Hindawi Publishing Corporation Mathematical Problems in Engineering Volume 2013, Article ID 914741, 10 pages http://dx.doi.org/10.1155/2013/914741



Research Article

Application of Optimal HAM for Finding Feedback Control of Optimal Control Problems

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Received 8 November 2012; Accepted 1 February 2013

Academic Editor: Trung Nguyen Thoi

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An optimal homotopy-analysis approach is described for Hamilton-Jacobi-Bellman equation (HJB) arising in nonlinear optimal control problems. This optimal approach contains at most three convergence-control parameters and is computationally rather efficient. A kind of averaged residual error is defined. By minimizing the averaged residual error, the optimal convergence-control parameters can be obtained. This optimal approach has general meanings and can be used to get fast convergent series solutions of different types of equations with strong nonlinearity. The closed-loop optimal control is obtained using the Bellman dynamic programming. Numerical examples are considered aiming to demonstrate the validity and applicability of the proposed techniques and to compare with the existing results.

1. Introduction

Many real-world problems in engineering, economics, and biomedicine can be formulated as optimal control problem of the form

minimum
$$J = h\left(x\left(t_f\right), t_f\right) + \int_{t_0}^{t_f} g\left(x\left(s\right), u\left(s\right), s\right) ds,$$

subject to $\dot{x}\left(t\right) = f\left(x\left(t\right), u\left(t\right), t\right),$
 $x\left(t_0\right) = x_0, \quad x\left(t_f\right) = x_f,$
(1)

where $u(\cdot)$ is the control function, $x(\cdot)$ is the state function, constant parameters, x_0 and x_f are the initial and the final states, $h(\cdot)$ is the salvage value or scrap value function, $f(\cdot)$ is the vector-valued transition function, $g(\cdot)$ is the integrand function, and s is the dummy variable of integration rather than t

There are various efficient methods such as those reported in [1–3] for the computation of open-loop optimal controls. However, feedback controls are much preferred in many engineering applications. In order to determine the

optimal control law, there is an approach using dynamic programming [4]. This approach leads to the HJB equation that is hard to solve in most cases. An excellent literature review on the methods for solving the HJB equation is provided in [5], where a successive Galerkin approximation (SGA) method is also considered. In the SGA, a sequence of generalized HJB equations is solved iteratively to obtain a sequence of approximations approaching the solution of HJB equation. However, the proposed sequence may converge very slowly or even diverge. Another approach is to treat the problem with a measure theory approach [6]. This changes the nonlinear OCP to a linear programming and gives a piecewise constant control law. In the past two decades, the indirect methods have been extensively developed. It is well known that the nonlinear OCP leads to a nonlinear two-point boundary value problem (TPBVP) or a Hamilton-Jacobi-Bellman partial differential equation. Many recent researches have been devoted to solve these two problems.

In particular, we will derive the fundamental first-order partial differential equation obeyed by the optimal value function, known as the HJB equation. This shift in our attention, moreover, will lead us to a different form for the optimal value of the control vector, namely, the feedback or

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closed-loop form of the control. This form of the optimal control typically gives the optimal value of the control vector as a function of the current date, the current state, and the parameters of the control problem. In contrast, the form of the optimal control vector derived via the necessary conditions of optimal control theory is termed open loop and in general gives the optimal value of the control vector as a function of the independent variable time, the parameters, and the initial and/or terminal values of the planning horizon and the state vector. Essentially, the feedback form of the optimal control is a decision rule, for it gives the optimal value of the control for any current period and any admissible state in the current period that may arise. In contrast, the open-loop form of the optimal control is a curve, for it gives the optimal values of the control as the independent variable time varies over the planning horizon. Thus, it is required to solve an HJB equation by numerical-analyticapproximate method. In [7], the authors used the basic ADM for an example of HJB equation and then finding optimal control signal. In [8–10], standard HPM, piecewise HPM and differential transform method (DTM) were used for finding feedback control of optimal control problems.

One of the semiexact methods for solving linear and nonlinear equation which does not need small/large parameters is homotopy analysis method (HAM), first proposed by Liao in 1992 [10–13]. Since Liao's book [14] for the homotopy analysis method was published in 2003, more and more researchers have been successfully applying this method to various nonlinear problems in science and engineering, such as the viscous flows of non-Newtonian fluids [15], the KdV-type equations [16], and finance problems [17].

The HAM contains a certain auxiliary parameter c_0 , which provides us with a simple way to adjust and control the convergence region and rate of convergence of the series solution. Moreover, by means of the so-called c_0 -curve, it is easy to determine the valid regions of c_0 to gain a convergent series solution. Thus, through HAM, explicit analytic solutions of nonlinear problems are possible.

However, as illustrated in [18], the usual HAM has only one convergence-control parameter c_0 , and it is a pity that curves for convergence-control parameter (i.e., c_0 -curves) cannot tell us which value of $c_0 \in \mathbb{R}$ gives the fastest convergent series. Recently, to overcome this shortcoming, Liao [18] proposed an optimal HAM with more than one convergence-control parameter. In this optimal method, Liao introduced the so-called averaged residual error to get the optimal convergence-control parameters efficiently. In general, the optimal HAM can greatly modify the convergence of homotopy-series solution.

The results obtained in this paper show that the solutions given by the optimal HAM give much better approximations and convergence much faster than those given by the usual HAM. In this paper, we employed a new proposal of Liao [18, 19], namely, optimal homotopy-analysis approach to solve an HJB equation obtained from (2)–(4). We use here special deformation functions, which are determined completely by only one characteristic parameter $|c_1| < 1$ and $|c_2| < 1$, respectively. In this way, there exist at most only three

convergence-control parameters c_0 , c_1 , and c_2 at any order of approximations.

2. Nonlinear Time-Variant HJB Equation

Consider a process described by the following system of nonlinear differential equations, which is called the equation of motion, on a fixed interval $[t_0, t_f]$

$$\dot{x}(t) = f(x(t), u(t), t), \tag{2}$$

where $x \in \mathbb{R}^n$ is the state vector. Let $U(\cdot) \in \mathbb{R}^n$ be a closed set. A piecewise continuous function $u:[t_0,t_f] \to \mathbb{R}^n$ is said to be an admissible control if $u(t) \in U(\cdot)$. Let \mathcal{U} be the class of such admissible controls. The function f is a real-valued continuously differentiable function and has continuous first partial derivative with respect to x. The initial condition for (2) is

$$x\left(t_{0}\right) = x_{0}.\tag{3}$$

Along with this controlled process, we have a cost functional of the form

$$J(x_0, u) = \Phi(x(t_f), t_f) + \int_{t_0}^{t_f} L(x(\tau), u(\tau), \tau) d\tau.$$
 (4)

Here, $L(x(\tau), u(\tau), \tau)$ is the running cost, and $\Phi(x(t_f), t_f)$ is the terminal cost. This cost functional depends on the initial position (x_0, t_0) and the choice of control $u(\cdot)$. The optimization problem is therefore to minimize $J(x_0, u)$, for each (x_0, u) , over all controls $u(t) \in U(\cdot)$. The pair (x_0, u) which achieves this minimum is called an optimal control. In fact, the optimization problem with performance index as in (4) is called a Bolza problem.

In dynamic programming, the minimum value of the performance index is considered as a function of this initial point. This function is called the value function. Whenever the value function is differentiable, it satisfies a nonlinear first-order hyperbolic partial differential equation called the partial differential equation of dynamic programming. This equation is used for constructing a nonlinear optimal feedback control law. If we consider a family of optimization problems with differential initial condition (x,t), we consider the dependence of the value of these optimization problems on their initial conditions. Thus, a value function is defined by

$$V(x,t) = J(x,u^*)$$

$$= \min_{u \in \mathcal{U}} \left\{ \Phi\left(x\left(t_f\right), t_f\right) + \int_t^{t_f} L(x(\tau), u(\tau), \tau) d\tau \right\}.$$
(5)

Theorem 1. Let (x,t) be any interior point of the set $\{(x,t) \in \mathbb{R}^{n+1} | \mathcal{U} \neq 0\}$ at which the function V(x,t) is differentiable. Function V(x,t) satisfies the partial differential inequality

$$\frac{\partial V}{\partial t} + \frac{\partial V}{\partial x} f(x, u, t) + L(x, u, t) \ge 0, \tag{6}$$

for all $u \in \mathcal{U}$. If there is an optimal control $u^* \in \mathcal{U}$, then the partial differential equation

$$\frac{\partial V}{\partial t} + \min_{u \in U} \left\{ \frac{\partial V}{\partial x} f(x, u, t) + L(x, u, t) \right\} = 0 \tag{7}$$

is satisfied [20].

This nonlinear time-variant differential equation is called "HJB equation." We have the following boundary condition:

$$J^{*}\left(x\left(t_{f}\right),t_{f}\right)=V\left(x\left(t_{f}\right),t_{f}\right)=\Phi\left(x\left(t_{f}\right),t_{f}\right),\tag{8}$$

and by introducing the Hamiltonian function

$$H(x, u, V_x, t) = \frac{\partial V}{\partial x} f(x, u, t) + L(x, u, t), \qquad (9)$$

we have

$$H\left(x,u^{*},V_{x},t\right)=\min_{u\in U}H\left(x,u,V_{x},t\right).\tag{10}$$

Therefore, by substitution of Hamiltonian function (10) in (7), we have

$$\frac{\partial V}{\partial t} + H\left(x, u^*, V_x, t\right) = 0. \tag{11}$$

3. Basic Idea of Optimal Homotopy Analysis Method

In this section, we give a brief description of optimal homotopy-analysis approaches in general cases. For a general nonlinear differential/integral equation as follows:

$$N\left(U\left(r,t\right)\right)=0,\tag{12}$$

where U(r,t) is an unknown function, r and t denote, respectively, spatial and temporal independent variables, we can always choose a proper initial guess $U_0(r,t)$ and a proper auxiliary linear operator L to construct the so-called zeroth-order deformation equation

$$[1 - B_{n'}(q;b)] L [\phi(r,t;q) - U_0(r,t)]$$

$$= c_0 A_{m'}(q,a) N [\phi(r,t;q)], \quad q \in [0,1],$$
(13)

where $A_{m'}(q,a)$ is a deformation function with m' ($m' \ge 0$) unknown convergence-control parameters denoted by c_1, c_2, \ldots, c'_m , and $B_{n'}(q,b)$ is a deformation function with n' ($n' \ge 0$) unknown convergence-control parameters denoted by $c_{m'+1}, c_{m'+2}, \ldots, c_{m'+n'}$, respectively. Here,

$$a = \{c_1, c_2, \dots, c_{m'}\}, \qquad b = \{c_{m'+1}, c_{m'+2}, \dots, c_{m'+n'}\}.$$
 (14)

Put l=m'+n'. Then, we have l+1 unknown convergence-control parameters $c_0, c_1, c_2, \ldots, c_l$. Assuming that the initial guess $U_0(r,t)$, the auxiliary linear operator L, and the l+1 convergence-control parameters c_1, c_2, \ldots, c_l are so properly chosen that the Taylor series

$$\phi(r,t;q) = U_0(r,t) + \sum_{n=1}^{+\infty} U_n(r,t) q^n$$
 (15)

converges at q = 1, we have the homotopy-series solution

$$U(r,t) = U_0(r,t) + \sum_{n=1}^{+\infty} U_n(r,t).$$
 (16)

Substituting the series (15) into the zeroth-order deformation equation (13) and then equating the coefficients of the like power of the embedding parameter q, we have the high-order deformation equation. Consider

$$L\left[U_{m}(r,t) - \sum_{k=1}^{m-1} \sigma_{m-k}(b) U_{k}(r,t)\right] = c_{0} \sum_{k=0}^{m-1} \mu_{m-k}(a) \delta_{k}(r,t),$$
(17)

where

$$\delta_k(r,t) = \left(\frac{1}{k!} \frac{\partial^k}{\partial q^k} N \left[\sum_{n=1}^{+\infty} U_n(r,t) \, q^n \right] \right) \bigg|_{q=0}, \quad (18)$$

and $\mu_k(a)$ and $\sigma_k(b)$ are coefficients of the Taylor series

$$A_{m'}(q;a) = \sum_{k=1}^{+\infty} \mu_k(a) q^k, \qquad B_{n'}(q;b) = \sum_{k=1}^{+\infty} \sigma_k(b) q^k.$$
 (19)

Let $A_{m'}(q; a)$, $B_{n'}(q; b)$ be complex functions analytic in the region $|q| \le 1$, which satisfy

$$A_{m'}(0;a) = B_{n'}(0;a) = 0, \quad A_{m'}(1;a) = B_{n'}(1;a) = 1.$$
 (20)

The special solution $U_m^*(r,t)$ of (17) is given by

$$U_{m}^{*}(r,t) = \sum_{k=1}^{m-1} \sigma_{m-k}(b) U_{k}(r,t) + c_{0} \sum_{k=1}^{m-1} \mu_{m-k}(a) S_{k}(r,t),$$
(21)

where

$$S_{k}\left(r,t\right)=L^{-1}\left[\delta_{k}\left(r,t\right)\right],\tag{22}$$

and L^{-1} is the inverse operator of L.

Now, we define a kind of averaged residual error [18]

$$E_{m} = \frac{1}{k} \sum_{i=0}^{k} \left[N \left(\sum_{i=0}^{m} U_{i} \left(j \Delta t \right) \right) \right]^{2}. \tag{23}$$

The value of k is depends to problem, for Examples 2 and 3, we have $\Delta t = 1/10$, k = 10, and $\Delta t = 1/20$, k = 20, respectively.

Note that E_m contains l+1 unknown convergence-control parameters c_0, c_1, \ldots, c_l , whose optimal values are given by the minimum of E_m , corresponding to a set of l+1 nonlinear algebraic equations

$$\frac{\partial E_m}{\partial c_i} = 0, \quad j = 0, 1, \dots, l.$$
 (24)

So, the above approach is called the l+1-parameter optimal homotopy-analysis approach. In general, the above-mentioned optimal homotopy-analysis approaches can greatly modify the convergence of homotopy-series solution. And the optimal homotopy-analysis approaches with one or two unknown convergence-control parameters are strongly suggested; an optimal approach with too many unknown convergence-control parameters is not efficient computationally.

4. Application

To illustrate the effectiveness of the optimal homotopy analysis method, we will consider two examples. Comparisons are made between the exact solution and optimal homotopy-analysis approaches.

Example 2. Consider the following purely mathematical optimal control problem:

$$\dot{x} = x(t) + u(t). \tag{25}$$

Suppose that we consider the following cost function for this system:

$$J = x^{2} (t_{f}) + \int_{0}^{t_{f}} u^{2} (t) dt.$$
 (26)

The Hamiltonian function will be

$$H(x, u, V_x, t) = u^2(t) + V_x(x, t) [x + u].$$
 (27)

Since the Hamiltonian, which as you know is the right-handside expression to be minimum, is a convex function of the state and control variables, a solution of the necessary conditions is a solution of the optimal control. Thus, the necessary and sufficient condition for the above minimization problem in the HJB equation is given by

$$\frac{\partial H}{\partial u} = 2u(t) + V_x(x, t) = 0, \tag{28}$$

which is easily solved to get

$$u^{*}(t) = -\frac{1}{2}V_{x}(x,t).$$
 (29)

Because $\partial^2 H/\partial u^2 = 2 > 0$, u^* is a minimum and acceptable. Now, by substitution of u^* in HJB equation, we have the following:

$$-V_t = -\frac{1}{4}V_x^2 + xV_x,$$

$$V\left(x\left(t_f\right), t_f\right) = x^2\left(t_f\right).$$
(30)

In Chapter 19 of [21], the authors obtained the solution of the above HJB equation in the form

$$V(x,t) = \frac{2x^2}{1 + e^{2(t-t_f)}}, \quad u^*(t) = -\frac{2x}{1 + e^{2(t-t_f)}}, \quad (31)$$

for simplicity, let $u^*(x,t) = k(t)x(t)$, where

$$k(t) = \frac{-2}{1 + e^{2(t - t_f)}}. (32)$$

To solve (30) by means of optimal homotopy analysis method, we choose the initial approximation, final time, and auxiliary linear operator

$$V_{0}(x,t) = x^{2}, \quad t_{f} = 1,$$

$$L\left[\phi(x,t;q)\right] = \frac{\partial\phi(x,t;q)}{\partial t}.$$
(33)

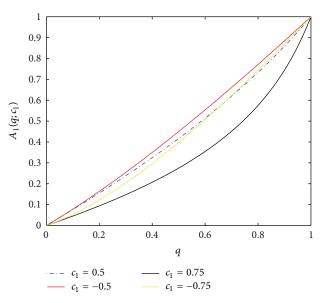


FIGURE 1: Deformation function $A_1(q; c_1)$ defined by (34) and (35).

There are an infinite number of deformation functions satisfying the properties (19). For the sake of computation efficiency, we use here the following one-parameter deformation functions:

$$A_{1}(q;c_{1}) = \sum_{m=1}^{+\infty} \mu_{m}(c_{1}) q^{m}, \qquad B_{1}(q;c_{2}) = \sum_{m=1}^{+\infty} \sigma_{m}(c_{2}) q^{m},$$
(34)

where $|c_1| < 1$ and $|c_2| < 1$ are constants, called the convergence-control parameter, and

$$\mu_m(c_1) = (1 - c_1) c_1^{m-1}, \quad m \ge 1,$$

$$\sigma_m(c_2) = (1 - c_2) c_2^{m-1}, \quad m \ge 1.$$
(35)

The different values of c_1 give different paths of $A_1(q; c_1)$, as shown in Figure 1.

Let $q \in [0, 1]$ denote the embedding parameter, $c_0 \neq 0$ an auxiliary parameter, called the convergence-control parameter, and $\phi(x, t; q)$ a kind of continuous mapping of V(x, t), respectively. Obviously, when q = 0 and q = 1, it holds

$$\phi(x,t;0) = V_0(x,t), \qquad \phi(x,t;1) = V(x,t),$$
 (36)

respectively. Thus, as q increases from 0 to 1, the solutions $\phi(x,t;q)$ vary from the initial guesses $V_0(x,t)$ to the solutions V(x,t). We construct the zeroth-order deformation equation:

$$[1 - B_{1}(q; c_{2})] L [\phi(x, t; q) - V_{0}(x, t)]$$

$$= c_{0} A_{1}(q, c_{1}) N [\phi(x, t; q)], \quad q \in [0, 1],$$
(37)

subject to the boundary condition

$$\phi(x(1), 1; 0) = x^{2}(1). \tag{38}$$

As mentioned, we have the mth-order deformation equation

$$L\left[V_{m}(x,t) - \sum_{k=1}^{m-1} \sigma_{m-k}(c_{2}) V_{k}(x,t)\right]$$

$$= c_{0} \sum_{k=0}^{m-1} \mu_{m-k}(c_{1}) \delta_{k}(x,t),$$
(39)

where

$$\delta_k(x,t) = \frac{\partial V_k}{\partial t} - \frac{1}{4} \sum_{j=0}^k \left(\frac{\partial V_j}{\partial x} \right) \left(\frac{\partial V_{k-j}}{\partial x} \right) + x \frac{\partial V_k}{\partial x}$$
(40)

and the coefficients $\mu_k(c_1)$ and $\sigma_k(c_2)$ are defined by (35). Let $V^*(x,t)$ denote a special solution of (39) and L^{-1} the inverse operator of L, respectively. We have

$$V_{m}^{*}(x,t) = \sum_{k=1}^{m-1} \sigma_{m-k}(c_{2}) V_{k}(x,t) + c_{0} \sum_{k=0}^{m-1} \mu_{m-k}(c_{1}) L^{-1} [\delta_{k}(x,t)].$$

$$(41)$$

We now successively obtain

$$V_{1}(x,t) = -c_{0}(-1+c_{1})(t-1)x^{2},$$

$$V_{2}(x,t) = c_{0}tx^{2} - c_{0}x^{2} - c_{0}c_{2}tx^{2} + c_{0}c_{2}x^{2}$$

$$+ c_{0}c_{2}c_{1}tx^{2} - c_{0}c_{2}c_{1}x^{2} - c_{0}c_{1}^{2}tx^{2}$$

$$+ c_{0}c_{1}^{2}x^{2} + c_{0}^{2}tx^{2} - c_{0}^{2}x^{2} - 2c_{0}^{2}c_{1}tx_{2}$$

$$+ 2c_{0}^{2}c_{1}x^{2} + c_{0}^{2}c_{1}^{2}tx^{2} - c_{0}^{2}c_{1}^{2}x^{2},$$

$$V_{3}(x,t) = c_{0}x^{2}t - c_{0}x^{2} - c_{0}c_{2}x^{2}t + c_{0}x^{2}c_{2}$$

$$+ c_{0}x^{2}c_{2}c_{1}t - c_{0}x^{2}c_{2}c_{1} - c_{0}x^{2}c_{1}^{2}t$$

$$+ c_{0}x^{2}c_{1}^{2} + c_{0}^{2}x^{2}t - c_{0}^{2}x^{2} - 2c_{0}^{2}x^{2}c_{1}t$$

$$+ 2c_{0}^{2}x^{2}c_{1} + c_{0}^{2}x^{2}c_{1}^{2}t - c_{0}^{2}x^{2}c_{1}^{2},$$

$$\vdots$$

$$(42)$$

It should be emphasized that $V_m(x,t)$ contains at most three unknown convergence-control parameters c_0 , c_1 , and c_2 , which determine the convergence region and rate of the homotopy-series solution. Obviously, if the convergence-control parameters c_0 , c_1 , and c_2 are properly chosen, the homotopy-series solution may converge fast. So, we should find out the good enough values of c_0 , c_1 , and c_2 , so that the homotopy-series solution converges fast enough.

4.1. Comparisons of Different Approaches for Example 2. In this section, we will give optimal homotopy-analysis approaches with different numbers of unknown convergence-control parameters and compare them in detail.

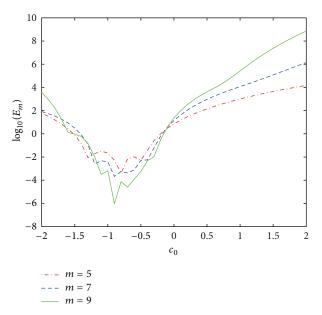


Figure 2: Averaged residual error E_m versus c_0 in case of $c_1 = c_2 = 0$.

Table 1: Comparison of averaged residual error given by different c_0 in case of $c_1 = c_2 = 0$ and x = 1.

		Minimum value of E_m
5 -	-0.8187	1.7876e - 004
7 -	-0.8193	1.1659e - 004
9 -	-0.8296	4.2456 <i>e</i> – 006

4.1.1. Optimal c_0 in Case of $c_1 = c_2 = 0$. In this case, only one convergence-control parameter c_0 is unknown. For given order of approximation m, the optimal value of c_0 is given by the minimum of E_m , corresponding to a nonlinear algebraic equation $dE_m/dc_0 = 0$.

The curves of E_m versus c_0 at a different order of approximation m=5,7, and 9 are shown in Figure 2. In case of $c_1=c_2=0$, there is only one unknown convergence-control parameter c_0 ; thus the optimal value of c_0 is determined by the minimum of E_9 , corresponding to the nonlinear algebraic equation $dE_9/dc_0=0$. According to Table 1, the value minimum of E_9 is obtained at -0.8296. It should be noted that, when we fixed $c_0=-1$ and $c_1=c_2=0$, automatically the problem turns into the so-called homotopy perturbation method (HPM). So, the HPM is only a special case of the HAM when $c_0=-1$.

In case of $c_1 = c_2 = 0$, one has the plain deformation functions $A_1(q, c_1) = B_1(q, c_2) = q$, which is exactly the same as that used in traditional HAM.

4.1.2. Optimal $c_1 = c_2$ in Case of $c_0 = -1$. In this case, E_9 has the value minimum of 2.8203×10^{-6} at the optimal point $c_1 = c_2 = 0.2458$. This illustrates that the second one-parameter optimal homotopy-analysis approach is as good as the first one mentioned in Section 4.1.1. (See Table 2).

4.1.3. Optimal c_0 in Case of $c_1 = c_2$. In this case, we obtain the unknown convergence-control parameters c_0 and c_1 in case of

Table 2: Comparison of averaged residual error given by different $c_1 = c_2$ in case of $c_0 = -1$ and x = 1.

m	Optimal value of $c_1 = c_1$	Minimum value of E_m
5	$c_1 = c_2 = 0.3971$	2.2134e - 004
7	$c_1 = c_2 = 0.3689$	1.3731e - 004
9	$c_1 = c_2 = 0.2458$	2.8203e - 006

Table 3: Comparison of averaged residual error given by different c_0 in case of $c_1 = c_2$.

m	Optimal value of c_0 and $c_1 = c_2$	Minimum value of E_m
5	$c_0 = -0.9238$ and $c_1 = c_2 = 0.1001$	1.0893e - 004
7	$c_0 = -0.9997$ and $c_1 = c_2 = 0.1003$	1.0425e - 005
9	$c_0 = -1.0012$ and $c_1 = c_2 = 0.0398$	1.4099e - 006

 $c_2 = c_1$. The corresponding residual error E_9 is now a function of both c_0 and c_1 , which has the value minimum of 1.4099 × 10^{-6} at the optimal point $c_0 = -1.0012$, $c_1 = c_2 = 0.0398$. (See Table 3).

4.1.4. Optimal c_0 , c_1 , and c_2 in Case of $c_1 \neq c_2$. Let us consider the optimal approach with the three unknown convergence-control parameters. The corresponding E_9 is now a function of c_0 , c_1 , and c_2 , which has the minimum 1.7716 \times 10⁻⁵ at the optimal values $c_0 = -0.6932$, $c_1 = -0.2440$, and $c_2 = -0.1039$. The corresponding homotopy-series solution converges much faster than homotopy-series solution in case of $c_0 = -1$ and $c_1 = c_2 = 0$, as shown in Table 4.

Based on the above calculations for this equation, we found that all optimal homotopy-analysis approaches can give much better approximations, which converge much faster than those without optimal convergence-control parameters in case of $c_0 = -1$ and $c_1 = c_2 = 0$, as shown in Tables 1–4.

The absolute error of the 20th-order approximate solution and analytic solution (31) with $c_0 = -1$, $c_1 = c_2 = 0$, and $c_0 = -0.8296$, $c_1 = c_2 = 0$ is shown in Figures 3 and 4, respectively. Comparison of the analytic solution (31) with the optimal homotopy analysis method solution by $c_0 = -0.8296$ and $c_1 = c_2 = 0$ is given in Figure 5. The absolute errors $|k_{\rm analytic} - k_{\rm approximate}|$ have been calculated for different cases of c_0 , c_1 , and c_2 in Table 5.

Example 3. Consider a single-input scalar system as follows:

$$\dot{x} = -2x(t) + u(t),$$

$$J = \frac{1}{2}x^{2}(1) + \frac{1}{2}\int_{0}^{1} (x^{2}(t) + u^{2}(t)) dt.$$
(43)

The corresponding Hamiltonian function will be

$$H(x, u, V_{x}, t) = \frac{1}{2}x^{2}(t) + \frac{1}{2}u^{2}(t) + \frac{\partial V(x, t)}{\partial x} [-2x(t) + u(t)].$$
(44)

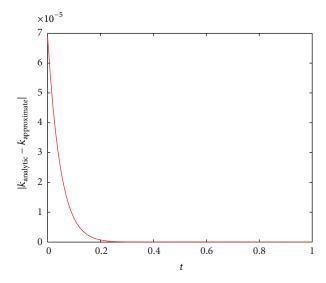


Figure 3: $|k_{\rm analytic} - k_{\rm approximate}|$ (m=20), with $c_0=-1$ and $c_1=c_2=0$.

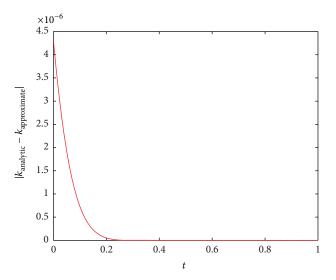


FIGURE 4: $|k_{\text{analytic}} - k_{\text{approximate}}|$ (m = 20), with $c_0 = -0.8296$ and $c_1 = c_2 = 0$.

For finding u^* , we have

$$\frac{\partial H}{\partial u} = u(t) + \frac{\partial V}{\partial x} = 0. \tag{45}$$

Therefore, we obtain

$$u^*\left(t\right) = -\frac{\partial V}{\partial x}.\tag{46}$$

m

5

7

9

1.4099e - 006

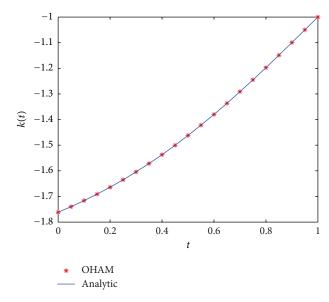
 $c_0 = -0.6932, \ c_1 = -0.2440, \ \text{and} \ c_2 = -0.1039$ $c_0 = -1, \ c_1 = c_2 = 0$ $c_0 = -1.0012, \ c_1 = c_2 = 0.0398$ 1.4e - 004 1.4357e - 003 1.0012e - 004 4.27026e - 004 4.0327e - 004 1.3265e - 004

6.5798e - 005

TABLE 4: Comparison of averaged residual error given by different approaches.

Table 5: The absolute error of approximate solution and exact solution of k(t) by 20th-order approximate.

t	$c_0 = -0.8296, \ c_1 = c_2 = 0$	$c_0 = -1, c_1 = c_2 = 0$	$c_0 = -1.0012, c_1 = c_2 = 0.0398$	$c_0 = -0.6932$, $c_1 = -0.2440$, and $c_2 = -0.1039$
0	2.3195e - 006	6.8965e - 005	3.0012e - 006	8.5935e - 006
0.2	1.2977e - 008	7.0978e - 007	2.3265e - 008	1.0202e - 007
0.4	2.2350e - 010	1.8553e - 009	3.4065e - 010	1.1207e - 009
0.6	4.3885e - 013	4.0035e - 013	1.0039e - 013	1.1423e - 013
0.8	1.9864e - 016	0	0	0
1.0	0	3.3307e - 016	0	0



1.7716e - 005

FIGURE 5: Comparison of the analytic solution (31) with the approximate solution of k(t) (m=20), by $c_0=-0.8296$ and $c_1=c_2=0$.

Because $\partial^2 H/\partial u^2 = 1 > 0$, u^* is a minimum and acceptable. Now, by substitution of u^* in HJB equation, we have the following:

$$-\frac{\partial V}{\partial t} = \frac{1}{2}x^{2}(t) + \frac{1}{2}\left(-\frac{\partial V(x,t)}{\partial x}\right)^{2} + \frac{\partial V(x,t)}{\partial x}\left[-2x(t) - \frac{\partial V(x,t)}{\partial x}\right], \quad (47)$$

$$V(x(1),1) = \frac{1}{2}x^{2}(1)$$

or

$$\frac{\partial V}{\partial t} = -\frac{1}{2}x^{2}(t) + \frac{1}{2}\left(\frac{\partial V(x,t)}{\partial x}\right)^{2} + 2x\frac{\partial V(x,t)}{\partial x},$$

$$V(x(1),1) = \frac{1}{2}x^{2}(1).$$
(48)

Note that, by (29), the optimal control law is $u^*(t) = -k(t)x(t) = f(t)x(t)$, where the exact solution of k(t) is [2]

$$k(t) = \frac{\sqrt{5}\cosh\sqrt{5}(1-t) - \sinh\sqrt{5}(1-t)}{\sqrt{5}\cosh\sqrt{5}(1-t) + 3\sinh\sqrt{5}(1-t)}.$$
 (49)

To solve (48) by means of optimal homotopy analysis method, we choose the initial approximation and auxiliary linear operator

$$V_{0}(x,t) = \frac{1}{2}x^{2},$$

$$L\left[\phi(x,t;q)\right] = \frac{\partial\phi(x,t;q)}{\partial t}.$$
(50)

We construct the zeroth-order deformation equation

$$[1 - B_{1}(q; c_{2})] L [\phi(x, t; q) - V_{0}(x, t)]$$

$$= c_{0} A_{1}(q, c_{1}) N [\phi(x, t; q)], \quad q \in [0, 1],$$
(51)

subject to the boundary condition

$$\phi(x(1), 1; 0) = \frac{1}{2}x^2(1).$$
 (52)

As mentioned, we have the mth-order deformation equation

$$L\left[V_{m}(x,t) - \sum_{k=1}^{m-1} \sigma_{m-k}(c_{2}) V_{k}(x,t)\right]$$

$$= c_{0} \sum_{k=0}^{m-1} \mu_{m-k}(c_{1}) \delta_{k}(x,t),$$
(53)

Table 6: Comparison of averaged residual error given by different c_0 in case of $c_1 = c_2 = 0$.

m	Optimal value of c_0	Minimum value of E_m
5	-0.42943	2.9072e - 004
7	-0.49327	2.9543e - 006
9	-0.44032	1.3871e - 007

where

$$\delta_{k}(x,t) = \frac{\partial V_{k}}{\partial t} - \frac{1}{2} \sum_{j=0}^{k} \left(\frac{\partial V_{j}}{\partial x} \right) \left(\frac{\partial V_{k-j}}{\partial x} \right) - 2x \frac{\partial V_{k}}{\partial x} + \frac{1}{2} x^{2}$$
(54)

and the coefficients $\mu_k(c_1)$ and $\sigma_k(c_2)$ are defined by (35). Let $V^*(x,t)$ denote a special solution of (53) and L^{-1} the inverse operator of L, respectively. We have

$$V_{m}^{*}(x,t) = \sum_{k=1}^{m-1} \sigma_{m-k}(c_{2}) V_{k}(x,t) + c_{0} \sum_{k=0}^{m-1} \mu_{m-k}(c_{1}) L^{-1} [\delta_{k}(x,t)].$$
(55)

We now successively obtain

$$V_{1}(x,t) = 2c_{0}(-1+c_{1})(t-1)x^{2},$$

$$V_{2}(x,t) = -2c_{0}tx^{2} + 2c_{0}x^{2} + 2c_{0}c_{2}tx^{2}$$

$$-2c_{0}c_{2}x^{2} - 2c_{0}c_{2}c_{1}tx^{2} + 2c_{0}c_{2}c_{1}x^{2}$$

$$+6c_{0}t^{2}x^{2} + 8c_{0}^{2}x^{2} - 12c_{0}^{2}c_{1}t^{2}x^{2}$$

$$-16c_{0}^{2}c_{1}x^{2} + 6c_{0}^{2}c_{1}^{2}t^{2}x^{2}$$

$$+8c_{0}^{2}c_{1}^{2}x^{2} + 2c_{0}c_{1}^{2}tx^{2} - 2c_{0}c_{1}^{2}x^{2}$$

$$-14c_{0}^{2}tx^{2} + 28c_{0}^{2}c_{1}tx^{2} - 14c_{0}^{2}c_{1}^{2}tx^{2},$$

$$\vdots$$
(56)

4.2. Comparisons of Different Approaches for Example 3. In this section, we will give optimal homotopy-analysis approaches with different numbers of unknown convergence-control parameters and compare them in detail.

4.2.1. Optimal c_0 in Case of $c_1 = c_2 = 0$. In this case, only one convergence-control parameter c_0 is unknown. We solved this example by standard HAM, and we investigated the influence of c_0 by means of the so-called c_0 -curves. As pointed out by Liao [14], the valid region of c_0 is a horizontal line segment. So, we can just determine the possible valid region of c_0 as shown in Figure 6. However, usually the c_0 -curves cannot tell us which value of c_0 gives the fastest convergent series.

To overcome this shortcoming, we determined the possible optimal value of c_0 by the minimum of averaged residual

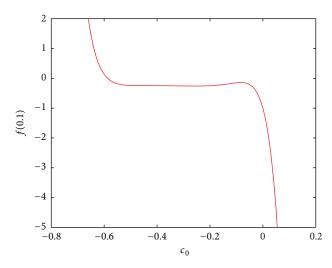


FIGURE 6: The c_0 -curve of the 9th-order approximation in case of $c_1 = c_2 = 0$.

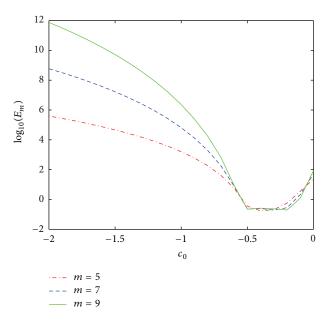


Figure 7: Averaged residual error E_m versus c_0 in case of $c_1 = c_2 = 0$.

error E_9 , corresponding to the nonlinear algebraic equation $E_9' = 0$. According to Table 6, the value minimum of E_9 is obtained at $c_0 = -0.44032$. The curves of E_m versus c_0 at different order of approximation m = 5, 7, and 9 are shown in Figure 7.

4.2.2. Optimal $c_1 = c_2$ in Case of $c_0 = -1$. In this case, E_9 has the value minimum of 8.2039×10^{-2} at the optimal point $c_1 = c_2 = 0.0228$. Our calculations showed that the corresponding E_9 in case of $c_0 = -1$, $c_1 = c_2 = 0$ has the minimum 21.865. This illustrates that the second one-parameter optimal homotopy-analysis approach is not obviously better than the first one mentioned in Section 4.2.1. But this approach can give much better approximation than

t	$c_0 = -0.44032, \ c_1 = c_2 = 0$	$c_0 = -1, c_1 = c_2 = 0$	$c_0 = -0.6084, \ c_1 = c_2 = 0.1611$	$c_0 = -0.1836$, $c_1 = -0.2070$, and $c_2 = -0.4554$
0	1.6173e - 009	5.0401e + 005	6.2742e - 002	3.6240e - 001
0.2	1.2106e - 010	1.6493e + 004	2.0901e - 003	1.1136e - 002
0.4	1.1105e - 010	1.9738e + 002	9.0034e - 005	2.1428e - 002
0.6	1.0013e - 010	3.7288e - 001	1.9358e - 005	1.7872e - 002
0.8	1.7154e - 011	7.4725e - 006	6.2182e - 007	9.5152e - 007
1.0	1.3831e - 012	1.6595e - 007	2.0572e - 011	3.4417e - 015

Table 7: The absolute error of approximate solution and exact solution of f(t) by 15th-order approximate.

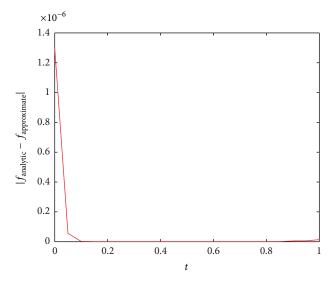


Figure 8: $|f_{\text{analytic}} - f_{\text{approximate}}|$ with $c_0 = -0.44032$ and $c_1 = c_2 = 0$.

those without optimal convergence-control parameters in case of $c_0 = -1$ and $c_1 = c_2 = 0$.

4.2.3. Optimal c_0 in Case of c_1 = c_2 . In this case, we obtain the unknown convergence-control parameters c_0 and c_1 in case of $c_2 = c_1$. The corresponding residual error E_9 is now a function of both c_0 and c_1 , which has the value minimum of 4.6895 × 10^{-4} at the optimal point $c_0 = -0.6084$, $c_1 = c_2 = 0.1611$.

4.2.4. Optimal c_0 , c_1 , and c_2 in Case of $c_1 \neq c_2$. Let us consider the optimal approach with the three unknown convergence-control parameters. The corresponding E_9 is now a function of c_0 , c_1 , and c_2 , which has the minimum 4.94×10^{-3} at the optimal values $c_0 = -0.1836$, $c_1 = -0.2070$, and $c_2 = -0.4554$.

Based on the above calculations for this equation, we found that all optimal homotopy-analysis approaches can give much better approximations, which converge much faster than those without optimal convergence-control parameters in case of $c_0 = -1$ and $c_1 = c_2 = 0$. But in this example, the first one-parameter optimal homotopy-analysis approach is better than other cases.

The absolute error and comparison of the 15th-order approximate solution and analytic solution (49) with $c_0 = -0.44032$, $c_1 = c_2 = 0$ are shown in Figures 8 and 9, respectively. The absolute errors $|f_{\rm analytic} - f_{\rm approximate}|$ have been calculated for different cases of c_0 , c_1 , and c_2 in Table 7.

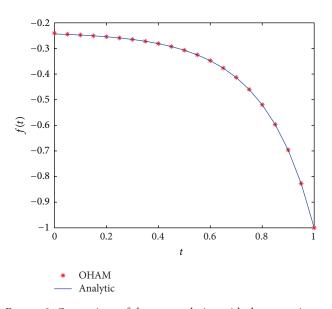


FIGURE 9: Comparison of the exact solution with the approximate solution of f(t) by $c_0 = -0.44032$ and $c_1 = c_2 = 0$.

5. Conclusion

In this paper, we have successfully developed an optimal homotopy-analysis approach for solving HJB equation arising in nonlinear optimal control problems. With the deformation functions defined, the method used here contains three auxiliary convergence-control parameters, which provide us with a simple way to adjust and control the convergence region of the solution. By minimizing the averaged square residual error, the optimal convergence-control parameters c_0 , c_1 , and c_2 can be obtained.

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