestamp = double_vector(2);
16
17 lin_pos_x = double_vector(3);
18 lin_pos_y = double_vector(4);
19 lin_pos_z = double_vector(5);
20
21 lin_vel_x = double_vector(6);
22 lin_vel_y = double_vector(7);
23 lin_vel_z = double_vector(8);
24
_{25} lin_acc_x = double_vector(9);
26 lin_acc_y = double_vector(10);
```

```
27 lin_acc_z = double_vector(11);
28
29 quaternion_x = double_vector(12);
30 guaternion_y = double_vector(13);
31 quaternion_z = double_vector(14);
32 quaternion_w = double_vector(15);
33
34 ang_vel_x = double_vector(16);
35 ang_vel_y = double_vector(17);
36 ang_vel_y = double_vector(18);
37
38 ang_acc_x = double_vector(19);
  ang_acc_y = double_vector(20);
39
40 ang_acc_z = double_vector(21);
41
42 button_1 = double_vector(22);
43 button_2 = double_vector(23);
44
45 global udp_timer;
46
47 global drone;
48
  if controller_id == '67C87001'
49
       drone(1).data_x=single(-lin_pos_z);
50
       drone(1).data_y=single(-lin_pos_x);
51
       drone(1).data_z=single(-lin_pos_y);
52
53
       drone(1).data_vx=single(-lin_vel_z);
54
       drone(1).data_vy=single(-lin_vel_x);
55
       drone(1).data_vz=single(-lin_vel_y);
56
57
       drone(1).quat = [quaternion_w,...
58
                       -quaternion_z,...
59
                       -quaternion_x,...
60
                         quaternion_y];
61
       tmp_eul = quat2eul(drone(1).quat) * 57.29578;
62
       drone(1).data_yaw=single(tmp_eul(1));
63
       drone(1).data_pitch=single(tmp_eul(2));
64
       drone(1).data_roll=single(tmp_eul(3));
65
66
       drone(1).data_q0 = single(drone(1).quat(1));
67
       drone(1).data_q1 = single(drone(1).quat(2));
68
       drone(1).data_q2 = single(drone(1).quat(3));
69
       drone(1).data_q3 = single(drone(1).quat(4));
70
71 end
72
73 if udp_timer == 5
r4 set(handles.data_show_x,'string',num2str(drone(1).data_x));
r5 set(handles.data_show_y,'string',num2str(drone(1).data_y));
r6 set(handles.data_show_z,'string',num2str(drone(1).data_z));
77
r8 set(handles.data_show_vx,'string',num2str(drone(1).data_vx));
r9 set(handles.data_show_vy,'string',num2str(drone(1).data_vy));
set(handles.data_show_vz,'string',num2str(drone(1).data_vz));
81
set(handles.data_show_roll, 'string',num2str(drone(1).data_roll));
83 set(handles.data_show_pitch,'string',num2str(drone(1).data_pitch));
```

```
s4 set(handles.data_show_yaw,'string',num2str(drone(1).data_yaw));
s5 udp_timer = 1;
s6 else
s7 udp_timer = udp_timer + 1;
s8 end
```

APPENDIX C

MARK3 FLIGHT CONTROLLER FIRMWARE

Mark3 Flight Controller Code - Main Loop

```
1 #include "Copter.h"
2 #include "Interrupt.h"
3
   _Copter Copter;
4 SBUS R9DS(Serial2);
   void setup()
\mathbf{5}
6 {
      InitComm(); //Teensy 3.2
7
8
      Copter.Copter_Init();
   }
9
   void loop()
10
11
   {
12
      Copter.loopClock1 = micros();
      Copter.Ctrl_timer1++; //100Hz
13
14
      RC_refine();
      Copter.AHRS();
15
      Copter.PEST();
16
      Copter.TranslationControl();
17
      Copter.AttitudeControl();
18
19
      Copter.AltitudeControl();
      Copter.InputTransform();
20
^{21}
      Copter.command_Comm();
      Copter.Copter_Check();
22
23 }
```



```
1 #include <Eigen.h>
2 #include <Eigen/LU>
3 #include "Arduino.h"
4 #include "i2c_t3.h"
5 #include "EEPROM.h"
6 #include SBUS.h>
7 #include "System.h"
8 #include "System.h"
9 #include "Sensor.h"
10 #include "Motor.h"
11 #include <cmath>
    #define LED0 13
12
13 #define LED1 31
    #define LED2 33
14
15
    #define Attitude_mode 1
    #define Altitude_mode 2
16
    #define loiter_mode 3
17
    using namespace Eigen;
18
    class _Copter
19
20
    {
       public:
21
22
                                                               -*/
         /*Copter.cpp*/
unsigned long loopClock1 = 0, loopClock2 = 0;
23
24
         void Copter_Init();
25
26
         void Copter_Check();
         struct _flag
27
^{28}
         {
            uint8_t ARMED = 0;
29
            uint8_t takingoff = 0;
30
            int8_t turnoff = 0;
31
            uint8_t CRASHED = 0;
32
            uint8_t AltEmergency = 0;
33
            int8_t calibratedA = 0;
34
            int8_t calibratedG = 0;
35
            int8_t calibrationOn = 0;
36
37
            uint8_t mode = 0;
```

```
38
           uint8_t momentstart = 0;
           uint8_t LoiterSwitch = 0;
39
40
         };
^{41}
         _flag flag;
         int16_t gltimer = 0, rltimer = 0;
42
         int8_t glch = 10, rlch = 10;
43
44
45
         /*Motor.cpp*/
46
         void MotorModel(double omega1, double
                           omega2, double omega3, double omega4);
47
         void MotorRun();
48
49
         void Motor_init();
         void Motor_stop();
50
         void InputTransform();
51
         /*Comm.cpp*/
52
         uint8_t xbee_data[500];
53
         int16_t xbee_length;
54
         int16_t xbeetime1 = 0;
55
         void command_Comm();
56
         void Xbee_comm();
57
         void Xbee_Packet();
58
         void Xbee_receive(int16_t order, uint16_t stmp);
59
         struct _RCsignal
60
61
         {
62
           short
                  ROLL;
           short
                  PITCH;
63
                  THROTTLE;
64
           short
65
           short
                  YAW;
           short
                  MODÉ;
66
67
           short
                  SWITCH:
                  CH7:
68
           short
69
           short
                  CH8:
70
           \operatorname{short}
                   CH9;
71
           short
                  CH10;
72
         }:
         RCsignal RCsignal;
73
         short Xbee_timer = 0;
74
         short Xbee_receive_timer = 0;
75
         short comorder; /*---Command---
short datalength = 0;
76
                                           -*/
77
78
         /*Interrupt.cpp*/
79
         struct _IRpulse
80
         {
           int32_t ringbuffer[30];
81
           unsigned long timer_up, timer_down;
82
83
         };
_IRpulse VRsensor1;
84
85
         /*Sensor.cpp*/
86
87
         void InitSensor();
         uint8_t I2Cwrite(uint8_t SENSOR_ADDRESS,
88
                            uint8_t SENSOR_REGISTER,
89
                            uint8_t SENSOR_VALUE,
90
                            bool sendStop);
91
         uint8_t I2CRead(uint8_t SENSOR_ADDRESS
92
                           uint8_t SENSOR_REGISTER,
93
                           uint8_t nbytes);
^{94}
         void MPU6050read();
95
         void MPU6050ThermalCompensation();
96
97
         void MPU6050Sixpoint();
         void MPU6050AccCali(uint8_t point);
98
         void MPU6050GyroCali();
99
         void AccPointRead();
100
         float GyroCollection [3] = \{0, 0, 0\};
101
         float gyro_temp, temperature;
102
103
         int16_t mpu_temperature;
         short GyroCaliFlag = 0;
104
         uint8_t i2cData[30];
105
```

```
106
          uint8_t i2c1Data[30];
          struct _float {
   float x;
107
108
             float y;
float z;
109
110
111
          };
          struct _lint16 {
112
             short x;
113
114
             short y;
             short z;
115
116
          };
117
          struct _trans {
   struct _lint16 origin;
118
             struct _float filter;
struct _float histor;
struct _float aftcal;
119
120
121
             struct _float quietf;
struct _float tempcp;
struct _float radian;
122
123
124
125
          };
126
          struct _sensor {
   struct _trans acc;
127
128
             struct _trans gyro;
129
          };
           _sensor gy89, gy86;
130
          struct _Acc_Cali {
131
             int16_t acc_calitimer = 0;
int32_t acc_calitmpx;
132
133
134
             int32_t acc_calitmpy;
135
             int32_t acc_calitmpz;
             int16_t accel_raw_ref[6][3];
136
             float acc_offset [3];
137
138
             float a[3][3];
             float T[3][3];
139
140
             float g = 8192; //+-4g
          };
141
          Acc_Cali Acc_Cali;
142
143
          /*AttitudeEstimator.cpp*/
144
          float inte_gyro[3];
struct _LKF
145
146
147
          {
             float p;
148
             float q;
149
150
             float p_bias;
151
             float q_bias;
             float p_raw;
float q_raw;
152
153
154
             float acc_roll;
155
             float acc_pitch;
156
          };
_LKF LKF;
157
158
                      -----Position Estimator-----*/
159
           /*-----
          union {
160
             float f;
161
162
             unsigned long ul;
          } otus_tmp;
163
          union {
float f;
164
165
             uint8_t ul[4];
166
          } xbee_tmp;
167
          struct _Otus
168
169
          {
             float x;
170
             float y;
171
172
             float z;
             float vx;
173
             float vy;
```

174

175	float vz;
176	float yaw;
177	float pitch;
178	float yow sin:
180	float vaw cos:
181	float q0:
182	float q1;
183	float q_2 ;
184	float $q3;$
185	};
186	LOtus Otus;
187	<pre>void Linear_Kalman_Filter();</pre>
188	<pre>struct _state {</pre>
189	float phi;
190	float theta;
191	float psi;
192	float theta rad:
194	float psi rad:
195	float phi_sin;
196	float theta_sin;
197	<pre>float psi_sin;</pre>
198	float phi_cos;
199	float theta_cos;
200	float psi_cos;
201	float a:
202	float r:
204	float p_rad;
205	$float$ $q_rad;$
206	float r_rad;
207	float ax_b;
208	float ay_b;
209	float az_D;
210	float av:
212	float az;
213	float vx;
214	float vy;
215	float vz;
216	float x;
217	float z:
218	int16 t comm:
220	,
221	$int16_t takeoff_t = 0;$
222	$int16_t landing_t = 0;$
223	uint8_t standby;
224	uint8_t takeoff;
225 226	uint8 t land.
220	bool flight state $[4]$.
228	float tmp_U1:
229	bool $update_phi = 0;$
230	bool $update_theta = 0;$
231	bool update_psi = $0;$
232	<pre>//bool update_p;</pre>
233	<pre>//bool update_q;</pre>
234	//bool update_r;
235	bool update_vx = $0;$
236	bool update_vy = 0; bool update $yz = 0$;
237 238	bool update $x = 0$;
239	bool update_ $v = 0;$
240	bool update_ $z = 0;$
241	};
242	_state state;
243	struct _IMU {
244	float phi;
245	float theta;

```
246
            float psi;
           float phi_rad;
float theta_rad;
247
248
249
            float psi_rad;
250
            float phi_sin;
            float theta_sin;
251
252
            float psi_sin;
253
            float phi_cos;
254
            float theta_cos;
255
            float psi_cos;
            float p;
256
            {\tt float} \ q;
257
258
            float r;
259
            float p_rad;
           float q_rad;
float r_rad;
260
261
262
         IMU IMU;
263
         struct _PosKF {
264
            float P[3][3];
265
            float tmp[3][3];
266
            float tmp_s[6];
267
268
            float state[3];
            float a;
269
270
            float v;
271
            float ps;
            float S[2][2];
272
273
            float y[3];
274
            float K[3][3];
275
            float Q;
            float R0;
276
277
            float R1;
278
         };
_PosKF PosX, PosY, PosZ;
279
         float q0 = 1.0 f;
280
281
         float q1 = 0.0 f;
         float q_2 = 0.0 f;
282
         float q3 = 0.0 f;
283
         float q3old = 0.0 f;
284
285
         float exInt = 0.0;
286
         float eyInt = 0.0;
287
         float ezInt = 0.0;
         float twoKp = twoKpDef;
288
         float twoKi = twoKiDef;
289
290
         float beta = betaDef;
291
         float integralFBx = 0.0f, integralFBy = 0.0f, integralFBz = 0.0f;
292
293
         void PEST();
         void Pos_Kalman(struct _PosKF *P_tmp);
294
         void AHRS_Check();
295
         void Madgwick_MARG_Update();
296
         //void MadgwickAHRSupdateIMU(float gx, float gy, float gz, float ax, float ay, float az);
297
298
         void MahonyAHRSupdate(float gx, float gy, float gz,
                                   float ax, float ay, float az,
float mx, float my, float mz);
299
300
         void MahonyAHRSupdateIMU(float gx, float gy, float gz,
301
                                       float ax, float ay, float az);
302
303
         void AHRS_filter_init();
         void KF_init();
304
305
         void AHRS();
         void State_Reset();
306
307
         void AHRS_filter();
         void gy86_Dataanl();
308
         struct _IIR {
  float b0;
309
310
            float b1;
311
312
            float b2;
            float a1;
313
            float a2;
314
```

315float element0; float element1; 316 float element2; 317 318 }; _IIR _IIR gyro_IIRx, gyro_IIRy, gyro_IIRz, acc_IIRx, acc_IIRy, acc_IIRz; 319 320 void IIR_set_cutoff_frequency(float sample_freq, 321float cutoff_freq , 322 323 struct _IIR *input_IIR); 324325float sample, struct _IIR *input_IIR); 326 double integral_r = 0; 327 328 /*Control part*/ float U1, U2, U3, U4; 329 330 331 uint8_t LockYaw = 0;struct _Ztransform { 332 float Input $[5] = \{0, 0, 0, 0, 0\};$ float Output $[5] = \{0, 0, 0, 0, 0\};$ 333 334 335float Integral; 336 }; -Ztransform Pcon, Qcon, Rcon, Phicon, Thetacon, Psicon, Vzcon, Zcon, Vxpre, 337 338 339 Xpre, Vxcon, Xcon, Vypre, Ypre, Vycon, Ycon; struct _Target 340 341{ float phi; 342 float theta; 343 344float psi; 345float phi_rad; float theta_rad; 346 347 float sin_phi; 348 float cos_phi; 349float sin_theta; float cos_theta; 350float psi_rad; 351 float p; 352353float q; float r; 354355float p_rad; float q_rad; 356 float r_rad; 357358int16_t throttle; 359float x; float y; 360 float z; 361 362 float vx; 363 float vy; float vz; 364 365 float plan_x; 366 float plan_y; float plan_z; 367368 float plan_psi; 369 }; struct _PIDpram 370371{ 372float Kp; float Ki; 373float Kd; 374 375376377 378 $uint 8_t Ctrl_timer 1 = 0;$ 379float EstimatedG; 380 void ControlReset(); 381 void TranslationControl(); 382 383 void AttitudeControl(); void AltitudeControl(); 384

```
385
          void ZControl();
386
          void VzControl();
387
          void AngularRateControl();
          struct _inertia
388
389
          {
             uint8_t timer_start = 0;
390
             unsigned long time_start = 0, time_end = 0, time_count = 0;
391
392
             uint16_t pendulum = 0;
393
             float memo = -1000.0;
             uint8_t xbee_timer = 0;
394
395
          };
396
          _inertia inertia;
397
          /*System.cpp*/
398
          uint16_t run_period;
          unsigned short time_out = 0;
unsigned short battery_warning = 0;
399
400
401
          void InitControl();
          void Moment_Check();
402
403
          void Otus_Clear();
          void Loop_Check();
404
          void Timer_Check();
405
          void Battery_Check();
406
          float Rad(float angle);
407
          float Degree(float rad);
408
          float data_limitation(float a, float b, float c);
409
          float invSqrt(float number);
410
411
          float voltage;
412
          float voltageavg;
413
414
          /*-
                                                               -*/
415
        private:
                                                                -*/
416
           /*-
417
          /*Copter.cpp*/
418
419
           /*Motor.cpp*
          float PWM1, PWM2, PWM3, PWM4;
420
          \begin{array}{l} \mbox{double omega12}\,,\,\,\mbox{omega22}\,,\,\,\mbox{omega32}\,,\\ \mbox{omega42}\,,\,\,\mbox{omega1}\,,\,\,\mbox{omega2}\,,\,\,\mbox{omega3}\,,\,\,\mbox{omega4}\,; \end{array}
421
422
423
          float pwm_factor = 65535.0 / 2500.0;
          float PWM;
424
          double InputK1;
425
          double InputK2;
426
          double InputK3;
427
          double InputK4;
428
429
430
          /*System.cpp*/
          unsigned long whole_timer;
431
432
433
          /*-
                                                                -*/
     };
434
```

Mark3 Flight Controller Code - State Estimation

```
1 #include "Copter.h"
\mathbf{2}
  /*
     MatrixXf Pos_F(9, 9);
3
     MatrixXf Pos_B(9, 9);
4
     MatrixXf Pos_H(9, 9);
\mathbf{5}
     MatrixXf Pos_Q(9, 9);
6
     MatrixXf Pos_R(9, 9);
7
     MatrixXf Pos_S(9, 9);
8
     MatrixXf Pos_K(9, 9);
9
     MatrixXf Pos_P(9, 9);
10
     MatrixXf Pos_I(9, 9);
11
     MatrixXf Pos_State(9, 1);
12
     MatrixXf Pos_Y(9, 1);
13
```

```
14
     MatrixXf Pos_U(9, 1);
15
     MatrixXf Pos_Z(9, 1);
16
   */
17
   void _Copter::PEST()
   {
18
     if (Ctrl_timer1 \ge 4)
19
20
     ł
       float OtusNorm = invSqrt(Otus.q0 * Otus.q0 + Otus.q1
21
22
       *  Otus.q1 + Otus.q2 *  Otus.q2 + Otus.q3 *  Otus.q3);
       Otus.q0 *= OtusNorm;
23
       Otus.q1 *= OtusNorm;
Otus.q2 *= OtusNorm;
24
25
26
       Otus.q3 *= OtusNorm;
27
28
29
       MatrixXf Otus_R(3, 3);
       MatrixXf Acc_B(3, 1);
30
       MatrixXf Acc_I(3, 1);
31
32
       33
34
35
36
       q0_2 = Otus.q0 * Otus.q0;
       q1_2 = Otus.q1 * Otus.q1;
37
       q_{2_-2} = Otus.q_2 * Otus.q_2;
38
       q_{3_2} = Otus.q_3 * Otus.q_3;
39
40
       q1q2 = Otus.q1 * Otus.q2;
41
       q0q3 = Otus.q0 * Otus.q3;
42
43
       q1q3 = Otus.q1 * Otus.q3;
       q0q2 = Otus.q0 * Otus.q2;
44
       q2q3 = Otus.q2 * Otus.q3;
45
       q0q1 = Otus.q0 * Otus.q1;
46
47
       Otus_R << q0_2 + q1_2 - q2_2 - q3_2, 2 *
48
               (q1q2 - q0q3), 2 * (q1q3 + q0q2),
49
               2 * (q1q2 + q0q3), q0_2 - q1_2 + q2_2 -
50
               51
52
               q0_2 - q1_2 - q2_2 + q3_2;
53
54
       Acc_B << gy86.acc.filter.x / 8192.0 * 9.8 ,
55
56
       gy86.acc.filter.y / 8192.0 * 9.8 ,
       gy86.acc.filter.z / 8192.0 * 9.8;
57
58
        Acc_I = Otus_R * Acc_B;
59
60
       state.ax = Acc_I(0, 0);
       {\tt state.ay}\,=\,-\,{\tt Acc\_I}\,(1\,,\ 0\,)\,;
61
       state.az = Acc_{I}(2, 0) - 9.8;
62
63
       float CF_a = 0.8, outerT_2 = outerT * outerT;
64
       state.vx = (state.vx + outerT * state.ax)
65
       * CF_a + Otus.vx * (1 - CF_a);
66
67
       state.vy = (state.vy + outerT * state.ay)
       * CF_a + Otus.vy * (1 - CF_a);
68
69
       state.vz = (state.vz + outerT * state.az)
70
       * CF_a + Otus.vz * (1 - CF_a);
71
       state.x = (state.x + outerT * state.vx +
72
       0.5 * outerT_2 * state.ax) * CF_a + Otus.x * (1 - CF_a);
73
       state.y = (state.y + outerT * state.vy +
74
       0.5 * outerT_2 * state.ay) * CF_a + Otus.y * (1 - CF_a);
75
       state.z = (state.z + outerT * state.vz +
76
77
       0.5 * \text{outerT}_2 * \text{state.az} * \text{CF}_a + \text{Otus.z} * (1 - \text{CF}_a);
78
     }
79
   }
   void _Copter:: Pos_Kalman(struct _PosKF *P_tmp)
80
```

```
81
           {
                  P_tmp \rightarrow tmp_s[0] = P_tmp \rightarrow a / 20000 + P_tmp \rightarrow state[0] +
  82
  83
                   P_tmp->state[1] / 100 - P_tmp->state[2] / 20000;
                   P_{tmp} \rightarrow tmp_s [1] = P_{tmp} \rightarrow a / 100 + P_{tmp} \rightarrow state [1] -
  84
                   P_tmp->state[2] / 100;
  85
                   P_{tmp} \rightarrow tmp_s[2] = P_{tmp} \rightarrow state[2];
  86
  87
                   P_{tmp} \rightarrow state[0] = P_{tmp} \rightarrow tmp_s[0];
  88
                   P_{tmp} \rightarrow state[1] = P_{tmp} \rightarrow tmp_s[1];
  89
                   P_{tmp} \rightarrow state[2] = P_{tmp} \rightarrow tmp_s[2];
  90
                  P_tmp \rightarrow tmp[0][0] = P_tmp \rightarrow P[0][0] +
  91
                  92
  93
  94
                   P_{tmp} \rightarrow P[1][2] / 2000000 - P_{tmp} \rightarrow P[2][0] / 20000 - P_{tmp}
  95
  96
                   P_{tmp} \rightarrow P[2][1] / 2000000 +
                   P_tmp->P[2][2]
                                                                    / 40000000;
  97
                   P_{tmp} \rightarrow tmp[0][1] = P_{tmp} \rightarrow P[0][1] -
  98
                  P_{tmp} \rightarrow P[0][2] / 100 +
 99
100
                   P_tmp \rightarrow P[1][1] / 100 - P_tmp \rightarrow P[1][2] / 10000 - P_tmp \rightarrow P_
                  P_{tmp} \rightarrow P[2][1] / 20000 + P_{tmp} \rightarrow P[2][2] / 2000000;
101
                   P_tmp \rightarrow tmp [0] [2] = P_tmp \rightarrow P[0] [2] +
102
                  P_tmp->P[1][2] / 100 -
P_tmp->P[2][2] / 20000;
103
104
                   P_{tmp} \rightarrow tmp[1][0] = P_{tmp} \rightarrow P[1][0] +
105
106
                   P_tmp \rightarrow P[1][1] / 100 -
                  P_tmp=>P[1][2] / 20000 - P_tmp=>P[2][0] / 100 -
P_tmp=>P[2][1] / 10000 + P_tmp=>P[2][2] / 20000
107
                                                                    / 10000 + P_tmp \rightarrow P[2][2] / 2000000;
108
                  P_{tmp} \rightarrow tmp[1][1] = P_{tmp} \rightarrow P[1][1]
109
                   P_tmp->P[1][2] / 100 -
110
111
                   P_{tmp} \rightarrow P[2][1] / 100 + P_{tmp} \rightarrow P[2][2] / 10000;
                  P_{tmp} \rightarrow tmp [1] [2] = P_{tmp} \rightarrow P [1] [2] -
112
113
                   P_tmp \rightarrow P[2][2] / 100;
                  P_{tmp} \rightarrow tmp[2][0] = P_{tmp} \rightarrow P[2][0] +
114
                   P_{tmp} \rightarrow P[2][1] / 100 - P_{tmp} \rightarrow P[2][2] / 20000;
115
                   P_{tmp} \to tmp[2][1] = P_{tmp} \to P[2][1] -
116
                  117
118
119
                   for (uint8_t i = 0; i < 3; i++)
120
                          for (uint8_t j = 0; j < 3; j++)
121
                                P_tmp \rightarrow P[i][j] = P_tmp \rightarrow tmp[i][j];
122
                                                   -y = Z - H * state;
123
                   P_{tmp} \rightarrow y[0] = P_{tmp} \rightarrow ps - P_{tmp} \rightarrow state[0];
124
125
                   P_{tmp} \rightarrow y[1] = P_{tmp} \rightarrow v - P_{tmp} \rightarrow state[1];
                                                        -S = H * P * H' + R; --
126
                   /*---
                                                                                                                                         --*/
                   P_tmp \rightarrow S[0][0] = P_tmp \rightarrow P[0][0] + P_tmp \rightarrow R0;
127
128
                   P_{tmp} > S[0][1] = P_{tmp} > P[0][1];
                   P_{tmp} \rightarrow S[1][0] = P_{tmp} \rightarrow P[1][0];
129
130
                   P_tmp \rightarrow S[1][1] = P_tmp \rightarrow P[1][1] + P_tmp \rightarrow R1;
131
                                                         -pinv(S)-
132
                   P_{tmp} \rightarrow tmp_s[1] = P_{tmp} \rightarrow S[0][0] *
133
                   P_{tmp} > S[0][0] + P_{tmp} > S[1][0] * P_{tmp} > S[1][0];
                   P_{tmp} \rightarrow tmp_s[3] = (P_{tmp} \rightarrow S[0][0] *
134
                   P_{tmp} \rightarrow S[0][1]) / P_{tmp} \rightarrow tmp_s[1];
135
136
                   P_tmp \rightarrow tmp_s[4] = (P_tmp \rightarrow S[1][0] *
                   P_tmp \rightarrow S[1][1]) / P_tmp \rightarrow tmp_s[1];
137
138
                   P_tmp \rightarrow tmp_s [5] = P_tmp \rightarrow S [0] [1] -
139
                   P_tmp \rightarrow S[0][0] * (P_tmp \rightarrow tmp_s[3] + P_tmp \rightarrow tmp_s[4]);
140
                   P_tmp \rightarrow tmp_s[0] = P_tmp \rightarrow S[1][1] -
141
                   P_{tmp} \rightarrow S[1][0] * (P_{tmp} \rightarrow tmp_s[3] + P_{tmp} \rightarrow tmp_s[4]);
142
                  P_{tmp} \rightarrow tmp_{s}[2] = P_{tmp} \rightarrow tmp_{s}[5] *
143
                   P_{tmp} \rightarrow tmp_s[5] + P_{tmp} \rightarrow tmp_s[0] * P_{tmp} \rightarrow tmp_s[0];
144
```

```
152
```

```
145
                  if (P_tmp \rightarrow tmp_s[1] = 0)
                       P_tmp \rightarrow tmp_s[1] = 0.0000001;
146
                  if (P_tmp \rightarrow tmp_s [2] = 0)
147
                       P_tmp \rightarrow tmp_s[2] = 0.0000001;
148
                 P_{tmp} \rightarrow tmp [0] [0] = P_{tmp} \rightarrow S [0] [0] /
149
                 P_tmp \rightarrow tmp_s[1] -
150
                  ((P_tmp \rightarrow tmp_s[5]) * (P_tmp \rightarrow tmp_s[3] +
151
                  P_tmp \rightarrow tmp_s[4])) / P_tmp \rightarrow tmp_s[2];
152
                 P_{tmp} \rightarrow tmp[0][1] = P_{tmp} \rightarrow S[1][0] / P_{tmp} \rightarrow tmp_{s}[1] - P
153
                  ((P_tmp \rightarrow tmp_s[0]) * (P_tmp \rightarrow tmp_s[3] +
154
                  P_tmp \rightarrow tmp_s[4])) / P_tmp \rightarrow tmp_s[2];
155
156
                 P_tmp \rightarrow tmp[1][0] = (P_tmp \rightarrow tmp_s[5]) /
                 P_tmp=>tmp_s[2];
P_tmp=>tmp[1][1] = (P_tmp=>tmp_s[0]) /
157
158
                 P_tmp \rightarrow tmp_s [2];
159
160
                                             -K = P*H'*pinv(S);
                 P_tmp \to K[0][0] = P_tmp \to P[0][0] *
161
                 P_{tmp} \rightarrow tmp [0] [0] + P_{tmp} \rightarrow P[0] [1] * P_{tmp} \rightarrow tmp [1] [0];
162
                 P_tmp \rightarrow K[0][1] = P_tmp \rightarrow P[0][0]
163
                 P_{tmp} \rightarrow tmp[0][1] + P_{tmp} \rightarrow P[0][1] * P_{tmp} \rightarrow tmp[1][1];
164
                 P_{tmp} \to K[1][0] = P_{tmp} \to P[1][0] *
165
166
                 P_{tmp} \rightarrow tmp[0][0] + P_{tmp} \rightarrow P[1][1] * P_{tmp} \rightarrow tmp[1][0];
                 P_{tmp} \rightarrow K[1][1] = P_{tmp} \rightarrow P[1][0]
167
168
                 P_tmp \rightarrow tmp[0][1] + P_tmp \rightarrow P[1][1] * P_tmp \rightarrow tmp[1][1];
                 P_{tmp} \rightarrow K[2][0] = P_{tmp} \rightarrow P[2][0] *
169
                 P_{tmp} \rightarrow tmp[0][0] + P_{tmp} \rightarrow P[2][1] * P_{tmp} \rightarrow tmp[1][0];
170
171
                 P_{tmp} \to K[2][1] = P_{tmp} \to P[2][0] *
                 P_{tmp} \rightarrow tmp[0][0] + P_{tmp} \rightarrow P[2][1] * P_{tmp} \rightarrow tmp[1][0];
172
                                                           -state = state + K*y;-
173
                 P_tmp \rightarrow tmp_s[0] = P_tmp \rightarrow state[0];
174
                 P_{tmp} \rightarrow tmp_s[1] = P_{tmp} \rightarrow state[1];
175
176
                 P_{tmp} \rightarrow tmp_s[2] = P_{tmp} \rightarrow state[2];
177
                 P_{tmp} \rightarrow state[0] = P_{tmp} \rightarrow tmp_{s}[0] +
178
                 P_tmp \rightarrow K[0][0] * P_tmp \rightarrow y[0] +
179
                 P_{tmp} \rightarrow K[0][1] * P_{tmp} \rightarrow y[1];
180
                 P_tmp \rightarrow state[1] = P_tmp \rightarrow tmp_s[1] +
181
                 182
183
                 P_{tmp} \rightarrow state[2] = P_{tmp} \rightarrow tmp_s[2] +
184
                 P_tmp \rightarrow K[2][0] * P_tmp \rightarrow y[0] +
185
186
                 P_tmp \to K[2][1] * P_tmp \to y[1];
187
                                           -state = state + K*y;
                  for (uint8_t i = 0; i < 3; i++)
188
                       for (uint8_t j = 0; j < 3; j++)
189
190
                             P_{tmp} \rightarrow tmp[i][j] = P_{tmp} \rightarrow P[i][j];
191
                  P_tmp \rightarrow P[0][0] = - P_tmp \rightarrow K[0][1] *
192
                 P_tmp \rightarrow tmp[1][0] - P_tmp \rightarrow tmp[0][0] *
193
194
                  (P_tmp \rightarrow K[0][0] - 1);
                 P_{tmp} \rightarrow P[0][1] = -P_{tmp} \rightarrow K[0][1] *
195
196
                 P_tmp \rightarrow tmp [1] [1] - P_tmp \rightarrow tmp [0] [1] *
197
                  (P_tmp \rightarrow K[0][0] - 1);
                 \dot{P}_{tmp} \rightarrow P[\dot{0}][\dot{2}] = - \dot{P}_{tmp} \rightarrow K[0][1] *
198
                 P_tmp \rightarrow tmp[1][2] - P_tmp \rightarrow tmp[0][2] *
199
200
                  (P_tmp \rightarrow K[0][0] - 1);
                 P_{tmp} \rightarrow P[1][0] = -P_{tmp} \rightarrow K[1][0] *
201
                 P_{tmp} \rightarrow tmp[0][0] - P_{tmp} \rightarrow tmp[1][0] * (P_{tmp} \rightarrow K[1][1] - 1);
202
203
                  P_{tmp} \rightarrow P[1][1] = -P_{tmp} \rightarrow K[1][0] *
204
205
                 P_tmp \rightarrow tmp[0][1] - P_tmp \rightarrow tmp[1][1] *
                  (P_tmp \rightarrow K[1][1] - 1);
206
                  \begin{array}{l} P_{tmp} \rightarrow P[1][2] = - P_{tmp} \rightarrow K[1][0] * \\ P_{tmp} \rightarrow tmp[0][2] - P_{tmp} \rightarrow tmp[1][2] * \end{array} 
207
```

```
208
```

```
209
       (P_tmp \rightarrow K[1][1] - 1);
       P_tmp \rightarrow P[2][0] = P_tmp \rightarrow tmp[2][0] -
210
       P_tmp=>K[2][0] * P_tmp=>tmp[0][0] -
P_tmp=>K[2][1] * P_tmp=>tmp[1][0];
211
212
       P_{tmp} \rightarrow P[2][1] = P_{tmp} \rightarrow tmp[2][1] -
213
       P_{tmp} \rightarrow K[2][0] * P_{tmp} \rightarrow tmp[0][1] -
214
       P_tmp \rightarrow K[2][1] * P_tmp \rightarrow tmp[1][1];
215
       216
217
       P_{tmp} \rightarrow K[2][1] * P_{tmp} \rightarrow tmp[1][2];
218
219
    }
220
    void _Copter::AHRS_Check()
221
    {
222
       state.p = IMU.p;
       state.p_rad = IMU.p_rad;
223
       state.q = IMU.q;
224
       state .q_rad = IMU.q_rad;
225
226
       state.r = IMU.r;
       {\tt state.r\_rad} \ = \ IMU.r\_rad;
227
228
       if (Ctrl_timer1 \ge 4)
229
230
       {
231
                                 -Phi-
                                                           -*/
         if (state.update_phi)
232
233
         {
            if (abs(IMU.phi - Otus.roll) < 5.0)
234
235
              state.phi = IMU.phi * 0.75 + Otus.roll * 0.25;
            else
236
              state.phi = IMU.phi * 0.99 + Otus.roll * 0.01;
237
238
         }
         else
239
            state.phi = IMU.phi;
240
         state.phi_rad = Rad(state.phi);
241
                               -Theta-
                                                            -*/
242
          /*-----
         if (state.update_theta)
243
244
         {
            i f
               (abs(IMU.theta - Otus.pitch) < 5.0)
245
              state.theta = IMU.theta * 0.75 + Otus.pitch * 0.25;
246
247
            else
248
              state.theta = IMU.theta * 0.99 + Otus.pitch * 0.01;
249
         }
250
         else
            state.theta = IMU.theta;
251
252
         state.theta_rad = Rad(state.theta);
253
254
         state.phi_sin = sin(state.phi_rad);
255
         state.theta_sin = sin(state.theta_rad);
256
         state.phi_cos = cos(state.phi_rad);
257
         state.theta_cos = cos(state.theta_rad);
258
         float pre_cos , pre_sin , ob_cos , ob_sin , inc , cof = 0.70; inc = (-state.phi_sin / state.theta_cos * state.q +
259
260
         state.phi_cos / state.theta_cos * state.r) * outerT;
261
262
         pre_cos = cos(Rad(state.psi + inc));
263
         pre_sin = sin(Rad(state.psi + inc));
264
         if (state.update_psi == 1)
265
         {
            ob_{-}cos = cos(Rad(Otus.yaw));
266
267
            ob_sin = sin(Rad(Otus.yaw));
268
         }
269
         else
270
         {
            ob_cos = pre_cos;
271
272
            ob_sin = pre_sin;
273
         }
274
         pre_cos = pre_cos * cof + ob_cos * (1 - cof);
         pre_sin = pre_sin * cof + ob_sin * (1 - cof);
275
```

```
276
277
        state.psi_rad = atan2(pre_sin , pre_cos);
        state.psi = Degree(state.psi_rad);
278
279
        state.psi_sin = sin(state.psi_rad);
        state.psi_cos = cos(state.psi_rad);
280
281
      }
282 }
    void _Copter::AHRS()
283
284
    {
      AHRS_filter();
                              //Digital Filter
285
      //Linear_Kalman_Filter();
286
287
      IMU.p = gy86.gyro.filter.x / 32.768;
      IMU.q = gy86.gyro.filter.y / 32.768;
288
      IMU.r = gy86.gyro.filter.z / 32.768;
289
      IMU. p_rad = Rad(IMU. p);
290
291
      IMU.q_rad = Rad(IMU.q);
      IMU.r_rad = Rad(IMU.r);
292
      inte_gyro [0] += IMU.p * 0.0025;
293
      inte_gyro[1] += IMU.q * 0.0025;
294
      inte_gyro \begin{bmatrix} 2 \end{bmatrix} += IMU.r * 0.0025;
295
      Madgwick_MARG_Update();
296
297
      AHRS_Check();
298
    }
299
    void _Copter :: AHRS_filter()
300
    {
      gy86_Dataanl();
301
302
      gy86.gyro.filter.x =
      IIR_filter_apply(L3GD20_DEFAULT_FILTER_FREQ,
303
304
      gy86.gyro.aftcal.x, &gyro_IIRx);
      gy86.gyro.filter.y =
305
      IIR_filter_apply (L3GD20_DEFAULT_FILTER_FREQ,
306
      -gy86.gyro.aftcal.y, &gyro_IIRy);
307
      gy86.gyro.filter.z =
308
      IIR_filter_apply(L3GD20_DEFAULT_FILTER_FREQ,
309
      -gy86.gyro.aftcal.z, &gyro_IIRz);
310
311
      gy86.acc.filter.x =
312
      IIR_filter_apply(LSM303D_ACCEL_DEFAULT_DRIVER_FILTER_FREQ,
313
314
      gy86.acc.aftcal.x, &acc_IIRx);
315
      gy86.acc.filter.y =
316
      IIR_filter_apply(LSM303D_ACCEL_DEFAULT_DRIVER_FILTER_FREQ,
317
      gy86.acc.aftcal.y, &acc_IIRy);
      gy86.acc.filter.z =
318
      IIR_filter_apply(LSM303D_ACCEL_DEFAULT_DRIVER_FILTER_FREQ,
319
320
      gy86.acc.aftcal.z, &acc_IIRz);
321
    }
    void _Copter::gy86_Dataanl()
322
323
    {
      MPU6050read();
324
    }
325
    void _Copter:: AHRS_filter_init()
326
327
    {
328
      IIR_set_cutoff_frequency (L3GD20_DEFAULT_RATE,
      L3GD20_DEFAULT_FILTER_FREQ, &gyro_IIRx);
329
      IIR_set_cutoff_frequency (L3GD20_DEFAULT_RATE,
330
331
      L3GD20_DEFAULT_FILTER_FREQ, &gyro_IIRy);
      IIR_set_cutoff_frequency (L3GD20_DEFAULT_RATE,
332
333
      L3GD20_DEFAULT_FILTER_FREQ, &gyro_IIRz);
334
335
      IIR_set_cutoff_frequency (LSM303D_ACCEL_DEFAULT_RATE,
      LSM303D_ACCEL_DEFAULT_DRIVER_FILTER_FREQ, &acc_IIRx);
336
      IIR_set_cutoff_frequency (LSM303D_ACCEL_DEFAULT_RATE,
337
      LSM303D_ACCEL_DEFAULT_DRIVER_FILTER_FREQ, &acc_IIRy);
338
339
      IIR_set_cutoff_frequency (LSM303D_ACCEL_DEFAULT_RATE,
      LSM303D_ACCEL_DEFAULT_DRIVER_FILTER_FREQ, &acc_IIRz);
340
```

```
155
```

```
341
    }
    void _Copter:: IIR_set_cutoff_frequency(float sample_freq,
342
    float cutoff_freq , struct _IIR *input_IIR)
343
344
    {
       if (cutoff_freq \ll 0.0f) {
345
         // no filtering
346
347
         return;
348
       }
       float fr = sample_freq / cutoff_freq;
349
       float ohm = tanf(M_PI_F / fr);
350
351
       float c = 1.0 f + 2.0 f *
       cosf(M_PI_F / 4.0 f) * ohm + ohm * ohm;
352
       input_IIR ->b0 = ohm * ohm / c;
input_IIR ->b1 = 2.0 f * input_IIR ->b0;
353
354
       input_{IIR} \rightarrow b2 = input_{IIR} \rightarrow b0;
355
       input_IIR \rightarrow a1 = 2.0 f * (ohm * ohm - 1.0 f) / c;
356
       input_{IIR} \rightarrow a2 = (1.0 f -
357
       2.0f * cosf(M_PI_F / 4.0f) *
358
       ohm + ohm * ohm) / c;
359
360
    ł
    float _Copter:: IIR_filter_apply(float cutoff_freq,
361
    float sample, struct _IIR *input_IIR)
362
363
    {
       if (cutoff_freq <= 0.0 f) {
364
         // no filtering
365
         return sample;
366
367
       }
       // do the filtering
input_IIR->element0 = sample -
368
369
       input_IIR -> element1 *
370
       input_IIR->a1 - input_IIR->element2 *
371
       input_IIR->a2;
372
       float output = input_IIR -> element0 *
373
374
       input_IIR->b0 +
       input_IIR->element1 * input_IIR->b1 +
375
       input_IIR->element2 * input_IIR->b2;
376
377
378
       input_IIR -> element2 = input_IIR -> element1;
       input_IIR -> element1 = input_IIR -> element0;
379
       return output;
380
381
    }
    void _Copter::State_Reset()
382
383
    {
384
       //q0 = Otus.q0;
       //q1 = Otus.q1;
385
       //q2 = Otus.q2;
386
       //q3 = Otus.q3;
387
388
389
       integralFBx = 0.0 f;
       integralFBy = 0.0 f;
390
       integralFBz = 0.0 f;
391
392
393
       state.vx = Otus.vx;
       state.vy = Otus.vy;
394
       state.vz = Otus.vz;
395
396
397
       state.x = Otus.x;
       state.y = Otus.y;
398
       state.z = Otus.z;
399
400
401
       state.psi = Otus.yaw;
    }
402
403
    void _Copter::KF_init()
404
    {
       PosX.Q = 2 / 10;
PosY.Q = 2 / 10;
405
406
       PosZ.Q = 2 / 10;
407
       PosX.R0 = 0.01;
408
```

```
409
       PosY.R0 = 0.01;
       PosZ.R0 = 0.01;
410
       PosX.R1 = 0.01;
411
412
       PosY.R1 = 0.01;
       PosZ.R1 = 0.01;
413
414 }
            -Complimentary Filter -----*/
415
    /*
    // Ref: "Nonlinear Complementary Filters on the Special Orthoganol Group"
416
417
     // By Robert Mahoney, published in 2007
     void _Copter::MahonyAHRSupdate(float gx, float gy,
418
     float gz, float ax, float ay, float az,
419
420
     float mx, float my, float mz) {
421
       float recipNorm;
             float \ q0q0 \ , \ q0q1 \ , \ q0q2 \ , \ q0q3 \ , \ q1q1 \ , \\
422
       q1q2, q1q3, q2q2, q2q3, q3q3;
float hx, hy, bx, bz;
float halfvx, halfvy, halfvz,
423
424
425
426
       halfwx, halfwy, halfwz;
       float halfex, halfey, halfez;
427
428
       float qa, qb, qc;
429
       if ((mx = 0.0 f) \&\& (my = 0.0 f)
430
       && (mz = 0.0 f)) {
431
         MahonyAHRSupdateIMU(\,gx\,,\ gy\,,\ gz\,,\ ax\,,\ ay\,,\ az\,)\,;
432
433
          return:
       }
434
435
       if (!((ax = 0.0f) \&\&
       (ay = 0.0 f) \&\& (az = 0.0 f))) \{
436
437
          // Normalise accelerometer measurement
438
         recipNorm = invSqrt(ax * ax +
439
440
         ay * ay + az * az);
         ax *= recipNorm;
441
442
         ay *= recipNorm;
         az *= recipNorm;
443
444
445
          // Normalise magnetometer measurement
446
          recipNorm = invSqrt(mx * mx +
         my * my + mz * mz);
447
448
         mx = recipNorm;
         my *= recipNorm;
449
450
         mz *= recipNorm;
451
452
          q0q0 = q0 * q0;
453
          q0q1 = q0 * q1;
454
          q0q2 = q0 * q2;
          q0q3 = q0 * q3;
455
          q1q1 = q1 * q1;
456
457
          q1q2 = q1 * q2;
          q1q3 = q1 * q3;
458
459
          q2q2 = q2 * q2;
          q2q3 = q2 * q3;
460
461
          q3q3 = q3 * q3;
462
         hx \;=\; 2\,.0\; f \;\; \ast \; \left(mx \;\ast \; \left(0\,.5\; f \;-\; q2q2 \;-\; q3q3\right) \;+\;
463
464
         my * (q1q2 - q0q3) + mz * (q1q3 + q0q2));
465
         hy = 2.0 f * (mx * (q1q2 + q0q3) +
         my \ \ast \ (0.5 \ f \ - \ q1q1 \ - \ q3q3) \ + \ mz \ \ast \ (q2q3 \ - \ q0q1));
466
467
         bx = sqrt(hx * hx + hy * hy);
         bz \; = \; 2.0 \; f \; * \; \left(mx \; * \; \left(q1q3 \; - \; q0q2 \right) \; + \;
468
469
         my * (q2q3 + q0q1) + mz * (0.5 f - q1q1 - q2q2));
470
          halfvx = q1q3 - q0q2;
471
472
          halfvy = q0q1 + q2q3;
          halfvz = q0q0 - 0.5f + q3q3;
473
          halfwx = bx * (0.5 f - q2q2 - q3q3) +
474
          bz * (q1q3 - q0q2);
475
476
          halfwy = bx * (q1q2 - q0q3) +
```

```
477
         bz * (q0q1 + q2q3);
478
         halfwz = bx * (q0q2 + q1q3) +
         bz * (0.5 f - q1q1 - q2q2);
479
480
481
         //direction and measured direction of field vectors
         halfex = (ay * halfvz - az * halfvy) +
482
483
         (my * halfwz - mz * halfwy);
         halfey = (az * halfvx - ax * halfvz) +
484
         (mz * halfwx - mx * halfwz);
485
         halfez = (ax * halfvy - ay * halfvx) +
486
         (mx * halfwy - my * halfwx);
487
488
         if (twoKi > 0.0f) {
489
           integralFBx += twoKi * halfex
490
            * (1.0f / sampleFreq);
491
           integralFBy += twoKi * halfey
492
           * (1.0 f / sampleFreq);
493
           integralFBz += twoKi * halfez
494
           * (1.0 f / sampleFreq);
495
           gx += integralFBx;
496
           gy += integralFBy;
497
           gz += integralFBz;
498
499
         }
500
         else {
501
           integralFBx = 0.0 f;
           integralFBy = 0.0 f;
502
           integralFBz = 0.0 f;
503
504
         }
505
         // Apply proportional feedback
506
         gx += twoKp * halfex;
gy += twoKp * halfey;
507
508
509
         gz += twoKp * halfez;
       }
510
511
       // Integrate rate of change of quaternion
512
       gx *= (0.5 f * (1.0 f / sampleFreq));
513
       gy *= (0.5 f * (1.0 f / sampleFreq));
514
       gz = (0.5 f * (1.0 f / sampleFreq));
515
       qa = q0;
516
517
       qb = q1;
518
       qc = q2;
       q0 += (-qb * gx - qc * gy - q3 * gz);
519
       q1 += (qa * gx + qc * gz - q3 * gy);
520
       q2 += (qa * gy - qb * gz + q3 * gx);
521
522
       q3 += (qa * gz + qb * gy - qc * gx);
523
524
       // Normalise quaternion
       recipNorm = invSqrt(q0 * q0 +
525
       q1 * q1 + q2 * q2 + q3 * q3);
526
       q0 = recipNorm;
527
528
       q1 *= recipNorm;
529
       q2 = recipNorm;
       q3 *= recipNorm;
530
531 }
    void _Copter::MahonyAHRSupdateIMU(float gx, float gy,
532
533
    float gz, float ax, float ay, float az) {
       float recipNorm;
534
       float halfvx, halfvy, halfvz;
float halfex, halfey, halfez;
535
536
537
       float \ qa\,,\ qb\,,\ qc\,;
538
       // Compute feedback only if accelerometer measurement valid (avoids NaN in accelerometer norm
539
       if (!((ax = 0.0f) \&\& (ay = 0.0f) \&\& (az = 0.0f))) 
540
541
542
         // Normalise accelerometer measurement
543
         \operatorname{recipNorm} = \operatorname{invSqrt}(\operatorname{ax} * \operatorname{ax} + \operatorname{ay} * \operatorname{ay} + \operatorname{az} * \operatorname{az});
```

544ax *= recipNorm; ay *= recipNorm; 545az *= recipNorm; 546 547548halfvx = q1 * q3 - q0 * q2;549halfvy = q0 * q1 + q2 * q3;550551halfvz = q0 * q0 - 0.5 f + q3 * q3;552halfex = (ay * halfvz - az * halfvy); halfey = (az * halfvx - ax * halfvz); halfez = (ax * halfvy - ay * halfvx); 553 554555556// Compute and apply integral feedback if enabled 557 $if (twoKi > 0.0 f) \{$ 558integralFBx += twoKi * halfex * (1.0 f / sampleFreq); 559integralFBy += twoKi * halfey * (1.0 f / sampleFreq); 560561integralFBz += twoKi * halfez * (1.0 f / sampleFreq); gx += integralFBx; // apply integral feedback 562563gy += integralFBy;564gz += integralFBz;565} 566else { 567integralFBx = 0.0 f; // prevent integral windupintegralFBy = 0.0 f;568integralFBz = 0.0 f; 569570} 571// Apply proportional feedback 572gx += twoKp * halfex;573gy += twoKp * halfey; 574gz += twoKp * halfez; 575576} 577578// Integrate rate of change of quaternion gx *= (0.5 f * (1.0 f / sampleFreq)); gy *= (0.5 f * (1.0 f / sampleFreq)); gz *= (0.5 f * (1.0 f / sampleFreq)); 579580581qa = q0;582583qb = q1;qc = q2;584q0 += (-qb * gx - qc * gy - q3 * gz);585q1 += (qa * gx + qc * gz - q3 * gy);586587q2 += (qa * gy - qb * gz + q3 * gx);588q3 += (qa * gz + qb * gy - qc * gx);589// Normalise quaternion 590recipNorm = invSqrt(q0 * q0 +591592q1 * q1 + q2 * q2 + q3 * q3);q0 = recipNorm;593q1 *= recipNorm; 594q2 *= recipNorm; 595596q3 *= recipNorm; } 597

Mark3 Flight Controller Code - Communication Process

```
1 #include "Copter.h"
\mathbf{2}
  void _Copter::command_Comm()
  {
3
^{4}
     //Counttimer1 = micros();
     if (RCsignal.THROTTLE > 250 && RCsignal.THROTTLE < 350
5
         && RCsignal.YAW < 350 && RCsignal.YAW > 250) {
6
       flag.ARMED = 1;
7
8
     if (flag.ARMED == 1 && RCsignal.THROTTLE < 350
9
```

```
10
         && RCsignal.YAW > 950)
                                   {
       flag .ARMED = 2;
11
12
       ControlReset();
     }
13
14
     //Stopping the motors: throttle low and yaw right.
     if (RCsignal.THROTTLE < 350 && RCsignal.YAW > 1650) {
15
       flag.ARMED = 0;
16
17
     if (RCsignal.MODE < 350 & RCsignal.MODE > 0)
18
19
       flag.mode = Attitude_mode;
20
     if (RCsignal.MODE < 1050 && RCsignal.MODE > 950)
       flag.mode = Altitude_mode;
21
     if (RCsignal.MODE < 2000 && RCsignal.MODE > 1650)
22
23
       flag.mode = loiter_mode;
     if (RCsignal.SWITCH < 350) flag.turnoff = 0;
24
     if (RCsignal.SWITCH > 1650) flag.turnoff = 1;
25
26
     Xbee_comm();
27
   }
   void _Copter::Xbee_comm()
^{28}
29
   {
30
^{31}
       if (comorder = 1062)
32
33
       Serial1.print(IMU.p, 3); //Serial.print("
       //Serial1.print(IMU.q, 3); Serial.print("
                                                          ");
34
        //Serial1.print(IMU.r, 3); Serial.print(")
35
       Serial1.println();
36
37
38
     Xbee_timer++;
39
     if (Xbee_timer == 8)
40
41
     {
42
       //Serial.print(state.x, 4); Serial.print('\t');
43
       //Serial.print(state.y, 4); Serial.print('t');
44
       //Serial.print(state.z, 4); Serial.print('\t');
45
46
47
       //Serial.print(Otus.x, 4); Serial.print('\t');
       //Serial.print(Otus.y, 4); Serial.print('\t');
48
       //Serial.print(Otus.z, 4); Serial.print('\t');
49
       //Serial.println();
50
51
       /*
          Serial.print(LKF.acc_roll); Serial.print('\t');
52
          Serial.print(LKF.acc_pitch); Serial.print('\t');
53
54
          Serial.print(Otus.yaw); Serial.print('\t');
55
          Serial.print(state.p); Serial.print('\t');
56
57
          Serial.print(state.q); Serial.print('\t');
          Serial.print(state.r); Serial.print('\t');
58
          {\tt Serial.println();}
59
60
       */
61
        //Serial.println();
62
        /*
          if (xbee_length != 0)
63
64
          Serial.print(Otus.x); Serial.print('\t');
65
          Serial.print(loopClock2); Serial.print('\t');
66
          Serial.print(xbee_length); Serial.print('\t');
67
68
          for (uint8_t i = 0; i < xbee_length; i++)
69
70
            Serial.print(xbee_data[100 + i]); Serial.print(" ");
71
          Serial.println();
72
73
74
       */
```

```
75
         switch (comorder)
76
         {
77
           case 1000:
             Serial1.print(RCsignal.ROLL);
78
79
             Serial1.print(' \ t');
             Serial1.print(RCsignal.PITCH);
80
             Serial1.print(' \ t');
81
             Serial1.print(RCsignal.THROTTLE);
82
             Serial1. print ( ' t ');
83
             Serial1.print(RCsignal.YAW);
84
             Serial1.print(' \ t');
85
             Serial1.print(RCsignal.MODE);
86
             Serial1.print(' \ t');
87
             Serial1.print(RCsignal.SWITCH);
88
             Serial1.print(' \ t');
89
             Serial1.print(RCsignal.CH7);
90
             Serial1.print(' \ t');
91
92
             Serial1.print(RCsignal.CH8);
93
             Serial1. print ( ' t ');
             Serial1.print(RCsignal.CH9);
94
             Serial1.print(' \ t');
95
             Serial1.print(RCsignal.CH10);
96
             Serial1.print('\t');
Serial1.print("Arm: ");
97
98
             Serial1.print(flag.ARMED);
99
100
             Serial1.print(' \ t');
             Serial1.print("Turn Off: ");
101
             Serial1.print(flag.turnoff); Serial1.print('\t');
102
103
             if (flag.mode == 1)
104
             {
105
               Serial1.print("Attitude mode");
               Serial1. print ( ' \ t ' );
106
107
             }
             else if (flag.mode == 2)
108
             {
109
               Serial1.print("Altitude mode");
110
               Serial1.print(' \setminus t');
111
112
             }
113
             else if (flag.mode == 3)
             {
114
               Serial1.print("loiter mode");
115
116
               Serial1.print(' \setminus t');
117
118
             Serial1.println();
             break;
119
           case 1010:
120
121
             State_Reset();
122
             break;
123
                                   -Gyro Test-
           /*
                                                                     ·*/
           case 1020: //Calculate Current Offset
124
125
             flag.calibratedG = 0;
             comorder = 0;
126
             inte_gyro[0] = 0;
127
128
             inte_gyro[1] = 0;
             inte_gyro [2] = 0;
129
130
             break;
           case 1021:
131
             Serial1.print(gy86.acc.origin.x); Serial1.print('\t');
132
             Serial1.print(gy86.acc.origin.y); Serial1.print(' t');
133
             Serial1.print(gy86.acc.origin.z); Serial1.print('\t');
134
             Serial1.print(mpu_temperature); Serial1.print('\t');
135
             Serial1.print(temperature); Serial1.print('\t');
136
             Serial1.print(gy86.gyro.origin.x); Serial1.print('\t');
137
             Serial1.print(gy86.gyro.origin.y); Serial1.print('\t');
138
             Serial1.print(gy86.gyro.origin.z); Serial1.print('\t');
139
```

140 Serial1.println(); break: 141**case** 1022: 142 143 Serial1.print(gy86.gyro.origin.x); Serial1.print('\t'); Serial1.print(gy86.gyro.aftcal.x); Serial1.print('\t'); 144 Serial1.println(); 145146 break: 147**case** 1023: Serial1.print(gy86.gyro.origin.x); Serial1.print('\t'); 148 Serial1.print(gy86.gyro.origin.y); Serial1.print('\t'); 149 $Serial1.print(gy86.gyro.origin.z); Serial1.print('\t');$ 150 151Serial1.println(); break: 152**case** 1024: 153154Serial1.print(gyro_temp); Serial1.print('\t'); Serial1.print(gy86.gyro.aftcal.x); Serial1.print('\t'); 155Serial1.print(gy86.gyro.aftcal.y); Serial1.print('\t'); 156157Serial1.print(gy86.gyro.aftcal.z); Serial1.print('\t'); 158 Serial1.println(); 159break: **case** 1025: 160 Serial1.print(gy86.gyro.aftcal.x); Serial1.print('\t'); 161 Serial1.print(gy86.gyro.filter.x); Serial1.print('\t'); 162163 Serial1.println(); break; 164**case** 1026: 165Serial1.print(gy86.gyro.origin.z); Serial1.print('\t'); 166 167 $Serial1.print(gy86.gyro.aftcal.z); Serial1.print(' \ t');$ Serial1.println(); 168 169 break: 170 **case** 1027: Serial1.print(gy86.gyro.filter.x); Serial1.print('\t'); 171Serial1.print(gy86.gyro.filter.y); Serial1.print('\t'); 172 $Serial1.print(gy86.gyro.filter.z); Serial1.print('\t');$ 173 174Serial1.println(); break: 175**case** 1028: 176 Serial1.print(inte_gyro[0]); Serial1.print('\t'); 177 Serial1.print(inte_gyro[1]); Serial1.print('\t'); 178Serial1.print(inte_gyro[2]); Serial1.print('t'); 179180 Serial1.println(); break: 181 -Accelerometer Test-------*/ 182 case 1031: 183 $Serial1.print(gy86.acc.origin.x); Serial1.print('\t');$ 184 Serial1.print(gy86.acc.origin.y); Serial1.print('\t'); 185186 Serial1.print(gy86.acc.origin.z); Serial1.print('\t'); Serial1.println(); 187 188 break **case** 1032: 189 Serial1.print(gy86.acc.aftcal.x); Serial1.print('\t'); 190 191 Serial1.print(gy86.acc.aftcal.y); Serial1.print('\t'); Serial1.print(gy86.acc.aftcal.z); Serial1.print('\t'); 192Serial1.println(); 193 194 break: **case** 1033: 195 $Serial1.print(gy86.acc.aftcal.x); Serial1.print('\t');$ 196 Serial1.print(gy86.acc.aftcal.y); Serial1.print('\t'); 197 198 Serial1.print(gy86.acc.aftcal.z); Serial1.print('\t'); Serial1.print(gy86.acc.filter.x); Serial1.print('\t'); 199 Serial1.print(gy86.acc.filter.y); Serial1.print(\t'); 200 Serial1.print(gy86.acc.filter.z); Serial1.print(' t'); 201 202 Serial1.println(); 203 break: **case** 1034: 204 Serial1.print(gy86.acc.origin.x); Serial1.print('\t'); 205

206 Serial1.print(gy86.acc.origin.y); Serial1.print('\t'); $Serial1.print(gy86.acc.origin.z); Serial1.print('\t');$ 207 Serial1.print(gy86.acc.aftcal.x); Serial1.print('\t'); Serial1.print(gy86.acc.aftcal.y); Serial1.print('\t'); 208 209Serial1.print(gy86.acc.aftcal.z); Serial1.print('\t'); 210 Serial1.println(); 211break: 212213/ *--Accelerometer Calibration -------*/ **case** 1041: //level - z + g214MPU6050AccCali(4); 215216 break: 217**case** 1042: //back - z - gMPU6050AccCali(5); 218 219break; $//\operatorname{nose}$ up – x + g 220 case 1043: MPU6050AccCali(0);221222 break: 223**case** 1044: //nose down - x - gMPU6050AccCali(1); 224225break; //left wing up - y +g **case** 1045: 226 227 MPU6050AccCali(2);228 break: 229**case** 1046: //left wing down - y -g MPU6050AccCali(3); 230231 break; 232**case** 1047: //reset 233 AccPointRead(); 234break; **case** 1048: 235236for $(uint8_t point = 0; point < 6; point++)$ 237 { 238Serial1.print(Acc_Cali.accel_raw_ref[point][0]); Serial1. print $(' \ t ');$ 239240Serial1.print(Acc_Cali.accel_raw_ref[point][1]); 241Serial1.print($' \setminus t'$); Serial1.print(Acc_Cali.accel_raw_ref[point][2]); 242Serial1.print($' \ t'$); 243244Serial1.println(); } 245comorder = 0;246 247break; case 1049: 248—"); Serial1.println("----249 for $(uint8_t i = 0; i < 3; i++)$ 250251{ for $(uint8_t j = 0; j < 3; j++)$ 252253{ $Serial1.print(Acc_Cali.a[i][j]);$ 254Serial1.print($' \setminus t'$); 255256} Serial1.println(); 257 258-"); Serial1.println("-----259for $(uint8_t i = 0; i < 3; i++)$ 260 { 261for $(uint8_t j = 0; j < 3; j++)$ 262263ł $Serial1.print(Acc_Cali.T[i][j]);$ 264Serial1.print($' \setminus t'$); 265266 } 267Serial1.println(); 268—"); Serial1.println("----269 comorder = 0;270break; 271

```
272
           /*Attitude Estimation*/
           case 1051:
273
             Serial1.print(state.phi); Serial1.print('\t');
274
             Serial1.print(state.theta); Serial1.print('\t');
275
276
             Serial1.print(state.psi); Serial1.print('\t');
277
             Serial1.println();
278
             break;
279
           case 1052:
             Serial1.print(state.p); Serial1.print('\t');
280
281
             Serial1.print(state.q); Serial1.print(' \ t');
             Serial1.print(state.r); Serial1.print('\t');
282
             Serial1.println();
283
284
             break:
           case 1053:
285
             Serial1.print(q0); Serial1.print('\t');
286
             Serial1.print(q1); Serial1.print('\t');
287
             Serial1. print (q2); Serial1. print ('\t');
288
             Serial1.print(q3); Serial1.print('\t');
289
290
             Serial1.println();
             break:
291
           case 1054:
292
293
             Serial1.print(state.ax); Serial1.print('\t');
             Serial1.print(state.ay); Serial1.print('\t');
294
             Serial1.print(state.az); Serial1.print('\t');
295
             Serial1.println();
296
297
             break:
298
                      -Linear Kalman Filter — —
                                                       —*/
           /*----
           case 1061:
299
             Serial1.print(LKF.acc_roll); Serial1.print('\t');
300
             Serial1.print(LKF.acc_pitch); Serial1.print('\t');
301
302
             Serial1.println();
303
             break;
           case 1062:
304
             Serial1.print(state.x, 4); Serial1.print('\t');
Serial1.print(Otus.x, 4); Serial1.print('\t');
305
306
307
             Serial1.println();
             break:
308
           case 1063:
309
             Serial1.print(state.y, 4); Serial1.print('\t');
310
311
             Serial1.print(Otus.y, 4); Serial1.print('\t');
             {\tt Serial1.println();}
312
313
             break:
           case 1064:
314
             Serial1.print(state.z, 4); Serial1.print('\t');
315
             Serial1.print(Otus.z, 4); Serial1.print('\t');
316
317
             Serial1.println();
318
             break:
           case 1065:
319
             Serial1.print(state.vx, 4); Serial1.print('\t');
320
             Serial1.print(Otus.vx, 4); Serial1.print('\t');
321
322
             Serial1.println();
             break;
323
           case 1066:
324
             Serial1.print(state.vy, 4); Serial1.print('\t');
325
             Serial1.print(Otus.vy, 4); Serial1.print('\t');
326
327
             Serial1.println();
             break;
328
           case 1067:
329
             Serial1.print(state.vz, 4); Serial1.print(' \ t');
330
             Serial1.print(Otus.vz, 4); Serial1.print('\t');
331
332
             Serial1.println();
333
             break;
           case 1101:
334
             Serial1.print(U1); Serial1.print('\t');
335
             Serial1.print(U2); Serial1.print('\t');
336
             Serial1.print(U3); Serial1.print('\t');
337
             Serial1.print(U4); Serial1.print('\t');
338
```

339 -"); break: 340 case 1102: 341 342 Serial1.print(PWM1); Serial1.print('\t'); $Serial1.print(PWM2); Serial1.print('\t');$ 343 $Serial1.print(PWM3); Serial1.print('\t');$ 344 Serial1.print(PWM4); Serial1.print('\t'); 345Serial1.println(); 346 347 break; -P Control-348 ----*/ **case** 1201: 349 350 Serial1.print(Target.p); Serial1.print('\t'); 351Serial1.print(state.p); Serial1.print('\t'); 352Serial1.println(); 353 break: **case** 1202: 354 $Serial1.print(Target.p_rad, 5); Serial1.print(' \ t');$ 355 Serial1.print(state.p_rad, 5); Serial1.print('\t'); 356 357 Serial1.println(); break; 358 **case** 1203: 359 $Serial1.print("P_Kp =$ "); Serial1.println(pvel.Kp, 4); 360 Serial1.print("P_Ki = "); Serial1.println(pvel.Ki, 4); 361 Serial1.print("P_Kd = "); Serial1.println(pvel.Kd, 4); 362 363 comorder = 0;break: 364365 **case** 1204: Serial1.print(U2, 5); Serial1.print('\t'); 366 367 Serial1.print(state.p_rad, 5); Serial1.println(); 368 369 break; -Roll Control--*/ 370 **case** 1211: 371 Serial1.print(Target.phi); Serial1.print('\t'); 372 373Serial1.print(state.phi); Serial1.print('\t'); Serial1.println(); 374375 break: **case** 1212: 376 $Serial1.print(Target.phi_rad, 5); Serial1.print(' \ t');$ 377 378 Serial1.print(state.phi_rad, 5); Serial1.print('\t'); 379 Serial1.println(); 380 break: 381 case 1213: Serial1.print("Phi_Kp = "); Serial1.println(phiang.Kp, 4); 382 383 comorder = 0;384break; 385 386 -----*/ **case** 1221: 387 $Serial1.print(Target.q); Serial1.print(' \ t');$ 388 Serial1.print(state.q); Serial1.print('\t'); 389 390 Serial1.println(); 391 break: **case** 1222: 392 393 Serial1.print(Target.q_rad, 5); Serial1.print('\t'); Serial1.print(state.q_rad, 5); Serial1.print('\t'); 394 395 Serial1.println(); 396 break: **case** 1223: 397 Serial1.print("Q_Kp = "); Serial1.println(qvel.Kp, 4); Serial1.print("Q_Ki = "); Serial1.println(qvel.Ki, 4); 398 399 Serial1.print("Q_Kd = "); Serial1.println(qvel.Kd, 4); 400 comorder = 0;401 402break; **case** 1224: 403 Serial1.print(U3, 5); Serial1.print('\t'); 404Serial1.print(state.q_rad, 5); 405

406 Serial1.println(); break; 407 ---Pitch Control-----*/ 408 409 **case** 1231: Serial1.print(Target.theta); Serial1.print('\t'); 410 Serial1.print(state.theta); Serial1.print('\t'); 411 Serial1.println(); 412break; 413**case** 1232: 414 415416 417Serial1.println(); break: 418 **case** 1233: 419 Serial1.print("Theta_Kp = "); Serial1.println(thetaang.Kp, 4); 420 comorder = 0;421 422 break; 423 -----r Control-----*/ case 1241: 424 Serial1.print(Target.r); Serial1.print('\t'); 425Serial1.print(state.r); Serial1.print('\t'); 426Serial1.println(); 427 428 break: **case** 1242: 429Serial1.print(Target.r_rad, 5); Serial1.print('\t'); 430Serial1.print(state.r_rad, 5); Serial1.print('\t'); 431 432 Serial1.println(); break; 433 **case** 1243: 434 Serial1.print("R_Kp = "); Serial1.println(rvel.Kp, 6); Serial1.print("R_Ki = "); Serial1.println(rvel.Ki, 6); Serial1.print("R_Kd = "); Serial1.println(rvel.Kd, 6); 435436 437 comorder = 0;438 break: 439440 case 1244: Serial1.print(U4, 5); Serial1.print('\t'); 441 442Serial1.print(state.r_rad, 5); Serial1.println(); 443 444 break; -Yaw Control--*/ 445case 1251: 446 Serial1.print(Target.psi); Serial1.print('\t'); Serial1.print(state.psi); Serial1.print('\t'); 447 448//Serial1.print(Psicon.Output[0]); Serial1.print('\t'); 449450Serial1.println(); 451break; case 1252: 452453Serial1.print(Target.psi_rad, 5); Serial1.print('\t'); Serial1.print(state.psi_rad, 5); Serial1.print('\t'); 454Serial1.println(); 455break: 456 457**case** 1253: Serial1.print("Psi_Kp = "); 458459Serial1.println(psiang.Kp, 4); 460 comorder = 0;break: 461 **case** 1254: 462 Serial1.println(Otus.yaw); 463 break; 464465---Vz Control------*/ **case** 1261: 466 467Serial1.print(Target.vz); Serial1.print('\t'); Serial1.print(state.vz); Serial1.print('\t'); 468 Serial1.println(); 469break: 470 **case** 1262: 471Serial1.print("Z_Kp = "); Serial1.println(Zalt.Kp); 472

```
Serial1.print("Vz_Kp = "); Serial1.println(Vzalt.Kp);
473
                                      "); Serial1.println(Vzalt.Ki);
             Serial1.print("Vz_Ki =
474
             Serial1.print("Vz_Kd = "); Serial1.println(Vzalt.Kd);
475
             comorder = 0;
476
477
            break:
478
           case 1263:
             Serial1.print(Vzcon.Output[0], 5); Serial1.print('\t');
479
480
             Serial1.print(state.vz, 5);
481
             Serial1.println();
482
             break:
          case 1264:
483
             Serial1.print(RCsignal.THROTTLE); Serial1.print('\t');
484
             Serial1.print(state.vz); Serial1.print('\t');
485
             Serial1.print(Target.vz); Serial1.print('\t');
486
             Serial1.print(state.z); Serial1.print('\t');
487
             Serial1.print(Target.z); Serial1.print('\t');
488
             Serial1.print(Vzcon.Output[0]); Serial1.print('\t');
489
             Serial1.print(U1);
490
491
             Serial1.println();
            break:
492
          case 1265:
493
             Serial1.print(state.flight_state[0]); Serial1.print('\t');
494
             Serial1.print(state.flight_state[1]); Serial1.print('\t');
495
             Serial1.print(state.flight_state[2]); Serial1.print('\t');
496
             Serial1.print(state.flight_state[3]); Serial1.print('\t');
497
             Serial1.print(state.takeoff_t); Serial1.print('\t');
498
499
             Serial1.print(state.landing_t); Serial1.print('\t');
500
             Serial1.print(U1); Serial1.print('\t');
             Serial1.println();
501
            break;
502
                               -VxVv Control-
503
                                                                */
          case 1271:
504
505
             Serial1.print("X_Kp =
                                     "); Serial1.println(Xpos.Kp);
             Serial1.print("Y_Kp =
                                     "); Serial1.println(Ypos.Kp);
506
            Serial1.print("Vx_Kp =
Serial1.print("Vx_Kd =
                                      "); Serial1.println(Vxpos.Kp);
507
                                      "); Serial1.println(Vxpos.Kd);
508
             Serial1.print("Vy_Kp = "); Serial1.println(Vypos.Kp);
509
             Serial1.print("Vy_Kd = "); Serial1.println(Vypos.Kd);
510
            comorder = 0;
511
512
            break:
          case 1272:
513
514
             Serial1.print(state.vx); Serial1.print('\t');
             Serial1.print(Target.vx); Serial1.print('\t');
515
516
             Serial1.println();
            break;
517
          case 1273:
518
             Serial1.print(state.vy); Serial1.print('\t');
519
             Serial1.print(Target.vy); Serial1.print('\t');
520
             Serial1.println();
521
             break;
522
          case 1274:
523
             Serial1.print(state.vz); Serial1.print('\t');
524
525
             Serial1.print(Target.vz); Serial1.print('\t');
             Serial1.println();
526
            break;
527
                         -Input/Output-
528
                                                     -*/
          case 1280:
529
             Serial1.print(state.x); Serial1.print('\t');
530
             Serial1.print(Target.x); Serial1.print('\t');
531
             Serial1.println();
532
            break:
533
          case 1281:
534
             Serial1.print(state.y); Serial1.print('\t');
535
536
             Serial1.print(Target.y); Serial1.print('\t');
             Serial1.println();
537
538
             break:
```
```
539
           case 1282:
540
             Serial1.print(state.z); Serial1.print('\t');
             Serial1.print(Target.z); Serial1.print('\t');
541
             Serial1.println();
542
543
             break:
           case 1283:
544
             Serial1.print(Target.phi); Serial1.print('\t');
545
             Serial1.print(Target.theta); Serial1.print('\t');
546
547
             Serial1.println();
             break:
548
549
                            -Plan-
                                                 */
550
           case 1290:
551
             Serial1.print(Target.plan_x); Serial1.print('\t');
552
             Serial1.print(Target.plan_y); Serial1.print('\t');
553
             Serial1.print(Target.plan_z); Serial1.print('\t');
554
             Serial1.print(Target.plan_psi); Serial1.print('\t');
555
556
             Serial1.print(Target.x); Serial1.print('\t');
557
             Serial1.print(Target.y); Serial1.print('\t');
558
             Serial1.print(Target.z); Serial1.print('\t');
559
             Serial1.print(Target.psi); Serial1.print('\t');
560
561
             Serial1.println();
             break:
562
           case 1301:
563
             Serial1.println();
564
             Serial1.println("////////PID PRAM/////////");
565
             Serial1.println();
566
567
             Serial1.print("P_Kp =
                                       "); Serial1.println(pvel.Kp);
             Serial1.print ("P_Ki =
                                       "); Serial1.println(pvel.Ki);
568
             Serial1.print("P_Kd =
                                       "); Serial1.println(pvel.Kd);
569
             Serial1.print("Q_Kp =
                                       "); Serial1.println(qvel.Kp);
570
             Serial1.print ("Q_Ki =
                                       "); Serial1.println(qvel.Ki);
571
             Serial1.print("Q_Kd =
                                       "); Serial1.println(qvel.Kd);
572
573
             delay (10);
             Serial1.print("R_Kp =
Serial1.print("R_Ki =
                                       "); Serial1.println(rvel.Kp);
574
                                      "); Serial1.println(rvel.Ki);
575
             Serial1.print("R_Kd = "); Serial1.println(rvel.Kd);
576
             Serial1.print("Phi_Kp = "); Serial1.println(phiang.Kp);
Serial1.print("Theta_Kp = "); Serial1.println(thetaang.Kp);
577
578
             Serial1.print("Psi_Kp = "); Serial1.println(psiang.Kp);
579
             delay(10);
580
             Serial1.println();
581
             Serial1. print ("Z_Kp =
                                      "); Serial1.println(Zalt.Kp);
582
             Serial1.print("Vz_Kp = "); Serial1.println(Vzalt.Kp);
583
             Serial1.print("Vz_Ki = "); Serial1.println(Vzalt.Ki);
Serial1.print("Vz_Kd = "); Serial1.println(Vzalt.Kd);
584
585
586
             Serial1.println();
             Serial1.print("Xpos_Kp = "); Serial1.println(Xpos.Kp);
587
             Serial1.print("Vxpos_Kp = "); Serial1.println(Vxpos.Kp);
588
             Serial1.print ("Vxpos_Ki =
Serial1.print ("Vxpos_Kd =
                                           "); Serial1.println(Vxpos.Ki);
589
                                           "); Serial1.println(Vxpos.Kd);
590
591
             delay (10);
             Serial1.print("Ypos_Kp = "); Serial1.println(Ypos.Kp);
592
             Serial1.print("Vypos_Kp = "); Serial1.println(Vypos.Kp);
593
             Serial1.print("Vypos_Ki = "); Serial1.println(Vypos.Ki);
Serial1.print("Vypos_Kd = "); Serial1.println(Vypos.Kd);
594
595
596
             Serial1.println();
             Serial1.print("Gravity = "); Serial1.println(EstimatedG);
597
598
             Serial1.println();
599
             comorder = 0;
600
601
             break;
           case 1411:
602
             Serial1.print(Otus.x); Serial1.print('\t');
603
```

604 Serial1.print(Otus.y); Serial1.print('\t'); 605 Serial1.print(Otus.z); Serial1.print('\t'); Serial1.println(); 606 break; 607 **case** 1412: 608 $Serial1.print(Otus.vx); Serial1.print(' \ t');$ 609 Serial1.print(Otus.vy); Serial1.print('\t'); 610 Serial1.print(Otus.vz); Serial1.print('\t'); 611 612 Serial1.println(); break: 613 **case** 1413: 614 615 Serial1.print(Otus.roll); Serial1.print('\t'); Serial1.print(Otus.pitch); Serial1.print('\t'); 616 617 Serial1.print(Otus.yaw); Serial1.print('\t'); Serial1.println(); 618 break; 619 **case** 1414: 620 Serial1.print(q0); Serial1.print('\t'); 621 Serial1.print(q1); Serial1.print('\t'); 622 Serial1.print(q2); Serial1.print('\t'); 623 Serial1.print(q3); Serial1.print('\t'); 624 Serial1.print(Otus.q0); Serial1.print($' \ t'$); 625 Serial1.print(Otus.q1); Serial1.print('\t'); Serial1.print(Otus.q2); Serial1.print('\t'); 626 627 Serial1.print(Otus.q3); Serial1.print('t'); 628 629 Serial1.println(); 630 break; **case** 1415: 631 632 Serial.print(LKF.acc_roll); Serial.print('t'); 633 $Serial.print(LKF.acc_pitch); Serial.print('\t');$ 634 $Serial.print(Otus.yaw); Serial.print(' \ t');$ 635 636 Serial.print(state.p); Serial.print('\t'); 637 Serial.print(state.q); Serial.print('\t'); 638 Serial.print(state.r); Serial.print('\t'); 639 640 Serial.println(); 641 break: 642 **case** 1501: 643 for $(uint8_t i = 0; i < 30; i++)$ 644 645{ Serial1.print(VRsensor1.ringbuffer[i]); 646 Serial1.println($' \ t'$); 647 648 } 649comorder = 0;650 break: case 1998: 651 Serial1.print(xbee_length); Serial1.println('\t'); 652 653 break: **case** 1999: 654Xbee_Packet(); 655656 break: 657 case 2001: Serial1.print(voltageavg); Serial1.println('\t'); 658 659 break; 660 661 Xbee_timer = 0;662 663 } 664} 665 void _Copter::Xbee_Packet() 666 { 667 -Test */ $uint8_t data_length = 21;$ 668uint8_t packet[data_length]; 669 packet[0] = 45;670

```
671
       packet[1] = 50;
       packet[2] = 55;
672
673
       packet[3] = 71;
674
       xbee_tmp.f = state.phi;
675
       packet[4] = xbee_tmp.ul[0];
676
       packet[5] = xbee_tmp.ul[1];
677
       packet [6] = xbee_tmp.ul[2];
678
       packet[7] = xbee_tmp.ul[3];
679
680
681
       packet[8] = 72;
       xbee_tmp.f = state.theta;
682
683
       packet[9] = xbee_tmp.ul[0];
684
       packet[10] = xbee_tmp.ul[1];
       packet[11] = xbee_tmp.ul[2];
685
       packet[12] = xbee_tmp.ul[3];
686
687
       packet[13] = 73;
xbee_tmp.f = state.theta;
688
689
       packet[14] = xbee_tmp.ul[0];
690
691
       packet[15] = xbee_tmp.ul[1];
       packet [16] = xbee_tmp.ul [2];
692
       packet[17] = xbee_tmp.ul[3];
693
694
       packet[18] = 100;
695
       packet[19] = 125;
696
       packet[20] = 150;
697
       Serial1.write(packet, data_length);
698
699 }
    void _Copter::Xbee_receive(int16_t order, uint16_t stmp)
700
701 {
       float pram = (float)stmp;
702
703
       switch (order)
704
       ł
         case 1011:
705
           pvel.Kp = pram / 10000;
EEPROM.write(10, stmp & 0b11111111);
706
707
           EEPROM.write(11, stmp >> 8);
Serial1.print("P_Kp = "); Serial1.print(pvel.Kp);
708
709
710
            Serial1.println();
711
           break;
         case 1012:
712
713
           pvel.Ki = pram / 1000;
           EEPROM. write(12, stmp \& 0b11111111);
714
           EEPROM. write(13, stmp >> 8);
Serial1.print("P_Ki = "); Serial1.print(pvel.Ki);
715
716
717
            Serial1.println();
           break;
718
         case 1013:
719
           pvel.Kd = pram / 100000;
720
           EEPROM. write (14, stmp & 0b11111111);
721
           EEPROM. write(15, stmp >> 8);
Serial1.print("P_Kd = "); Serial1.print(pvel.Kd);
722
723
            Serial1.println();
724
           break;
725
726
         case 1021:
           qvel.Kp = pram / 10000;
727
           EEPROM. write(18, stmp & 0b11111111);
728
           EEPROM. write(19, stmp >> 8);
Serial1.print("Q_Kp = "); Serial1.print(qvel.Kp);
729
730
            Serial1.println();
731
           break:
732
         case 1022:
733
734
            qvel.Ki = pram / 1000;
735
           EEPROM. write (20, stmp & 0b11111111);
736
```

```
737
           EEPROM. write (21, \text{ stmp} \gg 8);
            Serial1.print ("Q_Ki = "); Serial1.print (qvel.Ki);
738
            Serial1.println();
739
            break;
740
         case 1023:
741
742
            qvel.Kd = pram / 100000;
743
744
           EEPROM. write (22, stmp & 0b11111111);
           EEPROM. write (23, \text{ stmp } >> 8);
745
            Serial1.print("Q_Kd = "); Serial1.print(qvel.Kd);
746
747
            Serial1.println();
748
            break;
         case 1031:
749
750
            rvel.Kp = pram / 100000;
751
           EEPROM. write (26, stmp & 0b11111111);
752
           EEPROM. write (27, \text{ stmp} \gg 8);
753
            Serial1.print("R_Kp = "); Serial1.print(rvel.Kp);
754
755
            Serial1.println();
            break;
756
757
         case 1032:
758
            rvel.Ki = pram / 10000;
759
           EEPROM. write(28, stmp & 0b11111111);
760
           EEPROM. write (29, \text{ stmp } >> 8);
761
            Serial1.print ("R_Ki = "); Serial1.print (rvel.Ki);
762
            Serial1.println();
763
764
            break;
765
         case 1033:
766
767
            rvel.Kd = pram / 1000000;
           EEPROM. write (30, stmp & 0b11111111);
768
           EEPROM. write(31, stmp >> 8);
Serial1.print("R_Kd = "); Serial1.print(rvel.Kd);
769
770
771
            Serial1.println();
            break;
772
773
         case 1051:
774
            phiang.Kp = pram / 100;
775
776
           EEPROM. write (16, stmp & 0b11111111);
           EEPROM. write(17, stmp >> 8);
Serial1.print("Phi_Kp = "); Serial1.print(phiang.Kp);
777
778
779
            Serial1.println();
780
            break;
         case 1052:
781
782
783
            thetaang.Kp = pram / 100;
           EEPROM. write (24, stmp & 0b11111111);
784
           EEPROM. write(25, stmp >> 8);
Serial1.print("Theta_Kp = "); Serial1.print(thetaang.Kp);
785
786
            Serial1.println();
787
            break;
788
         case 1053:
789
790
            psiang.Kp = pram / 100;
791
           EEPROM. write (32, stmp & 0b11111111);
792
           EEPROM. write (33, \text{ stmp} \gg 8);
793
            Serial1.print("Psi_Kp = "); Serial1.print(psiang.Kp);
794
            Serial1.println();
795
            break;
796
         case 1071:
797
798
            {\rm Zalt.Kp} = {\rm pram} \ / \ 100;
799
           EEPROM. write (40, stmp & 0b11111111);
800
801
           EEPROM. write (41, \text{ stmp} \gg 8);
            Serial1.print("Z_Kp = "); Serial1.print(Zalt.Kp);
802
            Serial1.println();
803
```

```
804
             break;
          case 1081:
805
806
807
             Vzalt.Kp = pram / 100;
             EEPROM. write (42, stmp & 0b11111111);
808
             EEPROM. write(43, stmp >> 8);
Serial1.print("Vz_Kp = "); Serial1.print(Vzalt.Kp);
809
810
             Serial1.println();
811
812
             break;
          case 1082:
813
814
             Vzalt.Ki = pram / 100;
815
            EEPROM. write (44, stmp % 0b11111111);
EEPROM. write (45, stmp >> 8);
Serial1.print("Vz_Ki = "); Serial1.print(Vzalt.Ki);
816
817
818
             Serial1.println();
819
             break:
820
          case 1083:
821
822
             Vzalt.Kd = pram / 100;
823
            EEPROM. write (46, stmp & 0b11111111);
EEPROM. write (47, stmp >> 8);
Serial1.print("Vz_Kd = "); Serial1.print(Vzalt.Kd);
824
825
826
             Serial1.println();
827
             break;
828
          case 1091:
829
830
             Xpos.Kp = pram / 1000;
EEPROM.write(50, stmp & 0b1111111);
831
832
             EEPROM. write (51, \text{ stmp } \gg 8);
833
             Serial1.print("Xpos_Kp = "); Serial1.print(Xpos.Kp);
834
835
             Serial1.println();
             break;
836
          case 1092:
837
838
             Vxpos.Kp = pram / 1000;
839
             EEPROM. write (52, stmp & 0b11111111);
840
             EEPROM. write (53, \text{ stmp} \gg 8);
841
             Serial1.print("Vxpos_Kp = '"); Serial1.print(Vxpos.Kp);
842
             Serial1.println();
843
844
             break;
845
          case 1093:
846
             \mathrm{Vxpos.\,Ki}\ =\ \mathrm{pram}\ /\ 1000;
847
             EEPROM. write (54, stmp & 0b11111111);
848
             EEPROM. write (55, \text{ stmp} \gg 8);
849
             Serial1.print("Vxpos_Ki = '"); Serial1.print(Vxpos.Ki);
850
             Serial1.println();
851
             break:
852
          case 1094:
853
854
             Vxpos.Kd = pram / 1000;
855
             EEPROM. write (56, stmp & 0b11111111);
856
            EEPROM. write(57, stmp >> 8);
Serial1.print("Vxpos_Kd = "); Serial1.print(Vxpos.Kd);
857
858
             Serial1.println();
859
             break;
860
861
          case 1095:
862
             Ypos.Kp = pram / 1000;
863
            EEPROM. write (60, stmp & 0b11111111);
EEPROM. write (61, stmp >> 8);
Serial1.print ("Ypos_Kp = "); Serial1.print (Ypos.Kp);
864
865
866
             Serial1.println();
867
868
             break;
          case 1096:
869
```

870

```
871
             Vypos.Kp = pram / 1000;
             EEPROM. write(62, stmp & 0b11111111);
872
             EEPROM. write (63, stmp >> 8);
Serial1.print ("Vypos_Kp = "); Serial1.print (Vypos.Kp);
873
874
             Serial1.println();
875
876
             break;
877
          case 1097:
878
             Vypos.Ki = pram / 1000;
879
            EEPROM. write(64, stmp & 0b11111111);
EEPROM. write(65, stmp >> 8);
Serial1.print("Vypos_Ki = "); Serial1.print(Vypos.Ki);
880
881
882
             Serial1.println();
883
884
             break:
          case 1098:
885
886
             \mathrm{Vypos.Kd} = \mathrm{pram} \ / \ 1000;
887
             EEPROM. write (66, stmp & 0b11111111);
888
             EEPROM. write (67, stmp >> 8);
Serial1.print ("Vypos_Kd = "); Serial1.print (Vypos.Kd);
889
890
891
             Serial1.println();
892
             break;
          case 1100:
893
894
895
             EstimatedG = pram / 1000;
             EEPROM. write (70, stmp & 0b11111111);
896
             EEPROM. write (71, \text{ stmp} >> 8);
897
             Serial1.print("Gravity = "); Serial1.print(EstimatedG);
898
             Serial1.println();
899
900
             break;
        }
901
902
903
    }
```

Mark3 Flight Controller Code - Library of Interrupt

```
1 #include "Arduino.h"
2 void InitComm();
3 void ISR1();
4 void ISR2();
                -SBUS-
5 /*-
                            -*/
6
  void RC_refine();
7 void OtusSerial();
8 void ComOrder();
9 void PramOrder();
10 void OtusMovingAverage();
   uint16_t channels[16];
11
12 uint8_t failSafe;
13 uint16_t lostFrames = 0;
14
   float moving_ave[13][5], sum_ave[13];
15
16
17
                            ----*/
   /*-
18
              -Lighthouse-
                                  -*/
19
  #define IRsensor1 23
20
   #define IRsensor2 22
21
22 #define IRsensor3 17
   #define IRsensor4 16
23
24 #define IRsensor5 24
25 #define IRsensor6 26
26 #define IRsensor7 27
27 #define IRsensor8 28
                            -*/
28
   /*
```

Mark3 Flight Controller Code - Interrupt

```
void InitComm()
1
2
   {
      Serial1.begin(230400);
3
      Serial1.begin(230400);
4
     R9DS.begin();
5
6
     pinMode(LED0, OUTPUT);
     pinMode(LED1, OUTPUT);
7
     pinMode(LED2, OUTPUT);
8
      digitalWrite(LED0, HIGH);
9
      digitalWrite(LED1, LOW);
10
      digitalWrite(LED2, LOW);
11
      Copter. RCsignal. ROLL = 1000;
12
      Copter. RCsignal.PITCH = 1000;
13
      Copter. RCsignal.THROTTLE = 250;
14
      Copter.RCsignal.YAW = 1000;
15
16
      Copter. RCsignal.MODE = 250;
      Copter. RCsignal.SWITCH = 1700;
17
18
   }
   void RC_refine()
19
20
   {
      if (R9DS.read(channels, &failSafe, &lostFrames))
21
^{22}
     {
        Copter. RCsignal. ROLL = channels [0];
23
        Copter. RCsignal.PITCH = channels[1]
24
25
        Copter. RCsignal. THROTTLE = channels [2];
        Copter.RCsignal.YAW = channels[3];
26
        Copter. RCsignal. MODE = channels [4];
27
^{28}
        Copter. RCsignal.SWITCH = channels [5];
        Copter. RCsignal.CH7 = channels [6];
29
        Copter. RCsignal.CH8 = channels[7];
30
        Copter. RCsignal. CH9 = channels [8];
31
        Copter. RCsignal. CH10 = channels [9];
32
33
      if (Copter.Ctrl_timer1 == 2)
34
35
      {
36
        Copter.Otus_Clear();
        String comdata =
37
        Copter.xbeetime1 = 0;
38
39
        while (Serial1.available() > 0)
          comdata += char(Serial1.read());
40
^{41}
        Copter.xbee_length = comdata.length();
        for (int i = 0; i < Copter.xbee_length; i++)
42
43
          Copter.xbee_data[100 + i] = \text{comdata}[i];
44
        if (Copter.xbee_length == 4)
45
        {
          //Copter.comorder = 0;
46
47
          short com_tmp = 0;
          for (uint8_t i = 0; i < 4; i++)
48
            com_tmp = com_tmp * 10 + (comdata[i] - '0');
49
          //ComOrder();
50
51
          /*
            Serial1.println(uint8_t(comdata[0]));
52
            Serial1.println(uint8_t(comdata[1]));
53
            Serial1.println(uint8_t(comdata[2]));
54
            Serial1.println(uint8_t(comdata [3]));
55
56
            Serial1.println(Copter.xbee_length);
            Serial1.println(Copter.comorder);
57
58
          //Serial1.flush();
59
          i f
             (\text{com}_{\text{tmp}} \ge 1000 \&\& \text{com}_{\text{tmp}} \le 5000)
60
            \hat{Copter.comorder} = com_tmp;
61
62
        }
```

```
63
        else if (Copter.xbee_length < 12
                 && Copter.xbee_length > 5
64
                 && (Copter.xbee_data[100 + 0] == '&'
65
                      && Copter.xbee_data[100 + 5] == '_'
66
67
                     && Copter.xbee_data [100 + Copter.xbee_length - 1] = '*')
          PramOrder();
68
69
        else if (Copter.xbee_length \geq 20)
70
          OtusSerial();
71
72
          OtusMovingAverage();
          //Serial1.println(Copter.xbee_length);
73
74
        }
75
      }
    }
76
77
    void OtusMovingAverage()
78
    {
      Copter.Otus.x =
79
        Copter.data_limitation(Copter.Otus.x, -10.0, 10.0);
80
81
      Copter.Otus.y =
        Copter.data_limitation(Copter.Otus.y, -10.0, 10.0);
82
83
      Copter.Otus.z =
        Copter.data_limitation(Copter.Otus.z, -5.0, 10.0);
84
      Copter.Otus.vx =
85
86
        Copter.data_limitation(Copter.Otus.vx, -50.0, 50.0);
      Copter.Otus.vy =
87
88
        Copter.data_limitation(Copter.Otus.vy, -50.0, 50.0);
89
      Copter. Otus. vz =
        Copter.data_limitation(Copter.Otus.vz, -50.0, 50.0);
90
91
      Copter.Otus.roll =
        Copter.data_limitation(Copter.Otus.roll, -180.0, 180.0);
92
93
      Copter.Otus.pitch =
        Copter.data_limitation(Copter.Otus.pitch, -90.0, 90.0);
94
95
      Copter.Otus.yaw =
        Copter.data_limitation(Copter.Otus.yaw, -180.0, 180.0);
96
      Copter.Otus.q0 =
97
        Copter.data_limitation(Copter.Otus.q0, -1.0, 1.0);
98
      Copter.Otus.q1 =
99
        Copter.data_limitation(Copter.Otus.q1, -1.0, 1.0);
100
      Copter.Otus.q2 =
101
        Copter.data_limitation(Copter.Otus.q2, -1.0, 1.0);
102
103
      Copter.Otus.q3 =
        Copter.data_limitation(Copter.Otus.q3, -1.0, 1.0);
104
105
106
      Copter.Target.plan_x =
        Copter.data_limitation(Copter.Target.plan_x, -1.5, 1.5);
107
108
      Copter. Target. plan_y =
        Copter.data_limitation(Copter.Target.plan_y, -1.5, 1.5);
109
110
      Copter.Target.plan_z =
        Copter.data_limitation(Copter.Target.plan_z, 0, 2.2);
111
112
      Copter.Target.plan_psi =
113
        Copter.data_limitation(Copter.Target.plan_psi, -180, 180);
114
                    -Moving Average-
                                                 */
      for (uint8_t j = 0; j < 13; j++)
115
        sum_ave[j] = sum_ave[j] - moving_ave[j][4] / 5;
116
117
      for (uint8_t i = 4; i > 0; i--)
118
        for (uint8_t j = 0; j < 13; j++)
119
          moving_ave[j][i] = moving_ave[j][i - 1];
120
121
      moving_ave[0][0] = Copter.Otus.x;
      moving_ave[1][0] = Copter.Otus.y;
122
      moving_ave[2][0] = Copter.Otus.z;
123
124
125
      moving_ave[3][0] = Copter.Otus.vx;
      moving_ave[4][0] = Copter.Otus.vy;
126
127
      moving_ave[5][0] = Copter.Otus.vz;
128
```

```
129
      moving_ave[6][0] = Copter.Otus.roll;
      moving_ave[7][0] = Copter.Otus.pitch;
130
131
      moving_ave[8][0] = Copter.Otus.yaw;
132
133
      moving_ave[9][0] = Copter.Otus.q0;
      moving_ave[10][0] = Copter.Otus.q1;
134
      135
136
137
      for (uint8_t j = 0; j < 13; j++)
138
        sum_ave[j] = sum_ave[j] + moving_ave[j][0] / 5;
139
140
      Copter.Otus.x = sum_ave[0];
141
142
      Copter.Otus.y = sum_ave[1];
      Copter.Otus.z = sum_ave[2];
143
144
      Copter.Otus.vx = sum_ave[3];
145
146
      Copter.Otus.vy = sum_ave[4];
      Copter.Otus.vz = sum_ave[5];
147
148
      Copter.Otus.q0 = sum_ave[9];
149
150
      Copter.Otus.q1 = sum_ave[10];
      Copter.Otus.q2 = sum_ave [11];
151
152
      Copter. Otus. q3 = sum_ave[12];
   }
153
   void OtusSerial()
154
    {
155
      for (int16_t i = 100 + 3; i < 100 + Copter.xbee_length - 5; i++)
156
157
      {
        switch (Copter.xbee_data[i])
158
159
        {
          case 21:
160
            if (Copter.xbee_data[i + 1] == 101)
161
162
            {
                 ((Copter.xbee_data[i - 1] == 131
163
              i f
                   & Copter.xbee_data[i - 2] = 121
164
165
                   && Copter.xbee_data[i - 3] == 111)
                  && (Copter.xbee_data[i + 6] = 22
166
167
                       & Copter.xbee_data [i + 7] = 102)
168
              {
                 Copter.state.update_x = 1;
169
                 Copter.otus_tmp.ul =
170
                   (Copter.xbee_data[i + 5] \ll 24)
171
172
                     (Copter.xbee_data[i + 4] \ll 16)
173
                     (Copter.xbee_data[i + 3] \ll 8)
                     Copter.xbee_data[i + 2];
174
175
                 Copter.Otus.x = Copter.otus_tmp.f;
176
              }
177
            break;
178
          case 22:
179
            if (Copter.xbee_data[i + 1] == 102)
180
181
            {
              if ((Copter.xbee_data[i - 6] = 21)
182
                   && Copter.xbee_data[i - 5] == 101)
183
                  && (Copter.xbee_data[i + 6] == 23
184
                       && Copter.xbee_data[i + 7] == 103))
185
186
              {
                 Copter.state.update_y = 1;
187
188
                 Copter.otus_tmp.ul =
                   (Copter.xbee_data[i + 5] \ll 24)
189
                     (Copter.xbee_data[i + 4] \ll 16)
190
191
                     (Copter.xbee_data[i + 3] \ll 8)
                    Copter.xbee_data[i + 2];
192
193
                 Copter.Otus.y = Copter.otus_tmp.f;
              }
194
```

195break; 196 case 23: 197 198 if (Copter.xbee_data[i + 1] = 103) { 199 if ((Copter.xbee_data[i - 6] == 22 && Copter.xbee_data[i - 5] == 102) 200 201 && (Copter.xbee_data $\dot{[i + 6]} = 24$ 202 && Copter.xbee_data[i + 7] == 104)) 203 204{ 205Copter.state.update_z = 1;206 Copter.otus_tmp.ul = $(Copter.xbee_data[i + 5] \ll 24)$ 207 $(Copter.xbee_data[i + 4] \ll 16)$ 208 $(Copter.xbee_data[i + 3] \ll 8)$ 209 Copter.xbee_data[i + 2];210 211Copter.Otus.z = Copter.otus_tmp.f; 212} 213break; 214 **case** 24: 215if (Copter.xbee_data[i + 1] == 104) 216217 { if $((Copter.xbee_data[i - 6] = 23)$ 218&& Copter.xbee_data[i - 5] == 103) 219 && (Copter.xbee_data[i + 6] = 25220 && Copter.xbee_data[i + 7] == 105)) 221222{ 223 Copter.state.update_vx = 1; Copter.otus_tmp.ul = 224 $(Copter.xbee_data[i + 5] \ll 24)$ 225 $(Copter.xbee_data[i + 4] << 16)$ 226227 $(Copter.xbee_data[i + 3] \ll 8)$ Copter.xbee_data[i + 2];228 229 Copter.Otus.vx = Copter.otus_tmp.f; } 230 231break; 232**case** 25: 233 if $(Copter.xbee_data[i + 1] == 105)$ 234235{ 236 if $((Copter.xbee_data[i - 6] = 24)$ && Copter.xbee_data [i - 5] = 104) 237&& (Copter.xbee_data[i + 6] = 26238 && Copter.xbee_data[i + 7] == 106)) 239240{ Copter.state.update_vy = 1; 241242 $Copter.otus_tmp.ul =$ 243 $(Copter.xbee_data[i + 5] \ll 24)$ $(Copter.xbee_data[i + 4] \ll 16)$ 244 $(Copter.xbee_data[i + 3] \ll 8)$ 245246 Copter.xbee_data[i + 2]; Copter.Otus.vy = Copter.otus_tmp.f; 247} 248 249break; 250**case** 26: 251if (Copter.xbee_data[i + 1] == 106) 252253{ if $((Copter.xbee_data[i - 6] = 25)$ 254255& Copter.xbee_data [i - 5] = 105&& (Copter.xbee_data[i + 6] = 27256& Copter.xbee_data[i + 7] == 107)) 257258{ Copter.state.update_vz = 1; 259Copter.otus_tmp.ul = 260

261 $(Copter.xbee_data[i + 5] \ll 24)$ $(Copter.xbee_data[i + 4] \ll 16)$ 262263 $(Copter.xbee_data[i + 3] \ll 8)$ 264Copter.xbee_data[i + 2];265 $Copter.Otus.vz = Copter.otus_tmp.f;$ } 266267 break: 268**case** 27: 269 if $(Copter.xbee_data[i + 1] == 107)$ 270 271{ if ((Copter.xbee_data[i - 6] == 26) 272&& Copter.xbee_data[i - 5] == 106) 273274&& (Copter.xbee_data[i + 6] == 28 && Copter.xbee_data[i + 7] = 108)275276{ Copter.state.update_psi = 1; 277Copter.otus_tmp.ul = 278 $(Copter.xbee_data[i + 5] \ll 24)$ 279 $(Copter.xbee_data[i + 4] \ll 16)$ 280 $(Copter.xbee_data[i + 3] \ll 8)$ 281 282Copter.xbee_data[i + 2];283 Copter.Otus.yaw = Copter.otus_tmp.f; 284Copter.Otus.yaw_sin = sin(Copter.Otus.yaw); 285Copter.Otus.yaw_cos = cos(Copter.Otus.yaw); 286 287 } 288 289 break; case 28: 290 291if (Copter.xbee_data[i + 1] = 108) 292{ $((Copter.xbee_data[i - 6] = 27)$ 293 && Copter.xbee_data [i - 5] == 107) 294&& (Copter.xbee_data[i + 6] == 29 295296&& Copter.xbee_data[i + 7] == 109)) 297 { Copter.state.update_theta = 1; 298 Copter.otus_tmp.ul = 299 $(Copter.xbee_data[i + 5] \ll 24)$ 300 $(Copter.xbee_data[i + 4] \ll 16)$ 301 302 $(Copter.xbee_data[i + 3] \ll 8)$ Copter.xbee_data[i + 2]; Copter.Otus.pitch = Copter.otus_tmp.f; 303 304 } 305 306 break; 307 **case** 29: 308 if (Copter.xbee_data[i + 1] == 109) 309 310 { if $((Copter.xbee_data[i - 6] = 28)$ 311&& Copter.xbee_data[i - 5] == 108)312 && (Copter.xbee_data[i + 6] == 30 313 314 && Copter.xbee_data[i + 7] == 110)) 315 { Copter.state.update_phi = 1; 316317 Copter.otus_tmp.ul = $(Copter.xbee_data[i + 5] \ll 24)$ 318 $(Copter.xbee_data[i + 4] \ll 16)$ 319 320 $(Copter.xbee_data[i + 3] \ll 8)$ Copter.xbee_data[i + 2]; 321 Copter.Otus.roll = Copter.otus_tmp.f; 322 323 } 324break; 325**case** 31: 326

327 if (Copter.xbee_data[i + 1] = 111) 328 { if ((Copter.xbee_data[i - 6] == 29 329 && Copter.xbee_data[i - 5] == 109) 330 && (Copter.xbee_data[i + 6] = 32331 && Copter.xbee_data [i + 7] = 112)332 333 { Copter.otus_tmp.ul = 334 $(Copter.xbee_data[i + 5] \ll 24)$ 335 $(Copter.xbee_data[i + 4] \ll 16)$ 336 $(Copter.xbee_data[i + 3] \ll 8)$ 337 Copter.xbee_data[i + 2];338 Copter.Otus. $q0 = Copter.otus_tmp.f$; 339 340Copter.Otus.q0 *= -1;341 } 342 break; 343 **case** 32: 344if $(Copter.xbee_data[i + 1] == 112)$ 345346 { if ((Copter.xbee_data[i - 6] == 31 347 && Copter.xbee_data [i - 5] == 111) 348 && (Copter.xbee_data [i + 6] == 33 349 350 && Copter.xbee_data[i + 7] == 113)) 351{ $Copter.otus_tmp.ul =$ 352 $(Copter.xbee_data[i + 5] \ll 24)$ 353 354 $(Copter.xbee_data[i + 4] \ll 16)$ $(Copter.xbee_data[i + 3] \ll 8)$ 355| Copter.xbee_data[i + 2];356 Copter.Otus.q1 = Copter.otus_tmp.f; 357 358Copter.Otus.q1 *= -1;} 359 360 break; 361 **case** 33: 362 if (Copter.xbee_data[i + 1] = 113) 363 364 { if ((Copter.xbee_data[i - 6] == 32 365 366 && Copter.xbee_data [i - 5] == 112) && (Copter.xbee_data [i + 6] = 34367 && Copter.xbee_data[i + 7] == 114)) 368 369 { Copter.otus_tmp.ul = 370 $(Copter.xbee_data[i + 5] << 24)$ 371 $(Copter.xbee_data[i + 4] \ll 16)$ 372 373 $(Copter.xbee_data[i + 3] \ll 8)$ Copter.xbee_data[i + 2]; 374Copter.Otus. $q2 = Copter.otus_tmp.f;$ 375 } 376 377 378 break; **case** 34: 379 380 if $(Copter.xbee_data[i + 1] == 114)$ { 381 382 if $((Copter.xbee_data[i - 6] == 33)$ & Copter.xbee_data [i - 5] = 113)383 && (Copter.xbee_data[i + 6] == 35 384 && Copter.xbee_data[i + 7] == 115)) 385 386 ${\rm Copter.otus_tmp.ul} \ =$ 387 $(Copter.xbee_data[i + 5] \ll 24)$ 388 $(Copter.xbee_data[i + 4] \ll 16)$ 389 $(Copter.xbee_data[i + 3] \ll 8)$ 390 Copter.xbee_data[i + 2]; 391 Copter.Otus.q3 = Copter.otus_tmp.f; 392

393 } 394 395 break; 396 **case** 35: if (Copter.xbee_data[i + 1] = 115) 397 398 { if ((Copter.xbee_data[i - 6] == 34 399 && Copter.xbee_data[i - 5] == 114) 400 && (Copter.xbee_data[i + 6] == 36 401 && Copter.xbee_data[i + 7] == 116)) 402403 { ${\rm Copter.otus_tmp.ul} =$ 404 $(Copter.xbee_data[i + 5] \ll 24)$ 405406 $(Copter.xbee_data[i + 4] \ll 16)$ $(Copter.xbee_data[i + 3] \ll 8)$ 407 Copter.xbee_data[i + 2];408 Copter. Target. plan_x = Copter.otus_tmp.f; 409} 410411 break; 412 **case** 36: 413if $(Copter.xbee_data[i + 1] == 116)$ 414 415{ if $((Copter.xbee_data[i - 6] == 35)$ 416 && Copter.xbee_data [i - 5] == 115) 417 418 && (Copter.xbee_data[i + 6] == 37 && Copter.xbee_data[i + 7] == 117)) 419 420 { Copter.otus_tmp.ul = 421 $(Copter.xbee_data[i + 5] \ll 24)$ 422 $(Copter.xbee_data[i + 4] \ll 16)$ 423 424 $(Copter.xbee_data[i + 3] \ll 8)$ 425Copter.xbee_data[i + 2];Copter.Target.plan_y = Copter.otus_tmp.f; 426} 427 428 break: 429**case** 37: 430 if $(Copter.xbee_data[i + 1] == 117)$ 431 432{ if ((Copter.xbee_data[i - 6] == 36 433 & Copter.xbee_data [i - 5] = 116) 434435&& (Copter.xbee_data[i + 6] == 38 && Copter.xbee_data[i + 7] = 118)436 437 { Copter.otus_tmp.ul = 438 439 $(Copter.xbee_data[i + 5] \ll 24)$ $(Copter.xbee_data[i + 4] \ll 16)$ 440 441 $(Copter.xbee_data[i + 3] \ll 8)$ Copter.xbee_data[i + 2];442 Copter.Target.plan_z = Copter.otus_tmp.f; 443} 444 445break; 446**case** 38: 447 448 if (Copter.xbee_data[i + 1] = 118) 449{ if ((Copter.xbee_data[i - 6] == 37 450&& Copter.xbee_data [i - 5] = 117) 451&& (Copter.xbee_data[i + 6] == 30 452&& Copter.xbee_data[i + 7] == 110)) 453454ł Copter.otus_tmp.ul = 455 $(Copter.xbee_data[i + 5] \ll 24)$ 456 $(Copter.xbee_data[i + 4] \ll 16)$ 457 $(Copter.xbee_data[i + 3] \ll 8)$ 458

```
459
                   | Copter.xbee_data[i + 2];
                 Copter.Target.plan_psi = Copter.otus_tmp.f;
460
461
               }
462
             break;
463
464
           case 30:
             if (Copter.xbee_data[i + 1] = 110)
465
466
             {
                 ((Copter.xbee_data[i - 6] == 38
467
               i f
                    && Copter.xbee_data [i - 5] == 118)
468
469
                   && (Copter.xbee_data[i + 4] == 50
                       && Copter.xbee_data[i + 5] = 75
470
                       && Copter.xbee_data[i + 6] = 100)
471
472
               {
                 Copter.state.comm =
473
                   (Copter.xbee_data[i + 3] \ll 8)
474
                     Copter.xbee_data[i + 2];
475
476
                 if (Copter.state.comm \geq 1000
                     && Copter.state.comm \leq 4000)
477
478
                   Copter.comorder = Copter.state.comm;
                 //Serial.println(Copter.state.comm);
479
480
               }
481
482
             break;
483
        }
484
      }
485
    }
486
    void PramOrder()
487
    {
      int16_t order = 0, num;
488
      uint16_t stmp = 0;
489
490
      for (num = 1; num \le 4; num++)
        order = order * 10 + (Copter.xbee_data[100 + num] - '0');
491
      for (num = 6; num < (Copter.xbee_length - 1); num++)
492
        stmp = stmp * 10 + (Copter.xbee_data[100 + num] - '0');
493
      Copter.Xbee_receive(order, stmp);
494
495
    }
```

Mark3 Flight Controller Code - Motor Driver

```
1 #include "Copter.h"
2 void _Copter:: Motor_init()
3
   {
      voltageavg = (float)analogRead(A14) * 0.013841;
4
5
6
     pinMode(motor1, OUTPUT);
     pinMode(motor2, OUTPUT);
\overline{7}
     pinMode(motor3, OUTPUT);
8
     pinMode(motor4, OUTPUT);
9
10
      analogWriteFrequency(motor1, 400);
11
      analogWriteFrequency(motor2, 400);
12
      analogWriteFrequency(motor3, 400);
13
14
      analogWriteFrequency(motor4, 400);
      analogWriteResolution(16);
15
16
                 -OutFunction.m-
                                        -*/
17
     InputK1 = 130958.617;
18
19
      InputK2 = 1290232.68;
20
      InputK3 = 1728826.63;
     InputK4 = 10113268.61;
21
22
     Motor_stop();
  }
23
   void _Copter::InputTransform()
^{24}
25
   {
```

```
26
     omega12 = InputK1 * U1 - InputK2 * U2 +
                InputK3 * U3 + InputK4 * U4;
27
     omega22 = InputK1 * U1 + InputK2 * U2 -
28
29
                InputK3 * U3 + InputK4 * U4;
     omega32 = InputK1 * U1 + InputK2 * U2 +
30
                InputK3 * U3 - InputK4 * U4;
31
     omega42 = InputK1 * U1 - InputK2 * U2 -
InputK3 * U3 - InputK4 * U4;
32
33
     if (\text{omega12} < 0) \text{omega12} = 0;
34
35
     if (omega22 < 0) omega22 = 0;
     if (omega32 < 0) omega32 = 0;
36
37
     if (omega42 < 0) omega42 = 0;
     omega1 = sqrt(omega12);
38
39
     omega2 = sqrt(omega22);
40
     omega3 = sqrt(omega32);
41
     omega4 = sqrt(omega42);
     MotorModel(omega1, omega2, omega3, omega4);
42
   }
43
   void _Copter::MotorModel(double omega1,
44
45
                              double omega2, double omega3, double omega4)
46
     double param_a = 1166.0, param_b = 5393,
47
             param_c = 299600, param_d = 1544, param_e = 894.5;
48
     PWM1 = (omega1 * omega1 + param_b * omega1 + param_c) /
49
50
             (param_a * voltageavg + param_d) + param_e;
51
     PWM2 = (omega2 * omega2 + param_b * omega2 + param_c) /
             (param_a * voltageavg + param_d) + param_e;
52
     PWMB = (omega3 * omega3 + param_b * omega3 + param_c) /
53
             (param_a * voltageavg + param_d) + param_e;
54
     PWM4 = (omega4 * omega4 + param_b * omega4 + param_c) /
55
56
             (param_a * voltageavg + param_d) + param_e;
     if (PWM1 < 1055) PWM1 = 1055;
57
58
     if (PWM2 < 1055) PWM2 = 1055;
     if (PWM3 < 1055) PWM3 = 1055;
59
60
     if (PWM4 < 1055) PWM4 = 1055;
        (PWM1 > 1550) PWM1 = 1550;
61
     i f
     if (PWM2 > 1550) PWM2 = 1550;
62
     if (PWM3 > 1550) PWM3 = 1550;
63
     if (PWM4 > 1550) PWM4 = 1550;
64
     MotorRun();
65
66
   }
   void _Copter::Motor_stop()
67
68
   {
     PWM = pwm_factor * 950;
69
70
     analogWrite(motor1, PWM);
     analogWrite (motor2, PWM);
71
72
     analogWrite(motor3, PWM);
73
     analogWrite(motor4, PWM);
74 }
   void _Copter::MotorRun()
75
76
   {
     if ((!flag.turnoff) && (flag.ARMED == 2))
77
78
     {
79
        float inputpwm1 = pwm_factor * PWM1;
       float inputpwm2 = pwm_factor * PWM2;
80
        float inputpwm3 = pwm_factor * PWM3;
81
^{82}
        float inputpwm4 = pwm_factor * PWM4;
       analogWrite(motor1, inputpwm1);
83
       analogWrite(motor2, inputpwm2);
84
       analogWrite(motor3, inputpwm3);
85
86
       analogWrite(motor4, inputpwm4);
87
     }
     else
88
       Motor_stop();
89
90
   }
```

```
182
```

Mark3 Flight Controller Code - Attitude Control

```
1 #include "Copter.h"
2 void _Copter::AttitudeControl()
3 {
      if (Ctrl_timer1 \ge 4)
4
\mathbf{5}
     {
                     ------Roll Command------*/
6
        if (flag.mode == Attitude_mode || flag.mode == Altitude_mode)
7
8
        {
          if (RCsignal.ROLL < 900)
9
10
          {
11
             //if (RCsignal.CH7 < 1000)
            Target.phi = (float)(RCsignal.ROLL - 900) / 40;
12
13
            //else
            // Target. phi = -20;
14
15
          }
          if (RCsignal.ROLL > 1100)
16
17
          {
            //if (RCsignal.CH7 < 1000)
18
            Target.phi = (float)(RCsignal.ROLL - 1100) / 40;
19
            //else
20
^{21}
            //Target.phi = 20;
          }
22
             (RCsignal.ROLL >= 900 && RCsignal.ROLL <= 1100)
^{23}
          i f
24
            Target.phi = 0;
25
                             -Pitch Command-
                                                     -----*/
          if (RCsignal.PITCH < 900)
26
27
          {
            //if (RCsignal.CH7 < 1000)
28
            Target.theta = (float)(RCsignal.PITCH - 900) / 40;
29
30
            //else
            //Target.theta = -15;
31
          }
32
          if (RCsignal.PITCH > 1100)
33
          {
34
35
             //if (RC signal.CH7 < 1000)
            Target.theta = (float)(RCsignal.PITCH - 1100) / 40;
36
            //else
37
38
            //Target.theta = 15;
39
          }
          i f
             (RCsignal.PITCH >= 900 && RCsignal.PITCH <= 1100)
40
            Target.theta = 0;
41
        }
42
43
44
        Target.phi = data_limitation (Target.phi, -25, 25);
        Target.theta = data_limitation (Target.theta, -25, 25);
45
46
        Target.phi_rad = Rad(Target.phi);
        Target.theta_rad = Rad(Target.theta);
47
48
                          -Yaw Command-
                                                         -*/
        if (RCsignal.THROTTLE > 350)
49
50
        ł
          if (LockYaw != 1)
51
52
          {
53
            LockYaw = 1;
            Target.psi = state.psi;
54
55
          }
56
        }
57
        else {
          if (U1 < 0.5)
58
59
          {
            LockYaw = 0;
60
            {\tt Target.psi} = {\tt state.psi};
61
62
          }
```

63 if ((RCsignal.YAW > 1075) || (RCsignal.YAW < 925)) 64 65if (RCsignal.YAW > 1075) 66 67 { //if (RCsignal.CH7 < 1000) 68Target.psi += ((RCsignal.YAW - 1075) / 250.0f); 69 //else 70// Target.psi += 0.5;71} 72if (RCsignal.YAW < 925) 73 74 { //if (RCsignal.CH7 < 1000) 75Target.psi += ((RCsignal.YAW - 925) / 250.0f); 7677 //else 78//Target.psi -= 0.5; 79 } if (Target.psi > 180.0f) Target.psi -= 360.0f; 80 else if (Target.psi < -180.0f)Target.psi += 360.0f; 81 } 82 83 if (RCsignal.CH8 > 1000)84 85 Target.psi = Target.plan_psi; 86 Target.psi_rad = Rad(Target.psi); 87 -P Control-88 -*/ //phi 89 Phicon.Input[0] = Target.phi_rad - state.phi_rad; 90 91 Phicon.Output[0] = phiang.Kp * Phicon.Input[0]; 9293 //theta Thetacon.Input [0] = Target.theta_rad - state.theta_rad; 94 95Thetacon. Output [0] = thetaang.Kp * Thetacon.Input [0]; 96 97 //psi if ((Target.psi_rad - state.psi_rad) >= M_PI || 98 (Target.psi_rad - state.psi_rad) < - M_PI) 99 100 101 if (Target.psi_rad > 0 && state.psi_rad < 0) $Psicon.Input[0] = (-M_PI - state.psi_rad) +$ 102(Target.psi_rad - M_PI); 103 if (Target.psi_rad < 0 && state.psi_rad > 0) 104 $Psicon.Input[0] = (M_PI - state.psi_rad) +$ 105 106 $(Target.psi_rad + M_PI);$ } 107Psicon.Input[0] = Target.psi_rad - state.psi_rad; else 108 109Psicon.Output[0] = psiang.Kp * Psicon.Input[0];110 111 } 112AngularRateControl(); 113 } 114void _Copter::AngularRateControl() { 115 116//p Target.p_rad = Phicon.Output [0];117 $Target.p = Degree(Target.p_rad);$ 118 119 120 //q $Target.q_rad = Thetacon.Output[0];$ 121122 $Target.q = Degree(Target.q_rad);$ 123//r -Nonlinear Constrain--*/ 124 /*- $Target.r_rad = Psicon.Output[0];$ 125 $Target.r = Degree(Target.r_rad);$ 126 127//p

```
128
        Pcon.Input[0] = Target.p_rad - state.p_rad;
        Pcon.Output[0] = Pcon.Input[0] * pvel.Kp +
129
        (Pcon.Input[0] - Pcon.Input[1]) * pvel.Kd / innerT;
130
131
        Pcon.Output[1] = Pcon.Output[0];
        Pcon.Input[1] = Pcon.Input[0];
132
133
        //q
        Qcon.Input[0] = Target.q_rad - state.q_rad;
134
        Qcon.Output[0] = Qcon.Input[0] * qvel.Kp +
(Qcon.Input[0] - Qcon.Input[1]) * qvel.Kd / innerT;
135
136
        Qcon.Output[1] = Qcon.Output[0];
137
        \operatorname{Qcon.Input}[1] = \operatorname{Qcon.Input}[0];
138
139
        //r
140
        \operatorname{Rcon.Input}[0] = \operatorname{Target.r_rad} - \operatorname{state.r_rad};
        Rcon. Output [0] = Rcon. Input [0] * rvel.Kp +
(Rcon. Input [0] - Rcon. Input [1]) * rvel.Kd / innerT;
141
142
143
        \operatorname{Rcon}. Output [1] = \operatorname{Rcon}. Output [0];
        \operatorname{Rcon.Input}[1] = \operatorname{Rcon.Input}[0];
144
        U2 = Pcon.Output[0];
145
        U3 = Qcon.Output[0];
146
        U4 = Rcon.Output[0];
147
148
149
     void _Copter::ControlReset()
150
151
     {
        Pcon.Integral = 0;
152
        Qcon.Integral = 0;
153
        Rcon.Integral = 0;
154
     }
155
```

Mark3 Flight Controller Code - Position Control

```
1 #include "Copter.h"
   void _Copter::TranslationControl()
\mathbf{2}
3
   {
     if (Ctrl_timer1 \ge 4)
4
5
     {
       if ((flag.mode == loiter_mode))
6
7
       {
          float tmp_roll, tmp_pitch;
8
          if (RCsignal.ROLL < 850)
9
10
            tmp_roll = ((float)(RCsignal.ROLL) - 850) / 100000;
          if (RCsignal.ROLL > 1150)
11
            tmp_roll = ((float)(RCsignal.ROLL) - 1150) / 100000;
12
          if (RCsignal.PITCH < 850)
13
            tmp_pitch = (850 - (float)(RCsignal.PITCH)) / 100000;
14
          if (RCsignal.PITCH > 1150)
15
           tmp_pitch = (1150 - (float)(RCsignal.PITCH)) / 100000;
16
          if (RCsignal.ROLL <= 1150 && RCsignal.ROLL >= 850)
17
            tmp_roll = 0;
18
          if (RCsignal.PITCH <= 1150 && RCsignal.PITCH >= 850)
19
20
            tmp_pitch = 0;
          Target.x += (tmp_pitch * state.psi_cos -
21
22
          tmp_roll * state.psi_sin);
          Target.y += (tmp_roll * state.psi_cos +
23
          tmp_pitch * state.psi_sin);
24
          Target.x = data_limitation (Target.x, -2.00, 2.00);
25
          Target.y = data_limitation (Target.y, -2.00, 2.00);
26
27
          if (RCsignal.CH8 > 1000)
28
29
          {
            Target.x = Target.plan_x;
30
            Target.y = Target.plan_y;
31
32
          //X Control;
33
```

```
34
          Xcon.Input[0] = Target.x - state.x;
         Xcon.Output[0] = Xpos.Kp * Xcon.Input[0];
35
36
          Target.vx = Xcon.Output[0];
37
          //Y Control;
          Ycon.Input[0] = Target.y - state.y;
38
          Ycon.Output[0] = Ypos.Kp * Ycon.Input[0];
39
          Target.vy = Y con.Output [0];
40
          //Vx Control
41
42
          Vxcon.Input[0] = (Target.vx - state.vx) / 57.3;
         Vxcon.Output[0] = Vxcon.Input[0] * Vxpos.Kp +
43
          (Vxcon.Input [0] - Vxcon.Input [1]) * Vxpos.Kd / outerT;
44
          Vxcon.Output[1] = Vxcon.Output[0];
45
46
          //Vv Control
47
          Vycon.Input[0] = (Target.vy - state.vy) / 57.3;
          Vycon.Output [0] = Vycon.Input [0] * Vypos.Kp +
48
49
          (Vycon.Input [0] - Vycon.Input [1]) * Vypos.Kd / outerT;
          Vycon.Output[1] = Vycon.Output[0];
50
51
          float tmp_a, tmp_b, tmp_c1, tmp_c2, tmp_x1, tmp_x2;
52
53
          tmp_a = state.psi_cos;
54
          tmp_b = state.psi_sin
          tmp_c1 = Vxcon.Output[0] * 0.647 * (U1 * 0.9);
55
56
          tmp_c2 = Vycon.Output[0] * 0.647 * (U1 * 0.9);
           /Target Phi
57
          Target.sin_phi = tmp_a * tmp_c2 - tmp_b * tmp_c1;
58
          Target.sin_phi = data_limitation(Target.sin_phi, -1, 1);
59
          Target.phi_rad = asin(Target.sin_phi);
60
61
          Target.phi = Degree(Target.phi_rad);
62
          Target.phi = data_limitation (Target.phi, -15, 15);
63
          Target.phi_rad = Rad(Target.phi);
64
          //Target Theta
65
          Target.cos_phi = cos(Target.phi_rad);
66
67
          Target.sin_theta = (-(tmp_a * tmp_c1 + tmp_b * tmp_c2))
68
          / Target.cos_phi;
          Target.sin_theta = data_limitation (Target.sin_theta, -1, 1);
69
70
          Target.theta_rad = asin(Target.sin_theta);
71
          Target.theta = Degree(Target.theta_rad);
72
          Target.theta = data_limitation (Target.theta, -15, 15);
73
          Target.theta_rad = Rad(Target.theta);
74
75
       }
76
     }
   }
77
   void _Copter :: AltitudeControl()
78
79
   {
     if (Ctrl_timer1 \ge 4)
80
81
     {
        if ((flag.mode == Altitude_mode) || (flag.mode == loiter_mode))
82
83
       {
         if (RCsignal.THROTTLE < 850)
84
85
          {
86
            if (RCsignal.CH7 < 1000)
              Target.z += ((float)(RCsignal.THROTTLE) - 850) / 100000;
87
88
            else
              Target.z -= 0.003;
89
90
          }
          if (RCsignal.THROTTLE > 1150)
91
92
          {
            if (RCsignal.CH7 < 1000)
93
94
              Target.z += ((float)(RCsignal.THROTTLE) - 1150) / 100000;
            else
95
              Target.z += 0.003;
96
97
          Target.z = data_limitation (Target.z, 0.20, 2.00);
98
```

```
99
         if (RCsignal.CH8 > 1000)
100
101
           Target.z = Target.plan_z;
        ZControl();
102
103
        VzControl();
104
      float StickThrust = 0.008193 * RCsignal.THROTTLE - 2.458;
105
      if (flag.mode == Attitude_mode)
106
107
      ł
        U1 = StickThrust / (state.theta_cos * state.phi_cos);
108
109
        Target.z = 0;
        state.flight_state [0] = 1; //stand by
110
        state.flight_state [1] = 0; //take off
111
        state.flight_state [2] = 0; //flight
112
        state.flight_state [3] = 0; //land
113
        state.takeoff_t = 0;
114
        state.landing_t = 0;
115
116
      }
      else if ((flag.mode == Altitude_mode) ||
117
118
      (flag.mode == loiter_mode))
119
      ł
        uint8_t i, fliorder;
120
121
        float tmp;
        for (i = 0; i < 4; i++)
122
           if (state.flight_state[i])
123
             fliorder = (i + 1) * 10;
124
         //Serial1.print(fliorder);Serial1.print('\t');
125
         //Serial1.print(state.takeoff_t);Serial1.print('\t');
126
        //Serial1.println();
127
        switch (fliorder)
128
129
        {
          case 10: //-
U1 = 0;
130
                                      -stand by
131
132
             Target.x = state.x;
             Target.y = state.y
133
             if (RCsignal.THROTTLE > 850 && RCsignal.THROTTLE
134
135
            < 1150 \&\& voltageavg >= 10.5)
136
             {
               state.takeoff_t = state.takeoff_t + 2;
137
               if (state.takeoff_t > 1000)
138
139
               {
                 state.takeoff_t = 1000;
140
                 state.flight_state [0] = 0; //stand by
141
                 state.flight_state [1] = 1; //take off
142
                 state.flight_state[2] = 0; //flight
143
144
                 state.flight_state [3] = 0; //land
               }
145
             }
146
             else if (RCsignal.THROTTLE < 350)
147
               state.takeoff_t = 0;
148
             break;
149
150
           case 20: //-
                                                          -take off
             if (state.takeoff_t > 0)
151
152
             {
153
               state.takeoff_t = state.takeoff_t - 2;
               if (state.takeoff_t < 0)
154
155
                 state.takeoff_t = 0;
156
             }
157
             else
             {
158
               state.flight_state [0] = 0; //stand by
159
               state.flight_state[1] = 0; //take off
160
               state.flight_state [2] = 1; //flight
161
               state.flight_state [3] = 0; //land
162
163
               Target.z = 0.35;
164
             }
```

165 $U1 = float(1000 - state.takeoff_t) / 1000 * 6.6;$ if (RCsignal.THROTTLE < 350) 166 167 { state.flight_state [0] = 1; //stand by 168state.flight_state[1] = 0; //take off 169 state.flight_state [2] = 0; //flight170state.flight_state [3] = 0; //land 171 172U1 = 0;173174break; **case** 30: //-175-flight 176U1 = (EstimatedG + Vzcon.Output[0]) /(state.phi_cos * state.theta_cos); 177 if (voltageavg ≤ 10.5) 178179 { Target.z = 0.20; 180 if (state.z <= 0.25) 181 182 { state.landing_t = 2000;183 state.flight_state [0] = 0; //stand by 184state.flight_state [1] = 0; //take off 185 state.flight_state [2] = 0; //flight186 187state.flight_state [3] = 1; //land state.tmp_U1 = U1; 188 } 189 } 190 if (RCsignal.THROTTLE < 350) 191 192 { 193 state.landing_t = state.landing_t + 3; if (state.landing_t > 2000) 194 state.landing_t = 2000;195 if (state.landing_t == 2000 && state.z <= 0.25) 196 197{ state.flight_state [0] = 0; //stand by 198 state.flight_state[1] = 0; //take off 199state.flight_state[2] = 0; //flight 200 201 state.flight_state [3] = 1; //land 202 state.tmp_U1 = U1; 203} } 204205else if (RCsignal.THROTTLE > 850)state.landing_t = 0; 206 207 break; case 40: //--landing 208 state.landing_t --; 209 $tmp = float(state.landing_t) / 2000;$ 210 $U1 = tmp * tmp * state.tmp_U1;$ 211if $(state.landing_t = 0)$ 212213{ state.flight_state [0] = 1; //stand by 214 215state.flight_state [1] = 0; //take off state.flight_state [2] = 0; //flight216 217state.flight_state [3] = 0; //land Target.z = 0;218219220 break; 221} } 222 223} void _Copter::ZControl() 224225{ $\operatorname{Zcon.Input}[0] = \operatorname{Target.z} - \operatorname{state.z};$ 226 $\operatorname{Zcon}.\operatorname{Output}[0] = \operatorname{Zalt}.\operatorname{Kp} * \operatorname{Zcon}.\operatorname{Input}[0];$ 227 Target.vz = Zcon .Output[0]; 228229230}

```
231
    void _Copter::VzControl()
232
    {
233
      if (state.z < 0.35 || voltageavg < 10.5)
        Target.vz = data_limitation (Target.vz, -0.2, 0.2);
234
      Vzcon.Input[0] = Target.vz - state.vz;
235
      Vzcon.Output[0] = Vzcon.Input[0] * Vzalt.Kp +
236
      (Vzcon.Input [0] - Vzcon.Input [1]) * Vzalt.Kd / outerT;
237
      Vzcon.Output[0] = data_limitation(Vzcon.Output[0], -4.0, 4.0);
238
239
      Vzcon.Input[1] = Vzcon.Input[0];
   }
240
```

```
System.cpp Mark3 Flight Controller Code - Sensor Read
```

```
1 #include "Copter.h"
  void _Copter::InitSensor()
\mathbf{2}
3 {
      Wire.begin();
4
      Wire.setRate(I2C_RATE_2000);
5
      Wire1.begin();
6
      Wire1.setRate(I2C_RATE_2000);
7
8
9
       /gy86
      I2Cwrite(MPU6050_ADDRESS,
10
11
               MPUREG_PWR_MGMT_1, MPU_CLK_SEL_PLLGYROZ, 0);
      I2Cwrite(MPU6050_ADDRESS,
12
13
               MPUREG_SMPLRT_DIV, 0 \times 07, 0;
14
      I2Cwrite (MPU6050_ADDRESS
               MPUREG_CONFIG, BITS_DLPF_CFG_42HZ, 0);
15
      I2Cwrite(MPU6050_ADDRESS,
16
               MPUREG_GYRO_CONFIG, BITS_FS_1000DPS, 0);
17
18
      I2Cwrite(MPU6050_ADDRESS,
               MPUREG_ACCEL_CONFIG, 0 \times 08, 0;
19
      I2Cwrite(MPU6050_ADDRESS,
20
               MPUREG_INT_PIN_CFG, 0 \times 02, 0;
21
22
     I2CRead (MPU6050_ADDRESS,
23
              MPUREG_WHOAMI, 1);
24
      if (i2cData[0] != 0x68)
        Serial1.println("Error reading sensor");
25
26
      AccPointRead();
27 }
   void _Copter::AccPointRead()
^{28}
29
   {
30
      uint8_t point;
      for (point = 0; point < 6; point++)
31
32
      ł
        Acc_Cali.accel_raw_ref[point][0] =
33
          (\text{EEPROM. read}(100 + 6 * \text{point} + 2) \ll 8)
34
          | EEPROM. read (100 + 6 * point + 1);
35
36
        Acc_Cali.accel_raw_ref[point][1] =
          (\texttt{EEPROM.read}(100 + 6 * \texttt{point} + 4) << 8)
37
38
           | EEPROM.read (100 + 6 * point + 3);
39
        Acc_Cali.accel_raw_ref[point][2] =
          (\text{EEPROM. read}(100 + 6 * \text{ point} + 6) << 8)
40
41
          | EEPROM.read (100 + 6 * point + 5);
42
     }
43
      Acc_Cali.acc_offset[0] =
44
45
        (float)(Acc_Cali.accel_raw_ref[0][0] +
                 Acc_Cali.accel_raw_ref[1][0]) / 2.0;
46
      Acc_Cali.acc_offset[1] =
47
        (float)(Acc_Cali.accel_raw_ref[2][1] +
^{48}
49
                 Acc_Cali.accel_raw_ref[3][1]) / 2.0;
      Acc_Cali.acc_offset [2] =
50
```

```
51
        (float)(Acc_Cali.accel_raw_ref[4][2] +
                 Acc_Cali.accel_raw_ref [5][2]) / 2.0;
52
53
      for (point = 0; point < 3; point++)
54
55
        Acc_Cali.a[0][point] =
          (float)Acc_Cali.accel_raw_ref[0][point] -
56
57
          Acc_Cali.acc_offset [point];
      for (point = 0; point < 3; point++)
58
        Acc_Cali.a[1][point] =
59
          (float)Acc_Cali.accel_raw_ref[2][point] -
60
61
          Acc_Cali.acc_offset [point];
62
      for (point = 0; point < 3; point++)
        Acc_Cali.a[2][point] =
63
64
          (float)Acc_Cali.accel_raw_ref[4][point] -
          Acc_Cali.acc_offset [point];
65
66
    }
    void _Copter::MPU6050read()
67
68
    {
      I2CRead (MPU6050_ADDRESS, MPUREG_ACCEL_XOUT_H, 14);
69
70
      gy86.acc.origin.x = ((i2cData[0] \ll 8) | i2cData[1]);
71
      gy86.acc.origin.y = ((i2cData[2] << 8) | i2cData[3]);
      gy86.acc.origin.z = ((i2cData[4] << 8) | i2cData[5]);
72
      mpu\_temperature = (i2cData[6] \iff 8) | i2cData[7];
73
      gy86.gyro.origin.x = (i2cData[8] \ll 8) | i2cData[9];
74
      gy86.gyro.origin.y = ((i2cData[10] << 8) | i2cData[11]);
75
76
      gy86.gyro.origin.z = ((i2cData[12] \ll 8) | i2cData[13]);
      MPU6050ThermalCompensation();
77
      MPU6050Sixpoint();
78
79
   }
    void _Copter :: MPU6050Sixpoint()
80
81
    {
      gy86.acc.quietf.x = (float)gy86.acc.origin.x -
82
83
                            Acc_Cali.acc_offset [0];
84
      gy86.acc.quietf.y = (float)gy86.acc.origin.y -
                           Acc_Cali.acc_offset [1];
85
      gy86.acc.quietf.z = (float)gy86.acc.origin.z -
86
                            Acc_Cali.acc_offset [2];
87
88
      gy86.acc.aftcal.x = gy86.acc.quietf.x *
                                                  Acc_Cali.T[0][0] +
89
                           gy86.acc.quietf.y *
                                                  Acc_Cali.T[1][0] +
90
                           gy86.acc.quietf.z *
91
92
                            Acc_Cali.T[2][0];
                                                  Acc_Cali.T[0][1] +
      gy86.acc.aftcal.y = gy86.acc.quietf.x *
93
                           gy86.acc.quietf.y *
                                                  Acc_Cali.T[1][1] +
94
    gy86.acc.quietf.z *
95
                           Acc_Cali.T[2][1];
96
      gy86.acc.aftcal.z = gy86.acc.quietf.x *
                                                  Acc_Cali.T[0][2] +
97
                                                  Acc_Cali.T[1][2] +
98
                           gy86.acc.quietf.y *
                           gy86.acc.quietf.z *
99
                           Acc_Cali.T[2][2];
100
101
    }
    void _Copter::MPU6050ThermalCompensation()
102
103
   {
      float tp3, tp2, tp;//, accx, accy, accz;
104
105
      temperature = (float) mpu_temperature / 340.00 + 36.53;
106
      tp = temperature;
107
108
      if (tp > 55.0) tp = 55.0;
      if (tp < 22.5) tp = 22.5;
109
110
      tp2 = tp * tp;
111
      tp3 = tp2 * tp;
112
113
      /*-
                           -Thermal Calibration ----
      gy86.gyro.tempcp.x = 0.000263 * tp3 -
114
                            0.03098 * tp2 + 0.03939 * tp - 29.4;
115
```

```
116
      gy86.gyro.tempcp.y = -0.0004279 * tp3 +
                              0.05322 * tp2 - 2.941 * tp + 80.16;
117
      gy86.gyro.tempcp.z = 0.0004163 * tp3 -
118
                              0.0332 * tp2 + 0.6652 * tp + 23.3;
119
120
      gy86.gyro.aftcal.x = (float)gy86.gyro.origin.x -
121
122
                              gy86.gyro.tempcp.x;
      gy86.gyro.aftcal.y =
123
                              (float)gy86.gyro.origin.y -
124
                              gy86.gyro.tempcp.y;
125
      gy86.gyro.aftcal.z = (float)gy86.gyro.origin.z -
126
                              gy86.gyro.tempcp.z;
127
      if (flag.calibratedG == 0 && GyroCaliFlag <= 1500)
128
129
      {
        GyroCaliFlag++;
130
        MPU6050GyroCali();
131
132
      }
133
      if (flag.calibratedG == 1)
134
      ł
135
        gy86.gyro.aftcal.x = gy86.gyro.aftcal.x -
136
                                gy86.gyro.radian.x;
137
        gy86.gyro.aftcal.y = gy86.gyro.aftcal.y -
                                gy86.gyro.radian.y;
138
        gy86.gyro.aftcal.z = gy86.gyro.aftcal.z -
139
140
                                gy86.gyro.radian.z;
      }
141
142
   }
    void _Copter::MPU6050AccCali(uint8_t point)
143
144
    {
145
       /*Point = 0 \ 1 \ 2 \ 3 \ 4 \ 5*/
      if (Acc_Cali.acc_calitimer == 100)
146
147
      {
148
        Acc_Cali.accel_raw_ref[point][0] =
           Acc_Cali.acc_calitmpx / 100;
149
         Acc_Cali.accel_raw_ref[point][1] =
150
151
           Acc_Cali.acc_calitmpy / 100;
        Acc_Cali.accel_raw_ref[point][2] =
152
           Acc_Cali.acc_calitmpz / 100;
153
         Acc_Cali.acc_calitmpx = 0;
154
        Acc_Cali.acc_calitmpy = 0;
155
156
        Acc_Cali.acc_calitmpz = 0;
157
         Acc_Cali.acc_calitimer = 0;
        comorder = 0;
158
        Serial1.print (Acc_Cali.accel_raw_ref [point][0]);
159
160
        Serial1. print ( ' t ');
        Serial1.print(Acc_Cali.accel_raw_ref[point][1]);
161
        Serial1.print ( ' t ');
162
163
        Serial1.print(Acc_Cali.accel_raw_ref[point][2]);
        Serial1.print(' \setminus t');
164
        Serial1.println();
165
        EEPROM. write (100 + 6 * \text{ point} + 1),
166
                       Acc_Cali.accel_raw_ref[point][0] & 0b11111111);
167
        EEPROM. write (100 + 6 * \text{ point} + 2),
168
                       Acc_Cali.accel_raw_ref[point][0] >> 8);
169
        EEPROM. write (100 + 6 * \text{ point} + 3),
170
                       Acc_Cali.accel_raw_ref[point][1] & 0b11111111);
171
        EEPROM. write (100 + 6 * \text{ point} + 4)
172
                       Acc_Cali.accel_raw_ref[point][1] >> 8);
173
174
        EEPROM. write (100 + 6 * \text{ point} + 5),
                       Acc_Cali.accel_raw_ref[point][2] & 0b11111111);
175
        EEPROM. write (100 + 6 * \text{ point } + 6),
176
                       Acc_Cali.accel_raw_ref[point][2] >> 8);
177
178
      }
      else
179
180
      ł
        Acc_Cali.acc_calitmpx += gy86.acc.origin.x;
181
        Acc_Cali.acc_calitmpy += gy86.acc.origin.y;
182
```

```
183
        Acc_Cali.acc_calitmpz += gy86.acc.origin.z;
        Acc_Cali.acc_calitimer++;
184
185
      }
    }
186
187
    void _Copter::MPU6050GyroCali()
188
    {
      if (GyroCaliFlag > 400 && GyroCaliFlag < 1001)
189
190
      {
        GyroCollection[0] += gy86.gyro.aftcal.x;
191
        GyroCollection [1] += gy86.gyro.aftcal.y;
192
        GyroCollection [2] += gy86.gyro.aftcal.z;
193
194
      if (GyroCaliFlag == 1001)
195
196
      {
        gy86.gyro.radian.x = GyroCollection[0] / 600;
197
198
        gy86.gyro.radian.y = GyroCollection[1] / 600;
        gy86.gyro.radian.z = GyroCollection[2] / 600;
199
200
        Serial1.print(GyroCollection[0]); Serial1.print("\t");
        Serial1.print (GyroCollection [1]); Serial1.print ("\t");
201
        Serial1.print (GyroCollection [2]); Serial1.print ("\t");
202
        GyroCaliFlag = 0;
203
        GyroCollection[0] = 0;
204
205
        GyroCollection[1] = 0;
        GyroCollection[2] = 0;
206
207
        flag.calibratedG = 1;
        Serial1.println("Gyro Offset Calculated");
208
        Serial1.print(gy86.gyro.radian.x); Serial1.print("\t");
209
        Serial1.print(gy86.gyro.radian.y); Serial1.print("\t");
210
        Serial1.print(gy86.gyro.radian.z); Serial1.print("\t");
211
212
      }
213
    ł
214
                        -I2C-
    uint8_t _Copter:: I2Cwrite(uint8_t SENSOR_ADDRESS,
215
                                uint8_t SENSOR_REGISTER,
216
217
                                uint8_t SENSOR_VALUE,
218
                                bool sendStop)
219
    {
      Wire.beginTransmission(SENSOR_ADDRESS);
220
221
      Wire.write(SENSOR_REGISTER);
222
      Wire.write (SENSOR_VALUE); //DEVICE_RESET
      //Wire.endTransmission()
223
      uint8_t rcode = Wire.endTransmission(sendStop);
224
225
      if (rcode) {
        Serial1.print(F("i2cWrite failed: "));
226
227
        Serial1.println(rcode);
      }
228
229
      return rcode;
230
    }
    uint8_t _Copter::I2CRead(uint8_t SENSOR_ADDRESS, uint8_t
231
232
                               SENSOR_REGISTER, uint8_t nbytes)
233
    ł
      uint32_t timeOutTimer;
234
      Wire.beginTransmission(SENSOR_ADDRESS);
235
236
      Wire.write(SENSOR_REGISTER);
      uint8_t rcode = Wire.endTransmission(false);
237
      if (rcode) {
238
        Serial1.print(F("i2cRead failed: "));
239
240
        Serial1.println(rcode);
        return rcode:
241
242
        // See: http://arduino.cc/en/Reference/WireEndTransmission
243
      Wire.requestFrom(SENSOR_ADDRESS, nbytes, (uint8_t)true);
244
      for (uint8_t i = 0; i < nbytes; i++) {
245
        if (Wire.available())
246
          i2cData[i] = Wire.read();
247
```

```
else {
248
         timeOutTimer = micros();
249
         250
251
         if (Wire.available())
252
           i2cData[i] = Wire.read();
253
         else {
254
           Serial1.println(F("i2cRead timeout"));
return 5;
255
256
257
         }
258
       }
259
     }
     return 0; // Success
260
   }
261
```

Mark3 Flight Controller Code - Sensor Address Library

1	//GY86		
2	#define	MPU6050_ADDRESS	0x68
3	#define	MPUREG_WHOAMI	0 x75
4	#define	MPUREG_SMPLRT_DIV	0 x 1 9
5	#define	MPUREG_CONFIG	0x1A
6	#define	MPUREG_GYRO_CONFIG	0x1B
7	#define	MPUREG_ACCEL_CONFIG	$0 \mathrm{x1C}$
8	#define	MPUREG_FIFO_EN	0x23
9	#define	MPUREG_INT_PIN_CEG	0x37
10	#define	MPUREG_INT_ENABLE	0x38
11	#define	MPUREG_INT_STATUS	0x3A
12	#define	MPUREG_ACCEL_XOUT_H	0x3B
13	#define	MPUREG_ACCEL_XOUT_L	0x3C
14	#define	MPUREG_ACCEL_YOUT_H	0x3D
15	#define	MPUREG_ACCEL_YOUT_L	0x3E
16	#define	MPUREG_ACCEL_ZOUT_H	0x3F
17	#define	MPUREG_ACCEL_ZOUT_L	0×40
18	#define	MPUREG TEMP OUT H	0x41
19	#define	MPUREG TEMP OUT L	0×42
20	#define	MPUREG GYRO XOUT H	0×43
21	#define	MPUREG GYRO XOUT L	0x44
22	#define	MPUREG GYRO YOUT H	0x45
23	#define	MPUREG GYRO YOUT L	0x46
24	#define	MPUREG GYBO ZOUT H	0x47
25	#define	MPUREG GYBO ZOUT L	0x48
26	#define	MPUREG USER CTRL	0x6A
27	#define	MPUREG PWR MGMT 1	0x6B
28	#define	MPUREG PWR MGMT 2	0x6C
29	#define	MPUREG FIFO COUNTH	0×72
30	#define	MPUREG_FIFO_COUNTL	0×73
31	#define	MPUREG_FIFO_R_W	0x74
32	// Conf	iguration bits	
33	#define	BIT SLEEP	0×40
34	#define	BIT H RESET	0x80
35	#define	BITS CLKSEL	0×07
36	#define	MPU CLK SEL PLLGYBOX	0x01
37	#define	MPU CLK SEL PLLGYBOZ	0x03
38	#define	MPU EXT SYNC GYROX	0×02
39	#define	BITS_FS_250DPS	$0 \times 0 0$
40	#define	BITS_FS_500DPS	0x08
41	#define	BITS FS 1000DPS	0x10
42	#define	BITS FS 2000DPS	0x18
43	#define	BITS FS MASK	0x18
44	#define	BITS_DLPF_CFG_256HZ	0x00
45	//Defau	lt settings LPF 256Hz/	8000Hz sample
46	#define	BITS DLPF CFG 188HZ	0x01
47	#define	BITS_DLPF_CFG 98HZ	0×02
48	#define	BITS DLPF CFG 42HZ	0x03
49	#define	BITS_DLPF_CFG 20HZ	0×04
50	#define	BITS_DLPF_CFG 10HZ	0x05
51	#define	BITS_DLPF_CFG_5HZ	0x06

52 #define BITS_DLPF_CFG_2100HZ_NOLPF $0 \ge 07$ #define BITS_DLPF_CFG_MASK $0 \ge 07$ 53#define BIT_INT_ANYRD_2CLEAR $0 \ge 10$ 54#define BIT_RAW_RDY_EN 55 $0 \ge 01$ #define BIT_I2C_IF_DIS $0 \, \mathrm{x10}$ 56#define BIT_INT_STATUS_DATA 57 $0 \ge 01$ 5859//GY89 #define L3GD20_ADDRESS $(0 \times D6 >> 1)$ 60 #define L3G_WHO_AM_I $0 \ge 0$ 6162 #define L3G_CTRL_REG1 0x2063 #define L3G_CTRL_REG2 64 0×21 65#define L3G_CTRL_REG3 0x22#define L3G_CTRL_REG4 0x2366 #define L3G_CTRL_REG5 0x2467 $0 \, \mathrm{x} 25$ #define L3G_REFERENCE 68 69 #define L3G_OUT_TEMP 0x2670 #define L3G_STATUS_REG 0x2771 #define L3G_OUT_X_L 0x2872#define L3G_OUT_X_H 0x2973 74#define L3G_OUT_Y_L 0x2A #define L3G_OUT_Y_H 0x2B75#define L3G_OUT_Z_L 0x2C76 #define L3G_OUT_Z_H 0x2D77 78 79#define L3G_FIFO_CTRL_REG 0x2E #define L3G_FIFO_SRC_REG 80 0x2F81 #define L3G_INT1_CFG 82 0×30 83 #define L3G_INT1_SRC 0×31 #define L3G_INT1_THS_XH 0x3284 #define L3G_INT1_THS_XL 0x3385#define L3G_INT1_THS_YH 86 0×34 87 #define L3G_INT1_THS_YL 0x35#define L3G_INT1_THS_ZH 0x3688 #define L3G_INT1_THS_ZL 0x3789 #define L3G_INT1_DURATION 0x38 90 91 #define LSM303D_ADDRESS $0\,b\,00\,1\,1\,10\,1$ 92#define LSM303D_CTRL_REG0 0x1F93 #define LSM303D_CTRL_REG1 0x2094#define LSM303D_CTRL_REG2 0x2195 96 #define LSM303D_CTRL_REG3 0x22#define LSM303D_CTRL_REG4 0x2397 #define LSM303D_CTRL_REG5 0x2498 #define LSM303D_CTRL_REG6 0×25 99 100 #define LSM303D_CTRL_REG7 0x26101#define LSM303D_OUT_X_L_A 0x28102#define L3GD20_DEFAULT_FILTER_FREQ 30103 #define L3GD20_DEFAULT_RATE 400 104 105#define LSM303D_ACCEL_DEFAULT_RANGE_G 106 16#define LSM303D_ACCEL_DEFAULT_RATE 400107#define LSM303D_ACCEL_DEFAULT_ONCHIP_FILTER_FREQ 50108 $\# define LSM303D_ACCEL_DEFAULT_DRIVER_FILTER_FREQ$ 109 30

Mark3 Flight Controller Code - System Check

```
1 #include "Copter.h"
2 void _Copter::InitControl()
3 {
4     pvel.Kp = (EEPROM.read(11) << 8) | EEPROM.read(10); pvel.Kp /= 10000;
5     pvel.Ki = (EEPROM.read(13) << 8) | EEPROM.read(12); pvel.Ki /= 1000;
6     pvel.Kd = (EEPROM.read(15) << 8) | EEPROM.read(14); pvel.Kd /= 100000;
7     phiang.Kp = (EEPROM.read(17) << 8) | EEPROM.read(16); phiang.Kp /= 100;
8</pre>
```

```
9
     qvel.Kp = (EEPROM.read(19) \ll 8)
10
     EEPROM. read (18); qvel. Kp /= 10000;
     qvel.Ki = (EEPROM.read(21) \ll 8)
11
12
     EEPROM.read (20); qvel.Ki /= 1000;
     qvel.Kd = (EEPROM.read(23) \ll 8)
13
     EEPROM. read (22); qvel.Kd /= 100000;
14
     thetaang.Kp = (\text{EEPROM.read}(25) \ll 8)
15
     EEPROM.read (24); thetaang.Kp /= 100;
16
17
     rvel.Kp = (EEPROM.read(27) \ll 8)
18
19
     EEPROM. read (26); rvel. Kp /= 100000;
20
     rvel.Ki = (EEPROM.read(29) \ll 8)
21
     EEPROM. read (28); rvel. Ki /= 10000;
     rvel.Kd = (EEPROM.read(31) \ll 8)
22
^{23}
     EEPROM.read(30); rvel.Kd /= 1000000;
24
     psiang.Kp = (\text{EEPROM.read}(33) \ll 8)
     EEPROM.read(32); psiang.Kp /= 100;
25
26
     Zalt.Kp = (\text{EEPROM.read}(41) \ll 8)
27
^{28}
     EEPROM. read (40); Zalt.Kp /= 100;
     Vzalt.Kp = (EEPROM.read(43) \ll 8)
29
     EEPROM. read (42); Vzalt.Kp /= 100;
30
     Vzalt.Ki = (EEPROM.read(45) \ll 8)
31
     EEPROM. read (44); Vzalt. Ki /= 100;
32
     Vzalt.Kd = (EEPROM.read(47) \ll 8)
33
     EEPROM.read (46); Vzalt.Kd /= 100;
34
35
     Xpos.Kp = (EEPROM.read(51) \ll 8) |
36
37
     EEPROM.read (50); Xpos.Kp /= 1000;
38
     Vxpos.Kp = (EEPROM.read(53) \ll 8)
     EEPROM. read (52); Vxpos.Kp /= 1000;
39
40
     Vxpos.Ki = (EEPROM.read(55) \ll 8)
     EEPROM. read (54); Vxpos. Ki /= 1000;
41
     Vxpos.Kd = (EEPROM.read(57) \ll 8)
42
     EEPROM.read (56); Vxpos.Kd /= 1000;
43
44
     Ypos.Kp = (EEPROM.read(61) \ll 8)
45
46
     EEPROM.read (60); Ypos.Kp /= 1000;
     Vypos.Kp = (EEPROM.read(63) \ll 8)
47
48
     EEPROM. read (62); Vypos. Kp /= 1000;
49
     Vypos.Ki = (\text{EEPROM.read}(65) \ll 8)
     EEPROM.read (64); Vypos.Ki /= 1000;
50
     Vypos.Kd = (EEPROM.read(67) \ll 8)
51
52
     EEPROM. read (66); Vypos.Kd /= 1000;
53
     EstimatedG = (EEPROM.read(71) \ll 8)
54
     EEPROM.read (70); EstimatedG /= 1000;
55
56
     state.flight_state [0] = 1; //stand by
57
     state.flight_state [1] = 0; //take off
58
     state.flight_state [2] = 0; // flight
59
60
     state.flight_state [3] = 0; //land
61
     state.takeoff_t = 0;
     state.landing_t = 0;
62
63
   }
   void _Copter::Loop_Check()
64
65
   {
     xbee_length = 0;
66
67
     if (Ctrl_timer1 \ge 4)
        Ctrl_timer1 = 0; //-
                                    -Check 100Hz
68
69
     Moment_Check();
     Battery_Check();
70
     Timer_Check();
71
72
   }
   void _Copter::Otus_Clear()
73
```

```
74 {
      state.update_phi = 0;
75
      state.update_theta = 0;
76
77
      state.update_psi = 0;
78
      state.update_vx = 0;
      state.update_vy = 0;
79
      state.update_vz = 0;
80
81
      state.update_x = 0;
^{82}
      state.update_y = 0;
      state.update_z = 0;
83
    }
84
    void _Copter::Moment_Check()
85
86
    {
87
      float temp_gyro;
88
      if (comorder >= 1401 && comorder <= 1403)
      {
89
90
        if (inertia.timer_start == 0)
91
        {
92
           inertia.timer_start = 1;
           inertia.time_start = micros();
93
^{94}
        }
        inertia.time_end = micros();
95
96
        inertia.time_count = inertia.time_end - inertia.time_start;
97
        if (gy86.gyro.filter.z > 400 \&\& inertia.memo < -400)
98
99
        {
           inertia.memo = gy86.gyro.filter.z;
100
101
           inertia.pendulum ++;
102
        if (gy86.gyro.filter.z < -400 \&\& inertia.memo > 400)
103
104
        ł
          inertia.memo = gy86.gyro.filter.z;
105
106
        ł
         if (inertia.xbee_timer == 20)
107
108
        {
           Serial1.print(inertia.time_count); Serial1.print("
                                                                   ");
109
           Serial1.print(gy86.gyro.filter.z); Serial1.print("
                                                                   ");
110
           Serial1.print(inertia.memo); Serial1.print("");
111
112
           Serial1.println(inertia.pendulum);
           inertia.xbee_timer = 0;
113
114
        inertia.xbee_timer++;
115
116
      }
117
      else
118
      {
119
        inertia.timer_start = 0;
        inertia.time_count = 0;
120
121
        inertia.time_end = 0;
        inertia.time_start = 0;
122
        inertia.pendulum = 0;
123
124
         inertia.memo = -1000;
125
      }
126
    }
127
    void _Copter::Battery_Check()
128
    {
129
      //voltage = (float)analogRead(A14) * 0.019586; //only for quad 2
      voltage = (float) analogRead(A14) * 0.013841;
130
      voltageavg = voltage * 0.005 + voltageavg * 0.995;
131
      voltageavg = data_limitation(voltageavg, 9.0, 17.0);
132
133
      if (voltageavg < 10.5)
        battery_warning = 1;
134
      else
135
        battery_warning = 0;
136
137
   }
138
    void _Copter::Timer_Check()
139
    {
      if (gltimer == 150)
140
```

```
141
      {
         if (glch > 0)
142
143
         {
           digitalWrite(LED2, LOW);
144
           if (voltageavg < 10.5)
145
             digitalWrite(LED1, HIGH);
146
           else
147
             digitalWrite(LED1, LOW);
148
         }
149
         else
150
151
         {
           digitalWrite(LED2, HIGH);
152
         }
153
154
         glch *= -1;
         gltimer = 0;
155
156
      }
157
      else
         gltimer++;
158
      run_period = micros() - whole_timer;
159
      if (comorder = 2002)
160
161
         Serial1.println(run_period);
      if (run_period > MainLoopPeriod)
162
163
      {
         time_out = 1;
164
165
         Serial1.print(run_period);
         Serial1.println(" <<<<<tire out>>>>");
166
167
      loopClock2 = micros() - loopClock1;
168
      while (micros() - whole_timer < MainLoopPeriod);</pre>
169
      whole_timer = micros();
170
171
    }
172
    float _Copter::Rad(float angle)
173
174
    {
      return (angle * M_PI / 180.0);
175
176
    }
177
    float _Copter::Degree(float rad)
178
    {
      return (rad / M_PI * 180.0);
179
180
    }
    float _Copter::data_limitation(float a, float b, float c)
181
182
    {
      if (a < b) a = b;
183
184
      if (a > c) a = c;
      return a;
185
186
    }
187
    float _Copter::invSqrt(float number) {
188
189
      long i;
      float x2, y;
const float threehalfs = 1.5F;
190
191
192
      x2 = number * 0.5F;
193
      y = number;
194
195
      i
         = * ( long * ) \&y;
      i = 0x5f3759df - (i >> 1);
196
      y = * (float *) \& i;
197
      y = y * ( threehalfs - ( x2 * y * y ) );
198
199
      return y;
```

```
200 }
```

APPENDIX D

HARDWARE ASSEMBLY INSTRUCTIONS & SOFTWARE INITIALIZATION

D.1 Hardware Assembly Instructions

The instructions of assembling a 250mm quadrotor platform are provided. Items needed for assembling the MARK3 flight controller are listed in Table D.1.

Item	Quantity
Teensy 3.2 MCU	1
GY-89 Sensor Board	1
Xbee 3.0	1
LED-Blue	1
LED-Yellow	1
1N4001	1
3p 2.54mm Connector	2
2p 2.54mm Connector	4
5p 2.54mm Connector	3
6p Triple Row 2.54mm Connector	1
8p Triple Row 2.54mm Connector	1
8p Double Patch 2.54mm Connector	1
10p 2.00mm Connector	2
Resistor 2k	1
Resistor 10k	1
Resistor 300Ω	2
I2C Logic Converter 3.3v 5v	1
5V to 3.3V Step Down Voltage Regulator	1

Table D.1: Items Needed for Assembling the MARK3 flight controller

Items needed for assembling the 250mm quadrotor platform are listed in Table D.2.

Item	Quantity
MARK3 flight controller	1
DJI Snail Propulsion System	1
DJI 5045 Propeller	4
250mm ATG Carbon-Fiber Frame	1
11.1v 3s Lipo Battery 20c	1
Radiolink R9DS Receiver	1
HTC VIVE Tracker	1
Matek V3 UBEC	1

Table D.2: Items Needed for Assembling the 250mm quadrotor platform



Figure D.1: MARK3 Flight Controller Wiring Instruction

The flight controller wiring instruction is shown in Figure D.1 with the following steps:

1. Power Distribution Board & Battery Connection

Solder the MATEK V3 UBEC board with all four ESCs and battery XT60 male connector. Two sets of 2.54mm wires need to be soldered for connection of power supply and battery voltage read of the MARK3 flight controller.

2. ESC PWM Signal Wire Connection

All four ESCs should be powered by the 3s Lipo battery. All four pwm signal wires should be connected with PWM output pin header (the signal pin is on the Left and the ground pin is on the right) on the flight controller with certain sequence.

3. Receiver Signal Pin Connection

The MARK3 flight controller supports receivers based on S.BUS protocol (the working voltage is 3.3v). The receiver should be connected with the flight controller RX pin shown in the diagram.

D.2 Software Initialization

1. Accelerometer 6-point Calibration

Based on Chapter 6, the accelerometer requires 6-point Calibration. The following commands is required step by step:

1041

To perform +z calibration

1042

To perform -z calibration

1043

To perform +x calibration

1044

To perform -x calibration

1045

To perform +y calibration

1046

To perform -y calibration

2. Control Parameters Initialization

The control parameters are stored in EEPROM. For the first time use, all control parameters should be typed via serial monitor on arduino:

&1011_0950* //P Kp &1012_0000* //P Ki &1013_0405* //P Kd &1021_0976* //Q Kp &1022_0000* //Q Ki &1023_0414* //Q Kd &1031_1550* //R Kp &1032_000* //R Ki &1033_0900* //R Kd &1051_1000* //Phi Kp &1052_1000* //Theta Kp

```
&1053_420* //Psi Kp
&1071_270* //Z Kp
&1081_420* //Vz Kp
&1083_036* //Vz Kd
&1091_1250* //X Kp
&1092_0920* //Vx Kp
&1094_0038* //Vx Kd
&1095_1250* //Y Kp
&1096_0920* //Vy Kp
&1098_0038* //Vy Kd
&1100_7550* //G 7000
```

3. <u>Set up Connection for MATLAB based GUI</u> Both SteamVR client and the MATLAB GUI should be turned on (any other high computing cost process should be killed)

🛃 Mark3_GUI				- 🗆 🗙	
Х	Vx	Phi			
Position_x	Velocity_Vx	Attitude_Phi			
Y	Vy	Theta			
Position_y	Velocity_Vy	Attitude_Thet			
Z	Vz	Psi			
Position_z	Velocity_Vz	Attitude_Psi			
		Open UDP	Close UDP	Exit	
			vbee packet		
			Abee packet	Close Se	erial
				Open Se	rial
		¥		Show Da	ata
	ircle 2		and Data	□ Write Date	
			Παιδαία		a

Figure D.2: MARK3 Ground Station

The interface of MATLAB based GUI is shown in Figure D.2. Turn on the switch for UDP protocol. If the dynamic state value is shown, then turn on the switch for serial protocol. Fill the tick of sending data, then the quadrotor will receive the flight state value from HTC VIVE Tracking System and the command from mission planner (the current mission planner is based on simple circle drawing). By clicking the circle tick, the quadrotor will follow the circle or else it will follow the commands from the transmitter.