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Cal Poly: San Luis Obispo | Mechanical Engineering Dept.

# Robotic Fingerspelling Hand for Deaf-Blind Communication 

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# MLD PM 

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## Capstone Project

Partial fulfillment of the requirements for a
Bachelor of Science degree in Mechanical Engineering

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Rehabilitation Engineering Research Center for Blindness and Low Vision

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## Introduction

Fluent communication is something that many people take for granted, but there is a population that faces extreme difficulties with communication due to disabilities such as deafblindness. Most adults with this condition have been diagnosed with Usher's Syndrome. The typical progression of Usher's Syndrome starts with deafness at birth, and blindness occurring later in life. This puts the affected individual into a position where they already know sign language but not braille when they lose their sight. The term deaf-blind encompasses those who have completely lost their hearing and sight as well as those who have only partially lost these senses. For people with this condition, tactile sensation eventually becomes their main form of communication.

Various methods of tactile communication have been developed, such as the Braille alphabet and the Tadoma method, but this project will focus on tactile finger-spelling. By feeling the hand of a finger-speller, a deaf-blind person can read a message letter-by-letter using a learned alphabet such as the American Sign Language alphabet. In this age of technology, a mechanical hand that could take the place of a fingerspeller and connect to a computer would be of huge value to someone who is deaf-blind. Currently there are no commercial mechanical fingerspelling hands. The deaf-blind community still relies on a translator to communicate with people who do not know sign language or fingerspelling. If there is a device that could fingerspell simply by typing message, fluent communication between a deaf-blind individual and an individual with no fingerspelling experience would achievable.

The Smith-Kettlewell Eye Research Institute in San Francisco, henceforth referred to as SKERI, had great interest in this project and has gotten universities to try to make it a reality. Several variations of a robotic fingerspelling hand have been initiated by SKERI, specifically by the Rehabilitation Engineering Research Center and Dr. Deborah Gilden, who has asked our team to approach this task from a new angle. The major stakeholders consist of SKERI, the deaf-blind community, and our team, as the success of this project is important to our education as engineers. Ultimately, the goal is to open the avenue of electronic communication to the fingerspelling deafblind community. Our main goal is to create a robust, working robotic fingerspelling hand that can fingerspell every letter in the American Sign Language alphabet. Other specifications that SKERI require are that the hand is the size of an average person and that is it portable. Specifications that

SKERI would like to see are: battery powered hand, hand size comparable to a small female, and text to speech.

## Capstone Project:

This project has been completed in partial fulfillment of the requirements for a Bachelor's Degree in Mechanical Engineering at California Polytechnic State University, San Luis Obispo. All three of the team members are students in the Mechanical Engineering Department. Trevor Wong and Colby Dixon will be leaving Cal Poly with their degrees upon completion of this project, and Brian Fang will be staying to earn his Masters in Mechanical Engineering. The Capstone Project in the Mechanical Engineering department is meant to be an exercise in teamwork and design, starting from the brainstorming process and moving all the way through the manufacturing and testing of a device. All Mechanical Engineering students go through this process with a team that has been assembled by the department to complement one another.

The process is three quarters; the students are enrolled in ME 428 in the fall, ME 429 in the winter, and ME 430 in the spring. The first two quarters involve assigned lab time with a project advisor assigned by the department. In the case of this team, Dr. John Ridgely was assigned our team due to his expertise in the area of mechatronics, or "Mechanical Electronics". Throughout the process, the students are constantly reminded that this is an exercise in the process of mechanical design. Upon completion of the capstone project, it is the departments hope that the students will be able to effectively work with a team to design and create a viable solution to some problem, as well as to communicate effectively with the sponsor who has an interest in the project and supplies the funding.

## Project Scope:

Because so many attempts have been made to create a usable finger-spelling hand, we made an attempt to build on past successes and failures rather than make the same mistakes. The goal of this project has increasingly been to just make something work, even if it does not perfectly mimic the movements of a human hand. We have made an attempt to describe our design to a point where someone can easily apply what we have learned to a newer design that will address some of the issues that we have had. A section of design recommendations is included at the end of the report.

## Unit System:

The U.S. Customary Unit system was chosen for this project because it is the most commonly used unit for engineers in the Cal Poly Mechanical Engineering Department. Conversions were very minimal, as most of the specifications for components of the project were described in U.S. Customary, sometimes in addition to Metric units. The anthropometric tables used to determine hand size provide an example of the need for U.S. Customary units, as there are no listings of Metric units in the anthropometric data.

## Terminology:

Team HandSpeak: Handspeak is a registered trademark as detailed at handspeak.com. The contents of the website are also copyrighted. The name "Team HandSpeak" is used solely for the purpose of the Mechanical Engineering Capstone project at California Polytechnic State University, San Luis Obispo in the time period of September 2011 through June 2012. The logo for Team HandSpeak is significantly different than the logo for handspeak.com. In the event of any content from handspeak.com being used in Team HandSpeak's final report, the proper citation will be added as per handspeak.com's specifications. HandSpeak is not to be used as a brand name or product name in any future revisions of the final design created by Team HandSpeak.

Deaf-blindess: There are various ways to write the term "deaf-blind". For this report, both "deaf" and "blind" will be fully lowercase unless beginning a sentence or title. Someone who is deaf-blind is considered to have impaired vision and hearing, it does not necessarily mean that they are both legally blind and deaf.

Cal Poly: This capstone project is completed for a bachelor's degree at California Polytechnic State University, San Luis Obispo. The name of the college is commonly referred to as simply "Cal Poly", and will be referred to as such for the rest of the report.

Proximal-Medial-Distal Phalanges: The segments of the fingers that are connected by joints are known as "phalanges". The term "proximal" describes the phalange closest to the hand, "medial" describes the middle phalange, and "distal" describes the tips of the fingers.

Cables: Many different actuating lines were used in the development of the hand. All of them had the characteristic of being small, flexible, able to carry tension, and easily tied at the ends. For this report, items with these characteristics are referred to as the "cables" that transfer power from the motors to the mechanisms. A more descriptive term for our final choice would be "coated wire rope", but we feel that "cable" is sufficient.

Servos: This term requires the most explanation because it is the least defined. Technically, a "servomechanism" is any mechanical device that has some sort of automatic feedback that tunes the performance of the device. "Servomechanism" is often shortened to "servo", but can still apply
to any device such as a valve or piston. The term "servo" in our report refers to small Hobby Servo Motors that contain a potentiometer and feedback circuit within the body of the device. This makes the motors much easier to control than attaching our own encoders for example, which would require many more connections and electronics.

Torsion Springs: Truly, a torsion spring is one that stores energy via torsion in the material. The springs used in the hand are referred to as "torsion springs" because they create and resist torque about the pivots. The metal itself is actually storing energy via bending as the coils get tighter.

## Background

The first attempt at creating a fingerspelling hand was patented in 1978 by the Southwest Research Institute, henceforth referred to as SWRI. It served to be a proof of concept but failed to make all the necessary hand-shapes and operate in a fluid manner. Since then there have been five notable attempts, along with five projects at Cal Poly, three of which are completed and two of which are currently in progress. Due to the history of engineering on this topic, our team has chosen to focus our background research on these previous hands and will forgo extensive research into other far more complicated robotic and prosthetic hands. The following paragraphs will provide a brief background of the four hands that we benchmarked against and why.


Figure 1. Dexter

## DEXTER:

The first hand we will focus on has been dubbed "Dexter" by SKERI. It was built by a team of Stanford Mechanical Engineering Students in 1985. Dexter was much improved over the hand built by SWRI and formed all the letters of the alphabet but was extremely bulky and required compressed air to drive the pneumatic actuators. Although the drive system was impractical and bulky, the hand itself was quite successful for the level of simplicity in its design. The whole hand had seven pneumatic actuators. Each finger was actuated by a single pneumatic with a linear spring to provide some resistance and return. The pneumatic pulled four metal cables. Three of the cables were used to bend each section of the finger and the last cable was used to straighten the finger. For the index finger, there was a second pneumatic that twisted the finger so that it could form the letter R. The thumb was controlled by two pneumatics actuators. The first one controlled the
bending of the thumb across the hand. The second one controlled the thumbs movement to and away from the hand. Since the hand was made of metal, it is very sturdy and robust. As other attempts have been bogged down by too many complications, we felt that Dexter was studying for inspiration. The cable system proved to be very effective in bending the fingers and its overall design is very robust. Two subsequent Dexter designs later came about and met with mild success.


Figure 2. Ralph

## Ralph:

The most successful of the designs seems to be RALPH, for Robotic ALPHabet. This hand was built in 1994 by the Rehabilitation Research and Development department of the Veterans Affairs. RALPH fixed many of the problems of the Dexter hands, but still wasn't quite robust or attractive enough to be picked up by any commercial companies. RALPH was also only half a hand as it only had the fingers, no forearm and no wrist. The hand is also very short, which made it hard to read as it is in an unnatural position for the reader. It was actuated with DC servo motors. The fingers were made with mechanical linkages rather than wire. RALPH connected to computers using a serial connection, RS232. The interface with the user was done through a computer. While all the control was done on the microcontroller in the hand.


Figure 3. Cal Poly Senior Project \#1

## Cal Poly Senior Project \#1:

In January 2008, a senior project team at Cal Poly took on this challenge, accomplishing a remarkable amount of research and development in their short time frame of six months. They built a working hand that met many of the requirements for the project. Unfortunately, they ran into a serious problem when they found that their choice of actuators overheated and limited the use time of the hand. They chose to build the hand out of aluminum. This resulted in a hand that was bulky and not lifelike enough to be successful. There is much to learn from their design process and trial and error.


Figure 4. Cal Poly Senior Project \#2

## Cal Poly Senior Project \#2:

We are also benchmarking against the hand of a Cal Poly interdisciplinary team. Of the many things that we can learn from this hand is the performance of hobby servos and manufacturing. The hand had issues with durability, and it broke in several places, but at one time it was a working device. Each joint was connected with a mechanical linkage, so only one servo was needed to completely bend a finger. This design does not allow for independent motion of the distal, intermediate phalanges to the proximal phalange.


Figure 5. Jerry Vin's Graduate Thesis Hand

## Jerry Vin:

Another hand is the work of Jerry Vin, a graduate student at Cal Poly. Jerry's project is currently in progress and he has expressed interest in offering his experiences to our team. His design uses eleven DC brushless motors and two DC hobby servos. The index finger is controlled by three motors. The motors rotate to pull on a cable that bends or straightens the joints. This distal phalange is linked to the intermediate phalange with a mechanical linkage. As the intermediateproximal joint bends, the distal-intermediate joint bends with it. The last motor pulls on a cable that moves the finger to the side so that it can make the letter V . The ring and pinky finger are controlled by one motor. The middle finger is actuated exactly like the index finger, except it does not have a third motor to move it side to side. They are the same as the middle finger, except they do not need independent control for the intermediate-proximal and proximal-metacarpal joints, so those cables are threaded through one motor. The thumb is controlled by four motors. One motor was used to control the distal-proximal joint and another to control the proximal-metacarpal joint. The third motor is used to move the thumb across the hand. The last motor is to control the thumbs movement to and away from the hand. As we are somewhat designing in parallel, it seems useful to benchmark against his work and collaborate with thoughts and positive criticisms.

## Objective

Our project was to build a device that would be able to communicate with a deaf-blind person through fingerspelling. The main goal of the project is to have the device form all 26 letters in the English alphabet and sequence them into words. The next major goal is to make the system as robust as possible. This means that it will work reliably and smoothly throughout its lifetime. The device should be portable, as well as allow the user the option of different orientations, such as horizontal and vertical. The operation of the device will be driven by a computer. This will require a substantial amount of coding. Few other smaller goals are that the device should not be too loud, look realistic and easy to fix. The product should be safe. Safety issues include: features ensuring the hand will not crush a user's hand, prevention of exposed wires shocking the user, etc.

## Sponsor's Requirements:

- The hand should be able to form all 26 letters of the American Manual Alphabet.
- The hand should be lifelike.
- The hand should be portable and be able to be read in different orientations.
- The hand should be the size of an average adult or smaller.
- The hand should not have any heating issues where the reader would get burned from touching the hand.
- The hand should be able to form letters at minimum a speed of one letter per second.
- The hand should be able to form letters based off of user input.
- The hand should cost under $\$ 1000$. Ideally in the $\$ 500$ range.

Based on the sponsors' requirements, we came up with the following categories of engineering targets:

- Internal Temperature - Sustainable heat dispersion
- External Temperature - Temperature on the exterior of the hand
- Input / Output - Ability to spell letters after being typed
- USB or serial port - The type interface with the computer
- Number of interfaces - What programs will be used to connect the computer and hand
- Delay between letters - The time delay between forming letters
- Delay between words - The time delay after finishing spelling a word
- Number of external controls - Number of buttons or switches on the exterior of the hand
- Ability to form letters - The accuracy and ability to form letters
- Ease of Use - How intuitive is the device and the length of the learning curve
- Double letter indication
- Noise Level
- Weight
- Time to attach/detach - The amount of time it will take to detach from a base
- Battery Life
- Usage Voltage - Amount of voltage used to operate the device
- Length of Hand
- Glove - Will a glove be used
- Horizontal - Can the device be used while it is parallel to the floor
- Vertical - Can the device be used while standing upright
- Lap held - Can the device be used while lying on someone's lap
- To scale - how to scale the fingers relative to each other and palm
- Interior accessibility - The ease of getting to the interior of the device
- Production cost
- Price
- Life-time
- Force to induce
- Force to withstand

Through the process of making a Quality Function Deployment (QFD), we could see what engineering requirements we should focus on. We weighted customer's requirements based off what we felt was most important. From there we put a number from 1-9. A " 1 " meant that the engineering requirement was not really relevant to requirement and a " 9 " for very relevant to requirement. With the requirements all weighted, we could see that the two most important engineering requirements we should focus on was the ease of use and weight. The two lowest rated categories were visual appeal and noise level.

At the bottom of the QFD, we have a set of targets we aimed to meet for each of the categories listed above. Along with our targets, we benchmarked previous projects on their performance in each category. Some of the categories were measured with a Yes/No. Yes was used if the previous projects were able to meet the category requirement and No if it was not able too. There is also $\mathrm{a}+, \mathrm{V},-$ system used to rate categories. A " + " means that the project greatly exceeds our desired target. $A$ " V " means that the project can meet our target. A "-" means that the project does not meet our target or cannot meet our target. A "?" meant that weren't able to obtain enough information to rate the project properly.

## Project Management

In the early stages of development, each member of the team was equally involved in all aspects of the project. This included background research, preliminary analysis, and production of conceptual models. Upon choosing the best model to follow through to a final design, each member's focus shifted to different tasks in order to accomplish more in the same amount of time. This is described below.

## Brian:

Originally, each member was to design a portion of the hand, Brian's being the palm. However, once it was realized that a shield was necessary to power all of the servos, his attention shifted to designing and building a custom shield. Brian was also in charge of developing the master program that would be programmed onto the Arduino.

## Colby:

Colby was initially in charge of designing the fingers and the base connection to the hand. He would later continue where Brian left off on designing the palm. This task took a considerable amount of time as Colby made a conscious effort to make the hand appear more realistic.

## Trevor:

Trevor was tasked with designing the thumb. The thumb is the only digit that was simplified by fixing a joint position and yet was to still be used to form all the letters of the alphabet. Trevor was also in charge of making the user_task code which is used by the master program, as well as the code used to tune the servo s/finger positions.

Though the tasks were divided, all the members of our group were able to assist one another. For example, the programming reached a point where nothing could be verified until the hand was made, so the team collaborated on the design. All of the members also took part in part procurement, machining, and assembling of the project.

A summary of the major tasks can be seen in the table below, as well as a list of milestones which follow. For a visual aide, see the Gantt chart in the appendix.

Table 1. Group/Individual Tasks

| Tasks | Brian | Colby | Trevor |
| :--- | :---: | :---: | :---: |
| Base design |  | x |  |
| Hand design | x | x | x |
| Machining/Rapid prototyping | x | x | x |
| Mechatronics | x |  | x |
| Progress documentation |  | x | x |
| Shield design | x |  |  |
| Testing/Evaluating | x | x | x |

## Milestones

1. Conceptual design review
2. Critical Design Review
3. Working finger model, open/close motion
4. Working thumb model, open/close/rotate
5. Project Update
6. Computer-to-hand recognition of alphabet
7. Palm and back of hand casing, hand assembled
8. Wrist movement and arm completed
9. Adjustable orientation/detachable base assembled
10. Final SKERI meeting
11. Design Expo
12. Industry Expo for SKERI

December $5^{\text {th }} 2011$
February $3^{\text {rd }} 2012$
February $20^{\text {th }} 2012$
March $26^{\text {th }} 2012$
March $26^{\text {th }} 2012$
April $19^{\text {th }} 2012$
April 30 ${ }^{\text {th }} 2012$
May $15^{\text {th }} 2012$
May $15^{\text {th }} 2012$
May $21^{\text {st }} 2012$
May $31^{\text {st }} 2012$
June $28^{\text {th }} 2012$

## Design Approach

Our project is somewhat unusual in that each component of the hand can be developed largely independent of the others. For example, the method by which we curl the individual fingers has little to do with the type of actuator we use, because almost all of our concepts for the curl can be driven by any type of spinning shaft. The one exception to this is the idea of linear actuators in the fingers that act directly on the joint. With this in mind, we assumed a mostly bottom-up design process in which we made decision matrices for each component. We split the hand into three major systems: the wrist, the fingers, and the thumb. To further divide the components, each of these groups has various subsystems that need to be decided on.

After brainstorming many different ideas, we weighed the pros and cons of each idea, allowing us to eliminate all but a few core concepts. All of these concepts then went into a group of decision matrices. As an example, four matrices were made for the fingers: the actuators, the drive mechanism, the curl mechanism, and the range of movement. Some of the matrices may seem repetitive, such as the drive mechanism for the fingers and for the thumb, but the weights of the criteria differ, which changes the output. After building our matrices, we can then look at what combinations will work the best. Each individual component will be tested and prototyped, and then the whole thing will be brought together.

## Design Development

## Unused Concepts:

## Linear Actuators

This design that we considered would use linear actuators to bend the finger at each joint. This idea would feasible with a PiezoWaveR motor. This linear actuator is only 24 mm long, 9.7 mm wide and 4.4 mm high. This makes it an ideal size to place into the inside the fingers, while keeping the fingers a small size. One thing we would need to look into would be the max weight of the finger segment. In figure 2 , it is a picture of a LegoR pneumatic hand. This picture was to show how the fingers would be moved using linear actuation. In this design, we would be using the PiezoWave Motor instead of the pneumatics in the picture. The problem with this concept was that the PiezoWaveR only has a dynamic force of 0.1 Newtons, which is not a lot. Also getting linear actuators that are small enough to fit inside the fingers are very expensive.


Figure 6. PiezoWave ${ }^{\circledR}$ motor (PiezoMotor.com)


Figure 7. Pneumatic hand using the concept of linear actuation (YouTube.com)

## Flexible Tubing

Our fourth concept is the simplest design. It would use a rubber or flexible material along with one pull string. There are grooves cut at where joints would be to allow the finger to bend properly. Linear springs could be inserted at the grooves to provide for a faster return to neutral position. The major problem with this design is that it would be hard to control the movement of the fingers because the slots would require precise material removal.


Figure 8. Hand with triangular cuts shown


Figure 9. Curled Hand

## Used Concepts:

## Digit Design

Our first model was inspired by DEXTER. We tried to recreate the mechanism of wrapping cables around joints and pulling on them like puppet strings. This model proved the concept, but after more testing we found that just a pulley method to be insufficient for our needs.


Figure 10. Dexter pulley system Top left: bent finger Top right: straight finger Bottom: Finger with pulley system and platform

Our next design used pulleys to curl the finger. The pulleys would have a 1:1 ratio so that the second knuckle will rotate with the same angle as the first. This was been incorporated into our final design to bend the distal knuckle with the medial knuckle. This eliminates many components as there is no need for a drive or return cable at the knuckle.


Figure 11. Pulley curl system Top: curled finger Bottom: straight finger

This mock-up displays many concepts, while also serving as a test platform. It will allow us to test many different components such as the cables, motors, controller board, springs and finger segments.


Figure 12. Test platform with bent finger
Inspired by the cable / housing system used on bicycles, we chose to use Bowden Cables for power transmission from the motors to the fingers, thumb and wrist. Using this type of system allows us to mount the motors in the forearm of the device, which will avoid considerable size constraints in the palm. With the housing passing through the wrist, the hand will be able to twist relative to the forearm without interrupting the control of the digits. Another advantage is the ease of adjustment for the cable length. As on bicycles, we can incorporate a threaded barrel adjuster that will lengthen or shorten the housing length, effectively collecting or releasing cable. Small Bowden Cable systems are sold for use in robotics such as remote controlled helicopters. We also have the option of buying the cable (or wire rope) individually and matching it with appropriately sized tubing. This would require some trial and error.


Figure 13. Bowden cable system

By incorporating torsion springs directly into the knuckles, we avoid the need for return cables. This cuts our number of cables in half and greatly simplifies the design.


Figure 14. Knuckle return springs

Initially, we thought that we would use pulleys to rotate the knuckles, but after prototyping, a better method was found. In this design the cable will be connected to a rod near the bottom of the finger that will provide a moment arm around the joint. It allows a much larger moment arm than a pulley would, and doesn't require any tedious installation. Another advantage is that the shaft for the knuckle does not need to be fixed to the desired phalange, again simplifying design.


Figure 15. Finger drive method

## Actuation:

There were many factors to consider when choosing an actuator: price, stall torque, extra circuitry, and available resources. The two best types of actuation devices for our design were hobby micro servos or stepper motors. In the end, we went with hobby micro servos. Other actuation devices like solenoids, DC brushless motors, and pneumatics were considered.


Figure 16. Rotary solenoid
(http://image.made-in-china.com/2f0j00TvgEwlkdnebz/Komatsu-Spare-Parts-Rotary-Solenoid-20Y-60-11713-.jpg)
Rotary solenoids can produce high torque while still being small. They are very fast and move in specified angles. They are also cheaper than dc brushless motors and do not require a controller. The disadvantage to rotary solenoids is that they produce too much heat. Solenoids produce motion through induction and convert current into heat making solenoids very inefficient as power is wasted. The heat generated could easily go over our desired limit. An exhaust fan could be used to get rid of the heat from inside the hand, but this would focus large amounts of heat and be prone to failure. Solenoids were not chosen because they produce large amounts of heat and are not very efficient.


Figure 17. Maxon Dc brushless motor with encoder
(http://maxonmotorusa.files.wordpress.com/2011/10/ec16_new-sterilizable-and-non-ster.jpg)
DC brushless motors are very durable and have a long life time. They are very efficient, which allows the hand to operate longer with a battery pack. The biggest DC brushless motors are expensive and much more expensive when they are very small. They also require motor controllers, which is extra cost, and a software controller to get exact positioning for the motor. DC brushless motors were not chosen because the high initial cost and the need of more complicated software and hardware to control them.


Figure 18. Tolomatic pneumatic cylinders
(http://www.motioncontrolproducts.com/pageimages/erdactuator_large.png)
Pneumatics was considered for a more comprehensive development, even though the sponsor made it clear that this method was not desirable. The benefit of pneumatics and hydraulics is that they could be small enough to fit inside the finger and actuate each section. But small pneumatics and hydraulics are expensive. Pneumatics and hydraulics also require controllers and a
fluid supply, which adds to the cost and weight of the device. Pneumatics was not chosen at the request of the sponsor.


Figure 19. Stepper motor
(http://www.designworldonline.com/uploads/ImageGallery/step-motor.jpg)
Stepper motors were a good candidate for actuating the hand. They are very accurate due to the fact that a full rotation is divided into many steps, like an encoder. There would be no need to write a software controller as stepper motors operate in open control loop. This allows for us to just send a voltage and the stepper would rotate to desired position. The downsides to stepper motors are that they tend to be heavy and can lose efficiency if any of the steps are skipped during a rotation. It is sometimes necessary for stepper motors to have additional hardware in the form of motor controller. Alone, these controllers would add approximately $\$ 120$ to the cost of the project, bringing the total cost of the motors to half of our desired budget.


Figure 20. Hitec HS-625MG Hobby Servo used in project

Hobby micro servos were our final selection. Hobby servos are small, cheap, and can provide large amounts of torque. Since hobby servos have a built in gear train, a micro servo can easily provide over 30 ounce-in of torque. Hobby micro servos cost about 13-15 dollars each, so our cost would only be around $\$ 150$. This makes servos one of the cheapest actuation devices. The biggest advantage to going with hobby servos is that they do not require an auxiliary position controller, which greatly saves cost. Servos have a built in position controller. This makes coding to control the servos very simple. Servos are also very light weight. Ten servos would weigh no more than 100 grams. The disadvantages of servos are that they do not have long life and may need to be replaced frequently. The main reason we chose servos were that they are cheap, light, and very compact.

## Microcontroller:

With 10 servos, we need 10 digital pins. This means we need at least ten I/O pins. We have two options for our circuit board. One option is to design a custom board; we would have a circuit board that does only what we need and doesn't have extra unnecessary features. The other option would be to buy a premade board. Designing a custom board may actually be a cheaper alternative. With a custom board we can choose a microprocessor that has enough pins for our application and a few extra for expandability and unplanned additions. Going this route would require a large amount of time. Designing the board would take 2-3 days. After designing the board, the design would need to be sent to a board making company. The board would take 1-2 weeks to be made. After finishing the board, we would need to spend some time to make sure the board is working properly before we can even start programming.

We decided to buy a premade board. We chose to work with the Arduino platform. The Arduino Uno is the most common model, with 14 digital pins and 6 analog pins. The other models like the Arduino Mega have more pins than we require for our application and are more expensive. Though, they could be easily swapped in place of the Uno for expandability in the future. The price of the Arduino Uno is around $\$ 20-\$ 30$. Arduino also has a large amount of $\mathrm{C}++$ libraries for servomotors. By choosing to go with the Arduino, it allowed us to spend more time on building and testing our hand.


Figure 21. Arduino Uno board
Since we could not control and power up all 11 servos with the Arduino, we needed a servo shield that could power the board while the Arduino could control them. All available servo shields could at most control 2-4 servos. We needed to control 11 servos. We decided to design a servo
shield. We used Eagle PCB to draw the schematic and the board layout. With the board layout done, we submitted it to a PCB manufacturer, Dorkbot. Their website is http://dorkbotpdx.org/wiki/pcb order.


Figure 22. Left PCB without components. Right PCB with all components
For our application, each servo needed to be provided with 6 V and 500 mA of current to run at full speed. This means we need a power supply or AC adapter that can supply our system with 6 V and 5.5 A . We decided that 4A was enough for the system since servos require 500 mA only when it is moving and does not require the full 500 mA when holding a position. When looking for AC adapters, 6V 4A AC adapters were not common, and were hard to find. So we found a 12 V 4 A AC adapter. This AC adapter is much more common. So for our board we had to look for a $2.5 \mathrm{mmID} \times 5 \mathrm{mmOD}$ power plug. From there, we had to regulate the 12 V down to 6 V so that the servos could use them. When looking for way to regulate high current, we had a choice between going with a high current voltage regulator or a two transistor circuit. The high current voltage regulators that we found had a thermal resistance of $3^{\circ} \mathrm{C} / \mathrm{W}$. If we go the two transistor route, the PNP transistor taking all the current would only have a thermal resistance of $2^{\circ} \mathrm{C} / \mathrm{W}$. This would make keeping the transistor from overheating and blowing up easier.


Figure 23. PnP transistor and voltage regulator setup to allow for high current voltage regulation
We chose a BDX54C for our PNP transistor and a LM317T for the voltage regulator. The PNP transistor acts as a pass transistor allowing all the current to pass through it while the voltage regulator regulates the voltage. The R3 resistor is there to allow some current to go to the voltage regulator so that it will regulate properly. Using the circuit above, we use a ratio of R1 and R 2 to regulator 12 V down to around 6 V . The resistors we used were 230 and 820 , which were available in our mechatronics room. This gave us an output voltage of 5.74 V . With the main part of our circuit done, it was just connecting pins to allow us to put pin headers to make attaching servos to the board easier. The servos connected to pins 2-12 of the Arduino board. Pin 13 has a 5 k pull down resistor attached to it to allow us to use a button to trigger a demo mode in the program. Another button is attached to the reset and ground pin to allow the user to reset the Arduino from outside the box.

When the board was completely assembled and tested, we noticed that the PNP would heat up too much and that the heat sink for it was not enough. We tried to fix that by doing two things. First we added a fan that would blow directly at the heat sink. Second we changed from a 12 V 4 A AC adapters to a 9V 4A one. This decreases the power the PNP transistor needs to dissipate by 12 W , which is about $25^{\circ} \mathrm{C}$ decrease in the temperature increase. But we still have a heat issue. The transistor's junction temperature is $150^{\circ} \mathrm{C}$. With the fan blowing and using a 9V 4A AC adapter, the transistor can get up to $95^{\circ} \mathrm{C}$ theoretically. With our infrared heat gun, we were able to see around how high the temperature got. The results of this testing can be seen in the testing section of the report. We are still working on a way to use our larger heat sink. We could not attach it directly to the transistor because of space restrictions. Before when we were testing with the board outside of the case, we had the larger heat sink attached. With the large
heat sink attached, we could run for a much longer time without worrying too much about overheating.

## Programming:

The coding for the project is done in $\mathrm{C}++$, one of the most common programming languages available. It is written in a very modular fashion, which allows for the program to be modified by others. If there is a need to change the actuation code or user interface, it can be easily done without affecting the overall code. With a computer, it uses a terminal program to talk with the Arduino. The user is able to type in sentences or words into the textbox, or have the hand perform real time movements using the real time box. The Arduino manufacturers include many libraries in C++ which is very convenient for us. One of the library files is for servomotors which we used to actuate the servos.

The main file consists of a constructor and an infinite loop, which runs the program using cooperative multi-tasking, which makes the runtime more efficient. There are two classes that are run inside the main file, master_task and user_task. The main file will be supported by other files which it will use to run, including a user class which takes user input from the computer, and master class that overlooks everything.

The user_task is in charge of getting user input. User will only accept letters and instruction keys, if any other key is pressed, nothing will happen. The instructions are: " 1 " to attach servos, " 0 " to detach servos, "[space]" to delay between words, "-" or " " to increase delay between letters or decrease spelling speed, and " + " or " $=$ " to decrease delay between letters or increase spelling speed.

User_task has 3 states. The first state waits for a character to be entered. After user gets a character, it goes to state 2 . In state 2 , it checks to see if the character is a valid input. If it is a valid input it will set valid to true, which tells master that a valid character has been gotten. After state 2, user stays in state 3 until master is done and is ready to get a new character.

The master_task class is the overseer of this entire program. It determines what to do when something is pressed. After the input of each letter from the user_task, master_task will get the servo positions that correspond with input letter by referencing a large look-up table. The lookup table will consist of an integer array of servo positions from $0-180^{\circ}$. These positions are determined through trial and error during the testing stages of the project. There are \#defines for different angles for each finger. This makes it easier to see if the look up table is correct and makes tuning the hand a much simpler job. Instead of having to go to each letter and changing the servo angle, it
can be done by changing the servo angle in the \#define. Another part of the master is to make sure that the fingers are not interfering with each other when moving.

There are 8 states to master. The first state is the idle state where it waits until user has gotten a letter. The gotten letter will be from 0-30 and put into a variable called "letter". 0-25 for az, 26 for increasing spelling speed, 27 for decreasing spelling speed, 28 for spacebar, 29 for detaching servos, and 30 for attaching servos. When attaching the servos, the hand will go back to neutral position. It will then move to state 2.

In state 2, master determines if the inputted character is a letter or instruction. If it is a letter, it will move to state $3,4,5$, or 6 . The next state is determined by the location of the thumb and it next destination. If it is an instruction, it will do the instruction than go back to state 1.

State 3 is for when the thumb is under the fingers and the next letter also has the thumb under the fingers. In this state, the fingers will move to neutral position, then the thumb will move to its next position, then the fingers will move to their next positions.

State 4 is for when the thumb is over the fingers and the next letter has the thumb under the fingers. In this state, the thumb will move to neutral position, then the fingers will move to neutral position, then the thumb will move to its next position, then the fingers will move to their next positions.

State 5 is for when the thumb is under the fingers and the next letter has the thumb over the fingers. In this state, the fingers will move to neutral position, then the thumb will move to neutral position, then the fingers will move to their next positions, then the thumb will move to its next position.

State 6 is for when the thumb is over the fingers and the next letter also has the thumb over the fingers. In this state, the thumb will move to neutral position, then the fingers will move to their next positions, then the thumb will move to its next position. When state $3,4,5$, or 6 are done moving the fingers, they automatically go to state 7.

In state 7, it delays. This delay can be increased or decrease. After the delay, it determines if master is in demo mode or regular typing mode. If it is in demo mode, it goes to state 8 or else it will return to state 1 to wait for the next input. In state 8 , it first determines if this is the first time running through demo. If it is, master sets "letter" to zero to spell the letter A and increments "letter" every time state 8 is entered to spell the next letter in the alphabet. Once "letter" has reached 26 , it means that the hand has spelled all 26 letters, which also means the demo is over.

Master will then detach the servos and delay so the PNP transistor can cool down. After 20 seconds, the hand will reattach the servo and go to state 1 so it is available to be used again.

We have also included a tuning program for the fingers. This tuning program allows the user to adjust the finger locations in case of slack in the cable or to change the accent of the hand. The servos start at a default angle of $140^{\circ}$. In the tuning program, you press " 1 " to decrease the angle and " 2 " is to increase the angle of the servo that controls the knuckle movement. You press " 3 " to decrease the angle and " 4 " to increase the angle of the servo that controls the medial joint. The program only allows the tuning to go from $20-170^{\circ}$. This is to prevent the user from going to $180^{\circ}$ or $0^{\circ}$, where the servo PWM messes up and tries to go beyond its limit. That will cause the servo to fry. When you want to change fingers to tune, you press " + " or " $=$ " to go to the next finger, and "-"or "_" to go back to the previous finger. The order that the tuning goes by is thumb, index finger, middle finger, ring finger, pinky, and wrist. If you press the next finger button when it is at wrist, it will loop back to the thumb, and if you press the previous finger button when it is at thumb, it will loop to wrist. You can also detach the servos with the " $s$ " key, and attach the servos with the " g " key.

## Hand Size:

The size of the hand needed to be comparable to that of an adult. To do this, data was obtained from the 1988 Hand Anthropometry of U.S. Army Personnel, and has been summarized in inches in the tables below. The data corresponds to the average measurements listed of women, along with their standard deviations. The dimensioning of the fingerspelling hand will closely adhere to the average values, and will be adjusted accordingly, within one standard deviation, to account for all the interior components. This didn't present too much of a problem as the majority of the larger components are located elsewhere in the design.

Table 2. Relevant digit measurements from 1988 Anthropometric study

|  | Digit 1 | $\begin{gathered} +/- \\ \text { (inches) } \end{gathered}$ | Digit 2 |  | Digit 3 |  | Digit 4 |  | Digit 5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thumb |  | Index |  | Middle |  | Ring |  | Pinky |  |
| Length | 2.5 | 0.19 | 2.74 | 0.18 | 3.04 | 0.2 | 2.84 | 0.2 | 2.3 | 0.18 |
| to wrist | 4.95 | 0.34 | 6.69 | 0.37 | 7.02 | 0.39 | 6.65 | 0.38 | 5.73 | 0.37 |
| Breadth | 0.81 | 0.05 | 0.78 | 0.05 | 0.76 | 0.05 | 0.72 | 0.05 | 0.65 | 0.04 |
| circumference | 2.48 | 0.1 | 2.41 | 0.08 | 2.41 | 0.07 | 2.26 | 0.08 | 1.99 | 0.07 |
| Distal | 1.21 | 0.1 | 1 | 0.08 | 1 | 0.03 | 1.03 | 0.09 | 0.93 | 0.08 |
| Medial | -- | -- | 0.83 | 0.09 | 0.99 | 0.11 | 0.9 | 0.1 | 0.64 | 0.09 |
| proximal | 0.76 | 0.11 | 2.22 | 0.21 | 1.96 | 0.17 | 1.91 | 0.13 | 1.49 | 0.12 |

Table 3. Relevant hand/forearm measurements from 1988 Anthropometric study

|  | Inches | +/- |
| :--- | :---: | :---: |
| hand length | 7.11 | 0.39 |
| hand circumference | 7.34 | 0.34 |
| palm length | 3.97 | 0.22 |
| hand breadth | 3.13 | 0.15 |
| wrist breadth | 2.24 | 0.14 |
| wrist circumference | 5.96 | 0.27 |
| wrist center-of-grip | 2.61 | 0.19 |
| elbow to hand | 17.46 | 0.93 |
| elbow to wrist | 10.35 | 0.61 |
| forearm circumference | 10 | 0.59 |

## Final Design

## Motor Housing:

To hold components such as the motors and the microcontroller, a rectangular case was made from 0.220 inch clear acrylic sheets. Acrylic was chosen to display the inner workings of the motors, as well as for its workability with the laser cutting machine on campus. See the manufacturing section for a further description of this process.

The case is sized so that an average-sized person will be able to rest their elbow on the table while feeling the hand, but the case also allows for other orientations. If preferred, the case can be turned around and the user's wrist can rest on the case. Also, the case can be turned onto its side to read the hand in a horizontal position.

## Wrist Movement:

The wrist mechanism allowed for major simplifications over previous hands. Many of the letters of the alphabet are formed by lowering a vertical wrist into a more horizontal position. Also, " J " and " Z " are considered dynamic letters and are formed with scoop and wiggle of the wrist, respectively. Because the wrist has to support the entire hand, it has been a weak spot in many past designs, with the tilt causing the most problems. Tilting the hand to the side applies a large moment to the wrist area, while also throwing off the balance of the entire device. For these reasons, we chose to design our wrist to spin only about a vertical axis by $180^{\circ}$.

This twist about the vertical axis provides us with a degree of freedom that is underutilized in the common ASL alphabet. With the presumption that the deaf-blind are adaptable enough to learn variations on the alphabet, the single twist of the wrist allows for 26 distinct movements and has the ability to replace the tilt of the wrist in letters such as " G " and " H ". This can be thought of as the hands "accent". Initially, an explanation of the wrist movement and the affected letters should be created using the most recognizable letters for the deaf-blind user.

The hand is supported by an aluminum shaft that was machined into the desired shape and size. The most significant aspect of the wrist shaft is the " D " shaped ends, which sink in to hand on one end, and the wrist servo attachment on the other. This shape acts as a key in the shaft to transfer rotational power. The hand is also screwed onto the shaft, but this is simply to stop it from falling off. Most of the torque should be transmitted through the " D " shape and not through shear in the screw. The lower end of the shaft is not screwed to the servo because its position is fixed by casing for the mechanism. The shaft was designed with a larger diameter section in the middle that sits between 2 flanged, sealed ball bearings. Not only does this hold the bearings into their position in the case, but also holds the wrist shaft in after the top to the case has been screwed in. The 2 bearing, stepped shaft design removes all axial force from the servo, which is not designed to such axial loads.

Problems: To fully utilize the movement of the wrist, it needs to turn by a complete $180^{\circ}$. Unfortunately, the servo that is turning the wrist cannot be driven a full $180^{\circ}$ without the likelihood of damage, so the wrist is restricted to move approximately $150^{\circ}$. For future designs, it is recommended to choose a servo that is designed to move more that the common $180^{\circ}$, such as a "sail winch" servo.

## Actuation:

In actuating the movements of the hand, our design mimics the human body in that the "muscles", or servos in our case, are housed remotely and "tendons" transfer mechanical power to the moving parts. A great example of this is readily seen in the way that bicycle brakes and derailleurs are actuated. The system consists of a length of housing that is maintained as some fixed length while flexible cable is allowed to slide through. The cable is fixed to the actuator on one end, and the mechanism on the other. When building the concept models, bicycle cable housing was used but the diameter was far too large for the application inside the hand, considering that the hand needs 11 independent lengths of these housings.

After experimenting with different cables and housings, the products chosen for the final design were found at the local hobby store. The housings are antennae coverings for remote controlled cars, and the cable is nylon-coated stainless steel cable used for actuating the flaps of remote controlled airplanes. The cables are crimped using common bead wire crimps that can be found at most arts and crafts stores. The crimps should be large enough that the cable can loop and pass twice through the crimp.

Problems: The $1 / 8^{\text {th }}$ inch housing is not flexible enough to allow for totally fluid movement of the wrist. The servo used to twist the wrist is strong enough to overcome this binding of the cable housings, but future designs should strive to find a type of cable housing with more flexibility.

When crimping the nylon-coated cable, the crimps have the tendency to strip the coating from the cable. When this happens, the cable will lose its tension and the exposed metal strands can be dangerous.

## Finger Mechanism:

By using springs to return the fingers to a straight position, there is only one actuation cable per joint, and it is simply anchored to the phalange which is desired to move. Past designs had problems with trying to use a continuous cable loop from the motor to the finger that would bend and straighten the finger. The use of springs greatly simplifies this system and allows the hand to be in a natural position even when it is not hooked up to a motor. The difficulty in the design chosen for the fingers is getting enough of a moment arm on the pivot. Because the fingers are so small, there is not much room to pass the cables by the pivot, so they end up with a small moment arm.

The distal and medial phalanges are kinematically tied, and the distal will move any time that the medial moves. This not only mimics the way that a human finger moves, but also eliminates the need for a third actuator on each finger. The movement is achieved by using a short cable anchored to the proximal phalange on one side and the distal phalange on the other and uses a cross pulley mechanism.

## Thumb Mechanism:

The thumb has two degrees of freedom, with the outermost joint fixed. With the tip of the thumb bent at a fixed angle, the hand still makes sufficient and intelligible movements and avoids the need for tip actuation. The base of the thumb has the ability to rotate on an axis in plane with the palm and perpendicular to the wrist. This allows for the necessary movements to form letters such as " $O$ ". Due to the positioning of this system, it made more sense to run a true "pull-pull" system as opposed to a single pull with a spring return such as with the fingers. To make the thumb sweep across the palm, the same method was used as with the fingers, but to achieve the letters such as " L ", the thumb needs to sweep $90^{\circ}$ from vertical in both directions. Where the fingers use $180^{\circ}$ springs that are bent to $90^{\circ}$, the thumb uses a $270^{\circ}$ spring that rotates to $90^{\circ}$. This allows the thumb to be held out away from the hand in its neutral position, yet still bend all the way into the palm when actuated.

## Springs:

Several different size springs were used in the hand. Initial calculations found that a spring constant of approximately $1 \mathrm{in}-\mathrm{lb}$ would be sufficient to hold the fingers in a straight position even if the hand was horizontal and provide the user with enough feedback to let the hand move. With the extremely light weight of the final design, and the small size of the fingers, it was determined that each joint would have a different spring constant, descending from 1 lb -in at the base knuckle, to $1 / 4$ lb -in at the tip joint. This is because of the larger moment on the base knuckle. Unfortunately, there is a slight problem with the spring at the base knuckle getting squeezed at a full bend, which causes the finger to stick a little bit. This problem has not caused much trouble because the base knuckle almost never needs to bend all the way to create our shapes.

To reduce slop in the joints, the springs were plastically deformed to rest neutrally at an angle of a little more than $180^{\circ}$. Although they are considered to be $180^{\circ}$ springs by the manufacturer, they all rest at some angle slightly less than that. This was an easy solution and made more a more solid hand design.

## Manufacturing

The manufacturing of the hand was done largely by the 3D printer (ObJet 250) at Cal Poly. This machine has the ability to take a solid model file from a program such as SolidWorks and create that model from a gel called EDEN FullCure 720. The process is fast and is referred to as "rapid prototyping" for obvious reasons. For example, each finger took close to two and a half hours to print, which is much quicker than many other manufacturing methods would have been. The fingers, thumb, palm, and hand were all made using this process. A few of the material properties are listed in Table 2, while the rest can be found in the appendix.

Table 4. Partial property list of FullCure 720

| Objet FullCure $\mathbf{7 2 0}$ Eden |  |  |
| :--- | ---: | :--- |
| Tensile Strength | 8744 | psi |
| Density | 0.0426 | $\mathrm{lb} / \mathrm{in} \wedge 3$ |
| Modulus of Elasticity | 416150 | psi |
| Hardness | 81 | M |

To be printed, the SolidWorks part was saved as a .STL file which could be read by the rapid prototyping software. The parts were then positioned on a virtual tray. This part of the process took some time because the orientation of the part determined how much filler material would need to be used. Every layer put down by the printer has to lay on top of another layer, so to create voids in the part the printer would use the filler, or "support" material as a base for the next layer. Our final print ended up using about 300 g of FullCure and 250 g of support material. Small modifications were made to the rapid prototyped parts with a drill and a Dremel tool to provide more clearance for moving parts.

The case built from the sheets of acrylic was cut from 18 " $\times 24$ " sheets of acrylic that were cut into pieces using the laser cutter in the Mustang 60 machine shop at Cal Poly. For the most part, these pieces were good to go as soon as they left the machine, but some pieces had to have their edges sanded down to provide for a more flush perpendicular fit. This is because the laser tends to create a slight slope to the edge of the sheet when it cuts through. Any modifications to the acrylic proved to be difficult, and the second version of the case that was created was done so with less need for modification. Drilling through the acrylic is doable but tricky. The material will melt and has a tendency to build up on the drill bit and cause problems for the next hole to be drilled. This can be somewhat remedied by passing the clogged drill bit through a block of wood. This will re-melt the
material and push it to the un-bladed portion of the drill bit, where it can remain or be pulled off of the end. Another tactic is to use pliers to break off the hardened acrylic, but this method is less consistent in its success. A 2-56 tap was used to make threaded holes for the servos to mount into.

Most of the case was assembles using Weld-On \#3 Acrylic solvent cement. Unable to find this adhesive at any hardware store, we eventually found it at a glass store. This adhesive works in much the same way as welding materials together, because it liquefies the material and forms a strong bond as long as the surfaces are flush. Care must be taken when working with the adhesive because any of the liquid that drops will mar the acrylic surface. Overall the adhesive worked well and produced clean and strong junctions.

Some components of the case need to be removable such as the top bank of servos. For this we used metal L-brackets to hold things together temporarily. JB Weld was used to fix nuts to the back of the brackets so that the screws could be driven directly into the case without needing access to the inside. On the first version of the case, all 4 sides were permanently fixed with adhesive. This made it very difficult to get down inside to the case, so the front wall of the second case was made to be removable, greatly easing the installation of all the components.

Although this project required relatively little time in the machine shop, some parts were still manufactured using traditional machines such as the lathe and mill. The wrist shaft required the most machining. First the shaft was cut to length using the chop-saw with a special blade for cutting aluminum, and then a lathe was used to face the ends and turn the entire length enough to give it a nice finish. While leaving the center section untouched, both ends were turned down to a diameter small enough to pass through the bearings. Then the mill was used to create the " $D$ " flats. Finally the wrist mount hole was drilled and trapped. Somewhat more tricky to machine was the pins for the finger joints. Each of these had to be grooved to allow for the e-clips to clip to the side. A custom grooving tool was made from an old broken parting tool to make the grooves the right size and depth.

In the future, this hand could be made through injection molding. This way, the hand can be cheap and affordable as parts will only cost cents to make. But to use injection molding, the demand for the hand would have to be in the hundreds of thousands. Another solution is to the hand made with CNC. This solution is more reasonable for production numbers in the hundreds. The last solution is to have the design and 3d drawings open to the public, so this hand could be personally made through a rapid prototyping company if this hand is not available commercially.

Using a computer numerical control (CNC) machine is another possible way to create our parts. CNC can make the parts with high tolerances. We would have blocks of plastic and place it in
the machine. Then based off our computer aided design (CAD) files, it would drill and mill a part for us. We choose not to go with this process because the machine shop on campus was closed due to budget cuts. This makes it inconvenient to make parts when we need them. But this is a viable option for small production amounts of the hand.

## Testing

The testing that has been done so far consists of our conceptual models. We have learned a great deal through tinkering with items easily obtained from the local hobby store. Because of this, we felt much more confident in our final design than if everything had just been done on paper. We built a test stand that initially was able to hold a finger or thumb. It later expanded to hold the entire hand and came into much use in the time leading to our final design. Various servos were set up and tested on this platform.


Figure 24. Strength test. Cables tied to weights at one end and tied to components on the other end
Strength tests were performed on the cables and fingers. For the cables, we had two, a weaker cable and our current cable. To test the cables, we tied weights at one end and lifted the weights with the cable. For the weaker cable, it snapped at 10 lbs . Our current cables snapped at 30lbs. A similar thing was done for the joints in the finger. We tied weights at one end of the cable and tied the other end to a particular joint we wanted to test. All rapid prototype parts were able to withstand more force than the cable. Through all this strength testing, we could conclude that the first thing to fail in our system would be the cables in normal use.


Figure 25. Finger in fatigue test setup hitting the bump switch
Fatigue tests were performed on the fingers, servos, and cables. The comprehensive test had the assembled prototype monitored while form the letters of the alphabet continuously in a loop for several hours or until a component breaks. The fingers went through a similar test in which they looped between fully open and fully closed while hitting a bump switch counter for every repetition. This test was only done once and it was done using the weaker cables. The weaker cable was able to last 2700 runs. If the weaker cables were able to perform that well, we expect the current cables to last at least 3 times longer.

One of our test plans involved the testing of the forces created by the digit. While the digit was in the test stand, a linear spring scale was placed at a measured distance from the joint in question. Measuring the forces for the purpose of satisfying our requirements, as well as check the torque of the motors and springs against the manufacturers' specifications. In particular, we intended to find out how much external force is necessary to move the hand out of position, and the grip strength of the hand in order to make sure the hand grip would not crush the user's hands. At the same time, we could make sure that the hand would still be strong enough to overcome the weight of the user's hands in order to form letters. A multimeter was simultaneously monitoring the current drawn by the motor. This test was never fully done. When we attempted, the cables snapped before we could get a reading, and we ran this test again with the stronger cables. We did hook up a multimeter to see how much current the servos drew when actuating. The servos drew about $500-800 \mathrm{~mA}$ when moving and used $300-400 \mathrm{~mA}$ when holding the finger in full curl position.

After examining previous models that Cal Poly students have produced, we noticed that many servo horns had sheared, rendering many components useless. Those projects were done using the standard nylon horns that came with the servos. An alternative to nylon horns is to use aluminum servo hubs. A fatigue test that will be performed simultaneously with the finger tests, as the servo hub will be pulling the cable back and forth. This test was never done due to time restraints. We used the stock nylon horns instead of getting aluminum horns. The stock nylon horns proved to be strong enough for the application as not one has failed in all our testing.


Figure 26. Infrared heat gun used to check temperature of different components
In addition to fatigue tests, we also planned to perform heat tests. Heat will be generated by the electronic components. Each servo will require at least 400 mA of current to produce its rated torque, and any leftover current will dissipate into heat. Therefore we used an infrared thermometer to monitor the hand. Ideally, the highest temperature wouldn't be much greater than $70^{\circ} \mathrm{F}$, which is considered comfortable to human touch. Since the board is enclosed in the case, there isn't a likely chance of someone getting burned by it.

The biggest problem that we encountered with our design was overheating of one of our transistors. This problem is described in detail in the Electrical Design section of the report. The results of our heat testing showed a remarkable drop in the temperature of the transistor when using the 9 V power supply (circles) instead of the 12 V power supply (triangles). It was encouraging to see a physical effect of our theoretical predictions about heat generation. In the test, there are 3 different states that the servos can be in. When attached (green), the controller is holding the
servos in a particular position but they are unmoving. When detached (yellow), the controller is not sending a signal to the servos but it is plugged in to the power supply. The active state (red) is when letters are being formed every 2 seconds and therefore the servos are moving often.


Figure 27. Compiled transistor temperature readings of heat tests
measure decibels, so we intend to compare the noise relative to other common devices or appliances. Ideally, the hand will produce less than 80 dB , which is the same amount of noise produced by a telephone dial tone. The hand does not get very loud. The hand makes the loudest noise when moving to position and makes a small humming noise when holding positions. Overall the hand is not that noisy and the sponsors had no comments on the noise.

When the time comes where we have a complete working prototype, it'd be used to interact with people in the deaf-blind community to test the readability of the hand-shapes. We had hoped to perform this testing well before the final report was due in order to make the hand positions as accurate as possible. This test was never done. We could never get in touch with someone in the deaf-blind community or someone who uses fingerspelling on a daily basis. Hopefully at the RESNA conference, feedback on the letters and the hand will be relayed back to us.

## Cost

## Rapid Prototyping:

For rapid prototyping, service providers will charge anywhere between five to ten dollars per cubic inch of the FullCure 720 material. However, the printing software used metric measurements and so for convenience, we determined the material cost using the FullCure density of $1.189 \mathrm{~g} / \mathrm{cm}^{3}$ and its common rate of $\$ 0.50 / \mathrm{cm}^{3}$. In addition to that, providers will also charge operating fees which would include the amount of electricity used and labor for cleaning the parts. As of 2011, the average cost of electricity for a medium sized company was about $\$ 0.16 / \mathrm{kWh}$. Also, the Objet 250 printer that was used consumes 1.5 kW , so we determined that the rate of electricity to be $\$ 0.24 / \mathrm{hr}$. In Table 3, we provide cost estimation for the material.

Table 5. FullCure 720 cost estimation

|  | Rate | Usage | Cost |  |
| :--- | :--- | :--- | :--- | ---: |
| Material | $\$ 0.50 / \mathrm{cm}^{3}$ | 300 g | $\$$ | 126.16 |
| Electricity | $\$ 0.24 / \mathrm{hr}$ | 15.5 hr | $\$$ | 3.72 |
| Cleaning | $\$ 20 / \mathrm{hr}$ | 0.333 hr | $\$$ | 6.67 |
| Total |  |  | $\$$ | 136.55 |

## Complete Design:

Below is summary of major components and the total cost of producing one unit. A full bill of materials separated by each component can be viewed in the appendix. Note that the cost of the hand differs from the table above due to the addition of parts; springs, washers, pins, etc.

Table 6. Total cost of one unit

| Component | Cost |
| :--- | :---: |
| Hand | $\$ 159.90$ |
| Electronics | $\$ 74.92$ |
| Case | $\$ 81.14$ |
| Servos \& Cables | $\$ 398.75$ |
| Total | $\$ 714.71$ |

## Results \& Conclusion

The two cases that were constructed yielded different results for the hand. The first case was made prior to the final presentation at The Smith-Kettlewell Eye Research Institute. At the time of the presentation, the case was not yet implemented, but it was desired by the sponsors to include more holes for ventilation as there were problems with the heat sink and transistor overheating. Until a replacement power adapter was delivered, work continued on the case in short intervals to keep the electronics moderately cool. When the hand was tuned and fully assembled in the first case, all but the dynamic letters of the alphabet were able to be displayed. There was not enough room for the housing to move freely if the wrist were to turn.

Although, the hand was able to account for double letters without having to return to a neutral position and would wiggle one or several digits depending on what letter was being repeated. This was accomplished due to the logical statements placed in the code. Though, the code didn't account for double letters of " $L$ " and " $\gamma$ " as the logic was based on the position of the thumb; in our code, both letters have the thumb in a zero position, which bypasses the conditional statements looking to see whether the thumb or fingers need to move from the previous letter. The major accomplishment of this design, however, was that it was able to demo the entire alphabet in less than four seconds by pressing a button on the side of the case. From the terminal, the hand was able to take letter input in real time, as well as spell out typed words at speeds specified by the user.

Having come that far, we felt that we would be able to construct a second case that would account for the ventilation and cable housing problem. By that time, we had also received an adapter using less voltage which we hoped would address some of the overheating problems. The end result was that the transistor is still overheating, though not as fast, and also that the speed of forming letters has dropped to being slightly faster than one letter a second. The hand now occasionally twitches when forming consecutive letters. We're not entirely sure what the root cause of this problem is, but it is being looked into.

Looking back at the requirements listed by our sponsor, we feel that we were or would be able to accomplish most of them. With a little more time, the wrist could be programmed to do the dynamic letters, making the hand able to form all the letters of alphabet. We believe the hand is the
smallest and the most lifelike of all the attempts made previously by Cal Poly students. The hand itself exerts no heat, it can be placed in different positions, and is controllable based off user input. While we weren't able to reach the target cost for the project, we feel that the cost is reasonable for something that can't be made cheaper through mass production.

## Future Designs:

If work is to be continued based off this design, here are some of the areas in which it could be improved:

- The first case design didn't allow enough room for the housing to move during the actuation of the wrist. Construction of the $2^{\text {nd }}$ case took longer than expected and prevented the actual implementation of the wrist actuation for dynamic letters.
- Double letter indication for the letters " $L$ " and " $Y$ " isn't included. Though, no word in the English language uses consecutive " $\gamma$ "s.
- The letter " $V$ " was simplified by not splitting the index and middle fingers. However, this may not be considered entirely acceptable.
- A housing that is more flexible and that will not increase friction is needed. The current housing is too still and makes assembling difficult
- Bending of the wrist is necessary to better distinguish between letters.
- A better way to disperse heat from the heat sink is needed. The power adapter was switched from 12 V to 9 V to reduce heat at the cost of letter formation speed.
- A rechargeable battery would make the design more portable.
- The clear case design was intended to show off the electronic actuation of the hand. Transitioning the case to a forearm design would also make the hand more portable.


## Appendix

1. Sources
2. American Manual Alphabet
3. Bill of Materials
4. Quality Function Deployment
5. Decision Matrices
6. Gantt Chart
7. Design Sequence flowchart
8. Other concepts
9. Solid models
10. Rapid Prototyping properties
11. Average electrical costs in California
12. Servo data sheets
13. Servo shield schematics \& layout
14. Servo shield components and data sheets
15. Program state transition diagrams and code
16. Torque calculation code
17. Anthropometric Data Excerpt
18. Hand Shapes
19. Installation tips

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## American Manual Alphabet


http://upload.wikimedia.org/wikipedia/en/thumb/6/6f/Aslfingerspellalpha.png/220pxAslfingerspellalpha.png

## Bill of Materials

| QTY | Part No. | ITEM |  | COST |
| :---: | :---: | :---: | :---: | :---: |
| 20 |  | \#10-24 Fasteners | \$ | 2.00 |
| 20 |  | \#10-24 x 1/2" Phillips pan head machine screw | \$ | 1.80 |
| 4 |  | \#2-56 x 1/4" Phillips pan head machine screw | \$ | 0.36 |
| 10 |  | 1" x 1/2" Zinc Corner Brace | \$ | 9.90 |
| 1 |  | 1/2" Vinyl Bumpers (9 pk) | \$ | 2.99 |
| 1 | MC-21 | Acrylic Sheet (Clear) 18"x24"x.22" | \$ | 18.49 |
| 1 | 8974 K113 | Aluminum 6061 round 3/4 OD, 12" | \$ | 4.27 |
| 10 |  | Black RC Antenna Housing 1/8" OD, 14" | \$ | 4.99 |
| 2 | 6384K363 | Steel Ball Bearing, Flanged for 1/2" Shaft | \$ | 21.34 |
| 1 |  | Weld-On: Acrylic | \$ | 15.00 |
| 1 | JFCT2S1.5G | \#2 Silver plated crimps (100 pk) | \$ | 3.24 |
| 48 |  | 2-56 x 1/2 Flat Phillips Machine Screws | \$ | 1.92 |
| 1 | 8930T16 | 5ft Nylon Coated SS Wire | \$ | 1.60 |
| 3 | \#517 | Du-Bro 2-56 Pull-Pull | \$ | 19.50 |
| 10 |  | Hi-Tec 625MG servo | \$ | 341.00 |
| 1 |  | Hi-Tec 645MG servo | \$ | 31.49 |
| 3 | 445-2868-ND | 10uF capacitor | \$ | 1.86 |
| 1 | CP-202B-ND | 2.5mm 5A power jack | \$ | 0.92 |
| 1 | CF14JT22R0 | 22 ohm resistor | \$ | 0.20 |
| 1 | CFR-25JR-52-220R | 220 ohm resistor | \$ | 0.20 |
| 1 |  | 450uF 35v capacitor | \$ | 0.60 |
| 1 | 12R831 | 830 ohm resistor | \$ | 0.20 |
| 1 | CENB1040A0903F01 | 9V 4A adapter | \$ | 22.36 |
| 1 |  | Arduino Uno | \$ | 21.45 |
| 1 | 275-644 | Black SPST pushbutton | \$ | 3.69 |
| 1 |  | CPU Cooler Fan 12V 0.08A | \$ | 4.99 |
| 2 | HS278-ND | Heatsink | \$ | 1.34 |
| 24 |  | Pin headers (Male) 2.54 mm | \$ | 2.64 |
| 1 | BDX54C-ND | PNP transistor | \$ | 0.62 |
| 1 | 275-644 | Red SPST pushbutton | \$ | 3.69 |
| 1 |  | Servo Shield | \$ | 9.45 |
| 1 | LM317TFS-ND | Voltage regulator | \$ | 0.71 |

Continued on next page


## Quality Function Deployment



## Robotic Hand Decision Matrices

Table 1. Weighted decision matrix to determine actuation of fingers

|  | weight | Cable |  | cable/pulley |  | belt/chain |  | Gears |  | linear actuator |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Friction | 5 | 1 | 5 | 2 | 10 | 3 | 15 | 3 | 15 | 3 | 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| Cost | 3 | 4 | 12 | 3 | 9 | 2 | 6 | 2 | 6 | 2 | 6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Size | 4 | 4 | 16 | 4 | 16 | 3 | 12 | 3 | 12 | 4 | 16 |  |  |  |  |  |  |  |  |  |  |  |  |
| wear/life | 2 | 2 | 4 | 2 | 4 | 4 | 8 | 4 | 8 | 2 | 4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Noise | 1 | 4 | 4 | 3 | 3 | 2 | 2 | 3 | 3 | 3 | 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Weight | 2 | 5 | 10 | 4 | 8 | 3 | 6 | 3 | 6 | 3 | 6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Implementation | 3 | 5 | 15 | 4 | 12 | 2 | 6 | 3 | 9 | 3 | 9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Fluidity | 3 | 1 | 3 | 3 | 9 | 3 | 9 | 3 | 9 | 3 | 9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Location | 3 | 3 | 9 | 3 | 9 | 3 | 9 | 3 | 9 | 3 | 9 |  |  |  |  |  |  |  |  |  |  |  |  |
| Total |  |  |  |  |  |  |  |  |  |  |  |  |  | 29 | 78 | 28 | 80 | 25 | 73 | 27 | 77 | 26 | 77 |

Table 2. Weighted decision matrix to determine actuation of thumb

|  | Weight | Cable |  | cable/pulley |  | belt/chain |  | Gears |  | linear actuator |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Friction | 3 | 1 | 3 | 2 | 6 | 3 | 9 | 3 | 9 | 3 | 9 |  |
| Cost | 2 | 4 | 8 | 3 | 6 | 2 | 4 | 2 | 4 | 2 | 4 |  |
| Size | 4 | 4 | 16 | 4 | 16 | 3 | 12 | 3 | 12 | 4 | 16 |  |
| wear/life | 3 | 2 | 6 | 2 | 6 | 4 | 12 | 4 | 12 | 2 | 6 |  |
| Noise | 1 | 4 | 4 | 3 | 3 | 2 | 2 | 3 | 3 | 3 | 3 |  |
| Weight | 3 | 5 | 15 | 4 | 12 | 3 | 9 | 3 | 9 | 3 | 9 |  |
| Implementation | 3 | 5 | 15 | 4 | 12 | 2 | 6 | 3 | 9 | 3 | 9 |  |
| Fluidity | 5 | 1 | 5 | 3 | 15 | 3 | 15 | 3 | 15 | 3 | 15 |  |
| Location | 2 | 3 | 6 | 3 | 6 | 3 | 6 | 3 | 6 | 3 | 6 |  |
| Total |  |  | 29 | 78 | 28 | 82 | 25 | 75 | 27 | 79 | 26 | 77 |

Table 3. Decision matrix to determine the DOF for the thumb

|  | 1 degree | 2 degree |
| :--- | :---: | :---: |
| Implementation | 3 | 2 |
| Cost | 3 | 2 |
| Fluidity | 1 | 4 |
| Total | 7 | 8 |

Table 4. Decision matrix to determine the motor type

|  | servo | stepper | DC Brushless | piezo | DC brush |
| :--- | :---: | :---: | :---: | :---: | :---: |
| size | 4 | 3 | 3 | 4 | 3 |
| cost | 4 | 2 | 1 | 1 | 4 |
| weight | 4 | 2 | 3 | 5 | 3 |
| noise | 3 | 4 | 5 | 3 | 3 |
| life | 2 | 3 | 4 | 1 | 2 |
| Voltage | 4 | 3 | 4 | 5 | 3 |
| Total | $\mathbf{2 1}$ | 17 | 20 | 19 | 18 |

Table 5. Decision matrix to determine the actuation of the wrist

|  | motor | gears | belt/chain |
| :--- | :---: | :---: | :---: |
| implementation | 4 | 3 | 4 |
| Cost | 3 | 3 | 3 |
| Size | 2 | 4 | 2 |
| Weight | 2 | 3 | 2 |
| Total | 11 | 13 | 11 |




## Assembly Concept

This concept shows the layout of where all the components would be located. Inside the hand itself will mostly be springs and cables. The cables will run into the forearm and attach to the servomotor arms. The motors located at the wrist will allow for a twisting motion to form the letters J and Z . A slot will be made near the base of the forearm for the USB connection to the microcontroller.


## Engineering Drawings














## Rapid Prototyping Properties

## Eden250" The 16 Micoronloper 3D P Piniting Sysiem

Technical Specifications


- Veroblue Opoque material
- Veroblack Opaque material

Support Type

- FullCure (7705 Support
- Nontoxic gellike photopolymer support easily removed by WaterJet


## Materials Cartridges

Seoled $2 \times 2 \mathrm{~kg}$ cartridges easily and instantly replaced through a frontloading door

## Power Requirements

$110-240$ VAC $50 / 60 \mathrm{~Hz}$
1.5 KW single phase

Machine Dimensions ( $\mathrm{W} \times \mathrm{DxH}$ )
$870 \times 735 \times 1200 \mathrm{~mm}$

## Machine Weight

Net 280 kg
Gross (in crote) 330 kg
Software
Objet Studio ${ }^{\text {TM }}$ feactures:

- Suggested build orientation and speed, Autoplacement
- Automatic reol time support structure
generation
- Slice on the fly
- Polylog ${ }^{\text {TM }}$ Materials Management
- Network version

Input Format
STL and SLC File
Operational Environment
Temperature $18^{\circ} \mathrm{C}-25^{\prime} \mathrm{C}$
Relative Humidity 30-70\%
Special Facility Requirements
None
Jetting Heads
SHR (Single Head Replocement), 4 units
Network Communication
LAN-TCP/IP
Compotibility
Windows XP, Windows 2000
Other Fectures

- Removable troy for high productivity
- Quiet office operation
*All specilication are sub|ect to change without notice



Please, find the complete FullCure@ General Purpose Family Data Charts Below:

| Property | ASTM | Results in Metric Units |  | Results in Imperial Units |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Tensile Strength | D-638-03 | MPa | 60.3 | psi | 8744 |
| Modulus of Elasticity | D-638-04 | MPa | 2870 | psi | 416150 |
| Elongation at Break | D-638-05 | \% | 20 | \% | 20 |
| Flexural Strength | D.790-03 | MPa | 75.8 | psi | 10981 |
| Flexural Modulus | D.790-04 | MPa | 1718 | psi | 248110 |
| Compressive Strength | D-685-02 | MPa | 84.3 | psi | 12224 |
| Izod Notched Impact | D-256-06 | $\mathrm{J} / \mathrm{m}$ | 21.3 | At lbín | 0.40 |
| Shore Hardness | Scale D | Scale D | 83 | Scale D | 83 |
| Rockwell Hardness | Scale M | Scale M | 81 | Scale M | 81 |
| HDT at 0.45 MPa | D-848-08 | ${ }^{\circ} \mathrm{C}$ | 48.4 | ${ }^{\circ} \mathrm{F}$ | 118 |
| HDT at 1.82 MPa | D-648-07 | ${ }^{\circ} \mathrm{C}$ | 44.4 | ${ }^{\circ} \mathrm{F}$ | 112 |
| Tg | DMA, E" | ${ }^{\circ} \mathrm{C}$ | 48.7 | ${ }^{\circ} \mathrm{F}$ | 120 |
| Ash Content | NA | \% | $<0.01$ | \% | $<0.01$ |
| Water Absorption | D570-88 24 Hr | \% | 1.53 | \% | 1.53 |

## SAFETY DATA SHEET

## Version-2

Mased on Directive 2001/s3/EC of the Cominnion of the Duropem Commitien

## FULLCURE 720

## Identification of the substance/preparation and of the company/undertaking

1.1 Identification of the substance or preparation:

| Synonyms: | none |  |  |  |
| :--- | :---: | :--- | :--- | :---: |
| CAS No. |  |  |  |  |
| EC index No. | $\vdots$ | N.A. |  |  |
| EINECS No. | $\vdots$ | N.A. | NFPA code | N.D. |
| RTECS No. | $\vdots$ | N.A. | Molecular weight | $\vdots$ |
| Normula | N.A. |  |  |  |

1.2 Use of the substance or the preparation:

Toner
1.3 Company/undertaking identification:

Objet Geometries Ltd - Europe
Leuvensesteenweg 388
B-1932 Sint-Stevens-Woluwe
Fax : +32 27176500
Email: infoê2objet.com, www.2objet.com
1.4 Telephone number for emergency:

See 1.3

## 2. Composition/information on ingredients

| Hazardous ingredients | CAS No. EINECS/ELINCS No. | $\operatorname{Conc}_{\text {\& }} \text { in }$ | Hazard symbol | Risks <br> (R-phrases) |
| :---: | :---: | :---: | :---: | :---: |
| Acrylic Monomer | Proprietary (2) | $<40$ | Xn | 22-41-43-48/22 (1) |
| $\begin{aligned} & \text { exo-1,7,7- } \\ & \text { trimethylbicyclo[2.2.1]hept-2-yl } \\ & \text { acrylate } \end{aligned}$ | $\begin{aligned} & 5888-33-5 \\ & 227-561-6 \end{aligned}$ | $<40$ | xi | 43 (1) |
| urethane acrylate oligomer | N.D. | 1-20 | $x i$ | $36 / 38$ (2) |
| acrylate oligoner | N.D. | 1-20 | xi | $38-43$ (2) |
| epoxy acrylate | $154608-99-8$ | 1-20 | Xn | $\begin{aligned} & 20 / 22-36 / 37 / 38-43 \\ & (1) \end{aligned}$ |
| acrylate oligoner | N.D. | $<20$ | xi | 36/38 (2) |
| Photoinitiator | Proprietary | $<1$ | $x i$ | 43-53 (2) |

## 3. Hazards identification

- Classified dangerous in accordance with Directives 67/548/EEC and
- In normal conditions of use, the components cannot be released


## 4. First aid measures

4.1 Eye contact:
= Consult a doctor/medical service if irritation persists

- Rinse immediately with plenty of water for 15 minutes
- Do not apply neutralizing agents


## FULLCURE 720

4.2 Skin contact:

- Consult a doctor/medical service if irritation persists
- Soap may be used
- Wash immediately with lots of water
4.3 After inhalation:
- Consult a doctor/medical service if breathing problems develop
- Remove the victim into fresh air
- Unconscious: maintain adequate airway and respiration
4.4 After ingestion:

After ingestion:

- Consult a doctor/medical service if you feel unwell
Immediately give lots of water to drink
- Never give water to an unconscious person
- Do not induce vomiting


## 5. Fire-fighting measures

5.1 Suitable extinguishing media:

- Water spray
- AFFF foam
- BC powder
- Carbon dioxide
5.2 Unsuitable extinguishing media:
- No data available
5.3 Special exposure hazards:
- Combustible
- On burning: release of toxic and corrosive gases/vapours (nitrous vapours, carbon monoxide - carbon dioxide)
5.4 Instructions:
- If exposed to fire cool the closed containers by spraying with water
- Dilute toxic gases with water spray
5.5 Special protective equipment for firefighters:
- Heat/fire exposure: compressed air/oxygen apparatus
- Protective clothing for exposure to chemicals


## Accidental release measures

6.1 Personal protection/precautions:

See heading 8.2/8.3/13
6.2 Environmental precautions:

- Contain leaking substance
6.3 Methods for cleaning up:
- Take up liquid spill into absorbent material, e.g.: sand
- Scoop absorbed substance into closing containers
- Clean contaminated surfaces with an excess of water
- Wash clothing and equipment after handling


## Handling and storage

7.1 Handling:

Accidental release of the contents:

- Observe very strict hygiene - avoid contact
- Remove contaminated clothing immediately
- Clean contaminated clothing
7.2 Storage:
- Keep container tightly closed
- Keep out of direct sunlight
- Store in a dry area
- Store in a dark area
- Keep away from: heat sources


## FULLCURE 720


7.3 Specific uses:

- See information supplied by the manufacturer


## 8. Exposure controls/Personal protection

8.1 Exposure limit values:

| TLV-TWA | : not listed |
| :--- | :---: |
| TLV-STEL | not listed |
| TLV-Ceiling | not listed |
| OES-LTEL | not listed |
| OES-STEL | not listed |
| MEL-LTEL | not listed |
| MEL-STEL | not listed |
| MAK | not listed |
| TRK | not listed |
| MAC-TGG 8 h not listed |  |
| MAC-TGG 15 min. | not listed |
| MAC-Ceiling | not listed |
| VME-8 h | not listed |
| VLE-15 min. | not listed |
| GWBB-8 h | not listed |
| GWK-15 min. | not listed |
| Momentary value | not listed |
| EC | not listed |
| EC-STEL | not listed |
| Sampling methods : |  |

- No data available
8.2 Exposure controls:
8.2.1 Occupational exposure controls:

Accidental release of the contents:

- Work under local exhaust/ventilation
8.2.2 Environmental exposure controls: see heading 13
8.3 Personal protection:
8.3.1 respiratory protection:
- Not required for normal conditions of use
8.3.2 hand protection:
- Accidental release of the contents: Gloves Suitable materials: No data available
- Breakthrough time: N.D.
8.3.3 eye protection:
- Accidental release of the contents: Safety glasses
8.3.4 skin protection:
- Accidental release of the contents: Protective clothing

Suitable materials: No data available

## FULLCURE 720

## Physical and chemical properties

### 9.1 General information:

| Appearance (at $\left.20^{\circ} \mathrm{C}\right)$ | Toner cartridge |
| :--- | :--- |
| Odour | $\vdots \mathrm{N} . \mathrm{D}$. |
| Colour | N. |

9.2 Important health, safety and environmental information:
pH value : N.D.
Boiling point/boiling range : N.D. ${ }^{\circ} \mathrm{C}$
Flashpoint
Explosion limits
Vapour pressure (at $20^{\circ} \mathrm{C}$ )
Vapour pressure (at $50^{\circ} \mathrm{C}$ )
vol\% ( ${ }^{\circ} \mathrm{C}$ )
N.D.

Relative density (at $20^{\circ} \mathrm{C}$ ) N.D.

Water solubility
Soluble in
Relative vapour density
Viscosity
N.D. vols

Partition coefficient n-octanol/water
Evaporation rate
ratio to butyl acetate : N.D.
ratio to ether $\vdots$ N.D.
9.3 Other information:

Melting point/melting range N.D. hPa N.D.

Auto-ignition point N.D. N.D. N. D
N.D.
N.D.

Pa.s

Saturation concentration
: N.D.
${ }^{\circ} \mathrm{C}$
N.D.
$\mathrm{g} / \mathrm{m}^{3}$
10. Stability and reactivity
10.1 Conditions to avoid/reactivity:

- Unstable on exposure to heat
- Unstable on exposure to light
10.2 Materials to avoid:
- Keep away from: heat sources
10.3 Hazardous decomposition products:
- Polymerizes on exposure to light
- On burning: release of toxic and corrosive gases/vapours (nitrous vapours, carbon monoxide - carbon dioxide)


## FULLCURE 720

## 11. Toxicological information

### 11.1 Acute toxicity:

4-acryloylmorpholine

11.2 Chronic toxicity:

| EC carc. cat. | not listed |
| :--- | :---: |
| EC muta. cat. | $\vdots$ not listed |
| EC repr. cat. | not listed |
| Carcinogenicity (TLV) | not listed |
| Carcinogenicity (MAC) | $\vdots$ not listed |
| Carcinogenicity (VME) | not listed |
| Carcinogenicity (GWBB) | not listed |
| Carcinogenicity (MAK) | not listed |
| Mutagenicity (MAK) | not listed |
| Teratogenicity (MAK) | not listed |
| IARC classification | : not listed |

11. 3 Routes of exposure:

- In normal conditions of use, the hazardous contents cannot be released
11.4 Acute effects/symptoms:
- The following symptoms may appear when the components are released:
- AFTER SKIN CONTACT
- Tingling/irritation of the skin
- AFTER EYE CONTACT
- Irritation of the eye tissue
- Redness of the eye tissue


### 11.5 Chronic effects:

- May produce an allergic reaction
- The following symptoms may appear when the components are released:
- ON CONTINUOUS/REPEATED EXPOSURE/CONTACT:
- Skin rash/inflammation


## FULLCURE 720

## 12. Ecological information

### 12.1 Ecotoxicity:

- No data available
12.2 Mobility:
- Volatile organic compounds (VOC): N.D. \%

For other physicochemical properties see heading 9
12.3 Persistence and degradability:

- biodegradation BOD $_{5}$ :
N. D.
\% ThOD
- water
$: \quad-$ N.D.
- soil : T $m_{2}:$ N.D. days
12.4 Bioaccumulative potential:
$=10{ }^{-10} P_{\text {ow }} \quad \vdots$ N.D.
=
12.5 Other adverse effects:
- WGK : N.V.T
- Effect on the ozone layer : Not dangerous for the ozone layer
- Greenhouse effect (1999/45/EC)
: $\quad$ no data available
- Effect on waste water purification : no data available


## 13. Disposal considerations

13.1 Provisions relating to waste:

- Waste material code $(91 / 689 / E E C$, Council Decision $2001 / 118 / \mathrm{EC}, 0 . \mathrm{J} . ~ L 47$ of 16/2/2001): $080317^{2}$ (waste printing toner containing dangerous substances)
- Hazardous waste (91/689/EEC)


### 13.2 Disposal methods:

- Refer to manufacturer/supplier for information on recovery/recycling - Remove to an authorized waste treatment plant
13.3 Packaging/Container:
- No available data


## FULLCURE 720

## 14. Transport information

14.1 Classification of the substance in compliance with UN Recommendations

UN number
CLASS
SUB RISKS
PACKING
PROPER SHIPPING NAME
14.2 ADR (transport by road)

CLASS
PACKING
CLASSIFICATION CODE
DANGER LABEL TANKS
DANGER LABEL PACKAGES

```
NOT SUBJECT
```

RID (transport by rail)
CLASS
NOT SUBJECT
PACKING
CLASSIFICATION CODE
DANGER LABEL TANKS
DANGER LABEL PACKAGES
ADNR (transport by inland waterways) CLASS

NOT SUBJECT
PACKING
CLASSIFICATION CODE
DANGER LABEL TANKS
DANGER LABEL PACKAGES

14.5 IMDG (maritime transport)

CLASS
NOT SUBJECT
SUB RISKS
PACKING
MFAG
EMS
MARINE POLLUTANT
14.6 ICAO (air transport)

CLASS
SUB RISKS
PACKING
PACKING INSTRUCTIONS PASSENGER AIRCRAFT
PACKING INSTRUCTIONS CARGO AIRCRAFT

## FULLCURE 720

## 15. Regulatory information

Classified dangerous in accordance with Directives 67/548/EEC and 1999/45/EC. In normal conditions of use, the components cannot be released because of the form in which the article or preparation is placed on the market.

Contains: acrylate oligomer; epoxy acrylate; exo-1,7,7-
trimethylbicyclo[2.2.1)hept-2-yl acrylate ; phenyl bis(2,4,6-
trimethylbenzoyl)-phosphine oxide; 4-acryloylmorpholine. May produce an
allergic reaction

## 16. Other information

The information provided on this MSDS is correct to the best of our knowledge, infornation and belief at the date of its publication. The infornation given is designed only as a guidance for safe handling, use, processing, storage, transportation, disposal and release and is not to be considered as a warranty or quality specification. The information relates only to the specific material designated and may not be valid for such material used in combination with any other material or in any process, unless specified in the text.
N.A. $=$ NOT APPLICABLE
N.D. $=$ NOT DETEFMINED
(*) $=$ INTERNAL CLASSIFICATION (NEPA)
Exposure limits:
TLV : Threshold Limit Value - ACGIH USA 2004
oes : Occupational Exposure Standards - United Kingdom 2003
MEL : Maximum Exposure Limits - United Kingdom 2003
MDX : Maximale Arbeitsplatzkonzentrationen - Germany 2002
TRK : Technische Richtkonzentrationen - Germany 2002
MAC : Maxinale aanvaarde concentratie - The Netherlands 2004
vas : Valeurs linites de Moyenne d'Exposition - France 1999
VLE : Valeurs linites d'Exposition a court terne - France 1999
$G W B B$ : Grenswaarde beroepsmatige blootstelling - Belgium 2002
GWK : Grenswaarde kortstondige blootstelling - Eelgium 2002
EC : Indicative occupational exposure linit values - directive 2000/39/EC
Chronic toxicity:
K : List of the carcinogenic substances and processes - The Netherlands 2004
Full text of any R-phrases referred to under heading 2 :


## Electricity Costs



SCE Average Bundled Rates by Class


Published by the Public Utilities Commission of California

## Servo Data Sheets

HS-625MG High Speed Metal Gear Servo

## $32625 S$



The powerful high speed HS-625MG is a perfect choice for those applications requiring a fast and strong standard size servo. Utilizing our M/P and metal gear train technology, the HS-625MG is a fantastic sport servo for larger planes and 10th scale sport vehicles.

## Specifications

| Motor Type: | 3 Pole |
| :--- | :--- |
| Bearing Type: | Dual Ball Bearing |
| Speed (4.8V/6.0V): | $0.18 / 0.15 ~ s e c ~$ <br> deg. 60 |
| Torque $02 . / \mathrm{in}$. <br> $(4.8 \mathrm{~V} / 6.0 \mathrm{~V}):$ | $76 / 94$ |
| Torque $\mathrm{kg} / \mathrm{/m}$. <br> $(4.8 \mathrm{~V} / 6.0 \mathrm{~V}):$ | $5.5 \times 6.8$ |
| Size in Inches: | $1.59 \times 0.77 \times 1.48$ |
| Size in Millimeters: | $40.39 \times 19.56 \times 37.59$ |
| Weight ounces: | 1.94 |
| Weight grams: | 55.00 |

Spare Parts
55402 - Case Set

## HS-645MG High Torque Metal Gear Servo



The powerful HS-44MG is one of hitects most popular servos. It's the perfect cholce for those larger sport planes of monster trucks and buggles requiring a durable high torque servo. Featuring bur unlague M/P and metal gear train techinology, the HS-645MG offers one of the strongest gear traling awallable in any servo.

## Specifications

| Motor Typer: | 3 Pole |
| :---: | :---: |
| Bearing Type: | Duall Ball Bearing |
| Speed (4.8v/8.0V): | $0.24 / 0.20$ |
| Torque oz_/ln. (4.8V/6.04): | $107 / 133$ |
| Torque kifon. (4,8V/6.0V) | 80.0/10.0 |
| Ste in Inches: | $1.59 \times 0.77$ 遃 1.48 |
| Stre in Mlilimeters: | $\begin{aligned} & 40.39 \times 19.564 \\ & 37.59 \end{aligned}$ |
| Welght ounces: | 1.94 |
| Welihit grame: | 55 |

Spare Parts
5g109-Gear Set
S9402-Cate St

## SERVO Shield Schematic



## SERVO Shield PCB Design



Bottom of Board

## SERVO Shield BOM




## FAIRCHILD

SEMICONDUCTOR*
www.fairchildsemi.com

## LM317

## 3-Terminal Positive Adjustable Regulator

## Features

- Output Current In Excess of 1.5A
- Output Adjustable Between 1. 2V and 37V
- Internal Thermal Overload Protection
- Internal Short Circuit Current Limiting
- Output Transistor Safe Operating Area Compensation
- TO-220 Package


## Description

This monolithic integrated circuit is an adjustable 3-terminal positive voltage regulator designed to supply more than 1.5 A of load current with an output voltage adjustable over a 1.2 to 37 V . It employs internal current limiting, thermal shut-down and safe area compensation.


## Internal Block Diagram



LM317

## Absolute Maximum Ratings

| Parameter | Symbol | Value | Unit |
| :--- | :---: | :---: | :---: |
| Input-Output Voltage Differential | $\mathrm{V}_{1}-\mathrm{V}_{\mathrm{O}}$ | 40 | V |
| Lead Temperature | T LEAD | 230 | ${ }^{\circ} \mathrm{C}$ |
| Power Dissipation | PD | Intemally limited | W |
| Operating Junction Temperature Range | Tj | $0 \sim+125$ | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature Range | TSTG | $-65 \sim+125$ | ${ }^{\circ} \mathrm{C}$ |
| Temperature Coefficient of Output Voltage | $\Delta \mathrm{Vol} / \Delta \mathrm{T}$ | $\pm 0.02$ | ${ }^{\circ} /{ }^{\circ} \mathrm{C}$ |

## Electrical Characteristics

$\left(\mathrm{VI}-\mathrm{VO}=5 \mathrm{~V}, \mathrm{IO}_{\mathrm{O}}=0.5 \mathrm{~A}, 0^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{J}} \leq+125^{\circ} \mathrm{C}, \mathrm{IMAX}=1.5 \mathrm{~A}, \mathrm{PDMAX}=20 \mathrm{~W}\right.$, unless otherwise specified)

| Parameter | Symbol | Conditions | Min | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Line Regulation (Note1) | Rline | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C} \\ & 3 \mathrm{~V} \leq \mathrm{V}-\mathrm{VO} \leq 40 \mathrm{~V} \end{aligned}$ | - | 0.01 | 0.04 | \% / V |
|  |  | $3 \mathrm{~V} \leq \mathrm{V}_{1}-\mathrm{VO} \leq 40 \mathrm{~V}$ | - | 0.02 | 0.07 | \% /V |
| Load Regulation (Note1) | Rload | $\begin{aligned} & \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, 10 \mathrm{~mA} \leq \mathrm{I}_{\mathrm{O}} \leq \mathrm{I}_{\mathrm{MAX}} \\ & \mathrm{VO}_{0}<5 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{O}} \geq 5 \mathrm{~V} \end{aligned}$ | - | $\begin{aligned} & 18 \\ & 0.4 \end{aligned}$ | $\begin{aligned} & 25 \\ & 0.5 \end{aligned}$ | mV\% / Vo |
|  |  | $\begin{aligned} & 10 \mathrm{~mA} \leq \mathrm{lO} \leq \operatorname{lmAX} \\ & \mathrm{Vo}_{\mathrm{O}}<5 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{O}} \geq 5 \mathrm{~V} \end{aligned}$ | - | $\begin{aligned} & 40 \\ & 0.8 \end{aligned}$ | $\begin{array}{r} 70 \\ 1.5 \end{array}$ | mV\% / Vo |
| Adjustable Pin Current | $l_{\text {ADJ }}$ | - | - | 46 | 100 | $\mu \mathrm{A}$ |
| Adjustable Pin Current Change | $\triangle \mathrm{A}, \mathrm{DJ}$ | $\begin{aligned} & 3 \mathrm{~V} \leq \mathrm{V} 1-\mathrm{VO} \leq 40 \mathrm{~V} \\ & 10 \mathrm{~mA} \leq \mathrm{lO} \leq \mathrm{IMAX} P \mathrm{PD} \leq \mathrm{PMAX} \end{aligned}$ | - | 2.0 | 5 | $\mu \mathrm{A}$ |
| Reference Voltage | VREF | $\begin{aligned} & 3 \mathrm{~V} \leq \mathrm{VIN}-\mathrm{VO} \leq 40 \mathrm{~V} \\ & 10 \mathrm{~mA} \leq \mathrm{IO} \leq \mathrm{ImAX} \\ & \mathrm{PD} \leq \mathrm{PmAX} \end{aligned}$ | 1.20 | 1.25 | 1.30 | V |
| Temperature Stability | STT | - | - | 0.7 | - | \% / Vo |
| Minimum Load Current to Maintain Regulation | IL(MIN) | $V_{1}-V_{O}=40 \mathrm{~V}$ | - | 3.5 | 12 | mA |
| Maximum Output Current | lo(maX) | $\begin{aligned} & \mid V_{1}-V_{0} \leq 15 \mathrm{~V}, \mathrm{PD} \leq \mathrm{PmAX} \\ & \mathrm{~V}_{1}-\mathrm{VO}_{\mathrm{O}} \leq 40 \mathrm{~V}, \mathrm{PD} \leq \mathrm{PmAx} \\ & T_{A}=25^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ | 1.0 | $\begin{aligned} & 2.2 \\ & 0.3 \end{aligned}$ | - | A |
| RMS Noise, \% of VOUT | eN | TA $=+25^{\circ} \mathrm{C}, 10 \mathrm{~Hz} \leq \mathrm{f} \leq 10 \mathrm{KHz}$ | - | 0.003 | 0.01 | \% / Vo |
| Ripple Rejection | RR | $\begin{aligned} & \mathrm{VO}=10 \mathrm{~V}, \mathrm{f}=120 \mathrm{~Hz} \\ & \text { without CADJ } \\ & \text { CADJ }=10 \mu \mathrm{~F} \text { (Note2) } \end{aligned}$ | 66 | $\begin{aligned} & 60 \\ & 75 \end{aligned}$ | - | dB |
| Long-Term Stability, $\mathrm{T}_{\mathrm{J}}=$ THIGH | ST | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ for end point measurements, 1000 HR | - | 0.3 | 1 | \% |
| Thermal Resistance Junction to Case | $\mathrm{R}_{\text {өJC }}$ | - | - | 5 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

Note:

1. Load and line regulation are specified at constant junction temperature. Change in VD due to heating effects must be taken into account separately. Pulse testing with low duty is used. (PMAX $=20 \mathrm{~W}$ )
2. CADJ, when used, is connected between the adjustment pin and ground.

## 2

## CENB1040



## Universal 40 Watt Series

## ITE Switch-Mode Power Supply

3 Year Warranty

-Impact-Resistant Polycarbonate Enclosure


| Specifications | All Specifications are typical at nominal input, full load at $25^{\circ} \mathrm{C}$ unless otherwise stated. |  |  |
| :---: | :---: | :---: | :---: |
| AC Input | 100-240VAC, $-10 \%, 47-63 \mathrm{~Hz}, 1 \varnothing$ | MTBF | >100,000 hours (calculated) |
| Input Current | 100VAC: 1.1A | Hold-up Time | 18 ms min @ $115 \mathrm{Vac}, 60 \mathrm{~ms}$ @ 230 Vac |
| Inrush Current | 60 A peak, 264 V , cold start | Overload Protection | Hiccup Mode |
| Input Fuse 3.15A, 250 V Int | 3.15A, 250V Internal Primary Current Fuse is provided | Short Circuit Protection | Hiccup Mode |
| Efficiency Mee | Meets EISA2007, CEC Efficiency Level V, EU (EC) No 278/2009 Phase II | Topology | Switching - Fixed Frequency Flyback |
| Output Voltage | See chart | Safety Standards | EN/EC/CSA/UL60950-1, $2^{\text {0 }}$ Edition, LPS |
| Output Power | See chart | EMC | See chart below |
| Ripple and Noise | 1\% pk-pk max., 20MHz BW | Dielectric Withstand | Input-Output: 4,242Vdc Input-GND: 1.500 Vac . Output-GND: 500 Vdc |
| Line \& Load Voltage Regulation | Line: $+1 / 1 \%$, Load: $+1 / 5 \%$ | Operating Temperature | $0^{\circ}$ to $40^{\circ} \mathrm{C}$, no derating |
| Transient Response | nse $\quad 500 \mu \mathrm{~s}$ max., $50 \%$ load step, typical | Storage Temperature | -30 to $+85^{\circ} \mathrm{C}$ |
| Minimum Load | Not required | Relative Humidity | $5 \%$ to $95 \%$, non-condensing |
| Case Material | Black 94V0 Polycarbonate | Altitude | 0 to 10,000 ft |
| Case Dimensions | s $102 \times 60 \times 32 \mathrm{~mm}$. See outline drawing | Output Cable | \#18AWG (UL1185), 1,500mm, 2 conductor |
| Weight | 250 g | Output Connector | 2.5 mm barrel type (Ault \#3), center positive ( + ) |


| EMC Specifications |  |
| :---: | :---: |
| Conducted Emissions | EN55022 Class B, FCC Part 15, Class B. |
| Radiated Emissions | EN55022 Class B, FCC Part 15, Class B. |
| Line Frequency Harmonics | EN61000-3-2, Class A |
| Voltage Fluctuations/Flicker | EN61000-3-3 |
| Static Discharge Immunity | EN61000-4-2, 6kV Contact Discharge, 8 kV air discharge |
| Radiated RF Immunity | EN61000-4-3, 3V/m. |
| EFT/Burst Immunity | EN61000-4-4, $2 \mathrm{kV} / 5 \mathrm{kHz}$. |
| Line Surge Immunity | EN61000-4-5, 1kV differential, 2kV common-mode |
| Conducted RF Immunity | EN61000-4-6, 3 Vms |
| Power Frequency Magnetic Field Immunity | EN61000-4-8, 3A/m |
| Voltage Dip Immunity | EN61000-4-11, Criteria B |

## Master Task



```
Master_task.h
//*****************************************************************************************
/**\file master_task.h
    * This file contains a task class for the master controller of the project.
*
* Revisions:
* \li 02-06-2012 Created
* \li 03-26-2012 Header file accepted by Arduino
* \li 04-17-2012 Constructor with pointers accepted in Arduino
* License:
* This file released under the Lesser GNU Public License, version 2. This program
* is intended for educational use only, but it is not limited thereto.
*/
//******************************************************************************************
/// This define prevents this .h file from being included more than once in a .cc file
#ifndef _MASTER_TASK_H_
#define _MASTER_TASK_H_
#include <stdlib.h>
#include <stdint.h>
#include <Servo.h>
#include <user_task.h>
#if defined(ARDUINO) && ARDUINO >= 100
    #include "Arduino.h"
#else
    #include "WProgram.h"
    #include <pins_arduino.h>
#endif
class master_task
{
    protected:
    bool write; // True if motor should be
running now
        bool demo;
        bool demo_begin;
        uint8_t state;
        uint8_t letter;
        uint8_t thumbdown;
        uint16_t wordtime; // amount of time to delay between words
        uint16_t lettertime; // amount of time to delay between
        uint8_t previousthumb;
        uint8_t currentthumb;
        Servo servo1;
        Servo servo2;
        Servo servo3;
        Servo servo4;
        Servo servo5;
        Servo servo6;
        Servo servo7;
        Servo servo8;
        Servo servo9;
        Servo servo10;
        Servo servo11;
        user_task *user;
        public:
            // The constructor creates a new task object
```

```
    master_task (user_task*, Servo, Servo)/*, Servo, Servo, Servo,
                            Servo, Servo, Servo, Servo, Servo, Servo); //(task_timer&, time_stamp&)*/;
    // Tells master that the button was pressed and to run the demo loop
    void run_demo(void);
    // Delay between words
    void wait(uint16_t);
    // Detaches servos
    void detach_servos(void);
    // writes the 0 position to the finger servos
    void neutral_fingers(void);
    // writes the zero position to the thumb servos
    void neutral_thumb(void);
    // reattaches servos
    void attach_servos(void);
    // The run method is where the task actually performs its function
    void run (void);
};
#endif // _MASTER_TASK_H_
```

```
Master_task.cpp
//***************************************************************************************
/** \file master_task.cpp
    * This file tells the hand what needs to be actuated and when. It also controls the
    * delay between letters, words, and each time the demo is run.
*
* Revisions:
* \li 02-06-2012 Created
* \li 03-26-2012 Header file accepted by Arduino
* \li 04-17-2012 Constructor with pointers accepted in Arduino
* \li 05-25-2012 fixed demo function/letter by letter/ sentence input
*
* License:
* This program is intended for fingerspelling use with The Smith-Kettlewell Eye
* Research Institute robotic hand, but it is not limited thereto.
*/
//**************************************************************************************
#include <stdlib.h>
#include <stdint.h>
#include <Arduino.h>
#include <user_task.h>
#include <Servo.h>
#include <master_task.h>
#define KNUCKLETHUMBO }14
#define KNUCKLETHUMB30 115
#define KNUCKLETHUMB45 100
#define KNUCKLETHUMB60 }8
#define KNUCKLETHUMB90 50
#define MEDIALTHUMB180 140
#define MEDIALTHUMB90 110
#define MEDIALTHUMB80 100
#define MEDIALTHUMB60 95
#define MEDIALTHUMB45 90
#define MEDIALTHUMB3O }8
#define MEDIALTHUMBO }8
#define KNUCKLEINDEXO }15
#define KNUCKLEINDEX15 130
#define KNUCKLEINDEX30 }12
#define KNUCKLEINDEX45 115
#define KNUCKLEINDEX60 105
#define KNUCKLEINDEX90 95
#define MEDIALINDEXO }11
#define MEDIALINDEX45 85
#define MEDIALINDEX90 65
#define KNUCKLEMIDDLEO }13
#define KNUCKLEMIDDLE30 110
#define KNUCKLEMIDDLE45 105
#define KNUCKLEMIDDLE60 95
#define KNUCKLEMIDDLE90 }8
#define MEDIALMIDDLEO 90
#define MEDIALMIDDLE45 65
#define MEDIALMIDDLE90 45
#define KNUCKLERINGO }11
#define KNUCKLERING3O }8
#define KNUCKLERING45 70
#define KNUCKLERING60 }6
#define KNUCKLERING90 55
```


## \#define MEDIALRINGO 135

\#define MEDIALRING45 105
\#define MEDIALRING90 80
\#define KNUCKLEPINKYO 105
\#define KNUCKLEPINKY30 90
\#define KNUCKLEPINKY45 75
\#define KNUCKLEPINKY60 70
\#define KNUCKLEPINKY90 60
\#define MEDIALPINKYO 140
\#define MEDIALPINKY45 100
\#define MEDIALPINKY90 80
\#define THUMBIN 1
\#define THUMBOUT 0
\#define WRISTSTILL 20
\#define WRISTTURN 150
uint8_t values [26][13]=
\{
\{'A',KNUCKLETHUMB0 ,MEDIALTHUMB90 ,KNUCKLEINDEX90 ,MEDIALINDEX90 ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE9 0 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
$\{' \mathrm{~B} ', K N U C K L E T H U M B O$,MEDIALTHUMBO ,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLEO ,MEDIALMIDDLEO ,KNUCKLERI NGO ,MEDIALRINGO ,KNUCKLEPINKYO ,MEDIALPINKYO ,WRISTSTILL ,THUMBOUT\},
 LERING45 ,MEDIALRING90 ,KNUCKLEPINKY45 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
$\{' D ', K N U C K L E T H U M B 30, M E D I A L T H U M B 45, K N U C K L E I N D E X O$,MEDIALINDEXO ,KNUCKLEMIDDLE45 ,MEDIALMIDDLE90 ,KNUCKL ERING45 ,MEDIALRING90 ,KNUCKLEPINKY45 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
$\{' E ', K N U C K L E T H U M B 0, M E D I A L T H U M B O$,KNUCKLEINDEXO ,MEDIALINDEX90 ,KNUCKLEMIDDLEO ,MEDIALINDEX90 ,KNUCKLERI NG0 ,MEDIALRING90 ,KNUCKLEPINKYO ,MEDIALPINKY90 ,WRISTSTILL ,THUMBIN \},
$\{$ 'F',KNUCKLETHUMB30,MEDIALTHUMB80 ,KNUCKLEINDEX30 ,MEDIALINDEX90 ,KNUCKLEMIDDLEO ,MEDIALMIDDLEO ,KNUCKL ERINGO ,MEDIALRINGO ,KNUCKLEPINKYO ,MEDIALPINKYO ,WRISTSTILL ,THUMBIN \},
$\{' G ', K N U C K L E T H U M B O$,MEDIALTHUMB90 ,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE90 ,KNUCKL ERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTTURN ,THUMBOUT\},
\{'H',KNUCKLETHUMBO ,MEDIALTHUMB90 ,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLEO ,MEDIALMIDDLEO ,KNUCKLE RING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTTURN ,THUMBOUT\},
$\{$ 'I',KNUCKLETHUMB0 ,MEDIALTHUMB90 ,KNUCKLEINDEX90 ,MEDIALINDEX90 ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE45 ,KNUCKL ERING90 ,MEDIALRING45 ,KNUCKLEPINKYO ,MEDIALPINKYO ,WRISTTURN ,THUMBOUT\},
\{'J',KNUCKLETHUMBO ,MEDIALTHUMB90 ,KNUCKLEINDEX90 ,MEDIALINDEX90 ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE4 5 ,KNUCKLERING90 ,MEDIALRING45 ,KNUCKLEPINKYO ,MEDIALPINKYO ,WRISTSTILL ,THUMBOUT\},
$\{$ 'K',KNUCKLETHUMBO ,MEDIALTHUMB80 ,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLE45 ,MEDIALMIDDLEO , KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
$\{' L ', K N U C K L E T H U M B O$,MEDIALTHUMB180,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE90 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
$\{' \mathrm{M} ', K N U C K L E T H U M B 0$,MEDIALTHUMB30 ,KNUCKLEINDEX60 ,MEDIALINDEX45 ,KNUCKLEMIDDLE60 ,MEDIALMIDDLE 45 ,KNUCKLERING45, MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBIN \},
$\{' N ', K N U C K L E T H U M B 0$,MEDIALTHUMB30 ,KNUCKLEINDEX60 ,MEDIALINDEX45 ,KNUCKLEMIDDLE60 ,MEDIALMIDDLE4 5 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBIN \},
\{'O',KNUCKLETHUMB30,MEDIALTHUMB45 ,KNUCKLEINDEX45 ,MEDIALINDEX90 ,KNUCKLEMIDDLE45 ,MEDIALMIDDLE 90 ,KNUCKLERING45 ,MEDIALRING90 ,KNUCKLEPINKY45 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBIN \},
\{'P',KNUCKLETHUMBO ,MEDIALTHUMB90 ,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLE60 ,MEDIALMIDDLE45 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
$\{$ 'Q',KNUCKLETHUMB45,MEDIALTHUMB90 ,KNUCKLEINDEX90 ,MEDIALINDEXO ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE9 0 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
\{'R',KNUCKLETHUMB30,MEDIALTHUMB45 ,KNUCKLEINDEX15 ,MEDIALINDEXO ,KNUCKLEMIDDLEO ,MEDIALMIDDLEO ,KNUCKLERING30 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
\{'S',KNUCKLETHUMB30,MEDIALTHUMB60 ,KNUCKLEINDEX90 ,MEDIALINDEX90 ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE9 0 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
\{'T',KNUCKLETHUMB0 ,MEDIALTHUMB45 ,KNUCKLEINDEX45 ,MEDIALINDEX90 ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE9 0 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBIN \},
$\{' U ', K N U C K L E T H U M B 30, M E D I A L T H U M B 30$,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLEO ,MEDIALMIDDLEO , KNUCKLERING30 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
\{'V',KNUCKLETHUMB30,MEDIALTHUMB80 ,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE9 0 ,KNUCKLERINGO ,MEDIALRINGO ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
\{'W',KNUCKLETHUMB30,MEDIALTHUMB30 ,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLEO ,MEDIALMIDDLEO ,KNUCKLERINGO ,MEDIALRINGO ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
$\{$ 'X',KNUCKLETHUMB30,MEDIALTHUMB30 ,KNUCKLEINDEXO ,MEDIALINDEX90 ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE9 0 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTSTILL ,THUMBOUT\},
$\{' Y ', K N U C K L E T H U M B 0$,MEDIALTHUMB180,KNUCKLEINDEX90 ,MEDIALINDEX90 ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE9 0 ,KNUCKLERING90 , MEDIALRING90 , KNUCKLEPINKYO ,MEDIALPINKYO ,WRISTSTILL ,THUMBOUT\},
\{'Z',KNUCKLETHUMB45,MEDIALTHUMB45 ,KNUCKLEINDEXO ,MEDIALINDEXO ,KNUCKLEMIDDLE90 ,MEDIALMIDDLE90 ,KNUCKLERING90 ,MEDIALRING90 ,KNUCKLEPINKY90 ,MEDIALPINKY90 ,WRISTTURN ,THUMBOUT\}
\};

```
master_task::master_task (user_task *usertask, Servo servoone, Servo servotwo)/*, servo servo3, servo servo4,
```

servo servo5, servo servo6, servo servo7, servo servo8, servo servo9, servo servo10, servo servo11)*/
\{
servo1 = servoone;
servo2 = servotwo;
user = usertask;
letter = 0;
write = false;
wordtime = 1000;
lettertime = 500;
previousthumb $=0$;
currentthumb $=0$;
state=0;
\}
void master_task::run_demo(void)
\{
demo = true;
demo_begin = true;

```
    state = 8;
}
void master_task::wait(uint16_t delaytime)
{
    for(volatile int i = 0; i<=delaytime; i++)
    {
    }
}
void master_task::detach_servos(void)
{
    servo1.detach();
    servo2.detach();
    servo3.detach();
    servo4.detach();
    servo5.detach();
    servo6.detach();
    servo7.detach();
    servo8.detach();
    servo9.detach();
    servo10.detach();
    servo11.detach();
}
void master_task::neutral_fingers(void)
{
    servo3.write(KNUCKLEINDEXO);
    servo4.write(MEDIALINDEXO);
    servo5.write(KNUCKLEMIDDLEO);
    servo6.write(MEDIALMIDDLEO);
    servo7.write(KNUCKLERINGO);
    servo8.write(MEDIALRINGO);
    servo9.write(KNUCKLEPINKYO);
    servo10.write(MEDIALPINKYO);
}
void master_task::neutral_thumb(void)
{
    servo1.write(KNUCKLETHUMBO);
    servo2.write(MEDIALTHUMB180);
}
void master_task::attach_servos(void)
{
    servo1.attach(11); // KNUCKLETHUMB
    servo2.attach(2); // MEDIALTHUMB
    servo3.attach(3); // KNUCKLEINDEX
    servo4.attach(4); // MEDIALINDEX
    servo5.attach(5); // KNUCKLEMIDDLE
    servo6.attach(6); // MEDIALMIDDLE
    servo7.attach(7); // KNUCKLERING
    servo8.attach(8); // MEDIALRING
    servo9.attach(9); // KNUCKLEPINKY
    servo10.attach(10); // MEDIALPINKY
    servo11.attach(12); // Wrist
    neutral_fingers();
    neutral_thumb();
}
void master_task::run (void)
{
    switch(state)
```

\{

```
case(0):
attach_servos();
state = 1;
    break;
case(1):
    write = user->got_letter();
    if(write==true)
    {
        letter = user->input_letter();
        user->reset();
        state=2;
    }
    break;
case(2):
currentthumb = values[letter][12];
    if(letter == 26)
    {
        if(lettertime >= 200)
        {
            lettertime -= 100;
            Serial.println(lettertime);
            }
            user->get_next_letter();
            state = 1;
    }
    else if(letter == 27)
    {
        if(lettertime <= 2000)
        {
            lettertime += 100;
            Serial.printIn(lettertime);
            }
            user->get_next_letter();
            state = 1;
    }
    else if (letter == 28)
    {
        neutral_finger();
        neutral_thumb();
        delay(wordtime);
        user->get_next_letter();
        state = 1;
    }
    else if (letter == 29)
    {
        detach_servos();
        user->get_next_letter();
        state = 1;
    }
    else if (letter == 30)
    {
    attach_servos();
    user->get_next_letter();
    state = 1;
}
else if (previousthumb == 1 && currentthumb == 1)
{
```

```
        state = 3;
    }
    else if (previousthumb == 0 && currentthumb == 1)
    {
        state = 4;
    }
    else if(previousthumb == 1&& currentthumb == 0)
    {
        state = 5;
    }
    else
    {
        state = 6;
}
previousthumb = currentthumb;
break;
case(3):
    Serial.println("thumb inside to another letter with thumb inside");
    Serial.println("Fingers move to zero");
    Serial.println("thumb Move to position");
    Serial.println("fingers move to position");
    neutral_fingers();
    delay(100);
    servo1.write(values[letter][1]);
    servo2.write(values[letter][2]);
    servo3.write(values[letter][3]);
    servo4.write(values[letter][4]);
    servo5.write(values[letter][5]);
    servo6.write(values[letter][6]);
    servo7.write(values[letter][7]);
    servo8.write(values[letter][8]);
    servo9.write(values[letter][9]);
    servo10.write(values[letter][10]);
    servo11.write(values[letter][11]);
    state = 7;
    break;
case(4):
    Serial.println("thumb outside to letter with thumb inside");
    Serial.printIn("thumb move to zero");
    Serial.println("fingers move to zero");
    Serial.println(" thumb Move to position");
    Serial.println(" fingers move to position");
    neutral_thumb();
    delay(100);
    neutral fingers();
    delay(100);
    servo1.write(values[letter][1]);
    servo2.write(values[letter][2]);
    delay(150);
    servo3.write(values[letter][3]);
    servo4.write(values[letter][4]);
    servo5.write(values[letter][5]);
    servo6.write(values[letter][6]);
    servo7.write(values[letter][7]);
    servo8.write(values[letter][8]);
    servo9.write(values[letter][9]);
```

```
    servo10.write(values[letter][10]);
    servo11.write(values[letter][11]);
    state = 7;
    break;
case(5):
    Serial.println("thumb inside to letter with thumb outside");
    Serial.println("fingers move to zero");
    Serial.printIn("thumb move to zero");
    Serial.println(" fingers move to position");
    Serial.println(" thumb Move to position");
    neutral_fingers();
    delay(100);
    neutral_thumb();
    delay(100);
    servo3.write(values[letter][3]);
    servo4.write(values[letter][4]);
    servo5.write(values[letter][5]);
    servo6.write(values[letter][6]);
    servo7.write(values[letter][7]);
    servo8.write(values[letter][8]);
    servo9.write(values[letter][9]);
    servo10.write(values[letter][10]);
    servo1.write(values[letter][1]);
    servo2.write(values[letter][2]);
    servo11.write(values[letter][11]);
    state = 7;
    break;
case(6):
    Serial.println("thumb outside to letter with thumb outside");
    Serial.println("thumb move to zero");
    Serial.println(" fingers move to position");
    Serial.println(" thumb Move to position");
    neutral_thumb();
    delay(100);
    servo3.write(values[letter][3]);
    servo4.write(values[letter][4]);
    servo5.write(values[letter][5]);
    servo6.write(values[letter][6]);
    servo7.write(values[letter][7]);
    servo8.write(values[letter][8]);
    servo9.write(values[letter][9]);
    servo10.write(values[letter][10]);
    servo1.write(values[letter][1]);
    servo2.write(values[letter][2]);
    servo11.write(values[letter][11]);
    state = 7;
    break;
case(7):
    Serial.println((char)values[letter][0]);
    delay(lettertime);
    user->get_next_letter();
    if(demo)
{
    state = 8;
}
```

```
    else
    {
            state = 1;
    }
    break;
    case(8):
        letter ++;
        if(demo_begin)
    {
        demo_begin = false;
        letter = 0;
        state = 2;
    }
    else if(letter == 26)
    {
        demo = false;
        delay(10000);
        state = 1;
    }
    else
    {
        state = 2;
    }
    break;
    default:
        Serial.println('Error State');
        break;
    }
}
```


## Servo Code

## Servo.h

Servo.h - Interrupt driven Servo library for Arduino using 16 bit timers- Version 2
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You should have received a copy of the GNU Lesser General Public License along with this library; if not, write to the Free Software Foundation, Inc., 51 Franklin St, Fifth Floor, Boston, MA 02110-1301 USA
*/
/*

A servo is activated by creating an instance of the Servo class passing the desired pin to the attach() method. The servos are pulsed in the background using the value most recently written using the write() method

Note that analogWrite of PWM on pins associated with the timer are disabled when the first servo is attached.
Timers are seized as needed in groups of 12 servos - 24 servos use two timers, 48 servos will use four.
The sequence used to sieze timers is defined in timers.h
The methods are:

Servo - Class for manipulating servo motors connected to Arduino pins.
attach(pin ) - Attaches a servo motor to an i/o pin.
attach(pin, min, max ) - Attaches to a pin setting min and max values in microseconds
default min is 544, max is 2400
write() - Sets the servo angle in degrees. (invalid angle that is valid as pulse in microseconds is treated as microseconds) writeMicroseconds() - Sets the servo pulse width in microseconds
read() - Gets the last written servo pulse width as an angle between 0 and 180.
readMicroseconds() - Gets the last written servo pulse width in microseconds. (was read_us() in first release)
attached() - Returns true if there is a servo attached.
detach() - Stops an attached servos from pulsing its i/o pin.
*/
\#ifndef Servo_h
\#define Servo_h
\#include <inttypes.h>
/*

* Defines for 16 bit timers used with Servo library
* 
* If _useTimerX is defined then TimerX is a 16 bit timer on the curent board
* timer16_Sequence_t enumerates the sequence that the timers should be allocated
* _Nbr_16timers indicates how many 16 bit timers are available.

```
*
*/
// Say which 16 bit timers can be used and in what order
#if defined(__AVR_ATmega1280__) || defined(__AVR_ATmega2560__)
#define _useTimer5
#define _useTimer1
#define _useTimer3
#define _useTimer4
typedef enum { _timer5, _timer1, _timer3, _timer4, _Nbr_16timers } timer16_Sequence_t ;
#elif defined(__AVR_ATmega32U4__)
#define _useTimer3
#define _useTimer1
typedef enum {_timer3, _timer1, _Nbr_16timers } timer16_Sequence_t ;
#elif defined(__AVR_AT90USB646__) || defined(__AVR_AT90USB1286__)
#define _useTimer3
#define _useTimer1
typedef enum {_timer3,_timer1, _Nbr_16timers } timer16_Sequence_t ;
#elif defined(__AVR_ATmega128__)||defined(__AVR_ATmega1281__)|defined(__AVR_ATmega2561__)
#define _useTimer3
#define _useTimer1
typedef enum {_timer3,_timer1, _Nbr_16timers } timer16_Sequence_t ;
#else // everything else
#define _useTimer1
typedef enum { _timer1,_Nbr_16timers } timer16_Sequence_t ;
#endif
#define Servo_VERSION 2 // software version of this library
#define MIN_PULSE_WIDTH 544 // the shortest pulse sent to a servo
#define MAX_PULSE_WIDTH 2400 // the longest pulse sent to a servo
#define DEFAULT_PULSE_WIDTH 1500 // default pulse width when servo is attached
#define REFRESH_INTERVAL 20000 // minumim time to refresh servos in microseconds
#define SERVOS_PER_TIMER 12 // the maximum number of servos controlled by one timer
#define MAX_SERVOS (_Nbr_16timers * SERVOS_PER_TIMER)
#define INVALID_SERVO 255 // flag indicating an invalid servo index
typedef struct {
    uint8_t nbr :6; // a pin number from 0 to 63
    uint8_t isActive :1; // true if this channel is enabled, pin not pulsed if false
} ServoPin_t ;
typedef struct {
    ServoPin_t Pin;
    unsigned int ticks;
} servo_t;
class Servo
{
public:
    Servo();
```

```
uint8_t attach(int pin); // attach the given pin to the next free channel, sets pinMode, returns channel number or 0 if
failure
    uint8_t attach(int pin, int min, int max); // as above but also sets min and max values for writes.
    void detach();
    void write(int value); // if value is < 200 its treated as an angle, otherwise as pulse width in microseconds
    void writeMicroseconds(int value); // Write pulse width in microseconds
    int read(); // returns current pulse width as an angle between 0 and 180 degrees
    int readMicroseconds(); // returns current pulse width in microseconds for this servo (was read_us() in first release)
    bool attached(); // return true if this servo is attached, otherwise false
private:
    uint8_t servolndex; // index into the channel data for this servo
    int8_t min; // minimum is this value times 4 added to MIN_PULSE_WIDTH
    int8_t max; // maximum is this value times 4 added to MAX_PULSE_WIDTH
};
```

\#endif

## Servo.cpp

Servo.cpp - Interrupt driven Servo library for Arduino using 16 bit timers- Version 2
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Lesser General Public License for more details.

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License along with this library; if not, write to the Free Software
Foundation, Inc., 51 Franklin St, Fifth Floor, Boston, MA 02110-1301 USA
*/
/*

A servo is activated by creating an instance of the Servo class passing the desired pin to the attach() method. The servos are pulsed in the background using the value most recently written using the write() method

Note that analogWrite of PWM on pins associated with the timer are disabled when the first servo is attached. Timers are seized as needed in groups of 12 servos - 24 servos use two timers, 48 servos will use four.

The methods are:

Servo - Class for manipulating servo motors connected to Arduino pins.
attach(pin ) - Attaches a servo motor to an i/o pin.
attach(pin, min, max ) - Attaches to a pin setting min and max values in microseconds
default min is 544 , max is 2400
write() - Sets the servo angle in degrees. (invalid angle that is valid as pulse in microseconds is treated as microseconds) writeMicroseconds() - Sets the servo pulse width in microseconds
read() - Gets the last written servo pulse width as an angle between 0 and 180.
readMicroseconds() - Gets the last written servo pulse width in microseconds. (was read_us() in first release)
attached() - Returns true if there is a servo attached.
detach() - Stops an attached servos from pulsing its i/o pin.

## */

\#include <avr/interrupt.h>
\#include <WProgram.h>
\#include "Servo.h"
\#define usToTicks(_us) (( clockCyclesPerMicrosecond()*_us) / 8) // converts microseconds to tick (assumes prescale of 8) // 12 Aug 2009
\#define ticksToUs(_ticks) (( (unsigned)_ticks * 8)/ clockCyclesPerMicrosecond() ) // converts from ticks back to microseconds
\#define TRIM_DURATION $2 \quad / /$ compensation ticks to trim adjust for digitalWrite delays // 12 August 2009
//\#define NBR_TIMERS (MAX_SERVOS / SERVOS_PER_TIMER)

```
static servo_t servos[MAX_SERVOS]; // static array of servo structures
static volatile int8_t Channel[_Nbr_16timers ]; // counter for the servo being pulsed for each timer (or -1 if refresh
interval)
uint8_t ServoCount = 0; // the total number of attached servos
// convenience macros
#define SERVO_INDEX_TO_TIMER(_servo_nbr) ((timer16_Sequence_t)(_servo_nbr / SERVOS_PER_TIMER)) // returns the timer
controlling this servo
#define SERVO_INDEX_TO_CHANNEL(_servo_nbr) (_servo_nbr % SERVOS_PER_TIMER) // returns the index of the servo on
this timer
#define SERVO_INDEX(_timer,_channel) ((_timer*SERVOS_PER_TIMER) + _channel) // macro to access servo index by timer
and channel
#define SERVO(_timer,_channel) (servos[SERVO_INDEX(_timer,_channel)]) // macro to access servo class by timer and
channel
#define SERVO_MIN() (MIN_PULSE_WIDTH - this->min * 4) // minimum value in uS for this servo
#define SERVO_MAX() (MAX_PULSE_WIDTH - this->max * 4) // maximum value in uS for this servo
/************ static functions common to all instances ***********************/
static inline void handle_interrupts(timer16_Sequence_t timer, volatile uint16_t *TCNTn, volatile uint16_t* OCRnA)
{
if(Channel[timer] < 0 )
    *TCNTn = 0; // channel set to -1 indicated that refresh interval completed so reset the timer
    else{
    if( SERVO_INDEX(timer,Channel[timer]) < ServoCount && SERVO(timer,Channel[timer]).Pin.isActive == true )
        digitalWrite( SERVO(timer,Channel[timer]).Pin.nbr,LOW); // pulse this channel low if activated
}
    Channel[timer]++; // increment to the next channel
if( SERVO_INDEX(timer,Channel[timer]) < ServoCount && Channel[timer] < SERVOS_PER_TIMER) {
    *OCRnA = *TCNTn + SERVO(timer,Channel[timer]).ticks;
    if(SERVO(timer,Channel[timer]).Pin.isActive == true) // check if activated
        digitalWrite( SERVO(timer,Channel[timer]).Pin.nbr,HIGH); // its an active channel so pulse it high
}
    else {
    // finished all channels so wait for the refresh period to expire before starting over
    if( (unsigned)*TCNTn < (usToTicks(REFRESH_INTERVAL) + 4) ) // allow a few ticks to ensure the next OCR1A not missed
        *OCRnA = (unsigned int)usToTicks(REFRESH_INTERVAL);
    else
        *OCRnA = *TCNTn + 4; // at least REFRESH_INTERVAL has elapsed
    Channel[timer] = -1; // this will get incremented at the end of the refresh period to start again at the first channel
}
}
#ifndef WIRING // Wiring pre-defines signal handlers so don't define any if compiling for the Wiring platform
// Interrupt handlers for Arduino
#if defined(_useTimer1)
SIGNAL (TIMER1_COMPA_vect)
{
    handle_interrupts(_timer1, &TCNT1, &OCR1A);
}
#endif
#if defined(_useTimer3)
SIGNAL (TIMER3_COMPA_vect)
```

```
{
    handle_interrupts(_timer3, &TCNT3, &OCR3A);
}
#endif
#if defined(_useTimer4)
SIGNAL (TIMER4_COMPA_vect)
{
    handle_interrupts(_timer4, &TCNT4, &OCR4A);
}
#endif
#if defined(_useTimer5)
SIGNAL (TIMER5_COMPA_vect)
{
    handle_interrupts(_timer5, &TCNT5, &OCR5A);
}
#endif
#elif defined WIRING
// Interrupt handlers for Wiring
#if defined(_useTimer1)
void Timer1Service()
{
    handle_interrupts(_timer1, &TCNT1, &OCR1A);
}
#endif
#if defined(_useTimer3)
void Timer3Service()
{
    handle_interrupts(_timer3, &TCNT3, &OCR3A);
}
#endif
#endif
static void initISR(timer16_Sequence_t timer)
{
#if defined (_useTimer1)
    if(timer == _timer1) {
    TCCR1A = 0; // normal counting mode
    TCCR1B =_BV(CS11); // set prescaler of 8
    TCNT1 = 0; // clear the timer count
#if defined(__AVR_ATmega8__)| | defined(__AVR_ATmega128__)
    TIFR |= _BV(OCF1A); // clear any pending interrupts;
    TIMSK |= _BV(OCIE1A) ; // enable the output compare interrupt
#else
    // here if not ATmega8 or ATmega128
    TIFR1 |= BV(OCF1A); // clear any pending interrupts;
    TIMSK1 |= _BV(OCIE1A) ; // enable the output compare interrupt
#endif
#if defined(WIRING)
    timerAttach(TIMER1OUTCOMPAREA_INT, Timer1Service);
#endif
    }
#endif
#if defined (_useTimer3)
```

```
if(timer == _timer3) {
    TCCR3A = 0; // normal counting mode
    TCCR3B =_BV(CS31); // set prescaler of 8
    TCNT3 = 0; // clear the timer count
#if defined(__AVR_ATmega128__)
    TIFR |=_BV(OCF3A); // clear any pending interrupts;
        ETIMSK |= _BV(OCIE3A); // enable the output compare interrupt
#else
    TIFR3 = _BV(OCF3A); // clear any pending interrupts;
    TIMSK3 = _BV(OCIE3A) ; // enable the output compare interrupt
#endif
#if defined(WIRING)
    timerAttach(TIMER3OUTCOMPAREA_INT, Timer3Service); // for Wiring platform only
#endif
    }
#endif
#if defined (_useTimer4)
    if(timer == _timer4) {
        TCCR4A = 0; // normal counting mode
        TCCR4B = _BV(CS41); // set prescaler of 8
        TCNT4 = 0; // clear the timer count
        TIFR4 = _BV(OCF4A); // clear any pending interrupts;
        TIMSK4 = _BV(OCIE4A); // enable the output compare interrupt
}
#endif
#if defined (_useTimer5)
    if(timer == _timer5) {
        TCCR5A = 0; // normal counting mode
        TCCR5B =_BV(CS51); // set prescaler of 8
        TCNT5 = 0; // clear the timer count
        TIFR5 = _BV(OCF5A); // clear any pending interrupts;
        TIMSK5 = _BV(OCIE5A) ; // enable the output compare interrupt
}
#endif
}
static void finISR(timer16_Sequence_t timer)
{
    //disable use of the given timer
#if defined WIRING // Wiring
    if(timer == _timer1) {
        #if defined(__AVR_ATmega1281__)||defined(__AVR_ATmega2561__)
        TIMSK1 &= ~_BV(OCIE1A) ; // disable timer 1 output compare interrupt
    #else
    TIMSK &= ~_BV(OCIE1A) ; // disable timer 1 output compare interrupt
    #endif
    timerDetach(TIMER1OUTCOMPAREA_INT);
}
else if(timer == _timer3) {
    #if defined(__AVR_ATmega1281__)||defined(__AVR_ATmega2561__)
    TIMSK3 &= ~_BV(OCIE3A); // disable the timer3 output compare A interrupt
    #else
    ETIMSK &= ~_BV(OCIE3A); // disable the timer3 output compare A interrupt
    #endif
    timerDetach(TIMER3OUTCOMPAREA_INT);
}
```

```
#else
    //For Arduino - in future: call here to a currently undefined function to reset the timer
#endif
}
static boolean isTimerActive(timer16_Sequence_t timer)
{
// returns true if any servo is active on this timer
for(uint8_t channel=0; channel < SERVOS_PER_TIMER; channel++) {
    if(SERVO(timer,channel).Pin.isActive == true)
        return true;
}
return false;
}
/****************** end of static functions *****************************/
Servo::Servo()
{
if( ServoCount < MAX_SERVOS) {
    this->servoIndex = ServoCount++; // assign a servo index to this instance
        servos[this->servolndex].ticks = usToTicks(DEFAULT_PULSE_WIDTH); // store default values -12 Aug 2009
}
else
    this->servoIndex = INVALID_SERVO ; // too many servos
}
uint8_t Servo::attach(int pin)
{
    return this->attach(pin, MIN_PULSE_WIDTH, MAX_PULSE_WIDTH);
}
uint8_t Servo::attach(int pin, int min, int max)
{
    if(this->servoIndex < MAX_SERVOS ) {
    pinMode( pin, OUTPUT) ; // set servo pin to output
    servos[this->servolndex].Pin.nbr = pin;
    // todo min/max check: abs(min - MIN_PULSE_WIDTH) /4 < 128
    this->min =(MIN_PULSE_WIDTH - min)/4; //resolution of min/max is 4 uS
    this->max = (MAX_PULSE_WIDTH - max)/4;
    // initialize the timer if it has not already been initialized
    timer16_Sequence_t timer = SERVO_INDEX_TO_TIMER(servolndex);
    if(isTimerActive(timer) == false)
        initISR(timer);
    servos[this->servolndex].Pin.isActive = true; // this must be set after the check for isTimerActive
}
return this->servolndex;
}
void Servo::detach()
{
    servos[this->servolndex].Pin.isActive = false;
    timer16_Sequence_t timer = SERVO_INDEX_TO_TIMER(servoIndex);
    if(isTimerActive(timer) == false) {
        finISR(timer);
    }
}
```

```
void Servo::write(int value)
{
if(value < MIN_PULSE_WIDTH)
{ // treat values less than 544 as angles in degrees (valid values in microseconds are handled as microseconds)
    if(value < 0) value = 0;
    if(value > 180) value = 180;
    value = map(value, 0, 180, SERVO_MIN(), SERVO_MAX());
}
this->writeMicroseconds(value);
}
void Servo::writeMicroseconds(int value)
{
    // calculate and store the values for the given channel
    byte channel = this->servolndex;
    if( (channel >= 0) && (channel < MAX_SERVOS) ) // ensure channel is valid
    {
    if(value < SERVO_MIN() ) // ensure pulse width is valid
        value = SERVO_MIN();
    else if( value > SERVO_MAX() )
        value = SERVO_MAX();
        value = value - TRIM_DURATION;
    value = usToTicks(value); // convert to ticks after compensating for interrupt overhead - 12 Aug 2009
    uint8_t oldSREG = SREG;
    cli();
    servos[channel].ticks = value;
    SREG = oldSREG;
}
}
int Servo::read() // return the value as degrees
{
    return map( this->readMicroseconds()+1, SERVO_MIN(), SERVO_MAX(), 0, 180);
}
int Servo::readMicroseconds()
{
    unsigned int pulsewidth;
    if( this->servolndex != INVALID_SERVO )
        pulsewidth = ticksToUs(servos[this->servoIndex].ticks) + TRIM_DURATION ; // 12 aug 2009
    else
    pulsewidth = 0;
    return pulsewidth;
}
bool Servo::attached()
{
    return servos[this->servoIndex].Pin.isActive ;
}
```


## User Task



```
User_task.h
//**************************************************************************************
/** \file user_task.h
    * This file contains a task class for running a user interface for the motor
* controller. It has a single-state task which just reads the serial port to see if
* the user typed anything
*
* Revisions:
* \li 02-06-2012 Created generic switch cases
* \li 03-26-2012 Header file accepted by Arduino
* \li 04-17-2012 Constructor with pointers accepted in Arduino
* \li 05-02-2012 Added functions to be used with Master_task
*
* License:
* This program is intended for fingerspelling use with The Smith-Kettlewell Eye
* Research Institute robotic hand, but it is not limited thereto.
*/
//****************************************************************************************
/// This define prevents this .h file from being included more than once in a .cc file
#ifndef_USER_TASK_H_
#define _USER_TASK_H_
#include <stdlib.h>
#include <stdint.h>
#if defined(ARDUINO) && ARDUINO >= 100
    #include "Arduino.h"
#else
    #include "WProgram.h"
    #include <pins_arduino.h>
#endif
//---------------------------------------------------------------------------------
/** This class contains a task which...
    */
class user_task //: public stl_task
{
    // This protected data can only be accessed from this class or its descendents
    protected:
            bool valid;
            bool next;
            uint8_t letter;
            uint8_t state;
            char input_char;
        public:
            // The constructor creates a new task object
            user_task ();
            // The run method is where the task actually performs its function
            void run (void);
            //This function will display an introduction in the serial monitor
            void intro(void);
            // This function is a flag to see if a valid letter was received
            bool got_letter(void);
            // This function returns the current letter received
            uint8_t input_letter(void);
            // This function clears the input variables
```

```
    void reset(void);
    // This function tells user when to get the next letter
    void get_next_letter(void);
};
#endif // _TASK_USER_H
```

```
User_task.cpp
//**************************************************************************************
/** \file user_task.cpp
* This file tells the master file what letters (A-Z) are to be formed by accepting
* input from the user. It also allows the user to modify the delay between letters.
*
* Revisions
* \li 02-06-2012 Created generic switch cases
* \li 03-26-2012 Header file accepted by Arduino
* \li 04-17-2012 Constructor with pointers accepted in Arduino
* \li 05-02-2012 Added functions to be used with Master_task
*
* License:
* This program is intended for fingerspelling use with The Smith-Kettlewell Eye
* Research Institute robotic hand, but it is not limited thereto.
*/
//**************************************************************************************
#include <stdlib.h>
#include <stdint.h>
#include "user_task.h"
#if defined(ARDUINO) && ARDUINO >= 100
    #include "Arduino.h"
#else
    #include "WProgram.h"
    #include <pins_arduino.h>
#endif
```



```
/** This constructor creates a user interface task object. It checks if the user has
    * typed a command at the serial port and if so tells the servos what to do.
    */
user_task::user_task ()//(task_timer& a_timer, time_stamp& t_stamp)
    //: stl_task (a_timer, t_stamp)
{
    letter = 0;
    state = 0;
    valid = false;
    next= false;
    input_char = 0;
}
```



```
/** This is the function which runs when it is called by the master file. */
void user_task::run (void)
{
    // There's no switch statement because this task only does one thing all the time:
    // check for a character, and perform a command
    if(state ==0)
    {
        state = 1;
        intro();
    }
    else if (state == 1)
    {
        if (Serial.available()>0)
```

```
    {
        input_char = Serial.read();
        state = 2;
    }
}
else if (state ==2)
{
    switch (input_char)
    {
        // Pressing the '+' key increases finger-spelling speed
        case ('+'):
        case ('='):
            Serial.print("\nIncreasing speed\n");
            valid = true;
            letter = 26;
            state = 3;
            break;
// Pressing the '-' key decreases finger-spelling speed
case ('_'):
case ('-'):
    Serial.print("\nDecreasing speed\n");
    valid = true;
    letter = 27;
    state = 3;
    break;
// Pressing the 'space' key provides a space between letters
case (' '):
            Serial.print(" ");
            valid = true;
            letter = 28;
            state = 3;
            break;
// Pressing the '0' key disconnects all servos
case ('0'):
            Serial.print("\nDetach servos\n");
            valid = true;
            letter = 29;
            state = 3;
            break;
// Pressing the '1' connects all servos for use
case ('1'):
            Serial.print("\nAttach servos\n");
            valid = true;
            letter = 30;
            state = 3;
            break;
// Pressing the 'A' key forms the corresponding letter of the alphabet
case ('A'):
case ('a'):
    Serial.print("A");
    valid = true;
    letter = 0;
    state = 3;
    break;
// Pressing the 'B' key forms the corresponding letter of the alphabet
case ('B'):
case ('b'):
    Serial.print("B");
```

```
    valid = true;
    letter = 1;
    state = 3;
    break;
// Pressing the 'C' key forms the corresponding letter of the alphabet
case ('C'):
case ('c'):
    Serial.print("C");
    valid = true;
    letter = 2;
    state = 3;
    break;
// Pressing the 'D' key forms the corresponding letter of the alphabet
case ('D'):
case ('d'):
    Serial.print("D");
    valid = true;
    letter = 3;
    state = 3;
    break;
// Pressing the 'E' key forms the corresponding letter of the alphabet
case ('E'):
case ('e'):
    Serial.print("E");
    valid = true;
    letter = 4;
    state = 3;
    break;
// Pressing the 'F' key forms the corresponding letter of the alphabet
case ('F'):
case ('f'):
    Serial.print("F");
    valid = true;
    letter = 5;
    state = 3;
    break;
// Pressing the 'G' key forms the corresponding letter of the alphabet
case ('G'):
case ('g'):
    Serial.print("G");
    valid = true;
    letter = 6;
    state = 3;
    break;
// Pressing the 'H' key forms the corresponding letter of the alphabet
case ('H'):
case ('h'):
    Serial.print("H");
    valid = true;
    letter = 7;
    state = 3;
    break;
// Pressing the 'l' key forms the corresponding letter of the alphabet
case ('I'):
case ('i'):
    Serial.print("I");
    valid = true;
    letter = 8;
```

state = 3;
break;
// Pressing the 'J' key forms the corresponding letter of the alphabet case ('J'):
case ('j'):
Serial.print("J");
valid = true;
letter = 9;
state = 3;
break;
// Pressing the ' $K$ ' key forms the corresponding letter of the alphabet case ('K'):
case ('k'):
Serial.print("K");
valid = true;
letter = 10;
state $=3$;
break;
// Pressing the 'L' key forms the corresponding letter of the alphabet case ('L'):
case ('I'):
Serial.print("L");
valid = true;
letter = 11;
state $=3$;
break;
// Pressing the ' M ' key forms the corresponding letter of the alphabet case (' M '):
case ('m'):
Serial.print(" M ");
valid = true;
letter = 12;
state $=3$;
break;
// Pressing the ' N ' key forms the corresponding letter of the alphabet case ('N'):
case (' $n$ '):
Serial.print("N");
valid = true;
letter = 13;
state $=3$;
break;
// Pressing the 'O' key forms the corresponding letter of the alphabet case ('O'):
case ('o'):
Serial.print("O");
valid = true;
letter = 14;
state $=3$;
break;
// Pressing the 'P' key forms the corresponding letter of the alphabet case ('P'):
case ('p'):
Serial.print("P");
valid = true;
letter = 15;
state $=3$;
break;
// Pressing the ' $Q$ ' key forms the corresponding letter of the alphabet case ('Q'):
case ('q'):
Serial.print("Q");
valid = true;
letter = 16;
state $=3$;
break;
// Pressing the 'R' key forms the corresponding letter of the alphabet case ('R'):
case ('r'):
Serial.print("R");
valid = true;
letter = 17;
state $=3$;
break;
// Pressing the 'S' key forms the corresponding letter of the alphabet case ('S'):
case ('s'):
Serial.print("S");
valid = true;
letter $=18$;
state $=3$;
break;
// Pressing the 'T' key forms the corresponding letter of the alphabet case ('T'):
case ('t'):
Serial.print("T");
valid = true;
letter = 19;
state $=3$;
break;
// Pressing the 'U' key forms the corresponding letter of the alphabet case ('U'):
case ('u'):
Serial.print("U");
valid = true;
letter = 20;
state $=3$;
break;
// Pressing the 'V' key forms the corresponding letter of the alphabet case ('V'):
case ('v'):
Serial.print("V");
valid = true;
letter = 21;
state $=3$;
break;
// Pressing the 'W' key forms the corresponding letter of the alphabet
case ('W'):
case ('w'):
Serial.print("W");
valid = true;
letter = 22;
state $=3$;
break;
// Pressing the ' $X$ ' key forms the corresponding letter of the alphabet case ('X'):

```
    case ('x'):
            Serial.print("X");
            valid = true;
            letter = 23;
            state = 3;
            break;
                // Pressing the 'Y' key forms the corresponding letter of the alphabet
                case ('Y'):
            case ('y'):
            Serial.print("Y");
            valid = true;
            letter = 24;
            state = 3;
            break;
                // Pressing the 'Z' key forms the corresponding letter of the alphabet
                    case ('Z'):
            case ('z'):
                    Serial.print("Z");
                valid = true;
                letter = 25;
                state = 3;
                break;
            // If the user types anything else, just ignore it
                default:
                    Serial.println("?");
                    state = 1;
            break;
        }
    }
    else if(state == 3)
    {
        if(next)
        {
            next = false;
            state = 1;
    }
    }
    return;
}
```

/** This function will display an introduction in the serial monitor*/
void user_task::intro(void)
\{
Serial.printIn("\nThe Smith-Kettlewell Eye Research Institute");
Serial.println("\tRobotic Fingerspelling Hand");
Serial.println("\nBy: Colby Dixon, Brian Fang, Trevor Wong");
Serial.printIn("Released: June 2012");
Serial.println("\nUser Commands:");
Serial.println("A-Z = Letter to finger-spell\n\"+\" = Increase Speed, \"-\" = Decrease speed");
\}
/** This function is a flag to see if a valid letter was received*/
bool user_task::got_letter(void)
\{
return valid;
\}

```
/** This function returns the current letter received*/
uint8_t user_task::input_letter(void)
{
        return letter;
}
/** This function clears the input variables*/
void user_task::reset(void)
{
    letter = 0;
    valid = false;
}
void user_task::get_next_letter(void)
{
    next = true;
}
```


## Motor Torque Code (EES)

## Formatted Equations:

Motor Torque
Fall '12
***********************************************************
-This program will determine the minimum amount of torque (oz-in) required of a motor when under a load. -If both weight and torque are known, the code can be modified to solve for gear ratios
*************************************************************

## Given Data:

$W_{L}=2[\mathrm{lb}]$ weight of load
$\mathrm{W}_{\mathrm{m}}=0.035$ [lb] weight of motor
$\mathrm{R}_{\mathrm{L}}=0.25$ [in] radius of load
$\mathrm{R}_{\mathrm{m}}=0.2$ [in] radius of motor
$g=386\left[i \mathrm{in} / \mathrm{s}^{2}\right]$ gravitational constant
Desired Kinematics
$\omega=\frac{\pi}{0.5[\mathrm{~s}]}$ desired angular velocity
$\alpha=\frac{\omega}{0.25[\mathrm{~s}]}$ desired angular acceleration

This segment of code will determine the total inertia for any one of the following setups: Direct Drive, Gears, Pulleys. -Note that two of the three must remain commented in $\}$
Direct Drive
$\mathrm{J}_{\mathrm{t}}=\mathrm{J}_{\mathrm{L}}+\mathrm{J}_{\mathrm{m}}$ total inertia
$\mathrm{J}_{\mathrm{L}}=\frac{\mathrm{W}_{\mathrm{L}} \cdot \mathrm{R}_{\mathrm{L}}{ }^{2}}{2 \cdot \mathrm{~g}}$ load inertia
$J_{m}=W_{m} \cdot \frac{R_{m}{ }^{2}}{2 \cdot g}$ motor inertia

## Torque

$T=J_{t} \cdot \alpha$ Torque in Ib-in
$T_{o z}=T \cdot 16$ [oz/16] Torque in oz-in

## Source Code:

## "Motor Torque Fall'12

-This program will determine the minimum amount of torque (oz-in) required of a motor when under a load. -If both weight and torque are known, the code can be modified to solve for gear ratios
"Given Data: "
$W_{-} L=2[\mathrm{lb}] \quad$ "weight of load"
W_m $=0.035[\mathrm{lb}] \quad$ "weight of motor"
R_L = $0.25[\mathrm{in}] \quad$ "radius of load"
R_m=0.20[in] "radius of motor"
$\mathrm{g}=386\left[\mathrm{in} / \mathrm{s}^{\wedge} 2\right] \quad$ "gravitational constant"

## "Desired Kinematics"

omega $=p i /(0.5[\mathrm{~s}]) \quad$ "desired angular velocity"
alpha = omega $/(0.25[\mathrm{~s}]) \quad$ "desired angular acceleration"
"This segment of code will determine the total inertia for any one of the following setups: Direct Drive, Gears, Pulleys. -Note that two of the three must remain commented in $\left\}^{\prime \prime}\right.$

## "Direct Drive"

J_t = J_L + J_m "total inertia"
$J \_L=\left(W \_L^{*} R \_L^{\wedge} 2\right) /\left(2^{*} g\right) \quad$ "load inertia"
J_m = W_m*R_m^2/(2*g) "motor inertia"
\{"Gears"
$N=2 \quad$ "gear ratio"
J_t = J_L/N^2 + J_m "total inertia"
$J_{-} L=\left(W_{-} L^{*} R_{-} L^{-} 2\right) /\left(2^{*} g\right) \quad$ "load inertia"
J_m = W_m*R_m^2/(2*g) "motor inertia"\}
\{"Pulleys"
R_i $=0.125[\mathrm{in}] \quad$ "pulley $I D$ "
R_o1 = $0.5[\mathrm{in}] \quad$ "pulley 10 OD "
R_o2 $=0.5[\mathrm{in}] \quad$ "pulley 20 OD "
R_o3 $=0.5[\mathrm{im}] \quad$ "pulley 30 OD "
$W_{-} p 1=0.3[\mathrm{lb}] \quad$ "weight of pulley 1 "
$W_{-}$p2 $=0.3[\mathrm{lb}] \quad$ "weight of pulley 2"
W_p3 $=0.3[\mathrm{lb}] \quad$ "weight of pulley 3"
$J_{-} t=\left(W_{-} L^{*} R \_L^{\wedge} 2\right) / g+J_{-} p 1+J_{-} p 2+J_{-} p 3 \quad$ "total inertia"
$J_{-} p 1=\left(W_{-} p 1 /\left(2^{*} g\right)\right){ }^{*}\left(R \_o 1^{\wedge} 2+R_{-} i^{\wedge} 2\right) \quad$ "pulley 1 inertia"
J_p2 $=\left(W_{1} p 2 /\left(2^{*} g\right)\right)^{*}\left(R \_o 2^{\wedge} 2+R \_i \wedge 2\right) \quad$ "pulley 2 inertia"
J_p3 $=\left(W_{-} p 3 /\left(2^{*} g\right)\right)^{*}\left(R-o 3^{\wedge} 2+R_{-} i^{\wedge} 2\right) \quad$ "pulley 3 inertia" $\}$
"Torque"

| $T=J t^{*}$ alpha | "Torque in Ib -in" |
| :--- | :--- |
| $\mathrm{T}^{T} \mathrm{oz}=\mathrm{T}^{*}(16[\mathrm{oz} / 16])$ | "Torque in oz-in" |

## 1988 Hand Anthropometric Excerpt



59-HAND LEAGIM MEASLRED
The length of the hand from the tip of digit 3 to the stylion landinark. This dinension was meacured diroctily during the survey with a poech sliding caliper. Sse Cordion, et al. (1989) pages 190-191.

Paired t-test corparisons of hand length frow the digitizer and from survey mearurement show that there is no significance difference between mean values for men ( $t=.51 \mathrm{df}=1002 \mathrm{p}=.610$ ), but that there is a significant difference between mean values for waran (tw-27.57 df=1303 $\mathrm{p}=.000$ ). This discrepancy may be due to the digitizing difficulties associatod with long finger nails, which are more comon anong women.


Illustration adapted fram Gordon, et al. (1989).

## 59-HDND LENGIIT YPASURED

## FENALES

| THE SLAMREY STATISTICS |  |  |
| :---: | :---: | :---: |
| Contmerivs |  | DNCAES |
| 18.07 | NEAN | 7.11 |
| 0.03 | SE(MEAN) | 0.01 |
| 0.98 | ST LEV: | 0.39 |
| 0.02 | SE(SD) | 0.01 |
| 14.90 | MINLMM | 5.87 |
| 21.50 | 1/2XIMM | 8.46 |
| Cozre. Of | Martation | 5.48 |
| SYMIEIRY | - EETA I | 0.20 |
| KUIRICSIS | -EEIA II | 3.15 |
| NMMERR OF | sumbects | 1304 |


| PERCBNIILES |  |  |
| :---: | :---: | :---: |
| CEAITMETEIS |  | Incoms |
| 15.94 | 15T | 6.28 |
| 16.18 | 2ND | 6.37 |
| 16.33 | 3RD | 6.43 |
| 16.53 | 51 H | 6.51 |
| 16.85 | 101H | 6.64 |
| 17.07 | 151H | 6.72 |
| 17.25 | 201\% | 6.79 |
| 17.40 | 25IH | 6.85 |
| 17.54 | 301H | 6.91 |
| 17.67 | 351H | 6.96 |
| 17.79 | 4OTH | 7.01 |
| 17.91 | 451H | 7.05 |
| 18.03 | 501\% | 7.10 |
| 18.15 | 551H | 7.15 |
| 18.28 | 601\% | 7.20 |
| 18.41 | 6514 | 7.25 |
| 18.55 | 7OIM | 7.30 |
| 18.70 | 751H | 7.36 |
| 18.87 | 801H | 7.43 |
| 19.08 | 851\% | 7.51 |
| 19.35 | 901H | 7.62 |
| 19.76 | 951H | 7.78 |
| 20.04 | 971H | 7.89 |
| 20.26 | 98TH | 7.98 |
| 20.61 | 997H | 8.11 |

MAIES


## PERCPNIIIES

| CEnTIMETERS |  | INCHES |
| :---: | :---: | :---: |
| 17.27 | 15 T | 6.80 |
| 17.50 | 2ND | 6.89 |
| 17.65 | 3FD | 6.95 |
| 17.85 | 5TH | 7.03 |
| 18.17 | 101\% | 7.15 |
| 18.39 | 15IH | 7.24 |
| 18.56 | 201H | 7.31 |
| 18.72 | 251H | 7.37 |
| 16.86 | 3014 | 7.42 |
| 18.99 | 351H | 7.47 |
| 19.11 | 4OTH | 7.52 |
| 19.23 | 45 TH | 7.57 |
| 19.35 | 501\% | 7.62 |
| 19.48 | 551\% | 7.67 |
| 19.60 | 6OIH | 7.72 |
| 19.74 | 65TH | 7.77 |
| 19.88 | 701\% | 7.83 |
| 20.03 | 751H | 7.89 |
| 20.21 | 801H | 7.96 |
| 20.41 | 851H | 8.04 |
| 20.68 | 901H | 8.14 |
| 21.09 | 95TH | 8.30 |
| 21.37 | 9714 | 8.41 |
| 21.57 | 98\%H | 8.49 |
| 21.90 | 991H | 8.62 |

## Hand Shapes



A


C


B


D




K


L


M


0


N


P


Q


S


R


T


U


W


V


X



Z (twist)

## Installation:

1. Go to the Arduino website and hit the Download tab, or follow this link http://arduino.cc/en/Main/Software
2. Download to your computer's OS.
3. Go to the download location and unzip the file
4. Locate the .exe and double click it.

Example:
C: \... \arduino-1.0.1-windows \arduino-1.0.1

## Uploading files to the Arduino:

1. Plug the USB into the Arduino before connecting it to the computer
2. Open Arduino.exe
3. File $\rightarrow$ Open $\rightarrow$ [file name].ino
4. Click the right arrow on the GUI to upload the file
( $\rightarrow$ 4

## Installing Arduino files to Arduino:

Tuning:
NOTE: The tuning program tunes one finger at a time. The tuning order is: thumb $\rightarrow$ index $\rightarrow$ middle $\rightarrow$ ring $\rightarrow$ pinky $\rightarrow$ wrist and loops back to the thumb.

1. First, loaded up the degrees ino to the Arduino.
2. Open terminal.exe
3. Engage the servos by pressing " $g$ ".
4. " 1 " will decrement the angle of the knuckle servo by 5 , which will bend the knuckle joint.
5. " 2 " will increment the angle of the knuckle servo by 5 , which will straighten the knuckle joint.
6. " 3 " will decrement the angle of the medial servo by 5 , which will bend the medial joint.
7. " 4 " will increment the angle of the medial servo by 5 , which will straighten the medial joint.
8. Record servo angle values that correspond with the angles in the \#defines in master_task.cpp
9. Press " + " to tune the next finger or "-" to tune the previous finger

## Hand Program:

WARNING: The transistor that controls the power does not have the heat sink properly attached due to space. Running the hand continuously for long periods of time will cause the transistor to die. It is best to run it at most 2 minutes and let it cool down. To let it cool down, you can press "1", " 0 " or the reset button. Even though when the hand is in the neutral position it is on, it is not drawing any power so the transistor will still cool down.

1. First, loaded up the matrix_test.ino to the Arduino.
2. Once program is uploaded, you can control the hand using the terminal or just run the demo.
3. To run demo, all you need to do is press the red demo button. The demo will spell through the alphabet then turn off for a minute to allow the transistor to cool down. Then reengage the servos and ready to use again.
4. To run real time, you will need to use the terminal.exe provided. In the textbox, you can type sentences or words and then press enter for the hand to do the commands. The lower box is for real time, so when you press a letter, the hand will immediately go to that letter.


Figure 28. Demo button to run the alphabet.


Figure 29. The box highlighted in blue is the Textbox for typing in sentences and words. The box highlighted in red is the Realtime box. When you enter a letter or command in here, the hand will do it immediately.

