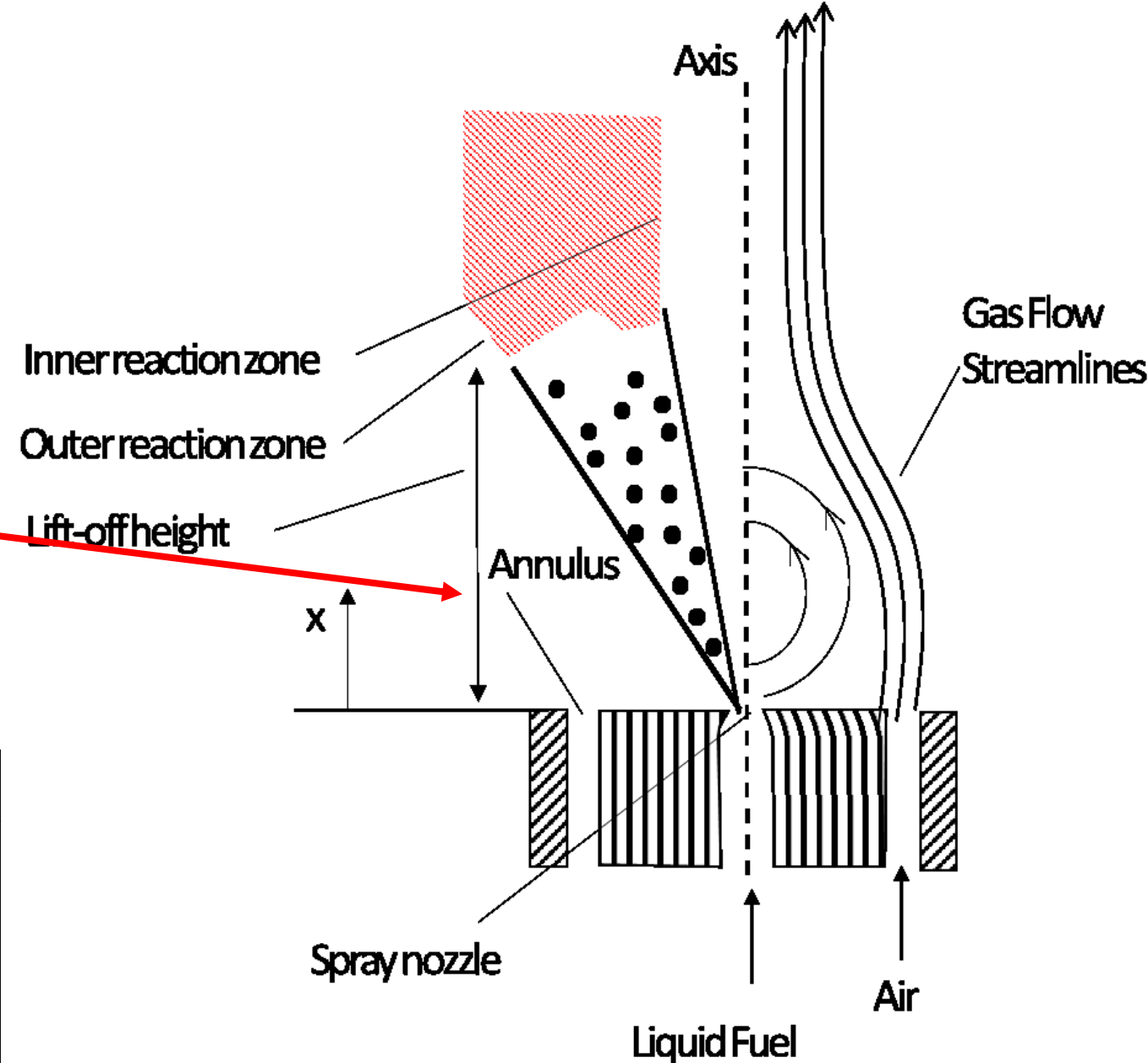
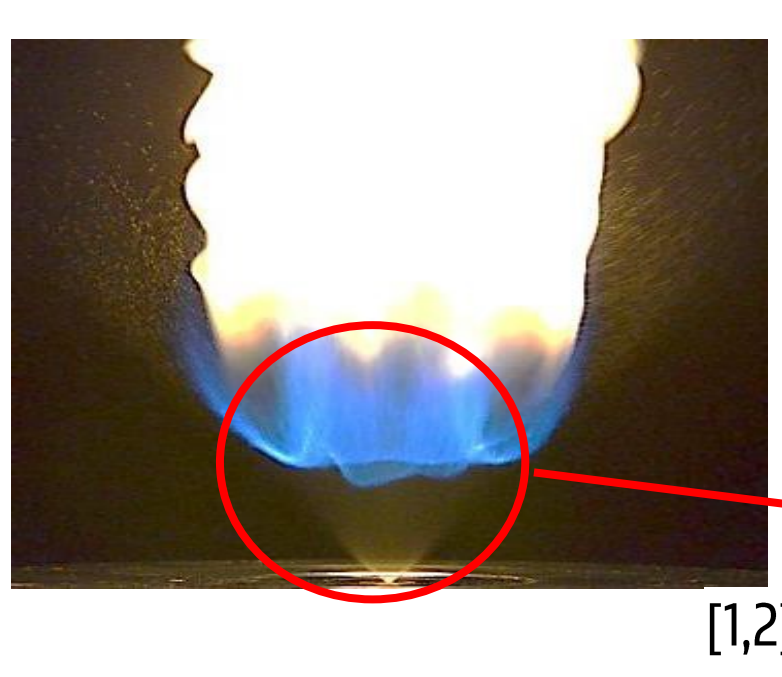


LES/CMC SIMULATION OF THE CORIA ROUEN SPRAY FLAME USING THE LAGRANGIAN POINT PARTICLE APPROACH

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1. Spray Lifted jet flame: challenges



Description of the experimental facility	
Inlet air conditions	6 g/s (T=298 K)
Inlet fuel conditions	0.28 g/s (T=298 K)
Injector orifice diameter	0.0002 m
Nozzle type	Simplex Fuel Injector
Spray angle	80°
Coflow jet type	Non-swirling
Inner coflow diameter	0.01m
Outer Coflow diameter	0.02 m
Reynolds Number	13000
Spray droplets size	[0.5-65 μm]

Challenges

- Spray modeling
- Evaporation → mixture fraction source term
- Micro-mixing → Scalar Dissipation Rate

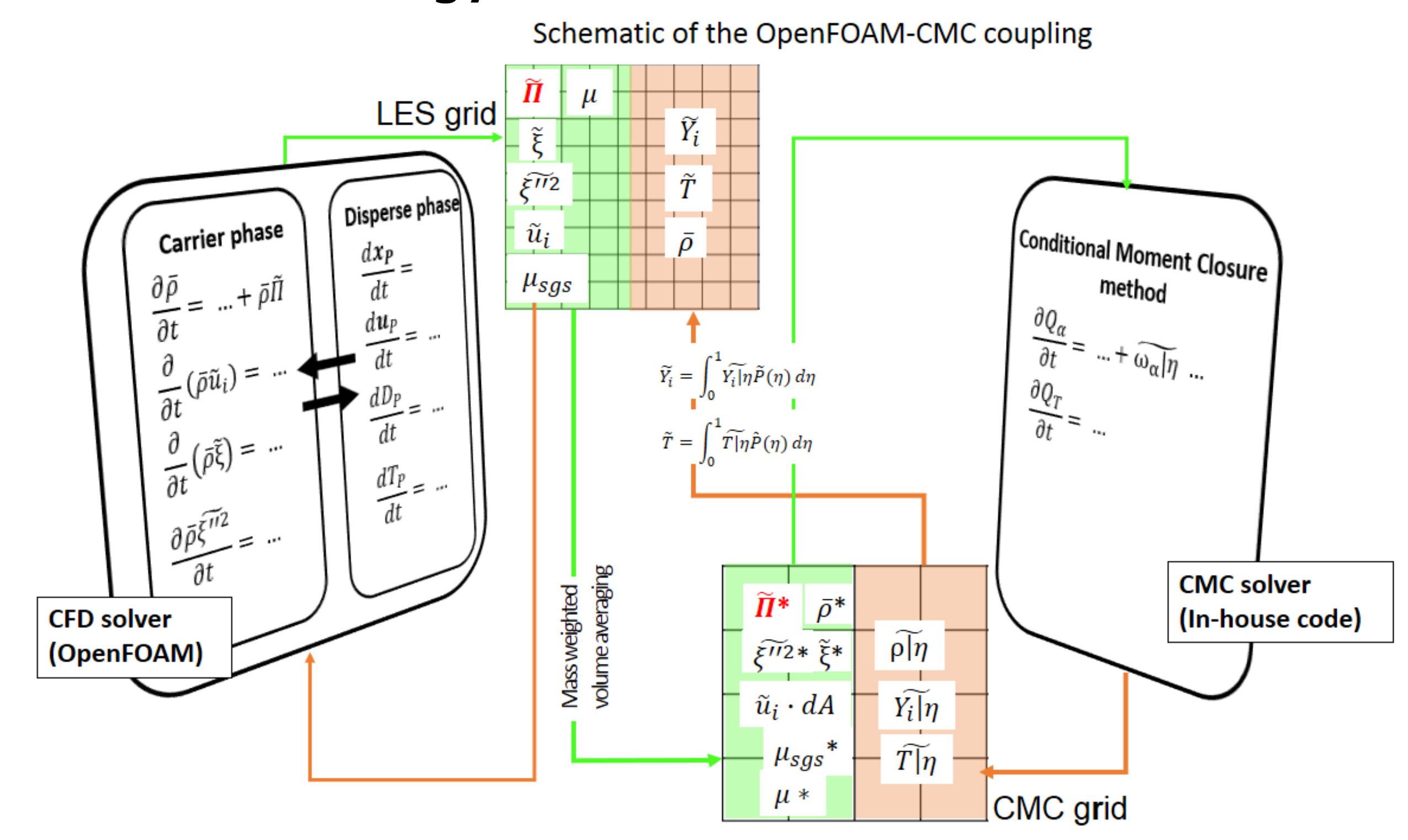
2. Conditional Moment Closure (CMC) for two phase flow [3,4]

- Mixture fraction based approach
- Fluctuations of mixture fraction ↔ Fluctuations of scalars (Y_α)
- $\eta \rightarrow$ sample space of mixture fraction (ξ)
- Transport equations are solved for conditionally filtered reacting scalars: $Q_\alpha = \overline{Y_\alpha | \eta}$

$$\frac{\partial Q_\alpha}{\partial t} = \overline{N | \eta} \frac{\partial^2 Q_\alpha}{\partial \eta^2} + \overline{w_\alpha | \eta} - \overline{u_i | \eta} \frac{\partial Q_\alpha}{\partial x_i} + \frac{\partial}{\partial x_i} \left(D_t \frac{\partial Q_\alpha}{\partial x_i} \right) + s(\overline{N | \eta})$$

- Diffusion in mixture fraction space
- Chemical source term
- Subgrid scale conditional flux
- Convection term
- Conditional spray source term (not include)

3. Numerical Strategy



Conclusions

In this WiPP a numerical study of the Coria Rouen spray flame using LES-CMC has been presented. Results reveal a good characterization of the discrete phase with some discrepancies in the flow field prediction both in the near nozzle region and far downstream. The simplified chemical mechanism adopted and/or the resolution of the grid size at the level both of the CMC and LES have been identified as possible causes of these discrepancies.

Future Work

- Inclusion spray source term
- Detailed chemical mechanism
- Mesh Refinement both in LES and CMC

References

- [1] F. Shum-Kivan, J. Marrero Santiago, A. Verdier, E. Riber, B. Renou, G. Cabot, B. Cuenot, Proceedings of the Combustion Institute, 2016.
- [2] A. Verdier, J. Marrero Santiago, A. Vandel, S. Saengkaew, G. Cabot, G. Grehan, B. Renou, Proceedings of the Combustion Institute, 2016.
- [3] A. Giusti, M. Kotzagianni, E. Mastorakos, Flow Turbulence Combustion, 97, 1165-1184, 2016.
- [4] P. Schroll, E. Mastorakos, Simulations of spark ignition of a swirling n-heptane spray flame with conditional moment closure, 48th AIAA, 2010, Orlando, Florida.

4. Computational details

LES

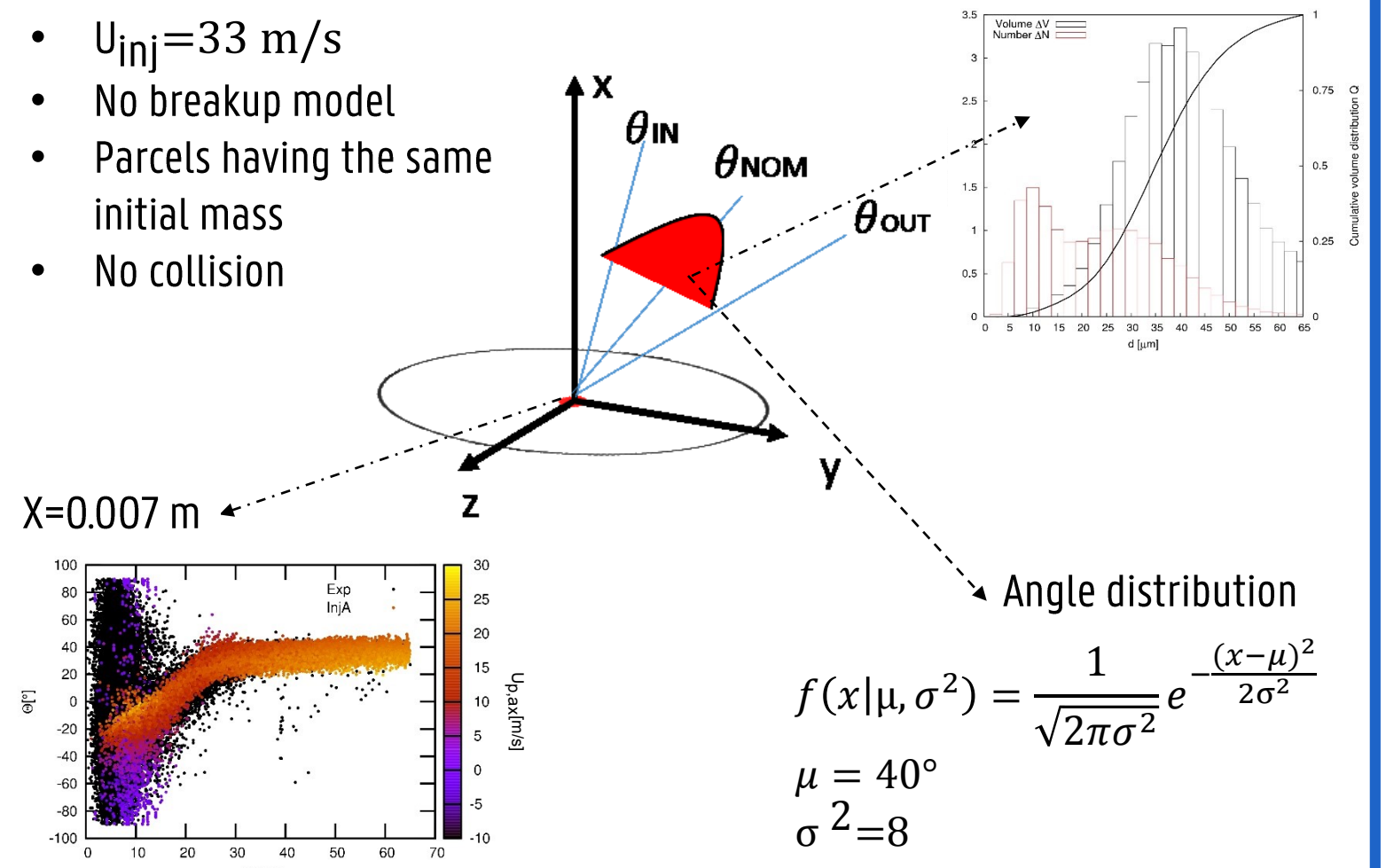
Mesh (cylindrical 0.24×0.26 m): 670000 cells
Parcels' number: 2 M/s

CMC

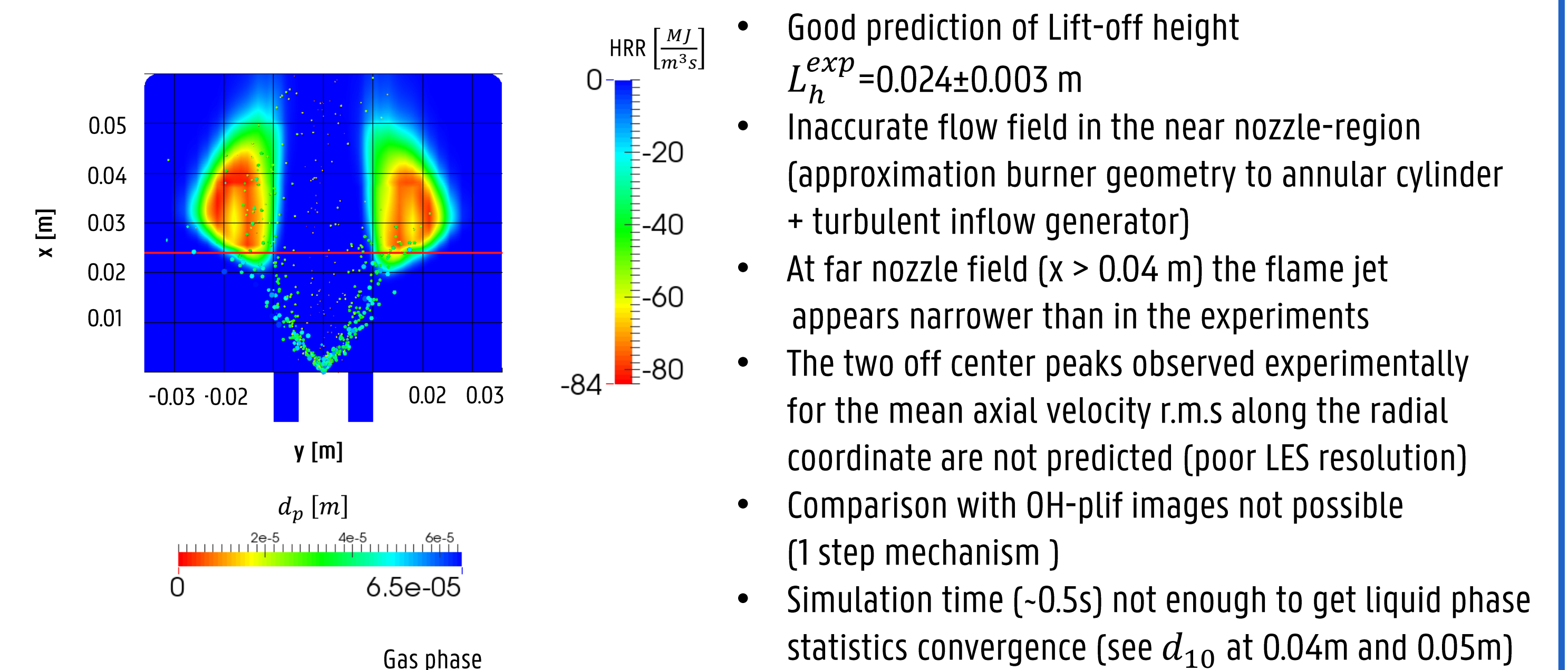
Mesh (cylindrical): 2880 cells
Mixture fraction space grid: 51 nodes
Chemical mechanism: single step
 $C_7H_{16} + 11O_2 \rightarrow 7CO_2 + 8H_2O$
 $q_c = A \exp\left(-\frac{E_a}{R_c T}\right) [C_7H_{16}]^{0.25} [O_2]^{1.5}$

5. Injection model

- $U_{inj} = 33$ m/s
- No breakup model
- Parcels having the same initial mass
- No collision



6. Results



- Good prediction of Lift-off height
 $L_h^{exp} = 0.024 \pm 0.003$ m
- Inaccurate flow field in the near nozzle-region (approximation burner geometry to annular cylinder + turbulent inflow generator)
- At far nozzle field ($x > 0.04$ m) the flame jet appears narrower than in the experiments
- The two off center peaks observed experimentally for the mean axial velocity r.m.s along the radial coordinate are not predicted (poor LES resolution)
- Comparison with OH-plif images not possible (1 step mechanism)
- Simulation time [-0.5s] not enough to get liquid phase statistics convergence (see d_{10} at 0.04m and 0.05m)

