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FWEH induced high bootstrap current on Tore Supra

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Abstract: Bootstrap current is regarded as a good candidate to sustain a large fraction of the plasma current, in the so-called "advanced" regimes of a tokamak reactor. It is thus important to study the stability of such discharges and to control them.

By means of fast wave electron heating (FWEH, up to 9.5 MW), stationary high bootstrap discharges (during 5 secondes, \dot{A} 40 %) were routinely obtained on Tore Supra. The bootstrap profile is computed with a matrix formulation(1,2) and is directly compared to the calculation of the non-inductive current.

The simulation of the loop voltage either with the code CRONOS (1D current diffusion code) using the profile of bootstrap current, or with the knowledge of the resistivity, allows also a self consistent determination of the bootstrap current. First results show that the energy enhancement factor H increases linearly with the fraction of bootstrap current.

The bootstrap induced by the FWEH is mainly due to the central pressure electron gradient (the central power deposition strongly peaks the electronic temperature). A 0D study shows that the bootstrap current (I_{bs}) varies linearly with the poloidal beta ($I_{bs}/I_p = C_{bs} \beta_p$).

The effect of various plasma parameters (toroidal field B_t , line-integrated density n_l , ion and electron temperature, plasma current I_p) on the bootstrap profile, fraction, C_{bs} and on the confinement are analysed.

BOOTSTRAP CURRENT INDUCED BY FWEH

Fast Wave Electron Heating (dipole operation, up to 9.5 MW) induces high bootstrap discharges by means of an electronic central power deposition. The electronic temperature, strongly peaked, is responsible for more than 80 % of the bootstrap current. The bootstrap profile is computed by two ways :

- a theoretical approach (with a matrix formulation (1,2), valid in all collisionality regime and aspect ratio)
- a determination of the non-inductive current which is, in our case, purely the bootstrap current.

A database of more than hundred shots (Fig. 1) was obtained in various plasma conditions ($T_e(0) = 2-8$ keV, $n_e(0) = 4.5-5.5 \cdot 10^{19} \text{ m}^{-3}$, $T_i(0) = 1-3$ keV, $I_p=0.4-1$ MA, $B_T=2.2, 2.8$ and 3.4 T, Helium). Many shots are considered as stationary shots (1 to 5 seconds) with respect to the diffusion time of the current. The electrons are in banana collisionality regime, and the ions in the plateau regime. This database allows a study of the effect of plasma parameters on the bootstrap current profile.

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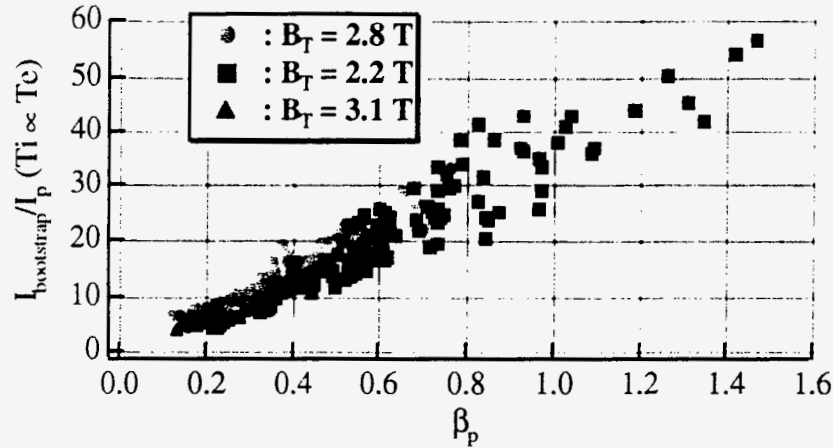


Figure I : Current bootstrap fraction versus poloidal beta

Validation of the model

The experimental bootstrap profile (non-inductive current) is determined by subtracting the ohmic current profile from the total current. The ohmic fraction of the current is inferred from the neoclassical resistivity and the loop voltage profile calculated by time sequences of kinetic equilibria (3). This current is fairly compared to the theoretical estimation. The slight difference between the experimental and predicted profile (Fig. II b)) is well explained by the indetermination on the charge effective (Z_{eff}).

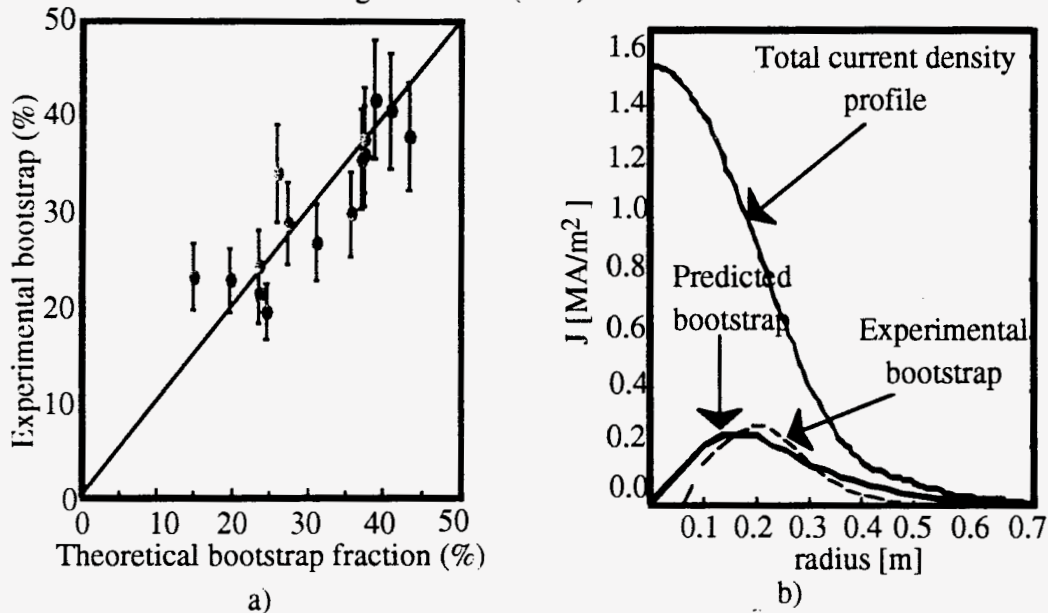


Figure II : a) Comparison for twelve shots between the non-inductive current and the theoretical prediction of the current bootstrap fraction ($B_T = 2.2$ T) b) Comparison of the profiles

Both determination of profiles requires the knowledge of Z_{eff} . As the Z_{eff} profile is not measured, it is assumed constant. But, recent measurements show that the Z_{eff} profile is slightly peaked, which pushes the non-inductive current towards the center of the plasma whereas it has a small effect on the predicted profile. Then, the two profiles tend to match well.

Another strong assumption is made on the ionic temperature (T_i) profile. T_i is supposed to be either homothetic to the electronic temperature, or to the electronic density. The last

hypothesis seems to be confirmed by new measurements of Ti made by charge exchange spectroscopy during ohmic discharges (4). The comparison between the two hypothesis (Fig. 3a)) allows an estimation of the error made on the bootstrap determination (Fig. 3b)) through the standard deviation of the gaussian fit : $\sigma \approx 10\%$.

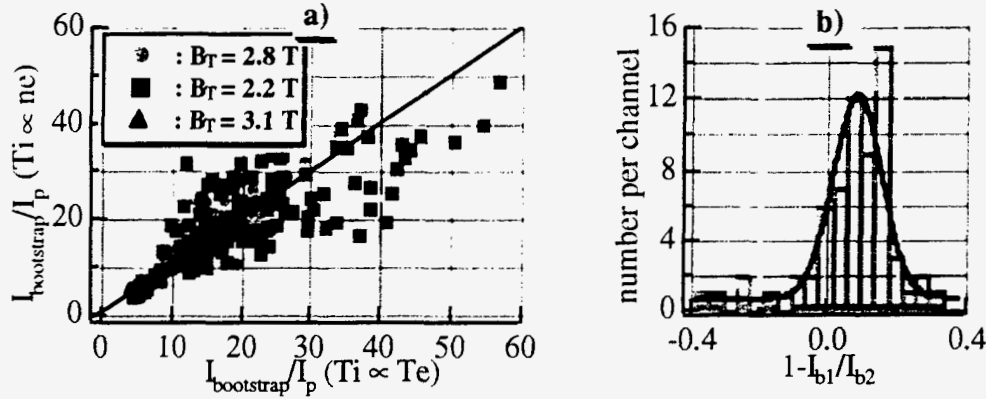


Figure III: a) Effect of Ti profile hypothesis (Ti proportional to ne or Te) on the current bootstrap fraction
 b) deviation between the two hypothesis ($1 - I_{b1}/I_{b2}$)

The simulation of the loop voltage, by a 1D current diffusion code (5) using as input the predicted bootstrap profile strengthen the use of matrix formulation to calculate the bootstrap current (i.e. the Faraday rotation angles, q profile and li profile are well simulated).

Scaling law for the bootstrap fraction

A systematic study was made to find the plasma parameters which play a role in the bootstrap current. In the case of bootstrap induced by FWEH the main parameter is the poloidal beta (β_p), as the fraction of bootstrap varies almost linearly with β_p (Fig. I):

$$\frac{I_{bootstrap}}{I_p} = 0.34 \beta_p^{1.09 \pm 0.04}$$

No effect of temperature or density gradient is observed (one must note that for the density gradient, the range of variation is rather small).

$$\frac{I_{bootstrap}}{I_p} = 0.36 \beta_p^{1.11 \pm 0.05} p_p^{-0.08 \pm 0.04} p_T^{0.03 \pm 0.08}$$

p_p and p_T are the pressure and temperature peakedness

The effect of $Te(0)$ and $\langle n \rangle$, independently of β_p , can also be deduced from the database

$$\frac{I_{bootstrap}}{I_p} = 0.28 Te(0)^{1.50 \pm 0.11} \langle n \rangle^{0.43 \pm 0.19}$$

The large error on the density coefficient is due to the small range of variation of $\langle n \rangle$ ($\langle n \rangle = 3.3 \pm 0.8 \cdot 10^{19} \text{ m}^{-3}$ for the database). The effect of temperature is clearly dominant over the effect of density.

BOOTSTRAP DEPENDENCE ON TE AND NE PROFILE

In the objective of increasing the bootstrap current fraction and of controlling the bootstrap profile, it is essential to study the effect of Te and ne profile on the bootstrap current.

The shape of the temperature (T_e) and density (n_e) profile can be defined with four parameters :

$$T_e(\rho) = T_e(0) \times (1 - \rho^{\alpha_{Te}})^{\beta_{Te}}, \quad n_e(\rho) = n_e(0) \times (1 - \rho^{\alpha_{ne}})^{\beta_{ne}}, \quad \text{with}$$

$$1 < \alpha < 5, \quad 0.5 < \beta < 4 \quad \text{and} \quad 2 < T_e(0) [\text{keV}] < 10, \quad 2 < n_e(0) [10^{19} \text{ m}^{-3}] < 9$$

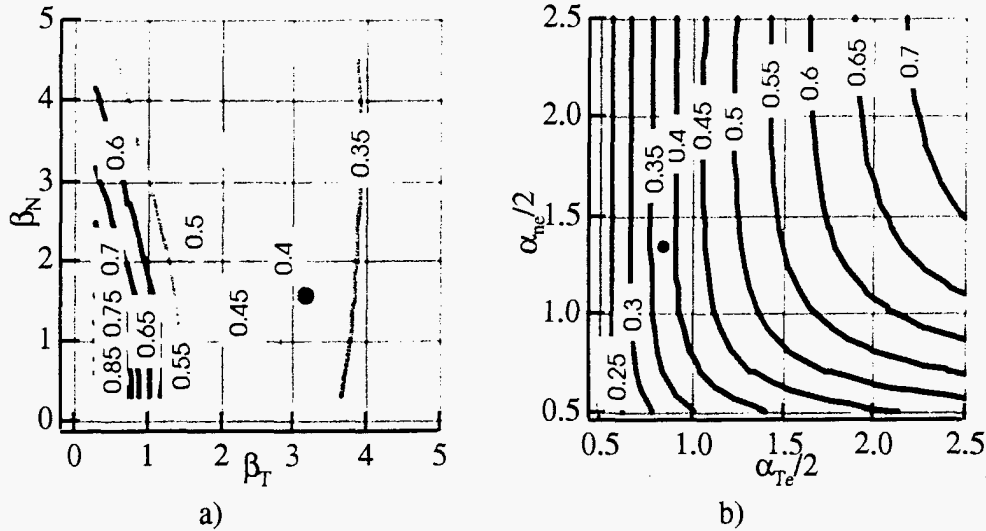


Figure IV: Effect on the bootstrap fraction of a) peakedness profile (β) b) gradient location (α) : ● shot 18805

The major trend of the simulation (Fig. 4) is that the temperature gradient has more effect on the bootstrap current than the density gradient. However, an increasing of the central density has the same effect on the current bootstrap than an increasing of the central temperature. Thus a pellet injection has an influence on the bootstrap fraction more by the fuelling effect than by a profile effect

Recent studies of non-inductive current during FWEH validated the use of matrix formulation to calculate the bootstrap current, show a major effect of the T_e profile and leads to a TS scaling law for the bootstrap fraction.

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