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### Crystal structure of the formal 20 electron zirconocene pentafulvene complex $Cp_2Zr(\eta^5,\eta^1-adamantylidenepentafulvene):$ toluene:*n*-hexane = 1:0.125:0.125

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The crystal structure of a solvated zirconocene pentafulvene complex with a bulky adamantylidene substitution pattern, namely  $(\eta^5, \eta^1$ -adamantylidenepentafulvene) bis $(\eta^5$ -cyclopentadienyl) zirconium(IV)-toluene-*n*-hexane (8/1/ 1), [Zr(C<sub>15</sub>H<sub>18</sub>)(C<sub>5</sub>H<sub>5</sub>)<sub>2</sub>]·0.125C<sub>7</sub>H<sub>8</sub>·0.125C<sub>6</sub>H<sub>14</sub>, is reported. Reducing zirconocene dichloride with magnesium results in the formation of a low-valent zirconocene reagent that reacts readily with adamantylidenepentafulvene to give the aforementioned complex. Single crystal X-ray diffraction proves the dianion-like  $\eta^5:\eta^1$  binding mode of the fulvene ligand to the central Zr<sup>IV</sup> atom. The asymmetric unit contains four independent molecules of  $[\eta^5:\eta^1-adamanty]$ idenepentafulvene]bis[ $(\eta^5)$ -cyclopentadienyl]zirconium(IV), together with half a molecule of toluene disordered with half a molecule of *n*-hexane (the solvent molecules have no direct influence on the complex). In each of the four complex molecules, the central Zr<sup>IV</sup> atom has a distorted tetrahedral coordination environment. The measured crystal consisted of two domains with a refined ratio of 0.77:0.23.

#### 1. Chemical context

Over the last few decades, pentafulvenes have found plenty of applications in organometallic chemistry (Preethalayam et al., 2017; Neuenschwander, 1989), one of which is their use as versatile ligands for a variety of early and late transition metals featuring a multitude of coordination modes and reactivity patterns (Preethalayam et al., 2017; Kreindlin & Rybinskaya, 2004). Whereas for late transition metals  $\eta^2$ - and  $\eta^4$ -bindng modes are known (Kim *et al.*, 2000; Rais & Bergman, 2004), most metals are bound in an  $\eta^6$ -manner. either in a neutral olefinic  $\eta^2: \eta^2: \eta^2$  (Konietzny *et al.*, 2010) or in a dianionic  $\eta^5:\eta^1$  fashion (Ebert *et al.*, 2014). The change of polarity at the exocyclic carbon atom of the pentafulvene ligand, resulting from its bonding to the central metal atom, enables a multitude of insertion reactions and C-H-activation reactions that are of great interest to our research group (Ebert et al., 2014; Manssen et al., 2015, 2017; Oswald et al., 2016). In this context we have recently reported the syntheses of the first zirconocene-based pentafulvene complexes and their reactivities (Jaroschik et al., 2017). Here we report the synthesis and crystal structure of the solvated title compound,  $(\eta^5, \eta^1$ -adamantylidenepentafulvene)bis $(\eta^5$ -cyclopentadienyl)zirconium(IV), 1.



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#### 2. Structural commentary

Compound 1 crystallizes in the triclinic space group  $P\overline{1}$  with four formula units per asymmetric unit together with one disordered solvent molecule (ratio toluene: n-hexane = 1:1). Fig. 1 shows one of the complex molecules present in the crystal of **1**. As a result of the high similarities with respect to structural parameters (bond lengths and angles) of the four complexes in the asymmetric unit, only this complex (Zr1) is discussed in detail. The molecular structure shows the zirconium(IV) atom to be in a distorted tetrahedral coordination environment. The zirconium atom lies 0.21 Å above the plane defined by the three centroids of the pentafulvene and cyclopentadienyl ligands, which is in good agreement with related complexes, e.g. 0.20 Å for the analogous complex with a 6,6'-di-para-tolylfulvene substitution pattern (Jaroschik et al., 2017) and 0.20 Å for Cp<sub>3</sub>ZrH (Edelbach et al., 1999). The molecular structure of 1 in the solid state clearly confirms the  $\pi - \eta^5 : \sigma - \eta^1$  binding mode of the fulvene moiety to the central metal atom. Characteristic parameters for this coordination mode are the deviation (bend angle  $\theta$ ) of the C<sub>exo</sub>-C<sub>ipso</sub> bond



Figure 1

One of the four independent complex molecules in the crystal structure of **1**. Displacement ellipsoids are drawn at the 50% probability level. H atoms and solvent molecules have been omitted for clarity.

toward the central zirconium(IV) atom (29.4 $^{\circ}$ ) as well as the ring slippage ( $\Delta$ ) toward the C<sub>ipso</sub> atom of the five-membered ring of the pentafulvene ligand (0.318 Å). The bond between the zirconium(IV) atom and the exocyclic carbon atom [Zr1-C16 = 2.605 (3) Å] is considerably longer than those of other zirconium complexes [Kraft et al., 2002 (2.37 Å); Novarino et al., 2011 (2.37 Å)], indicating a weak  $Zr - C_{exo}$  contact, but in good agreement with  $[\pi - \eta^5: \sigma - \eta^1 - C_5 H_4 = C(para-tolyl)_2]$ -Zr(THF) (2.70 and 2.71 Å) reported previously by our group (Ebert et al., 2014). Regarding the fulvene moiety, the coordination to the zirconocene fragment leads to the loss of the alternating single- and double-bond pattern of free pentafulvene. This is indicated by the narrow range of the C-Cbond lengths within the five-membered ring of the fulvene ligand [1.406 (4) to 1.437 (4) Å] in comparison with free fulvene [1.327 (3) to 1.459 (2) Å] (Garcia et al., 1989). Hence, the hybridization of the exocyclic carbon atom lies between  $sp^2$  and  $sp^3$ , which is further confirmed by the sum of angles around the C16 carbon atom  $[C11-C16-C17 = 116.9 (2)^{\circ},$  $C17 - C16 - C21 = 109.4 (2)^{\circ}, C11 - C16 - C21 = 118.7 (3)^{\circ} =$ 345°].

#### 3. Supramolecular features

No significant supramolecular features between the complex molecules or between the complex molecules and the solvent





A view along the a axis showing the packing of molecules in the crystal structure of compound **1**. Solvent molecules have been omitted for clarity. No significant supramolecular features can be observed. Color code: C grey, H white, Zr plum spheres.

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Table 1	
Experimental details.	
Crystal data	
Chemical formula	$[Zr(C_{15}H_{18})(C_5H_5)_2] \cdot 0.125C_7H_8 - 0.125C_6H_{14}$
M <sub>r</sub>	441.98
Crystal system, space group	Triclinic, $P\overline{1}$
Temperature (K)	105
<i>a</i> , <i>b</i> , <i>c</i> (Å)	13.6751 (6), 16.0733 (7), 19.5889 (9)
$lpha,eta,\gamma(^\circ)$	98.6919 (18), 109.4236 (16), 90.5484 (16)
$V(Å^3)$	4005.8 (3)
Z	8
Radiation type	Μο Κα
$\mu (\text{mm}^{-1})$	0.56
Crystal size (mm)	$0.28 \times 0.24 \times 0.04$
Data collection	
Diffractometer	Bruker APEXII CCD
Absorption correction	Multi-scan ( <i>TWINABS</i> ; Bruker, 2013)
$T_{\min}, T_{\max}$	0.900, 1.000
No. of measured, independent and observed $[I > 2\sigma(I)]$ reflections	67120, 67120, 48102
$(\sin \theta / \lambda)_{\max} ( \mathring{A}^{-1} )$	0.746
Refinement	
$R[F^2 > 2\sigma(F^2)], wR(F^2), S$	0.044, 0.110, 1.01
No. of reflections	67120
No. of parameters	1058
No. of restraints	72
H-atom treatment	H-atom parameters constrained
$\Delta \rho_{\rm max},  \Delta \rho_{\rm min} \ ({\rm e} \ {\rm \AA}^{-3})$	1.04, -0.91

Computer programs: APEX2 and SAINT (Bruker, 2013), SHELXS2013 (Sheldrick, 2015a), SHELXL2014 (Sheldrick, 2015b), DIAMOND (Brandenburg & Putz, 2006) and publCIF (Westrip, 2010).

molecules are observed. Hence the intermolecular forces appear to be dominated by van der Waals interactions only. In the crystal structure of **1**, the solvent molecules are located in the voids resulting from the packing arrangements of the complex molecules. Fig. 2 shows the packing without solvent molecules and Fig. 3 the packing with the contribution of the solvents.

#### 4. Synthesis and crystallization

All reactions were carried out under a dry nitrogen atmosphere using Schlenk techniques or in a glove box. Zirconocene dichloride was purchased from Strem Chemicals and used as received. Adamantylidenepentafulvene was prepared according to a published procedure (Miller & Bercaw, 2006). Solvents were dried according to standard procedures over Na/K alloy with benzophenone as indicator and distilled under a nitrogen atmosphere.

Zirconocene dichloride (1.000 g, 3.421 mmol), magnesium (0.083 g, 3.421 mmol) and adamantylidenefulvene (0.884 g, 3.421 mmol) were added to a Schlenk tube under argon. THF (40 ml) was added, and the reaction was stirred for 16 h at room temperature. THF was evaporated under vacuum and 40 ml of toluene were added to the crude product. After filtration, toluene was evaporated under vacuum to give **1** as a yellow solid in 81% yield.



Figure 3

A view along the a axis showing the packing of molecules in the asymmetric unit. Color code: C grey, H white, Zr plum spheres. Solvent molecules are highlighted in black.

Crystals suitable for single crystal X-ray diffraction were obtained from a saturated solution of 1 in toluene, layered with *n*-hexane at room temperature.

#### 5. Refinement

Crystal data, data collection and structure refinement details are summarized in Table 1.

The measured crystal consisted of two domains. *TWINABS* was therefore used to model the absorption correction and to generate a reflection file in the HKLF5 format. The refined ratio of the two domains was 0.77:0.23. Hydrogen atoms bonded to the carbon atoms were located from difference-Fourier maps but were subsequently fixed to idealized positions using appropriate riding models with  $U_{iso}(H) = 1.2U_{eq}(C)$ . Reflections (001) and (001) were obstructed from the primary beam stop and consequently omitted from the refinement. The solvent molecules toluene and *n*-hexane were located from difference maps and refined with RIGU commands, with site occupancies fixed to 0.50 each.

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Crystal structure of the formal 20 electron zirconocene pentafulvene complex  $Cp_2Zr(\eta^5,\eta^1-adamantylidenepentafulvene):toluene:$ *n*-hexane = 1:0.125:0.125

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**Computing details** 

Data collection: *APEX2* (Bruker, 2013); cell refinement: *SAINT* (Bruker, 2013); data reduction: *SAINT* (Bruker, 2013); program(s) used to solve structure: *SHELXS2013* (Sheldrick, 2015*a*); program(s) used to refine structure: *SHELXL2014* (Sheldrick, 2015*b*); molecular graphics: *DIAMOND* (Brandenburg & Putz, 2006); software used to prepare material for publication: *publCIF* (Westrip, 2010).

 $(\eta^5, \eta^1$ -Adamantylidenepentafulvene)bis $(\eta^5$ -cyclopentadienyl)zirconium(IV)-toluene-*n*-hexane (8/1/1)

### Crystal data

 $[Zr(C_{15}H_{18})(C_{5}H_{5})_{2}] \cdot 0.125C_{7}H_{8} \cdot 0.125C_{6}H_{14}$   $M_{r} = 441.98$ Triclinic,  $P\overline{1}$  a = 13.6751 (6) Å b = 16.0733 (7) Å c = 19.5889 (9) Å a = 98.6919 (18)°  $\beta = 109.4236$  (16)°  $\gamma = 90.5484$  (16)° V = 4005.8 (3) Å<sup>3</sup>

### Data collection

Bruker APEXII CCD diffractometer Radiation source: sealed tube  $\varphi$  and  $\omega$  scans Absorption correction: multi-scan (*TWINABS*; Bruker, 2013)  $T_{\min} = 0.900, T_{\max} = 1.000$ 

#### Refinement

Refinement on  $F^2$ Least-squares matrix: full  $R[F^2 > 2\sigma(F^2)] = 0.044$  $wR(F^2) = 0.110$ S = 1.0167120 reflections 1058 parameters 72 restraints Primary atom site location: structure-invariant direct methods Z = 8 F(000) = 1844  $D_x = 1.466 \text{ Mg m}^{-3}$ Mo K $\alpha$  radiation,  $\lambda = 0.71073 \text{ Å}$ Cell parameters from 6013 reflections  $\theta = 2.2-31.9^{\circ}$   $\mu = 0.56 \text{ mm}^{-1}$ T = 105 K Plate, yellow  $0.28 \times 0.24 \times 0.04 \text{ mm}$ 

67120 measured reflections 67120 independent reflections 48102 reflections with  $I > 2\sigma(I)$  $\theta_{\text{max}} = 32.0^{\circ}, \theta_{\text{min}} = 1.3^{\circ}$  $h = -20 \rightarrow 20$  $k = -23 \rightarrow 23$  $l = -29 \rightarrow 29$ 

Secondary atom site location: difference Fourier map Hydrogen site location: difference Fourier map H-atom parameters constrained  $w = 1/[\sigma^2(F_o^2) + (0.040P)^2 + 4.P]$ where  $P = (F_o^2 + 2F_c^2)/3$  $(\Delta/\sigma)_{max} = 0.002$  $\Delta\rho_{max} = 1.04$  e Å<sup>-3</sup>  $\Delta\rho_{min} = -0.91$  e Å<sup>-3</sup>

### Special details

**Geometry**. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Refinement. Refined as a 2-component twin

	x	у	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	Occ. (<1)
Zr1	0.34828 (2)	0.23916 (2)	0.66261 (2)	0.01264 (6)	
C1	0.4036 (2)	0.11710 (19)	0.7380 (2)	0.0277 (7)	
H1	0.4576	0.1313	0.7840	0.033*	
C2	0.4159 (2)	0.08779 (19)	0.6707 (2)	0.0295 (8)	
H2	0.4799	0.0757	0.6634	0.035*	
C3	0.3174 (2)	0.07918 (17)	0.61545 (19)	0.0239 (6)	
Н3	0.3034	0.0645	0.5641	0.029*	
C4	0.2435 (2)	0.09648 (18)	0.65087 (19)	0.0236 (6)	
H4	0.1702	0.0916	0.6276	0.028*	
C5	0.2957 (2)	0.12171 (19)	0.72507 (19)	0.0260 (7)	
Н5	0.2645	0.1391	0.7612	0.031*	
C6	0.2160 (2)	0.33703 (19)	0.69904 (18)	0.0222 (6)	
H6	0.2347	0.3591	0.7498	0.027*	
C7	0.15621 (19)	0.26119 (18)	0.66255 (18)	0.0211 (6)	
H7	0.1248	0.2244	0.6841	0.025*	
C8	0.1513 (2)	0.24974 (19)	0.58924 (18)	0.0232 (6)	
H8	0.1178	0.2029	0.5527	0.028*	
С9	0.2046 (2)	0.3198 (2)	0.57885 (19)	0.0258 (6)	
H9	0.2131	0.3286	0.5342	0.031*	
C10	0.2429 (2)	0.37398 (18)	0.6462 (2)	0.0251 (7)	
H10	0.2805	0.4267	0.6550	0.030*	
C11	0.50795 (18)	0.31699 (16)	0.70541 (16)	0.0149 (5)	
C12	0.45190 (19)	0.35608 (17)	0.64371 (16)	0.0162 (5)	
H12	0.4286	0.4116	0.6464	0.019*	
C13	0.43710 (19)	0.29892 (18)	0.57876 (16)	0.0175 (5)	
H13	0.3993	0.3081	0.5305	0.021*	
C14	0.48798 (19)	0.22570 (18)	0.59757 (16)	0.0175 (5)	
H14	0.4904	0.1769	0.5642	0.021*	
C15	0.53463 (18)	0.23734 (17)	0.67431 (16)	0.0158 (5)	
H15	0.5770	0.1987	0.7013	0.019*	
C16	0.48953 (19)	0.32835 (18)	0.77477 (16)	0.0175 (5)	
C17	0.5652 (2)	0.29025 (19)	0.83666 (16)	0.0202 (6)	
H17	0.5805	0.2326	0.8171	0.024*	
C18	0.5207 (2)	0.2850(2)	0.89840 (18)	0.0282 (7)	
H18A	0.4553	0.2488	0.8790	0.034*	
H18B	0.5707	0.2595	0.9377	0.034*	
C19	0.4996 (2)	0.3735 (2)	0.92980 (19)	0.0327 (8)	
H19	0.4703	0.3698	0.9698	0.039*	

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(\AA^2)$ 

C20	0.4203 (2)	0.4103 (2)	0.86754 (18)	0.0304 (7)
H20A	0.3550	0.3740	0.8482	0.036*
H20B	0.4044	0.4672	0.8868	0.036*
C21	0.4643 (2)	0.41597 (19)	0.80549 (17)	0.0225 (6)
H21	0.4128	0.4405	0.7654	0.027*
C22	0.6668 (2)	0.3476 (2)	0.86836 (18)	0.0243 (6)
H22A	0.7178	0.3233	0.9080	0.029*
H22B	0.6971	0.3510	0.8294	0.029*
C23	0.5999 (3)	0.4300 (2)	0.96032 (19)	0.0333 (8)
H23A	0.6512	0.4062	1.0003	0.040*
H23B	0.5857	0.4869	0.9808	0.040*
C24	0.5656 (2)	0.4735 (2)	0.83771 (19)	0.0281 (7)
H24A	0.5949	0.4790	0.7986	0.034*
H24B	0.5504	0 5305	0.8574	0.034*
C25	0.6443(2)	0.3363(2)	0 89874 (19)	0.021
H25	0.7101	0.4731	0.9187	0.034*
7r2	0.33274(2)	0.74120(2)	0.66375(2)	0.031
C26	0.33271(2) 0.4932(2)	0.71120(2) 0.8472(3)	0.60375(2)	0.0361(9)
H26	0.5029	0.8891	0.7395	0.043*
C27	0.3029 0.4365 (2)	0.8540(2)	0.6258 (2)	0.045 0.0276(7)
H27	0.4031	0.0040 (2)	0.6094	0.0270(7)
C28	0.4031 0.4371(2)	0.7024	0.58141(18)	0.033
C28	0.4371(2)	0.7770 (2)	0.58141(10) 0.5302	0.0275(7)
C20	0.4010	0.7023	0.5502	0.033
U29	0.5009 (5)	0.7201(2)	0.0208 (2)	0.0380 (10)
П29 С20	0.5100 0.5224(2)	0.0713 0.7678(2)	0.0111	$0.040^{\circ}$
C30	0.5554 (2)	0.7078 (3)	0.0977 (2)	0.0423 (10)
П30 С21	0.3700	0.7404	0.7390 0.7418 (2)	$0.031^{\circ}$
	0.3003 (3)	0.0190(2)	0.7410(2) 0.7024	0.0377(8)
ПЭТ С22	0.3838	0.0372	0.7934	$0.043^{\circ}$
0.52	0.4224 (3)	0.0010(2)	0.0991(3)	0.0407 (10)
П32 С22	0.4901	0.6020	0.7107	$0.049^{\circ}$
(33	0.3600 (4)	0.5831 (2)	0.62/1(3)	0.0476(12)
H33	0.3828	0.5097	0.5801	0.05/*
C34	0.2572 (3)	0.58/3 (2)	0.6246 (3)	0.0499 (12)
H34	0.1973	0.5780	0.5817	0.060*
035	0.2586 (3)	0.6076 (2)	0.6958 (3)	0.041/(11)
H35	0.1992	0.6124	0.7106	0.050*
C36	0.22181 (19)	0.83159 (16)	0.70249 (15)	0.0148 (5)
C37	0.15190 (18)	0.75914 (17)	0.66475 (16)	0.0166 (5)
H37	0.1218	0.7226	0.6872	0.020*
C38	0.13525 (19)	0.75110 (19)	0.58924 (16)	0.0194 (6)
H38	0.0946	0.7070	0.5524	0.023*
C39	0.1891 (2)	0.81971 (18)	0.57744 (16)	0.0195 (5)
H39	0.1915	0.8296	0.5314	0.023*
C40	0.2386 (2)	0.87093 (17)	0.64555 (15)	0.0162 (5)
H40	0.2770	0.9230	0.6529	0.019*
C41	0.30012 (19)	0.83558 (17)	0.77373 (16)	0.0165 (5)
C42	0.3601 (2)	0.92080 (19)	0.80907 (17)	0.0222 (6)

H42	0.3795	0.9464	0.7715	0.027*
C43	0.4583 (2)	0.9108 (2)	0.87292 (18)	0.0302(7)
H43A	0.4959	0.9665	0.8950	0.036*
H43B	0.5048	0.8737	0.8547	0.036*
C44	0.4288 (2)	0.8724 (2)	0.93092 (18)	0.0316(7)
H44	0.4932	0.8655	0.9723	0.038*
C45	0.3719 (2)	0.7856 (2)	0.89559 (18)	0.0280(7)
H45A	0.4182	0.7482	0.8775	0.034*
H45B	0.3532	0.7596	0.9326	0.034*
C46	0.2733 (2)	0.79519 (19)	0.83160 (16)	0.0195 (6)
H46	0.2361	0.7387	0.8090	0.023*
C47	0.2898 (2)	0.97955 (19)	0.83913 (18)	0.0265 (7)
H47A	0.3271	1.0354	0.8615	0.032*
H47B	0.2263	0.9877	0.7985	0.032*
C48	0.3582 (3)	0.9296 (2)	0.96019 (19)	0.0323 (8)
H48A	0.3393	0.9044	0.9976	0.039*
H48B	0.3951	0.9853	0.9837	0.039*
C49	0.2023 (2)	0.85360 (19)	0.86180 (17)	0.0226 (6)
H49A	0.1377	0.8602	0.8214	0.027*
H49B	0.1831	0.8281	0.8989	0.027*
C50	0.2600 (2)	0.9406 (2)	0.89689 (18)	0.0266 (7)
H50	0.2139	0.9784	0.9159	0.032*
Zr3	0.17259 (2)	0.02164 (2)	0.35641 (2)	0.01183 (5)
C51	0.2177 (3)	0.15654 (19)	0.3091 (2)	0.0295 (7)
H51	0.2407	0.1475	0.2680	0.035*
C52	0.2799 (2)	0.16506 (18)	0.3813 (2)	0.0263 (7)
H52	0.3535	0.1650	0.3987	0.032*
C53	0.2165 (2)	0.17380 (18)	0.42502 (18)	0.0233 (6)
H53	0.2390	0.1769	0.4768	0.028*
C54	0.1140 (2)	0.17722 (18)	0.3784 (2)	0.0243 (7)
H54	0.0552	0.1871	0.3934	0.029*
C55	0.1135 (2)	0.16350 (19)	0.3063 (2)	0.0286 (7)
H55	0.0541	0.1596	0.2632	0.034*
C56	-0.0062 (2)	-0.0617 (2)	0.3120 (2)	0.0342 (9)
H56	-0.0303	-0.0868	0.2617	0.041*
C57	-0.0243 (2)	0.02045 (19)	0.34153 (19)	0.0242 (7)
H57	-0.0646	0.0602	0.3148	0.029*
C58	0.0274 (2)	0.0321 (2)	0.41629 (19)	0.0266 (7)
H58	0.0281	0.0816	0.4498	0.032*
C59	0.0777 (3)	-0.0391 (2)	0.4347 (2)	0.0337 (8)
H59	0.1209	-0.0462	0.4825	0.040*
C60	0.0545 (2)	-0.09897 (19)	0.3716 (2)	0.0370 (10)
H60	0.0758	-0.1551	0.3691	0.044*
C61	0.2692 (2)	-0.06680 (17)	0.30162 (17)	0.0183 (6)
C62	0.2524 (2)	-0.11713 (18)	0.35200 (17)	0.0202 (6)
H62	0.2097	-0.1680	0.3385	0.024*
C63	0.3090 (2)	-0.0795 (2)	0.42394 (19)	0.0248 (6)
H63	0.3086	-0.0989	0.4673	0.030*

C64	0.3669 (2)	-0.0073 (2)	0.42099 (19)	0.0249 (6)
H64	0.4116	0.0303	0.4619	0.030*
C65	0.3463 (2)	-0.00141 (19)	0.34688 (18)	0.0224 (6)
H65	0.3783	0.0394	0.3292	0.027*
C66	0.1889 (2)	-0.05370 (18)	0.23524 (17)	0.0196 (6)
C67	0.2210 (3)	-0.0062(2)	0.18306 (19)	0.0269 (7)
H67	0.2693	0.0435	0.2120	0.032*
C68	0.1258 (3)	0.0237 (2)	0.1271 (2)	0.0364 (8)
H68A	0.0898	0.0635	0.1530	0.044*
H68B	0.1482	0.0538	0.0938	0.044*
C69	0.0517 (3)	-0.0514 (3)	0.0829 (2)	0.0415 (9)
H69	-0.0107	-0.0314	0.0470	0.050*
C70	0.0179 (3)	-0.0972(2)	0.1348 (2)	0.0365 (8)
H70A	-0.0307	-0.1460	0.1063	0.044*
H70B	-0.0188	-0.0587	0.1610	0.044*
C71	0.1129 (2)	-0.1280(2)	0.19077 (18)	0.0257 (6)
H71	0.0901	-0.1583	0.2244	0.031*
C72	0.2770 (3)	-0.0669(2)	0.1411 (2)	0.0370 (9)
H72A	0.3000	-0.0370	0.1079	0.044*
H72B	0 3391	-0.0866	0 1764	0.044*
C73	0.1075 (4)	-0.1122(3)	0.0413(2)	0.0483 (11)
H73A	0.0593	-0.1610	0.0119	0.058*
H73B	0.1296	-0.0828	0.0074	0.058*
C74	0.1684(3)	-0.1886(2)	0.1486(2)	0.0331 (8)
H74A	0.2301	-0.2088	0.1838	0.040*
H74B	0.1208	-0.2381	0.1205	0.040*
C75	0.2020(3)	-0.1429(2)	0.0962(2)	0.0401 (9)
H75	0.2381	-0.1823	0.0694	0.048*
Zr4	0.16561(2)	0 52009 (2)	0.35633(2)	0.01146(5)
C76	0.10501(2) 0.2956(2)	0.52009(2) 0.41870(19)	0.32033(2) 0.3221(2)	0.0279(7)
е76 H76	0.2749	0.3925	0.2722	0.024*
C77	0.2735(2)	0.3923 0.38672 (19)	0.2722 0.3785 (2)	0.0290(7)
H77	0.2381	0.3340	0.3739	0.0258
C78	0.2301 0.3130(2)	0.5510 0.4463 (2)	0.44286 (19)	0.025 0.0263 (7)
H78	0.3061	0.4424	0.4890	0.0205 (7)
C79	0.3649(2)	0.51291 (19)	0.42664 (18)	0.0223 (6)
H79	0.4011	0.5610	0.4606	0.0223 (0)
C80	0.3538(2)	0.49636 (19)	0.35210 (19)	0.027
H80	0.3807	0.5311	0.3265	0.029*
C81	0.2010(3)	0.65239 (19)	0.3203	0.029
H81	0.2182	0.6415	0.2588	0.0255 (7)
C82	0.2102 0.2712(2)	0.6405(17)	0.2588	0.031
H82	0.2712(2) 0.3447	0.6655	0.3877	0.0210(0)
C83	0.2138 (2)	0.67337 (17)	0.3077	0.020
H83	0.2130 (2)	0.6782	0.42211(17) 0.4740	0.0201 (0)
C84	0.2713 0 1083 (2)	0.0702	0 37968 (10)	0.024
U07 H8/	0.1005 (2)	0.6834	0.37908(19)	0.0237 (0)
C 85	0.0020	0.000-	0.3901	0.0267(7)
005	0.0999 (2)	0.03900 (19)	0.30333 (19)	0.0207(7)

H85	0.0373	0.6553	0.2653	0.032*	
C86	0.00649 (18)	0.44439 (17)	0.29543 (16)	0.0164 (5)	
C87	-0.02264 (19)	0.51655 (18)	0.33577 (16)	0.0178 (5)	
H87	-0.0615	0.5607	0.3150	0.021*	
C88	0.0155 (2)	0.5111 (2)	0.41062 (17)	0.0226 (6)	
H88	0.0103	0.5523	0.4493	0.027*	
C89	0.0627 (2)	0.4343 (2)	0.41867 (17)	0.0223 (6)	
H89	0.0945	0.4144	0.4637	0.027*	
C90	0.0549 (2)	0.39190 (17)	0.34873 (17)	0.0195 (6)	
H90	0.0779	0.3373	0.3384	0.023*	
C91	0.0358(2)	0.44995 (18)	0.23175 (16)	0.0194 (6)	
C92	0.0661(2)	0.36983 (19)	0.19246 (18)	0.0241 (6)	
H92	0 1139	0 3387	0 2292	0.029*	
C93	0.1192 (3)	0.3925(2)	0.1394(2)	0.0361 (9)	
H93A	0.1837	0.4282	0.1672	0.043*	
H93B	0.1383	0.3404	0.1142	0.043*	
C94	0.0470(3)	0.4397(3)	0.0825(2)	0.0421(10)	
H04	0.0470 (3)	0.4544	0.0485	0.051*	
C95	0.0020	0.4344 0.5201 (2)	0.0485	0.0365 (8)	
С95 Н05л	-0.0272	0.5201 (2)	0.0850	0.044*	
1195A 1105B	0.0272	0.5565	0.0000	0.044*	
C06	-0.0342(2)	0.3303 0.4087(2)	0.17408(18)	0.0250 (6)	
U90	-0.0525	0.4987 (2)	0.17498 (18)	0.0239 (0)	
C07	-0.0323	0.3318 0.3126(2)	0.2003 0.1473(2)	$0.031^{\circ}$	
U07A	-0.0157	0.3130 (2)	0.1473(2) 0.1220	0.0322 (8)	
П9/А Ц07D	-0.0137	0.2011	0.1220	0.039*	
П9/D С09	-0.0093	0.2979 0.2925(2)	0.1800	$0.039^{\circ}$	
	-0.0329 (3)	0.3833 (3)	0.0383(2)	0.0404 (10)	
1100D	-0.1002	0.4156	0.0014	0.056*	
П98D С00	-0.0332	0.3313 0.4425(2)	0.0122 0.1205 (2)	$0.030^{\circ}$	
U99	-0.1343(3)	0.4423 (2)	0.1303 (2)	0.0331 (8)	
П99А 1100D	-0.1700	0.4283	0.1038	0.042*	
H99B	-0.1819	0.4/35	0.0941	$0.042^{+}$	
C100	-0.1066 (3)	0.3012 (2)	0.0908 (2)	0.0380 (9)	
H100	-0.1/14	0.3250	0.0624	$0.040^{*}$	0.5
C101	0.2208 (8)	0.2042 (6)	-0.0633(9)	0.050(2)	0.5
C102	0.2427 (5)	0.1823 (5)	-0.0513 (6)	0.0411 (18)	0.5
H102	0.2244	0.1372	-0.0915	0.049*	0.5
C103	0.2883 (7)	0.16//(6)	0.0150 (6)	0.057(2)	0.5
H103	0.2962	0.1109	0.0229	0.068*	0.5
C104	0.3251 (10)	0.2308 (9)	0.0735 (9)	0.077 (4)	0.5
H104	0.3608	0.2203	0.1218	0.092*	0.5
C105	0.3052 (7)	0.3174 (6)	0.0563 (7)	0.062 (3)	0.5
H105	0.3317	0.3638	0.0950	0.074*	0.5
C106	0.2523 (10)	0.3332 (6)	-0.0101 (9)	0.058 (3)	0.5
H106	0.2376	0.3887	-0.0198	0.070*	0.5
C107	0.1697 (15)	0.2892 (17)	-0.1291 (12)	0.126 (7)	0.5
H10F	0.1629	0.3503	-0.1213	0.189*	0.5
H10G	0.1005	0.2600	-0.1506	0.189*	0.5

H10H	0.2092	0.2754	-0.1624	0.189*	0.5
C108	0.2677 (9)	0.2072 (9)	0.1250 (9)	0.107 (5)	0.5
H10A	0.2311	0.2368	0.1559	0.160*	0.5
H10B	0.3106	0.1656	0.1509	0.160*	0.5
H10C	0.2169	0.1784	0.0790	0.160*	0.5
C109	0.3356 (8)	0.2694 (8)	0.1086 (7)	0.065 (3)	0.5
H10D	0.3155	0.3273	0.1208	0.078*	0.5
H10E	0.4089	0.2656	0.1390	0.078*	0.5
C110	0.3242 (14)	0.2513 (13)	0.0296 (10)	0.115 (6)	0.5
H11A	0.3894	0.2704	0.0234	0.138*	0.5
H11B	0.3132	0.1896	0.0126	0.138*	0.5
C111	0.2397 (13)	0.2919 (13)	-0.0149 (9)	0.092 (5)	0.5
H11C	0.2572	0.3530	-0.0095	0.111*	0.5
H11D	0.1763	0.2840	-0.0022	0.111*	0.5
C112	0.2243 (10)	0.2438 (11)	-0.0980 (8)	0.083 (4)	0.5
H11E	0.2881	0.2525	-0.1100	0.100*	0.5
H11F	0.2098	0.1825	-0.1019	0.100*	0.5
C113	0.1355 (10)	0.2802 (9)	-0.1492 (6)	0.046 (2)	0.5
H11G	0.0781	0.2844	-0.1297	0.069*	0.5
H11H	0.1127	0.2437	-0.1972	0.069*	0.5
H11I	0.1572	0.3365	-0.1544	0.069*	0.5

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	U <sup>22</sup>	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
Zr1	0.01101 (10)	0.00916 (11)	0.01929 (14)	0.00180 (8)	0.00651 (10)	0.00375 (10)
C1	0.0270 (14)	0.0175 (15)	0.037 (2)	0.0013 (11)	0.0042 (13)	0.0142 (14)
C2	0.0225 (13)	0.0138 (14)	0.061 (2)	0.0082 (10)	0.0222 (15)	0.0144 (15)
C3	0.0317 (15)	0.0100 (12)	0.0349 (18)	0.0012 (10)	0.0178 (13)	0.0030 (11)
C4	0.0185 (12)	0.0142 (13)	0.043 (2)	-0.0006 (10)	0.0150 (13)	0.0071 (13)
C5	0.0326 (15)	0.0188 (15)	0.0362 (19)	0.0034 (11)	0.0209 (14)	0.0128 (13)
C6	0.0154 (11)	0.0207 (14)	0.0286 (17)	0.0068 (10)	0.0069 (11)	-0.0012 (12)
C7	0.0126 (11)	0.0178 (14)	0.0348 (18)	0.0027 (9)	0.0092 (11)	0.0077 (12)
C8	0.0135 (11)	0.0214 (15)	0.0298 (17)	0.0037 (10)	0.0021 (11)	0.0016 (13)
C9	0.0187 (12)	0.0278 (16)	0.0337 (18)	0.0105 (11)	0.0080 (12)	0.0145 (14)
C10	0.0153 (11)	0.0129 (13)	0.048 (2)	0.0046 (9)	0.0106 (13)	0.0084 (13)
C11	0.0108 (10)	0.0124 (12)	0.0214 (14)	0.0000 (8)	0.0056 (10)	0.0024 (10)
C12	0.0142 (11)	0.0112 (12)	0.0247 (15)	-0.0008(8)	0.0082 (10)	0.0039 (10)
C13	0.0156 (11)	0.0185 (13)	0.0178 (14)	-0.0023 (9)	0.0046 (10)	0.0033 (11)
C14	0.0150 (11)	0.0169 (13)	0.0223 (15)	-0.0014 (9)	0.0097 (10)	0.0010 (11)
C15	0.0107 (10)	0.0146 (12)	0.0239 (15)	0.0010 (8)	0.0081 (10)	0.0036 (11)
C16	0.0154 (11)	0.0191 (13)	0.0181 (14)	0.0041 (9)	0.0063 (10)	0.0016 (11)
C17	0.0198 (12)	0.0227 (15)	0.0173 (14)	0.0052 (10)	0.0050 (11)	0.0032 (11)
C18	0.0286 (15)	0.0373 (19)	0.0205 (16)	0.0072 (13)	0.0085 (13)	0.0095 (14)
C19	0.0316 (16)	0.048 (2)	0.0198 (17)	0.0105 (15)	0.0118 (13)	0.0015 (15)
C20	0.0266 (15)	0.0396 (19)	0.0239 (17)	0.0113 (13)	0.0100 (13)	-0.0023 (14)
C21	0.0227 (13)	0.0214 (15)	0.0216 (16)	0.0072 (11)	0.0064 (11)	0.0001 (12)
C22	0.0192 (12)	0.0288 (17)	0.0217 (16)	0.0049 (11)	0.0045 (11)	-0.0005 (13)

C23	0.0331 (16)	0.039 (2)	0.0194 (17)	0.0084 (14)	0.0029 (13)	-0.0061 (15)
C24	0.0315 (15)	0.0203 (15)	0.0277 (18)	0.0040 (12)	0.0071 (13)	-0.0034 (13)
C25	0.0254 (14)	0.0284 (18)	0.0258 (18)	0.0015 (12)	0.0045 (13)	-0.0049 (14)
Zr2	0.01016 (10)	0.00995 (11)	0.01683 (13)	0.00053 (8)	0.00541 (9)	0.00342 (10)
C26	0.0283 (15)	0.051 (2)	0.0274 (19)	-0.0275 (15)	0.0169 (14)	-0.0126 (16)
C27	0.0225 (13)	0.0207 (15)	0.048 (2)	0.0009 (11)	0.0193 (14)	0.0150 (14)
C28	0.0214 (13)	0.0385 (19)	0.0226 (16)	-0.0117 (12)	0.0111 (12)	-0.0015 (14)
C29	0.0312 (16)	0.0276 (17)	0.075 (3)	0.0058 (13)	0.040 (2)	0.0155 (18)
C30	0.0115 (12)	0.073 (3)	0.050 (2)	-0.0005 (15)	0.0089 (14)	0.038 (2)
C31	0.069 (3)	0.0175 (15)	0.033 (2)	0.0068 (15)	0.0220 (19)	0.0119 (14)
C32	0.0271 (16)	0.0268 (18)	0.079 (3)	0.0139 (13)	0.0219 (19)	0.029 (2)
C33	0.101 (4)	0.0120 (15)	0.056 (3)	0.0115 (18)	0.059 (3)	0.0083 (16)
C34	0.054 (2)	0.0108 (16)	0.061 (3)	-0.0111 (15)	-0.013 (2)	0.0071 (17)
C35	0.0412 (19)	0.0165 (15)	0.091 (4)	0.0084 (13)	0.048 (2)	0.0222 (19)
C36	0.0141 (10)	0.0109 (12)	0.0195 (14)	0.0013 (8)	0.0066 (10)	0.0006 (10)
C37	0.0109 (10)	0.0165 (13)	0.0222 (15)	0.0016 (9)	0.0062 (10)	0.0014 (11)
C38	0.0138 (11)	0.0226 (14)	0.0176 (14)	0.0033 (10)	0.0019 (10)	-0.0017 (11)
C39	0.0204 (12)	0.0201 (14)	0.0186 (14)	0.0098 (10)	0.0060 (11)	0.0051 (11)
C40	0.0190 (11)	0.0128 (12)	0.0183 (14)	0.0054 (9)	0.0075 (10)	0.0043 (10)
C41	0.0157 (11)	0.0155 (13)	0.0179 (14)	-0.0033(9)	0.0060 (10)	0.0012 (10)
C42	0.0256 (13)	0.0209 (14)	0.0188 (15)	-0.0105(11)	0.0085 (11)	-0.0022(12)
C43	0.0242 (14)	0.042 (2)	0.0197 (16)	-0.0152(13)	0.0050 (12)	-0.0020(14)
C44	0.0265 (15)	0.045 (2)	0.0178 (16)	-0.0069(14)	0.0018 (12)	0.0026 (15)
C45	0.0320 (15)	0.0330(18)	0.0203 (16)	0.0007 (13)	0.0084 (13)	0.0097 (14)
C46	0.0220(12)	0.0194 (14)	0.0178 (14)	-0.0039(10)	0.0078(11)	0.0025 (11)
C47	0.0362 (16)	0.0173 (14)	0.0244 (17)	-0.0071(12)	0.0110 (13)	-0.0031(12)
C48	0.0362(17)	0.039 (2)	0.0190 (17)	-0.0152(14)	0.0099 (14)	-0.0044(15)
C49	0.0242 (13)	0.0226 (15)	0.0220 (16)	-0.0065(11)	0.0120 (12)	-0.0029(12)
C50	0.0316 (15)	0.0217 (16)	0.0257 (17)	-0.0086(12)	0.0141 (13)	-0.0077(13)
Zr3	0.01074 (10)	0.00897 (11)	0.01757 (13)	0.00172 (8)	0.00685 (9)	0.00275 (9)
C51	0.0496 (19)	0.0124 (14)	0.036 (2)	-0.0010(12)	0.0284 (17)	0.0020 (13)
C52	0.0173(12)	0.0122 (13)	0.050(2)	-0.0018(10)	0.0132 (13)	0.0039 (14)
C53	0.0305(14)	0.0122 (13)	0.0247(17)	-0.0042(11)	0.0081 (13)	-0.0013(12)
C54	0.0213 (13)	0.0104 (13)	0.047 (2)	0.0022 (10)	0.0197 (14)	0.0032 (13)
C55	0.0314 (15)	0.0122 (14)	0.0326 (19)	-0.0019(11)	-0.0032(13)	0.0073 (13)
C56	0.0212 (14)	0.042 (2)	0.039 (2)	-0.0178 (13)	0.0184 (14)	-0.0141 (16)
C57	0.0123 (11)	0.0239 (15)	0.042 (2)	0.0035 (10)	0.0122 (12)	0.0133 (14)
C58	0.0259 (14)	0.0272 (16)	0.0342 (19)	-0.0019(12)	0.0219 (14)	0.0007 (14)
C59	0.0302 (16)	0.044 (2)	0.040 (2)	0.0052 (14)	0.0217(15)	0.0230 (17)
C60	0.0292(15)	0.0121 (14)	0.085(3)	0.0031 (11)	0.0368 (19)	0.0135 (17)
C61	0.0165(11)	0.0135(12)	0.0295 (16)	0.0053 (9)	0.0148 (11)	0.0010 (11)
C62	0.0189(12)	0.0144 (13)	0.0314 (17)	0.0070 (10)	0.0122 (12)	0.0072 (12)
C63	0.0219(13)	0.0240(15)	0.0307(18)	0.0106 (11)	0.0085(12)	0.0112(13)
C64	0.0150 (12)	0.0263 (16)	0.0308 (18)	0.0064 (10)	0.0038 (12)	0.0058 (13)
C65	0.0132(11)	0.0202(14)	0.0377 (19)	0.0033 (10)	0.0133(12)	0.0058 (13)
C66	0.0243 (13)	0.0161 (13)	0.0221 (15)	0.0063 (10)	0.0135 (12)	0.0014 (11)
C67	0.0404(17)	0.0208 (15)	0.0267(17)	0.0073 (12)	0.0206 (14)	0.0041 (13)
C68	0.057(2)	0.035(2)	0.0243(18)	0.0160(12)	0.0213(17)	0.0064(15)
	····· (	····· (=)	···- ·· (··)	0.0100 (10)	··· · · · · · · · · · · · · · · · · ·	·····

C69	0.056 (2)	0.045 (2)	0.0195 (18)	0.0146 (18)	0.0081 (17)	0.0051 (16)
C70	0.0372 (18)	0.040 (2)	0.0255 (19)	0.0024 (15)	0.0056 (15)	-0.0041 (16)
C71	0.0312 (15)	0.0217 (15)	0.0236 (16)	-0.0004 (12)	0.0111 (13)	-0.0027 (12)
C72	0.057 (2)	0.0297 (19)	0.040 (2)	0.0103 (16)	0.0371 (19)	0.0060 (16)
C73	0.080 (3)	0.041 (2)	0.028 (2)	0.008 (2)	0.026 (2)	-0.0011 (18)
C74	0.048 (2)	0.0225 (17)	0.0300 (19)	0.0049 (14)	0.0192 (16)	-0.0050 (14)
C75	0.065 (2)	0.032 (2)	0.032 (2)	0.0141 (17)	0.0308 (19)	-0.0003 (16)
Zr4	0.01103 (10)	0.00883 (11)	0.01512 (13)	0.00078 (8)	0.00556 (9)	0.00119 (9)
C76	0.0174 (12)	0.0202 (15)	0.042 (2)	0.0051 (10)	0.0097 (13)	-0.0080 (14)
C77	0.0152 (12)	0.0145 (14)	0.056 (2)	0.0041 (10)	0.0095 (14)	0.0077 (14)
C78	0.0182 (12)	0.0272 (16)	0.0357 (19)	0.0060 (11)	0.0073 (12)	0.0160 (14)
C79	0.0137 (11)	0.0221 (15)	0.0281 (17)	0.0006 (10)	0.0032 (11)	0.0033 (12)
C80	0.0142 (11)	0.0229 (15)	0.0384 (19)	0.0026 (10)	0.0136 (12)	0.0037 (13)
C81	0.0452 (18)	0.0130 (14)	0.0231 (16)	-0.0045 (12)	0.0168 (14)	0.0020 (12)
C82	0.0210 (12)	0.0116 (13)	0.0348 (18)	-0.0014 (10)	0.0135 (12)	0.0022 (12)
C83	0.0232 (13)	0.0134 (13)	0.0212 (15)	-0.0016 (10)	0.0068 (11)	-0.0026 (11)
C84	0.0202 (12)	0.0118 (13)	0.0387 (19)	0.0015 (10)	0.0114 (13)	-0.0003 (12)
C85	0.0286 (14)	0.0130 (14)	0.0289 (18)	-0.0022 (11)	-0.0039 (13)	0.0067 (13)
C86	0.0102 (10)	0.0137 (12)	0.0246 (15)	-0.0031 (8)	0.0051 (10)	0.0029 (11)
C87	0.0123 (10)	0.0184 (13)	0.0260 (16)	0.0025 (9)	0.0090 (10)	0.0072 (11)
C88	0.0195 (12)	0.0271 (16)	0.0270 (16)	0.0031 (11)	0.0149 (12)	0.0054 (13)
C89	0.0195 (12)	0.0282 (16)	0.0251 (16)	0.0027 (11)	0.0106 (11)	0.0146 (13)
C90	0.0167 (11)	0.0134 (12)	0.0319 (17)	0.0002 (9)	0.0108 (11)	0.0080 (11)
C91	0.0189 (12)	0.0178 (14)	0.0201 (15)	-0.0058 (10)	0.0066 (11)	-0.0009 (11)
C92	0.0249 (14)	0.0213 (15)	0.0239 (16)	-0.0087 (11)	0.0102 (12)	-0.0069 (12)
C93	0.0405 (18)	0.040 (2)	0.0284 (19)	-0.0181 (15)	0.0214 (16)	-0.0151 (16)
C94	0.059 (2)	0.046 (2)	0.0190 (18)	-0.0270 (18)	0.0164 (17)	-0.0082 (16)
C95	0.047 (2)	0.037 (2)	0.0199 (17)	-0.0193 (16)	0.0041 (15)	0.0050 (15)
C96	0.0285 (14)	0.0235 (16)	0.0192 (16)	-0.0075 (12)	-0.0004 (12)	0.0035 (12)
C97	0.0335 (16)	0.0238 (17)	0.033 (2)	-0.0135 (13)	0.0094 (15)	-0.0082 (15)
C98	0.060 (2)	0.047 (2)	0.0222 (19)	-0.0241 (19)	0.0063 (18)	-0.0071 (17)
C99	0.0296 (16)	0.036 (2)	0.0288 (19)	-0.0106 (14)	-0.0046 (14)	0.0076 (15)
C100	0.0388 (18)	0.036 (2)	0.0271 (19)	-0.0216 (15)	0.0002 (15)	-0.0054 (16)
C101	0.041 (4)	0.032 (4)	0.093 (7)	0.004 (3)	0.044 (5)	0.013 (5)
C102	0.028 (3)	0.020 (3)	0.074 (5)	0.006 (2)	0.019 (3)	0.000 (3)
C103	0.050 (5)	0.036 (5)	0.071 (6)	0.004 (4)	0.010 (4)	-0.008 (4)
C104	0.066 (7)	0.067 (7)	0.067 (7)	0.026 (5)	-0.006 (6)	-0.015 (5)
C105	0.048 (5)	0.040 (5)	0.095 (7)	-0.002 (4)	0.034 (5)	-0.017 (5)
C106	0.055 (5)	0.020 (4)	0.107 (8)	-0.008 (4)	0.042 (5)	0.001 (4)
C107	0.090 (13)	0.167 (17)	0.145 (12)	-0.007 (11)	0.045 (9)	0.083 (11)
C108	0.072 (8)	0.101 (11)	0.146 (13)	-0.006(7)	0.015 (8)	0.067 (10)
C109	0.038 (5)	0.063 (7)	0.088 (8)	-0.005 (5)	0.009 (5)	0.023 (6)
C110	0.114 (11)	0.130 (15)	0.104 (9)	0.010 (9)	0.028 (8)	0.049 (9)
C111	0.079 (9)	0.152 (16)	0.058 (7)	0.031 (10)	0.035 (6)	0.025 (9)
C112	0.052 (6)	0.133 (13)	0.083 (8)	0.016 (7)	0.045 (6)	0.021 (8)
C113	0.057 (6)	0.048 (5)	0.034 (5)	-0.009 (4)	0.019 (4)	0.003 (4)

Geometric parameters (Å, °)

Zrl—C11	2.334 (2)	C51—C55	1.413 (4)	
Zr1—C15	2.482 (2)	C51—H51	0.9500	
Zr1—C12	2.487 (2)	C52—C53	1.401 (4)	
Zr1—C3	2.578 (3)	С52—Н52	0.9500	
Zr1—C1	2.601 (3)	C53—C54	1.403 (4)	
Zr1—C9	2.604 (3)	С53—Н53	0.9500	
Zr1—C16	2.605 (3)	C54—C55	1.395 (5)	
Zr1—C6	2.613 (3)	C54—H54	0.9500	
Zr1—C5	2.614 (3)	С55—Н55	0.9500	
Zr1-C10	2.615 (3)	C56—C60	1.410 (6)	
Zr1—C8	2.619 (3)	C56—C57	1.418 (5)	
Zr1—C2	2.620 (3)	C56—H56	0.9500	
Zr1C14	2.620(2)	C57—C58	1.380 (5)	
Zr1—C13	2.623 (3)	С57—Н57	0.9500	
Zr1—C4	2.631 (3)	C58—C59	1.373 (5)	
Zr1—C7	2.653 (2)	C58—H58	0.9500	
C1—C2	1.397 (5)	C59—C60	1.389 (5)	
C1—C5	1.415 (4)	С59—Н59	0.9500	
C1—H1	0.9500	С60—Н60	0.9500	
С2—С3	1.409 (5)	C61—C62	1.439 (4)	
С2—Н2	0.9500	C61—C65	1.441 (4)	
C3—C4	1.412 (4)	C61—C66	1.442 (4)	
С3—Н3	0.9500	C62—C63	1.400 (5)	
C4—C5	1.383 (5)	С62—Н62	0.9500	
C4—H4	0.9500	C63—C64	1.417 (4)	
С5—Н5	0.9500	С63—Н63	0.9500	
C6—C10	1.411 (4)	C64—C65	1.402 (5)	
С6—С7	1.412 (4)	C64—H64	0.9500	
С6—Н6	0.9500	С65—Н65	0.9500	
С7—С8	1.399 (4)	C66—C71	1.524 (4)	
С7—Н7	0.9500	C66—C67	1.532 (4)	
С8—С9	1.412 (4)	C67—C68	1.533 (5)	
C8—H8	0.9500	C67—C72	1.551 (4)	
C9—C10	1.400 (5)	С67—Н67	1.0000	
С9—Н9	0.9500	C68—C69	1.520 (5)	
C10—H10	0.9500	C68—H68A	0.9900	
C11—C15	1.437 (4)	C68—H68B	0.9900	
C11—C12	1.437 (4)	C69—C70	1.524 (5)	
C11—C16	1.448 (4)	C69—C73	1.546 (5)	
C12—C13	1.406 (4)	С69—Н69	1.0000	
C12—H12	0.9500	C70—C71	1.537 (5)	
C13—C14	1.408 (4)	С70—Н70А	0.9900	
С13—Н13	0.9500	С70—Н70В	0.9900	
C14—C15	1.406 (4)	C71—C74	1.547 (4)	
C14—H14	0.9500	C71—H71	1.0000	
C15—H15	0.9500	C72—C75	1.538 (5)	

016 017	1 522 (4)		0.0000
	1.525 (4)	C/2—H/2A	0.9900
	1.535 (4)	C/2—H/2B	0.9900
	1.536 (4)	C/3-C/5	1.522 (6)
C17—C22	1.547 (4)	С/3—Н/ЗА	0.9900
С17—Н17	1.0000	С/3—Н/3В	0.9900
C18—C19	1.531 (5)	C74—C75	1.528 (5)
C18—H18A	0.9900	С74—Н74А	0.9900
C18—H18B	0.9900	С74—Н74В	0.9900
C19—C23	1.527 (5)	С75—Н75	1.0000
C19—C20	1.538 (5)	Zr4—C86	2.329 (2)
C19—H19	1.0000	Zr4—C87	2.468 (2)
C20—C21	1.538 (4)	Zr4—C90	2.502 (3)
C20—H20A	0.9900	Zr4—C83	2.571 (3)
C20—H20B	0.9900	Zr4—C91	2.574 (3)
C21—C24	1.547 (4)	Zr4—C78	2.594 (3)
C21—H21	1.0000	Zr4—C76	2.605 (3)
C22—C25	1.534 (4)	Zr4—C88	2.619 (2)
С22—Н22А	0.9900	Zr4—C81	2.622 (3)
С22—Н22В	0.9900	Zr4—C77	2.623 (3)
C23—C25	1.534 (5)	Zr4—C79	2.625 (3)
C23—H23A	0.9900	Zr4—C84	2.628 (3)
C23—H23B	0 9900	Zr4—C82	2.631(3)
$C_{24}$ $C_{25}$	1 523 (5)	Zr4—C80	2.632(2)
C24—H24A	0.9900	Zr4—C85	2.632(2)
$C_{24}$ H24R	0.9900	Zr4	2.633(3)
C25_H25	1,0000	C76-C77	1.402(5)
7r2 C36	2337(2)	C76 $C80$	1.402(3)
$7r^2 - C_{30}$	2.337(2)	C76 H76	0.0500
7-2 C27	2.470(3)	C77 - C78	1.404(5)
$Z_{12} - C_{37}$	2.499(2)	$C_{77} = U_{77}$	1.404(3)
212-034	2.373(3)	C//-n//	0.9300
Zf2—C33	2.600 (3)	C78_U79	1.410 (4)
Zr2—C28	2.602 (3)	C/8—H/8	0.9500
Zr2—C26	2.603 (3)	C79—C80	1.400 (4)
Zr2—C39	2.606 (3)	С/9—Н/9	0.9500
Zr2—C41	2.609 (3)	C80—H80	0.9500
Zr2—C35	2.612 (3)	C81—C82	1.394 (5)
Zr2—C31	2.613 (3)	C81—C85	1.413 (4)
Zr2—C30	2.614 (3)	C81—H81	0.9500
Zr2—C38	2.628 (3)	C82—C83	1.407 (4)
Zr2—C27	2.630 (3)	C82—H82	0.9500
Zr2—C29	2.633 (3)	C83—C84	1.408 (4)
Zr2—C32	2.641 (3)	С83—Н83	0.9500
C26—C27	1.385 (5)	C84—C85	1.393 (5)
C26—C30	1.394 (6)	С84—Н84	0.9500
С26—Н26	0.9500	С85—Н85	0.9500
C27—C28	1.402 (5)	C86—C90	1.434 (4)
C27—H27	0.9500	C86—C87	1.439 (4)
C28—C29	1.392 (5)	C86—C91	1.446 (4)
	× /		× /

620 1120	0.0500	G07 G00	1 400 (4)
C28—H28	0.9500	C87—C88	1.400 (4)
C29—C30	1.371 (6)	С87—Н87	0.9500
С29—Н29	0.9500	C88—C89	1.405 (4)
С30—Н30	0.9500	C88—H88	0.9500
C31—C35	1.377 (6)	C89—C90	1.404 (4)
C31—C32	1.379 (5)	С89—Н89	0.9500
C31—H31	0.9500	С90—Н90	0.9500
C32—C33	1 369 (6)	C91—C96	1 529 (4)
$C_{32} = H_{32}$	0.9500	C91 - C92	1.529(1) 1 531(4)
$C_{32}$ $C_{34}$	1 303 (6)	$C_{02}$ $C_{03}$	1.531(4)
$C_{22} = U_{22}$	1.595 (0)	$C_{92} = C_{93}$	1.534(4)
C33—R35	0.9300	$C_{92} = C_{97}$	1.349 (4)
C34—C35	1.376 (6)	C92—H92	1.0000
С34—Н34	0.9500	C93—C94	1.526 (6)
С35—Н35	0.9500	С93—Н93А	0.9900
C36—C37	1.437 (4)	С93—Н93В	0.9900
C36—C41	1.441 (4)	C94—C95	1.521 (5)
C36—C40	1.442 (4)	C94—C98	1.545 (5)
C37—C38	1.405 (4)	С94—Н94	1.0000
С37—Н37	0.9500	C95—C96	1.527 (4)
C38—C39	1.410 (4)	С95—Н95А	0.9900
C38—H38	0.9500	C95—H95B	0.9900
$C_{39}$ $C_{40}$	1 405 (4)	C96—C99	1 548 (4)
C30_H30	0.9500	C96—H96	1.0000
C40 1140	0.9500	$C_{90} = 1190$	1.0000
C40—F140	0.9300	C97 - C100	1.329 (3)
C41 - C46	1.528 (4)	C97—H97A	0.9900
C41—C42	1.531 (4)	С9/—Н9/В	0.9900
C42—C43	1.530 (5)	C98—C100	1.527 (5)
C42—C47	1.546 (4)	С98—Н98А	0.9900
C42—H42	1.0000	C98—H98B	0.9900
C43—C44	1.532 (5)	C99—C100	1.535 (5)
C43—H43A	0.9900	С99—Н99А	0.9900
C43—H43B	0.9900	С99—Н99В	0.9900
C44—C48	1.528 (5)	C100—H100	1.0000
C44—C45	1.535 (5)	C101—C106	1.357 (18)
C44—H44	1 0000	$C_{101} - C_{107}$	1 37 (2)
$C_{45}$ $C_{46}$	1 533 (4)	C101 - C102	1.390(12)
C45 H45A	0.0000	$C_{102}$ $C_{102}$	1.390(12) 1.208(14)
$C_{45} = H_{45} R$	0.9900	$C_{102} = C_{103}$	0.0500
C45 - H45B	0.9900	C102 - H102	0.9300
C46—C49	1.551 (4)	C103—C104	1.360 (15)
C46—H46	1.0000	С103—Н103	0.9500
C47—C50	1.535 (4)	C104—C105	1.488 (19)
C47—H47A	0.9900	C104—H104	0.9500
C47—H47B	0.9900	C105—C106	1.33 (2)
C48—C50	1.528 (5)	C105—H105	0.9500
C48—H48A	0.9900	C106—H106	0.9500
C48—H48B	0.9900	C107—H10F	0.9800
C49—C50	1.541 (4)	C107—H10G	0.9800
C49—H49A	0.9900	С107—Н10Н	0.9800

C49—H49B	0.9900	C108—C109	1.498 (15)
C50—H50	1.0000	C108—H10A	0.9800
Zr3—C61	2,332 (2)	C108—H10B	0.9800
Zr3—C65	2 471 (2)	C108—H10C	0.9800
Zr3-C62	2 495 (3)	C109-C110	1.49(2)
Zr3	2 567 (3)	C109—H10D	0.9900
Zr3C66	2.507 (3)	C109—H10E	0.9900
7r3 C56	2.577(3)		1.43(2)
Zr3 C50	2.500(3)	C110 H11A	0.0000
7r3 C57	2.577(3)		0.9900
Zr3C57	2.010(2)		1.64(2)
215 - C52 7r3 C58	2.012(3)		1.04(2)
ZIS-C58	2.010(3)		0.9900
$Z_{13} - C_{04}$	2.010(3)		0.9900
213-051	2.025(3)		1.48 (2)
213-031	2.027(3)	CI12—HITE	0.9900
Zr3	2.634 (3)	CII2—HIIF	0.9900
Zr3	2.646 (3)	CII3—HIIG	0.9800
Zr3—C54	2.650 (3)	С113—Н11Н	0.9800
C51—C52	1.371 (5)	C113—H111	0.9800
$C_{11} - 7r_{1} - C_{15}$	34 54 (9)	$C62 - 7r^{3} - C52$	122 63 (9)
$C_{11} = 7r_1 = C_{12}$	34 50 (9)	$C_{52} = 2r_{5}^{-2} = 0.52$	31 38 (9)
$C_{12} = C_{12}$	54 73 (9)	$C_{55} = 213 = C_{52}$	103.48(10)
$C_{11} = C_{12}$	12633(0)	$C_{00} = 213 = C_{52}$	103.40(10) 140.13(11)
$C_{11} = C_{11} = C_{12}$	120.33(9)	$C_{50} = 215 = C_{52}$	149.13(11) 130.06(12)
$C_{13} = Z_{11} = C_{3}$	32.23(9)	$C_{55} = 215 = C_{52}$	130.00(12)
$C_{12}$ $Z_{11}$ $C_{12}$	133.13(9)	$C_{57} = C_{15} = C_{52}$	119.67(9)
C15 Tr1 C1	98.05 (10) 70.87 (0)	$C_{01} = 213 = C_{38}$	140.03(10) 157.99(11)
C13 - Zr1 - C1	79.87(9)	C(2) = Z(3) = C(5)	137.88 (11)
C12— $Zr1$ — $C1$	131.40 (9)	$C_{02}$ $Z_{13}$ $C_{58}$	115.14(10)
$C_3 = Z_{\Gamma} = C_{\Gamma}$	52.17 (11)	$C_{53}$ $Z_{r3}$ $C_{58}$	81.23 (10)
C11-Zr1-C9	110.83 (10)	C66 - Zr3 - C58	135.81 (10)
C15—Zr1—C9	127.83 (9)	C56—Zr3—C58	51.37 (10)
C12—Zr1—C9	77.99 (9)	C59—Zr3—C58	30.55 (10)
C3—Zr1—C9	110.24 (11)	C57—Zr3—C58	30.64 (10)
C1 - Zr1 - C9	150.55 (10)	C52—Zr3—C58	112.24 (10)
C11—Zr1—C16	33.52 (9)	C61—Zr3—C64	55.60 (10)
C15—Zr1—C16	59.31 (8)	C65—Zr3—C64	31.85 (10)
C12—Zr1—C16	60.17 (9)	C62—Zr3—C64	52.98 (10)
C3—Zr1—C16	132.33 (10)	C53—Zr3—C64	87.56 (10)
C1—Zr1—C16	83.66 (10)	C66—Zr3—C64	87.85 (10)
C9—Zr1—C16	117.42 (10)	C56—Zr3—C64	137.06 (12)
C11—Zr1—C6	106.60 (9)	C59—Zr3—C64	103.17 (11)
C15—Zr1—C6	141.11 (9)	C57—Zr3—C64	154.31 (10)
C12—Zr1—C6	94.71 (9)	C52—Zr3—C64	73.56 (10)
C3—Zr1—C6	125.77 (9)	C58—Zr3—C64	126.11 (11)
C1—Zr1—C6	115.03 (10)	C61—Zr3—C60	96.13 (10)
C9—Zr1—C6	51.85 (10)	C65—Zr3—C60	122.75 (10)
C16—Zr1—C6	85.69 (9)	C62—Zr3—C60	68.12 (9)

C11—Zr1—C5	125.43 (10)	C53—Zr3—C60	129.84 (10)
C15—Zr1—C5	111.34 (9)	C66—Zr3—C60	95.70 (11)
C12—Zr1—C5	159.73 (10)	C56—Zr3—C60	31.37 (12)
C3—Zr1—C5	51.83 (10)	C59—Zr3—C60	30.85 (12)
C1—Zr1—C5	31.50 (9)	C57—Zr3—C60	51.40 (10)
C9-Zr1-C5	119.68 (10)	C52 - 7r3 - C60	160.80 (12)
$C_{16}$ $Z_{r1}$ $C_{5}$	100.67 (10)	C58 - Zr3 - C60	50.58 (10)
C6-Zr1-C5	89 99 (10)	C64 - 7r3 - C60	108.34(11)
$C_{11}$ $Z_{r1}$ $C_{10}$	92.94 (9)	C61 - Zr3 - C51	94 79 (10)
$C_{15}$ $Z_{r1}$ $C_{10}$	123 24 (9)	C65 - 7r3 - C51	76.03 (10)
$C_{12}$ $Z_{r1}$ $C_{10}$	69.00 (8)	C62 - 7r3 - C51	127.84(9)
$C_{3}$ $-7r_{1}$ $-C_{10}$	137.93(10)	$C_{53}$ $Z_{r3}$ $C_{51}$	51.35(10)
$C_1 - 2r_1 - C_{10}$	146 14 (10)	$C66 - 7r^{3} - C51$	82 54 (10)
$C_{1} = 211 = C_{10}$	31 11 (10)	$C_{56} = \frac{7r^3}{c_{51}} = \frac{C_{51}}{c_{51}}$	126.20(13)
$C_{2} = 211 = C_{10}$	98 26 (0)	$C_{50} = 215 = C_{51}$	120.29(13)
$C_{10} = 211 = C_{10}$	30.20(9)	$C_{57} = Z_{15} = C_{51}$	140.00(11) 107.42(10)
$C_{0} = Z_{11} = C_{10}$	120.21(10)	$C_{57} = 215 = C_{51}$	107.42(10)
$C_{3}$	120.21(9)	$C_{52}$ $Z_{13}$ $C_{51}$	50.54(11)
C15 - Zr1 - C8	141./5(10) 152.01(10)	$C_{58}$ $Z_{13}$ $C_{51}$	117.02(10)
C12 - Zr1 - C8	155.01 (10)	$C_{04} = Z_{13} = C_{51}$	94.32 (11)
C12— $Zr1$ — $C8$	109.33 (9)	C60 - Zr3 - C51	157.22 (12)
$C_3 - Zr_1 - C_8$	86.62 (10)	C61 - Zr3 - C63	55.18 (10)
C1 - Zr1 - C8	119.21 (10)	C65 - Zr3 - C63	52.87 (10)
C9—Zr1—C8	31.38 (9)	C62—Zr3—C63	31.52 (10)
C16—Zr1—C8	136.36 (9)	C53—Zr3—C63	110.49 (10)
C6—Zr1—C8	51.55 (10)	C66—Zr3—C63	87.45 (10)
C5—Zr1—C8	88.99 (10)	C56—Zr3—C63	105.99 (12)
C10—Zr1—C8	51.39 (9)	C59—Zr3—C63	78.33 (10)
C11—Zr1—C2	98.90 (9)	C57—Zr3—C63	126.84 (10)
C15—Zr1—C2	68.29 (9)	C52—Zr3—C63	104.08 (10)
C12—Zr1—C2	121.92 (9)	C58—Zr3—C63	107.37 (10)
C3—Zr1—C2	31.45 (10)	C64—Zr3—C63	31.31 (9)
C1—Zr1—C2	31.05 (11)	C60—Zr3—C63	77.23 (10)
C9—Zr1—C2	141.18 (11)	C51—Zr3—C63	125.18 (10)
C16—Zr1—C2	101.20 (10)	C61—Zr3—C55	119.01 (11)
C6—Zr1—C2	141.32 (10)	C65—Zr3—C55	106.90 (10)
C5—Zr1—C2	51.35 (9)	C62—Zr3—C55	153.18 (10)
C10—Zr1—C2	168.14 (9)	C53—Zr3—C55	51.44 (11)
C8—Zr1—C2	117.29 (10)	C66—Zr3—C55	94.64 (10)
C11—Zr1—C14	55.37 (9)	C56—Zr3—C55	99.36 (12)
C15—Zr1—C14	31.84 (9)	C59—Zr3—C55	119.17 (11)
C12—Zr1—C14	52.94 (9)	C57—Zr3—C55	76.46 (10)
C3—Zr1—C14	82.72 (9)	C52—Zr3—C55	50.86 (10)
C1—Zr1—C14	97.79 (10)	C58—Zr3—C55	88.63 (11)
C9—Zr1—C14	103.26 (9)	C64—Zr3—C55	123.40 (10)
C16—Zr1—C14	87.24 (8)	C60—Zr3—C55	127.48 (10)
C6—Zr1—C14	145.34 (9)	C51—Zr3—C55	31.09 (10)
C5—Zr1—C14	124.67 (9)	C63—Zr3—C55	154.65 (10)
C10—Zr1—C14	114.65 (9)	C61—Zr3—C54	145.55 (9)

C8—Zr1—C14	121.68 (10)	C65—Zr3—C54	119.91 (9)
C2—Zr1—C14	73.34 (9)	C62—Zr3—C54	171.19 (10)
C11—Zr1—C13	55.30 (9)	C53—Zr3—C54	31.14 (10)
C15—Zr1—C13	52.91 (9)	C66—Zr3—C54	125.18 (10)
C12—Zr1—C13	31.79 (9)	C56—Zr3—C54	99.94 (10)
C3 - Zr1 - C13	105.38 (9)	C59—7r3—C54	95.31 (10)
C1 - Zr1 - C13	128.67 (9)	C57 - Zr3 - C54	69.09 (9)
C9-Zr1-C13	75 52 (9)	C52 - 7r3 - C54	50.89 (8)
$C_{16} - 7r_{1} - C_{13}$	87.61 (9)	$C58 - 7r^{3} - C54$	67.01 (9)
C6-7r1-C13	114 57 (9)	C64 - 7r3 - C54	11849(10)
$C_{5}$ $Z_{r1}$ $C_{13}$	154 74 (9)	C60-7r3-C54	116.25 (9)
C10-7r1-C13	83 54 (9)	$C_{51}$ $Z_{r3}$ $C_{54}$	50 77 (9)
$C_{8}^{-7}r_{1}^{-13}$	101 47 (9)	C63 - 7r3 - C54	140.09(11)
$C_2 - 7r_1 - C_{13}$	101.47(0) 103.79(0)	$C55 - 7r^3 - C54$	30.54(11)
$C_{14}$ $-7r_{1}$ $-C_{13}$	31 15 (9)	$C_{22}$ $C_{21}$ $C_{22}$ $C_{21}$ $C_{22}$ $C_{21}$ $C_{22}$ $C_{23}$ $C$	1084(3)
$C_{11} - Z_{r1} - C_{13}$	148.27(10)	$C_{52} = C_{51} = C_{55}$	74.22(18)
$C_{12} = C_{12} = C_{12}$	140.27(10) 110.31(0)	$C_{52} = C_{51} = Z_{15}$	75.18 (18)
$C_{13} = Z_{11} = C_{4}$	119.31(9) 165.27(10)	$C_{55} = C_{51} = C_{15}$	125.8
$C_{12}$ $Z_{r1}$ $C_{4}$	105.27(10) 21.42(0)	$C_{52} = C_{51} = H_{51}$	125.8
$C_3 = Z_1 = C_4$	51.45(9)	$7r^{2}$ C51 H51	125.8
$C_1 = Z_1 = C_4$	100.62(10)	213 - C31 - 1131	110.8
$C_{2} = C_{1} = C_{4}$	100.02(10) 120.05(10)	$C_{51} = C_{52} = C_{55}$	108.0(3)
$C_{10}$ $Z_{11}$ $C_{4}$	130.93(10)	$C_{31} - C_{32} - Z_{13}$	73.44(17)
$C_0 = Z_1 = C_4$	95.81(9)	$C_{55} - C_{52} - Z_{15}$	12.55 (10)
$C_{3}$	50.58 (10) 117.07 (0)	С51—С52—Н52	125.7
$C_{10}$ Zr1 $C_{4}$	11/.0/(9)	C55—C52—H52	125.7
$C_{8} = 2r_{1} = C_{4}$	69.97 (10)	Zr3—C52—H52	118.2
$C_2$ — $Zr_1$ — $C_4$	51.17 (9)	$C_{52}$ $C_{53}$ $C_{54}$	10/.5(3)
C14— $Zr1$ — $C4$	114.13 (9)	$C_{52} = C_{53} = Z_{13}$	/6.09 (17)
C13 - Zr1 - C4	133.51 (9)	$C_{54} = C_{53} = Z_{r_3}$	//./0(1/)
CII - ZrI - C/	137.70(9)	С52—С53—Н53	126.3
C15 - Zr1 - C7	172.12 (9)	С54—С53—Н53	126.3
C12— $Zr1$ — $C7$	120.17 (9)	Zr3—C53—H53	112.5
C3— $Zr1$ — $C/$	95.22 (9)	C55—C54—C53	108.0 (3)
C1— $Zr1$ — $C7$	102.75 (9)	C55—C54—Zr3	74.56 (17)
C9—Zr1—C7	51.36 (9)	C53—C54—Zr3	71.16 (16)
C16—Zr1—C7	113.32 (9)	С55—С54—Н54	126.0
C6—Zr1—C7	31.10 (9)	С53—С54—Н54	126.0
C5—Zr1—C7	71.72 (9)	Zr3—C54—H54	120.1
C10—Zr1—C7	51.17 (9)	C54—C55—C51	107.3 (3)
C8—Zr1—C7	30.76 (10)	C54—C55—Zr3	74.90 (18)
C2—Zr1—C7	117.66 (9)	C51—C55—Zr3	73.74 (19)
C14—Zr1—C7	152.20 (10)	С54—С55—Н55	126.3
C13—Zr1—C7	126.86 (9)	C51—C55—H55	126.3
C4—Zr1—C7	67.17 (9)	Zr3—C55—H55	117.1
C2—C1—C5	107.4 (3)	C60—C56—C57	106.8 (3)
C2—C1—Zr1	75.22 (18)	C60—C56—Zr3	75.73 (17)
C5—C1—Zr1	74.78 (18)	C57—C56—Zr3	75.00 (16)
C2C1H1	126.3	С60—С56—Н56	126.6

C5—C1—H1	126.3	С57—С56—Н56	126.6
Zr1—C1—H1	115.9	Zr3—C56—H56	115.1
C1—C2—C3	108.5 (3)	C58—C57—C56	107.4 (3)
C1—C2—Zr1	73.73 (17)	C58—C57—Zr3	74.91 (15)
$C_3 - C_2 - Z_{r_1}$	72.64 (16)	$C_{56} - C_{57} - Z_{r_3}$	73 34 (15)
C1 - C2 - H2	125.8	C58—C57—H57	126.3
$C_{1} = C_{2} = H_{2}$	125.8	C56-C57-H57	126.3
7r1 C2 H2	110 7	7r3 C57 H57	117.5
$C_{1}^{2} = C_{2}^{2} = C_{4}^{2}$	119.7	$213 - C_{3} - 1137$	117.5 100 5 (3)
$C_2 = C_3 = C_4$	107.0(3)	$C_{59} = C_{58} = C_{57}$	109.5(3)
$C_2 = C_3 = Z_{11}$	75.91(17)	$C_{59} = C_{50} = Z_{15}$	73.97(10)
C4 - C3 - ZFI	/0.30 (10)	$C_{50} = C_{50} = L_{50}$	/4.45 (15)
$C_2 = C_3 = H_3$	126.5	С59—С58—Н58	125.3
C4—C3—H3	126.5	С57—С58—Н58	125.3
Zr1—C3—H3	113.8	Zr3—C58—H58	118.1
C5—C4—C3	108.6 (3)	C58—C59—C60	108.3 (3)
C5—C4—Zr1	74.04 (17)	C58—C59—Zr3	75.48 (17)
C3—C4—Zr1	72.21 (15)	C60—C59—Zr3	75.68 (18)
C5—C4—H4	125.7	С58—С59—Н59	125.9
C3—C4—H4	125.7	С60—С59—Н59	125.9
Zr1—C4—H4	119.8	Zr3—C59—H59	115.2
C4—C5—C1	108.3 (3)	C59—C60—C56	107.9 (3)
C4—C5—Zr1	75.38 (17)	C59—C60—Zr3	73.47 (17)
C1—C5—Zr1	73.72 (17)	C56—C60—Zr3	72.90 (17)
С4—С5—Н5	125.9	С59—С60—Н60	126.0
С1—С5—Н5	125.9	С56—С60—Н60	126.0
Zr1—C5—H5	117.0	Zr3—C60—H60	119.5
C10—C6—C7	107.4 (3)	C62—C61—C65	104.9(3)
C10 - C6 - 7r1	74 42 (15)	C62 - C61 - C66	1233(2)
C7-C6-7r1	76.01 (15)	C65 - C61 - C66	123.3(2) 122.7(3)
C10-C6-H6	126.3	C62 - C61 - 7r3	78 99 (15)
C7 $C6$ $H6$	126.3	C65 C61 Zr3	77.01 (15)
7 = 20 = 10	115.5	$C_{00} = C_{01} = Z_{10}$	82 40 (15)
$2\Pi - C0 - H0$	113.3 109.1(2)	$C_{00} = C_{01} = Z_{13}$	62.49(13)
$C_{0} = C_{1} = C_{0}$	106.1(3)	C(2) = C(2) = C(1)	109.5(3)
$C_8 = C_7 = Z_{11}$	73.28 (15)	$C_{03} = C_{02} = Z_{13}$	/9./1(1/)
$C_{0}$ $C_{7}$ $L_{1}$	/2.89 (14)	C61 - C62 - Zr3	66.55 (14)
C8—C/—H/	126.0	C63—C62—H62	125.3
C6—C/—H/	126.0	С61—С62—Н62	125.3
Zr1—C7—H7	119.7	Zr3—C62—H62	119.9
C7—C8—C9	108.3 (3)	C62—C63—C64	108.3 (3)
C7—C8—Zr1	75.97 (16)	C62—C63—Zr3	68.77 (16)
C9—C8—Zr1	73.71 (16)	C64—C63—Zr3	73.64 (17)
С7—С8—Н8	125.8	С62—С63—Н63	125.9
С9—С8—Н8	125.8	С64—С63—Н63	125.9
Zr1—C8—H8	116.5	Zr3—C63—H63	123.3
С10—С9—С8	107.6 (3)	C65—C64—C63	107.8 (3)
C10—C9—Zr1	74.90 (17)	C65—C64—Zr3	68.40 (15)
C8—C9—Zr1	74.91 (17)	C63—C64—Zr3	75.05 (16)
С10—С9—Н9	126.2	С65—С64—Н64	126.1

С8—С9—Н9	126.2	С63—С64—Н64	126.1
Zr1—C9—H9	116.2	Zr3—C64—H64	122.1
C9—C10—C6	108.5 (3)	C64—C65—C61	109.4 (3)
C9—C10—Zr1	73.99 (16)	C64—C65—Zr3	79.75 (15)
C6-C10-Zr1	74 27 (16)	C61 - C65 - Zr3	67 32 (13)
$C_{9}$ $C_{10}$ $H_{10}$	125.8	C64 - C65 - H65	125.3
C6 C10 H10	125.8	C61 C65 H65	125.3
<b>Z</b> <sub>r</sub> 1 C10 H10	117.0	7+2 C65 H65	125.5
211 - 010 - 1110	117.9 105.2 (2)	213 - 003 - 1103	119.2
C15 - C11 - C12	103.3(2)	$C_{01} = C_{00} = C_{11}$	116.2(3)
	121.7(2)		117.3 (2)
	124.6 (2)	C/1 - C66 - C6/	109.4 (3)
CI5—CII—ZrI	78.38 (14)	C61—C66—Zr3	63.80 (14)
C12—C11—Zr1	78.57 (14)	C71—C66—Zr3	119.42 (18)
C16—C11—Zr1	83.55 (15)	C67—C66—Zr3	122.33 (19)
C13—C12—C11	109.0 (2)	C66—C67—C68	111.0 (3)
C13—C12—Zr1	79.43 (15)	C66—C67—C72	108.5 (3)
C11—C12—Zr1	66.92 (13)	C68—C67—C72	108.7 (3)
C13—C12—H12	125.5	С66—С67—Н67	109.6
C11—C12—H12	125.5	С68—С67—Н67	109.6
Zr1—C12—H12	119.7	С72—С67—Н67	109.6
C12—C13—C14	108.2 (3)	C69—C68—C67	110.0 (3)
C12—C13—Zr1	68.78 (14)	С69—С68—Н68А	109.7
C14-C13-Zr1	74.31 (15)	C67—C68—H68A	109.7
$C_{12}$ $C_{13}$ $H_{13}$	125.9	C69 - C68 - H68B	109.7
C14 $C13$ $H13$	125.9	C67 C68 H68B	109.7
7r1 C13 H13	122.5	H68A C68 H68B	109.7
211 - C15 - 1113	102.0	1108A - C08 - 1108B	100.2
C15 - C14 - C13	106.1(2)	$C_{08} = C_{09} = C_{70}$	109.2(3)
C12 = C14 = Z11	00.00(15)	C08 - C09 - C73	109.4 (3)
C13 - C14 - Zr1	/4.54 (14)	C/0 - C69 - C/3	109.4 (3)
C15—C14—H14	126.0	С68—С69—Н69	109.6
C13—C14—H14	126.0	С70—С69—Н69	109.6
Zr1—C14—H14	122.5	С73—С69—Н69	109.6
C14—C15—C11	109.1 (2)	C69—C70—C71	110.3 (3)
C14—C15—Zr1	79.47 (14)	С69—С70—Н70А	109.6
C11—C15—Zr1	67.08 (13)	С71—С70—Н70А	109.6
C14—C15—H15	125.5	С69—С70—Н70В	109.6
C11—C15—H15	125.5	С71—С70—Н70В	109.6
Zr1—C15—H15	119.5	H70A—C70—H70B	108.1
C11—C16—C17	116.9 (2)	C66—C71—C70	110.4 (3)
C11—C16—C21	118.7 (3)	C66—C71—C74	108.5 (2)
C17—C16—C21	109.4 (2)	C70—C71—C74	108.6 (3)
C11—C16—Zr1	62.92 (14)	С66—С71—Н71	109.8
C17-C16-Zr1	123.48 (19)	C70—C71—H71	109.8
$C_{21} - C_{16} - Z_{r1}$	118 71 (18)	C74—C71—H71	109.8
$C_{16}$ $C_{17}$ $C_{18}$	111 1 (2)	C75 - C72 - C67	109 3 (3)
$C_{16}$ $C_{17}$ $C_{22}$	1083(2)	C75-C72-H72A	109.5 (5)
C18 C17 C22	100.5(2) 108.6(3)	$C_{13} - C_{12} - C_{12} - C_{12} + C$	109.0
$C_{10} - C_{17} - C_{22}$	100.0 (5)	$C_{0} = C_{12} = \Pi_{12} \Lambda_{12}$	109.0
U10-U1/-H1/	109.0	$U_{13} - U_{12} - H_{12}B$	109.8

C18—C17—H17	109.6	С67—С72—Н72В	109.8
С22—С17—Н17	109.6	H72A—C72—H72B	108.3
C19—C18—C17	109.8 (3)	C75—C73—C69	109.4 (3)
C19—C18—H18A	109.7	С75—С73—Н73А	109.8
C17—C18—H18A	109.7	С69—С73—Н73А	109.8
C19—C18—H18B	109.7	С75—С73—Н73В	109.8
C17—C18—H18B	109.7	С69—С73—Н73В	109.8
H18A—C18—H18B	108.2	H73A—C73—H73B	108.2
$C_{23}$ $C_{19}$ $C_{18}$	110.3 (3)	C75-C74-C71	109.9(3)
$C_{23}$ $C_{19}$ $C_{20}$	109.7(3)	C75—C74—H74A	109.7
$C_{18}$ $C_{19}$ $C_{20}$	108.1(3)	C71 - C74 - H74A	109.7
$C^{23}$ $C^{19}$ $H^{19}$	109.6	C75-C74-H74B	109.7
$C_{18}$ $C_{19}$ $H_{19}$	109.6	C71 - C74 - H74B	109.7
$C_{10} - C_{10} - H_{10}$	109.6	H74A - C74 - H74B	109.7
$C_{20} C_{10} C_{10}$	109.0	C73 $C75$ $C74$	100.2
$C_{21} = C_{20} = C_{12}$	100.6	$C_{13}^{} C_{13}^{} C_{14}^{}$	110.1(3) 109.5(3)
$C_{21} = C_{20} = H_{20A}$	109.0	C74 $C75$ $C72$	109.5(3) 108.9(3)
$C_{19}$ $C_{20}$ $H_{20R}$	109.0	C/4 - C/3 - C/2	100.9 (3)
$C_{21} = C_{20} = H_{20B}$	109.0	$C_{73} - C_{73} - H_{73}$	109.5
$H_{20}$ $H$	109.0	C/4 - C/3 - H/3	109.5
$H_{20}A = C_{20} = H_{20}B$	108.2	C/2 - C/3 - H/3	109.5
C16 - C21 - C20	110.5 (3)	$C_{80} = Z_{14} = C_{87}$	34.75 (9)
C16 - C21 - C24	108.8 (2)	C85 - Zr4 - C90	34.31 (10)
$C_{20} = C_{21} = C_{24}$	108.1 (3)	$C_8/-Z_r4-C_{90}$	54.72 (9)
С16—С21—Н21	109.8	C86—Zr4—C83	132.39 (9)
С20—С21—Н21	109.8	C87—Zr4—C83	98.55 (9)
C24—C21—H21	109.8	C90—Zr4—C83	142.17 (9)
C25—C22—C17	110.0 (2)	C86—Zr4—C91	33.84 (9)
C25—C22—H22A	109.7	C87—Zr4—C91	60.07 (9)
C17—C22—H22A	109.7	C90—Zr4—C91	59.99 (10)
C25—C22—H22B	109.7	C83—Zr4—C91	134.28 (10)
C17—C22—H22B	109.7	C86—Zr4—C78	118.07 (10)
H22A—C22—H22B	108.2	C87—Zr4—C78	130.64 (9)
C19—C23—C25	109.5 (3)	C90—Zr4—C78	84.54 (10)
С19—С23—Н23А	109.8	C83—Zr4—C78	99.37 (10)
С25—С23—Н23А	109.8	C91—Zr4—C78	125.61 (10)
С19—С23—Н23В	109.8	C86—Zr4—C76	102.33 (9)
С25—С23—Н23В	109.8	C87—Zr4—C76	136.89 (10)
H23A—C23—H23B	108.2	C90—Zr4—C76	87.52 (9)
C25—C24—C21	109.9 (3)	C83—Zr4—C76	124.43 (9)
C25—C24—H24A	109.7	C91—Zr4—C76	84.50 (10)
C21—C24—H24A	109.7	C78—Zr4—C76	51.81 (11)
C25—C24—H24B	109.7	C86—Zr4—C88	55.31 (10)
C21—C24—H24B	109.7	C87—Zr4—C88	31.78 (9)
H24A—C24—H24B	108.2	C90—Zr4—C88	52.75 (9)
C24—C25—C23	109.6 (3)	C83—Zr4—C88	90.09 (9)
C24—C25—C22	109.6 (3)	C91—Zr4—C88	87.66 (9)
C23—C25—C22	108.9 (3)	C78—Zr4—C88	102.87 (10)
C24—C25—H25	109.6	C76—Zr4—C88	137.11 (10)

C23—C25—H25	109.6	C86—Zr4—C81	116.39 (10)
С22—С25—Н25	109.6	C87—Zr4—C81	104.40 (10)
C36—Zr2—C40	34.76 (9)	C90—Zr4—C81	150.47 (10)
C36—Zr2—C37	34.37 (9)	C83—Zr4—C81	51.73 (10)
C40—Zr2—C37	54.85 (9)	C91—Zr4—C81	92.22 (10)
C36—Zr2—C34	112.54 (13)	C78—Zr4—C81	122.70 (10)
C40—Zr2—C34	127.93 (12)	C76—Zr4—C81	100.41 (10)
C37—Zr2—C34	79.37 (12)	C88—Zr4—C81	122.02 (10)
C36—Zr2—C33	143.00 (11)	C86—Zr4—C77	95.22 (9)
C40—Zr2—C33	153.28 (14)	C87—Zr4—C77	122.33 (9)
C37—Zr2—C33	110.60 (12)	C90—Zr4—C77	67.66 (9)
C34—Zr2—C33	31.23 (13)	C83—Zr4—C77	128.99 (10)
C36—Zr2—C28	124.58 (10)	C91—Zr4—C77	94.62 (10)
C40—Zr2—C28	90.57 (10)	C78—Zr4—C77	31.22 (11)
C37—Zr2—C28	135.72 (10)	C76—Zr4—C77	31.12 (11)
C34—Zr2—C28	110.53 (14)	C88—Zr4—C77	108.44 (10)
C33—Zr2—C28	87.93 (11)	C81—Zr4—C77	129.29 (10)
$C_{36}$ — $Z_{r2}$ — $C_{26}$	98.65 (10)	C86—Zr4—C79	146.40 (10)
C40— $Zr2$ — $C26$	81.99 (12)	C87— $Zr4$ — $C79$	158.15 (10)
C37—Zr2—C26	132.45 (11)	C90—Zr4—C79	115.10 (9)
C34— $Zr2$ — $C26$	148.09 (14)	C83—Zr4—C79	79.20 (9)
C33—Zr2—C26	116.88 (14)	C91—Zr4—C79	135.54 (9)
C28—Zr2—C26	51.39 (10)	C78—Zr4—C79	31.35 (9)
C36—Zr2—C39	55.56 (9)	C76—Zr4—C79	51.33 (10)
C40—Zr2—C39	31.98 (9)	C88—Zr4—C79	126.45 (10)
C37—Zr2—C39	53.04 (9)	C81—Zr4—C79	91.35 (10)
C34—Zr2—C39	102.03 (12)	C77—Zr4—C79	51.26 (9)
C33—Zr2—C39	121.60 (13)	C86—Zr4—C84	101.91 (9)
C28—Zr2—C39	82.82 (10)	C87—Zr4—C84	70.22 (9)
C26—Zr2—C39	101.06 (12)	C90—Zr4—C84	122.99 (9)
C36—Zr2—C41	33.30 (9)	C83—Zr4—C84	31.40 (9)
C40—Zr2—C41	59.52 (9)	C91—Zr4—C84	105.97 (10)
C37—Zr2—C41	59.62 (8)	C78—Zr4—C84	128.28 (11)
C34—Zr2—C41	119.76 (13)	C76—Zr4—C84	149.17 (9)
C33—Zr2—C41	137.08 (10)	C88—Zr4—C84	73.21 (9)
C28—Zr2—C41	129.71 (9)	C81—Zr4—C84	51.25 (10)
C26—Zr2—C41	82.96 (9)	C77—Zr4—C84	159.41 (11)
C39—Zr2—C41	87.35 (9)	C79—Zr4—C84	110.55 (9)
C36—Zr2—C35	94.17 (10)	C86—Zr4—C82	144.70 (10)
C40—Zr2—C35	123.59 (9)	C87—Zr4—C82	120.51 (9)
C37—Zr2—C35	68.87 (10)	C90—Zr4—C82	173.47 (9)
C34—Zr2—C35	30.77 (14)	C83—Zr4—C82	31.36 (9)
C33—Zr2—C35	50.69 (11)	C91—Zr4—C82	122.81 (10)
C28—Zr2—C35	138.38 (11)	C78—Zr4—C82	97.21 (10)
C26—Zr2—C35	145.22 (14)	C76—Zr4—C82	98.52 (9)
C39—Zr2—C35	112.79 (11)	C88—Zr4—C82	120.75 (9)
C41—Zr2—C35	90.63 (11)	C81—Zr4—C82	30.78 (10)
$C_{36} - Zr_{2} - C_{31}$	106.40 (11)	C77—Zr4—C82	116.71 (9)

C40—Zr2—C31	141.15 (10)	C79—Zr4—C82	67.60 (9)
C37—Zr2—C31	92.85 (11)	C84—Zr4—C82	51.24 (8)
C34—Zr2—C31	51.07 (13)	C86—Zr4—C80	132.47 (9)
C33—Zr2—C31	50.71 (12)	C87—Zr4—C80	166.93 (10)
C28—Zr2—C31	127.68 (11)	C90—Zr4—C80	117.13 (9)
C26—Zr2—C31	114.70 (13)	C83—Zr4—C80	93.28 (9)
C39—Zr2—C31	142.67 (11)	C91—Zr4—C80	107.43 (9)
C41—Zr2—C31	86.75 (10)	C78—Zr4—C80	51.76 (10)
C35—Zr2—C31	30.57 (13)	C76—Zr4—C80	31.21 (9)
C36—Zr2—C30	126.34 (12)	C88—Zr4—C80	154.62 (10)
C40—Zr2—C30	112.79 (11)	C81—Zr4—C80	78.66 (10)
C37—Zr2—C30	160.27 (12)	C77—Zr4—C80	51.40 (9)
$C_{34}$ 7. r <sup>2</sup> C <sub>30</sub>	117.50 (14)	C79—Zr4—C80	30.90 (10)
$C_{33} = 7r_{2} = C_{30}$	86 64 (15)	C84 - 7r4 - C80	119 65 (9)
$C_{28} = 7r^2 = C_{30}$	51.07 (11)	C82 - 7r4 - C80	68 43 (9)
$C_{26} = 2r_{2} = C_{30}$	30.99(12)	$C_{86} - 7r_{4} - C_{85}$	93 83 (10)
$C_{20} = 2i2 = C_{30}$	126.36(11)	C87 - 7r4 - C85	73 93 (9)
$C_{3}^{-2} = C_{3}^{-2} = C_{$	120.30(11) 101.33(12)	$C_{0}^{0}$ $Z_{r4}^{r4}$ $C_{85}^{85}$	13.93(9)
$C_{41} = 212 = C_{50}$	101.55(12) 110.82(12)	$C_{90} = 214 = C_{83}$	120.30(9)
$C_{33} = Z_{12} = C_{30}$	119.02(12)	$C_{01} = \frac{7}{2} + \frac{1}{2} + \frac{1}{$	31.03(10)
$C_{31} = Z_{12} = C_{30}$	90.95 (12) 55.18 (0)	$C_{21}^{-21} = C_{23}^{-1} =$	82.80 (10)
$C_{30} = Z_{12} = C_{38}$	55.18 (9)	C/8 - Zr4 - C85	147.88 (10)
C40 - Zr2 - C38	53.00 (9)	C/6-Zr4-C85	128.56 (11)
$C_3/-Z_{r2}-C_{38}$	31.69 (9)	C88—Zr4—C85	91.87 (10)
C34—Zr2—C38	75.14 (11)	C81—Zr4—C85	31.19 (10)
C33—Zr2—C38	102.14 (13)	C77—Zr4—C85	159.46 (11)
C28—Zr2—C38	106.89 (10)	C79—Zr4—C85	118.55 (9)
C26—Zr2—C38	131.84 (12)	C84—Zr4—C85	30.72 (10)
C39—Zr2—C38	31.24 (9)	C82—Zr4—C85	51.11 (9)
C41—Zr2—C38	87.14 (8)	C80—Zr4—C85	109.85 (10)
C35—Zr2—C38	81.55 (11)	C86—Zr4—C89	54.90 (10)
C31—Zr2—C38	111.60 (11)	C87—Zr4—C89	52.66 (9)
C30—Zr2—C38	156.48 (10)	C90—Zr4—C89	31.52 (10)
C36—Zr2—C27	97.99 (9)	C83—Zr4—C89	112.14 (9)
C40—Zr2—C27	68.36 (9)	C91—Zr4—C89	87.38 (9)
C37—Zr2—C27	122.77 (9)	C78—Zr4—C89	77.98 (9)
C34—Zr2—C27	141.41 (14)	C76—Zr4—C89	106.43 (10)
C33—Zr2—C27	117.66 (11)	C88—Zr4—C89	30.96 (9)
C28—Zr2—C27	31.10 (10)	C81—Zr4—C89	152.98 (9)
$C_{26}$ $Z_{r2}$ $C_{27}$	30.68 (11)	C77— $Zr4$ — $C89$	77.60 (9)
$C_{39} - 7r_{2} - C_{27}$	75 71 (10)	C79 - 7r4 - C89	107 72 (9)
$C_{41} - 7r^2 - C_{27}^2$	98 76 (9)	C84 - 7r4 - C89	107.01(9)
$C_{35} - 7r^2 - C_{27}^2$	167 76 (10)	C82 - 7r4 - C89	103.01(9) 142.69(10)
$C_{33} = 212 = C_{27}$	107.70(10) 141.62(12)	$C_{02} = 214 + C_{03}$	142.00(10)
$C_{31} = Z_{12} = C_{27}$	50.70(11)	$C85_7r4_C89$	127.12(10) 127.12(10)
$C_{30} - Z_{12} - C_{27}$	106.61 (10)	$C_{0}^{-}$	122.77(10)
$C_{30} = 212 = C_{27}$	100.01(10) 147.40(10)	C77 C76 7 - 4	100.3(3)
$C_{30}$ $Z_{12}$ $C_{29}$ $C_{40}$ $Z_{r2}$ $C_{20}$	147.40(10) 119.25(10)	$C_{1} = C_{1} = C_{1$	75.14(10)
$C_{40} - Z_{I2} - C_{29}$	118.23(10)	$C_{00} - C_{10} - C_{14}$	13.47 (13)
U3/—Zr2—U29	165.16 (12)	C / / - C / 6 - H / 6	125.8

C34—Zr2—C29	99.56 (14)	С80—С76—Н76	125.8
C33—Zr2—C29	69.59 (12)	Zr4—C76—H76	115.7
C28—Zr2—C29	30.84 (11)	C76—C77—C78	108.1 (3)
C26—Zr2—C29	50.63 (11)	C76—C77—Zr4	73.74 (17)
C39—Zr2—C29	113.48 (11)	C78—C77—Zr4	73.26 (17)
C41—Zr2—C29	130.91 (11)	С76—С77—Н77	126.0
C35—Zr2—C29	117.27 (10)	С78—С77—Н77	126.0
$C_{31} - 7r_{2} - C_{29}$	97.94 (12)	Zr4—C77—H77	118.9
$C_{30}$ $Z_{r2}$ $C_{29}$	30.30(12)	C77—C78—C79	107.5 (3)
$C_{38} = 7r^2 = C_{29}^2$	133 58 (12)	C77-C78-Zr4	75 53 (18)
$C_{27} - 7r_{2} - C_{29}$	50 49 (10)	C79-C78-Zr4	75 56 (17)
$C_{36} - 7r_{2} - C_{32}$	136 79 (11)	C77—C78—H78	126.2
$C40 - 7r^2 - C32$	171 54 (11)	C79 - C78 - H78	126.2
$C_{37}$ $-7r_{2}$ $C_{32}$	118 85 (10)	Zr4—C78—H78	115.0
$C_{34}$ $-7r_{2}$ $-C_{32}$	50.65 (13)	$C_{80}$ $C_{79}$ $C_{78}$	108.5(3)
$C_{33} = 7r^2 = C_{32}^3$	30.26 (14)	C80-C79-7r4	74.83 (16)
$C_{28} = 7r^2 = C_{32}^2$	97.63 (11)	C78 - C79 - 7r4	73.09(16)
$C_{26} = Z_{12} = C_{32}$	101 53 (13)	$C_{10} = C_{10} = C$	125 7
$C_{20} = 212 = C_{32}$	101.33(13) 151.10(12)	$C_{30} = C_{79} = H_{79}$	125.7
$C_{3} = 212 = C_{3}^{2}$	131.19(12) 112.00(12)	Zr4 C70 H70	123.7
$C_{+1} = 212 = C_{32}$	50.05(10)	C79 $C80$ $C76$	110.2 107 5 (3)
$C_{33} = 212 = C_{32}$	30.03(10)	C79 - C80 - C70	74.28(15)
$C_{31} = 212 = C_{32}$	50.45(11)	C76 C80 Zr4	74.28(13)
$C_{30} = 212 = C_{32}$	(12)	C70 C80 H80	126.2
$C_{30} = Z_{12} = C_{32}$	123.33(11) 118.26(10)	C76 $C80$ $H80$	120.5
$C_2 / - Z_1 Z_{} C_{32}$	(10, 50, (10))	$C/0 - C_{80} - H_{80}$	120.5
$C_{29} = C_{12} = C_{32}$	09.27(11)	214 - C80 - H80	110.1
$C_{27} = C_{20} = C_{30}$	107.8(3)	$C_{82} = C_{81} = C_{83}$	108.0(3)
$C_2/-C_{20}-Z_{12}$	75.75(17)	C82 - C81 - Zr4	74.95 (17)
$C_{30}$ $C_{26}$ $Z_{r_2}$	/4.96 (18)	C82 - C81 - Zr4	/4.82 (18)
$C_2/-C_{20}-H_{20}$	120.1	C82 - C81 - H81	126.0
C30—C26—H26	126.1	C85—C81—H81	126.0
Zr2—C26—H26	115.4	Zr4—C81—H81	116.3
C26—C27—C28	108.1 (3)	C81 - C82 - C83	108.0 (3)
$C_{26} - C_{27} - Z_{r_{2}}$	73.59 (17)	C81—C82—Zr4	74.27 (16)
$C_{28} = C_{27} = Z_{r_{2}}$	73.35 (16)	C83—C82—Zr4	71.97 (15)
С26—С27—Н27	125.9	C81—C82—H82	126.0
С28—С27—Н27	125.9	С83—С82—Н82	126.0
Zr2—C27—H27	119.0	Zr4—C82—H82	119.6
C29—C28—C27	106.9 (3)	C82—C83—C84	107.8 (3)
C29—C28—Zr2	75.84 (17)	C82—C83—Zr4	76.66 (16)
C27—C28—Zr2	75.55 (16)	C84—C83—Zr4	76.52 (16)
C29—C28—H28	126.6	С82—С83—Н83	126.1
C27—C28—H28	126.6	С84—С83—Н83	126.1
Zr2—C28—H28	114.5	Zr4—C83—H83	113.2
C30—C29—C28	108.9 (3)	C85—C84—C83	108.0 (3)
C30—C29—Zr2	74.08 (17)	C85—C84—Zr4	74.84 (17)
C28—C29—Zr2	73.31 (16)	C83—C84—Zr4	72.08 (16)
С30—С29—Н29	125.6	C85—C84—H84	126.0

С28—С29—Н29	125.6	С83—С84—Н84	126.0
Zr2—C29—H29	118.9	Zr4—C84—H84	119.0
C29—C30—C26	108.1 (3)	C84—C85—C81	108.0 (3)
C29—C30—Zr2	75.62 (18)	C84—C85—Zr4	74.44 (18)
C26—C30—Zr2	74.04 (17)	C81—C85—Zr4	73.99 (18)
С29—С30—Н30	125.9	С84—С85—Н85	126.0
С26—С30—Н30	125.9	С81—С85—Н85	126.0
Zr2—C30—H30	116.5	Zr4—C85—H85	117.6
C35—C31—C32	107.4 (4)	C90—C86—C87	105.3 (3)
$C_{35} - C_{31} - Z_{r_{2}}^{2}$	74.7 (2)	C90—C86—C91	123.6 (2)
$C_{32} - C_{31} - Z_{r_{2}}^{2}$	759(2)	C87—C86—C91	122.2(3)
C35—C31—H31	126.3	C90-C86-Zr4	79.46 (15)
$C_{32}$ $C_{31}$ $H_{31}$	126.3	C87 - C86 - Zr4	77.95 (15)
Zr2—C31—H31	115.4	C91 - C86 - Zr4	82 42 (15)
$C_{33}$ $C_{32}$ $C_{31}$	108 7 (3)	$C_{88}$ $C_{87}$ $C_{86}$	1090(3)
$C_{33} = C_{32} = Zr^2$	732(2)	$C_{88} = C_{87} = 7r_4$	80.04 (15)
$C_{31} = C_{32} = 7r^2$	73 68 (19)	$C_{86} C_{87} Z_{r4}$	67 31 (13)
$C_{33}$ $C_{32}$ $H_{32}$	125.7	$C_{88}$ $C_{87}$ $H_{87}$	125 5
$C_{31} = C_{32} = H_{32}$	125.7	C86-C87-H87	125.5
7r2H32	110.2	Zr4_C87_H87	123.5
$C_{32}$ $C_{32}$ $C_{33}$ $C_{34}$	107.8 (3)	214 - C67 - 1167 C87 - C88 - C89	108.7
$C_{32} = C_{33} = C_{34}$	76 5 (2)	C87 - C88 - Zr4	68 18 (14)
$C_{32} = C_{33} = Z_{12}$	70.3(2)	C89 - C88 - 7r4	75.48(15)
$C_{32}$ $C_{33}$ $H_{33}$	126.1	C87 C88 H88	125.0
$C_{32} = C_{33} = H_{33}$	126.1	$C_{80} = C_{80} = H_{80}$	125.9
7r2 C33 H33	120.1	7r4 C88 H88	123.9
212 - C35 - 1135	110.2	214 - 0.00 - 0.00 - 0.000 -	122.1
$C_{35} = C_{34} = C_{35}$	107.4(4)	$C_{90} = C_{89} = C_{88}$	108.5(3)
$C_{33} = C_{34} = Z_{12}$	70.2(2)	$C_{90} = C_{89} = Z_{14}$	72.56(15)
$C_{33} = C_{34} = Z_{12}$	126.2	$C_{00} = C_{00} = L_{14}$	125.8
$C_{33} = C_{34} = H_{34}$	120.3	$C_{90} = C_{89} = 1189$	125.8
C35-C34-H34	120.5		123.6
212 - C34 - H34	114.3	214 - 0.09 - 0.09	123.3
$C_{34} = C_{35} = C_{31}$	108.0(3)	$C_{89} = C_{90} = C_{80}$	108.9(2)
$C_{34} = C_{35} = Z_{12}$	73.1(2)	$C_{89} = C_{90} = Z_{r4}$	79.80 (10) 66.22 (14)
$C_{31} = C_{35} = Z_{12}$	/4./0(19) 125.7	$C_{80} = C_{90} = Z_{14}$	00.23 (14)
C34—C35—H35	125.7	$C_{89} = C_{90} = H_{90}$	125.6
C31—C35—H35	125.7	C86—C90—H90	125.6
Zf2-C35-H35	118.3	Zr4—C90—H90	119.9
$C_{37} = C_{36} = C_{41}$	124.0 (3)	C86-C91-C96	116.4 (2)
$C_{3}/-C_{3}6-C_{40}$	105.3 (2)	C86-C91-C92	118.5 (3)
C41 - C36 - C40	122.2 (2)	C96—C91—C92	109.5 (3)
$C_{37} - C_{36} - Zr_{2}$	78.98 (14)	C86—C91—Zr4	63.74 (15)
C41 - C36 - Zr2	83.75 (15)	C96—C91—Zr4	123.97 (19)
C40—C36—Zr2	77.67 (14)	C92—C91—Zr4	118.07 (19)
$C_{38} - C_{37} - C_{36}$	109.0 (2)	C91—C92—C93	110.1 (3)
C38—C37—Zr2	79.23 (14)	C91—C92—C97	108.7 (2)
C36—C37—Zr2	66.65 (13)	C93—C92—C97	108.3 (3)
С38—С37—Н37	125.5	С91—С92—Н92	109.9

С36—С37—Н37	125.5	С93—С92—Н92	109.9
Zr2—C37—H37	120.1	С97—С92—Н92	109.9
C37—C38—C39	108.3 (3)	C94—C93—C92	110.6 (3)
C37—C38—Zr2	69.08 (14)	С94—С93—Н93А	109.5
C39—C38—Zr2	73.52 (15)	С92—С93—Н93А	109.5
C37—C38—H38	125.9	С94—С93—Н93В	109.5
C39—C38—H38	125.9	С92—С93—Н93В	109.5
Zr2—C38—H38	123.2	H93A—C93—H93B	108.1
C40-C39-C38	108.2 (3)	C95-C94-C93	108.7(3)
$C40-C39-7r^2$	68 67 (15)	C95 - C94 - C98	100.7(3)
$C_{38} = C_{39} = 7r^{2}$	75 23 (16)	C93 - C94 - C98	109.7(3) 109.4(3)
C40-C39-H39	125.9	C95—C94—H94	109.6
$C_{38}$ $C_{39}$ $H_{39}$	125.9	C93 - C94 - H94	109.6
7r2-C39-H39	125.9	C98—C94—H94	109.6
$C_{39}$ $C_{40}$ $C_{36}$	108.9(2)	C94 $C95$ $C96$	109.0 110.2(3)
$C_{39} - C_{40} - C_{30}$	79 35 (16)	$C94 - C95 - H95 \Delta$	109.6
$C_{35} = C_{40} = Z_{12}$	67.57(14)	$C_{06}$ $C_{05}$ $H_{05A}$	109.6
$C_{30} = C_{40} = Z_{12}$	125.5	$C_{90} - C_{93} - 11_{93$	109.0
$C_{39} = C_{40} = H_{40}$	125.5	$C_{94} - C_{93} - H_{93} - H$	109.0
$C_{30} - C_{40} - H_{40}$	125.5	$C_{90} - C_{93} - H_{93} - H$	109.0
212 - C40 - H40	119.2	H93A - C93 - H93B	108.1
$C_{30} - C_{41} - C_{40}$	116.4(2)	C95 - C96 - C91	111.0(3)
$C_{30} - C_{41} - C_{42}$	110.8(2) 100.7(2)	C95 - C96 - C99	108.7(3)
$C_{40} = C_{41} = C_{42}$	109.7(2)	C91 - C96 - C99	108.3 (3)
$C_{36}$ $C_{41}$ $Z_{r2}$	62.95 (14)	C95—C96—H96	109.6
C46 - C41 - Zr2	120.21 (18)	C91—C96—H96	109.6
C42 - C41 - Zr2	121.86 (16)	C99—C96—H96	109.6
C43 - C42 - C41	111.0 (3)	C100-C97-C92	109.8 (3)
C43—C42—C47	108.4 (3)	C100—C9/—H9/A	109.7
C41 - C42 - C47	108.7 (2)	С92—С97—Н97А	109.7
C43—C42—H42	109.6	С100—С97—Н97В	109.7
C41—C42—H42	109.6	С92—С97—Н97В	109.7
С47—С42—Н42	109.6	Н97А—С97—Н97В	108.2
C42—C43—C44	109.7 (2)	C100—C98—C94	109.2 (3)
С42—С43—Н43А	109.7	C100—C98—H98A	109.8
C44—C43—H43A	109.7	С94—С98—Н98А	109.8
C42—C43—H43B	109.7	С100—С98—Н98В	109.8
C44—C43—H43B	109.7	С94—С98—Н98В	109.8
H43A—C43—H43B	108.2	H98A—C98—H98B	108.3
C48—C44—C43	110.2 (3)	C100—C99—C96	109.6 (3)
C48—C44—C45	109.7 (3)	С100—С99—Н99А	109.7
C43—C44—C45	108.7 (3)	С96—С99—Н99А	109.7
C48—C44—H44	109.4	С100—С99—Н99В	109.7
C43—C44—H44	109.4	С96—С99—Н99В	109.7
C45—C44—H44	109.4	H99A—C99—H99B	108.2
C46—C45—C44	109.9 (3)	C98—C100—C97	109.8 (3)
C46—C45—H45A	109.7	C98—C100—C99	109.4 (3)
C44—C45—H45A	109.7	C97—C100—C99	109.4 (3)
C46—C45—H45B	109.7	C98—C100—H100	109.4

C44—C45—H45B	109.7	С97—С100—Н100	109.4
H45A—C45—H45B	108.2	C99—C100—H100	109.4
C41—C46—C45	110.7 (2)	C106—C101—C107	109.2 (14)
C41—C46—C49	108.4 (2)	C106—C101—C102	123.9 (14)
C45—C46—C49	108.4 (3)	C107—C101—C102	126.8 (17)
C41—C46—H46	109.8	C103—C102—C101	119.8 (10)
C45—C46—H46	109.8	C103—C102—H102	120.1
C49—C46—H46	109.8	C101—C102—H102	120.1
C50—C47—C42	109.7 (3)	C102—C103—C104	122.4 (11)
С50—С47—Н47А	109.7	C102—C103—H103	118.8
С42—С47—Н47А	109.7	C104—C103—H103	118.8
С50—С47—Н47В	109.7	C103—C104—C105	115.0 (14)
C42—C47—H47B	109.7	C103—C104—H104	122.5
H47A—C47—H47B	108.2	C105—C104—H104	122.5
C50—C48—C44	109.4 (3)	C106—C105—C104	123.4 (11)
C50—C48—H48A	109.8	C106—C105—H105	118.3
C44—C48—H48A	109.8	C104—C105—H105	118.3
C50—C48—H48B	109.8	C105-C106-C101	115.1 (11)
C44—C48—H48B	109.8	C105—C106—H106	122.4
H48A—C48—H48B	108.2	C101—C106—H106	122.4
C50-C49-C46	109.6 (2)	C101—C107—H10F	109.5
C50-C49-H49A	109.7	C101 - C107 - H10G	109.5
C46—C49—H49A	109.7	H10F—C107—H10G	109.5
C50—C49—H49B	109.7	C101—C107—H10H	109.5
C46—C49—H49B	109.7	H10F—C107—H10H	109.5
H49A—C49—H49B	108.2	H10G—C107—H10H	109.5
C48—C50—C47	109.5 (3)	C109—C108—H10A	109.5
C48—C50—C49	109.2 (3)	C109—C108—H10B	109.5
C47—C50—C49	109.4 (3)	H10A—C108—H10B	109.5
C48—C50—H50	109.6	C109—C108—H10C	109.5
С47—С50—Н50	109.6	H10A—C108—H10C	109.5
C49—C50—H50	109.6	H10B—C108—H10C	109.5
C61— $Zr3$ — $C65$	34.77 (10)	C110—C109—C108	109.6 (13)
C61— $Zr3$ — $C62$	34.46 (10)	C110—C109—H10D	109.7
C65 - Zr3 - C62	54.74 (9)	C108—C109—H10D	109.7
C61 - Zr3 - C53	129.88 (9)	C110—C109—H10E	109.7
C65 - Zr3 - C53	96.00 (9)	C108—C109—H10E	109.7
C62 - Zr3 - C53	140.09 (10)	H10D—C109—H10E	108.2
C61 - Zr3 - C66	33.70 (10)	C111—C110—C109	112.4 (15)
C65 - 7r3 - C66	60.12 (10)	C111—C110—H11A	109.1
C62 - 7r3 - C66	59.95 (10)	C109-C110-H11A	109.1
$C_{53}$ $Z_{r3}$ $C_{66}$	133 08 (9)	C111—C110—H11B	109.1
C61 - 7r3 - C56	102.48(10)	C109—C110—H11B	109.1
C65 - Zr3 - C56	137 01 (10)	H11A—C110—H11B	107.9
$C_{62} = Z_{12} = C_{56}$	87 42 (11)	C110 - C111 - C112	107.9 (14)
$C_{3}$ $Z_{r_{3}}$ $C_{56}$	126 91 (10)	C110—C111—H11C	111 2
$C_{66} = 7r_{3} = C_{56}$	84 74 (10)	C112_C111_H11C	111.2
$C_{00}$ $Z_{13}$ $C_{50}$ $C_{61}$ $Z_{r3}$ $C_{50}$	110 11 (11)		111.2 111.2
C01-LIJ-CJ9	119.11 (11)		111.2

C65—Zr3—C59	131.17 (11)	C112—C111—H11D	111.2
C62—Zr3—C59	85.40 (10)	H11C—C111—H11D	109.1
C53—Zr3—C59	100.06 (11)	C113—C112—C111	107.4 (11)
C66—Zr3—C59	126.39 (11)	C113—C112—H11E	110.2
C56—Zr3—C59	51.76 (12)	C111—C112—H11E	110.2
C61—Zr3—C57	133.05 (10)	C113—C112—H11F	110.2
C65—Zr3—C57	167.57 (10)	C111—C112—H11F	110.2
C62—Zr3—C57	117.43 (9)	H11E—C112—H11F	108.5
C53—Zr3—C57	95.31 (10)	C112—C113—H11G	109.5
C66 - 7r3 - C57	108.03 (10)	C112—C113—H11H	109.5
$C_{56} - Zr_{3} - C_{57}$	31.66 (10)	H11G-C113-H11H	109.5
C59 - 7r3 - C57	51.17 (11)	C112—C113—H11I	109.5
C61 - Zr3 - C52	100 23 (9)	H11G-C113-H11I	109.5
C65 - 7r3 - C52	69 21 (9)	H11H—C113—H11I	109.5
000 210 002	09.21 (9)		109.5
C5—C1—C2—C3	3.6 (3)	C52—C53—C54—C55	4.9 (3)
Zr1—C1—C2—C3	-64.8(2)	Zr3—C53—C54—C55	-66.0(2)
C5—C1—C2—Zr1	68.4 (2)	C52—C53—C54—Zr3	70.9 (2)
C1—C2—C3—C4	-5.1 (3)	C53—C54—C55—C51	-3.4(3)
Zr1—C2—C3—C4	-70.7 (2)	Zr3—C54—C55—C51	-67.2(2)
C1—C2—C3—Zr1	65.6 (2)	C53—C54—C55—Zr3	63.8 (2)
C2—C3—C4—C5	4.7 (3)	C52—C51—C55—C54	0.5 (4)
Zr1—C3—C4—C5	-65.6(2)	Zr3—C51—C55—C54	67.9 (2)
C2—C3—C4—Zr1	70.4 (2)	C52—C51—C55—Zr3	-67.4 (2)
C3—C4—C5—C1	-2.5 (3)	C60—C56—C57—C58	1.9 (3)
Zr1—C4—C5—C1	-67.0 (2)	Zr3—C56—C57—C58	-67.75 (19)
C3—C4—C5—Zr1	64.4 (2)	C60—C56—C57—Zr3	69.68 (19)
C2-C1-C5-C4	-0.7 (3)	C56—C57—C58—C59	0.4 (3)
Zr1—C1—C5—C4	68.1 (2)	Zr3—C57—C58—C59	-66.3 (2)
C2—C1—C5—Zr1	-68.7 (2)	C56—C57—C58—Zr3	66.69 (18)
C10—C6—C7—C8	3.0 (3)	C57—C58—C59—C60	-2.6(3)
Zr1—C6—C7—C8	-65.35 (19)	Zr3—C58—C59—C60	-69.2 (2)
C10—C6—C7—Zr1	68.39 (18)	C57—C58—C59—Zr3	66.6 (2)
C6—C7—C8—C9	-2.1(3)	C58—C59—C60—C56	3.8 (3)
Zr1—C7—C8—C9	-67.22 (19)	Zr3—C59—C60—C56	-65.3(2)
C6—C7—C8—Zr1	65.09 (19)	C58—C59—C60—Zr3	69.1 (2)
C7—C8—C9—C10	0.4 (3)	C57—C56—C60—C59	-3.5(3)
Zr1—C8—C9—C10	-68.36 (19)	Zr3—C56—C60—C59	65.6 (2)
C7—C8—C9—Zr1	68.7 (2)	C57—C56—C60—Zr3	-69.17 (18)
C8—C9—C10—C6	1.5 (3)	C65—C61—C62—C63	5.2 (3)
Zr1—C9—C10—C6	-66.8 (2)	C66—C61—C62—C63	-142.3 (3)
C8—C9—C10—Zr1	68.37 (19)	Zr3—C61—C62—C63	-68.98 (19)
C7—C6—C10—C9	-2.8 (3)	C65—C61—C62—Zr3	74.18 (16)
Zr1—C6—C10—C9	66.66 (19)	C66—C61—C62—Zr3	-73.3 (2)
C7—C6—C10—Zr1	-69.49 (19)	C61—C62—C63—C64	-3.0 (3)
C15—C11—C12—C13	5.4 (3)	Zr3—C62—C63—C64	-63.5 (2)
C16—C11—C12—C13	-142.9 (3)	C61—C62—C63—Zr3	60.50 (17)
Zr1—C11—C12—C13	-69.05 (17)	C62—C63—C64—C65	-0.6 (3)

C15—C11—C12—Zr1	74.44 (16)	Zr3—C63—C64—C65	-60.95 (19)
C16—C11—C12—Zr1	-73.8 (2)	C62—C63—C64—Zr3	60.38 (19)
C11—C12—C13—C14	-3.4(3)	C63—C64—C65—C61	3.9 (3)
Zr1—C12—C13—C14	-64.32 (18)	Zr3—C64—C65—C61	-61.37 (17)
C11—C12—C13—Zr1	60.92 (16)	C63—C64—C65—Zr3	65.3 (2)
C12-C13-C14-C15	-0.1(3)	C62-C61-C65-C64	-5.6(3)
Zr1—C13—C14—C15	-60.85(17)	C66-C61-C65-C64	142.2 (3)
$C_{12}$ $C_{13}$ $C_{14}$ $Z_{r_1}$	60 76 (17)	$7r_{3}$ —C61—C65—C64	69 4 (2)
$C_{13}$ $C_{14}$ $C_{15}$ $C_{11}$	35(3)	$C_{62}$ $C_{61}$ $C_{65}$ $Z_{r3}$	-74.98(16)
$2r_1 - C_1 4 - C_1 5 - C_{11}$	-61.09(16)	$C_{66} - C_{61} - C_{65} - Z_{r3}$	72 8 (2)
$C_{13}$ $C_{14}$ $C_{15}$ $Z_{r1}$	64 62 (17)	C62 - C61 - C66 - C71	-394(4)
$C_{12}$ $C_{11}$ $C_{15}$ $C_{14}$	-55(3)	$C_{65} - C_{61} - C_{66} - C_{71}$	1787(2)
$C_{16}$ $C_{11}$ $C_{15}$ $C_{14}$	144.0(2)	$7r_{3}$ C61 C66 C71	-1109(2)
$2r_1 - C_{11} - C_{15} - C_{14}$	69.13(18)	213 - 201 - 200 - 271 C62 - C61 - C66 - C67	-173.9(2)
$C_{12} = C_{11} = C_{15} = C_{14}$	-74.59(16)	$C_{02} = C_{01} = C_{00} = C_{07}$	173.9(2)
$C_{12} = C_{11} = C_{13} = Z_{11}$	74.8 (2)	7*3 C61 C66 C67	114.6(2)
$C_{10} = C_{11} = C_{13} = Z_{11}$	74.0(2)	213-001-000-007	714.0(2)
C12 - C11 - C16 - C17	43.0(4)	$C_{02} = C_{01} = C_{00} = Z_{13}$	71.3(2)
C12-C11-C16-C17	-1/2.9(2)	$C_{00} = C_{01} = C_{00} = Z_{13}$	-70.4(2)
$2r_1 - c_1 - c_1 - c_1 / c_1$	115.8 (2)	C01 - C00 - C07 - C08	-104.5(3)
C15-C11-C16-C21	1/8.4 (2)		57.4 (3)
	-38.3(4)	Zr3	-89.6 (3)
Zr1—C11—C16—C21	-109.6 (2)	C61—C66—C67—C72	76.2 (3)
CI5—CII—CI6—ZrI	-72.1 (2)	C/I_C66_C67_C72	-62.0(3)
C12—C11—C16—Zr1	71.3 (2)	Zr3—C66—C67—C72	151.0 (2)
C11—C16—C17—C18	-164.1 (3)	C66—C67—C68—C69	-58.8 (3)
C21—C16—C17—C18	57.3 (3)	C72—C67—C68—C69	60.4 (4)
Zr1—C16—C17—C18	-90.2 (3)	C67—C68—C69—C70	59.2 (4)
C11—C16—C17—C22	76.6 (3)	C67—C68—C69—C73	-60.5 (4)
C21—C16—C17—C22	-61.9 (3)	C68—C69—C70—C71	-59.6 (4)
Zr1—C16—C17—C22	150.59 (18)	C73—C69—C70—C71	60.1 (4)
C16—C17—C18—C19	-60.0 (3)	C61—C66—C71—C70	165.1 (2)
C22-C17-C18-C19	59.0 (3)	C67—C66—C71—C70	-57.2 (3)
C17—C18—C19—C23	-59.6 (4)	Zr3—C66—C71—C70	90.9 (3)
C17—C18—C19—C20	60.3 (3)	C61—C66—C71—C74	-76.0 (3)
C23-C19-C20-C21	59.9 (3)	C67—C66—C71—C74	61.7 (3)
C18—C19—C20—C21	-60.4 (4)	Zr3C66C71C74	-150.2 (2)
C11—C16—C21—C20	165.5 (2)	C69—C70—C71—C66	59.2 (3)
C17—C16—C21—C20	-56.9(3)	C69—C70—C71—C74	-59.7 (4)
Zr1-C16-C21-C20	92.4 (3)	C66—C67—C72—C75	60.9 (4)
C11—C16—C21—C24	-76.0 (3)	C68—C67—C72—C75	-59.9 (4)
C17—C16—C21—C24	61.7 (3)	C68—C69—C73—C75	60.1 (4)
Zr1—C16—C21—C24	-149.0(2)	C70—C69—C73—C75	-59.5 (4)
C19—C20—C21—C16	59.3 (3)	C66—C71—C74—C75	-60.9 (4)
C19—C20—C21—C24	-59.7 (3)	C70-C71-C74-C75	59.1 (4)
C16—C17—C22—C25	60.6 (3)	C69—C73—C75—C74	59.6 (4)
$C_{18}$ $C_{17}$ $C_{22}$ $C_{25}$	-60.2 (3)	C69—C73—C75—C72	-60.1(4)
C18 - C19 - C23 - C25	59.9 (4)	C71—C74—C75—C73	-59.9(4)
$C_{20}$ $C_{19}$ $C_{23}$ $C_{25}$	-59 1 (3)	C71-C74-C75-C72	60 1 (4)
0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 =		0,1 0,1 0,0 0,2	~~~ ( )

C16-C21-C24-C25	-59.8(3)	C67 - C72 - C75 - C73	60.3(4)
$C_{20}$ $C_{21}$ $C_{24}$ $C_{25}$	60 3 (3)	C67 C72 C75 C74	-60.1(4)
$C_{20} = C_{21} = C_{24} = C_{25}$	(0.3(3))	$C_{0}^{0} = C_{12}^{-1} = C_{13}^{-1} = C_{14}^{-1}$	21(2)
$C_{21} = C_{24} = C_{25} = C_{25}$	-60.8(3)		5.1 (5)
$C_{21} - C_{24} - C_{25} - C_{22}$	58.6 (3)	Zr4 - C/6 - C/7 - C/8	-65.7(2)
C19—C23—C25—C24	59.9 (4)	C80—C/6—C//—Zr4	68.8 (2)
C19—C23—C25—C22	-60.0 (4)	C76—C77—C78—C79	-3.3 (3)
C17—C22—C25—C24	-59.2 (3)	Zr4—C77—C78—C79	-69.4 (2)
C17—C22—C25—C23	60.7 (3)	C76—C77—C78—Zr4	66.1 (2)
C30—C26—C27—C28	3.0 (3)	C77—C78—C79—C80	2.4 (3)
Zr2—C26—C27—C28	-65.75 (19)	Zr4—C78—C79—C80	-67.0 (2)
C30-C26-C27-Zr2	68.7 (2)	C77—C78—C79—Zr4	69.4 (2)
C26—C27—C28—C29	-4.1 (3)	C78—C79—C80—C76	-0.5(3)
Zr2—C27—C28—C29	-70.00 (19)	Zr4—C79—C80—C76	-66.35 (19)
C26—C27—C28—Zr2	65.91 (19)	C78—C79—C80—Zr4	65.88 (19)
C27—C28—C29—C30	3.7 (3)	C77—C76—C80—C79	-1.6(3)
Zr2—C28—C29—C30	-66.1(2)	Zr4—C76—C80—C79	67.0 (2)
$C_{27}$ $C_{28}$ $C_{29}$ $T_{r^2}$	69 80 (19)	C77—C76—C80—Zr4	-68.6(2)
$C_{28}$ $C_{29}$ $C_{30}$ $C_{26}$	-1.9(3)	$C_{85}$ $C_{81}$ $C_{82}$ $C_{83}$	36(3)
$7r^2 - C^2 9 - C^3 0 - C^2 6$	-67.5(2)	7r4-C81-C82-C83	-64.6(2)
$C_{12}^{-} = C_{23}^{-} = C_{30}^{-} = C_{20}^{-} = C_{$	67.5(2)	$C_{14} = C_{01} = C_{02} = C_{03}$	68.1(2)
$C_{20} = C_{20} = C_{30} = C_{12}$	-0.7(2)	$C_{83} - C_{81} - C_{82} - C_{84}$	-4.8(2)
$C_2/-C_20-C_30-C_29$	-0.7(3)	$C_{01} = C_{02} = C_{03} = C_{04}$	-4.0(3)
$2f_2 - C_2 - C_3 - C_2 - C_2$	08.0(2)	2r4 - c82 - c83 - c84	-70.89(19)
$C_2/-C_{26}-C_{30}-Z_{f_2}$	-69.24(19)	C81 - C82 - C83 - Zf4	66.1 (2)
C35—C31—C32—C33	3.2 (4)	C82—C83—C84—C85	4.2 (3)
Zr2—C31—C32—C33	-65.4 (3)	Zr4—C83—C84—C85	-66.8 (2)
C35—C31—C32—Zr2	68.6 (2)	C82—C83—C84—Zr4	70.98 (19)
C31—C32—C33—C34	-1.6 (4)	C83—C84—C85—C81	-2.0 (3)
Zr2—C32—C33—C34	-67.2 (3)	Zr4—C84—C85—C81	-67.0 (2)
C31—C32—C33—Zr2	65.7 (2)	C83—C84—C85—Zr4	64.9 (2)
C32—C33—C34—C35	-0.7 (4)	C82—C81—C85—C84	-1.0 (4)
Zr2—C33—C34—C35	-70.1 (2)	Zr4—C81—C85—C84	67.3 (2)
C32—C33—C34—Zr2	69.4 (3)	C82—C81—C85—Zr4	-68.2 (2)
C33—C34—C35—C31	2.7 (4)	C90—C86—C87—C88	5.4 (3)
Zr2—C34—C35—C31	-66.9 (2)	C91—C86—C87—C88	-142.9(3)
C33—C34—C35—Zr2	69.6 (3)	Zr4—C86—C87—C88	-70.01 (19)
C32—C31—C35—C34	-3.7 (4)	C90—C86—C87—Zr4	75.38 (16)
Zr2—C31—C35—C34	65.8 (2)	C91—C86—C87—Zr4	-72.9(2)
$C_{32}$ — $C_{31}$ — $C_{35}$ — $Z_{r_{2}}$	-69.4(2)	C86—C87—C88—C89	-3.7(3)
C41 - C36 - C37 - C38	-1433(2)	Zr4-C87-C88-C89	-6540(19)
C40-C36-C37-C38	51(3)	$C_{86} = C_{87} = C_{88} = 7r4$	61.68 (16)
$7r^2 - C^3 6 - C^3 7 - C^3 8$	-68.67(19)	C87 - C88 - C89 - C90	05(3)
$C_{12} = C_{30} = C_{37} = C_{30}$	-74.6(2)	7r4 C88 C89 C90	-60.19(18)
$C_{11} = C_{10} = C$	73.81(16)	217 - 000 - 000 - 000	60.60 (18)
$C_{40} - C_{50} - C_{57} - C_{12}$	-20(2)	$C_{0} = C_{0} = C_{0} = C_{0} = C_{0}$	(10)
-100 - 100	5.0(5)	-00 - 00 - 00 - 00	2.7 (3)
212 - 03 / - 038 - 039	-03.30(19)	$\angle I4 - \angle \delta y - \angle y 0 - \angle \delta b$	-00.38(10)
$C_{30} - C_{3} / - C_{38} - Z_{12}$	00.52 (17)	las = las	03.30 (19)
C37—C38—C39—C40	-0.5 (3)	C87—C86—C90—C89	-5.0 (3)
Zr2—C38—C39—C40	-61.15 (18)	C91—C86—C90—C89	142.7 (3)

$C37$ $C38$ $C30$ $7r^{2}$	60 66 (18)	7r4 C86 C90 C89	60.21(10)
$C_{38} = C_{39} = C_{40} = C_{36}$	3 8 (3)	C87 - C86 - C90 - Zr4	-74.26(16)
$7r^2 - C^{39} - C^{40} - C^{36}$	-61.64(17)	C01 - C86 - C90 - 7r4	73 5 (2)
$C_{38}$ $C_{39}$ $C_{40}$ $Z_{r2}$	65 41 (19)	C90 - C86 - C91 - C96	171.3(2)
$C_{37}$ $C_{36}$ $C_{40}$ $C_{39}$	-5.4(3)	$C_{87}$ $C_{86}$ $C_{91}$ $C_{96}$	-46.2(4)
$C_{41}$ $C_{36}$ $C_{40}$ $C_{39}$	3.7(3)	7r4 - C86 - C91 - C96	-116.8(2)
$7r^2$ C36 C40 C39	60.33(18)	214 - 280 - 291 - 290	373(4)
212 - C36 - C40 - C39	-74.77(17)	$C_{90} = C_{80} = C_{91} = C_{92}$	$\frac{37.3(4)}{170.8(2)}$
$C_{37} = C_{30} = C_{40} = Z_{12}$	74.77(17)	$7_{r4} = 686 = 691 = 692$	1/9.8(2) 100.2(2)
$C_{41} = C_{30} = C_{40} = Z_{12}$	74.4(2)	214 - 0.00 - 0.001 - 0.000 -	109.2(2)
$C_{37} - C_{30} - C_{41} - C_{40}$	-39.3(4)	C90 - C80 - C91 - Z14	-71.9(2)
	1/7.4(2)	$C_{8} = C_{80} = C_{91} = C_{14}$	166.2(2)
212 - C30 - C41 - C40	-111.3(2)	$C_{80} - C_{91} - C_{92} - C_{93}$	-100.3(3)
$C_{3} = C_{3} = C_{4} = C_{4} = C_{4}$	-1/3.9(2)	C96-C91-C92-C93	56.8(3)
C40 - C36 - C41 - C42	42.8 (3)	Zr4-C91-C92-C93	-92.6 (3)
$2r_2 - C_{36} - C_{41} - C_{42}$	113.9 (2)	C86—C91—C92—C97	75.3 (3)
$C_{37} - C_{36} - C_{41} - Z_{r2}$	72.2 (2)	C96—C91—C92—C97	-61.6 (3)
C40—C36—C41—Zr2	-71.2 (2)	Zr4—C91—C92—C97	149.0 (2)
C36—C41—C42—C43	-164.6 (2)	C91—C92—C93—C94	-59.1 (3)
C46—C41—C42—C43	57.1 (3)	C97—C92—C93—C94	59.6 (4)
Zr2—C41—C42—C43	-91.2 (3)	C92—C93—C94—C95	59.8 (3)
C36—C41—C42—C47	76.3 (3)	C92—C93—C94—C98	-60.0 (4)
C46—C41—C42—C47	-62.0 (3)	C93—C94—C95—C96	-59.5 (4)
Zr2—C41—C42—C47	149.7 (2)	C98—C94—C95—C96	60.2 (4)
C41—C42—C43—C44	-59.4 (3)	C94—C95—C96—C91	59.2 (4)
C47—C42—C43—C44	59.9 (3)	C94—C95—C96—C99	-59.8 (4)
C42—C43—C44—C48	-60.1 (3)	C86—C91—C96—C95	164.8 (3)
C42—C43—C44—C45	60.1 (4)	C92—C91—C96—C95	-57.3 (3)
C48—C44—C45—C46	60.4 (3)	Zr4—C91—C96—C95	89.9 (3)
C43—C44—C45—C46	-60.2 (3)	C86—C91—C96—C99	-75.9 (3)
C36—C41—C46—C45	165.6 (2)	C92—C91—C96—C99	62.0 (3)
C42—C41—C46—C45	-56.9 (3)	Zr4—C91—C96—C99	-150.8 (2)
Zr2-C41-C46-C45	92.1 (3)	C91—C92—C97—C100	60.0 (4)
C36—C41—C46—C49	-75.6 (3)	C93—C92—C97—C100	-59.6 (4)
C42—C41—C46—C49	61.9 (3)	C95—C94—C98—C100	-59.8 (5)
Zr2—C41—C46—C49	-149.14 (18)	C93—C94—C98—C100	59.4 (4)
C44—C45—C46—C41	59.1 (3)	C95—C96—C99—C100	59.9 (4)
C44—C45—C46—C49	-59.7 (3)	C91—C96—C99—C100	-60.8 (4)
C43—C42—C47—C50	-60.4 (3)	C94—C98—C100—C97	-60.1 (4)
C41—C42—C47—C50	60.3 (3)	C94—C98—C100—C99	60.0 (4)
C43—C44—C48—C50	59.3 (3)	C92—C97—C100—C98	60.8 (4)
C45—C44—C48—C50	-60.3 (4)	C92—C97—C100—C99	-59.3 (3)
C41—C46—C49—C50	-60.3(3)	C96—C99—C100—C98	-60.5(4)
C45—C46—C49—C50	59.9 (3)	C96—C99—C100—C97	59.8 (4)
C44—C48—C50—C47	-59.3 (3)	C106—C101—C102—C103	6.1 (14)
C44—C48—C50—C49	60.5 (3)	C107—C101—C102—C103	-177.2 (13)
C42—C47—C50—C48	60.4 (3)	C101—C102—C103—C104	-6.5(15)
C42—C47—C50—C49	-59.2 (3)	C102-C103-C104-C105	2.5 (17)
C46—C49—C50—C48	-60.6(3)	C103 - C104 - C105 - C106	2.4(18)
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C46—C49—C50—C47	59.2 (4)	C104—C105—C106—C101	-2.8 (17)
C55—C51—C52—C53	2.5 (4)	C107—C101—C106—C105	-178.5 (13)
Zr3—C51—C52—C53	-65.5 (2)	C102—C101—C106—C105	-1.4 (16)
C55—C51—C52—Zr3	68.0 (2)	C108—C109—C110—C111	86.9 (18)
C51—C52—C53—C54	-4.6 (3)	C109—C110—C111—C112	-165.7 (13)
Zr3—C52—C53—C54	-72.0 (2)	C110—C111—C112—C113	178.6 (14)
C51—C52—C53—Zr3	67.4 (2)		