Article





Life Cycle Assessment of the New Generation GT-MHR Nuclear Power Plant

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Abstract: This study describes a life cycle assessment (LCA) of a fourth generation (4G) nuclear power plant. A high temperature helium cooled reactor and gas turbine technology with modular helium reactor (GT-MHR) is used in this study as an example. This is currently one the safest design of a nuclear power plant. The study also takes into account impact of accidents and incidents (AI) which happened around the world at nuclear power generation facilities. The adopted method for the study is a hybrid LCA analysis. The analysis of each phase of the life cycle was done on the basis of process chain analysis (PCA). Where detailed data were not available, the Input/Output (I/O) databases was employed. The obtained results show that greenhouse gases (GHG) emissions and energy intensity per unit of electricity production are relatively low. In fact, these are even lower than emissions from a number of renewable energy sources. The results show considerably different greenhouse gases (GHG) emissions and energy intensity per unit of electricity production when effects of AI are taken into account.

Keywords: energy generation; nuclear power plant; LCA; accidents and incidents (AI)

1. Introduction

The constructive utilisation of energy is of paramount importance for the enhancement of society's standard of living. The global demand for energy is growing even faster than the population. The escalating demand from developing countries will further exacerbate this situation. The current energy utilisation worldwide is about 14 TWh (1TWh = 10^{12} W·hour). By the end of the 21st century it may reach 50 TWh [1]. Today, approximately 80% of the world's energy comes from fossil fuels [2]. About 30% of the primary energy is used for electricity production. Most of the remaining 70% is used either for transportation or converted into hot water, steam and heat. Nuclear energy is now being used to produce about 14% of the world electricity [3]

Over the next 50 years, unless patterns change dramatically, energy production and use will contribute to global warming through large scale greenhouse gas emissions. This amounts to hundreds of billions of tonnes of carbon dioxide. Nuclear power could be one option for reducing carbon dioxide emissions. An interest in nuclear power, despite the Fukushima disaster, has been revived. More than 40 developing countries have approached United Nations officials to express interest in starting nuclear power programs [4].

A number of countries (France, Argentina, Brazil, Canada, Japan, the Republics of Korea, South Africa, the US, UK, Russia, China, etc.) joined together on a mission to develop and implement the next wave of safe nuclear reactors. They created the Generation IV International Forum (GIF) to oversee this development [5]. The GIF takes a top-down approach in choosing which designs are most promising versus the challenges of sustainability, safety, economics, proliferation resistance and

physical protection. The results of the efforts have been updated several times. The forum's members agreed to concentrate their efforts and funds on six reactor designs seeking to become commercially viable between 2015 and 2025 [6]. Among those reactors the very high temperature reactor (VHTR) is the most attractive nuclear technology. The Next Generation Nuclear Plant (NGNP) prototype concept is based on what is judged to be the lowest risk technology. That technology should achieve the needed commercial functional requirements to provide an economically competitive nuclear energy source [5]. The technology has the following substantial gains:

- (a) coupling of gas turbine with a high temperature gas-cooled reactor (HTGR) allows a net electrical efficiency in the range of 50% to be achieved;
- (b) building modular HTGR (usually called GT-MHR) results in lower capital cost due to plant simplification and time reduction for construction;
- (c) use of the ceramic TRISO (triple coated small balls) fuel specifically developed for this type of reactors. This fuel has a high degree of passive safety and flexibility to adopt uranium/plutonium, thorium (Th) based fuel cycle and reprocess spent nuclear fuel (SNF) from currently used reactors;
- (d) high burn-up of the reactor (between 80–120 GWd/ton (1 GWd = 10^9 W·day)). This substantially decreases radioactive waste from SNF and makes its SNF much less radioactive [7];
- (e) high temperature, which allows HTGR to be applied to hydrogen production. Due to this circumstance HTGRs may be also applied to other high and low temperature process heat applications such as water desalination. In this way non-electric energy needs may be efficiently addressed [8]. Some such reactors already have been built, for example HTR-PM, China (first operation expected in 2019) [9] and GTHTR300, Japan (planned to test in 2020). Few such reactors are working in the Russian Federation (RF) (GT-MHR is working from 2014, MHR-T for hydrogen production is working from 2017).

Unfortunately, the risk of AI for complex technological systems cannot be minimised to zero. Highly cited sociologist Charles Perrow in his book says: "Multiple and unexpected failures are built into society's complex and highly-coupled systems. Such accidents are unavoidable and cannot be designed around" [10]. The reasons for those AI may be not only human errors, but also adverse nature factors (tsunami, earth quakes, etc.) The environmental impacts of those AI can be substantial (e.g., Chernobyl, Fukushima) and also have a big social impact.

2. Purpose of the Study and Methodology

The overall objective of this study is to identify and analyse potential life cycle environmental impacts (GHG emissions, energy consumption) from the fourth-generation nuclear power plants. The evaluated impact also takes into account the impact from AI of the nuclear power plants and efforts required to eliminate the consequences of such AI based on available data. Only two stages of the nuclear power plants life cycle are taken into account in this study for evaluating environmental impact from AI, namely: electricity production and waste disposal (as the major contributors to the AI statistics). Unfortunately, the works done on mitigation of AI consequences are sparsely reported, however the costs of those works are broadly presented. Therefore, environmental impact from AI is assessed mostly using costs of those works.

The study uses also hybrid LCA, which is based on a mix of process LCA and input/output (I/O) LCA. Such an approach is an effective method for assessing environmental and other aspects associated with generation of electricity independently of its source over the whole life cycle—"from-cradle-to-grave". Such approach allows fill all data gaps, which sometimes occur in the processes based LCA. The study follows the LCA standard developed by the International Organisation for Standardisation (ISO 14040) as guidelines [11]. This standard is required to meet another standard—ISO 14044, which presents more detailed sub-standards and procedures [12]. Following these standards ensures a measure of accuracy and therefore credibility.

To compare results of this study with LCA studies of other sources of energy that might meet power requirements in the world in an objective manner we assume that power station will be built in Australia. Thus, whenever it's required the life cycle inventory (LCI) data are taken for Australian conditions.

3. Nuclear Power Generation Life Cycle.

3.1. Main Phases of Nuclear Power (NP) Cycles

The reference concept under consideration for this LCA study includes a helium-cooled, graphite moderated, thermal neutron spectrum reactor. The reactor outlet temperature will be in the range from 900 to 950 °C. The reactor core technology will be a prismatic block concept. The NGNP can produce both electricity and hydrogen using an indirect cycle. However, for this study only the production of electricity is taken into account.

The LCA study described here is based on the following phases of the nuclear power generation cycle:

- (a) power plant design and construction;
- (b) power plant operation,
- (c) spent fuel storage;
- (d) back end of the cycle involving decommissioning the power plant, land reclamation, final storage (repository) of high, medium and low-level radioactive wastes (HLW, MLW and LLW) disposal. The LCA study of nuclear power generation cycle is also based on a production capacity of 1 Giga Watts of electricity (1 GWe) during life time span of the power plant (average 60 years) and a load factor during life span of the power plant of between 80–90% (average 85%). Such values are commonly used in designs of HTGR (for example, [13,14]).

The system boundaries for this study comprehensively cover all aspects of the included phases taking into account impacts from materials used in the manufacture of equipment and spares (during operation and maintenance), construction of buildings and repositories.

It is clear that judgment for possible nuclear power generation should be based not only on environmental impacts (including others not considered here), but also on other issues such as economic and social impacts. A more comprehensive LCA study with some assessment of the economic and social impacts would provide a scientific basis for examining the suitability of using state of the art nuclear technology for power generation.

3.2. Main Phases of Nuclear Power (NP) Cycles

The scope of our material flow and energy analysis includes both direct and indirect material inputs. The scope for the energy requirements and emissions in this respect, however, is broader. It includes also the energy used for the production of materials used in the manufacture of capital equipment, energy used in the design phase of nuclear power plant construction, decommissioning and waste storage. Within the energy analysis for auxiliary materials which are used in relatively small quantities (i.e., solvents, balance of system (BOP) devices, joints, etc.) capital equipment was not taken into account. Figure 1 illustrates the definition of the system boundaries for the materials and energy analyses of the LCA study.

The functional unit for our LCA study for nuclear power was 1 Mega Watt hours of electricity (1MWhe). The power plant under consideration is capable to produce 26.8 PJ ($1PJ = 10^{15}$ J) of electrical energy per annum (average) during 60 years.

The scope of this study is limited due to omitting the following factors:

- (a) local infrastructure impacts and related road modifications;
- (b) some subsidiary materials due to a lack of available data, such as personal protective equipment, solvents used in cleanup, etc.

- (c) material production burdens for office equipment, moveable partitions, and furniture;
- (d) custodial and small replacement materials (e.g., light bulbs, window glass, air filters, cleaning supplies, etc.).

3.3. Major Assumptions

The LCA study of the nuclear power cycle is based on already developed technology for the HTGR for power generation. The main characteristics of the power generation system (average) adopted in the study are taken from [15–17] and presented in Table 1 (for comparison the main characteristics of the mostly popular pressurised water reactors (PWR) are also presented in Table 1, taken from our previous study [18]). This study assumes that existing technologies ("off-shelf" technologies) are used for all phases of the power generation cycle including reactors, fuel fabrication, energy conversion, power plant, designs, etc. As Europe is one of the most advanced and experienced places for nuclear power generation in the world we have assumed that all main equipment for nuclear reactors were made there (thus the consumptions and emissions for reactors equipment production based on European technologies).

All data related to the nuclear power (NP) cycle based on HTGR technology in terms of power capacity, weights, materials, production processes, etc., where necessary have been scaled up or down using parameters of known models of NP cycles.

Collection of primary data sets for the study was quite a difficult process (not uncommon) and collection of detailed data for the specific technologies in terms of power capacity, weights, materials, production processes, etc. has been based on many different sources. It is unavoidable that data have been scaled up and down, averaged, some estimations have had to be performed on the basis of economic models. Arising uncertainties have been evaluated using a "pedigree matrix" approach [19].

We assumed within the study that power plant has four standard modules with a capacity of 0.285GWe each (see Table 1), however overall capacity of the power plant has been scaled back to 1GWe for this study to be able to make comparison with other LCA studies of the NP cycle and our previous study [18].

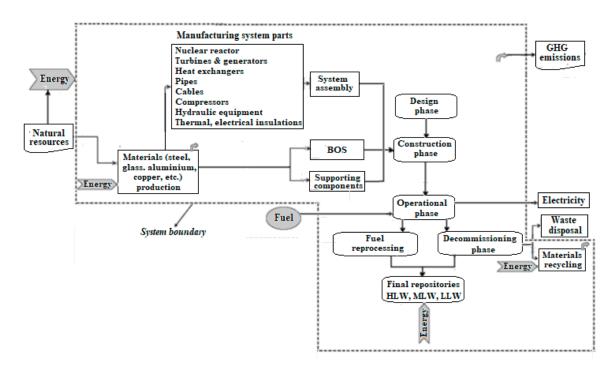


Figure 1. System boundary for the part of nuclear cycle under consideration.

Table 1. The main characteristics of high temperature gas-cooled reactor (HTGR) power generation system (the characteristics of currently most popular pressurised water reactor system are shown for comparison).

Feature/Parameter	Unit	Value	
reature/r arameter	Ollit	HTGR	PWR
Plant thermal power	GWth	2.4 [2.1]	3.12
Net power output	MWe	1140 [1000]	1000
Number of units per site	-	4 (600 MWth each)	1
Thermodynamic efficiency	%	47.5	32
Load factor	%	90	85
Plant life time	Years	60	40
Cycle Length	Months	18	18
Lifetime gross (net) electricity production	TWh	539.2 (534.1) [473.0 (469.5)]	297.8 (294.8)
Average burnup	GWd/tU	100	35
Average uranium enrichment	%	10.0	3.2
Total (per GWh) mass of enriched uranium	t (kg/GWh)	421.2 [369.5] (0.781)	413.6 (1.389)
SWU Demand (average)	10 ³ kg-SWU/GWY	221	135
Turbine type	-	Gas (Brayton cycle)	Steam (Rankine cycle)
Cooling/working primary (secondary) fluid	-	Helium (Nitrogen/ Helium mixture)	Water (Water)
Reactor safety system	-	No active emergency system	3–4 independent emergency systems

Figures in square brackets are adjusted for 1 GWe capacity.

The power conversion system (PCS) adopted in this study is based on a gas turbine, which allows the use of a more efficient thermodynamically cycle (gas turbines use the Bryton cycle with an efficiency of high temperature cycle up to 50% and above). The intermediate heat exchanger (IHX) is also used for the PCS system. Although the IHX increases the complexity of the plant, it creates the possibility of using part of the heat for other purposes rather than for electricity generation (for example, hydrogen production) and also increases the safety of the system, as the second circuit is completely detached from the reactor.

Data for materials production, energy requirements, and GHG emissions related to the materials production have been taken from the SimaPro databases [20] for European conditions or using Australian conditions when those materials originated in Australia taking into account all necessary transportation.

Within the use phase of the nuclear power plant we assumed that the spent fuel will be stored as a solid material in spent fuel casks within a specifically designed building (such a scenario is used in currently designed HTGR power plants, for example, [15]). The spent fuel is being sent later to a reprocessing plant to Europe (for example, [21]) or to final repository depending upon the adopted scenario.

We also assumed within the study that all parts of the power plant except nuclear heat generation and conversion are similar to conventional power plant based on same technology (i.e., gas turbine power plant) with the same electrical capacity. Manufacturing of balance of plant (BOP) components such as heat exchangers, compressors, pipeline, valves, etc. and their accessories are also included in the LCA boundary (see Figure 1) and they are similar to conventional power plants, as well.

At the end of the power plant's lifetime it will be decommissioned and an environmental remediation programme will be conducted, and the resulting waste will be disposed of in a responsible way. As this event can occur at least 60 years after the power plant begins operating, we assumed that the recycling rates for the major material will be at least similar to current recycling rates. Therefore 30% of construction materials, 50% of steels and 80% of copper, aluminium and glass will be recycled.

Because it is hard to obtain any data on the recycling of auxiliary materials, we did not consider their recycling in our study.

The transportation of all necessary components to the construction site of the power plant and transportation of fuel and fuel reprocessing, as well as, final repository at the end of the system life have been also taken into account. The typical transport distances estimated for the nuclear power cycle phases under consideration are: (a) the manufacturing of main equipment and fuel (in Europe), (b) construction materials mainly produced locally. We also assumed that the power plant will be located near sea water to allow access for cooling (although this type of NP plant does need cooling water, it can be useful to supply heat for a desalination or hydrogen production plant) and integrated into the electricity grid. The transport distances for the phases in the nuclear power cycle are summarised in Table 2. The processes under consideration in the LCA study of the nuclear power cycle are shown in Figure 2.

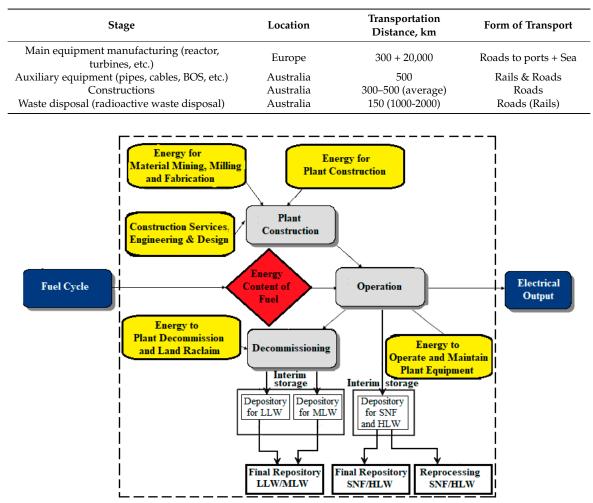


Table 2. Transport distances adopted by the study.

Figure 2. Processes for the nuclear power generation cycle adopted for this part of the study (The processes outside of dashed lines are out of scope of the study).

All statistics for power generation by nuclear power plants and occurred AI are taken from 1965 up to the year 2012, when the nuclear power generation became a mature technology and reliable statistics on mitigation works exists. Data on AI of nuclear power generation plants and nuclear waste disposals in the world are presented in Table 3, which are extraction of data presented in [22,23]. The reported fatalities from the accidents were treated as reduction of the average population life span for the country where disaster has occurred. However, data on fatalities from nuclear power plants

accidents are low [22] and have a negligible effect on human health of the whole population of the country in comparison, for example, with GHG emissions. Therefore, those data are not presented in LCA results of the study. Based on published data for the price of carbon dioxide abatement process (US\$65 per 1 tonne of CO_2) [24], the costs of the works done on mitigation of AI have been converted back to the GHG impact. The energy consumed for such works are estimated based on data from [25]: 5.86 MJ per 1 kg of CO_2 .

Date (Day/Month/Year)	Location	Description	Dead	Cost (\$US Mln)	INES Level
05/10/1966	Michigan, USA	Partial core meltdown at the Enrico Fermi Nuclear Generating Station	0	132	
21/01/1969	Vaud, Switzerland	Loss-of-coolant accident, leading to a partial core meltdown	0		5
06/02/1975 and 15/03/1992	Leningrad Oblast, Russia	Partial nuclear meltdown in reactor unit. Leaked radioactive gases.	3	1500	
07/12/1975	Greifswald, Germany	Electrical error causes fire five main coolant pumps	0	443	3
05/01/1976 and 22/02/1977	Bohunice, Slovakia	Corrosion of reactor and release of radioactivity	2	1700	4
28/03/1979	Pennsylvania, USA	Loss of coolant and partial core meltdown.	0	2400	5
15/09/1984	Alabama, USA	Safety violations, operator error.	0	110	
09/03/1985	Alabama, USA	Systems malfunction during start-up	0	1830	
11/04/1986	Massachusetts, USA	Recurring equipment problems.	0	1001	
26/04/1986	Chernobyl, Ukraine	Overheating, steam explosion.	61	6700	7
04/05/1986	Hamm-Uentrop, Germany	Experimental THTR-300 reactor releases small amounts of fission products.	0	267	
31/03/1987	Pennsylvania, USA	Peach Bottom units 2 and 3 shutdown due to cooling malfunctions.	0	400	
19/12/1987	New York, USA	Malfunctions, force to shut down Nine Mile Point Unit 1	0	150	
17/03/1989	Maryland, USA	Inspections at reveal cracks at pressurized heater sleeves	0	120	
20/02/1996	Connecticut, USA	Leaking valve, multiple equipment failures.	0	254	
02/09/1996	Florida, USA	Balance-of-plant equipment malfunction	0	384	
30/09/1999	Ibaraki, Japan	Radiation levels above permissible limits.	2	54	4
16/02/2002	Ohio, USA	Severe corrosion of control rod	0	143	3
09/08/2004	Fukui, Japan	Steam explosion	4	9	1
25/07/2006	Forsmark, Sweden	An electrical fault	0	100	2
11/03/2011	Fukushima, Japan	A tsunami flooded and damaged the plant's 5 active reactors.	2	187,000	7
12/09/2011	Marcoule, France	The explosion took place in a furnace used to melt metallic waste.	1	10	1
	Wa	aste Disposal Accidents and Incidents			
15/05/1988	Cádiz, Spain	Radioactive contamination in scrap metal processing plant by a caesium-137 (up to 1000 times higher than normal)	0	132	
From 1951 up to 2016	Lake Karachay, Cheliabinsk Oblast, Russia	The lake accumulated about 4.44 exabecquerels (EBq) of radioactivity, including 3.6 EBq of caesium-137and 0.74 EBq of strontium-90.	0	263	

Table 3. Main Nuclear power plant and radioactive waste disposal accidents and incidents (with multiple fatalities and/or more than US\$10 million in damage, 1965–2011) [22,23].

Date (Day/Month/Year)	Location	Description	Dead	Cost (\$US Mln)	INES Level
From 1980 up to 2000	Somalia	A criminal organisation from Calabria (Italy) has been involved in radioactive waste dumping	0	0.26	
Start 1949 up to now	River "Techa", Cheliabinsk Oblast, Russia	The Mayak complex dumped radioactive waste water, a cumulative dispersal of 102 Petabecquerel (PBq) of radioactivity.	21	6	

Table 3. Cont.

0 Data which have not been presented in this table at the referred source are taken from other sources on Wikipedia.

4. Results and Discussion

The amount of major required materials and produced waste for the whole life cycle of the GT-MHR power plant under consideration is presented in Table 4. (The amount of HLW presented is based on the once throughout cycle without reprocessing).

The results obtained for the primary energy consumption and GHG emissions during the LCA study are shown in Table 4. Based on the presented results the calculated GHG emissions per 1 MWhe produced are—6.42 kg of CO₂ eq. and 6.72 kg of CO₂ eq. with and without figures for recycling, respectively. To obtain values for the whole nuclear power cycle, the values for the front-end, i.e., ore mining, enrichment, fuel fabrication and delivery have to be added, as well as for any fuel reprocessing). The GHG footprint of the front-end (uranium mining and enrichment) was estimated previously [18] as 3.15 kg of CO₂ eq./MWhe (10% U-235) with gas centrifuge enrichment technology. Thus, the overall GHG footprint of the NP cycle is 9.57 kg of CO₂ eq./MWhe and 9.87 kg of CO₂ eq./MWhe, respectively.

The impact of AI during power generation and waste disposal are calculated for this study based on table for AI relevant to electricity production [22] and radioactive waste disposal from nuclear power plants [23].

Table 4. Main materials used	during life cycle of GT-MHR	power plant (1GWe capacity).

Required Main Materials	Amount (t)
Concrete	440,000
Iron and Steel	132,000
Other metals	10,000
Uranium (10% enriched)	369.5
Plastics	3000
Other materials	53,000
Main Waste Streams	Amount (t)
LLW	18,600
MLW	11,300
HLW	2930
Inert waste	460,000
Recyclable waste	146,000

The costs for the LLW repository and MLW/HLW geological repository are based on averaged figures presented in [26], the cost of landfill disposal is taken from [27]; prices for recycling materials are based on data from different sources: metals from London Metal Exchange (LME) and concrete and glass are based on current market prices in Australia.

The results obtained for primary energy consumption and GHG emission through whole life cycle of NP plant (Table 5) have been used to calculate energy and GHG payback time based on a methodology developed in [28]. The calculated energy payback time for the NP plant under consideration is:

$$PBT_E = \frac{E_C \times p}{(E_P - E_L) \times k/t} = \frac{35,511 \times 0.33}{(473.0 - 3.5) \times 3600/60} = 1.26 \text{ (year)}$$
(1)

where, *Ec*—is total energy consumption through the whole life cycle of the NP plant (Table 5); p = 0.33—is adopted within the study as the efficiency of converting primary energy to electricity; E_p and *t*—are total energy production by the plant and its life time (Table 1); E_L —is parasitic electric load (the energy consumed by the plant for its own needs); k = 3600—is coefficient for converting TWh to TJ. The calculated GHG payback time is:

$$PBT_{GHG} = \frac{T_{GHG}/c}{(E_P - E_L) \times k/t} = \frac{(3018.57 \times 10^3)/262}{(473.0 - 3.5) \times 3600/60} = 0.41 \text{ (year)}$$
(2)

where T_{GHG} —is total GHG emissions through the whole life cycle of the NP plant; *c*—is the GHG average emissions per 1GJ of produced electricity in Australia (*c* = 262 t of CO₂ eq. per 1TJ [20]).

The energy and GHG payback time including data for AI calculated using Equations (1) and (2), are, respectively: $PBT_{E(AI)} = 2.69$ year; $PBT_{GHG(AI)} = 1.32$ year.

The contribution to the price of the unit of energy produced by the GT-MHR plant has also been calculated from data presented in Table 5 for the LCA cost of the NP plant life cycle, which is approximately 0.95 c/kWh (1.05 c/kWh including AI) for electrical energy in 2010 US dollars.

The obtained results of our study are in broad agreement with the majority of results of other reports and publications dealing with this subject (although there are some others which are contradictory to our results, e.g., [29]). A comparison of the results for GHG emissions per unit of electrical energy are shown in Figure 3.

Some reviews of the studies on the topic are done in [30], where results of GHG emissions from LCA studies for different energy production technologies are provided. This work presents life-cycle mostly emissions for current power generation technologies, although some estimation of GHG emissions for advanced and future technologies are also provided. Only original studies have been used to ensure that all data can be traced back to the original references. The LCA studies and reports used were published between 2000 and 2006. Figure 4 presents a summary of the surveyed results (it should be noted that figure shown for this study presents result using the following scenario: (a) at the front-end: only primary fuel (no reprocessed fuel) is used based on 10% U-235 enrichment with 100% centrifuge technology; (b) NP plant cycle and back-end is based on the results obtained in this report).

	LCA Phase	Cost (M\$)	Energy Consumption (TJ)	GHG Emissions $(10^3 \text{ t CO}_2 \text{ eq.})$
	Engineering & Design	115.5	381.3	60.17
	Equipment fabrication	1163.2	15014.2	1503.42
Pre-use	Construction materials	286.2	3697.1	239.08
	Non-process equipment	69.3	553.5	45.87
	Construction works	462.8	356.7	74.74
Use	Use	1452	9422.0	739.00
Post-use	Decommissioning (decontamination & demolition works)	342.4	1638.7	106.43
T T XA7 - 1 1	LLW waste site construction and maintenance	31.70		72.70
LLW disposal	Drums &Cement	66.9	1375.6	
	Transportation	3.8		
MLW/HLW disposal	Geological repository: construction & maintenance	375.3		290.42
	TAD and drums	89.3	4803	
*	Transportation	9.9		
Non-radioactive	Landfill disposal	13.8	13.3	0.73
waste disposal	Transportation	11	346	23.37

Table 5. Economic cost, energy consumption and greenhouse gas (GHG) emissions from the whole life cycle of HTGR power plant (1 GWe capacity).

LCA Phase		Cost (M\$)	Energy Consumption (TJ)	GHG Emissions (10 ³ t CO ₂ eq.)
	Concrete	1.5	149	17.9
	Carbon Steel	9.6	614.4	26.88
Recycling credits	Stainless Steel	12	209.4	14.36
	Copper	6.4	211.5	18.43
	Aluminium	7.7	878.4	58.51
	Glass	0.03	27.6	1.28
Total (without recycling)		4493.1	37,601.4	3155.93
Total (including recycling)		4455.87	35,511.1	3018.57
Additions (due to accidents and incidents)		447.58	40,351.0	6686.00

Table 5. Cont.

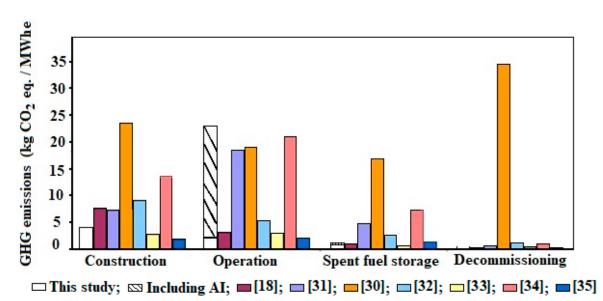


Figure 3. Comparison results for GHG emissions per unit of electrical energy production from different studies of nuclear power (NP) plant cycle: [18,30–35] and this study.

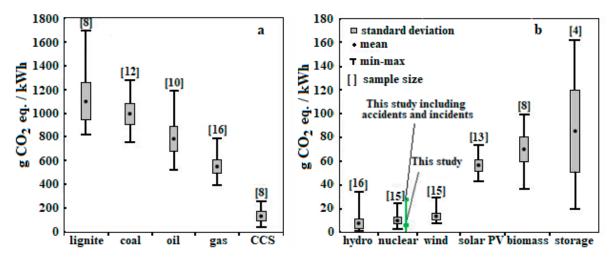


Figure 4. Results of life cycle GHG emissions from surveyed studies [32]. (a) fossil fuels; (b) renewables).

5. Conclusions

Australian energy demands, which are largely met by fossil fuel, keep growing along with associated greenhouse gas emissions. Electricity production from nuclear power could potentially be part of the solution to reduce these greenhouse gas emissions. The purpose of this LCA study was to evaluate the likely effect of the new reactor technology (HTGR) for the greenhouse gas footprint of nuclear power.

The GT-MHR design offers several advantageous performance characteristics. These include:

- **High Plant Efficiency**—Use of the Brayton Cycle helium gas turbine in the GT-MHR provides electric generating capacity at a net plant efficiency of 47.5%. The high plant efficiency reduces power generation costs, thermal discharge to the environment and high-level waste generation per unit electricity produced.
- **Superior High-Level Waste Form**—Coated particle fuel (TRISO) provides a superior spent fuel waste form for both long-term interim storage and permanent geologic disposal. As such, they provide defense-in-depth to ensure that the spent fuel radionuclides are contained for geologic time frames and do not migrate to the biosphere.
- Low Carbon Impact—The GT-MHR has very low GHG emissions per unit of electricity production of about 6.5 g CO₂ eq./kWh for the GT-MHR NP plant life cycle. With all fuel enrichment by gas centrifuge technology in combination with the GT-MHR, the overall GHG footprint of nuclear was estimated to be: -9.6 g CO₂ eq./kWh.

Included in LCA study environmental impact (in terms of GHG emissions and energy requirements) based on available statistics of AI from nuclear power generation. It shows that although cost of power generation should be increased by about 10%, although, energy requirement is doubled and GHG emissions even tripled to about 30 g CO_2 eq./kWh. However, even these figures are relatively small in comparison with current energy generation technologies (Figure 4). Thus, nuclear technology remains attractive in that respect, even taking into account data on AI happened so far.

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Abbreviations

Fourth generation
Accidents and Incidents
Balance of plant
Carbon dioxide
Greenhouse gases
Generation IV International Forum
Gas-turbine modular helium reactor
Giga Watt*days/ton
High level radioactive waste
High temperature gas-cooled reactor
The name of a small modular nuclear reactor developed in China
Input/Output
Intermediate heat exchanger

ISO	International Organisation for Standardisation
LCA	Life cycle assessment
LCI	Life cycle inventory
LLW	Low level radioactive waste
LME	London Metal Exchange
MLW	Medium level radioactive waste
MWhe	Mega Watt (10 ⁹ Watt)*hours (electricity)
NGNP	Next Generation Nuclear Plant
NP	Nuclear power
РВТ	Pay back time
PCA	Process chain analysis
PCS	Power conversion system
PWR	Pressurised water reactor
SNF	Spent nuclear fuel
SWU/GWY	Separative work unit (the amount of separation done by an enrichment process)/Giga
3WU/GW1	Watt*year
TRISO	The ceramic fuel: -triple coated small balls
TW	Terra Watt = 10^{12} Watt
VHTR	Very high temperature reactor

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