Data-Driven Robust Control for Type 1 Diabetes Under Meal and Exercise Uncertainties

Nicola Paoletti[1], Kin Sum Liu[1], Scott A. Smolka[1], and Shan Lin[2]

[1] Department of Computer Science, Stony Brook University, USA
[2] Department of Electrical and Computer Engineering, Stony Brook University, USA

Abstract. We present a fully closed-loop design for an artificial pancreas (AP) which regulates the delivery of insulin for the control of Type I diabetes. Our AP controller operates in a fully automated fashion, without requiring any manual interaction (e.g. in the form of meal announcements) with the patient. A major obstacle to achieving closed-loop insulin control is the uncertainty in those aspects of a patient's daily behavior that significantly affect blood glucose, especially in relation to meals and physical activity. To handle such uncertainties, we develop a data-driven robust model-predictive control framework, where we capture a wide range of individual meal and exercise patterns using uncertainty sets learned from historical data. These sets are then used in the controller and state estimator to achieve automated, precise, and personalized insulin therapy. We provide an extensive *in silico* evaluation of our robust AP design, demonstrating the potential of this approach, without explicit meal announcements, to support high carbohydrate disturbances and to regulate glucose levels in large clusters of virtual patients learned from population-wide survey data.

1 Introduction

Type 1 diabetes (T1D) is an autoimmune disease where the pancreas is not able to autonomously produce a sufficient amount of insulin to regulate blood glucose (BG) levels, thereby inhibiting glucose uptake in muscle and adipose (fatty) tissue. In healthy subjects, pancreatic β cells are responsible for the release of insulin in amounts commensurate with current BG levels. This regulation maintains healthy BG values within tight ranges, normally between 70-200 mg/dL. In T1D, T cell–mediated destruction of insulin-producing β cells occurs, leading to high BG levels.

In the U.S. alone, more than 29 million people suffer from diabetes, among which about 5% have T1D [2]. T1D patients need to wear an insulin pump for the injection of *basal* and *bolus* insulin. Basal insulin is a low and continuous dose that covers insulin needs outside meals. Bolus insulin is a single high dose for covering meals.

The concept of closed-loop control of insulin, a.k.a. the artificial pancreas (AP), involves a continuous glucose monitor (CGM) that provides glucose measurements (with a typical period of 5 minutes) to a control algorithm running

inside the insulin pump or on a peripheral device (e.g. smartphone or tablet) connected to the pump [38]. The controller adjusts the insulin therapy to maintain healthy BG levels and to avoid *hyperglycemia* (BG above the healthy range) as well as *hypoglycemia* (BG below the healthy range). AP systems have been extensively studied in the last 20 years [10], but only lately cleared for clinical trials [17, 22] and commercialization.

The recently FDA-approved MINIMED 670G by Medtronic[3] is the first commercial AP system, and can regulate the basal insulin rate automatically. It is referred to as a "hybrid closed-loop" device as patients need to manually announce the amount of carbohydrate (CHO) and time of each meal to receive the appropriate bolus insulin dose. This manual procedure is a burden to the patient and inherently dangerous as incorrect information can lead to incorrect insulin dosage and, in turn, harmful BG levels.

While meals are the major source of uncertainty in BG control, another important factor is physical activity, which accelerates glucose absorption and thus requires a reduced insulin dosage. To build fully automated *closed-loop* AP systems, it is essential to design insulin control algorithms that are *robust* to the patient's behavior and activities.

In this paper, we propose a *data-driven, robust model-predictive control* (robust MPC) framework for the closed-loop control of insulin administration, both basal and bolus, for T1D patients under uncertain meal and exercise events. Such a framework seeks to eliminate the need for meal announcements by the patient, to fully automate insulin regulation. We capture the wide range of individual meal and exercise patterns using *uncertainty sets* learned from historical data.

Following [1], we construct uncertainty sets from data so that they cover the underlying (unknown) distribution with prescribed probabilistic guarantees. Leveraging such information, our robust MPC system computes the insulin administration profile that minimizes the worst-case performance with respect to these uncertainty sets, so providing a principled way to deal with uncertainty.

Besides uncertainty, another challenging aspect of closed-loop control is *state estimation*, which is needed to recover the full state of the model (used within MPC) from CGM measurements. Not only are these measurements noisy and delayed with respect to BG (the CGM detects glucose in the interstitial fluid), but we also need to estimate, along with the state, current meal and exercise uncertainties.

For this purpose, we designed a moving-horizon state estimator (MHE) [6, 20, 27] that, similar to MPC, exploits a prediction model to find the most likely state estimate given the observations. Crucially, data-driven uncertainty sets improve the estimation by constraining the admissible meal and exercise uncertainties.

To the best of our knowledge, our robust MPC design for an AP is the first approach to leverage data-driven techniques to enhance robust insulin control and state estimation, supporting at the same time both meal and exercise uncertainties. In summary, our main contributions are the following.

---

[3] https://www.medtronicdiabetes.com/products/minimed-670g-insulin-pump-system

- We formulate a closed-loop AP design based on robust MPC to optimize BG levels under meal and exercise uncertainties.
- We apply data-driven techniques to construct uncertainty sets that provide probabilistic guarantees on the robust MPC solution.
- We design an MHE that leverages data to make informed estimates for BG and uncertainty parameters.
- We provide an extensive *in-silico* evaluation of our design, including one-meal simulations, one-day high carbohydrate intake scenarios, and one-day simulations of large clusters of virtual patients learned from population-wide survey data sets (CDC NHANES).
- Overall, our robust closed-loop AP is able to keep BG within safe levels between 84% and 100% of the time, outperforming an implementation of a hybrid closed-loop AP and state-of-the art robust control algorithms [31].

2 System Overview

The design of our proposed data-driven robust artificial pancreas is illustrated in Figure 1. The *robust MPC* component (described in Section 4) is responsible for computing the insulin administration strategy (both basal and bolus) that optimizes, over a finite time horizon, the predicted BG profile against worst-case realizations of the uncertainty parameters, used to capture unknown meal and exercise information.

Uncertainty sets describe the domains of the uncertainty parameters and are derived by the *data-driven learning* component (see Section 4.2), starting from a dataset about the patient's meal and exercise schedules. Uncertainty sets can be also updated online as new data (estimated or announced) comes along, in this way enabling the continuous learning of the patient's behavior.

At this stage, we analyze our robust artificial pancreas design *in silico*. Thus, the *plant* is given by a system of differential equations (see Section 3) describing the gluco-regulatory dynamics of a virtual T1D patient, as well as the effects of insulin and random disturbances (i.e. unknown realizations of the uncertainty parameters).

In order to faithfully reproduce real-life settings, we assume that the state of the

Fig. 1: Robust artificial pancreas design.

plant (BG) cannot be observed by the controller, but that we can only access (noisy) CGM measurements. We designed a *moving-horizon state estimator* (described in Section 4.1) that, based on a bounded history of CGM measurements
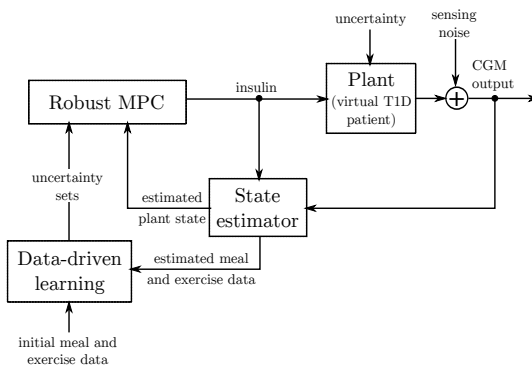
and estimations, computes the most likely plant state. Importantly, this component also provides estimates for the uncertainty parameters, which can be used to update the uncertainty sets.

3 Plant Model

3.1 Uncertainty parameters

To account for uncertainty in meal consumption, we consider the parameter D_G^t, which describes the *rate of CHO ingestion* at time t. As in the exercise model of [9, 13, 21, 28], physical activity is represented by parameters MM^t, the *percentage of active muscular mass* at time t, and $O2^t$, the *percentage of maximum oxygen consumption* which can be combined to reproduce arbitrary kinds of physical activity.

MM^t corresponds to the ratio between the active muscular mass and the total muscular mass, with typical values being $MM^t = 0\%$ at rest and $MM^t = 25\%$ for a two-legged exercise. $O2^t$ describes the oxygen consumed relative to the maximum oxygen consumption of the subject, and thus, represents a subject-independent measure of exercise workload. As in [9, 21], typical values are 8% at rest, 30% for light activity, 60% for moderate activity, and 90% for intense activity. In our scenario, these meal and exercise parameters are not observed or measured, and are thus represented by an uncertainty parameter vector $\mathbf{u}^t = (D_G^t, MM^t, O2^t)$. The effects of these parameters on blood glucose are described in Section 3.2, in which the patient's gluco-regulatory model is presented.

3.2 Patient Model

We consider the nonlinear ODE gluco-regulatory model of Jacobs et al. [13, 28], which extends Hovorka's well-established model [11, 36, 37] to capture the effect of exercise on BG. The model describes the dynamics of glucose and insulin in the human body, i.e., their absorption, metabolism, excretion and transport between compartments (tissues and organs). In addition to insulin, Jacobs' model also allows for the automated control of glucagon, i.e. the hormone antagonistic to insulin that protects against hypoglycemia. In our work, however, we leave aside glucagon. Model parameters (listed in Table 2 of the appendix) are deterministic and represent the physiological characteristics (e.g. transport or consumption rates) of a single virtual subject.

At time t, the inputs to the system are the subcutaneous insulin infusion rate, ι^t (mU/min), and the uncertainty parameter values, $\mathbf{u}^t = (D_G^t, MM^t, O2^t)$. The output corresponds to the CGM measurement. The state-space representation of the system is as follows:

$$\dot{\mathbf{x}}(t) = \mathbf{F}\left(\mathbf{x}(t), \iota^t, \mathbf{u}^t\right) \tag{1}$$

$$y(t) = h\left(\mathbf{x}(t)\right) + v^t \tag{2}$$

where $\mathbf{x}$ is the 14-dimensional state vector that evolves according to the ODE system $\mathbf{F}$, which is given below (see Appendix A for the full set of equations). Eq. 2 describes the CGM measurement y, which is derived from $\mathbf{x}$ with the measurement model h and subject to an additive measurement noise $v^t \in \mathcal{N}(0, q^t)$, where q^t is the noise variance. We fix $q^t = 0.1521$ mmol^2/L^2 constant for all t, corresponding to a standard deviation equal to 5% of the ideal glucose value.

Figure 2 illustrates a high-level schema of the ODE system $\mathbf{F}$. The *gut absorption* subsystem [37] uses a chain of two compartments, G_1 and G_2 (mmol), to describe digestion of ingested CHO, given by the uncertainty parameter D_G^t.

The *glucose kinetics* subsystem describes the glucose masses in the accessible (where BG measurements are made) and non-accessible compartments, respectively through variables Q_1 and Q_2 (mmol). BG concentration, G (mmol/L), is the main variable we aim to control, and is derived from Q_1 as $G(t) = Q_1(t)/V_G$, where V_G is the glucose distribution volume. Variable C is the glucose concentration in the interstitial fluid, which has a delayed response w.r.t. the concentration in the blood G. C corresponds to the glucose detected by the CGM sensor and thus, the measurement function h of Eq. 2 maps the state vector $\mathbf{x}(t)$ to $C(t)$.

The *insulin kinetics* subsystem models the absorption of the fast-acting insulin ι^t, i.e. our control input (in mU/min), and its transport through compartments Q_{1a}, Q_{1b}, Q_{2i} and Q_3 (in mU) [36]. This model assumes a slow insulin absorption pathway consisting of compartments Q_{1a} (subcutaneous insulin mass) and Q_{2i} (non-accessible insulin), and a fast pathway that includes only Q_{1b} (subcutaneous). K represents the proportion in which the input insulin ι^t is distributed into the two pathways. Q_3 is the plasma insulin mass, from
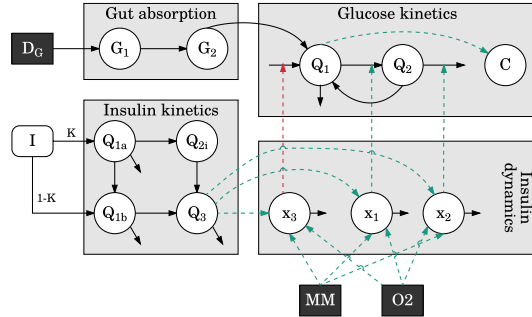

Fig. 2: Schema of the gluco-regulatory ODE system and its four main subsystems. White circles: ODE variables; black boxes: uncertainty parameters; white rounded box: insulin input; solid black arrows: flows of glucose or insulin; dashed green/red arrows: positive/negative interactions between variables.

which we derive the plasma insulin concentration I (mU/L) as $I(t) = Q_3(t)/V_I$, where V_I is the insulin distribution volume.

The *insulin dynamics* subsystem defines the effects of insulin on blood glucose through variables x_1, x_2, x_3. Variable x_1 (min^{-1}) promotes glucose distribution; x_2 (min^{-1}) promotes glucose disposal ; and x_3 (unitless) inhibits endogenous glucose production. The overall subsystem decrease blood glucose masses Q_1 and Q_2 and in turn, BG concentration G. Plasma insulin levels I directly increase x_1, x_2, x_3. Uncertainty parameters MM^t (active muscular mass) and $O2^t$ (target workload in terms of oxygen consumption) increase x_1, x_2, x_3 indirectly,

through state variables UA (mg/min) and $O2_m$ (unitless), not shown in the figure. They characterize physical activity and describe, respectively, the glucose uptake due to active muscular tissue and the actual percentage of maximum oxygen consumption.

Initial conditions: The initial state of the system is derived at a steady-state BG level of 7.8 mmol/L [31], assuming no meal and exercise. We use a nonlinear equation solver (MATLAB's `fsolve`) to find $\mathbf{x}(0)$ and the basal insulin level $\bar{\iota}$ such that $\dot{\mathbf{x}}(0) = F\left(\mathbf{x}(0), \bar{\iota}, \mathbf{u}^0\right) = \mathbf{0}$ (see Eq. 1), where the uncertainty parameters $\mathbf{u}^0$ are given by $D_G^0 = 0$, $MM^0 = 0$ and $O2^0 = 8$ (oxygen consumption at rest). Following [13], we further assess the physiologic feasibility of the initial conditions by checking that: 1) in absence of insulin, steady-state BG is above 300 mg/dL, and 2) delivery of high-dose insulin (15 U/h) results in a steady-state BG below 100 mg/dL.

4 Robust MPC

Since we want to optimize the BG profile against worst-case realizations of the uncertainty parameters, at each time step t, the robust MPC computes the insulin infusion ι^t as the solution of the following non-linear minimax optimization problem:

$$\min_{\iota^t, \ldots, \iota^{t+N_c-1}} \max_{\mathbf{u}^t, \ldots, \mathbf{u}^{t+N_p-1}} \sum_{k=1}^{N_p} d(\tilde{\mathbf{x}}(t+k)) + \beta \cdot \sum_{k=0}^{N_c-1} (\Delta\iota^{t+k})^2 \tag{3}$$

$$\text{subject to: } \iota^{t+k} \in D_\iota \qquad (k = 0, \ldots, N_c - 1) \tag{4}$$

$$\iota^{t+k} = \bar{\iota} \qquad (k = N_c, \ldots, N_p - 1) \tag{5}$$

$$\mathbf{u}^{t+k} \in \mathcal{U}^{t+k} \qquad (k = 0, \ldots, N_p - 1) \tag{6}$$

$$\tilde{\mathbf{x}}(t) = \hat{\mathbf{x}}(t) \tag{7}$$

$$\dot{\tilde{\mathbf{x}}}(t+k) = F(\tilde{\mathbf{x}}(t+k), \iota^{t+k}, \mathbf{u}^{t+k}) \qquad (k = 0, \ldots, N_p - 1) \tag{8}$$

where N_c and N_p are the control and prediction horizon (in minutes), respectively; constraint (4) states that the control input ι must belong to some set D_ι of admissible insulin infusion rates; through (5), we impose that ι is fixed to the basal insulin rate $\bar{\iota}$ outside the control horizon; (6) states that, at any time point $t + k$ in the prediction horizon, uncertainty parameters $\mathbf{u}^{t+k}$ must belong to the corresponding uncertainty sets $\mathcal{U}^{t+k}$; constraint (7) and (8) restrict how the robust MPC computes the predicted state vector $\tilde{\mathbf{x}}$: for the initial state, it uses the estimated plant state at time t, $\hat{\mathbf{x}}(t)$, while following states are predicted using the same plant model (see Equation 1). We set control and prediction horizons to $N_c = 100$ min and $N_p = 150$ min, respectively, as opposed to [28] where $N_c = 20$ and $N_p = 200$: preliminary experiments suggested that large N_p values and small N_c values cause excessive insulin therapy and hypoglycemia.

We design the cost function so as to optimize the following two objectives:

1. Minimize the sum of squared distances between the predicted BG level $\tilde{\mathbf{x}}_G(t+k)$ and a target trajectory $R(t+k)$:
$$d(\tilde{\mathbf{x}}(t+k)) = \gamma(t+k) \cdot (\tilde{\mathbf{x}}_G(t+k) - R(t+k))^2 \tag{9}$$

where $\gamma(t + k) = \gamma$ if $\tilde{\mathbf{x}}_G(t + k) < R(t + k)$ and 1 otherwise. (Remind that $\mathbf{x}_G(t) = G(t) = Q_1(t)/V_G$ in the glucose kinetics subsystem) Parameter $\gamma \geq 1$ allows defining asymmetric cost functions where predicted BG values below the target are penalized more than those above the target. Glucose control is naturally asymmetric given that hypoglycemia leads to more severe consequences than (temporary) hyperglycemia, and, as shown in [7], asymmetric costs effectively contribute avoiding hypoglycemia.

2. Minimize step-wise changes in the control input $(\Delta\iota^{t+k})^2$, where $\Delta\iota^{t+k} = \iota^{t+k} - \iota^{t+k-1}$, and ι^{t-1} corresponds to the control input in the previous iteration, or to the basal insulin rate $\bar{\iota}$ if $t = 0$.

In our setup, we fix the target trajectory to $R(t + k) = 7.8$ mmol/L for all time instants and set penalty β to $1/50$. We set the asymmetric cost penalty to $\gamma = 2$, after experimenting with different values (see Appendix D).

Optimization algorithm: We solve problem (3) using non-linear optimization techniques, where, for a fixed control strategy $\iota^t, \ldots, \iota^{t+N_c-1}$, the objective function value is given in turn as the result of maximizing the objective function over the uncertainty parameters (and with fixed $\iota^t, \ldots, \iota^{t+N_c-1}$). To solve both minimization and maximization problems, we use MATLAB's `fmincon`. To reduce the computational cost of this optimization method, we decrease the number of decision variables by assuming that, in the prediction model, control inputs change with period 10 min, and uncertainty parameters with period 30 min.

Hybrid closed-loop (HCL) variant: To compare with our robust MPC approach, we develop a hybrid closed-loop insulin pumps where only basal insulin is automatically regulated and the patient is responsible for bolus insulin. This reduces to a MPC that has no knowledge of meals and exercise, and thus, approximates the behavior of a current state-the-art approved device that requires explicit meal announcement. In our settings, this is equivalent to fixing the uncertainty parameters to their default values at rest.

Then the optimization problem of the HCL controller reduces to:

$$\min_{\iota^t,\ldots,\iota^{t+N_c-1}} \sum_{k=1}^{N_p} d(\tilde{\mathbf{x}}(t + k)) + \beta \cdot \sum_{k=0}^{N_c-1} (\Delta\iota^{t+k})^2 \tag{10}$$

subject to $(4, 5, 7, 8)$ and $\mathbf{u}^{t+k} = (0, 0, 8) \quad (k = 0, \ldots, N_p - 1)$.

Note that the constraints on the insulin therapy are the same of the robust controller (4-5) meaning that the HCL controller is free to synthesize boluslike therapy profiles too. This will also serve as the baseline controller in the evaluation part of Section 5.

4.1 State estimation

This component allows to recover an estimate of the current state, which is used in the following iteration by the robust MPC as the initial state for its predictions (see Eq. 7). Following [8,27], we designed a moving-horizon state estimator (MHE) that works in a finite-horizon fashion similar to an MPC problem, and

allows estimating the current state starting from previous estimations and a bounded history of observed CGM measurements.

For an estimation window of size N, MHE is based on simulating a model of the plant from time $t - N$ to t and aims at finding the model trajectory $\mathbf{x}(t - N), \ldots \mathbf{x}(t)$ that minimizes the discrepancies between simulated and estimated states, and between simulated and measured outputs (CGM). Then, $\hat{\mathbf{x}}(t)$ is chosen as the final state of the optimal trajectory.

Crucially, our estimator also works as a meal and physical activity detector [3, 19, 34]: in addition to the plant state, we compute the most likely sequence of uncertainty parameters $\mathbf{u}^{t-N}, \ldots, \mathbf{u}^t$, corresponding to decision variables in our optimization problem as they are inputs of the model. The MHE problem boils down to the following non-linear optimization problem:

$$\min_{\mathbf{x}(t-N), \ldots \mathbf{x}(t), \mathbf{u}^{t-N}, \ldots, \mathbf{u}^t} \mu \cdot \|\mathbf{x}(t-N) - \hat{\mathbf{x}}(t-N)\|^2 + \sum_{k=0}^{N-1} \frac{\|v^{t-k}\|^2}{q^{t-k}} \tag{11}$$

$$\text{subject to: } v^{t-k} = y(t-k) - h(\mathbf{x}(t-k)) \qquad (k = N-1, \ldots, 0) \tag{12}$$

$$\dot{\mathbf{x}}(t-k) = F(\mathbf{x}(t-k), \iota^{t-k}, \mathbf{u}^{t-k}) \qquad (k = N, \ldots, 0) \tag{13}$$

$$\mathbf{u}^{t-k} \in \mathcal{U}^{t-k} \qquad (k = N, \ldots, 0) \tag{14}$$

where (12) defines the measurement discrepancy v^{t-k} at time $t - k$ as the difference between the measured and simulated output, $y(t - k)$ and $h(\mathbf{x}(t - k))$, respectively (see also Eq. 2); and (13) states that $\mathbf{x}$ evolves according to the same ODE model of the plant, with ι^{t-k} being the insulin input previously computed by the robust MPC. We remark that data-driven uncertainty sets play an important role also in state estimation, since they constrain the domain of the corresponding estimated uncertainty parameters, as per (14). The problem is solved using MATLAB's `fmincon` non-linear solver.

The first addend of the cost function penalizes the discrepancy between the initial state of the simulated trajectory and the corresponding state estimation, where $\mu > 0$ is a weighting factor. The second addend penalizes measurement discrepancies, weighted by the inverse of the measurement noise variance q^{t-k} (see Eq. 2). In the original formulation of the MHE [8, 27], the cost function includes discrepancies for all the states in the trajectory. Our simplification comes from the fact that we do not consider random noise in the model (but only in the measurements), and thus, the trajectory $\mathbf{x}(t - N), \ldots, \mathbf{x}(t)$ is fully determined by the initial state $\mathbf{x}(t - N)$ and by the uncertainty parameters $\mathbf{u}^{t-N}, \ldots, \mathbf{u}^t$. Further, this greatly improves computational efficiency because variables $\mathbf{x}(t-N+1), \ldots, \mathbf{x}(t)$ are strictly constrained by the ODE in Eq. (13). In practice, this means that the decision variables reduce to $\mathbf{x}(t-N), \mathbf{u}^{t-N}, \ldots, \mathbf{u}^t$.

The MHE has an important probabilistic interpretation: when $N = t$ (unbounded horizon), the MHE problem corresponds to maximizing the joint probability for the trajectory of states $\mathbf{x}(t - N), \ldots, \mathbf{x}(t)$ given the measurements $y(t - N), \ldots, y(t)$ [27].

4.2 Building data-driven uncertainty sets

In this section, we describe how to build the uncertainty sets used within the robust MPC and the state estimator to restrict the domain of the admissible meal and exercise parameters. We apply the approach of [1] where the authors present a general schema for designing uncertainty sets from data for robust optimization (of which robust MPC is an instance). The key idea is to define an uncertainty set that captures possible realizations of the uncertain parameters and then optimize against worst-case realizations within this set. Importantly, this method requires no information about the underlying distribution of the parameters and provides a probabilistic guarantee (an upper bound) on the likelihood that the true realized cost is higher than the optimal 'worst-case' cost computed by the robust controller.

Let us characterize an uncertainty set $\mathcal{U}$ by means of a so-called robust constraint $f(\mathbf{u}, \mathbf{x}) \leq 0$, where $\mathbf{u}$ is the uncertainty parameter and $\mathbf{x}$ is the optimization variable, corresponding in our case to the state vector plus insulin input. Recall that the true distribution $\mathbb{P}^*$ of $\mathbf{u}$ is unknown. Given confidence level $\epsilon > 0$, $\mathcal{U}$ should satisfy two conditions: (1) the robust constraint f is computationally tractable. (2) $\mathcal{U}$ *implies a probabilistic guarantee for* $\mathbb{P}^*$ *at level* ϵ, that is, for any solution $\mathbf{x}^* \in \mathbb{R}^k$ and for any function $f(\mathbf{u}, \mathbf{x})$ concave in $\mathbf{u}$ for all $\mathbf{x}$,

$$\text{if } f(\mathbf{u}, \mathbf{x}^*) \leq 0 \ \forall \mathbf{u} \in \mathcal{U}, \text{then } \mathbb{P}^*(f(\mathbf{u}, \mathbf{x}^*) \leq 0) \geq 1 - \epsilon.$$

The data-driven schema we follow is based on sampling a set of data points $\mathcal{S}$ i.i.d. from the true distribution $\mathbb{P}^*$ and uses hypothesis testing to construct the uncertainty sets with such guarantees. In particular, for confidence level $\alpha < 1$, the schema employs the corresponding $(1-\alpha)$ confidence region to build $\mathcal{U}$. With the proper construction, the following theorem from [1, Sect. 3.2] holds.

Theorem 1. *With probability at least $1 - \alpha$ with respect to the sampling, the resulting set $\mathcal{U}(\mathcal{S}, \epsilon, \alpha)$ implies a probabilistic guarantee at least ϵ for $\mathbb{P}^*$.*

In [1], the authors show how different uncertainty sets are built depending on the assumptions about $\mathbb{P}^*$, and, in turn, on the suitable statistical test. In this work we consider box sets (i.e. multi-dimensional intervals), which make no assumptions on $\mathbb{P}^*$ and are suitable for data with missing values. The assumptions and the full construction are described in Appendix B. The application of other types of uncertainty sets, able for instance to capture temporal dependencies and correlation between meals and exercise, is in our future plans.

To shrink the size of uncertainty set, we employ the following two strategies: 1) prior to set construction, we classify the input data and partition it into a number of clusters so as to obtain tighter sets and more customized, patient-specific control strategies. 2) based on Algorithm 1 of [1], we use bootstrapping [5] to approximate the threshold of the test statistics, by estimating the sampling distribution of the statistics through re-sampling with replacement.

We remark that the construction of uncertainty sets is performed off-line and thus has no computational footprint on the robust controller.

5 Results and Discussion

We evaluate our robust control algorithm through a number of experiments for simulating: intake of a single meal (Section 5.1), exercise (Section 5.2), one-day meal intake scenario with patient behavior learned from population-wide survey data (Section 5.3), and two-day scenario with irregular meal timing and unusually high CHO intake (Section 5.4). Section 5.5 is dedicated to the analysis of state estimation. For each experiment, we compare the robust controller with the non-robust, hybrid closed-loop (HCL) variant introduced in Section 4. We also report the ideal performance by running a so-called *perfect controller*, that can access both the full plant state (i.e. does not need state estimation) and the exact values of the uncertainty parameters in the plant.

Hardware and performance: We ran the experiments on a Windows 8 machine with an Intel Core i7 processor and 32GB of DDR3 memory. We used MATLAB version 2016b. With this configuration, the average time to compute the insulin therapy over all the experiments ranged from 4 to 18 seconds, which is well within the CGM measurement period of 5 minutes. This means that the controller works faster than real-time. Given the significant performance improvement of modern embedded and mobile devices, we expect our algorithm to perform similarly as well once deployed on such hardware platforms.

Performance indicators: To measure the efficacy of our robust controller design over multiple runs, we consider the following indicators:

- $t_{<3.9}$, $t_{3.9-11.1}$, $t_{>11.1}$: mean percentage of time spent in, respectively, hypoglycemia (BG $<$ 3.9 mmol/L), normal ranges (BG between 3.9 and 11.1), and hyperglycemia (BG $>$ 11.1). Clearly, we wish to maximize $t_{3.9-11.1}$ and minimize the other two indicators, keeping in mind that we can tolerate some temporary postpandrial hyperglycemia while hypoglycemia should be avoided as much as possible.
- $BG_{\min}$, $BG_{\max}$: average low BG level and peak BG level, respectively, in mmol/L. An effective robust controller should keep $BG_{\min}$ and $BG_{\max}$ as close as possible to the target BG level.
- $\sum \iota$: mean total non-basal insulin (in U). This indicator measures the amount of insulin injected by the controller in order to cover meals, and thus excludes the contribution of basal insulin.

To evaluate state estimation, we further consider indicators E_{D_G}, E_{MM}, E_{O2}, i.e. the mean absolute error between plant and estimated uncertain variable values, and E_{BG}, the mean absolute error between plant BG and estimated BG.

5.1 One-meal experiments

We consider 300-minute simulations comprising a single meal, and three different synthetic scenarios (illustrated in Figure 3 (a-c)), i.e. where meals are sampled from arbitrary distributions. For each scenario and controller, we collect results

for 50 repetitions. Details on the construction of uncertain sets from arbitrary distributions are given in Appendix C.

Scenario 1, meals as expected: in the uncertain plant, we assume a uniformly distributed meal with start time $t_s = \text{unif}(30, 90)$, total amount of CHO (grams) $\mathsf{CHO} = \text{unif}(42, 78)$ and meal duration fixed to 20 minutes, during which CHO ingestion happens at a constant rate. Given that uniform distributions have bounded support, we can build tight box-type uncertainty sets (i.e. intervals) that contain all possible realizations. This scenario allows us evaluating the adequacy of the controller when the plant behaves according to a known distribution, in other words, when we have accurate information for building uncertainty sets.

Scenario 2, outliers: in this case, random meals behave as statistical outliers, i.e. they are constantly distant from the expected value of the underlying distribution. To this purpose, we build the uncertainty sets under the assumption that meals are normally distributed with parameters $t_s = \mathcal{N}(60, 15)$ and $\mathsf{CHO} = \mathcal{N}(60, 9)$. The uncertainty sets are built so as to cover all possible realizations with z-score between -3 and 3 (i.e. between -3 S.D. and +3 S.D. around the mean). However, to reproduce outliers, meals in the uncertain plant are sampled from the tails of the distributions (z-scores in $[-4, -3]$ and $[3, 4]$).

Scenario 3, late meals: here we consider the same settings as in Scenario 1, but with each random meal delayed of one hour. This models the situation where the controller has wrong information about the meal schedule, since it expects the meal to start, on the average, one hour earlier.
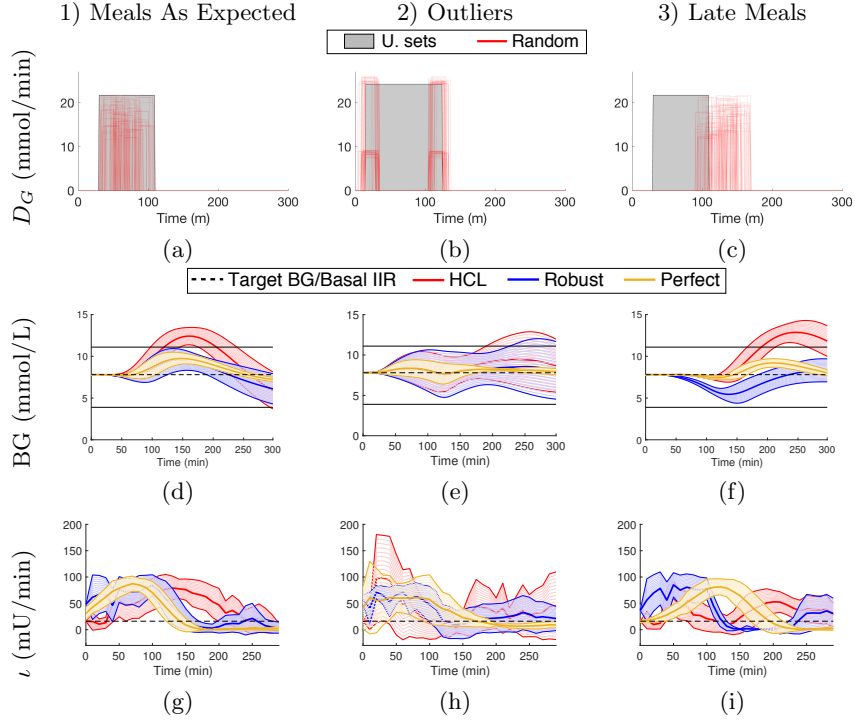
Results in Figure 3 show that our robust controller attains very good performance, closely following the ideal behavior of the perfect controller in the first and third scenarios, where the virtual patient stays in normal ranges for >97% of the time. In the outliers scenario, we register some postprandial hyperglycemia, because this scenario is characterized by frequent high CHO intake. Overall, the robust controller is able to limit the time spent in hypoglycemia below 1% and consistently outperforms the HCL controller, staying in normal BG ranges for 3% to 31% more. Full statistics are reported in Table 4 of the Appendix.

5.2 Regulation during exercise

We evaluate the behavior of the robust controller when the virtual patient is involved in physical activity, which, contrarily to meals, contributes to decreasing BG levels. We simulate a two-legged exercise consisting of two phases:

1. **Moderate activity**, with start time $t_s = \text{unif}(40, 80)$, duration $d = \text{unif}(24, 36)$, active muscular mass $MM = \text{unif}(0.15, 0.35)$, and oxygen consumption $O2 = \text{unif}(45, 75)$; followed by
2. **Light activity**, where parameters stay as in the previous phase except for $02 = \text{unif}(15, 45)$.

Results, reported in Figure 4, evidence that both the robust and the HCL controller can maintain BG within very tight ranges, as confirmed by the $BG_{\min}$

Fig. 3: One-meal, 300-minute experiments (50 repetitions). **Top:** uncertainty sets and random realizations of parameter D_G (rate of CHO ingestion). **Middle:** BG profiles (with solid black lines indicating the normal BG range). **Bottom:** synthetized insulin therapies. Thick solid lines indicate average BG/insulin values, and are surrounded by an area spanning $\pm$ 1 S.D. In the table, we highlight in bold the best value of each index between the robust and the HCL controllers.

(a) *MM*   (b) *O2*   (c) BG   (d) IIR

	$t_{<3.9}$	$t_{3.9-11.1}$	$t_{>11.1}$	$BG_{\min}$	$BG_{\max}$	E_{MM}	E_{O2}	E_{BG}	$\sum \iota$
Perfect	0%	100%	0%	7.64	7.92	N.A.	N.A.	N.A.	-0.29
HCL	0%	100%	0%	7.13	**7.88**	0.05	6.97%	0.42	-0.26
Robust	0%	100%	0%	**7.5**	7.98	0.05	**5.04%**	0.42	-0.22

Fig. 4: Regulation during random exercise (50 repetitions). a) and b) show uncertainty sets and realizations for active muscular mass (*MM*) and oxygen consumption (*O2*). Legend is as in Figure 3.

and $BG_{\max}$ indicators. BG profiles are almost indistinguishable from the ideal ones (i.e. those of the perfect controller) and for 100% of the times within healthy ranges. Note that both controllers correctly reduce the insulin therapy below the basal level to counteract the decrease of BG due to exercise. Hence, the negative values of $\sum \iota$. The main difference is that the robust controller, due to the superior predictive capabilities, is more timely in cutting insulin therapy than the HCL controller, leading to a smaller excursion from the target BG value.

Resalat et al. [28] realized a similar scenario to test their dual-hormone MPC (300-minute simulation with a 45-minute exercise at fixed *O2* = 60 and *MM* = 0.8). While we use their same plant model, their MPC design is different in two ways: it can regulate both insulin and glucagon (to prevent hypoglycemia) and is not robust, meaning that exercise must be announced in order for the controller to make correct predictions. Despite that, however, their evaluation resulted into some episodes of hypoglycemia and hyperglycemia, while our controller is able to keep BG for 100% of the time in healthy ranges without meal announcements.

5.3 One-day experiments using NHANES survey data

We test our robust controller with real population data from the CDC's National Health and Nutrition Examination Survey (NHANES) database.[4] We consider the 2013 survey, comprising 8,611 participants, and classify the participants into 10 groups using k-means clustering. In this experiment, we selected the cluster whose meal patterns are characterized by a CHO-rich breakfast at around 9am, as visible in the uncertainty set of Figure 5(a). From this cluster, we extract meal information to parameterize the virtual patient and build the uncertainty sets as explained in Section 4.2 (choosing $\alpha = 0.2$ and $\epsilon = 0.2$). Due to the poor quality of physical activity data in NHANES, we generated one random exercise event

---

[4] https://www.cdc.gov/nchs/nhanes/

for each patient. Details on the other clusters and on extraction and processing of data are given in Appendix E.

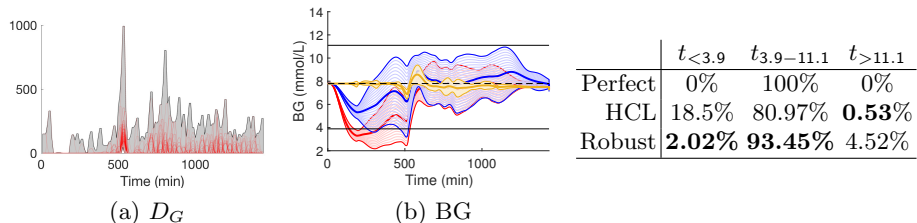|	$t_{<3.9}$	$t_{3.9-11.1}$	$t_{>11.1}$
Perfect	0%	100%	0%
HCL	18.5%	80.97%	**0.53**%
Robust	**2.02%**	**93.45%**	4.52%

(a) D_G (b) BG

Fig. 5: BG regulation for virtual patient learned from NHANES database (20 repetitions). Legend is as in Figure 3.

Results were obtained with 20 repetitions and are reported in Figure 5. In this experiment, our robust controller has a close-to-ideal performance, with $>93\%$ of time spent in normal BG ranges. It outperforms the HCL controller, which fails to predict the correct BG levels during sleep (time < 500 min), leading to excessive insulin therapy and to dangerous overnight hypoglycemia.

5.4 High carbohydrate intake scenario

We assess the behavior of the controller under irregular meal timing and unusually high CHO intake, following the protocol of [31], reported in Table 1. In this protocol, no physical activity is considered. Uncertainty sets were derived following the same construction of the one-meal experiments. Results, obtained with 50 repetitions, are shown in Figure 6.

Our robust controller resulted in 87.56% of time within healthy BG ranges, against the 80.6% of the HCL controller. Despite hypoglycemia amounts to 3.11% of the total time, it corresponds only to minor episodes, as visible by the standard deviation intervals in the plot and by the average minimum BG ($BG_{\min} = 3.84$ mmol/L) that falls only slightly below the hypoglycemic level (3.9 mmol/L).

We also report that our approach outperforms the robust LPV approach of Jacobs et al. [31], discussed in the

	Chance of occurrence	CHO (g)	Time of day (h)
Breakfast	100%	40-60	6:00-10:00
Snack 1	50%	5-25	8:00-11:00
Lunch	100%	70-110	11:00-15:00
Snack 2	50%	5-25	15:00-18:00
Dinner	100%	55-75	18:00-22:00
Snack 3	50%	5-15	22:00-00:00

Table 1: High carbohydrate intake simulation parameters of [31]. Meals in the plant are sampled uniformly based on the above intervals and probabilities.

related work (Section 6). With the same plant model and scenario, they obtain $t_{<3.9} = 0\%$, $t_{3.9-11.1} = 83.08\%$ and $t_{>11.1} = 16.92\%$, meaning that our robust controller stays $> 4\%$ of the time longer in healthy ranges. We remark that the results of Jacobs et al. are as reported in [31], and were not obtained by running their controller on our machine.

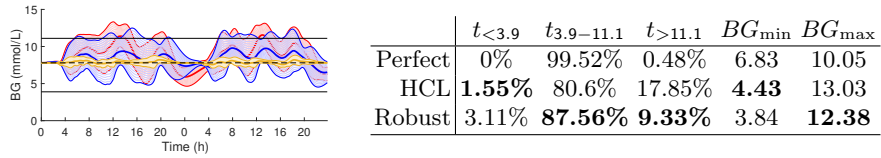|	$t_{<3.9}$	$t_{3.9-11.1}$	$t_{>11.1}$	$BG_{\min}$	$BG_{\max}$
Perfect	0%	99.52%	0.48%	6.83	10.05
HCL	**1.55%**	80.6%	17.85%	**4.43**	13.03
Robust	3.11%	**87.56%**	**9.33%**	3.84	**12.38**

Fig. 6: BG profile (left) and performance indicators (right) for the high carbo-hydrate intake scenario (50 repetitions). Legend is as in Fig. 3.

5.5 Evaluation of state estimator

We chose an MHE scheme for state estimation (see Section 4.1) after having evaluated *extended Kalman filters (EKF)* [35], which are commonly employed for the state estimation of non-linear systems. MHE overcomes some of the typical problems of Kalman filtering, namely, the inability to accurately incorporate state constraints (e.g. non-negative concentrations); poor use of the nonlinear model [8]; and estimations that often diverge, or converge to wrong state predictions [26,32]. Moreover, "off-the-shelf" Kalman filters only support zero-mean disturbances (white Gaussian noise), thus preventing the estimation of random meal and exercise episodes.
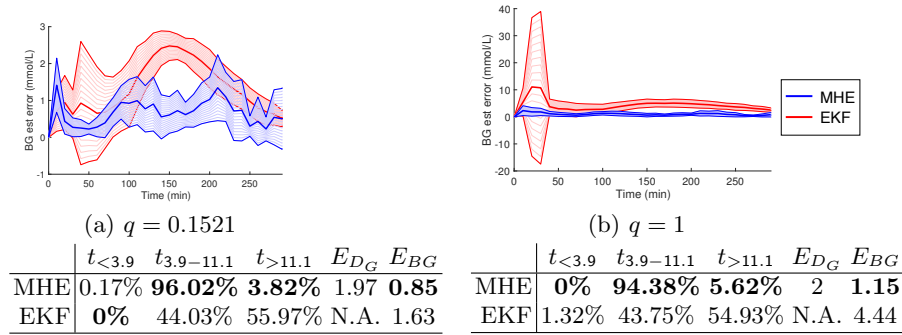

(a) $q = 0.1521$

(b) $q = 1$

	$t_{<3.9}$	$t_{3.9-11.1}$	$t_{>11.1}$	E_{D_G}	E_{BG}
MHE	0.17%	**96.02%**	**3.82%**	1.97	**0.85**
EKF	**0%**	44.03%	55.97%	N.A.	1.63

	$t_{<3.9}$	$t_{3.9-11.1}$	$t_{>11.1}$	E_{D_G}	E_{BG}
MHE	**0%**	**94.38%**	**5.62%**	2	**1.15**
EKF	1.32%	43.75%	54.93%	N.A.	4.44

Fig. 7: BG estimation error of Moving Horizon Estimator (MHE) and Extended Kalman Filter (EKF), at different sensing noise variances q (20 repetitions).

We compare the state estimation accuracy between our MHE design and an EKF scheme, according to the *meals as expected* scenario (see Section 5.1). In the EKF, to predict the state estimate at time t, $\hat{\mathbf{x}}(t)$, we use the model of Section 3 as follows: $\dot{\hat{\mathbf{x}}}(t) = F(\hat{\mathbf{x}}(t), \iota^t, \mathrm{E}[\mathbf{u}^t])$, where ι^t is the (known) insulin input and uncertainty parameters $\mathbf{u}^t$ are replaced with their expected value $\mathrm{E}[\mathbf{u}^t]$[5].

To evaluate if the estimators are robust with respect to sensing noise, we tested two different variance values for the sensing noise: $q = 0.1521$ (default) and $q = 1$ (increased noise). As visible in Figure 7, the MHE outperforms the EKF, with a consistently lower state estimation error. The imprecise state predictions of the EKF lead to a wrong behavior of the overall closed-loop system, with

---

[5] The real expected value of $\mathbf{u}^t$ is known because here we work with arbitrary distributions.

only $\sim 44\%$ of time spent within normal BG ranges, against $> 94\%$ of the MHE. Unlike the EKF, the MHE is robust to sensing noise, with an average estimation error (column E_{BG}) that stays relatively constant from $q = 0.1521$ to $q = 1$.

6 Related Work

Robust control methods are able to minimize the impact of input disturbances on the plant, and thus have the potential to enable fully closed-loop insulin delivery. Earlier approaches [14, 25, 29] are based on the theory of H_∞ control [30], a technique where the robust controller is synthesized offline as the result of an optimization problem that minimizes the worst-case closed-loop performance of the controlled system. However, H_∞ control only supports linear systems, thus requiring linearization of physiological, non-linear gluco-regulatory models, with inevitable loss of accuracy.

Kovacs et al. [15, 16, 31] introduce robust linear parameter varying (LPV) control, a technique that consists on deriving a piecewise-linear approximation of the non-linear plant and synthesizing a robust H_∞ controller for each linear region, and thus, improves on previous H_∞ approaches. In Section 5.4, we have compared our robust controller to [31], showing that our algorithm is able keep glucose levels within normal ranges for a longer time.

In contrast to the above techniques, our data-driven robust MPC supports not just meal disturbances, but also physical activity, and is based on non-linear optimization, meaning that it does not require to approximate the system dynamics, leading to more precise predictions. Further, MPC is known to be superior for individualized control strategies [4, 23, 33], even though is computationally more demanding than offline techniques like H_∞ or LPV control, but still feasible within the update periods typical of the artificial pancreas (5-10 minutes). Finally, our data-driven scheme supports continuous learning of the patient's behavior, thus enabling the synthesis of robust and adaptive insulin therapies. On the other hand, H_∞ and LPV controllers are offline and need to be synthesized from scratch in order to adapt to changing patient conditions.

A simpler strategy employed in a number of AP studies, see e.g. [12, 18], is that of PID control, where the control input results from applying tunable gains to the error between the system output and a desired setpoint. Synthesizing these gains to obtain robustness guarantees, however, becomes difficult for systems with nonlinear and probabilistic dynamics.

7 Conclusions

Thanks to modern wearable sensing devices, patient-specific data about meals and physical activity is becoming more readily available, making it possible to offer significantly enhanced personalized medical therapy for type 1 diabetes. Accordingly, we presented a data-driven robust MPC framework for T1D that leverages meal and exercise data to provide enhanced control and state estimation. Our results show that learning a patient's behavior from data is key

to achieving fully closed-loop therapy that does not require meal and exercise announcements.

References

1. D. Bertsimas, V. Gupta, and N. Kallus. Data-driven robust optimization. *arXiv preprint arXiv:1401.0212*, 2013.
2. Centers for Disease Control and Prevention. National diabetes statistics report: estimates of diabetes and its burden in the United States, 2014. *Atlanta, GA: US Department of Health and Human Services*, 2014.
3. E. Dassau, B. W. Bequette, B. A. Buckingham, and F. J. Doyle. Detection of a meal using continuous glucose monitoring. *Diabetes care*, 31(2):295–300, 2008.
4. G. De Nicolao, L. Magni, C. Dalla Man, and C. Cobelli. Modeling and control of diabetes: Towards the artificial pancreas. *IFAC Proceedings Volumes*, 44(1):7092–7101, 2011.
5. B. Efron and R. J. Tibshirani. *An introduction to the bootstrap*. CRC press, 1994.
6. R. Gondhalekar, E. Dassau, and F. J. Doyle. Moving-horizon-like state estimation via continuous glucose monitor feedback in MPC of an artificial pancreas for type 1 diabetes. In *Decision and Control (CDC), 2014 IEEE 53rd Annual Conference on*, pages 310–315. IEEE, 2014.
7. R. Gondhalekar, E. Dassau, and F. J. Doyle. Periodic zone-MPC with asymmetric costs for outpatient-ready safety of an artificial pancreas to treat type 1 diabetes. *Automatica*, 71:237–246, 2016.
8. E. L. Haseltine and J. B. Rawlings. Critical evaluation of extended Kalman filtering and moving-horizon estimation. *Industrial & engineering chemistry research*, 44(8):2451–2460, 2005.
9. M. Hernandez-Ordonez and D. Campos-Delgado. An extension to the compartmental model of type 1 diabetic patients to reproduce exercise periods with glycogen depletion and replenishment. *Journal of biomechanics*, 41(4):744–752, 2008.
10. R. Hovorka. Closed-loop insulin delivery: from bench to clinical practice. *Nature Reviews Endocrinology*, 7(7):385–395, 2011.
11. R. Hovorka et al. Nonlinear model predictive control of glucose concentration in subjects with type 1 diabetes. *Physiological measurement*, 25(4):905, 2004.
12. L. M. Huyett, E. Dassau, H. C. Zisser, and F. J. Doyle III. Design and evaluation of a robust PID controller for a fully implantable artificial pancreas. *Industrial & engineering chemistry research*, 54(42):10311–10321, 2015.
13. P. G. Jacobs et al. Incorporating an exercise detection, grading, and hormone dosing algorithm into the artificial pancreas using accelerometry and heart rate. *Journal of diabetes science and technology*, page 1932296815609371, 2015.
14. K. H. Kienitz and T. Yoneyama. A robust controller for insulin pumps based on H-infinity theory. *IEEE Transactions on Biomedical Engineering*, 40(11):1133–1137, 1993.
15. L. Kovács, B. Benyó, J. Bokor, and Z. Benyó. Induced L2-norm minimization of glucose-insulin system for Type I diabetic patients. *Computer Methods and Programs in Biomedicine*, 102(2):105–118, 2011.

16. L. Kovács, P. Szalay, Z. Almássy, and L. Barkai. Applicability results of a nonlinear model-based robust blood glucose control algorithm. *Journal of diabetes science and technology*, 7(3):708–716, 2013.

17. B. Kovatchev et al. Feasibility of long-term closed-loop control: a multicenter 6-month trial of 24/7 automated insulin delivery. *Diabetes Technology & Therapeutics*, 2017.

18. S. Laxminarayan, J. Reifman, and G. M. Steil. Use of a food and drug administration-approved type 1 diabetes mellitus simulator to evaluate and optimize a proportional-integral-derivative controller. *Journal of diabetes science and technology*, 6(6):1401–1412, 2012.

19. H. Lee, B. A. Buckingham, D. M. Wilson, and B. W. Bequette. A closed-loop artificial pancreas using model predictive control and a sliding meal size estimator. *Journal of diabetes science and technology*, 3(5):1082–1090, 2009.

20. J. J. Lee, R. Gondhalekar, and F. J. Doyle. Design of an artificial pancreas using zone model predictive control with a moving horizon state estimator. In *Decision and Control (CDC), 2014 IEEE 53rd Annual Conference on*, pages 6975–6980. IEEE, 2014.

21. P. J. Lenart and R. S. Parker. Modeling exercise effects in type i diabetic patients. *IFAC Proceedings Volumes*, 35(1):247–252, 2002.

22. T. T. Ly et al. Day and night closed-loop control using the integrated Medtronic hybrid closed-loop system in type 1 diabetes at diabetes camp. *Diabetes Care*, 38(7):1205–1211, 2015.

23. L. Magni et al. Model predictive control of glucose concentration in type I diabetic patients: An in silico trial. *Biomedical Signal Processing and Control*, 4(4):338–346, 2009.

24. F. Miao, S. Han, S. Lin, and G. J. Pappas. Robust taxi dispatch under model uncertainties. In *2015 54th IEEE Conference on Decision and Control (CDC)*, pages 2816–2821. IEEE, 2015.

25. R. S. Parker, F. J. Doyle, J. H. Ward, and N. A. Peppas. Robust H_∞ glucose control in diabetes using a physiological model. *AIChE Journal*, 46(12):2537–2549, 2000.

26. L. Perea, J. How, L. Breger, and P. Elosegui. Nonlinearity in sensor fusion: divergence issues in ekf, modified truncated gsf, and ukf. In *AIAA Guidance, Navigation and Control Conference and Exhibit*, page 6514, 2007.

27. C. V. Rao, J. B. Rawlings, and D. Q. Mayne. Constrained state estimation for nonlinear discrete-time systems: Stability and moving horizon approximations. *IEEE transactions on automatic control*, 48(2):246–258, 2003.

28. N. Resalat, J. El Youssef, R. Reddy, and P. G. Jacobs. Design of a dual-hormone model predictive control for artificial pancreas with exercise model. In *Engineering in Medicine and Biology Society (EMBC), 2016 IEEE 38th Annual International Conference of the*, pages 2270–2273. IEEE, 2016.

29. E. Ruiz-Velázquez, R. Femat, and D. Campos-Delgado. Blood glucose control for type I diabetes mellitus: a robust tracking H_∞ problem. *Control Engineering Practice*, 12(9):1179–1195, 2004.

30. A. A. Stoorvogel. *The H_∞ Control Problem: A State Space Approach*. Prentice Hall, 1992.

31. P. Szalay, G. Eigner, and L. A. Kovács. Linear matrix inequality-based robust controller design for type-1 diabetes model. *IFAC Proceedings Volumes*, 47(3):9247–9252, 2014.

32. R. Van Der Merwe. *Sigma-point Kalman filters for probabilistic inference in dynamic state-space models*. PhD thesis, Oregon Health & Science University, 2004.

33. Y. Wang, H. Zisser, E. Dassau, L. Jovanovič, and F. J. Doyle. Model predictive control with learning-type set-point: Application to artificial pancreatic β-cell. *AIChE Journal*, 56(6):1510–1518, 2010.

34. J. Weimer, S. Chen, A. Peleckis, M. R. Rickels, and I. Lee. Physiology-invariant meal detection for type 1 diabetes. *Diabetes Technology & Therapeutics*, 18(10):616–624, 2016.

35. G. Welch and G. Bishop. An Introduction to the Kalman Filter. Technical report, University of North Carolina at Chapel Hill, Chapel Hill, NC, USA, 1995.

36. M. E. Wilinska et al. Insulin kinetics in type-1 diabetes: continuous and bolus delivery of rapid acting insulin. *IEEE Transactions on Biomedical Engineering*, 52(1):3–12, 2005.

37. M. E. Wilinska et al. Simulation environment to evaluate closed-loop insulin delivery systems in type 1 diabetes. *Journal of diabetes science and technology*, 4(1):132–144, 2010.

38. S. Zavitsanou, A. Chakrabarty, E. Dassau, and F. J. Doyle. Embedded control in wearable medical devices: Application to the artificial pancreas. *Processes*, 4(4):35, 2016.

A   Gluco-regulatory ODE model

We describe the details of the ODE system used in our controller design, which consists of the following subsystems:

Glucose kinetics: describes the glucose masses in the accessible (where BG measurements are made) and non-accessible compartments, respectively through variables Q_1 and Q_2 (mmol) as follows:

$$\dot{Q}_1(t) = -F_{01c} - x_1 \cdot Q_1(t) + k_{12} \cdot Q_2(t) - F_R + U_g(t) + EGP_0 \cdot (1 - x_3(t)) \quad (15)$$
$$\dot{Q}_2(t) = x_1(t) \cdot Q_1(t) - k_{12} \cdot Q_2(t) - x_2(t) \cdot Q_2(t)$$

where F_{01c} and F_R (mmol min^{-1}) are the corrected non-insulin mediated glucose uptake and renal glucose clearance, respectively, derived as per [11]; x_1, x_2, x_3 describe the effect of insulin on glucose (see the *insulin dynamics* subsystem); U_g is the gut absorption rate (see the *gut absorption* subsystem); and EGP_0 (mmol min^{-1}) is the glucose production at a theoretical zero-insulin concentration. BG concentration, G (mmol L^{-1}), is derived from Q_1 as $G(t) = Q_1(t)/V_G$, where V_G is the glucose distribution volume. In our robust MPC controller (Section 4), G is the main state variable that we want to control.

Interstitial glucose: subcutaneous glucose concentration C (mmol/L) detected by the CGM sensor has a delayed response w.r.t. the blood concentration G, and is given by:

$$\dot{C}(t) = k_{a\_int} \cdot (G(t) - C(t)) \quad (16)$$

Therefore, the measurement function h of Eq. 2 maps the state vector at time t to $C(t)$.

Gut absorption: this subsystem uses a chain of two compartments, G_1 and G_2 (mmol), to model the absorption dynamics of ingested food (given by the uncertainty parameter D_G^t) [37]:

$$\dot{G}_1(t) = -G_1(t)/T_{\max} + A_g \cdot D_G^t, \quad \dot{G}_2(t) = (G_1(t) - G_2(t))/T_{\max} \qquad (17)$$

where A_g (unitless) is the CHO bio-availability, and $T_{\max}$ (mins) is the time of maximum appearance rate of glucose, computed as per [37]. The gut absorption rate $U_g(t) = G_2(t)/T_{\max}$ (mmol min^{-1}) characterizes the flow into the plasma glucose compartment Q_1 (see Eq. 15).

Insulin kinetics: models the absorption of the fast-acting insulin ι^t (i.e. our control input, in mU min^{-1}) and its transport through compartments Q_{1a}, Q_{1b}, Q_{2i} and Q_3 (in mU) [36]:

$$\dot{Q}_{1a}(t) = K \cdot \iota^t - k_{ia1} \cdot Q_{1a}(t) - \frac{V_{\max,LD} \cdot Q_{1a}(t)}{k_{m,LD} + Q_{1a}(t)} \qquad (18)$$

$$\dot{Q}_{1b}(t) = (1 - K) \cdot \iota^t - k_{ia2} \cdot Q_{1b}(t) - \frac{V_{\max,LD} \cdot Q_{1b}(t)}{k_{m,LD} + Q_{1b}(t)}$$

$$\dot{Q}_{2i}(t) = k_{ia1} \cdot Q_{1a}(t) - k_{ia1} \cdot Q_{2i}(t)$$

$$\dot{Q}_3(t) = k_{ia1} \cdot Q_{2i}(t) + k_{ia2} \cdot Q_{1b}(t) - k_e \cdot Q_3(t)$$

This model assumes a slow insulin absorption pathway consisting of compartments Q_{1a} (subcutaneous insulin mass) and Q_{2i} (non-accessible insulin), and a fast pathway that includes compartment Q_{1b} (subcutaneous). K represents the proportion in which the input insulin ι^t is distributed into the two pathways. Q_3 is the plasma insulin mass. The plasma insulin concentration I (mU L^{-1}) is derived as $I(t) = Q_3(t)/V_I$, where V_I is the insulin distribution volume. $V_{\max,LD}$ (mU min^{-1}) and $k_{m,LD}$ (mU) are the Michaelis-Menten constants characterizing local insulin degradation.

Insulin dynamics: defines the effects of insulin on glucose distribution with variable x_1 (min^{-1}), on glucose disposal with x_2 (min^{-1}), and on the endogenous glucose production x_3 (unitless):

$$\dot{x}_1(t) = k_{a1} \cdot (-x_1(t) + M_{PGU}(t) \cdot M_{PIU}(t) \cdot S_{IT} \cdot I(t)) \qquad (19)$$

$$\dot{x}_2(t) = k_{a2} \cdot (-x_2(t) + M_{PGU}(t) \cdot M_{PIU}(t) \cdot S_{ID} \cdot I(t))$$

$$\dot{x}_3(t) = k_{a3} \cdot (-x_3(t) + M_{HGP}(t) \cdot S_{IE} \cdot I(t))$$

where M_{PGU}, M_{PIU} and M_{HGP} (unitless) are factors depending on the patient's physical activity (described below).

Physical activity: consists of two state variables: the glucose uptake due to active muscular tissue UA (mg min^{-1}), and the experienced activity level, which is captured by the percentage of maximum oxygen consumption $O2_m$ (unitless):

$$\dot{UA}(t) = k_{UA} \cdot (\overline{UA}(t) - UA(t)), \quad \dot{O2}_m(t) = k_{O2} \cdot (O2_m(t) - O2^t) \qquad (20)$$

where $O2^t$ is the input uncertainty parameter describing the target workload, and $\overline{UA}(t) = f\left(O2_m(t)\right)$ is the steady-state value of UA which is computed as a function of $O2_m$, where f is estimated in [21] using quadratic regression.

The effects of exercise on peripheral glucose uptake (M_{PGU}), on peripheral insulin uptake (M_{PGU}), and on hepatic glucose production (M_{HPG}) are affected by UA and $O2_m$ as follows:

$$
\begin{aligned}
M_{PGU}(t) &= 1 + k_{PGU} \cdot UA(t) \cdot MM^t \\
M_{PIU}(t) &= 1 + k_{PIU} \cdot MM^t \\
M_{HPG}(t) &= 1 + k_{HPG} \cdot UA(t) \cdot MM^t
\end{aligned}
\tag{21}
$$

where MM^t is the uncertainty parameter for the active muscular mass.

B   Construction of uncertainty sets from data

We will describe the assumptions and the details of the construction for the box type uncertainty sets. We follow the notations similar in [1]. $\mathbf{u} \in \mathbb{R}^d$ denotes the random uncertainty vector and u_i denotes its components. $\mathbb{P}^*$ refers to the true and unobserved probability measure for $\mathbf{u}$. The set of sample data points $\mathcal{S} = \{\hat{\mathbf{u}}^1, \dots, \hat{\mathbf{u}}^S\}$ is constructed by drawing i.i.d. $S = |\mathcal{S}|$ times from $\mathbb{P}^*(\mathbf{u})$. Here, we do not need to assume the marginal distributions of $\mathbb{P}^*$ to be independent. That is consistent to the observation that the elements in uncertainty parameter $\mathbf{u}$ for artificial pancreas controller is correlated. Moreover, the box type is designed to be suitable for the case when the sample data contains many missing values or we are only able to collect samples asynchronously.

Box type The univariate hypothesis test for the $1 - \epsilon/d$ quantile in David and Nagaraja is extended to the multivariate case in [1]. Given $\bar{q}_{i,0}, \underline{q}_{i,0} \in \mathbb{R}, \forall i = 1, \dots, d,$

$$
\begin{aligned}
H_0 : &\inf\{v : \mathbb{P}(u_i \leq v) \geq 1 - \epsilon/d\} \geq \bar{q}_{i,0} \text{ and} \\
&\inf\{v : \mathbb{P}(-u_i \leq v) \geq 1 - \epsilon/d\} \geq \underline{q}_{i,0} \forall i = 1, \dots, d
\end{aligned}
$$

Assume that we have S random samples. The index s is defined as

$$
s = \min\left\{ k \in \mathbb{N} : \sum_{j=k}^{S} \binom{S}{j} (\frac{\epsilon}{d})^{S-j} (1 - \frac{\epsilon}{d})^j \leq \frac{\alpha_h}{2d} \right\}.
$$

For each component u_i of $\mathbf{u}$ and we re-order them in an increasing order $u_i^{(1)}, u_i^{(2)}, \dots, u_i^{(S)}$. So the test is rejected at level α_h if

$$
\hat{u}_i^{(s)} < \bar{q}_i \text{ or } -\hat{u}_i^{(S-s+1)} < \underline{q}_i
$$

Value		Unit	Ref	Description
Glucose Kinetics				
F_{01}	$0.0104 \cdot BW$	[mmol min^{-1}]	[13]	Non-insulin mediated glucose uptake
$F_{01,thr}$	4.5	[mmol L^{-1}]	[11]	Non-insulin mediated glucose uptake threshold
EGP_0	$0.0158 \cdot BW$	[mmol min^{-1}]	[13]	Endogenous glucose production extrapolated to zero insulin concentration
k_{12}	0.0793	[min^{-1}]	[13]	Inflow rate from non-accessible compartment
V_G	$0.1797 \cdot BW$	[L]	[13]	Glucose distribution volume
R_{thr}	9	[mmol L^{-1}]	[11]	Renal clearance threshold
R_{cl}	0.003	[min^{-1}]	[11]	Renal clearance rate
Insulin Kinetics				
K	0.7958	unitless	[13]	Proportion of insulin in slow compartment
k_{ia1}	0.0113	[min^{-1}]	[13]	Rate constant - slow insulin compartment
k_{ia2}	0.0197	[min^{-1}]	[13]	Rate constant - fast insulin compartment
k_e	0.1735	[min^{-1}]	[13]	Plasma insulin elimination rate
$V_{max,LD}$	2.9639	[mU min^{-1}]	[13]	Insulin max velocity of local degradation / saturation level
$k_{m,LD}$	47.5305	[mU]	[13]	Michaelis constant - insulin
Insulin Dynamics				
k_{a1}	0.007	[min^{-1}]	[13]	Rate of effect of remote insulin on glucose distribution/transport
k_{a2}	0.0331	[min^{-1}]	[13]	Rate of effect of remote insulin on glucose disposal
k_{a3}	0.0308	[min^{-1}]	[13]	Rate of effect of remote insulin on EGP suppression
S_{IT}	0.0046	[min^{-1} mU^{-1} L]	[13]	Insulin sensitivity on glucose distribution/transport
S_{ID}	0.0006	[min^{-1} mU^{-1} L]	[13]	Insulin sensitivity on glucose disposal
S_{IE}	0.0384	[mU^{-1} L]	[13]	Insulin sensitivity on EGP suppression
V_I	$0.1443 \cdot BW$	[L]	[13]	Insulin distribution volume
Gut absorption				
A_g	0.8121	[unitless]	[13]	Carbohydrate bio-availability of the ingested food (Proportion of absorbed carbs)
$U_g^\top$	$0.0275 \cdot BW$	[mmol min^{-1}]	[37]	Maximum glucose flux from the gut
$T_{max}^\perp$	48.8385	[mmol min^{-1}]	[13]	Lower bound for time-of-maximum appearance rate of glucose in the accessible compartment
Interstitial (sensor) glucose				
k_{a_int}	0.025	[min^{-1}]	[37]	Peripheral glucose uptake factor
Exercise				
k_{UA}	$\frac{1}{30}$	[min^{-1}]	[13]	Rate affecting the dynamics of peripheral glucose uptake during exercise
k_{O2}	$\frac{5}{3}$	[min^{-1}]	[21]	Rate affecting the time needed to reach the target exercise level
k_{MPGU}	35	[mg min^{-1}]	[13]	Basal peripheral glucose uptake
k_{HPG}	155	[mg min^{-1}]	[13]	Basal hepatic glucose production
k_{PIU}	2.4	unitless	[13]	Peripheral insulin uptake factor
a_{UA-O2}	0.006	[mg min^{-1}]	[13]	Quadratic coefficient in UA-$O2_m$ law
b_{UA-O2}	1.2264	[mg min^{-1}]	[13]	Linear coefficient in UA-$O2_m$ law
c_{UA-O2}	-10.1958	[mg min^{-1}]	[13]	Constant coefficient in UA-$O2_m$ law

Table 2: Model parameters. BW (kg) is the body weight of the virtual patient. For our experiments, we set $BW = 75$ kg.

by union bound. By this construction, the Theorem 7 in [1] shows that if s is defined by the above equation satisfies $S - s + 1 < s$, then, with probability at least $1 - \alpha_h$ over the sample, the set

$$\mathcal{U}_\epsilon^M = \left\{ \mathbf{u} \in \mathbb{R}^d : \hat{u}_i^{(S-s+1)} \leq u_i \leq \hat{u}_i^{(s)} \forall i = 1, \ldots, d \right\}$$

implies a probabilistic guarantee for $\mathbb{P}^*$ at level ϵ.

C   Building uncertain sets from probabilistic models

We show how to build tight time-varying uncertainty sets when the uncertain meal and exercise episodes are uniformly or normally distributed. Importantly, such distributions can also be derived from sample data through the bootstrapping method [5], as done in the robust taxi dispatch approach of [24].

For each meal, we assume that the start time, t_s, and the total amount of ingested carbohydrates, CHO, are uncertain. Meal duration (d) is fixed, during which carbohydrate ingestion happens at a constant rate. Similarly, each exercise episode has uncertain start time t_s, percentage of muscular mass MM, percentage of maximum oxygen consumption $O2$ and duration d.

According to which distribution the meal or exercise event is sampled from, we derive the lower and upper bound of the corresponding uncertainty parameters. The intuition is that when at time t a random variable, say $O2$, is uniformly distributed in the interval $[O2^\perp, O2^\top]$, written as $O2 \sim \text{Unif}(O2^\perp, O2^\top)$, then the lower and upper bound is $[O2^\perp, O2^\top]$. Note that such a defined uncertain set covers all possible realizations of the random variable. Instead, when $O2$ is normally distributed with mean μ_{O2} and standard deviation σ_{O2}, written as $O2 \sim \mathcal{N}(\mu_{O2}, \sigma_{O2})$, we set the bounds to be $[\mu_{O2} - k \cdot \sigma_{O2}, \mu_{O2} + k \cdot \sigma_{O2}]$, with $k > 0$. Since the normal distribution has unbounded support, we cannot cover all possible realizations with an interval. In our experiments, we select $k = 3$, which covers $\approx 99.74\%$ of all possible values.

Besides the lower and upper bounds, the uncertain sets $\mathcal{U}^t$ are also conditioned by the range of the (uncertain) start time $[t_s^\perp, t_s^\top]$ and the range of duration $[d^\perp, d^\top]$ for each meal/exercise episode. (The duration of meal is fixed so the range is only a single value d). Table 3 illustrates the rule for the construction of uncertainty set at time t.

D   Asymmetric costs

We evaluate glucose regulation under different asymmetric costs. By choosing $\gamma > 1$ in the controller (see Equation 9), predicted BG trajectories below the target BG level are penalized more than those above the target. As discussed in [7], this strategy contributes to reducing hypoglycemic episodes and is substantiated by the fact that hypoglycemia leads to more severe consequences than those of (temporary) hyperglycemia.

$\mathcal{U}^t[D_G]$	$D_G^{t\perp} = CHO^\perp/d$ if $t_s^\top \le i \le t_s^\perp + d$, 0 o/w
$= [D_G^{t\perp}, D_G^{t\top}]$	$D_G^{t\top} = CHO^\top/d$ if $t_s^\perp \le i \le t_s^\top + d$, 0 o/w
$\mathcal{U}^t[MM]$	$MM^{t\perp} = MM^\perp$ if $t_s^\top \le i \le t_s^\perp + d^\perp$, 0 o/w
$= [MM^{t\perp}, MM^{t\top}]$	$MM^{t\top} = MM^\top$ if $t_s^\perp \le i \le t_s^\top + d^\top$, 0 o/w
$\mathcal{U}^t[O2]$	$O2^{t\perp} = O2^\perp$ if $t_s^\top \le i \le t_s^\perp + d^\perp$, $O2_0$ o/w
$= [O2^{t\perp}, O2^{t\top}]$	$O2^{t\top} = O2^\top$ if $t_s^\perp \le i \le t_s^\top + d^\top$, $O2_0$ o/w

Table 3: Uncertain sets at time t for CHO ingestion rate D_G, active muscular mass MM and oxygen consumption $O2$. $O2_0 = 8$ is the basal oxygen consumption at rest.

	$t_{<3.9}$	$t_{3.9-11.1}$	$t_{>11.1}$	$BG_{\min}$	$BG_{\max}$	$\sum \iota$
Scenario 1, perfect	0%	99.69%	0.31%	7.15	9.91	4.38
Scenario 1, HCL	1.6%	69.4%	29%	**5.61**	12.85	8.19
Scenario 1, robust	**0.51%**	**97.7%**	**1.79%**	5.57	**9.96**	6.23
Scenario 2, perfect	0%	100%	0%	7.03	8.84	4.67
Scenario 2, HCL	1.03%	81.51%	17.45%	**5.75**	11.32	6.31
Scenario 2, robust	**0.28%**	**84.19%**	**15.53%**	5.16	**10.94**	5.82
Scenario 3, perfect	0%	100%	0%	7.22	9.3	5.06
Scenario 3, HCL	**0%**	67.25%	32.75%	**7.19**	13.34	5.05
Scenario 3, robust	0.79%	**99.03%**	**0.18%**	5.09	**8.77**	5.64

Table 4: Complete statistics for the one-meal experiments of Section 5.1.

We tested the robust controller with $\gamma = 1, 2, 4$ (symmetric, 2x, and 4x penalty, respectively). Simulations were conducted according to the *outliers* scenario (see Section 5.1), which typically generates hypoglycemic episodes and thus, is an ideal testbed for tuning γ.

	$t_{<3.9}$	$t_{3.9-11.1}$	$t_{>11.1}$	$BG_{\min}$	$BG_{\max}$
$\gamma = 1$	1.5%	85.35%	13.15%	5.17	11.05
$\gamma = 2$	0%	80.13%	18.87%	5.4	11.38
$\gamma = 4$	0%	76.8%	23.2%	5.6	11.63

Table 5: Indicators for different asymmetric cost strategies.

Table 5 reports the performance indicators obtained with 20 repetitions for each value of γ. While for $\gamma = 1$ (symmetric cost) we record some minor hypoglycemic episodes, hypoglycemia is totally avoided for $\gamma = 2, 4$. Between these two values, we chose $\gamma = 2$ since it yields smaller hyperglycemia. The indicators for average BG peaks and lows confirm that glucose levels increase with γ.

E   Data extraction from NHANES database

Below, we describe how we extracted meal data from the CDC's NHANES database and generated the corresponding uncertainty sets.

– We retrieve meal information from the dietary interview, where each participant reports the timings, types and amounts of each meal during a typical day.

- Through a moving average filter, we transform the meal events of each participant into a one-day trajectory describing the CHO intake rate, so that it can be mapped into the uncertainty parameter D_G.
- Note that a building a single uncertainty set built from the whole database would result in a overly-conservative sets that allows for essentially unrestricted random behaviors. To avoid this, we classify the database based on the above CHO trajectories into 10 groups using k-means clustering, and select a cluster consisting of 274 people.
- Such data is then used to construct the uncertainty sets, as described in Section 4.2, and to parameterize the virtual patient, where random meal uncertainties are sampled from the set of participants.
- Due to the lack of good quality data for physical activity in the NHANES database, we generated synthetic exercise data (1 random one-hour exercise episode for each patient) as follows:
  - draw uniformly a random start time for exercise between 9am and 6pm
  - set CHO intake rate to zero for the corresponding time window, since it is unlikely if not impossible that eating and exercise happen at the same time
  - uniformly sample among light, moderate and intense exercise
  - depending on the above outcome, sample oxygen consumption and active muscular mass according to the below predefined ranges:
    * light: $MM = \text{unif}(0.1, 0.25)$, $O2 = \text{unif}(15, 45)$;
    * moderate: $MM = \text{unif}(0.2, 0.35)$, $O2 = \text{unif}(45, 75)$;
    * intense: $MM = \text{unif}(0.3, 0.5)$, $O2 = \text{unif}(75, 100)$.

(a) Cluster # 2: 368 people (b) Cluster # 3: 592 people (c) Cluster # 4: 440 people

(d) Cluster # 5: 4663 people (e) Cluster # 6: 325 people (f) Cluster # 7: 662 people

(g) Cluster # 8: 128 people (h) Cluster # 9: 658 people (i) Cluster # 10: 551 people
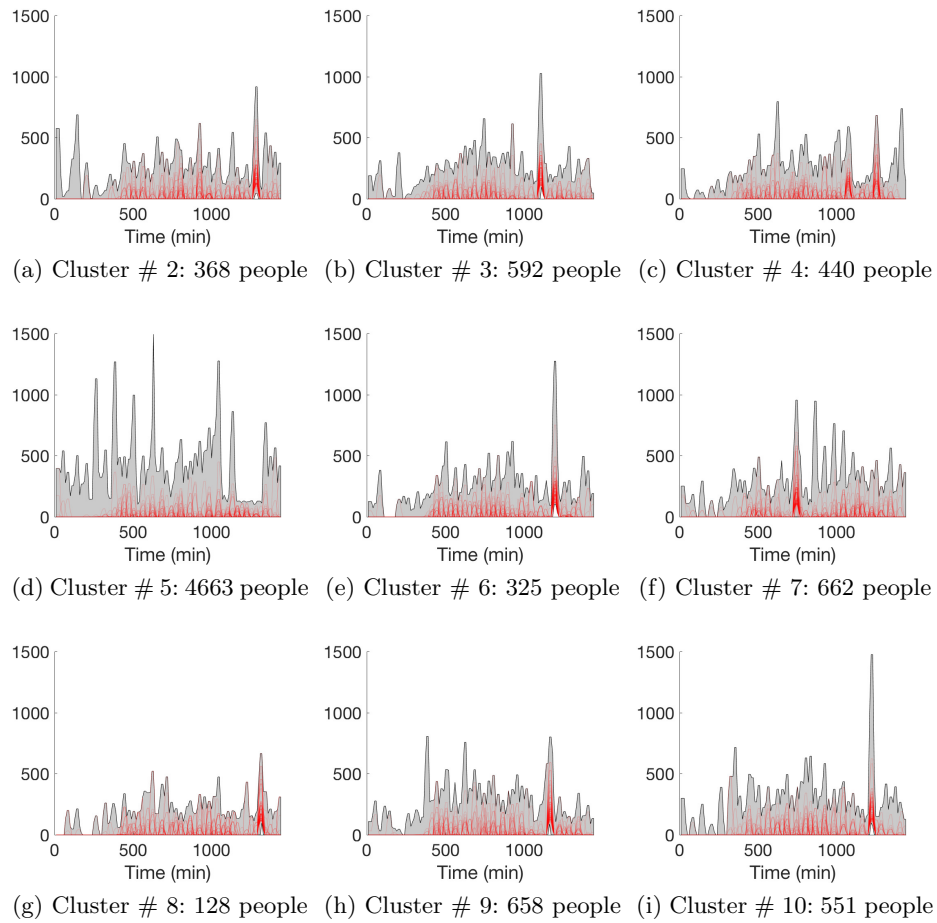
Fig. 8: Uncertainty sets for clusters 2-10 extracted from the NHANES database. Cluster # 1 was used for our experiments and is reported in Figure 5. Cluster # 2, 3, 4, 6, 8, 9, 10 show peaks at about minute 1200, indicating schedules characterized by CHO-rich dinners. Participant in cluster # 7 are characterized by a rich lunch, while no particular patterns can be observed for cluster # 5.