

Research Article

Time Irreversibility from Time Series for Analyzing Oil-in-Water Flow Transition

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We first experimentally collect conductance fluctuation signals of oil-in-water two-phase flow in a vertical pipe. Then we detect the flow pattern asymmetry character from the collected signals with multidimensional time irreversibility and multiscale time irreversibility index. Moreover, we propose a novel criterion, that is, AMSI (average of multiscale time irreversibility), to quantitatively investigate the oil-in-water two-phase flow pattern dynamics. The results show that AMSI is sensitive to the flow pattern evolution that can be used to predict the flow pattern transition and bubble coalescence.

1. Introduction

Oil-in-water two-phase flow widely exists in petroleum industry such as crude oil production and transportation. Due to the existence of fluid turbulence and phase interfacial interaction, the mixed fluid often exhibits complex behaviors. In particular, under very low mixture velocity, the existence of bubble coalescence phenomenon leads to more complex fluid dynamics. In this regard, characterizing the oil-in-water two-phase flow structure and dynamics is still quite a challenging problem which is helpful for the flow parameters measurement and pipe pressure drop prediction.

Study on oil-in-water two-phase flow dates back to the 1960s, and early researchers' main focus is on the flow pattern observation and definition. Govier et al. [1] first define the dispersed oil phase in 1.04-inch inner diameter pipe as oil bubble and slug. Then Flores et al. [2] redefine the dispersed oil phase as three different flow patterns, that is, slug flow, bubble flow, and dispersed bubble. This definition for dispersed oil phase is more elaborate that has been approved by several researchers [3, 4]. Recently, researchers are more concerned about oil-in-water two-phase flow under certain flow conditions, such as two-phase flow in bend pipe

[5], two-phase flow in microchannels [6], and high-viscosity oil-water two-phase flow [7]. In addition, more advanced experimental methods are adopted to explore the oil bubble characteristics. The methods such as miniprobe detection [8], high speed photography [9], microwave measurement [10], process tomography [11], and PIV technology [12] have been applied to study the characteristics of oil-in-water two-phase flow.

In recent years, characterizing complex systems from time series has attracted much attention [13, 14]. These signals are time series that are collected to reflect the conductance or pressure fluctuations of the mixed fluid. Note that adopting different signal processing methods would reveal different aspects of flow characteristics. For example, time-frequency method [15] focuses on revealing the motion behaviors of dispersed phase, wavelet analysis [16] and Hilbert-Huang transform method [17] mainly reflect the multiscale and polymorphism dynamics, and nonlinear information analysis techniques [18] are advanced in complex fluid dynamic indication. It is worth noting that complex network has been proved to be an effective tool to characterize the system dynamics [19–21], and the fluid dynamic can also be revealed with mapping the fluctuating signals to networks [22–26].

In general, the flow dynamics revealed from experiment fluctuation signals are less affected by flow condition such as flow rate, pipe diameter, and pipe direction; these methods have attracted many researchers' attention in recent years.

It is a remarkable fact that under low mixture velocity the oil-in-water two-phase flow exhibits quite complex dynamics. First, the fluid exhibits spatial asymmetry structure due to the bubble coalescence. How to characterize this fluid asymmetry is still a difficult problem. In addition, how to effectively characterize the flow pattern transition phenomenon, for example, from slug flow to bubble flow, is still unsolved. Therefore, developing a reliable tool to characterize the oil-in-water two-phase flow dynamics and flow pattern evolution character is quite a necessary issue. Recently, time irreversibility index has been proved to be a powerful tool to detect system dynamics and quantify the existence of system disequilibrium [27]. If the statistical properties of a time series are invariant with respect to time reversal, we can say that this time series is reversal. Otherwise it is time irreversible. Till now, many indexes have been proposed to quantify the time series irreversibility of a complex system, such as multiscale time irreversibility [27–31], symbolic time series irreversibility [32], time irreversibility extracted from Poincaré plot [33–35], complex network time irreversibility [36, 37], and time irreversibility in high dimensional space [38, 39]. The scientific and engineering applications of time series irreversibility also involve many fields including financial system [40, 41], human heart rate [42–44], human brain [45], and seismicity [46]. Employing the time irreversibility index to analyze the two-phase flow fluctuating signals can effectively reveal the flow pattern formation, coalescence, and evolution characteristics. Also, the time irreversibility index can be an indicator for the flow pattern transition phenomenon, for example, from slug to bubble.

In this paper, we first carry out low flow rate oil-water two-phase flow experiment in vertical 20 mm inner diameter Plexiglass pipe and the conductance fluctuation time series which reflect the oil-in-water two-phase flow characteristics have been collected. Then we investigate the time irreversibility of the collected fluctuation series. Note that the dimension of an oil-water two-phase system is typically 5 or more [47]; we use Casali's multiple testing strategy [38] to detect the oil bubble flow time irreversibility. Multiscale analysis method has also been employed to the time irreversibility detection, considering that oil-water two-phase flow dynamics can be revealed more clearly under different scales [48–50]. Moreover, we propose a novel criterion, that is, average of multiscale time irreversibility (AMSI) to quantitatively characterize the two-phase flow system time irreversibility. The results suggest that AMSI can be a sensitive indication to predict the flow pattern transition phenomenon.

2. Experiments and Data Acquisition

2.1. Experimental Setup. We carried out the low flow rate oil-water two-phase flow experiment in a vertical 20 mm inner diameter Plexiglass pipe. As shown in Figure 1, the oil-water two-phase flow loop consists of a water tank, an oil tank, a mix tank, two peristaltic metering pumps, and testing pipes.

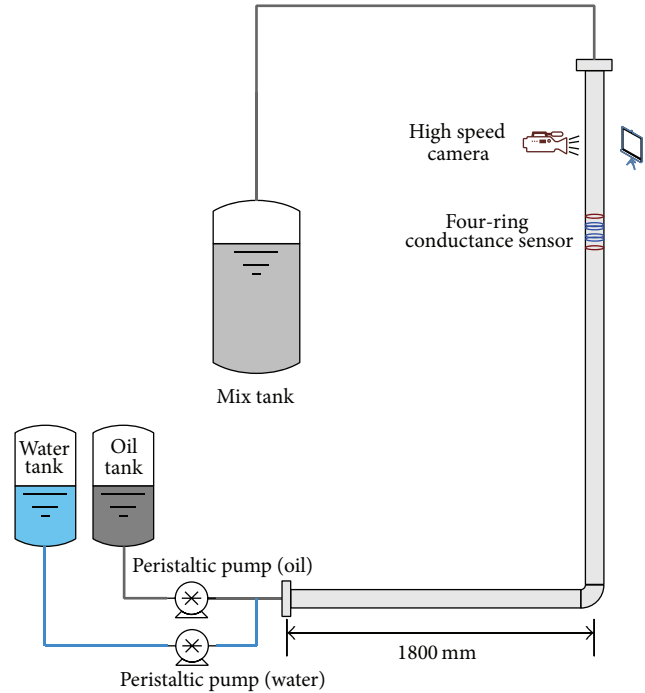


FIGURE 1: Schematic of oil-water flow loop facility.

During the experiment, the two phases, that is, oil and water, are first pumped out from the tanks, respectively, and mixed in the horizontal pipe section. Then the mixed fluid flows into the vertical test pipe, on which the measurement facility and sensor are installed. After the flow parameters and fluctuation measurement are done, the mixed fluid is drained into the mix tank to separate. The peristaltic pumps we used in the experiment are high precision metering pump, which can ensure precision of inlet flow rate and phase fraction.

In the experiment we employ a four-ring conductance sensor to collect the fluctuation signals. As shown in Figure 2, the sensor consists of four stainless steel pieces which are axially separated and flush mounted on the inside wall of the testing pipe. E1-E2 are the excitation electrodes that connected to a 20 KHz sinusoidal signal. H1-H2 are the measuring electrodes and the conductance fluctuating signals measured from H1-H2 are mainly correlated with the fluid fluctuations and dynamics. The detailed description of sensor geometry and working principle refers to our previous literatures [4, 51]. During the experiment, we also use a high speed digital camera to take snapshots of the fluid to identify the flow patterns and monitor the flow state.

The experimental schedule is as follows: we first fix the value of water phase fraction and then gradually increase the total velocity of the oil-water mixture flow. When the total flow rate reaches a preset value, the conductance fluctuation signal is collected. In the experiment, the water phase fraction is in the range of 70%–100%, while the mixture total flow rate was set at 0.01842 m/s, 0.03684 m/s, 0.07368 m/s, 0.11052 m/s, 0.14737 m/s, 0.18421 m/s, and 0.22105 m/s, respectively. The experiential mediums were tap water and white oil with a density of 856 kg/m³ and a viscosity of 11.984 cP (40 1C).

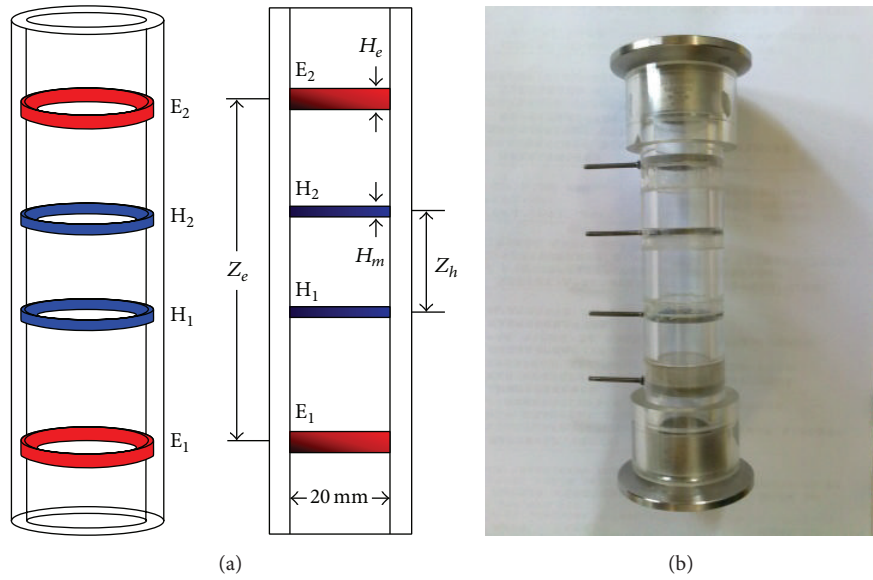


FIGURE 2: The four-ring conductance sensor. (a) Schematic of the sensor. (b) Real photo of the sensor.

The fluctuation signals from four-ring conductance sensor were recorded by National Instrument Corporation’s data acquisition card PXI 4472 which operated by LabVIEW software. During the experiment, we set the sampling rate as 6000 and the sampling duration as 30 s.

2.2. Flow Patterns and the Collected Conductance Fluctuation Signals. In the experiment we observed three kinds of oil dispersed flow patterns, that is, oil slug flow, oil bubble flow, and the very fine dispersed oil bubble flow (VFD bubble flow). The collected typical conductance signals under different mixture velocity are shown in Figure 3. Oil slug flow is the flow pattern that often occurs in very low mixture velocity. In this situation, the dispersed oil phase coalesces into oil slugs. With the aid of high speed camera, we observed that the oil slugs intermittently pass through the vertical testing pipe, and the intervals between two slugs exhibit some disequilibrium. As shown in Figure 3, the conductance signals of oil slug flow show obvious intermittent fluctuations indicating the large oil slugs passing through the sensitive area of the sensor. We also observed that the slug fluctuation amplitude is much higher than that of the other two flow patterns.

With increasing the total mixture velocity, the flow pattern changes to oil bubble flow. From the snapshots taken by high speed camera we find that the oil phase of bubble flow is distributed in the continuous water phase in the form of discrete bubbles, and the random motions of oil bubbles resulting in the conductance fluctuation signals show stochastic character. With even more increasing of the total mixture velocity, the discrete oil bubbles change to very small oil droplets that are uniformly distributed in the continuous water phase which is known as VFD bubble flow. The fluctuation signals of this flow pattern are noise-like but with even lower fluctuation amplitude than that of oil bubble flow.

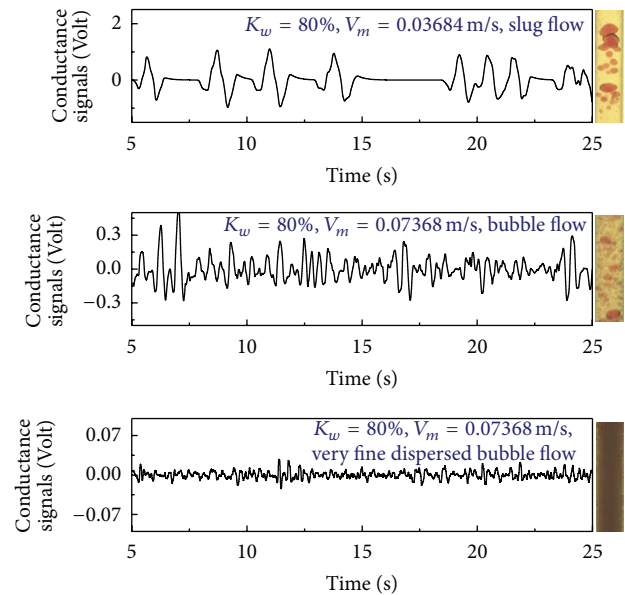


FIGURE 3: The conductance signals of three typical flow patterns.

3. Multiscale Time Irreversibility Index in m -Dimensional Phase Space

Note that the underlying flow dynamics of oil-in-water two-phase flow can be revealed more clearly and efficiently in multidimensional phase space; we employ Casali’s multitest strategy [38] to detect the m -dimensional time irreversibility of the oil-in-water two-phase flow. In addition, we extend this m -dimensional time irreversibility index with multiscale method, in the sense that oil-water two-phase flow exhibits various flow dynamics on different scales.

3.1. Multiple Testing Strategy for Irreversibility. Given a time series $x(i) = \{x_1, x_2, \dots, x_n\}$, the reconstructed m -dimensional vector can be expressed as

$$X(t) = [x(t), x(t + \tau), \dots, x(t + (m - 1)\tau)], \quad (1)$$

where τ refers to the delay time and m refers to the embedded dimension. The irreversibility of a time series in the bidimensional space can be revealed by quantified distribution of data points in the bidimensional plane $(x(i), x(i + 1))$ [33] or can be extracted by the probability characteristics of increments time series $y_L(t) = x(i + 1) - x(i)$ [27]. In order to detect multidimensional time irreversibility of a complex system, Casali et al. [38] first project the reconstructed phase space on to any orthogonal two-dimensional plane $(x(i), x(i + L))$, where $L = 0, \dots, m - 1$; then the m -dimensional time irreversibility can be evaluated by analyzing data distribution in each two-dimensional plane.

Here we employ Costa's index [27] to detect the time irreversibility of each projected plane. First we map the projections in each plane into increment series:

$$y_L(i) = x(i + L) - x(i), \quad 1 < i \leq n - m + 1, \quad (2)$$

where $y_L(i)$ refers to the increment series of plane $(x(i), x(i + L))$, and the time irreversibility index of this plane can be defined as follows:

$$A(L) = \frac{\sum_{y_L > 0} P(y_L) \ln [P(y_L)] - \sum_{y_L < 0} P(y_L) \ln [P(y_L)]}{\sum_{y_L} P(y_L) \ln [P(y_L)]}. \quad (3)$$

In (3) Shannon entropy is adopted to evaluate the system irreversibility, where $P(y_L)$ denotes the probability of the value y_L . Histogram of y_L is calculated to get the probability $P(y_L)$, and bin size is selected as the inverse of the signal sampling frequency. The number of data points in each bin and the bin number give the probability $P(y_L) = H(n)/N$, where $H(n)$ refers to the number of positive or negative data points in each bin and N refers to the divided bin number. $A(L)$ denotes the time irreversibility in plane $(x(i), x(i + L))$. The time irreversibility of an m -dimensional complex system then can be quantified by the following equation:

$$R = \frac{1}{m - 1} \sum_{L=1}^{m-1} A(L). \quad (4)$$

The system irreversibility can be characterized by (4). If R equals 0, the system is reversible, and the more R deviate from 0 the more irreversible the system is.

3.2. Multiscale Time Series Irreversibility. Complex systems always exhibit various behaviors at different scales, so it is an effective way to characterize the system dynamics from multiscale prospective. In this paper we extend the multiple testing strategy [38] for irreversibility with multiscale method [27]. First, we map the original time series $x(i) = \{x_1, x_2, \dots, x_n\}$ to coarse-grained time series as follows:

$$z^s(j) = \frac{1}{s} \sum_{i=(j-1)s+1}^{js} x(i), \quad 1 \leq j \leq \frac{n}{s}, \quad (5)$$

where $z^s(j)$ denotes the coarse-grained time series at scale s . Then by using $z^s(j)$, we can calculate the m -dimensional time irreversibility at each scale with (4):

$$R(s) = \frac{1}{m} \sum_{L=1}^{m-1} A_s(L), \quad (6)$$

where $R(s)$ refers to the m -dimensional time irreversibility at scale s and $A_s(L)$ denotes the time irreversibility index in projected plane $(x(i), x(i + L))$ at scale s . With this defined multiscale m -dimensional time irreversibility, we can detect the system disequilibrium in the multidimensional space which would provide rich dynamic information. In addition, adopting multiscale strategy provides a new way to reveal the system asymmetry from micro to the macro, which can characterize the complex system more precisely and clearly.

We now demonstrate how to quantitatively characterize the system disequilibrium with the average value of multiscale irreversibility (AMSI). This quantitative index can be expressed as follows:

$$\text{AMSI} = \sum_{s=1}^k R(s), \quad (7)$$

where AMSI refers to the average value of multiscale irreversibility and the scale range is from 1 to k .

4. Time Irreversibility Dynamics of Oil-in-Water Two-Phase Flow

4.1. Multidimensional Phase Space of Dispersed Oil Bubble and Slug Fluctuating Signals. With the defined multiple time irreversibility testing strategy, we explore the disequilibrium and underlying dynamics of three typical flow patterns, that is, oil slug flow, oil bubble flow, and very fine dispersed oil bubble flow. According to the embedded theory and the previous study of oil-water two-phase flow at similar flow conditions [47], we here choose the embedded dimension $m = 5$ and delay time $\tau = 6$ ms. Figure 4 shows the return maps of three different oil-water two-phase flow patterns at each projected two-dimensional plane. In order to spread the attractor and get a clear view, in Figure 4, we use coarse-grained signals at scale 20 to reconstruct the phase space. As we can see, the return map of slug flow shows up as obvious evolution trajectory and the range of the data points is relatively wider than that of the other two flow patterns, indicating the large signal fluctuations caused by the existence of oil slugs. The data range of oil bubble flow decreases comparing to that of the oil slug flow, due to the lower signal fluctuating amplitude. Also, we find that there still exist trajectories in the return map, indicating the existence of large oil bubbles formed by the bubble coalescence. Data points of VFD oil bubble flow are uniformly distributed in even smaller range, which show the stationary and stochastic character of small dispersed oil droplets. In Figure 4, the return maps in different projection plane contain rich dynamic information. Detecting the flow pattern disequilibrium from different projected plan can provide a novel way to characterize the flow pattern dynamic and evolution characteristic.

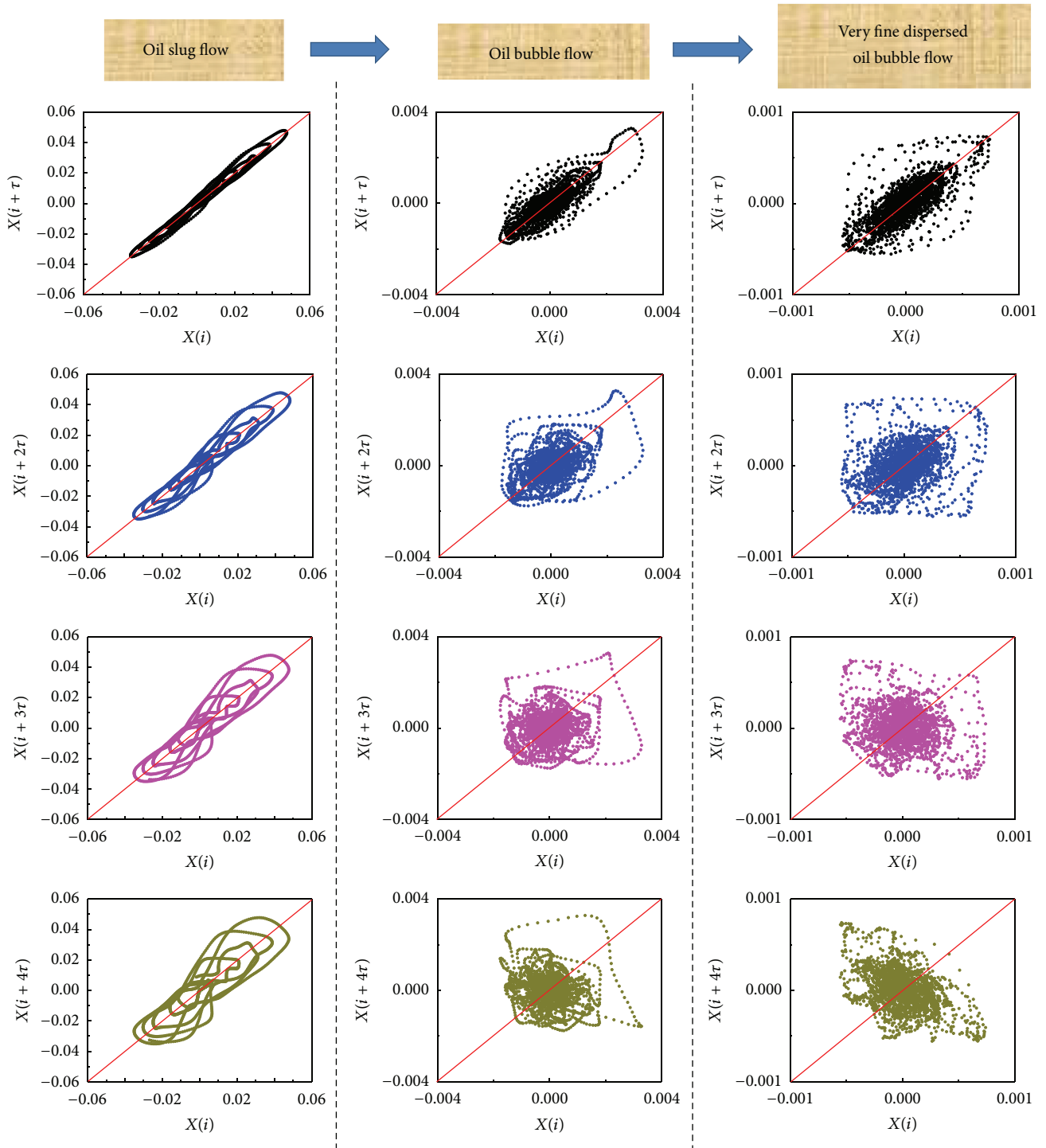


FIGURE 4: Return maps of three typical flow patterns at each projected two-dimensional plane. Each column represents the orthogonal projected planes of a typical flow pattern.

We also adopt the surrogate data approach [52, 53] to check the irreversibility of the collected fluctuation signals. Each of the 120 collected fluctuation signals has been used to generate surrogate data; thus a set of 120 surrogate types of data have been obtained. Figure 5 shows the return map of typical surrogate data and original signals for slug flow

and bubble flow. We find that the original signals of oil slug flow demonstrate clear asymmetry while the surrogate data of slug flow shows symmetry. This indicated the irreversibility feature of oil slug flow. What is more, compared to that of slug flow, original signals of bubbly flow show less asymmetry in the sense of the uniform distribution of oil bubbles.

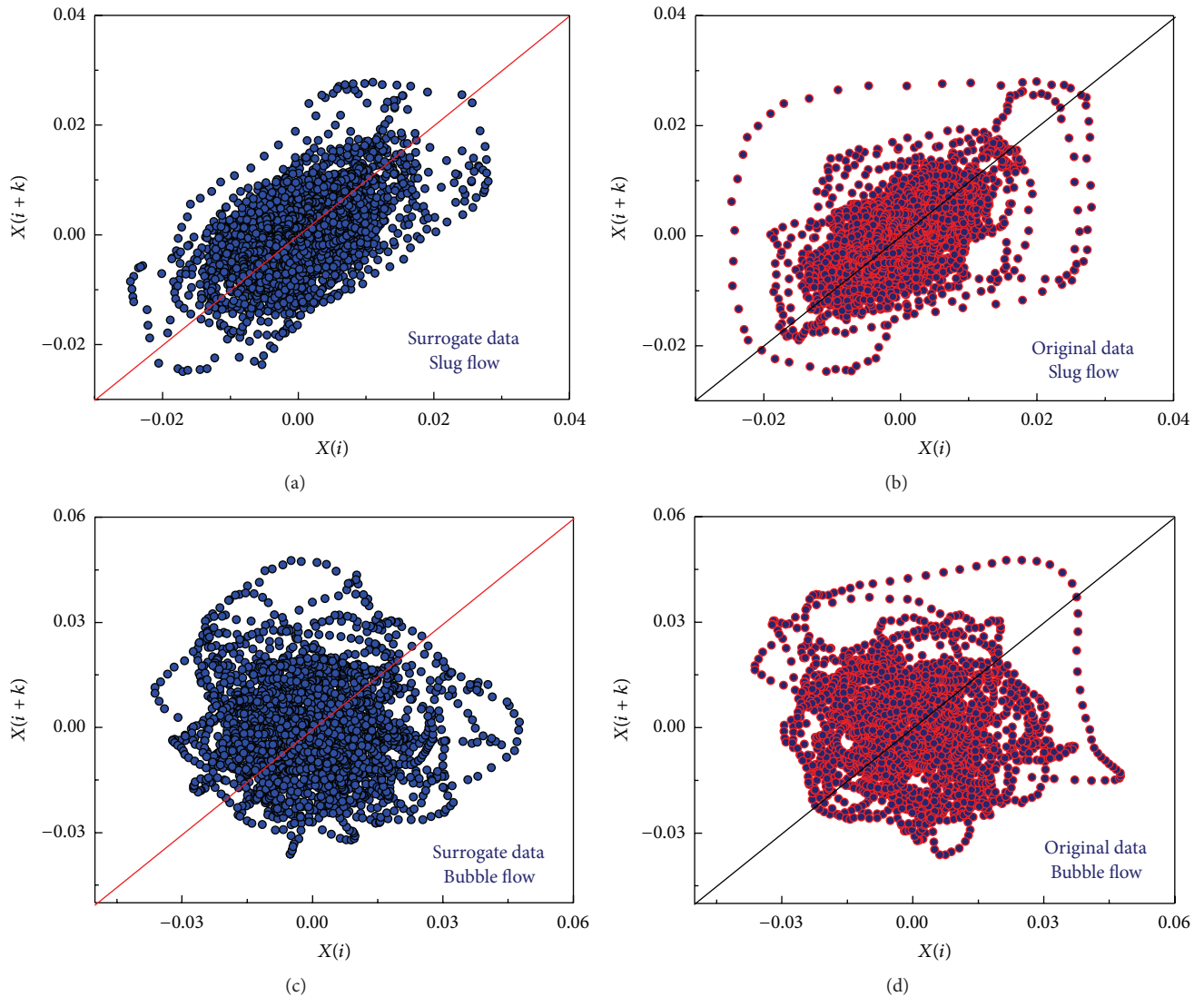


FIGURE 5: Return map of original signal and surrogate data. (a) Typical surrogate data of slug flow, (b) typical original signal of slug flow, (c) typical surrogate data of bubble flow, and (d) typical original signal of bubble flow.

The irreversibility index (AMSI) of original signals and surrogate signals is calculated and the results are shown in Figure 6, as we can see from original data irreversibility index, there exist obvious irreversibility changes when the flow pattern transition occurs (the flow pattern evolves from slug to bubble). However, the surrogate data irreversibility indexes of three different flow patterns are close to 0 and have no obvious changes, indicating that the nonlinear dynamics associate with flow pattern transition which is responsible for the data asymmetric distribution.

4.2. Detecting Oil-in-Water Two-Phase Flow Dynamics with Multiscale Time Irreversibility Index. Oil-water two-phase flow is quite a complex system such that the evolution of the flow pattern exhibits obvious polymorphism. In this regard, characterizing the flow pattern dynamics and irreversibility at a fixed time scale seems inadequate. Multiscale analysis

method provides an effective way to investigate the system characteristics from macro to micro. Investigating the multiscale time irreversibility of typical flow pattern signals can not only reveal the flow pattern disequilibrium, but also detect the flow pattern evolution character such as the bubble coalescence and breakup. We calculate the multiscale time irreversibility index of oil-water two-phase flow fluctuating signals with (6) and the scale range is from 1 to 50. The length of original analyzed signals is 60000 points with the sampling frequency of 6000. At the scale of 50 the length of the coarse-grained signal is 1200 points which keeps a sufficient number to safely estimate the irreversibility index. As shown in Figure 7 we list the multiscale index of eight typical flow conditions at a fixed water-cut (84%) while increasing the mixed velocity (from 0.01842 m/s to 0.22105 m/s). Three typical flow patterns are observed, that is, oil slug flow, oil bubble flow, and VFD oil bubble flow. As we can see in

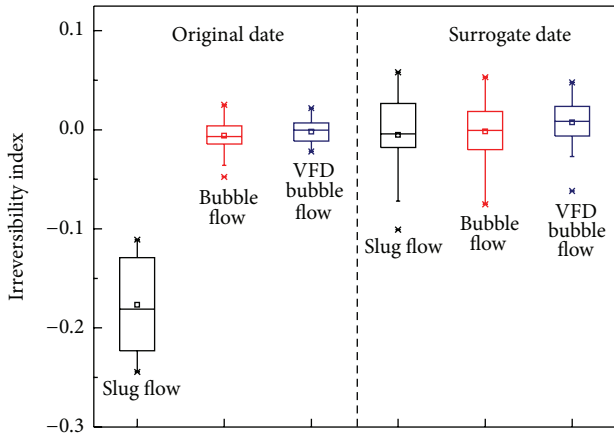


FIGURE 6: Time irreversibility index of original signals and the surrogate data.

Figure 7, the time irreversibility index of VFD bubble flow is around zero, which shows that the dispersed oil droplets are uniformly distributed in water and the mixed fluid is symmetrical. We also notice that the time irreversibility index has no obvious change from scale 1 to scale 50, indicating that the fluid structure of VFD bubble flow is symmetrical from micro to macro; that is, the mixed flow is spatially homogeneous along the pipe. Comparing to the VFD oil bubble flow, the time irreversibility of oil bubble flow has no obvious changes; the value of the irreversibility is still around 0 and independent of time scale. It reveals that although the mixture velocity of oil bubble flow decreases and the very fine dispersed oil droplets begin to coalesce into discrete oil bubbles, the oil bubbles still remain uniformly distributed and the flow structure shows spatially symmetrical character. It is also worth noticing that, under certain flow condition of low mixture velocity, the time irreversibility index of bubble flow slightly deviates from 0. This is probably due to the occasional presence of very large oil bubbles which are formed by the coalescence of discrete oil bubbles under low turbulence intensity. Oil slug flow occurs at very low mixture velocity; in this situation the flow turbulence intensity is extremely low and the dispersed oil phase coalesces into oil slug and bubble clusters. The intermittent presence of oil slugs in the pipe makes the fluid show disequilibrium and asymmetry feature. The multiscale time irreversibility index of slug flow has verified this phenomenon. As shown in Figure 7, the irreversibility index of oil slug flow is obvious which deviates from 0, showing the asymmetry character of slug flow. We also notice that the time irreversibility of slug flow increases with scale (the absolute value of irreversibility index increases with scale), indicating the disequilibrium and asymmetry of slug flow increase from micro special scale to macro special scale along the pipe.

We now demonstrate how to quantitatively characterize the flow disequilibrium under certain flow conditions with the average value of multiscale irreversibility (AMSI). Figure 8 shows the AMSI under different mixture velocity where the water-cut is fixed at 70%, 72%, 80%, 82%, 90%, and 92%, respectively. As shown in the figure, with increasing

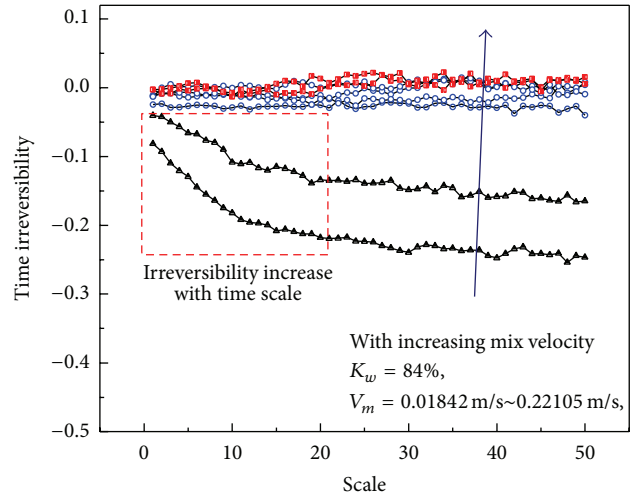


FIGURE 7: Multiscale time irreversibility of three typical flow patterns (water-cut $K_w = 84\%$ and mixture velocity $V_m = 0.01842 \text{ m/s} \sim 0.22105 \text{ m/s}$).

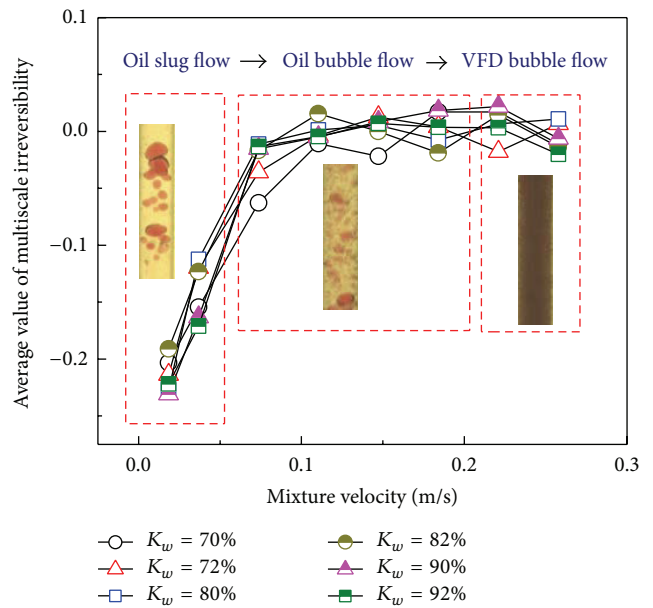


FIGURE 8: Average value of multiscale irreversibility under different mixture velocity.

the mixture velocity, the flow pattern evolves from oil slug flow to oil bubble flow and then VFD oil bubble flow. Correspondingly, the AMSI gradually increases. That is, the asymmetry of the mixed fluid decreases with increasing the mixture flow rate (the more the time irreversibility index deviated from 0, the more the asymmetry of the mixed fluid is). This can also be interpreted by the flow pattern evolution characteristics. Oil slug flow occurs at very low mixture velocity and the dispersed oil phase coalesces into large intermittent oil slugs, which lead to asymmetric

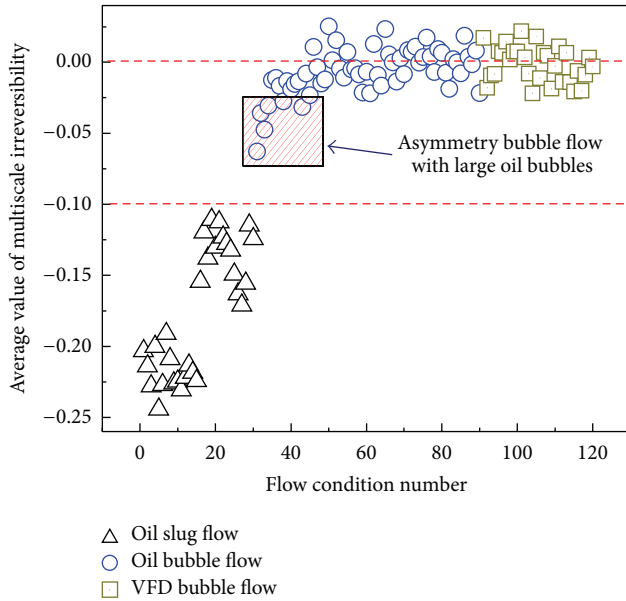


FIGURE 9: The average value of multiscale irreversibility of all the flow conditions.

character of the fluid structure. With increasing the mixture velocity, the turbulent intensity is high enough to break up the oil slugs into uniformly distributed oil bubbles and flow pattern changes to oil bubble flow. In this situation the flow structure changes from asymmetric to symmetric and the time irreversibility index is around 0. With even more increasing the mixture velocity, discrete oil bubbles are broken into smaller oil droplets which are also uniformly distributed. In this regard, the flow structure shows symmetry and the time irreversibility index is also around 0.

Figure 9 shows the AMSI of all 120 flow conditions. As we can see, most AMSI indexes of bubble flow and VFD bubble flow are around 0, indicating that oil bubble flow and VFD oil bubble flow are basically symmetric. Also, it is worth noticing that some AMSI indexes of oil bubble flow slightly derived from 0, which is probably because of the occasional presence of large oil bubbles that change the symmetry of the mixed fluid. The AMSI index of oil slug flow is lower than that of the other two flow patterns, and it is obviously deviated from 0 (below -0.1), which shows the asymmetrical character of the intermittent oil slugs. From this point of view the AMSI index can not only be used to characterize the two-phase flow spatial asymmetry and detect the flow pattern dynamic but also be employed as a criterion to identify the pattern transition and bubble coalescence.

We also compared the proposed AMSI index with other two time irreversibility indexes, that is, Porta's index [33] and Guzik's index [34]. As shown in Figure 10, both the AMSI index and Porta's index [33] can effectively demonstrate the system irreversibility when the flow pattern transition occurs (both the AMSI index and Porta's index [33] have obvious changes with the flow pattern evolving from slug to bubble flow). However, Guzik's index [34] is less sensitive for characterizing the flow pattern transition dynamics. So

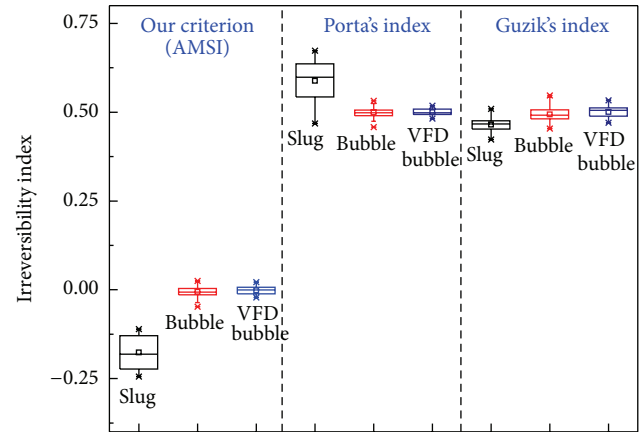


FIGURE 10: Comparison of AMSI index, Porta's index [33], and Guzik's index [34].

we think that the proposed AMSI index is sufficient and effective for characterizing the dynamics associated with the flow pattern transition.

5. Conclusions

Characterizing the low flow rate oil-in-water two-phase flow disequilibrium with experimental measurement signals has been a challenging problem in the fields of time series analysis and fluid dynamics. In this paper, we first experimentally investigate the oil-in-water two-phase flow in a vertical pipe and collect conductance fluctuating time series that reflect the fluid dynamics. Then we detected the flow disequilibrium with two strategies, that is, multidimensional time irreversibility and multiscale time irreversibility. We find that the collected fluctuating signals of oil bubble flow and very fine dispersed oil bubble flow are reversible while the signals of slug flow show irreversible character. This indicates that both the oil bubble flow and very fine dispersed oil bubble flow have the symmetric structure while oil slug flow shows asymmetric flow characteristics due to the intermittent presence of oil slugs. Moreover, we propose a novel criterion, that is, AMSI, to quantitatively characterize the flow asymmetry character. The results show that the AMSI which is sensitive to the flow conditions can be used to identify flow patterns and predict dispersed phase coalescence phenomenon. Our research not only reveals the oil-water two-phase flow pattern evolution character but also provides a novel application of time series irreversibility analysis to uncover the fluid dynamics.

Competing Interests

The authors declare that they have no competing interests.

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