

Mesoscopic model for soft flowing systems with tunable viscosity ratioLinlin Fei,^{1,2} Andrea Scagliarini,² Andrea Montessori,^{2,3} Marco Lauricella,² Sauro Succi,^{2,4,5}
and Kai H. Luo^{1,6,*}¹*Center for Combustion Energy, Key Laboratory for Thermal Science and Power Engineering of Ministry of Education, Department of Energy and Power Engineering, Tsinghua University, Beijing 100084, China*²*Istituto per le Applicazioni del Calcolo, Consiglio Nazionale delle Ricerche,
Via dei Taurini 19, 00185 Rome, Italy*³*Department of Engineering, University of Rome "Roma Tre," Via della Vasca Navale 79, 00141 Rome, Italy*⁴*Center for Life Nano Science at La Sapienza, Istituto Italiano di Tecnologia,
viale Regina Elena 295, I/00161 Rome, Italy*⁵*Harvard Institute for Applied Computational Science, Cambridge, Massachusetts 02138, USA*⁶*Department of Mechanical Engineering, University College London, Torrington Place,
London WC1E 7JE, United Kingdom*

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We propose a mesoscopic model of binary fluid mixtures with tunable viscosity ratio based on a two-range pseudopotential lattice Boltzmann method, for the simulation of soft flowing systems. In addition to the short-range repulsive interaction between species in the classical single-range model, a competing mechanism between the short-range attractive and midrange repulsive interactions is imposed within each species. Besides extending the range of attainable surface tension as compared with the single-range model, the proposed scheme is also shown to achieve a positive disjoining pressure, independently of the viscosity ratio. The latter property is crucial for many microfluidic applications involving a collection of disperse droplets with a different viscosity from that of the continuum phase. As a preliminary application, the relative effective viscosity of a pressure-driven emulsion in a planar channel is computed.

DOI: [10.1103/PhysRevFluids.3.104304](https://doi.org/10.1103/PhysRevFluids.3.104304)**I. INTRODUCTION**

Soft flowing systems, such as emulsions, foams, colloidal glasses, among others, are ubiquitous in nature and engineering, and a better understanding of their rheology is crucial to the advancement of many fields of science and technology [1–8]. Usually, soft flowing systems show very complex rheology, such as anomalous enhanced viscosity, structural and dynamical arrest, aging under moderate shear, etc., whose precise and quantitative description requires major extensions of nonequilibrium statistical mechanics [1,9]. These complex phenomena portray a complicated scenario, which is quite challenging even for the most advanced computational methods based on the solution of the Navier-Stokes (N-S) equations for nonideal fluids. First, tracking the time evolution of complex interfaces between species and phases presents a serious hurdle for the macroscopic methods. Moreover, these methods are based on the continuum assumption, which makes it very challenging to capture the fundamental physics at micro- and mesoscales [10].

During the last three decades, a number of mesoscale methods based on kinetic theory have been developed [11,12]. Among them, the lattice Boltzmann method (LBM) has achieved remarkable

*K.Luo@ucl.ac.uk

successes for the simulation of complex flowing systems [11,13–21]. In LBM simulations, the fluid is usually represented by populations of fictitious particles colliding locally and streaming to adjacent nodes along the links of a regular lattice. The scale-bridging nature of LBM allows its natural incorporation of microscopic and/or mesoscopic physics, while the efficient collision-streaming algorithm makes it computationally appealing [10,13,19]. Among the existing LB models for multiphase and multicomponent systems, a very popular and widely used scheme is the pseudopotential model, originally proposed by Shan and Chen (S-C) [15]. In the original pseudopotential model (also named the S-C model), the interactions between populations of molecules are modeled by a pseudointeraction between the fictitious particles based on a density-dependent pseudopotential, and the phase separation is achieved through a short-range interaction between the two fluid phases (liquid-gas in the case of multiphase single-component systems, and liquid-liquid for mixture of immiscible fluids, as in the present case). A two-range pseudopotential LBM has been proposed [22] that was proved able to simulate flowing soft-glassy materials [23,24], through the competition between the standard S-C short-range interaction and an added mid-range interaction. This method has obtained success in reproducing many features of the physics of these systems, such as structural frustration, aging, elastoplastic rheology, in confined and unbounded flows of microemulsions [25–28].

However, the two-range mesoscopic LBM suffers from the problem of a spurious viscosity dependence in the pressure tensor, due to the discrete lattice effects introduced by the velocity shift forcing scheme [23,24]. As analyzed by Benzi *et al.* [24], the kinetic part of the pressure tensor includes τ -dependent terms [see Eq. (12) therein], which means that the surface tension and equilibrium densities for the components in the model depend on the viscosities of the fluid components. In addition, the model usually suffers numerical instabilities for multicomponent flows with different viscosities. Guo *et al.* argued that the discrete lattice effects must be considered in the introduction of the force field into LBM, and they proposed an alternative representation of the forcing term [29]. In this work, we propose a merger between these two techniques, which proves capable of achieving a new scheme with (1) tunable surface tension over a sizable range of values, (2) a positive disjoining pressure, and (3) no spurious dependence on the fluid viscosity. The new scheme is then used to compute the relative effective viscosity of pressure-driven emulsions in a planar flow at nonunit viscosity ratios.

The remainder of this paper is structured as follows. In Sec. II we present the proposed two-range pseudopotential model in detail. Section III gives extensive numerical experiments that validate and highlight the most salient features of the model, including an application to pressure-driven emulsions in a planar flow with different dynamic viscosities. Finally, concluding remarks are given in Sec. IV.

II. TWO-RANGE PSEUDOPOTENTIAL LATTICE BOLTZMANN MODEL WITH TUNABLE VISCOSITY RATIO

A. Forcing scheme

In the two-range pseudopotential model for complex flows, the motion of the fluid is represented by a set of populations of fictitious particles (distribution functions) $f_{k,i}(\mathbf{x}, t)$ at position \mathbf{x} and time t , where the subscripts k and i denote fluid component and discrete velocity direction, respectively. In this paper, two-dimensional flow problems are considered and the D2Q9 lattice $\mathbf{e}_i = [|e_{ix}\rangle, |e_{iy}\rangle]$ ($i = 0, 1, \dots, 8$; see Fig. 1) is used. The lattice speed $c = \Delta x / \Delta t = 1$ and the lattice sound speed $c_s = 1/\sqrt{3}$ are adopted, in which Δx and Δt are the lattice spacing and time step. The evolution equation for the distribution functions (DFs) is given by

$$f_{k,i}(\mathbf{x} + \mathbf{e}_i \Delta t, t + \Delta t) - f_{k,i}(\mathbf{x}, t) = -\frac{\Delta t}{\tau_k} [f_{k,i}(\mathbf{x}, t) - f_{k,i}^{eq}(\rho_k, \mathbf{u}^{eq})] + \Delta t C_{k,i}, \quad (1)$$

where τ_k is the relaxation time for each component which is related to the kinematic viscosity by $\nu_k = (\tau_k - 0.5\Delta t)c_s^2$, and $C_{k,i}$ is the forcing term by which a force field \mathbf{F}_k is incorporated into

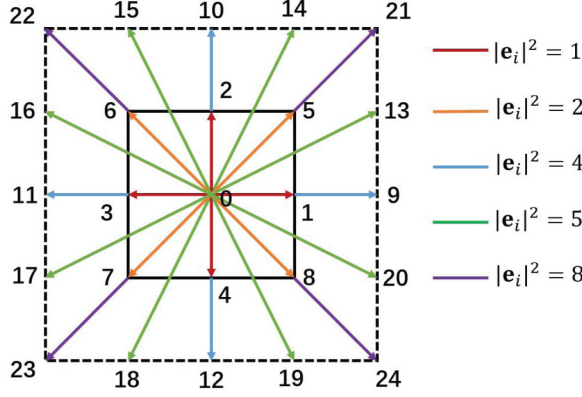


FIG. 1. The discrete lattice used in this work. The fluid lives in the D2Q9 lattice, while the interactions extend to the full D2Q25.

Eq. (1). The local equilibrium distribution function (EDF) is usually given by a low-Mach-number truncation form as

$$f_{k,i}^{eq}(\rho_k, \mathbf{u}^{eq}) = w(|\mathbf{e}_i|^2) \rho_k \left[1 + \frac{\mathbf{u}^{eq} \cdot \mathbf{e}_i}{c_s^2} + \frac{\mathbf{u}^{eq} \mathbf{u}^{eq} : (\mathbf{e}_i \mathbf{e}_i - c_s^2 \mathbf{I})}{c_s^4} \right], \quad (2)$$

where ρ_k is the density for each component, the weights are $w(0) = 4/9$, $w(1) = 1/9$, and $w(2) = 1/36$, and \mathbf{u}^{eq} is an effective velocity. To conserve the total momentum of particles of all components in the absence of interparticle forces, the effective velocity must be given as [30]

$$\mathbf{u}^{eq} = \frac{\sum_k \frac{\rho_k \mathbf{u}_k}{\tau_k}}{\sum_k \frac{\rho_k}{\tau_k}}, \quad (3)$$

where $\rho_k \mathbf{u}_k$ is the k th component momentum. In the original formulation proposed by Shan *et al.* [15,31] and the recent two-range model [23–26], the force field is implemented via a shift of the velocity in the EDF of each component, while the forcing term $C_{k,i}$ is not written explicitly. Using the general form in Eq. (1), it can be shown that the velocity-shift method corresponds to an explicit forcing term [32]:

$$C_{k,i}^{SC} = \frac{1}{\tau_k} [f_{k,i}^{eq}(\rho_k, \mathbf{u}^{eq} + \mathbf{F}_k \tau_k / \rho_k) - f_{k,i}^{eq}(\rho_k, \mathbf{u}^{eq})]. \quad (4)$$

In addition, the component momentum in the original S-C model is calculated as $\rho_k \mathbf{u}_k = \sum_i f_{k,i} \mathbf{e}_i$, which is independent of the forcing field. The velocity-shift method can be regarded as a first-order approach (in time), because the change in the momentum due to the force field is calculated using the first-order numerical integration. As shown by different researchers [24,32–34], some additional viscosity-dependent terms (related to the viscous stress tensor) are recovered in the macroscopic equations by the velocity shift method, while the method by Guo *et al.* [29] eliminates this effect by introducing extra compensating terms. It may be noted that the method by Guo *et al.* is not the only way to accurately incorporate the force field into the lattice Boltzmann equation. It is also possible to construct a forcing scheme using the second-order trapezoidal integration of the change of the distribution due to the force field [35,36]. On the other hand, it has been shown recently that a forcing scheme can be constructed based on the second-order time-splitting scheme [37,38], where the changes in the momentum due to the force field, obtained via integration using a second-order Crank-Nicholson scheme, are introduced by means of two half forcing time steps around the collision step. More information on the recent discussions about the forcing schemes can be found in Refs. [39–42] and references therein.

In the present work we adopt the methodology of Guo *et al.*, and the forcing term in Eq. (1) is given by

$$C_{k,i}^{Guo} = \left(1 - \frac{\Delta t}{2\tau_k}\right) w(|\mathbf{e}_i|^2) \left[\frac{\mathbf{e}_i - \mathbf{u}^{eq}}{c_s^2} + \frac{(\mathbf{e}_i \cdot \mathbf{u}^{eq})}{c_s^4} \mathbf{e}_i \right] \cdot \mathbf{F}_k. \quad (5)$$

In the forcing term, the velocity is the same as the effective velocity in the EDF, as suggested by Guo *et al.*, while the density and momentum for the k th component are calculated as

$$\rho_k = \sum_{i=0}^8 f_{k,i}, \quad \rho_k \mathbf{u}_k = \sum_{i=0}^8 f_{k,i} \mathbf{e}_i + \Delta t \mathbf{F}_k / 2. \quad (6)$$

The barycentric velocity of the fluid mixture is

$$\mathbf{u} = \sum_k \rho_k \mathbf{u}_k / \rho, \quad (7)$$

where the total density is $\rho = \sum_k \rho_k$. It is seen that the barycentric velocity is not equal to \mathbf{u}^{eq} unless all the components have the same viscosity. In the original method proposed by Guo *et al.* [29] where the single-component flow is considered, the actual fluid velocity, the velocity in the forcing term and the velocity in the EDF coincide. We wish to point out that, by replacing \mathbf{u}^{eq} in Eqs. (2) and (5) by \mathbf{u} , unphysical deformation of a dispersed droplet is observed unless a unity viscosity ratio is used.

B. Competing mechanism and pressure tensor

A crucial characteristic of the two-range pseudopotential model is the competing mechanism between the short-range attractive and mid-range repulsive interactions. The short-range interactions act between the nearest-neighbor lattice nodes (connecting through the D2Q9 lattice), while the mid-range interactions act between the next-to-nearest-neighbor lattice nodes extending up to a D2Q25 lattice $\mathbf{e}_j = [|\mathbf{e}_{jx}|, |\mathbf{e}_{jy}|]$ ($j = 0, 1, \dots, 24$; see Fig. 1). The competing interaction force is explicitly written as [23,24]

$$\mathbf{F}_k^c = -G_{k,1} \psi_k(\mathbf{x}) \sum_{i=0}^8 w(|\mathbf{e}_i|^2) \psi_k(\mathbf{x} + \mathbf{e}_i) \mathbf{e}_i - G_{k,2} \psi_k(\mathbf{x}) \sum_{j=0}^{24} p(|\mathbf{e}_j|^2) \psi_k(\mathbf{x} + \mathbf{e}_j) \mathbf{e}_j, \quad (8)$$

where $G_{k,1}$ and $G_{k,2}$ are the strength coefficients for the short-range and mid-range interactions, respectively, and the weights for D2Q25 lattice are $p(0) = 247/420$, $p(1) = 4/63$, $p(2) = 4/135$, $p(4) = 1/180$, $p(5) = 2/945$, and $p(8) = 1/15120$. The pseudopotential originally suggested by SC [15,31], $\psi_k(\rho_k) = \rho_0(1 - e^{-\rho_k/\rho_0})$ (with a uniform reference density $\rho_0 = 1.0$ for each component) is adopted.

For a multicomponent fluid system, a repulsive force acts among all components as usual [15],

$$\mathbf{F}_k^r = -\rho_k(\mathbf{x}) \sum_{\bar{k}} G_{k\bar{k}} \sum_{i=0}^8 w(|\mathbf{e}_i|^2) \rho_{\bar{k}}(\mathbf{x} + \mathbf{e}_i) \mathbf{e}_i, \quad (9)$$

where $G_{k\bar{k}} = G_{\bar{k}k}$ are the strength coefficients for the intercomponent interaction. Supplemented with the body force \mathbf{F}_k^b , the total force in Eq. (5) is $\mathbf{F}_k = \mathbf{F}_k^c + \mathbf{F}_k^r + \mathbf{F}_k^b$. Although the model is in principle able to simulate a system with an arbitrary number of components, we will restrict ourselves to the most common case of a two-fluids mixture (i.e., $k = A, B$) with the same strength coefficients ($G_{A,1} = G_{B,1}$, $G_{A,2} = G_{B,2}$, $G_{AB} = G_{BA}$) in practice [23,24]. More specifically, a positive (negative) strength coefficient represents a repulsive (attractive) interaction. For the competing interactions in Eq. (8) imposed within each species, phase-separating fluids (vapor and liquid phases for each species) are confined to the condition [43] $G_{A,1} + G_{A,2} < 0$,

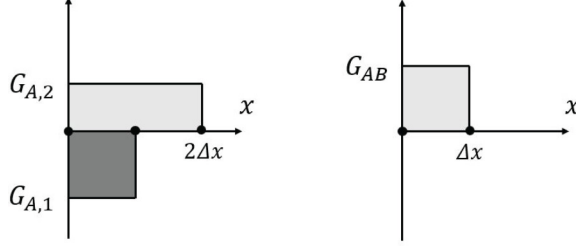


FIG. 2. A sketch of different interactions on component A. Left panel: short-range attractive ($G_{A,1} < 0$) and mid-range repulsive ($G_{A,2} > 0$) interactions within component A. Right panel: short-range repulsive ($G_{AB} > 0$) interaction between components A and B.

while in the present paper we set $G_{A,1} + G_{A,2} = -1$. The repulsive interactions between species are used as usual, $G_{AB} > 0$. A sketch of different interactions on component A is shown in Fig. 2.

To capture the complex rheological features of the soft flowing systems, it is crucial to analyze the pressure tensor associated with the two-range pseudopotential model. According to the analysis by Benzi *et al.* [24], the pressure tensor is defined as the sum of an interaction part plus a kinetic part,

$$P_{ab} = P_{ab}^{\text{int}} + P_{ab}^{\text{kin}}, \quad (10)$$

where a and b run over the spatial coordinates. The bulk equation of state reads as follows:

$$p_b(\rho_A, \rho_B) = \sum_{k=A,B} \left[\rho_k + \frac{1}{2}(G_{k,1} + G_{k,2})\psi_k^2 \right] c_s^2 + G_{AB}\rho_A\rho_B c_s^2. \quad (11)$$

The interaction tensor is defined by the condition

$$\partial_b P_{ab}^{\text{int}} = - \sum_k \mathbf{F}_{ka}, \quad (12)$$

which is independent of the specific forcing scheme and can be obtained based on the expression proposed by Shan [44]. Calculation details of P_{ab}^{int} can be found in Dollet *et al.* [27] and Sbragaglia and Belardinelli [45].

For the kinetic part, however, this is not the case. For the static interface problem considered in the next subsection, the kinetic part in Eq. (10) is given by

$$P_{ab}^{\text{kin}} = \sum_{k,i} f_{k,i} e_{ia} e_{ib}. \quad (13)$$

In the original two-range model [23,24], the explicit expression of P_{ab}^{kin} is, $P_{ab}^{\text{kin}} = \sum_k \rho_k c_s^2 \delta_{ab} + K_{ab}^\tau$, where K_{ab}^τ denotes the following extra τ -dependent terms:

$$K_{ab}^\tau = \left(\tau - \frac{1}{2} \right)^2 \frac{F_a F_b}{\rho} + c_s^4 \frac{\rho_A \rho_B}{\rho} \left(\tau - \frac{1}{2} \right)^2 \left(\frac{\partial_a \rho_A}{\rho_A} - \frac{\partial_a \rho_B}{\rho_B} \right) \left(\frac{\partial_b \rho_A}{\rho_A} - \frac{\partial_b \rho_B}{\rho_B} \right), \quad (14)$$

where $F_a = (F_{A,a} + F_{B,a})$ and $\tau = (\rho_A \tau_A + \rho_B \tau_B) / \rho$. Due to the τ -dependent terms, the original two-range model suffers numerical instability for two-component flow with a relative large viscosity ratio. Moreover, the surface tension and disjoining pressure are dependent on the viscosity ratio. Remarkably, the τ -dependent terms can be removed in the present model, due to proper consideration of discrete lattice effects in the forcing scheme in Eqs. (5) and (6). As a result, the present two-range model shows significant improvements compared with the original two-range model in terms of tunable viscosity ratio and also in terms of eliminating the dependence of surface

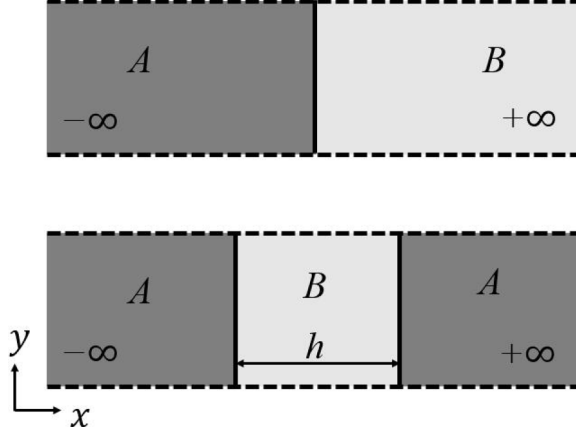


FIG. 3. A sketch for one and two interfaces between components A and B. Top panel: one interface case for the calculation of the surface tension γ in Eq. (15). Bottom panel: two interfaces separated by a distance h for the calculation of the overall line tension $\gamma_f(h)$ in Eq. (16). When the distance h is large enough, $\gamma_f(h)$ is convergent to 2γ . By setting a series of h , the disjoining pressure can be calculated through Eq. (18).

tension and disjoining pressure on the viscosity ratio (see Sec. III). In addition, the total mass of both species in the present model is conserved to machine accuracy.

C. Macroscopic effect of the mesoscopic interaction: The disjoining pressure

Paradigmatic soft materials, such as foams and emulsions, consist of dispersion of one fluid (a gas in the case of foams, a liquid for emulsions) in another liquid; the dispersion is stabilized against full phase separation by the presence of surfactants, which lower the interfacial energy, thus inhibiting droplet (bubble) coalescence. A mechanical *translation* of this (microscopic) stabilization effect of surfactants at mesoscopic level can be done borrowing the concept of disjoining (or Derjaguin) pressure Π from the theory of thin liquid films [46]. In such a framework, the disjoining pressure emerges as a repulsive force per unit area between opposing interfaces, due to interface-interface interactions [46], that stabilizes the thin film. Analogously, for a thin film formed between two droplets or bubbles to be stable, a (positive) disjoining pressure has to overcome the capillary pressure at the curved interface [47]. As analyzed by Sbragaglia *et al.* [25], the pure short-range interaction in the original S-C model [corresponding to $G_{k,1} = G_{k,2} = 0$ in Eq. (8)] always yields a negative disjoining pressure. Notably, a positive disjoining pressure can be achieved in the two-range model by tuning the strength coefficients at a fixed $G_{k,1} + G_{k,2}$.

To quantitatively determine Π in our model, let us first consider a one-dimensional problem: a flat interface orthogonal to the x coordinate (see Fig. 3). The surface tension can, then, be defined as the integral of the mismatch between the normal (P_{xx}) and tangential (P_{yy}) components for the pressure tensor,

$$\gamma = \int_{-\infty}^{+\infty} (P_{xx} - P_{yy}) dx, \quad (15)$$

where $(P_{xx} - P_{yy})$ can be explicitly obtained via Eq. (10). We then consider two flat interfaces, separated by a distance h (see Fig. 3); now the integral in Eq. (15) is defined as the overall line tension,

$$\gamma_f(h) = \int_{-\infty}^{+\infty} (P_{xx} - P_{yy}) dx. \quad (16)$$

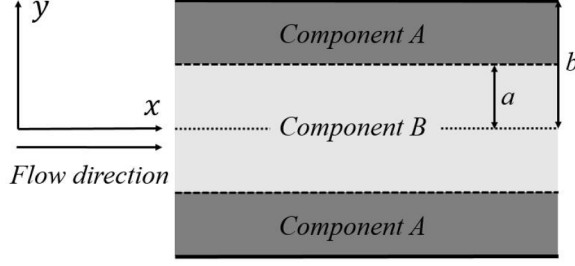


FIG. 4. Sketch of the two-component Poiseuille flow.

As we can see, γ_f is a function of h , and the limit condition is $\gamma_f(h \rightarrow \infty) = 2\gamma$. According to Refs. [25,47], the disjoining pressure Π is defined as

$$\int_{\Pi(h=\infty)}^{\Pi(h)} h d\Pi = s(h), \quad (17)$$

where $s(h) = \gamma_f(h) - 2\gamma$. A simple differentiation of Eq. (17) yields $ds(h)/dh = h d\Pi/dh$. Supplementing with the boundary condition $\Pi(h \rightarrow \infty) = 0$, the disjoining pressure finally reads as

$$\Pi(h) = \frac{s(h)}{h} - \int_h^\infty \frac{s(\tilde{h})}{\tilde{h}^2} d\tilde{h}. \quad (18)$$

By setting a series of interface distances, Eq. (18) can be calculated using standard numerical integration methods.

III. NUMERICAL SIMULATIONS

In this section, numerical simulations are conducted to verify the aforementioned arguments and highlight the main features of the present two-range pseudopotential model. Unless otherwise specified, the strength coefficients in Eq. (8) are set the same for both components ($G_{A,1} = G_{B,1}$ and $G_{A,2} = G_{B,2}$) with $G_{A,1} + G_{A,2} = -1$ [25,27], and the coefficient G_{AB} is chosen such that the interface width is about four lattice spacings [48].

A. Two-component Poiseuille flow

First, a two-component Poiseuille flow (along the x direction) driven by a body force is studied (see also Fig. 4). In this flowing system, the nonwetting phase (component B) flows in the central region of the channel, $0 < |y| < a$, the wetting phase (component A) flows between the nonwetting phase and the walls, $a < |y| < b$, and the dynamic viscosity ratio is $M = \frac{\mu_B}{\mu_A} = \frac{\nu_B}{\nu_A}$ (M simplifies to the kinematic viscosity ratio due to the unit density ratio considered). In our simulations, periodic boundary conditions are applied along the x direction, the half-way bounce-back boundary scheme is applied to the top and bottom walls, and the computational domain is covered by 10×160 lattice nodes. The analytical solution for the problem is given by [48]

$$u(y) = \begin{cases} \frac{F_b}{2\mu_B}(a^2 - y^2) + \frac{F_b}{2\mu_A}(b^2 - a^2), & 0 < |y| < a \\ \frac{F_b}{2\mu_A}(b^2 - y^2), & a < |y| < b \end{cases}, \quad (19)$$

where the body force F_b acts on both components and b is set to $80\Delta x$, with $b = 2a$.

It is known that the velocity shift forcing scheme suffers numerical instability for two-component flow with a relatively high kinematic viscosity ratio M [49]. All implementations of the original two-range model so far were for $M = 1$ [23–25]. Figure 5 shows the comparison between numerical

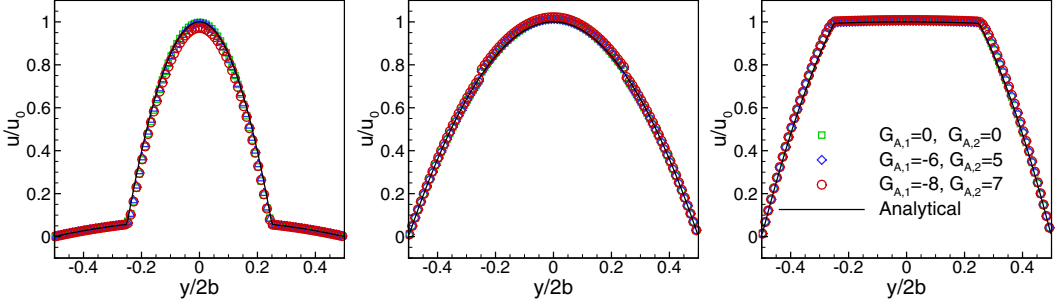


FIG. 5. Steady velocity profiles for two-component Poiseuille flow with different viscosity ratios, $M = \{1/50, 1, 50\}$ (from left to right); the profiles are normalized by the centerline velocity $u_0 = 0.05$ (lbu). The symbols are numerical results by the present two-range pseudopotential model, and the lines are the analytical solutions.

results obtained by the present two-range model and the analytical solutions at different viscosity ratios, $M = \{1/50, 1, 50\}$ (from left to right). For the original two-range model, the simulation is unstable for $M > 5$, thus it is not shown in the figure. For the present model, we consider three cases: two of them corresponding to positive disjoining pressures ($G_{A,1} = -6$ and -8) and a reference case ($G_{A,1} = G_{A,2} = 0$). It can be seen that the numerical results are in good agreement with the analytical solutions, except for some small discrepancies near the interface. As analyzed in Refs. [48,50], the small discrepancies may be related to the diffused interface feature in LBM and have no significant effects on the flow away from the interface. These results prove that, with our model, the viscosity ratio can be tunable over a relatively large range, still reproducing physically correct results.

B. Tunable surface tension

In the single-range pseudopotential model, the surface tension can only be varied through the parameter G_{AB} . Because of the introduction of the competing mechanism, the surface tension in the present two-range model can be also adjusted by tuning the parameters $G_{A,1}$ and $G_{A,2}$. To confirm this statement, a series of Laplace's tests are carried out to measure the surface tension under different conditions. Four different cases ($G_{A,1} = 0, G_{A,2} = 0$; $G_{A,1} = -10, G_{A,2} = 9$; $G_{A,1} = 0, G_{A,2} = -1$ and $G_{A,1} = 10, G_{A,2} = -11$) are considered, in which the first case corresponds to the classical single-range model. The tunable range of G_{AB} and the achievable range of γ are shown in Table I. The parameter G_{AB} is tuned progressively with a 0.1 interval to find a range over which the measured interface thickness W is within $2\Delta x \leq W \leq 5\Delta x$; such a range is constrained since interfaces that are too sharp ($W < 2\Delta x$) suffer from numerical instability, and those that are too wide ($W > 5\Delta x$) deteriorate the numerical accuracy near the interface. The interface width W is defined by fitting a hyperbolic tangent curve to the density profile [34], which can be rewritten as $W = (\rho_{A,\max} - \rho_{A,\min}) / (\partial \rho_A / \partial x)|_{\bar{\rho}_A}$ with $\bar{\rho}_A = (\rho_{A,\max} + \rho_{A,\min}) / 2$ and solved using the finite difference method (see Fig. 6).

TABLE I. Tunable range of G_{AB} and the corresponding range of the surface tension γ for the present model under different cases. The case without two-range interactions ($G_{A,1} = 0, G_{A,2} = 0$) is shown for comparison.

Case	$G_{A,1} = 0,$ $G_{A,2} = 0$	$G_{A,1} = -10,$ $G_{A,2} = 9$	$G_{A,1} = 0,$ $G_{A,2} = -1$	$G_{A,1} = 10,$ $G_{A,2} = -11$
Range of G_{AB}	[2.8,5.0]	[2.0,3.4]	[2.3,5.1]	[2.9,7.2]
Range of γ	[0.031,0.14]	[0.0006,0.041]	[0.028, 0.16]	[0.081,0.27]

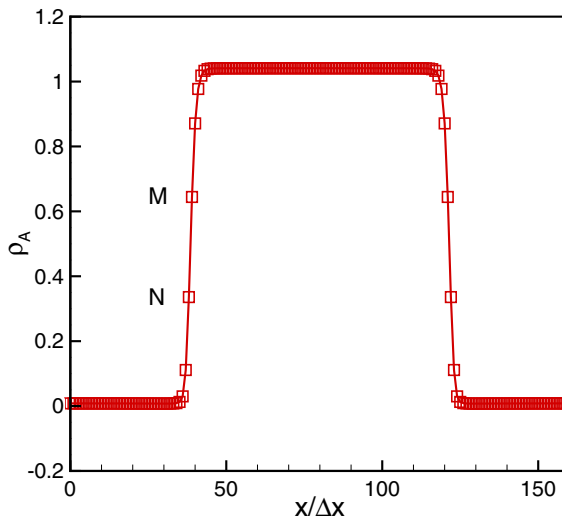


FIG. 6. The density profile along the horizontal centerline for a steady droplet (component A) with radius $R = 42\Delta x$ in the center of a periodic box: we measure the interface thickness as $W = (\rho_{A,\max} - \rho_{A,\min})\Delta x / [\rho_A(M) - \rho_A(N)]$, where M and N are the two points near the location where $\bar{\rho}_A = (\rho_{A,\max} + \rho_{A,\min})/2$. The interface thickness is $W = (1.041 - 0.008)\Delta x / (0.644 - 0.336) = 3.35\Delta x$.

It can be seen from Table I that the achievable range for the single-range model is $0.031 \leq \gamma \leq 0.14$. For the two-range model, we have more freedom to tune the surface tension due to the additional competing interactions, and for the four cases considered in this work, the achievable range is $6 \times 10^{-4} \leq \gamma \leq 0.27$. Specifically, larger (smaller) $G_{A,1}$ gives larger (smaller) surface tension, because, at fixed $G_{A,1} + G_{A,2}$, the diagonal elements of the interaction pressure tensor P_{ab}^{int} are proportional to $G_{A,1}$ [see Eqs. (14)–(16) in Ref. [24]].

In addition, unlike the original two-range model [24], where the surface tension is viscosity-dependent, in the present model the surface tension and viscosity ratio are decoupled, as will be discussed in the next subsection.

C. Independence of surface tension and disjoining pressure on the viscosity ratio

The emergence of positive disjoining pressure is a unique feature of the two-range model, which supports the stable thin film between two interfaces and distinguishes the two-range model from the classical single-range model. To measure the disjoining pressure Π , we consider two planar interfaces, separated by a distance h (see also Fig. 3). After $\gamma_f(h)$ is obtained through Eq. (16) for various h , the disjoining pressure can be calculated according to Eq. (18). To be general, we introduce a dimensionless disjoining pressure $\Pi^* = \Pi h_0 / \gamma$, where $h_0 \sim O(10\Delta x)$ is a length scale defined as $\gamma_f(h > h_0) = 2\gamma$. Firstly, we choose $G_{AB} = 3.0$, and calculate the dimensionless disjoining pressure as a function of the dimensionless distance $h^* = h/h_0$ for the present model with different pairs of $(G_{A,1}, G_{A,2})$, as shown in Fig. 7. From the figure, we can see that for the case $(G_{A,1} = 0, G_{A,2} = 0)$, corresponding to the classical single-range model, the disjoining pressure is always negative and decreases with h^* . For other cases with the two-range competing interactions, the disjoining pressure increases with the decrease of h^* first and then goes down, attaining positive values in between.

Then we compare the original two-range model [23,24] with the present model in Fig. 8. For the original model, some τ -dependent terms are reproduced in P_{ab}^{kin} [see Eq. (14)], thus the surface tension is dependent on the viscosity for each component. In this simulation, the measured surface tensions at viscosity ratio $M = \{1/2, 1, 3\}$ are 0.056, 0.043, and 0.039, respectively. Remarkably,

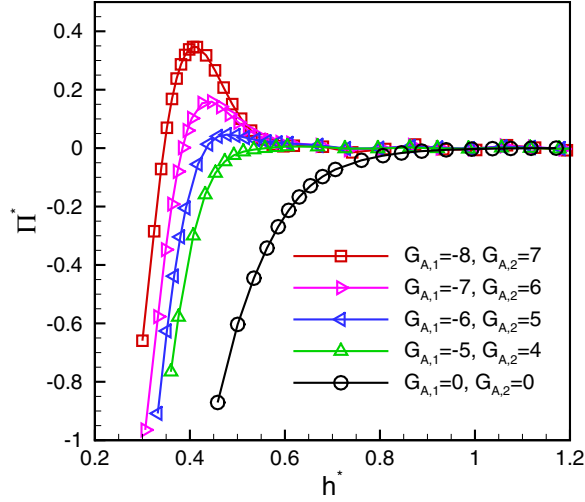


FIG. 7. Dimensionless disjoining pressure Π^* as a function of dimensionless distance h^* for different cases. For the case $G_{A,1} = 0, G_{A,2} = 0$ (without two-range competing interactions), the disjoining pressure decreases with h^* , thus it cannot support a stable thin film between two interfaces. For other cases (with two-range competing interactions), with the decrease of h^* , the disjoining pressure increases gradually to a peak and then goes down, which stabilizes the thin film. The peak value of disjoining pressure increases with decreasing $G_{A,1}$.

the τ -dependent terms in P_{ab}^{kin} are removed by using the present forcing scheme. Under different viscosity ratio $M = \{1/10, 1, 10\}$, the surface tension is approximately constant (with a maximum relative error of 1.2%). As a result, the disjoining pressure depends on M significantly for the original model in Refs. [23,24], while it is independent of M for the present model. To highlight this point, we consider collisions of droplets of component A in a liquid matrix of component B . We wish to point out that the configuration here is consistent with Fig. 3, because a thin film (component

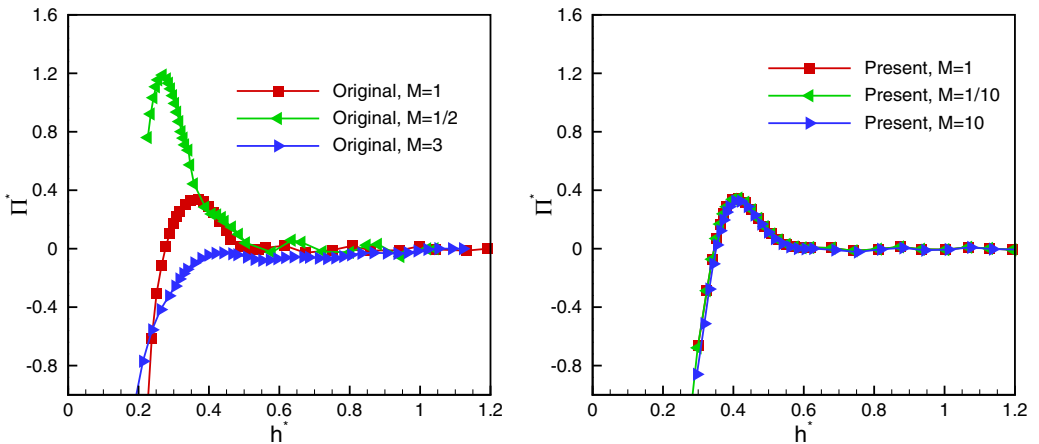


FIG. 8. Comparison of the obtained disjoining pressure Π^* at different viscosity ratio M by the original (left) and present (right) two-range models. For the original model [23,24], Π^* changes substantially and even changes the sign when M varies. For the present model, Π^* is independent of M . It may be noted that the profiles for the two models at $M = 1$ are approximately the same.

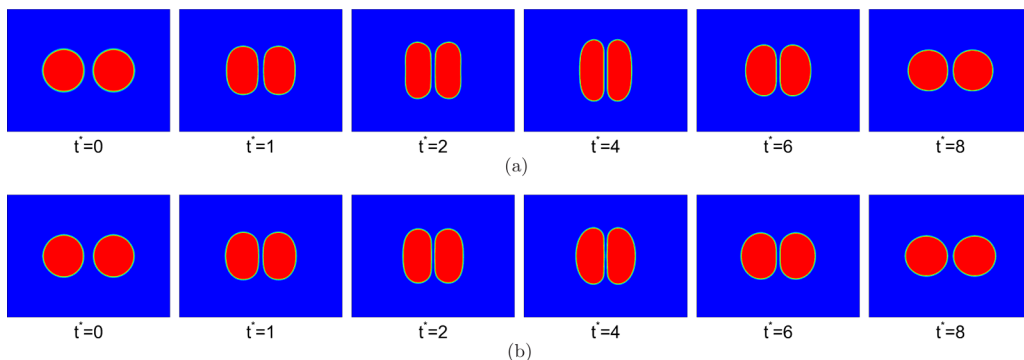


FIG. 9. Snapshots ($t^* = tU/D$) of two equal-sized droplets collision at viscosity ratio $M = 1$: (a) the original two-range model and (b) the present two-range model.

B) is produced between the two droplets (component *A*) when the two droplets are approaching each other. Two equal-sized droplets with a diameter D are initialized with a relative velocity U , which leads to a capillary number $\text{Ca} = \frac{\mu_A U}{\gamma} \approx 0.3$ and a Weber number $\text{We} = \frac{\rho_A D U^2}{\gamma} \approx 15$. First, we choose a unity viscosity ratio $\mu_A = \mu_B = 0.1$. Due to the positive disjoining pressure, a stable thin film between the droplets is supported, and the two droplets bounce back in the end, as shown in Fig. 9. Then we change μ_B to 0.3. For the present model, the disjoining pressure is viscosity-independent, thus the two droplets still bounce back in Fig. 10. However, the disjoining pressure changes to be negative for the original model when $M = \frac{\mu_B}{\mu_A} = 3$. As a result, the thin film cannot be supported any longer, and the two droplets eventually coalesce.

The present model, which displays a disjoining pressure independent of the viscosity ratio, represents a significant improvement with respect to the original model and makes it of major significance for many applications where nonunit viscosity ratios are needed [51–56].

D. Pressure-driven emulsion in a planar channel

The method we have presented, because of its built-in properties, is particularly suitable to simulate the hydrodynamics of emulsions, especially in dense situations. We move therefore to simulate a multidroplet situation. We consider a pressure-driven flow in a planar channel of a monodisperse emulsion, made of a regular arrangement of equal-size droplets (component *A*) dispersed in a continuous matrix (component *B*). The simulations are performed on a $L \times L$

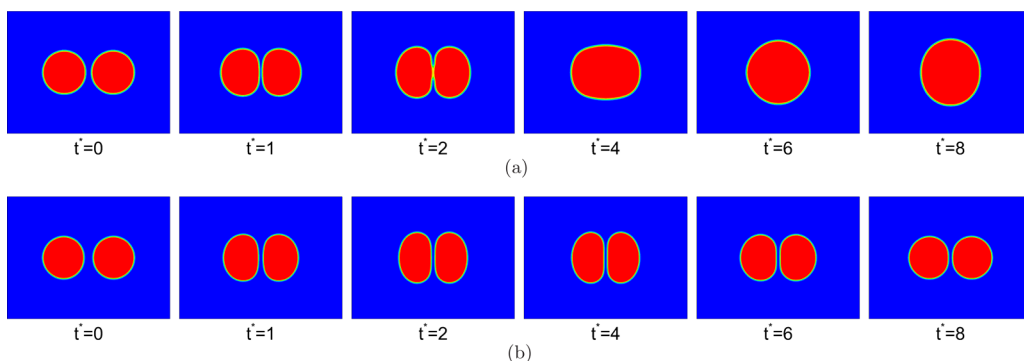


FIG. 10. Snapshots ($t^* = tU/D$) of two equal-sized droplets collision at viscosity ratio $M = 3$: (a) the original two-range model and (b) the present two-range model.

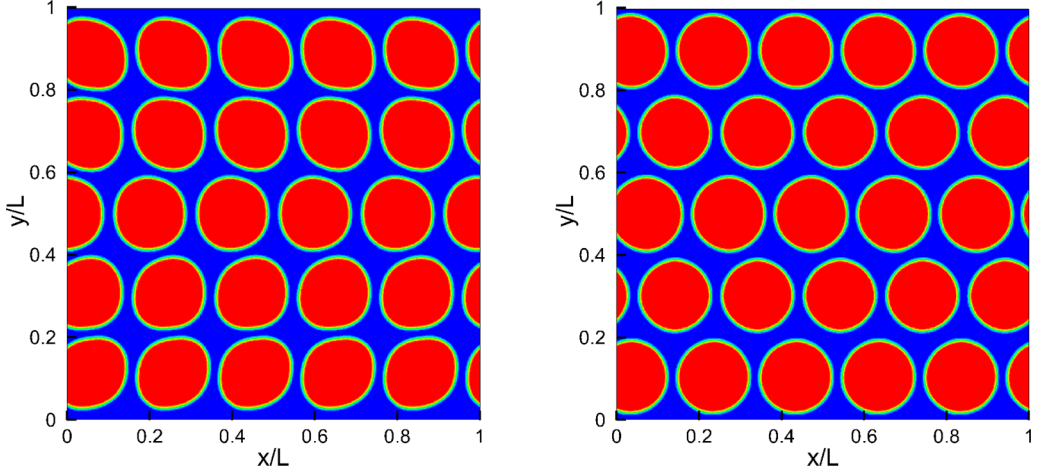


FIG. 11. Snapshots of pressure-driven emulsion in a planar channel at volume fraction $\Phi = 0.64$ with $M = \mu_B/\mu_A = 1$ (left panel), and $M = 1/10$ (right panel).

domain, with $L = 220\Delta x$; no-slip boundary conditions for the velocity are imposed on the top ($y = L$) and bottom ($y = 0$) walls; nonwetting boundary conditions for droplets apply, i.e., a contact angle of $\theta = 180^\circ$ is set for component A on both walls. A body force F_b in the x direction is imposed to mimic a constant pressure gradient, which can be expressed in nondimensional form as $\bar{F}_b = F_b L^3 \rho_B / (8\mu_B^2)$ (notice that such an expression coincides with the Reynolds number that would be achieved in the corresponding Poiseuille flow in the pure continuous phase, for the given forcing F_b). The coupling parameters are $G_{AB} = 3.0$, $G_{A,1} = -7.4$, $G_{A,2} = 6.4$, giving $\gamma = 0.04$, and the droplet radius is set within $10\Delta x < R < 20\Delta x$ to obtain different volume fractions Φ of the dispersed phase, $\Phi \in [0.18, 0.64]$ (typical snapshots of $\Phi = 0.64$ are shown in Fig. 11).

When no droplets are present in the system ($\Phi = 0$), the usual Poiseuille flow profile for a pure fluid is obtained, as shown in the left panel of Fig. 12. In Fig. 12, left panel, we show the velocity

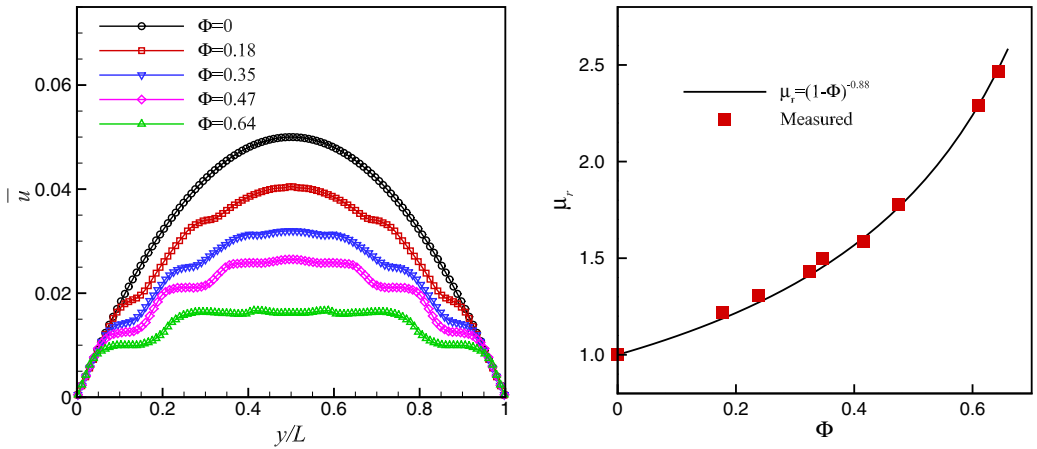


FIG. 12. Rheological feature of pressure-driven emulsion in a planar channel at $\bar{F}_b = 37$. Left panel: x -direction average velocity profile as a function of y at different droplets volume fractions Φ . Right panel: measured μ_r (symbols) as a function of droplets volume fraction Φ , where the solid line is a fit by a model based on the differential effective medium theory [58].

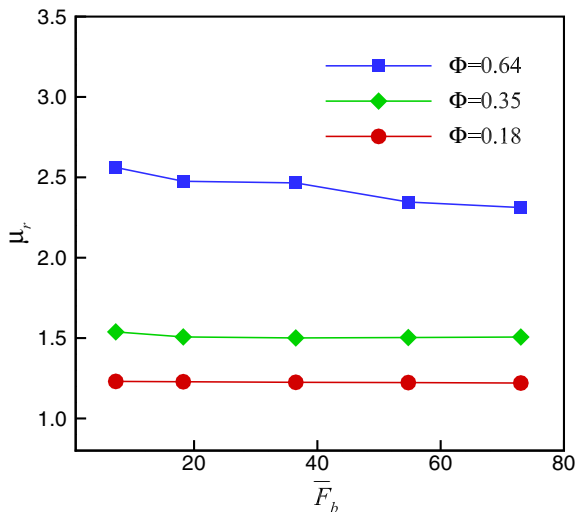


FIG. 13. Relative effective viscosity μ_r as a function of \bar{F}_b at different volume fractions Φ .

profile for different volume fractions at $\bar{F}_b = 37$ and $M = 1$, where \bar{u} is the average velocity along x direction. As expected, when Φ is increased, the velocity profile flattens gradually in the central region of the channel, which is consistent with previous results [25,54]. To quantify the effect of increasing the volume fraction, we estimate the relative effective viscosity $\mu_r \equiv \mu_{\text{eff}}/\mu_B$ as the ratio of flow rates $\mu_r(\Phi) = Q(\Phi = 0)/Q(\Phi)$, where $Q = \int_0^L \bar{u}(y) dy$. A plot of μ_r as a function of Φ at $\bar{F}_b = 37$ is shown in the right panel of Fig. 12. It can be seen that the relative effective viscosity increases nonlinearly with Φ , as observed also for a similar system with neutral wetting boundaries for the droplets [54]. A number of expressions for the effective viscosity of an emulsion as a function of the volume fraction are available in the literature [57,58]. Based on the differential effective medium theory, Bullard *et al.* [58] proposed the following model:

$$\mu_r = (1 - K\Phi)^{-[\eta]/K}, \quad (20)$$

where the factor K is set to be 1.0, and $[\eta]$ represents the *intrinsic viscosity*. For the present system with slightly deformable droplets (see Fig. 11), the *intrinsic viscosity* $[\eta]$ is confined between the undeformable limit of Taylor [59] $[\eta]_T = (1/M + [\eta]_\infty)/(1/M + 1)$ and the freely deformable limit of Douglas *et al.* [60] $[\eta]_D = (1 - 1/M)/[(1 - 1/M)/[\eta]_\infty + 1/M]$, where $[\eta]_\infty = 2.5$. In Fig. 12, we show a very good fit by Eq. (20) with $[\eta] = 0.88$.

We now proceed to investigate the effect of body force by exploring a range of nondimensional body forces $7 \leq \bar{F}_b \leq 73$. Figure 13 plots μ_r as a function of \bar{F}_b at different volume fractions. From Fig. 13 we can see that μ_r is almost independent of the forcing in the parameter range we considered, as expected for a Newtonian fluid. For the highest volume fraction tested, $\Phi = 0.64$, instead, a slight decrease of μ_r with the increasing forcing can be appreciated, hinting at a moderate shear thinning behavior, as expected for this kind of systems.

We address now the effect of the viscosity ratio $M = \mu_B/\mu_A$ on the rheology of the emulsion. We stress here incidentally that the capability of simulating viscosity ratios other than one extends the applicability of our method to study the physics of more general soft flowing systems. In this sense, the limit $M \rightarrow 0$ is that of solid suspensions, while $M \gg 1$ would correspond to foams. In Fig. 14 we plot the relative effective viscosity μ_r as a function of the viscosity ratio M . We can see an asymmetric effect of M : for $M > 1$, μ_r is approximately independent of M , while for $M < 1$, μ_r increases with the decrease of M , and this effect is more significant at larger volume fractions. As

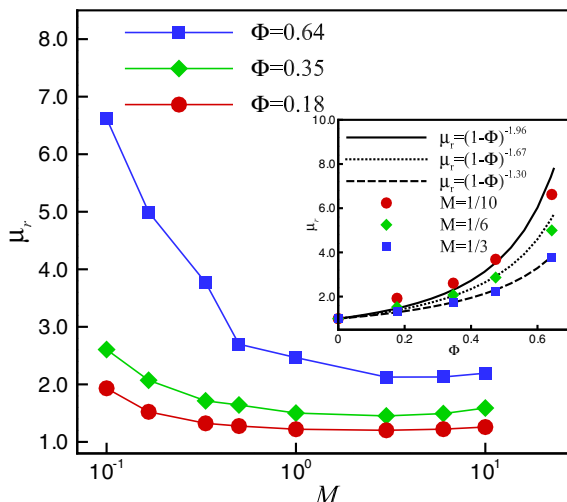


FIG. 14. Relative effective viscosity μ_r as a function of viscosity ratio $M = \mu_B/\mu_A$ at different volume fractions Φ and $\bar{F}_b = 37$. The left branch of the figure, $M < 1$, corresponds to more viscous, hence less deformable, droplets ($M \rightarrow 0$ is the solid sphere limit), while in the right branch $M > 1$ they are less viscous than the matrix, and correspondingly more deformable ($M \gg 1$ is the bubble case). This figure can be also seen then as the effective viscosity of a suspension of soft deformable particles, as a function of their stiffness. Inset: Plot of μ_r versus Φ for $M = 1/10, 1/6, \text{ and } 1/3$.

shown in the inset, we also find good fits by Eq. (20) for $M = 1/10, 1/6, 1/3$, where the *intrinsic viscosity* $[\eta]$ in each fitting line is confined between $[\eta]_T$ and $[\eta]_D$ for the specified condition.

IV. CONCLUSIONS

A mesoscopic numerical method for the simulation of soft flowing systems based on a two-range pseudopotential lattice Boltzmann construction has been proposed. Our method is remarkable as it features adjustable surface tension, positive disjoining pressure, tunable viscosity ratio, and fully resolved hydrodynamics, unlike, to our knowledge, any other existing alternative methods (such as boundary integral methods [61] or “bubble models” [62]). In contrast to the previous literature, the present model removes the viscosity dependence in the original two-range pseudopotential LBM, thus opening the way to the simulation of multicomponent fluids with nonunit viscosity ratios and a viscosity-independent disjoining pressure. Such a capability is demonstrated by computing the relative effective viscosity of a pressure-driven emulsion in a planar flow as a function of the viscosity ratio between the disperse and continuum phases.

It is hoped that the present upgrade will permit us to extend the range of applications of the LBM for complex soft flowing systems.

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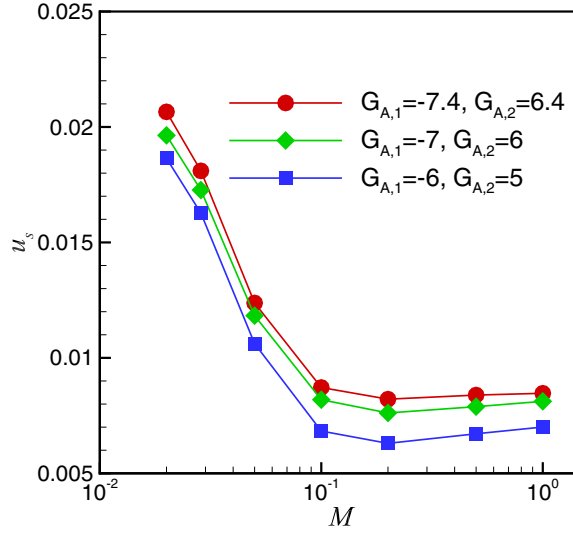


FIG. 15. Maximum spurious currents u_s , measured from a steady droplet in a continuous matrix at different viscosity ratios M and strength coefficients $G_{A,1}$.

APPENDIX: SPURIOUS CURRENTS

It is known that the diffusive interface models lead to spurious velocity currents around interfaces due to the numerical imbalances of various discretized forces. The maximum spurious currents, u_s , produced for a steady droplet ($R = 20\Delta x$) under different conditions are shown in Fig. 15. The parameters used in the simulations are the same as those in Sec. III D. As can be seen, the maximum spurious current is relatively small for viscosity ratio $M > 1/10$ (the range considered in Sec. III D), while it increases gradually when M is further decreased. For a given viscosity ratio, u_s is reduced when the strength coefficient $G_{A,1}$ is increased, which corresponds to smaller disjoining pressure (see Fig. 7). For the time being, we mainly focus on the removal of the viscosity dependence in the original two-range model, while strategies or parameter optimization methods [10,55,63,64] for reducing the spurious currents can be adopted for future applications with quite small (or quite large) viscosity ratios.

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