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# Effect of Random Ethylene Comonomer on Relaxation of Flow-Induced Precursors in Isotactic Polypropylene

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#### Abstract

The effect of comonomer on structure and relaxation of flow-induced precursors was investigated in a series of isotactic polypropylene and random propylene–ethylene copolymers. The polymers were subjected to flow by fiber pulling and allowed to relax above their nominal melting temperature for specific times. The type of morphology developed after cooling revealed whether flow-induced precursors were still present or the melt had fully reequilibrated. Precursors were long-lived and, at fixed temperature, decayed significantly faster with higher ethylene content. The critical time for precursor relaxation followed an Arrhenius-type dependence with temperature. The apparent energy of activation for precursor dissolution decreased with increasing comonomer content, indicating that the rate-limiting step of the relaxation process becomes less difficult with higher ethylene fraction. This effect is attributed to ethylene co-units acting as disruptors of precursor structure and is discussed in terms of quasi-crystalline nature and characteristic chain stem length of precursor bundles.



#### 1. Introduction

Imposition of flow onto a polymer melt is well-known to have a tremendous impact on kinetics of crystallization, type of morphology that develops, and, consequently, final material properties. Flow-induced crystallization (FIC) can for instance trigger the formation of highly oriented crystallites and accelerate crystallization kinetics by orders of magnitude, resulting in an increase of the elastic modulus and tensile strength.<sup>1,2</sup> Most processing techniques of polymers involve the application of strong flows, so understanding the basic mechanism of FIC is key to optimizing the final material properties of a particular resin.

Flow-induced precursors are at the heart of flow-induced crystallization, but they are still not fully understood.<sup>3-19</sup> FIC oriented precursors are thought to be thread-like quasicrystalline structures that form in the melt during flow and which subsequently template the growth of oriented lamellae, thus dictating the final morphology.<sup>20,21</sup> The precursors themselves are difficult to probe directly because of their small dimensions and because they are typically present in dilute concentrations, which oftentimes renders them undetectable due to experimental sensitivity limits.<sup>22,23</sup> Nevertheless, FIC precursors have been detected directly with small-angle X-ray scattering (SAXS) and have also been correlated with an unusual upturn in birefringence during flow.<sup>10,24</sup> A different approach for studying precursors involves indirect detection: by tracking the development of oriented crystallites which are templated on precursors, the presence of FIC precursors can be inferred. Real-time optical and X-ray measurements as well as exsitu examination of the final morphology have been used to expose oriented morphologies that indirectly reveal FIC precursors.7,9,25,26 Other indirect approaches use rheological measurements or differential scanning calorimetry to follow the increased rates of crystallization associated with flow-induced precursors.13,17

FIC precursors are known to survive for long times at high temperatures even above the nominal melting temperature.7 Several studies have investigated the relaxation behavior of flow-induced precursors with the objective of revealing information about their structure and nature. Generally, it has been found that relaxation of FIC precursors follows an Arrhenius-type dependence with an apparent energy of activation that is much larger than the flow activation energy, so the rate-limiting step of relaxation is not controlled by the rheological processes in the melt.7-9,13,26-28 A few studies have probed FIC precursors as a function of processing conditions. Balzano et al. found that the imposed shear stress influenced the aspect ratio of oriented precursors of isotactic polypropylene (iPP) which, in turn, determined their stability at high temperatures.<sup>12</sup> Hamad and coworkers observed that FIC precursors created at increasing levels of specific work needed longer annealing times to fully decay.<sup>13</sup> Furthermore, above certain specific work, the stability of precursors saturated and their response to annealing was independent of flow conditions. Cavallo et al. also reported longer lifetimes for precursors that had formed at higher shear rates, but they established that the rate-determining step of precursor relaxation was unaffected by the level of applied shear rate.<sup>9</sup> Only a few studies have probed the role of molecular characteristics onto structure and relaxation of FIC precursors. For example, Azzurri et al. found that the relaxation time of precursors of both isotactic polystyrene (iPS) and isotactic polybutene (iPBu) increased with increasing molecular weight  $M_{wi}$ however, the rate-limiting step for relaxation of precursors did not depend on  $M_{\rm w}$  implying that the structure of precursors was unchanged by differences in length of the polymer chains.<sup>7,8</sup>

The effect of comonomer content on structure and relaxation of flowinduced precursors of a random polypropylene-ethylene polymer has not previously been explored. Random comonomers can lead to significant changes in the type of crystalline structure that develops, the rates of crystallization, and the final material properties. Specifically, the incorporation of random ethylene co-units onto isotactic polypropylene results in improved impact resistance and mechanical properties at low temperatures as well as increased transparency.<sup>29</sup> Random ethylene co-units act as defects and therefore hinder the process of crystallization under quiescent conditions, decreasing rate of crystallite growth, attainable degree of crystallinity, crystallization temperature, and melting temperature.<sup>30</sup> Also, the presence of ethylene co-units has been associated with the development of  $\gamma$ -phase in addition to the more common  $\alpha$ -morph due to an increased number of short crystallizable sequences.<sup>30,31</sup> Although early reports assumed that ethylene co-units were fully excluded from the crystal,<sup>32</sup> it was later shown that the isotactic polypropylene crystal can include ethylene

defects to certain extent.<sup>33,34</sup> Flow-induced crystallization of random propylene-*co*-ethylene can also be affected by the presence of random co-units in the polymer chain, in terms of both formation of FIC precursors and subsequent crystalline growth from the precursors.<sup>35</sup>

In the current study, the impact of comonomer units on precursor structure and decay for random propylene–ethylene with up to ~7% ethylene is investigated. To do so, precursors are formed by imposing flow via a fiber-pulling protocol; then, the relaxation behavior of the FIC precursors is examined to provide insights into the rate-determining step of their decay and into the structure of the precursors themselves.

#### 2. Experimental Section

#### 2.1. Materials

Three semicrystalline polymers from Borealis were studied: an isotactic polypropylene homopolymer (Borealis HD234CF) and two propylene/ethylene random copolymers (Borealis RD204CF and RD208CF, respectively), synthesized by bulk polymerization in the gas phase using a Ziegler–Natta catalyst.<sup>29</sup> Their molecular and physical characteristics have been previously reported in the literature<sup>29,36</sup> and are summarized in Table 1. Differential scanning calorimetry scans can be found in the Supporting Information. Here, the homopolymer is denoted as "iPP" while the copolymers are denoted as "RACO3" and "RACO7", according to their respective ethylene content of 3.4 and 7.3 mol %. All three grades possess a weight-average molecular weight  $M_w$  of 310 kg/mol and a polydispersity index  $M_w/M_n$  of 3.4.

Glass-coated fibers Flexstrand 110EM13347 with diameter of 17  $\pm$  1  $\mu$ m were kindly provided by Fiber Glass Industries and used as received. The fibers were examined with a Quanta 200 FEG environmental scanning electron microscope and were found to have a smooth surface without observable defects or particles. Control crystallization experiments were performed which verified that these glass fibers do not induce preferential crystallization—called transcrystallinity—on the fiber surface under quiescent conditions, i.e., in the absence of flow.

Polypropylene films of approximately 250  $\mu$ m of thickness were compression molded at 215 °C for 2 min in a Specac hydraulic press and then allowed to slowly cool. Rectangular pieces of 10 mm × 5 mm were cut from the compression-molded films. To prepare the polymer–fiber composite, a single glass fiber was first carefully extracted from a bundle containing approximately 2000 fibers, and it was inspected to ensure that no bending had occurred. The glass fiber was placed between two ~250  $\mu$ m thick polymer films. The assembly was then examined to verify that the embedded



Figure 1. Thermomechanical protocol for relaxation experiments.

fiber was completely straight without any observable curvature. The polymer-fiber composite was subsequently sandwiched between a glass slide and a cover glass which had previously been cleaned with ethanol. The assembly was placed in a Mettler Toledo FP82HT hot stage coupled with a FP90 control system.

#### 2.2. Thermomechanical Protocol

The thermal and flow protocol is schematized in **Figure 1**. First, the assembly was heated to an erase temperature  $T_e = 215$  °C, which is above the equilibrium melting point of iPP ( $T_{m'eq} = 208$  °C).<sup>37</sup> A slight pressure was then applied onto the coverslip to ensure that the fiber was well embedded within the polymer and to avoid air bubbles. After pressing, the temperature was held at 215 °C for  $t_e = 5$  min to erase the previous thermal history of the polymer. Then, the temperature was decreased at a rate of 20 °C/min to the chosen relaxation temperature  $T_{R'}$  which was always selected to be above the nominal melting temperature  $T_m$  (**Table 1**). After equilibration at  $T_R$  for 1 min, the fiber was manually pulled through the molten polymer at a linear velocity of 5–10 mm/s over a distance of 5–10 mm. It

polymer	grade	ethylene content (mol %)ª	Х <sub>с</sub> (%) <sup>ь</sup>	Τ <sub>m</sub> (°C) <sup>b</sup>	Т <sub>с</sub> (°С) <sup>ь</sup>
iPP RACO3	HD234CF RD204CF	0 3.4	49.5 41.3	164 153	110 105
RACO7	RD208CF	7.3	33.9	139	98

Table 1. Molecular and Physical Properties of the Materials from the Literature<sup>29,36</sup>

a. Measured by NMR.

b. From differential scanning calorimetry at 10 °C/min.

has previously been found that small differences in pulling velocity or total displacement that may occur when manually pulling the fiber do not appear to affect the results of flow relaxation experiments.<sup>7</sup> Care was taken to ensure that the movement of the fiber occurred solely in the direction of its axis. After cessation of flow, the sample was allowed to relax at  $T_R$  for a specified relaxation time  $t_R$ . It should be noted that both flow and relaxation occur at temperatures well above the nominal melting temperature, i.e., at temperatures where lamellar growth rates are negligible.

After the relaxation time  $t_{R}$  had elapsed, the sample was quickly cooled down at 20 °C/min to a suitable crystallization temperature  $T_{c'}$  chosen such that linear growth rates were relatively high and bulk nucleation densities were relatively low (135–138 °C for iPP, 128 °C for RACO3, and 120–122 °C for RACO7). A reference time  $t_{0}$  was started once  $T_{c}$  was reached. Polarized optical micrographs were obtained every minute up to  $t_{0} = 30$  min with an Olympus BX51 polarizing optical microscope at 20× magnification. Different areas of the sample were examined in order to account for any possible inhomogeneity in the glass fiber coating. At the end of the experiment, the assembly was removed from the hot stage and air-cooled. The composite was then removed from the slides, and its final thickness was measured.

The axial movement of a fiber in a molten polymer imposes a shear rate  $\dot{\gamma}$  with a cylindrical symmetry. Monasse<sup>38</sup> showed that the shear rate  $\dot{\gamma}$  at a distance *r* from the fiber axis can be expressed as

$$\dot{\gamma} = \frac{1-n}{n} \frac{1}{r_f^{1/n}} \left[ \frac{1}{r_f^{1-1/n} - r_e^{1-1/n}} \right] V_f$$
(1)

where *n* is the exponent in the viscosity power law equation,  $r_f$  is the radius of the glass fiber (8.5 µm),  $r_e$  is the external radius (half thickness of the polymer film), *r* is the radius, and  $V_f$  is the velocity of pulling. According to Eq. 1, the shear rate under our flow conditions reaches values in the order of several hundreds of s<sup>-1</sup> near the surface of the fiber.

#### 3. Results

#### 3.1. Flow-Induced Crystallization Morphology

Imposition of flow by axial movement of a glass fiber embedded in an iPP matrix can result in subsequent growth of a shear-induced oriented morphology near the fiber surface (**Figure 2**b). This oriented structure is not caused by transcrystallinity effects on the fiber surface: control quiescent experiments—in which no flow is applied—developed only a bulk spherulitic morphology throughout the polymer, and there was no preferential



**Figure 2.** (a) Spherulitic morphology formed after 15 min at  $T_c = 135$  °C in a quiescent experiment where no flow has been imposed. (b) Cylindritic morphology formed after 15 min at  $T_c = 135$  °C in a shear experiment where the glass fiber was pulled ( $T_R = 172.5$  °C,  $t_R = 40$  min).

crystalline growth on the fiber surface (Figure 2a). In contrast, a cylindritic oriented morphology can develop in experiments where the fiber has been pulled due to the shear flow imposed by the moving fiber (Figure 2b). The highly oriented structures can also be observed in the wake of the fiber (white arrow in Figure 2b), further confirming that they were not due to transcrystallinity on the fiber surface.<sup>27,39</sup> When shear flow resulted in oriented crystallization, development of oriented crystallites only took place close to the fiber surface, where the highest levels of shear rate occurred. Further from the fiber surface, only spherulites typical of quiescent conditions were obtained due to the rapid decrease of shear rate with distance from the fiber. Both the cylindritic and the spherulitic structures developed with identical linear growth rate *G*, indicating that lamellar growth rate is not affected by the previous flow history.<sup>7</sup>

In shear experiments, a small birefringent zone around the fiber was briefly observed while the fiber was being pulled and can be attributed to increased orientation of polymer chains while subjected to high shear rates. Even though that melt birefringence quickly disappears after cessation of flow, the effects of shear on final morphology can persist for very long times, in agreement with other studies. For example, iPP still retains some orientation after a relaxation time of ~15 min at 180 °C and of ~3 h at 175 °C (see Relaxation Experiments section). Long-lived effects of flow have also been reported by other authors, such as relaxation times between 1 and 32 min at 190 °C.<sup>9,26,28,40,41</sup> In other words, the conformation of polymer chains in the melt is distorted by the imposition of flow, and such distortion can persist for relatively long times, determining the type of semicrystalline morphology that forms upon cooling down.

#### 3.2. Determination of Critical Holding Time t\*

The growth of a cylindritic morphology around the fiber after cessation of flow is a clear and exceptionally sensitive indicator of remaining perturbation in the polymer melt, i.e., of the presence of flow-induced precursors (FIC precursors). The development of an oriented morphology implies that even if the sample was allowed to relax for a given relaxation time  $t_{R}$ , complete re-equilibration of the polymer melt was not attained. In contrast, the absence of high nucleation density around the fiber for experiments with large enough relaxation times  $t_{R}$  indicates that the melt was able to fully reach a re-equilibrated state.

To quantify the melt re-equilibration process, a critical relaxation time  $t^*$  is defined as the holding time necessary to completely erase the effect of the applied flow. Here,  $t^*$  at each relaxation temperature  $T_R$  is calculated as the average of two values: the maximum relaxation time  $t^*_{MAX}$  for which some preferential nucleation on the fiber surface is still observed upon cooling to  $T_c$  and the minimum relaxation time  $t^*_{MIN}$  for which only a spherulitic morphology is detected.

Increasing the relaxation time  $t_R$  at a fixed relaxation temperature  $T_R$  generally resulted in a decline of nucleation density near the fiber. For example, increasing  $t_R$  from 5 s to 15 min at  $T_R = 180$  °C resulted in a partial disappearance of flow-induced precursors, as inferred from the observed morphologies (**Figure 3**a–c). Once  $t_R$  exceeded the critical time  $t^*$ , the melt memory due to flow was fully erased and only spherulites developed throughout (i.e.,  $t_R = 20$  min in Figure 3d).

#### **3.3. Relaxation Experiments**

The critical holding time  $t^*$  was determined at different relaxation temperatures  $T_R$  by examining the final morphology that appeared after allowing



**Figure 3.** Morphological evolution of iPP after 15 min at  $T_c = 135$  °C in fiber pull experiments with  $T_R = 180$  °C and relaxation times  $t_R$  of (a) 5 s, (b) 10 min, (c) 15 min, and (d) 20 min.

relaxation to occur for a specific relaxation time  $t_{\rm R}$  and then cooling to a suitable crystallization temperature  $T_c$ . In this way, the morphological outcome of each fiber pull experiment was classified to construct a morphological map for each type of material. Selection criteria were based on Figure 3: extensive cylindritic morphology was denominated "high orientation" (Figure 3a,b), decreased nucleation along the fiber—but still preferential was regarded as "low orientation" (Figure 3c), and the presence of only bulk spherulitic morphology was denominated "spherulitic" (Figure 3d). It should be noted that the distinction between high and low orientation was qualitative only. The morphological map of iPP is shown in Figure 4, while those of RACO3 and RACO7 can be found in the Supporting Information. The dashed line in Figure 4 represents the critical time t\* calculated as the average between the maximum holding time  $t^*_{MAX}$  for observing some cylindritic morphology and the minimum time *t*<sup>\*</sup><sub>MIN</sub> for which only a spherulitic morphology is obtained. The values for  $t^*_{MAX}$  and  $t^*_{MIN}$  at different relaxation temperatures  $T_{R}$  for all three materials are reported in **Table 2**.

For a given material, the strong temperature dependence of the critical times  $t^*$  (dashed line in Figure 4) indicates that the lifetime of flow-induced precursors is a highly sensitive function of relaxation temperature  $T_R$ . As an example, the time required to fully erase the shear-induced nucleation for iPP increases from ~16 min at 180 °C to more than 30 h at 172.5 °C. Such strong temperature dependence is consistent with previous studies; for example, work on poly(1-butene) found that the critical time increased by 3 orders of magnitude when the relaxation temperature was decreased by 10 °C.<sup>7</sup>

For a given relaxation temperature  $T_{R'}$ , the critical time for disappearance of the oriented morphology  $t^*$  significantly decreases with increasing comonomer content. For example, at 172.5 °C, iPP needs more than 30 h to



**Figure 4.** iPP morphological map for relaxation experiments. Dashed line corresponds to a linear fit of the calculated critical relaxation times *t*\*.

		t* (s)	
$T_{R}$ (°C)	iPP	RACO3	RACO7
182.5	60-90		
180	900-990	120-150	
177.5	3600-3750	210-240	
175	11700-12600	750-810	
174	36000-43200		
172.5	108000-136800	8520-9000	180–210
170		36000-43200	480-510
168.5			2250-2325
165			10320-10800
162.5			30600-39600

Table 2. Critical Holding Times t\* at Different T<sub>R</sub> for iPP, RACO3, and RACO7<sup>a</sup>

a. The first and second value in each pair correspond to  $t_{M}^{*}AX_{i}^{*}Max_{i}^{*$ 

completely relax the oriented morphology, while RACO3 and RACO7 only need ~2.5 h and 3.5 min, respectively (Table 2). Likewise, with increasing ethylene content, the temperature of relaxation  $T_{\rm R}$  needs to be lowered in order to obtain similar values of critical relaxation time t\*. It was also found that the highest temperature  $T_{\rm p}$  for which oriented crystallization could be obtained—using the shortest possible holding times—decreases with increasing comonomer content. Indeed, it was not possible to obtain cylindritic structures after fiber pulling for  $T_{\rm R}$  above 182.5, 180, and 172.5 °C for iPP, RACO3, and RACO7, respectively. Such a threshold on  $T_{R}$  may have been caused in part by limitations in cooling speed: at the highest relaxation temperatures where  $t^*$  is on the order of ~5 s or smaller, the experimental setup cannot be cooled fast enough to prevent some relaxation of flow-induced structures during the early stages of cooling. Additionally, it is possible that flow-induced structures are not able to form at the highest temperatures if crystallizable sequences are not long enough, particularly as the comonomer content increases.

The apparent activation energy  $E_a$  for complete disappearance of flowinduced structures was found to decrease with increasing copolymer content. To calculate  $E_a$ , the average critical time  $t^*$  was first plotted against the inverse of temperature in an Arrhenius plot (**Figure 5**). A set of straight lines was obtained, so Eq. 2 was used to obtain values of  $E_a$  for each material:

$$\ln(t^*) = \ln(A) - \frac{E_a}{R} \left(\frac{1}{T}\right)$$
(2)



**Figure 5.** Arrhenius plot of critical holding times  $t^*$  as a function of relaxation temperature  $T_{R}$  for iPP ( $\blacksquare$ ), RACO3 ( $\bullet$ ), and RACO7 ( $\blacktriangle$ ).

where  $t^*$  (in s) is the critical relaxation time, A is a preexponential factor, R is the gas constant (8.314 J K<sup>-1</sup> mol<sup>-1</sup>), and T is the absolute temperature (in K). Energies of activation of 1180 ± 60, 1000 ± 50, and 860 ± 40 kJ/mol were obtained for iPP, RACO3, and RACO7, respectively.

#### 4. Discussion

The development of an oriented morphology near the fiber surface is an extremely sensitive indicator of the presence of oriented precursors that formed during strong enough flows. These oriented precursors are thought to be crystalline or quasi-crystalline thread-like nuclei, although their exact structure remains the subject of discussion. In the present experiments, flow-induced precursors form during flow in the region subjected to the highest level of shear stress—near the fiber surface. After cessation of flow, the oriented precursors can undergo a gradual disappearance process if the polymer melt is held at sufficiently high relaxation temperature for a long time. The dissolution of precursors is reflected in a decrease in oriented morphologies developed after cooling to the crystallization temperature.

The Arrhenius-type dependence with temperature of the critical times for relaxation provides some insight into the manner in which oriented precursors decay. The process of flow-induced precursor relaxation is believed to occur by detachment of polymer chain segments from the oriented nuclei and their subsequent diffusion into the melt. The apparent energies of activation for precursor relaxation of iPP, RACO3, and RACO7 are much larger than the energy of activation for viscous flow (~44 kJ/mol for iPP).<sup>42</sup> Therefore, it appears that detachment of a chain stem from an oriented nuclei is the limiting step in the process of precursor relaxation—not diffusion of the detached stem into the melt. This observation is in agreement with studies of relaxation in iPP, iPS, and iPBu.<sup>7,9,26</sup>

The decrease of apparent activation energies  $E_a$  with increasing ethylene content indicates that the rate of the relaxation process is altered by the presence of comonomer. This may be attributed to the disruption of the structure of oriented precursors and thus to the process of chain stem detachment from quasi-crystalline precursor bundles. It is well-known that random ethylene co-units in polypropylene play a major role by acting as perturbations of the resulting crystalline structure, so the reduction of  $E_a$ with increasing ethylene content suggests that those random co-units are also effective at perturbing the morphological nature of the precursors.

The apparent activation energies  $E_a$  can be used to obtain information about the structure of flow-induced precursors, which have been proposed to consist of partially ordered bundles of chains with a quasi-crystalline nature and a characteristic bundle length  $L_s$ .<sup>8</sup> In this model, it is envisioned that precursors decay by having chain segments of length  $L_s$  disengage from the precursor bundles. The length  $L_s$  may then be determined as

$$L_{\rm s} = \frac{E_{\rm a}}{\Delta H_{\rm m}^{\,0}} \times L_{\rm u} \tag{3}$$

where  $L_u$  corresponds to the length of the repeating unit along the *c*-axis in the crystalline lattice,  $E_a$  is the apparent activation energy for disappearance of oriented precursors, and  $\Delta H_m^0$  is the melting enthalpy of the polymer crystals. For iPP,  $L_u$  is ~0.22 nm<sup>43</sup> and the thermodynamic melting enthalpy of its crystals  $\Delta H_m^0$  is 8.7 kJ/mol.<sup>44</sup> However, if the melting enthalpy of a perfect iPP crystal is used in calculations for random copolymers, their detaching chain length  $L_s$  may be underestimated. Indeed, random ethylene co-units are known to be partially included into the crystalline phase of iPP, locally distorting it and resulting in a decrease of the energy required to melt it.<sup>34,45</sup> Consequently, the melting enthalpies of copolymer crystallites are projected to be lower than 8.7 kJ/mol.

For random copolymers, the exact dependence of the melting enthalpy of the crystalline phase with the fraction of incorporated comonomer units is unknown. One approach for obtaining an estimate of the melting enthalpy is to use the Sanchez–Eby theory of copolymers, which considers an excess free energy  $\varepsilon$  associated with comonomers incorporated into the crystalline phase as defects.<sup>46</sup> Although the variation of the melting enthalpy with  $\varepsilon$  remains elusive, some authors have assumed a linear dependency  $\Delta H_{cryst,cop} = \Delta H_{cryst,homo} - \varepsilon X_c$ , where  $\Delta H_{cryst,cop}$  is the heat of fusion per mole of crystalline copolymer,  $\Delta H_{cryst,homo}$  is the heat of fusion per mole of crystalline homopolymer (8.7 kJ/mol), and  $X_c$  is the mole fraction of ethylene co-units in the crystalline phase of the copolymer.<sup>47,48</sup> For polypropylene–ethylene copolymers, Alamo et al. experimentally obtained data for  $X_c$  and calculated a penalty energy  $\varepsilon$  of ~2.94 kJ/mol.<sup>34,47</sup> Using these literature values, it is estimated that the  $\Delta H_{cryst,RACO7}$  would only decrease by ~0.9% when compared to 8.7 kJ/mol of the iPP homopolymer, indicating that the ethylene counits only slightly distort the energy landscape of the crystalline structure. The corresponding detaching stem lengths  $L_s$  are 30, 25, and 22 nm for iPP, RACO3, and RACO7, respectively (**Table 3**).

Another approach to estimate the melting enthalpy of 100% crystalline phase  $\Delta H_{cryst.cop}$  involves measuring the experimental heat of fusion of a given sample with differential scanning calorimetry and then determining its crystallinity with an alternative experimental technique. Laihonen et al. normalized the experimental heat of fusion by the crystallinity obtained from wide-angle X-ray diffraction and determined that  $\Delta H_{\text{cryst,cop}}$  decreased by ~30-40 J/g per 10% of ethylene content.<sup>49</sup> Using Laihonen's result, a  $\Delta H_{\text{crvst.RACO7}}$  of ~7.7 kJ/mol can be estimated for RACO7, i.e., a steeper decrease than that calculated with  $\varepsilon$ . The resulting values of  $L_s$  still show a decrease with increasing copolymer percentage: 30, 27, and 24 nm for iPP, RACO3, and RACO7 (Table 3). Finally, in another study, Alamo et al. also obtained measurements of experimental enthalpy of fusion and corresponding NMR crystallinities for a series of polypropylene-ethylene copolymers.<sup>34</sup> If the experimental melting enthalpies are normalized by their corresponding <sup>13</sup>C NMR crystallinities, an even stronger decrease in enthalpy with ethylene content is predicted: for RACO7,  $\Delta H_{cryst RACO7}$  would be ~6.6 kJ/mol. In this case, however, the obtained detaching stem lengths  $L_s$ display an almost constant value of approximately 30 nm (Table 3).

While the decrease in  $E_a$  indicates that the process of chain stem detachment from quasi-crystalline bundles becomes less difficult with increasing ethylene content, the exact interpretation in terms of structural parameters of precursors is complicated by the uncertainty in  $\Delta H_{cryst,cop}$ . The values of  $L_s$  obtained with  $\varepsilon$  and with Laihonen's data suggest that ethylene counits mainly disrupt structure of precursors by decreasing the

**Table 3.** Values of Apparent Energy of Activation for Precursor Relaxation  $E_a$  and Stem Length  $L_s$  Calculated with  $\Delta H_{cryst,cop}$  Estimated Using Excess Free Energy  $\epsilon$ , a Decrease of 30–40 J/g per 10 mol % Ethylene,<sup>49</sup> and Data on Heat of Fusion and on <sup>13</sup>C NMR Crystallinities<sup>34</sup> (further details are available in the Supporting Information).

sample	E <sub>a</sub> (kJ/mol)	L <sub>s,excess free energy</sub> (nm)	L <sub>s,Laihonen</sub> (nm) <sup>49</sup>	L <sub>s,Alamo</sub> (nm) <sup>34</sup>
iPP	1180	30	30	30
RACO3	1000	25	27	30
RACO7	860	22	25	29



**Figure 6.** Schematic of flow-induced precursors of (a) a homopolymer and (b, c) a copolymer. (a) The homopolymer forms precursors with a characteristic detaching stem length  $L_s$ . (b) The copolymer forms precursors with  $L_s$  similar to that of the homopolymer if its counits predominantly increase the degree of imperfection within the internal structure of bundles (decrease in  $\Delta H_{cryst,cop}$ ). (c) The copolymer forms precursors with decreases the average length of precursor bundles ( $\Delta H_{cryst,cop}$  nearly invariant).

average length of precursor bundles—and thus, the length of chain stem  $L_{\rm s}$  that must detach during decay (schematically illustrated in **Figure 6**, compare a and c). In contrast,  $L_{\rm s}$  determined by normalizing with <sup>13</sup>C NMR crystallinities suggests that ethylene comonomers predominantly disturb precursor structure by increasing the internal degree of imperfection of quasi-crystalline bundles (Figure 6, compare a and b). This divergence may be due to the fact that <sup>13</sup>C NMR crystallinity considers the fraction of ordered 3/1 helical sites (crystallites) but does not take into account how perfectly packed those helices are.<sup>34</sup> Imperfections in packing of helices can result in decreased calorimetry or wide-angle X-ray diffraction crystallinities without significantly changing the magnitude of NMR crystallinity, yielding differing estimates of  $\Delta H_{\rm cryst,cop}$  (and  $L_{\rm s}$ ) depending on which experimental technique is used.

Because of the uncertainty in melting enthalpy of copolymer crystals, it is not possible to discern between the effect of comonomer units on precursors as depicted in Figure 6b,c. Also, qualitative arguments can be made for both possible scenarios. On one hand, if the characteristic lamellar thickness of a polymer is considered to be related to precursor stem length  $L_s$ , a reduction in  $L_s$  with increasing coethylene content—as estimated from calculations based on Sanchez–Eby and Laihonen (Table 3)—would be expected. Indeed, lamellar thickness in polypropylene–ethylene random copolymers generally decreases with increasing ethylene percentage,<sup>29,50–52</sup> although invariance of lamellar thickness with comonomer content has also been reported.<sup>33</sup> The decrease in crystallite thickness with higher comonomer percentage is generally explained as follows: because a fraction of ethylene units must be excluded from the polypropylene crystals, a resin with higher copolymer content has a smaller average length of crystallizable sequences which can then only participate in lamellae of reduced thickness. On the other hand, it can be hypothesized that due to their quasi-crystalline nature, flow-induced precursors are able to accommodate ethylene counits more easily than a "regular"  $\alpha$ -crystal because defects impose less strain on their structure. In other words, the more disordered structure of precursors—as compared to iPP  $\alpha$ -phase—would experience less disruption due to inclusion of ethylene defects and would not be as limited by available crystallizable lengths, leading to invariance of  $L_s$  with increasing copolymer content as computed from <sup>13</sup>C NMR data.

The activation energy  $E_{a}$  and, consequently, the detaching stem length  $L_{\rm s}$  obtained here for iPP are somewhat greater than in previous relaxation experiments of iPP (~30 nm vs ~7 nm). Notably, an  $L_{s}$  ~ 30 nm for iPP is commensurate with the periodicity of layer-like precursors of iPP previously inferred from real-time small-angle X-ray scattering (~43 nm)<sup>3</sup> and similar to the detaching stem length obtained for relaxation of other types of polymers, namely polyoxyethylene and ipolybutene (~20 nm).<sup>8,27</sup> The value of 30 nm is also comparable to the lamellar thickness of iPP characteristic of relatively high crystallization temperature: under quiescent conditions at 152 °C, a lamellar thickness of ~20 nm and corresponding long period of ~30 nm would be expected,48 while early kebabs grown after flow at low undercoolings can display a long period of up to ~60 nm.<sup>53</sup> The larger activation energy E<sub>a</sub> obtained here for iPP (~1180 kJ/mol vs a range of ~122-350 kJ/mol in other reports)<sup>9,13,26-28</sup> may be due to differences in experimental protocol. Indeed, discrepancies in E<sub>a</sub> are ubiquitous in the literature and have been ascribed to variability in the experimental approach. For example, Janeschitz-Kriegl obtained an  $E_a \sim 224$  kJ/mol for iPB,<sup>26</sup> about one-third of the value of ~720 kJ/mol previously found by Azzurri.<sup>7</sup> For iPP, Nazari et al. obtained an apparent activation energy of 122 kJ/mol,<sup>13</sup> much smaller than that of 334 kJ/mol previously reported by Janeschitz-Kriegl.<sup>26</sup> These disparities were attributed to using different criteria when determining t\*—assessment of complete disappearance of orientation vs a criterion of partial decay—and to employing different techniques to detect precursors, which can lead to dissimilar definitions of "presence of precursors". Experimental conditions such as flow geometry, range of shear rate, and range of relaxation temperature also vary widely among different studies, but it is unclear whether sufficiently large variations could generate structural differences in precursors that affect the process of stem detachment and the apparent energy of activation. For example, Cavallo et al. reported that changing shear rate  $\dot{y}$  from 16 to 32 s<sup>-1</sup> does not noticeably affect the

apparent activation energy for relaxation of precursors in iPP (i.e., the ratedetermining step for relaxation is independent of shear rate within the explored range), although the critical time for disappearance of the precursors is larger for higher shear rates.<sup>9</sup> In the current study, fiber pulling can impose shear rates on the order of several hundreds of s<sup>-1</sup>, but it is undetermined whether such difference in flow conditions would significantly affect precursor structure. Likewise, here precursors have formed in a range of temperatures. However, the role of shearing temperature on the structure of flow-induced precursors has not previously been explored, and consequently, whether it has a significant impact on the rate-limiting step of relaxation remains unknown.

#### 5. Conclusion

The relaxation behavior of flow-induced precursors in iPP provides information about their nature and underlying structure. These oriented precursors are key to the effects of flow-induced crystallization but are extremely difficult to directly probe due to their small size and to their scarce concentration in the melt. In this study, the presence or absence of flow-induced precursors was deduced from the type of semicrystalline morphology that forms near the surface of a previously pulled fiber, i.e., in the region that was subjected to the highest shear rate. The process of decay of precursors was explored by first imposing flow and then allowing the melt to relax at relatively high temperatures  $T_R$  for specific relaxation times  $t_R$  before cooling down to a crystallization temperature  $T_c$ .

It was found that the process of decay of flow-induced precursors is affected by the presence of random ethylene counits in the polypropylene chain. The critical times for precursor relaxation  $t^*$  followed an Arrheniustype dependence with temperature, and the apparent energy of activation for precursor dissolution  $E_a$  clearly decreased with increasing ethylene content. Such a decrease indicated that the limiting step in the process of precursors decay is effectively altered by the presence of random comonomer units.  $E_a$  values for all three materials were much larger than the activation energy for viscous flow of iPP so, in agreement with other studies, it is deduced that the limiting step in precursor decay is detachment of a chain stem from an oriented nuclei—not diffusion of the detached stem into the melt.

The decrease of apparent activation energy  $E_a$  indicates that the process of chain stem detachment becomes easier with increasing ethylene content. This effect is attributed to disruption of the structure of precursors caused by the random ethylene counits. Oriented precursors are envisioned as quasicrystalline bundles from which chain stems of a characteristic length  $L_{\rm s}$  become detached—with an associated enthalpy—during the relaxation process. The enthalpy of crystallization of polypropylene-*random*-ethylene copolymers  $\Delta H_{\rm cryst,cop}$  is however not well-known, leading to some uncertainty when estimating the detaching stem length  $L_{\rm s}$ . Estimations of  $\Delta H_{\rm cryst,cop}$  based on available experimental data suggest two possible scenarios: one in which ethylene counits mainly disrupt structure of precursors by decreasing the average length of precursor bundles—and therefore the detaching stem length  $L_{\rm s}$ —and another one in which ethylene comonomers primarily disturb precursor structure by increasing the degree of imperfection of the quasi-crystalline bundles.

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#### **SUPPORTING INFORMATION**

# Effect of Random Ethylene Comonomer on Relaxation of Flow-Induced Precursors in Isotactic Polypropylene

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#### **Morphological maps of RACO3 and RACO7**



**Figure S1**. RACO3 morphological map for relaxation experiments. Dashed line corresponds to a linear fit of the calculated critical relaxation times t\*.



**Figure S2**. RACO7 morphological map for relaxation experiments. Dashed line corresponds to a linear fit of the calculated critical relaxation times t\*.

#### Estimation of melting enthalpy of copolymer crystals

The melting enthalpy of copolymer crystals  $\Delta H_{cryst,cop,\epsilon}$  estimated using the excess free energy  $\epsilon$  assumed a linear relationship  $\Delta H_{cryst,cop} = \Delta H_{cryst,homo} - \epsilon X_c$ , where  $X_c$  is the mole fraction of ethylene co-units in the crystal. Data for  $X_c$  was extracted from a copolymer study by Alamo *et al.*<sup>1</sup>, excess free energy  $\epsilon \sim 2.94$  kJ/mol was obtained from previous work by the same author,<sup>2</sup> and 8.7 kJ/mol was used for  $\Delta H_{cryst,homo}$ .  $\Delta H_{cryst,RACO3}$  (with 3.4% ethylene) was taken as the average of the values calculated for 2.2% and 4.59%, and  $\Delta H_{cryst,RACO3}$  (with 7.3% ethylene) was taken as that calculated for 7.47% (Table S1).

Ethylene content (mol %)	X <sub>c</sub> <sup>1</sup>	$\Delta H_{cryst,cop, \epsilon} = \Delta H_{cryst,homo} - \epsilon X_c $ (kJ/mol)
0.79	0.0035	8.69
2.2	0.0103	8.67
3.4		8.66
4.59	0.0202	8.64
7.47	0.031	8.61

**Table S1.** Calculations for estimating  $\Delta H_{cryst,cop,\epsilon}$ .

The melting enthalpy of copolymer crystalline phase  $\Delta H_{cryst,cop NMR}$  was estimated by using <sup>13</sup>C NMR crystallinity and experimental heat of fusion ( $\Delta H_{cop}$ ) measured by Alamo *et al.* (Table S2). The enthalpy value for the 0.79% copolymer (considered the homopolymer here) is somewhat smaller than 8.7 kJ/mol (= 209 J/g), so all enthalpy values were normalized to the reference of 8.7 kJ/mol by assessing the relative decrease in enthalpy caused by comonomer (denoted as ratio "r" in Table S2). Note that due to the quasi-crystalline nature of flow-induced precursors, the enthalpy of fusion is in fact expected to be lower (for example, 8.7 kJ/mol would be an overestimation for homopolymer precursors) but the magnitude of that difference is unknown. Thus, in the present work, 8.7 kJ/mol has been used as the reference for the iPP homopolymer.

Ethylene content (mol %)	NMR crystallinity (%) <sup>1</sup>	ΔH <sub>cop</sub> (J/g)	$\Delta H_{cryst,cop} = \Delta H_{cop} / X_c$ (J/g)	$r = \Delta H_{cryst,cop} / \Delta H_{cryst,0.79\%}$	ΔH <sub>cryst,cop NMR</sub> = 8.7 kJ/mol * r (kJ/mol)
0.79	0.66	92	139.4	1.00	8.7
2.2	0.65	84	129.2	0.93	8.1
3.4					7.4
4.59	0.63	68	107.9	0.77	6.7
7.47	0.58	61	105.2	0.75	6.6

**Table S2.** Calculations for estimating  $\Delta H_{cryst,cop,NMR}$ .

**Differential scanning calorimetry** 



Figure S3. Melting endotherms at a heating rate of 10 °C/min



**Figure S4**. Melting exotherms at a cooling rate of 10 °C/min

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