

Research Article

Preparation and Characterization of Magnetic Mesoporous Bioactive Glass/Carbon Composite Scaffolds

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The magnetic Fe-MBG/C composite scaffolds with enhanced mechanical strength and multifunctionality have been successfully prepared. The study showed that the Fe-MBG/C composite scaffolds with the porosity of ca. 80% had interconnected macropores (200–500 μm) and mesopores (3.7–4.4 nm) and significantly enhanced the compressive strength compared to the pure MBG scaffolds. Importantly, the Fe-MBG/C composite scaffolds exhibited good bioactivity and sustained drug release property. At the same time, the Fe-MBG/C composite scaffolds could generate heat to raise the temperature of surrounding environment in an alternating magnetic field due to their superparamagnetic behavior. Therefore, the magnetic Fe-MBG/C composite scaffolds could form a multifunctional platform with bone regeneration, magnetic hyperthermia, and local drug delivery and have more potential for use in the regeneration of the critical-sized bone defects caused by bone tumors.

1. Introduction

Mesoporous bioactive glass (MBG), as a bioactive material, has drawn growing interest in bone regeneration in recent years [1, 2]. As a result of its high specific surface area, large pore volume, and mesoporous structure, MBG exhibits the enhanced bone-forming bioactivity, degradation and drug delivery properties, compared to the conventional bioactive glass (BG) [3–10].

In order to repair large bone defects, the scaffolds mimicking the three-dimensional (3D) tissue structure have been considered as the most promising solution, because ideal 3D scaffolds with a highly interconnected macroporous network facilitate cell migration, proliferation, nutrients delivery, bone ingrowth, and eventually vascularization [11–13]. To date, many efforts have been made to develop 3D MBG scaffolds for large bone regeneration [14–25]. For example, Yun et al. synthesized the hierarchically mesoporous-macroporous 3D BG scaffolds by combining sol-gel, double polymers templating, and rapid prototyping technique, and the MBG

scaffolds exhibited better in vitro bioactivity compared to the normal BG scaffolds [14, 15]. We have successfully prepared the CaO-SiO₂-P₂O₅ MBG scaffolds by a combination of polyurethane sponge and PI23 surfactant as cotemplates and evaporation-induced self-assembly (EISA) process [17, 18]. The results indicated that the chemical compositions influenced the apatite forming ability and cell attachment [17]. Wu et al. used the same strategy to prepare the iron, boron, strontium, copper, and cobalt-containing CaO-SiO₂-P₂O₅ MBG scaffolds for bone tissue engineering [19–23].

However, major drawback of the above mentioned MBG scaffolds is low mechanical strength due to their brittle characteristic. Therefore, the composite scaffolds of MBG and other components are being developed with the aim of increasing the mechanical strength. For example, Wu et al. prepared silk-modified MBG scaffolds by coating silk on the pore walls surfaces [26]. The results indicated that silk modification did not change the interconnected pore network and improved mechanical strength (250 KPa) and BMSC proliferation and differentiation. We proposed

a strategy to incorporate zirconium (Zr) into the CaO-SiO₂-P₂O₅ MBG scaffolds, and the Zr-incorporated MBG scaffolds enhanced the compressive strength (214 KPa) and also exhibited a better physiochemical and biological properties [27]. Other researchers focused on the preparation of the MBG/polymer composite scaffolds [28–31]. Yun et al. prepared the MBG/PCL composite scaffolds by using rapid prototyping technique [28]. The combination of MBG and PCL brings about a significant enhancement of the molding capacity, mechanical property, and in vitro bone-forming bioactivity of the scaffolds compared to the pure PCL scaffolds. Li et al. and Su et al. reported the preparation of MBG/polycaprolactone (PCL) and MBG/polyamide composite scaffolds by using a solvent-casting-particulate-leaching method, respectively [29, 30]. But this method was difficult to control the mechanical stability and both the structure and interconnectivity of pores, which may limit their application in terms of cell migration in tissue engineering.

It has been demonstrated that carbon composites have great prospect in bone repair field due to the excellent mechanical property, especially their elastic modulus close to that of human bones [32]. Furthermore, carbon materials are biocompatible and had been applied widely to clinic. For example, the carbon materials made by isothermal chemical vapor infiltration had represented as artificially heart valve materials with the highest level [33]. On the other hand, carbon materials, such as carbon nanotubes and carbon fibers, are often used to reinforce the mechanical characteristics of bioceramics [34, 35]. For example, Boccaccini et al. reported the coating of 3D porous Bioglass scaffolds with multiwalled carbon nanotubes (CNTs), and the presence of CNTs enhanced the mechanical strength of the scaffolds [35]. We hypothesized that the formation of MBG/C composite scaffolds would enhance the mechanical strength and, at the same time, would not influence the mesoporous structure and bioactivity of the MBG scaffolds. As far as we know there are no reports on the development of the MBG/C composite scaffolds with enhanced mechanical strength for bone regeneration.

On the other hand, many research groups have tried to design magnetic bioactive composites to repair bone defects caused by bone tumors, such as magnetic bioactive glass ceramics, CaP ceramics and composites [36–43]. Magnetic bioactive composites can be used for hyperthermia in an alternating magnetic field to destroy the tumor cells, because cancer cells generally perish around 43°C due to hemorrhage, stasis, and vascular occlusion, whereas normal cells are not damaged until higher temperature [41, 42]. At the same time, the bioactive matrices could induce bone regeneration. Recently, we reported a type of magnetic Fe₃O₄-CaO-SiO₂-P₂O₅ MBG scaffolds, which formed a potential multifunctional platform, combining bone regeneration, magnetic hyperthermia, and local drug delivery [43]. However, their low mechanical strength (ca. 64 kPa) was similar to that of the conventional CaO-SiO₂-P₂O₅ MBG scaffolds [17–23].

In this study, we proposed an improved strategy to prepare magnetic MBG/C composite scaffolds with enhanced mechanical strength by polyurethane (PU) sponge

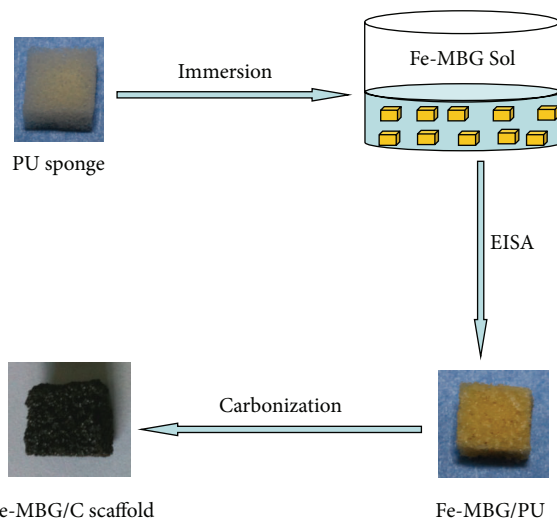


FIGURE 1: The schematic procedure for the preparation of the Fe-MBG/C composite scaffolds.

templating method and the carbonization process. As shown in Figure 1, the first step involved the preparation of Fe-containing MBG (Fe-MBG) sol using P123 as structure-directing agent and the immersion of PU sponges in the Fe-MBG sol. In the next step, the PU sponges adsorbed with Fe-MBG sol could form the Fe-MBG/PU composite scaffolds after evaporation-induced self-assembly (EISA) process. Finally, magnetic Fe-MBG/C composite scaffolds were obtained after the carbonization under argon atmosphere. To the best of our knowledge, reports on such strategy to prepare magnetic MBG/C composite scaffolds have not been found before.

2. Experimental Methods

2.1. Preparation of Magnetic Fe-MBG/C Composite Scaffolds. Magnetic Fe-MBG/C composite scaffolds were prepared following our previously reported method after some modification [17, 31]. As an example, to prepare magnetic Fe-MBG/C composite scaffolds containing 10% Fe (10Fe-MBG/C), typically 4.0 g of P123 (Mw = 5800, Aldrich), 6.7 g of tetraethyl orthosilicate (TEOS, 98%, Acros), 0.47 g of calcium nitrate (Ca (NO₃)₂·4H₂O), 1.08 g of ferric chloride hexahydrate (FeCl₃·6H₂O), 0.73 g of triethyl phosphate (TEP, 99.8%, Sigma-Aldrich), and 1.0 g of 0.5 M HCl were dissolved in 60 g ethanol and stirred at room temperature for 1 day (molar ratio of Fe : Ca : Si : P = 10 : 5 : 80 : 5). Afterwards, the PU sponges (20ppi, Shanghai Zhengyang) were completely immersed into the sol for 10 min and transferred to a petri dish to squeeze out the excess sol. After evaporating the solution for 12 h at room temperature, the same procedure was repeated for 8 times. When the samples were completely dry, they were carbonized at 700°C (ramp of 2°C/min) under argon atmosphere for 6 h to obtain 10Fe-MBG/C composite scaffolds. The MBG/C composite scaffolds without Fe (0Fe-MBG/C) and with 5% Fe (5Fe-MBG/C) were prepared by the same method. The chemical compositions and the amounts

TABLE 1: Chemical composition and the amounts of the reagents of different MBG sol solutions.

Sample names	Molar ratio Fe : Ca : Si : P	P123 (g)	TEOS (g)	Ca(NO ₃) ₂ ·4H ₂ O (g)	FeCl ₃ ·6H ₂ O (g)	TEP (g)	0.5 M HCl (g)	C ₂ H ₅ OH (g)
0Fe-MBG	0 : 15 : 80 : 5	4	6.7	1.40	0	0.73	1.0	60
5Fe-MBG	5 : 10 : 80 : 5	4	6.7	0.94	0.54	0.73	1.0	60
10Fe-MBG	10 : 5 : 80 : 5	4	6.7	0.47	1.08	0.73	1.0	60

of reagents used to prepare different Fe-MBG sol solutions are listed in Table 1.

The wide angle X-ray diffraction (WAXRD) patterns were obtained on a Stoe Stadi P powder diffractometer equipped with a curved germanium (III) monochromator and linear PSD using Cu K α 1 radiation (1.5405 Å) in transmission geometry. Scanning electron microscopy (SEM) was carried out with a FEI Quanta 450 field emission scanning electron microscope. Transmission electron microscopy (TEM) was performed with a JEM-2010 UHR electron microscope operated at an acceleration voltage of 200 kV. N₂ adsorption-desorption isotherms were obtained on a Quadrasorb SI automated surface area and pore size analyzer at -196°C under continuous adsorption condition. Brunauer-Emmett-Teller (BET) and Barrett-Joyner-Halenda (BJH) methods were used to determine the surface area, the pore volume, and the pore size distribution. Magnetic measurement was performed using a vibrating sample magnetometer (VSM).

2.2. Porosity and Mechanical Strength of Magnetic Fe-MBG/C Composite Scaffolds. The porosity of magnetic Fe-MBG/C scaffolds was measured using Archimedes' principle: magnetic MBG/C scaffolds with a size of 5 × 5 × 5 mm were used for the measurement, and water was used as liquid medium. The porosity (P) was calculated according to the following formulation $P = (W_{\text{sat}} - W_{\text{dry}})/(W_{\text{sat}} - W_{\text{sus}}) \times 100\%$, where W_{dry} is the dry weight of magnetic Fe-MBG/C scaffolds, W_{sus} is the weight of magnetic MBG/C scaffolds suspended in water, and W_{sat} is the weight of magnetic MBG/C scaffolds saturated with water.

The compressive strength of the 5 × 5 × 5 mm sized magnetic Fe-MBG/C scaffolds was tested using a Zwick static materials testing machine (5 kN) at a cross head speed of 0.5 mm/min.

2.3. Apatite Formation of Magnetic Fe-MBG/C Composite Scaffolds in Simulated Body Fluids. To investigate the apatite formation ability of magnetic MBG/C scaffolds, simulated body fluid (SBF) was prepared and buffered at pH 7.4 with tris(hydroxymethyl)aminomethane [(CH₂OH)₃CNH₂] and hydrochloric acid (HCl) according to Kokubo's method [44]. Generally, magnetic Fe-MBG/C scaffolds were soaked in SBF solution in a polyethylene bottle at 37°C for different periods, and the ratio of the solution volume to the scaffold mass was 200 mL/g. After soaking, magnetic MBG/C scaffolds were collected from SBF solution, rinsed with ethanol, and dried. SEM observation was used to study the apatite formation on the surfaces of magnetic Fe-MBG/C scaffolds.

2.4. Cytotoxicity Evaluation of Magnetic Fe-MBG/C Composite Scaffolds. To investigate the cytotoxicity of magnetic Fe-MBG/C composite scaffolds, human bone mesenchymal stem cells (BMSCs) and MTT assay were used in this study. Isolation and culture of BMSCs were conducted following previously published protocols [22]. BMSCs were cultured on 5 × 5 × 5 mm scaffolds placed in 96-well culture plates, at an initial density of 1 × 10⁵ cells/scaffold. For the next 3 h, 100 μL of growth medium was carefully added to the base of the culture plate every 20 min, until there was enough growth medium to cover the scaffold. MTT assay was performed in triplicate according to the previous study protocol [23]. Briefly, three cell/scaffold constructs from each group (0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C) were cultured in growth medium for 1, 3, and 7 days. 40 μL of 0.5 mg/mL of MTT solution (Sigma-Aldrich) was added to each construct with 360 μL growth medium at each time point. After incubated for 4 h at 37°C, the medium was removed and the formazan product was solubilized in 200 μL of dimethyl sulfoxide (DMSO). An aliquot of 100 μL was taken from each well and transferred to a fresh 96-well plate. The absorbance was measured at $\lambda = 495$ nm on a microplate reader (SpectraMax, Plus 384, Molecular Devices, Inc., USA). All the results were demonstrated as the optical density values minus the absorbance of blank wells.

2.5. Magnetic Heating Property of Magnetic Fe-MBG/C Composite Scaffolds. For the magnetic heating experiment, a high frequency generator with 5 KW was used. The used inductor was a water-cooled copper coil with 11 turns on a length of 105 mm and a diameter of 42.5 mm. For measurement, an open topped vessel with a dispersion of magnetic Fe-MBG/C particles grinded from the scaffolds (150 mg/mL) was placed in the inductor. Whilst application of the alternating magnetic field, the temperature was monitored using a pyrometer that was placed above the inductor and focused on the dispersion surface. To obtain the heating curve of the magnetic Fe-MBG/C scaffolds, a reference measurement of the pure solvent (equivalent volume) was subtracted from the data.

2.6. Loading and In Vitro Release of Ibuprofen. Ibuprofen (IBU, 99%, Sigma-Aldrich) was used as a model drug to evaluate drug delivery property of magnetic Fe-MBG/C composites scaffolds in this study. Typically, 1.0 g of magnetic Fe-MBG scaffolds was immersed in 50 mL of IBU solution (40 mg/mL). After shaking on a shaking bed for 24 h, the IBU-loaded Fe-MBG/C composite scaffolds were separated

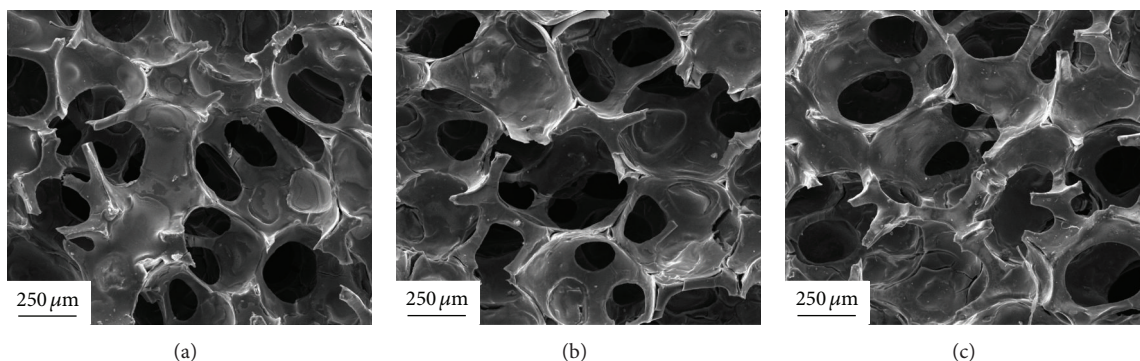


FIGURE 2: SEM images of the 0Fe-MBG/C (a), 5Fe-MBG/C (b), and 10Fe-MBG/C (c) composite scaffolds.

and dried in vacuum drying oven at 50°C for 48 h. The estimation of IBU loading in magnetic Fe-MBG/C composite scaffolds was carried out by measuring the absorbance values at 264 nm before and after loading [8]. Before determination, a calibration curve was recorded by taking absorbance versus IBU concentration between 0 and 2 mg/mL as parameters.

In vitro release of IBU from the drug-loaded Fe-MBG/C scaffolds was following the previous reported method after some modification [8]. The IBU-loaded Fe-MBG/C scaffolds (0.5 g) were placed in a cover-sealed plastic bottle within 50 mL of SBF solution, and the plastic bottle was fixed on shaking bed with a 50 ramp of shaking speed at 37°C. IBU release was determined by UV analysis. The release medium was withdrawn at the predetermined time intervals and replaced with fresh SBF solution each time. The extracted release medium was diluted with SBF and analyzed with a NanoDrop 2000C at the wavelength of 264 nm.

3. Results and Discussion

SEM images of the Fe-MBG/C composite scaffolds with different Fe content are shown in Figure 2. All three Fe-MBG/C composite scaffolds exhibited a highly porous structure with a comparable interconnected macropore size, ranging from 200 to 500 μm . Using Archimedes' principle, the porosities of the open pores were $80.0 \pm 2.4\%$, $78.1 \pm 3.0\%$, and $79.5 \pm 0.8\%$, for 0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C composite scaffolds, respectively. The results are similar to those of the previously reported MBG scaffolds [17–23], which suggested that the carbonization process could keep the interconnected macroporous structure of PU sponges. Previous studies demonstrated that the scaffold pores larger than 150 μm and high porosity facilitated cells' proliferation, vascular ingrowth, and internal mineralized bone formation [45, 46]. Therefore, from the viewpoint of porous structure, these prepared magnetic Fe-MBG/C composite scaffolds had suitable 3D macroporous structure for bone regeneration.

The WAXRD patterns of the Fe-MBG/C composite scaffolds with different Fe content are shown in Figure 3. A broad reflection at $2\theta = 15\text{--}30^\circ$ associated with amorphous carbon and silicate can be observed on all WAXRD patterns of the

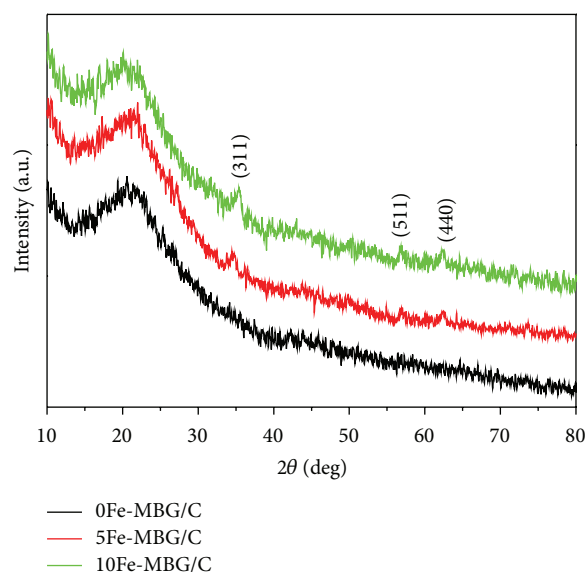


FIGURE 3: The WAXRD patterns of the Fe-MBG/C composite scaffolds with different Fe content.

Fe-MBG/C composite scaffolds. The 10Fe-MBG/C and 5Fe-MBG/C composite scaffolds exhibited weak and broad characteristic diffraction peaks of $\gamma\text{-Fe}_2\text{O}_3$ corresponding to the (311), (511), and (440) reflections, suggesting that very small $\gamma\text{-Fe}_2\text{O}_3$ nanocrystals have been formed in the Fe-MBG/C composite scaffolds. It might be attributed to the formation of $\gamma\text{-Fe}_2\text{O}_3$ from Fe^{3+} ions during the carbonization of the Fe-MBG/PU scaffolds. Generally, $\gamma\text{-Fe}_2\text{O}_3$ and Fe_3O_4 have the same spinel structure, and their XRD peak positions are quite close to each other. Previous studies demonstrated that Fe^{3+} ions in the polymeric frameworks could form $\gamma\text{-Fe}_2\text{O}_3$ nanocrystals, but not Fe_3O_4 nanocrystals, during the carbonization of the polymeric frameworks [47, 48].

Figure 4 shows TEM images of the Fe-MBG/C composite scaffolds with different Fe content. Each type of Fe-MBG/C composite scaffolds exhibited an ordered mesoporous structure, which was similar to those previously reported MBG powders and scaffolds [3–10, 17–25]. However, the $\gamma\text{-Fe}_2\text{O}_3$

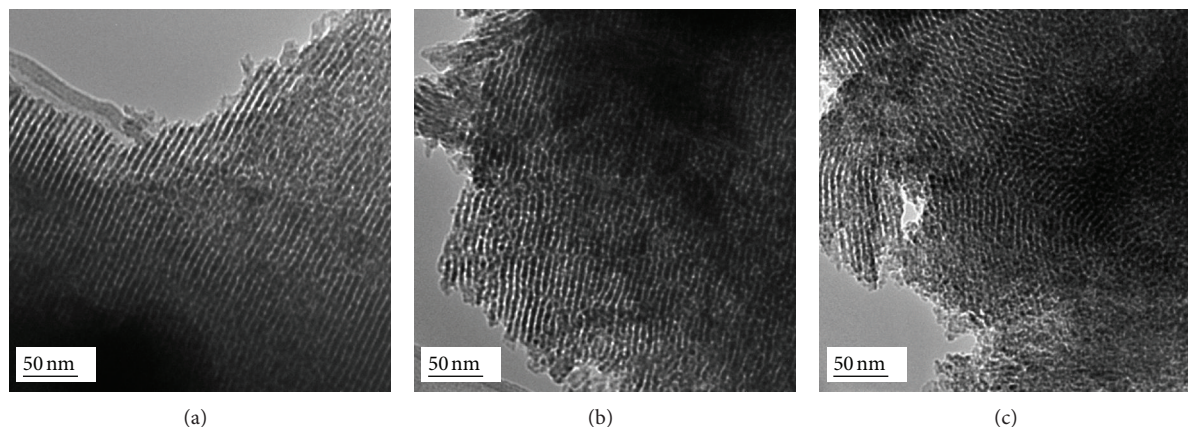


FIGURE 4: TEM images of the 0Fe-MBG/C (a), 5Fe-MBG/C (b), and 10Fe-MBG/C (c) composite scaffolds.

TABLE 2: Structural parameters and drug loading of the Fe-MBG/C and other MBG composite scaffolds.

Samples	S_{BET} (m^2/g)	V_p (cm^3/g)	D_p (nm)	Porosity (%)	Compressive strength (kPa)	Drug loading (%)	References
0Fe-MBG/C	254.4	0.248	4.4	80.0 ± 2.4	246.5 ± 69.6	16.2 ^a	/
5Fe-MBG/C	219.3	0.226	3.7	78.1 ± 3.0	284.9 ± 25.5	13.5 ^a	/
10Fe-MBG/C	189.7	0.189	3.9	79.5 ± 0.8	323.1 ± 77.5	12.6 ^a	/
MBG	327.3	0.357	4.07	88.6	52.8 ± 12.4	11.3 ^b	[24]
10Fe-MBG	268	/	4.5	82.9 ± 2.9	46 ± 5.4	12.5 ^c	[19]
5.0Silk-MBG	/	/	5.0	94.0	250	15.7 ^d	[26]
60% MBG/PCL	505 ^e	0.5 ^e	5.4 ^e	/	$9.3 \pm 3.9 \text{ MPa}^f$	/	[28]

^aibuprofen loading; ^bgentamicin loading; ^{c,d}dexamethasone loading; ^ethe surface area, pore volume, and pore size for MBG materials; ^f3D rapid prototyping technique for the fabrication of MBG/PCL scaffolds.

nanoparticles or aggregates in the 5Fe-MBG/C and 10Fe-MBG/C composite scaffolds cannot be clearly observed. It might be that the Fe^{3+} ions substituted the Ca^{2+} ions in the MBG framework during the sol-gel process and the carbonization under argon atmosphere but did not form the magnetic nanoparticles inside the channels, which are similar to the results reported by Gu et al. and Wu et al. [49, 50].

Figure 5 shows N_2 adsorption-desorption isotherms of the magnetic Fe-MBG/C composite scaffolds together with the corresponding pore size distributions. The data of the surface area, pore volume, and pore size are listed in Table 2. As shown in Figure 5(a), these Fe-MBG/C composite scaffolds exhibited the type IV isotherms, indicating the mesoporous structure. However, the magnetic Fe-MBG/C composite scaffolds showed a decrease in the N_2 adsorbed volume with the increase of Fe content, which suggested that the incorporation of $\gamma\text{-Fe}_2\text{O}_3$ could influence their BET surface area and pore volume. The specific surface areas of the 0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C composite scaffolds were 254.4, 219.3, and 189.7 m^2/g , respectively. The single point adsorption total volumes at $P/P_0 = 0.99$ were 0.248, 0.226, and 0.189 cm^3/g , respectively. It might be attributed to the decrease of the ordered degree of the magnetic Fe-MBG/C composite with increasing Fe content, because the

substitution of Fe for Ca in the Fe-MBG/C scaffolds may cause a large number of defects in the mesoporous framework due to the difference of valence and atom diameter. The results were similar to those of the doped MBG materials [20–25, 51, 52]. The pore size distributions in Figure 5(b) were calculated from the adsorption branches using the BJH model. These magnetic Fe-MBG/C composite scaffolds exhibited relatively narrow pore size distributions, and the peak pore radii of the 0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C composite scaffolds were 2.20, 1.85, and 1.95 nm, respectively. Therefore, these magnetic Fe-MBG/C composite scaffolds with high surface area, pore volume, and uniform mesoporous channels could be potential carriers for drug loading and delivery.

To determine the carbon content in the magnetic Fe-MBG/C composite scaffolds, thermogravimetric (TG) analysis was used in this study. As shown in Figure 6(a), each type of Fe-MBG/C composite scaffolds exhibited two weight losses. Weight losses below 200°C were the physical loss of water. Weight losses that occurred between 200 and 800°C were attributed to the carbon loss. Therefore, the carbon contents of the 0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C composite scaffolds could be estimated to be 9.43, 9.89, and 11.54%, respectively. As shown in Figure 6(b),

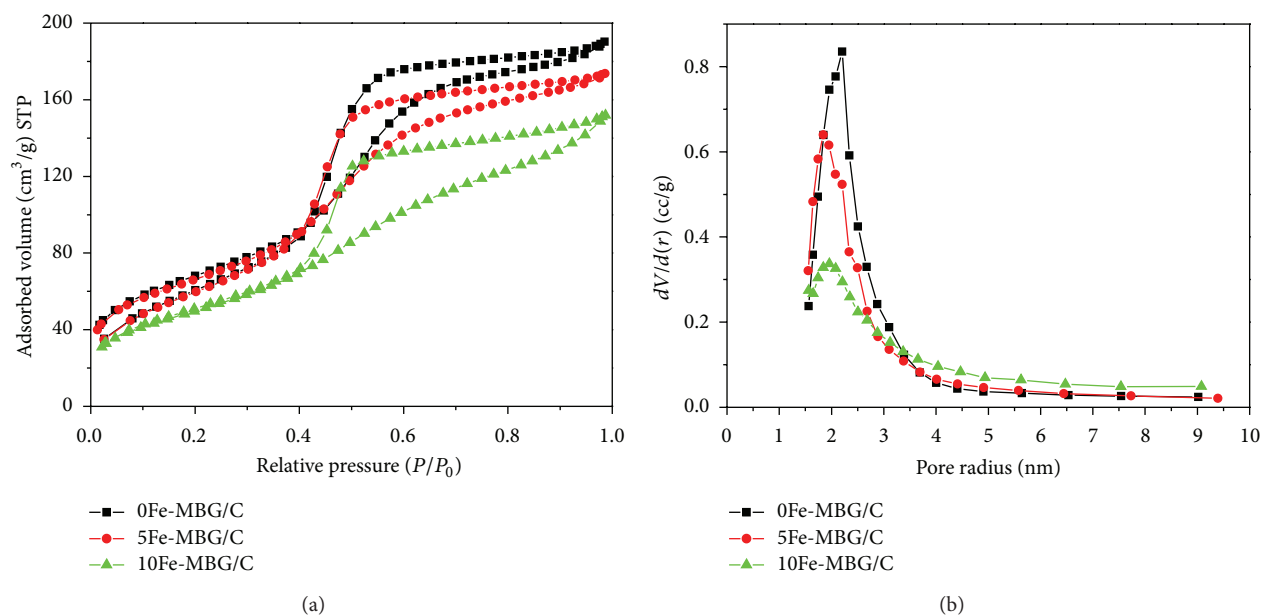


FIGURE 5: N_2 adsorption isotherms (a) and the corresponding pore size distributions (b) of different Fe-MBG/C composite scaffolds.

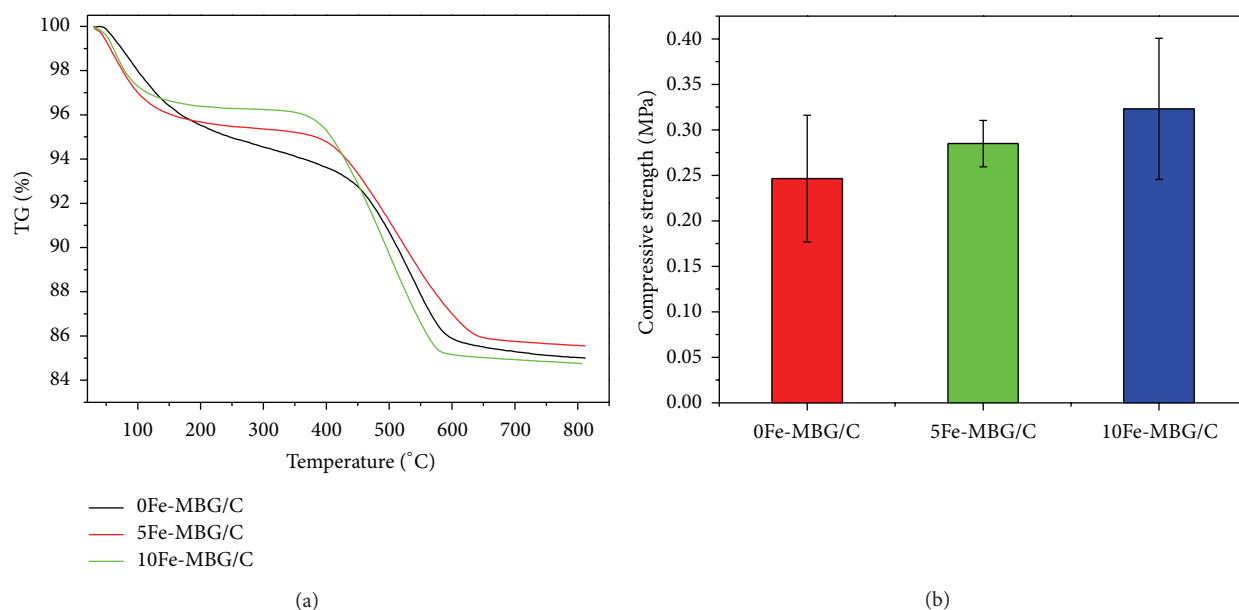


FIGURE 6: TG curves (a) and mechanical strength (b) of the Fe-MBG/C composite scaffolds with different Fe content.

the compressive strengths of the 0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C composite scaffolds were, respectively, estimated to be 246 ± 69.6 , 284 ± 25.5 , and 323 ± 77.5 KPa, which showed a significant enhancement in the compressive strength compared to the pure MBG and doped MBG scaffolds (ca. 55 kPa) [19–24], and were close to those of the silk modified MBG scaffolds (ca. 250 kPa) [26]. It might be that the carbon component played an important role in the enhancement of the mechanical strength for the Fe-MBG/C composite scaffolds. On the other hand, the Fe-substitution in the MBG network might also contribute to more stable

network for the MBG scaffold, because Fe^{3+} ions provide more bonding to Si and O network than Ca^{2+} ions.

The room temperature magnetization curves of the 0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C composite scaffolds are shown in Figure 7(a). The magnetization of the Fe-MBG/C composite scaffolds increased with increasing Fe content. The 0Fe-MBG/C composite scaffolds had no magnetization due to no magnetic component in the scaffolds. But the 5Fe-MBG/C and 10Fe-MBG/C composite scaffolds reached 0.73 and 1.32 emu/g at 25 K Oe, respectively. It also can be observed that there are almost no hysteresis

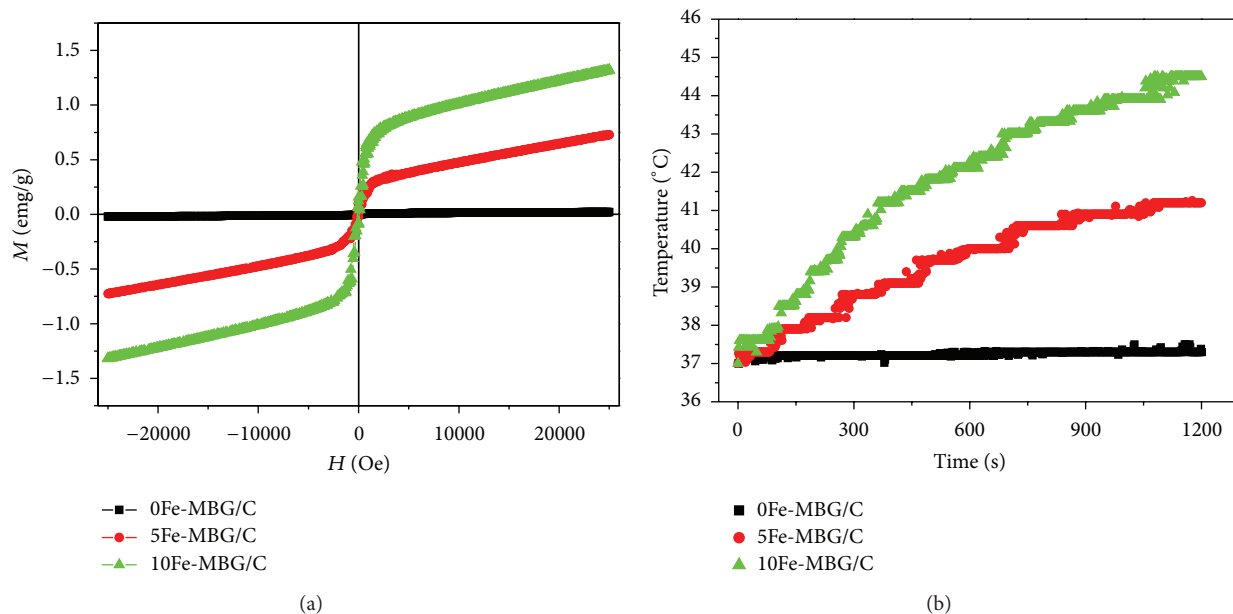


FIGURE 7: (a) Magnetization curves as a function of the applied magnetic field for different Fe-MBG/C composite scaffolds at room temperature; (b) magnetic heating curves of different Fe-MBG/C composite scaffolds in an alternating magnetic field.

loops (near-zero coercivity and remanence) for the 5Fe-MBG/C and 10Fe-MBG/C composite scaffolds, suggesting the superparamagnetic behavior of both Fe-MBG/C composite scaffolds because of the very small size of $\gamma\text{-Fe}_2\text{O}_3$ crystals, which were restrained by the MBG framework.

Regarding the magnetic heating properties of the Fe-MBG/C composite scaffolds, Figure 7(b) shows the temperature increases of the Fe-MBG/C composite scaffolds in an alternating magnetic field whose magnetic field strength and frequency were 1.86 kA/m and 200 kHz, respectively. It can be observed that the temperature of the 0Fe-MBG/C suspension experienced minimal variation, starting at 37 $^{\circ}\text{C}$ at the beginning of the magnetic field application and ending at 37.5 $^{\circ}\text{C}$ after the observation period. However, the temperatures of the 5Fe-MBG/C and 10Fe-MBG/C suspensions increased from 37 $^{\circ}\text{C}$ to 41.2 and 44.5 $^{\circ}\text{C}$ after measuring 20 min, respectively. The results indicated that the 5Fe-MBG/C and 10Fe-MBG/C composite scaffolds could generate heat to raise the temperature of the surrounding environment due to the delay in Neel relaxation of the magnetic moment in the composite scaffolds [53], allowing for magnetic hyperthermia application.

The bioactivity of the scaffold biomaterials is their ability to bond with living bone through the formation of an apatite layer on their surface both in vitro and in vivo [24]. Therefore, the apatite-forming ability is very important for magnetic Fe-MBG/C composite scaffolds. As shown in Figure 8, three Fe-MBG/C composite scaffolds had smooth surfaces before soaking in SBF solutions. However, it can be observed that a large amount of microparticles was deposited on the surfaces of three Fe-MBG/C composite scaffolds after soaking in SBF solutions for 3 days, which is similar to the previously reported formation of apatite particles on

the MBG powders and scaffolds [3–7, 14–25]. The results indicated that the magnetic Fe-MBG/C composite scaffolds are bioactive according to Kokubo's view [44].

The cytotoxicities of three Fe-MBG/C composite scaffolds were evaluated by cell viability assay. As shown in Figure 9, there was no discernible cytotoxicity for three Fe-MBG/C composite scaffolds, by the fact that all experimental groups had close values to those of the controls. With the increase of culture time, the cell numbers significantly increased on the Fe-MBG/C composite scaffolds. It indicated that these magnetic Fe-MBG/C composite scaffolds were biocompatible, allowing cell attachment, proliferation, and differentiation, further determining the bone formation and bonding.

To understand the drug delivery property of these magnetic Fe-MBG/C composite scaffolds, ibuprofen (IBU), an analgesic and anti-inflammatory drug with molecular size of $\approx 1.0 \times 0.6$ nm, was used as a model drug to introduce into the mesopores of the Fe-MBG/C composite scaffolds [54, 55], which might be useful for bone tissue regeneration. IBU loading efficiency (mass of IBU/mass of scaffolds) of the 0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C composite scaffolds was decreased with increasing Fe content and estimated to be 16.2%, 13.5%, and 12.6%, respectively (Table 2). Comparing the specific surface area, pore volume, and IBU loading efficiency of these Fe-MBG/C composite scaffolds, it can be suggested that the IBU loading efficiency was dependent on the specific surface area and pore volume of the scaffolds. The higher specific surface area and pore volume resulted in the higher loading efficiency. The release tests were performed in SBF solutions. As shown in Figure 10, three Fe-MBG/C composite scaffolds exhibited a similar sustained release behavior during the whole test period. The incorporation of $\gamma\text{-Fe}_2\text{O}_3$ into the MBG/C scaffolds did not change the

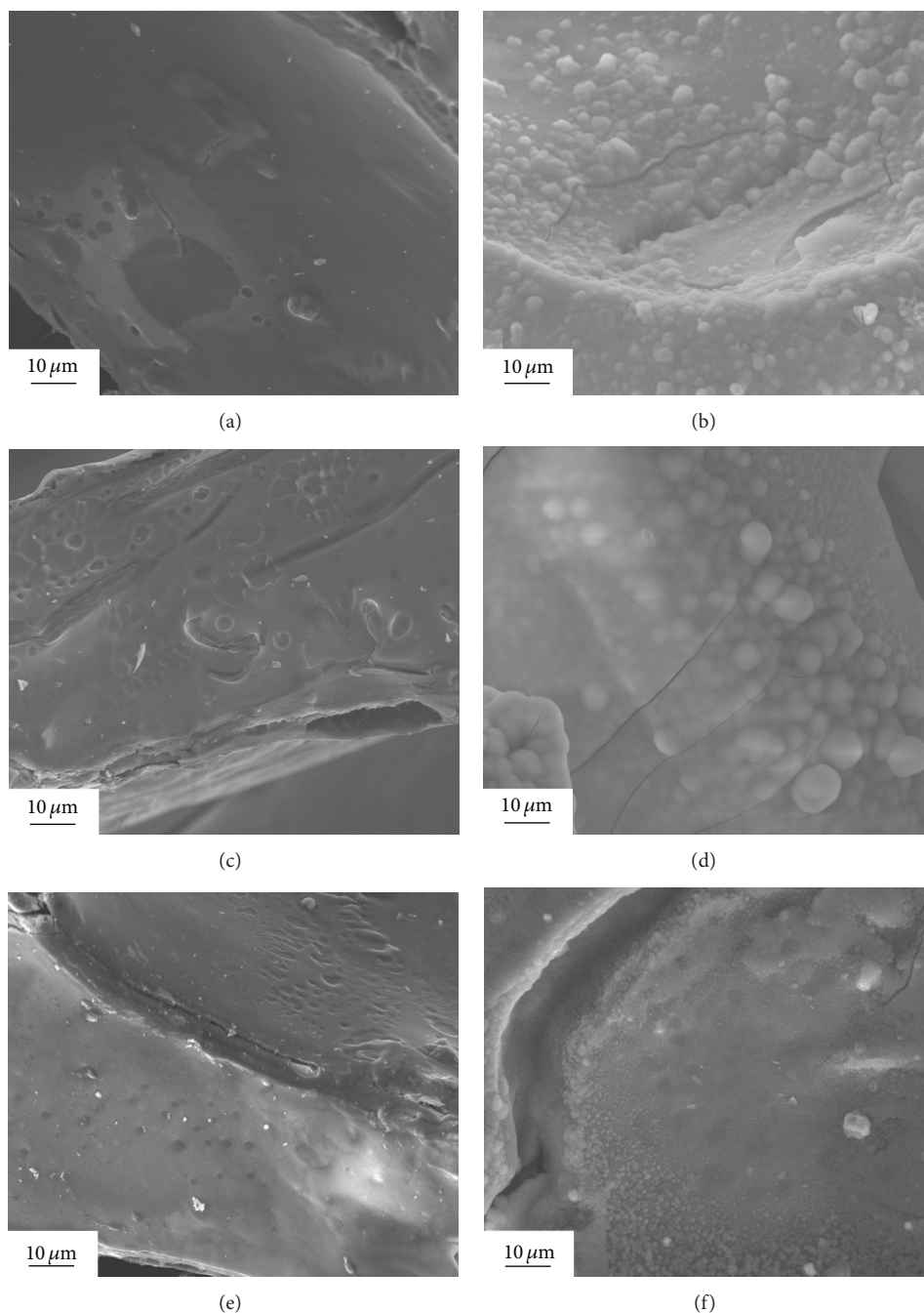


FIGURE 8: SEM images of the Fe-MBG/C composite scaffolds before (a, c, and e) and after (b, d, and f) soaking in SBF solutions for 3 days ((a) and (b) for the 0Fe-MBG/C scaffolds; (c) and (d) for the 5Fe-MBG/C scaffolds; (e) and (f) for the 10Fe-MBG/C scaffolds).

release kinetics of IBU, an initial fast release followed by a relatively slow release with increasing the release time. It is similar to those previously reported sustained drug release systems based on mesoporous silica and MBG materials due to the presence of mesoporous channels [8–10, 56, 57]. However, the release rates from these magnetic Fe-MBG/C composite scaffolds exhibited a little decrease with increasing Fe content, which is similar to the previously reported IBU release from the $\text{Fe}_3\text{O}_4\text{-CaO-SiO}_2\text{-P}_2\text{O}_5$ MBG composites by Li et al. [8]. Generally, the drug release from mesoporous

materials dominated by Fickian diffusion mechanism was dependent on the mesoporous structure, mesopore size, surface chemistry, and the release environment. In this study, the 0Fe-MBG/C, 5Fe-MBG/C, and 10Fe-MBG/C composite scaffolds had similar mesoporous structure, mesopore size, and surface chemistry. However, the ion dissolution rate of the Fe-MBG/C composite scaffolds decreased with increasing the Fe substitution due to the easier dissolution of Ca species than that of Fe species in SBF solution [8]. Therefore, the limited control of drug release was due to the limited change

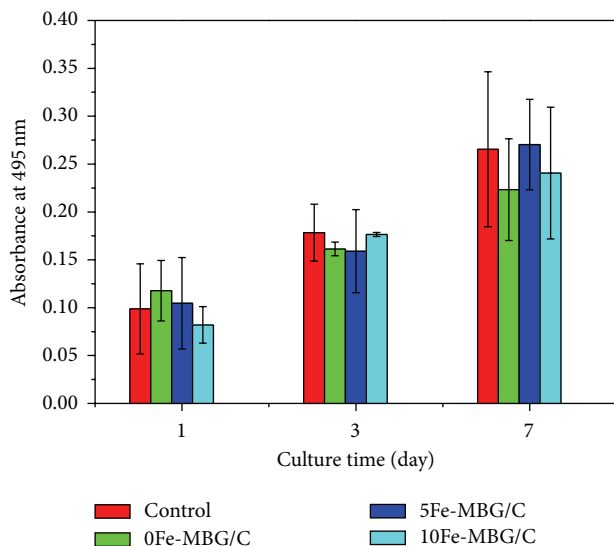


FIGURE 9: The cytotoxicities of the Fe-MBG/C composite scaffolds evaluated by MTT assay.

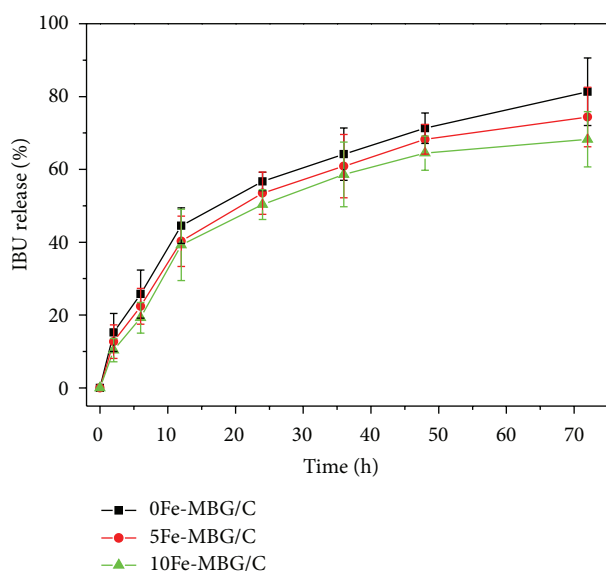


FIGURE 10: Ibuprofen release profiles from the Fe-MBG/C composite scaffolds with different Fe content.

of the ion dissolution rate of different Fe-MBG/C composite scaffolds during the release period. Wu et al. also reported that the faster dissolution rate of mesoporous SrO-SiO₂ particles contributed to the faster rate of dexamethasone (DEX) release [58]. Therefore, these magnetic Fe-MBG/C composite scaffolds have potential as a local sustained drug delivery system for bone regeneration.

4. Conclusions

The magnetic Fe-MBG/C composite scaffolds with enhanced mechanical strength and multifunctionality have been successfully prepared. The Fe-MBG/C composite scaffolds had

interconnected macropores of 200–500 μm and mesoporous walls with mesopores of ca. 3.7–4.4 nm and enhanced the compressive strength with four times compared to the MBG scaffolds with similar porosity due to the reinforcement of carbon component. The Fe-MBG/C composite scaffolds exhibited good bioactivity and sustained drug release property. Importantly, the Fe-MBG/C composite scaffolds were superparamagnetic and could generate heat in an alternating magnetic field for potential hyperthermia application. Therefore, the magnetic Fe-MBG/C composite scaffolds have potential for the regeneration of the critical-sized bone defects caused by bone tumors by a combination of magnetic hyperthermia and local drug delivery.

Acknowledgments

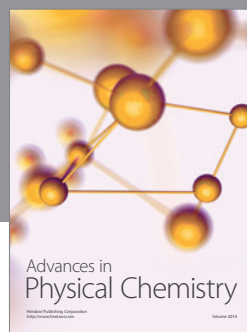
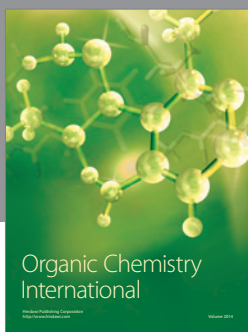
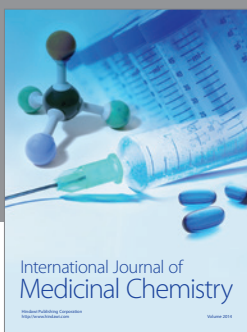
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