

Revision_2**On the *P*-induced behavior of the zeolite phillipsite:
an in-situ single-crystal synchrotron X-ray diffraction study**

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Abstract

The elastic behavior and the structural evolution at high pressure of a natural phillipsite have been investigated by *in situ* single-crystal X-ray diffraction up 9.44 GPa, using a diamond anvil cell and the nominally penetrating *P*-transmitting fluid methanol:ethanol:water (16:3:1) mix. Although no phase transition was observed within the *P*-range investigated, two different compressional regimes occur. Between 0.0001 and 2.0 GPa, the refined elastic parameters, calculated by a second-order Birch-Murnaghan Equation of State (BM-EoS) fit, are $V_0 = 1005(1) \text{ \AA}^3$, $K_0 = 89(8) \text{ GPa}$ for the unit cell volume; $a_0 = 9.914(7) \text{ \AA}$, $K_a = 81(12) \text{ GPa}$ for the *a*-axis; $b_0 = 14.201(9) \text{ \AA}$, $K_b = 50(5) \text{ GPa}$ for the *b*-axis and $c_0 = 8.707(2) \text{ \AA}$, $K_c = 107(8) \text{ GPa}$ for the *c*-axis ($K_a: K_b: K_c \sim 1.62:1:2.14$). Between 2.0 and 9.4 GPa, a *P*-induced change in the configuration of H₂O molecule, coupled with a change of the tilting mechanisms of the framework tetrahedra, give rise to a second compressional regime, in which the phillipsite structure is softer if compared to the first compressional range. In the second compressional regime, the refined elastic parameter,

30 calculated by a second-order BM-EoS fit, are $V_0 = 1098(7) \text{ \AA}^3$, $K_0 = 18.8(7) \text{ GPa}$ for the unit-cell volume; a_0
31 $= 10.07(3) \text{ \AA}$, $K_a = 30(2) \text{ GPa}$ for the a -axis; $b_0 = 14.8(1) \text{ \AA}$, $K_b = 11(1) \text{ GPa}$ for the b -axis and $c_0 = 8.94(2) \text{ \AA}$,
32 $K_c = 21(1) \text{ GPa}$ for the c -axis ($K_a: K_b: K_c \sim 2.72:1:1.90$). The evolution of the monoclinic β angle with
33 pressure shows two distinct trends in the two compressional regimes: with a negative slope between 0.0001-
34 2.0 GPa, and a positive slope between 2.0-9.4 GPa. The mechanisms, at the atomic scale, that govern the two
35 compressional regimes of the phillipsite structure are described.

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38 **Keywords:** Phillipsite; high pressure; compressibility; elastic behavior; structure evolution; synchrotron X-
39 ray diffraction.

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42 1. Introduction

43 Phillipsite is one of the most common natural zeolites with ideal composition
44 $K_2(\text{Na}, \text{Ca}_{0.5})_3[\text{Al}_5\text{Si}_{11}\text{O}_{32}] \cdot 12\text{H}_2\text{O}$ (Passaglia and Sheppard 2001), commonly found in altered sediments in
45 “closed” or “open” hydrologic systems, as saline lakes, deep-sea sediments, hot spring deposits, as well as in
46 vugs of basalt and in tuffs (Galli and Loschi Ghittoni 1972; Rinaldi et al. 1974; Gottardi and Galli 1985;
47 Armbruster and Gunter 2001). In Langella et al. (2001) is reported how the formation of phillipsite requires
48 low silica activity, along with high pH.

49 Phillipsite is monoclinic (space group $P2_1/m$, $a \sim 9.865 \text{ \AA}$, $b \sim 14.300 \text{ \AA}$, $c \sim 8.693 \text{ \AA}$, $\beta \sim 124.92^\circ$), with
50 framework density: $15.8 \text{ T}/1000 \text{ \AA}^3$ (Baerlocher et al. 2007). In nature, crystals are often found in spherical
51 radiating aggregates, frequently twinned on [001], [021] and [110] (Rinaldi et al. 1974). Several examples of
52 intergrowths with other zeolites (*e.g.*, faujasite, offretite, gismondine, garrionite and gobbinsite) are reported
53 in literature (Rinaldi et al. 1975, Passaglia and Sheppard 2001). In a very recent paper, Danisi et al. (2015)
54 reported coherent twinned intergrowths of merlinoite and phillipsite in a sample originated from Monte
55 Somma, Vesuvius (Italy). The framework of phillipsite (PHI topology, Baerlocher et al. 2007) is built up by
56 four corner-shearing Si/Al tetrahedra, which form four- and eight- membered rings. The four-membered
57 rings (hereafter 4-mRs) and the eight-membered rings (hereafter 8-mRs) are also referred as the secondary
58 building units of PHI framework type (SBU, code 4 and 8 respectively, Baerlocher et al. 2007). In PHI

59 framework, the 4-mRs are connected to form double crankshaft chains running parallel to [100]. The PHI
60 framework contains two independent channel systems, running along [100] and [010] (hereafter: 8-mRs[100]
61 and 8-mRs[010] channels, respectively) (Fig. 1). The two sets of channels intersect each other's (Gatta and
62 Lee 2007, Gatta et al. 2009a). The channel running along [100] is confined by two different 8-mRs, hereafter
63 8-mRs[100]-1 and 8-mRs[100]-2. In the 8-mRs[100]-1, the distance $O9-O8 < O7-O7$, whereas, in the 8-
64 mRs[100]-2, $O9-O8 > O7-O7$ (Fig. 1). The double 4-mRs crankshaft chains form a 8-mRs, here referred as
65 8-mRs(001) (Fig. 1). As pointed out by Rinaldi et al. (1974) and Gatta et al. (2009a, 2010, 2015), the Si/Al
66 distribution between the tetrahedral sites is completely disordered in natural phillipsite.

67 In phillipsite from Richmond, Victoria, Australia (*i.e.*, the same natural species used in this study),
68 the extra-framework population (Fig. 1) is represented by two main cations sites in which Ca (or Na) and K
69 lie. Viewing the structure perpendicular to (010), the Ca-site lies above and below the mirror plane, where
70 the two independent systems of channels intersect. As reported by Gatta et al. (2009a), the coordination shell
71 of Ca site is complex: with a maximum distance of $\sim 3 \text{ \AA}$, at least 9 mutually excluding configurations are
72 possible. The coordination number (CN) of the Ca sites is 6-7: three oxygen atoms of the tetrahedral
73 framework (O4, O3, O7) and three or four H₂O molecules (among W1, W3, W4-W4', W5, W6). The K site
74 is actually split in two subsites, K1 and K2, only 0.5 \AA apart. The two K-sites lie close to the 8-mRs[100]
75 channel wall. If a maximum bond length of 3.4 \AA is considered, the CN of both sites is 9 (five oxygen atoms
76 of the framework and four H₂O molecules) (Gatta et al. 2009a). As shown in Gatta et al. (2009a), the H₂O
77 molecules are distributed over 7 independent sites: only W1 and W2 lie on the mirror plane, occupying the
78 *Wyckoff* special position *2e*; the others sites (*i.e.*, W3, W5, W6, W4, W4' in Gatta et al. 2009a) occupy the
79 general *Wyckoff* position *4f*. W4 and W4' are two subsites only 0.4 \AA apart, and mutually exclusive. The
80 sites W4, W4', W5, W6 occupy central positions in the 8-mRs[010] channel, whereas the W3 site lies close
81 to the channel wall. Among them, W4, W4' and W6 lie at the intersection of the two channels. The W1 and
82 W2 sites lie approximately in the center of the 8-mRs[100] channel (Fig. 1).

83 The high-temperature behavior of natural and synthetic phillipsites has been object of several
84 investigations (*e.g.*, Steinfink 1962; Stuckenschmidt et al. 1990; Gualtieri et al. 1999a, 1999b, 2000;
85 Passaglia et al. 2000; Sani et al. 2002). The thermal behavior, and in particular the dehydration mechanisms,
86 are connected to the nature of the extra-framework population. Due to the lack of single crystals of phillipsite

87 suitable for non-ambient conditions experiments, Gatta and Lee (2007) investigated the high-pressure
88 behavior of a natural phillipsite powder from Richmond, Victoria, Australia, up to 3.64 GPa, by *in situ*
89 synchrotron X-ray powder diffraction with a diamond anvil cell, using the methanol:ethanol:water = 16:3:1
90 mix as *P*-transmitting fluid. Axial and volumetric bulk moduli were reported. No unambiguous evidence of
91 phase transition was observed within the *P*-range investigated. Moreover, the quality of the high-*P* powder
92 data, as well as the complex structure of phillipsite, prevented a fulfill discussion about the role played by the
93 extra-framework population on the elastic behavior. Although the general aspects of the high-*P* behavior of
94 the zeolite phillipsite were discussed by Gatta and Lee (2007), a comprehensive characterization of the
95 mechanisms which involve framework and extra-framework population is still missing. In addition, the
96 previous high-*P* study explored a modest *P*-range. In this light, the aim of this work is to reinvestigate the *P*-
97 induced structural evolution of a natural phillipsite (using the sample natural sample previously used by
98 Gatta and Lee 2007) by *in situ* single-crystal synchrotron X-ray diffraction, using a diamond anvil cell.

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100 2. Experimental Methods

101 The HP-synchrotron X-ray single-crystal diffraction experiments were conducted at the Extreme
102 Conditions Beamline P02.2 at PETRA-III/DESY, Hamburg, Germany. Data collections were performed with
103 an incident beam of 42.7 keV in energy, and a focusing spot of ~ 8.5 (H) μm x 1.8 (V) μm originated from a
104 compound refractive lenses system, consisting of 121 Be lenses with a radius of 50 μm (400 μm beam
105 acceptance) and a focal length of 1221 mm. A single crystal of phillipsite ($\sim 50 \times 50 \times 20$ μm), free of twinning
106 under polarized-light microscope and with lamellar morphology, was selected for the experiment. The crystal
107 was loaded in a symmetric DAC equipped with Bohler-Almax design diamonds/seats with a 70° opening
108 and 300 μm culets size. A 250- μm -thick foil of stainless steel was used as gasket, which was pre-indented to
109 ~ 60 μm and then drilled with a hole of ~ 200 μm in diameter, using a spark-erosion device. A few ruby
110 spheres were added into the gasket hole for *P*-measurement, by the ruby-fluorescence method (Mao et al.
111 1986; pressure uncertainty ± 0.05 GPa). The mix methanol:ethanol:water = 16:3:1 (hereafter *m.e.w.*) was
112 used as hydrostatic *P*-transmitting fluid (Angel et al. 2007). This pressure medium is considered potentially
113 “penetrating” (Gatta and Lee 2014), as at least the molecules of H₂O ($\varnothing \sim 2.65$ Å) and CH₃OH ($\varnothing \sim 3.76$ Å)
114 may theoretically be incorporated into the 8-mRs[100] channels of phillipsite ($\varnothing \sim 3.8$ Å, Baerlocher et al.

115 2007). Pressure was increased (up to $P_{\max} = 9.4$ GPa, Table 1) with an automated pressure-driven system
116 from Sanchez Technology (Viarmes, France) and measured with the online ruby/alignment system powered
117 by a 100 mW 458-nm laser. Diffraction images were collected with a Perkin Elmer XRD 1621 flat panel
118 detector, using an in-house script for collecting step-scan diffraction images. The sample to detector distance
119 (402.34 mm) was calibrated using a CeO₂ standard (NIST 674a). A few data collections were performed in
120 decompression (Table 1). The diffraction images were then converted to conform to the “Esperanto” format
121 of the program CrysAlis (Agilent 2012; Rothkirch et al. 2013). At all pressure points, the adopted data
122 collection strategy consisted in a pure ω -scan ($-28^\circ \leq \omega \leq +28^\circ$), with a step size of 1° and an exposure time
123 of 1 s/frame; then Bragg peaks were indexed. Intensities of the diffraction peaks were integrated and
124 corrected for Lorentz-polarization effects, using the CrysAlis package (Agilent 2012). Corrections for
125 adsorption (due to the DAC components) was applied by the semi-empirical *ABSPACK* routine implemented
126 in CrysAlis. The refined unit-cell parameters are listed in Table 1.

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129 **3. Structure refinement protocol**

130 All the structure refinements, at different pressures, were performed using the software JANA2006
131 (Petříček et al. 2014) in the space group $P2_1/m$, as suggested by the reflection conditions. Reflections were
132 “observed” down to an interplanar distance $d \sim 0.8$ Å. At $P \geq 2.57$ GPa, it was observed an abrupt decrease
133 in the number of observed reflections, with a consequent increase of the R_1 factor (Table 2, deposited). The
134 isotropic structure refinements were possible up to 4.85 GPa (P_{11}). For the first refinement (P_1 , 0.2 GPa),
135 the input fractional coordinates of the framework sites were taken from Gatta et al. (2009a). The positions of
136 the extra-framework sites were obtained by a careful analysis of the difference-Fourier maps of the electron
137 density. At P_1 , one Ca site and two mutually independent K sites were identified, along with six independent
138 sites assigned to the H₂O molecules, according to the structure model of Gatta et al. (2009a); the same sites
139 labeling scheme was used (*i.e.*, Ca, K1, K2 and W1-6, Table 3, deposited). Briefly, W1 and W2 sites lie in
140 the center of 8-mRs[100]-1 and 8-mRs[100]-2, respectively, whereas W3 and W5 occupy the 8-mRs[010]
141 channel; the W4 and W6 sites lie at the intersection of the two channel systems. As the analysis of the
142 difference-Fourier maps revealed only one strong peak lying on the mirror plane between the position of the

143 sites W4-W4' in Gatta et al. (2009a), in the structure model of this study we refined only one site (labelled as
144 W4, Table 3). No specific restrains were applied to the Ca site, whereas the K1-K2 sites were refined with
145 the same displacing parameter (DP). The same restriction was applied to all the H₂O sites. This protocol was
146 used in all the refinements at different pressures, with the following exceptions:

147 - The DPs of the H₂O sites were forced to have an U_{iso} value fixed to 0.075 Å². This value is arbitrary,
148 although very reasonable: the refined U_{iso} of H₂O sites at P_1 was $\sim 0.079(4)$ Å² (Table 3).

149 - The occupancy of the Ca site was fixed to the one obtained from the refinement of P_1 . The sum of
150 the K1 and K2 site occupancies, in all the refinements at $P > P_1$, were forced to assume the value found at
151 P_1 .

152 - The R_1 factors were all $\leq 10\%$ up to 2.56 GPa (P_8). At $P > P_8$, the R_1 values increased significantly;
153 the last refinement which reached convergence is that at 4.85 GPa (P_{11}). At $P > P_8$, the occupancy of the
154 H₂O sites showed an anomalous increase. As the adsorption of H₂O molecule at this pressure is not realistic
155 (*i.e.*, all the previous experimental findings available in literature reported P -induced over-hydration effects
156 at $P < 1$ GPa, Gatta and Lee 2014 for a review), we introduced a further restrain: the *sum* of the H₂O site
157 occupancies was fixed to the value obtained by the refinement at P_8 (*i.e.*, 14.36 ± 1.16 molecules per formula
158 unit, m.p.f.u.). The sum at P_8 is equal, within 1σ , to that obtained at P_1 (*i.e.*, 14.00 ± 0.84 m.p.f.u.).

159 For all the structure refinements, Table 2 lists the principal statistical parameters. Site coordinates and
160 occupancies are given in Table 3 (deposited). Refined bond distances are reported in Tables 4 and 5
161 (deposited). Other relevant structural parameters are reported in Table 6, 7, 8, 9.

162

163 4. Results

164 4.1 High-pressure elastic behavior

165 The unit-cell parameters at eighteen P -points up to 9.44(5) GPa, and three points in decompression, are
166 reported in Table 1. The P -induced evolution of the unit-cell parameters is shown in Fig. 2. The evolution of
167 the unit-cell parameters show at least two different compressional regimes. From P_1 to P_6 (1.82 GPa),
168 phillipsite is stiffer than in the second regime [*i.e.*, from P_9 (3.13 GPa) to P_{19} (9.44 GPa)]. Up to P_8 (2.56
169 GPa), the value of the β angle decreases, whereas at $P \geq P_9$ there is a clear inversion of the trend (Fig. 2).
170 The evolution of the β angle is diagnostic for the change of the compressional regimes. For the two regimes,

171 a Birch-Murnaghan Equation of State truncated to the second order was fitted to the experimental P - V data
 172 using the *EoSFit 7.0* software (Angel et al. 2000, 2014). We did not consider the unit-cell parameters of $P7$
 173 (2.14 GPa) and $P8$ in the calculation of the elastic parameters, considering the P -range between $P7$ and $P8$ as
 174 a transitional interval between the two regimes. The refined elastic parameters are reported in Table 10. Bulk
 175 moduli K_V , K_a , K_b , K_c of the first regime (hereafter named K_x^1), are significantly higher than the ones
 176 obtained for the second regime (hereafter named K_x^2), suggesting that, at low pressure, phillipsite is “stiffer”.
 177 In the second regime, the linear bulk moduli decrease drastically and anisotropically (*e.g.*, K_a decreases by
 178 about 2.5 times, whereas K_b and K_c decrease by about 5 times). The reasons of such changes of the elastic
 179 behavior, at the atomic level, will be discussed in the next sessions.

180

181 **4.2 Pressure-induced structural evolution: deformation of the Si/Al framework**

182 The intra-tetrahedral T-O distances (reported in Table 4) do not show drastic changes within the P -
 183 range investigated. The most significant changes of the inter-tetrahedral angles are those observed for the
 184 T1-O7-T3, T2-O8-T2, T4-O6-T2, and T4-O1-T3 angles, reported in Table 11. Fig. 3 shows the trends of
 185 these T-O-T angles (normalized to the value at $P1$). At $P7$, all trends change markedly. The inter-tetrahedral
 186 tilting gives rise to a pronounced increase of the ellipticity of all the 8-mRs. In order to explain the behavior of
 187 the 8-mRs, we introduce the ε parameter (*i.e.*, the ellipticity ratio) as the b/a ratio, where b is the minor and a
 188 the major axis of any given ring (*e.g.*, Gatta and Lee 2007; Gatta et al. 2009a). The ε -ratio for the 8-
 189 mRs[100]-1 (hereafter $\varepsilon_{8\text{-mRs}[100]-1}$) is defined as O9-O8/O7-O7 (with O7-O7 > O9-O8); for the 8-mRs[100]-2,
 190 the ε -ratio (hereafter $\varepsilon_{8\text{-mRs}[100]-2}$) is defined as O7-O7/O9-O8 (as O7-O7 < O9-O8). For the 8-mRs[010] and
 191 the 8-mRs(001) (hereafter $\varepsilon_{8\text{-mRs}[010]}$ and $\varepsilon_{8\text{-mRs}(001)}$), the ε ratios are defined as O3-O3/O1-O1 and O9-O8/O5-
 192 O5, respectively. The trend of all the ε values of the 8-mRs are shown in Fig. 4. Every ring tends to increase
 193 its ellipticity with the pressure increase, as previously observed in several others zeolites (*e.g.* Gatta et al.
 194 2005, 2009b; Lotti et al. 2016). Contrarily to what observed by Gatta et al. (2007), the ε ratio of the 8-
 195 mRs[100]-2 is more pronounced than that of the 8mRs[100]-1 one. This feature is maintained at high- P and,
 196 interestingly, the trends of $\varepsilon_{8\text{-mRs}[100]-1}$, $\varepsilon_{8\text{-mRs}[100]-2}$ and $\varepsilon_{8\text{-mRs}[010]}$ are practically parallel (Fig. 4). However, at a
 197 careful analysis from $P7$ to $P11$, $\varepsilon_{8\text{-mRs}[100]-2}$ decreases more pronouncedly than $\varepsilon_{8\text{-mRs}[100]-1}$ and $\varepsilon_{8\text{-mRs}[010]}$. In
 198 fact, in the considered P -range, the slope of $\varepsilon_{8\text{-mRs}[100]-2}$ is -0.059(2), whereas the slope of both $\varepsilon_{8\text{-mRs}[100]-1}$ and

199 $\varepsilon_{8\text{-mRs}[010]}$ is -0.052(3): the 8-mRs[100]-2 is, therefore, more affected by the P -induced deformation than 8-
200 mRs[100]-1 and 8-mRs[010].

201 If the normalized O3-O3 and O7-O7 diameters of the 8-mRs[010] are plotted vs. P , the trend are
202 almost parallel up to $P7$ (Fig 5). At $P > P7$, the diameter O3-O3 begins to decrease abruptly, whereas O7-O7
203 slightly increases. As the diameter O7-O7 is parallel to [100] and O3-O3 almost parallel to [001], this can
204 explain the observed $K_a > K_c$ at $P > P7$ (Table 10).

205 It is also interesting to note that at $P8$ the β angle reverses its negative trend with P , and begins to
206 increase. The change of β is somehow related to some T-O-T angles. We expect that the evolution of β might
207 depend on the evolution of the inter-tetrahedral angles of the 8-mRs[010], and in particular on a combination
208 of the T3-O1-T4 and T2-O6-T4 angles (Fig. 1). More in detail, if T3-O1-T4 and T2-O6-T4 were lying on the
209 same plane (perpendicular to [010]), at an increase of their values would correspond a decrease of β . They
210 actually do not lie on the same plane; however, if the value of the difference [(T2-O6-T4)-(T3-O1-T4)] is
211 plotted vs. pressure (Fig. 6), an almost overlapped trend to that of β is observed. This finding suggests that
212 the combined effect of the T3-O1-T4 and T2-O6-T4 angles evolution can play a role in the evolution of the β
213 angle, and thus on the distortion of the (monoclinic) unit-cell.

214

215 **4.3 Pressure-induced structural evolution: evolution of the extra-framework population**

216 *4.3.1 W sites*

217 The first changes in the evolution of the extra-framework population are already observed at low- P
218 regime. At $P2$, the analysis of the difference-Fourier maps of the electron density showed the presence of a
219 maximum close (but distinct) to the position of W2. This peak, labelled as W2' in this study, was not found
220 in the analysis of the difference-Fourier maps at $P1$. Although we cannot exclude that the occupancies of the
221 H₂O sites are influenced by the constrains adopted for the DP values, it is possible that the sum of the
222 occupancies of W2 and W2' (which are mutually exclusive) at $P2$ is equal, within the *e.s.d.*, to the
223 occupancy of W2 site at $P1$. The distances W2'-O8 (*i.e.*, 2.878(3) Å) and W2'-O2 (*i.e.*, 2.893(3) Å) at $P2$ are
224 shorter than the distances W2-O8 (*i.e.*, 3.205(3) Å) and W2-O2 (*i.e.*, 3.076(3) Å), and this suggests that the
225 new W2' site is involved in an energetically more favorable H-bonding network if compared to W2. At $P9$,
226 the two maxima ascribable to W2 and W2' were not distinctly observed anymore: only one distinct electron-

227 density peak was found. As the distance between the two subsites decreases significantly from P_6 to P_8
228 (from $\sim 1 \text{ \AA}$ to $\sim 0.75 \text{ \AA}$, respectively), it is highly likely that they converge to one site at P_9 (3.13 GPa), here
229 re-labelled as W2 (Table 3, Fig. 7). It is worth to point out that the occupancy of W2 at P_9 is slightly lower
230 than the sum of the W2 and W2' sites at P_8 (Table 3).

231 As pressure increases, the distance between W1 and Ca decreases (Table 5), toward non-realistic
232 values expected for a Ca-W distance (Fig. 7). This finding suggests that Ca and W1 are actually two
233 mutually exclusive sites, even in the low- P regime. An additional finding concerns the “migration” of W1
234 out of the 8-mRs[100]-1. Such a behaviour implies a change of its H-bonding scheme. As reported in Table
235 5, at P_1 the distance W1-O9 and W1-O3 are 2.940(3) and 3.081(3)Å, respectively. The same distances at
236 P_{11} are 2.690(3) and 3.229(3) Å, respectively, which means that the distance W1-O9 decreases by $\sim 9\%$,
237 whereas the W1-O3 increases by $\sim 4.5\%$.

238 The analysis of the difference-Fourier maps, based on the refinements at P_{10} and P_{11} , revealed the
239 presence of two new maxima, here labeled as W2'' and W1', lying in the 8-mRs[100]-2 and 8-mRs[100]-1
240 rings, respectively (Table 3, Fig. 7), with partial site occupancy and mutually exclusive with the co-
241 respective W1 and W2 (Table 3). These new sites have distances with some framework oxygen sites
242 ascribable to H-bond interactions (*e.g.*, W1'-O9 $\sim 2.9 \text{ \AA}$, W2''-O8 $\sim 2.5 \text{ \AA}$, W2''-O2 $\sim 2.6 \text{ \AA}$).

243 Additional effects of H₂O migration among the W sites are observed at W4, W5 and W6. The
244 fractional coordinates of the W3, W5 and W6 sites do not show any substantial change with the increase of
245 pressure. The occupancy of the W4 sites decreases as pressure rises, whereas the occupancies of W5 and W6
246 increase. At $P > P_9$, no evidence of the W4 site was found in the difference-Fourier maps, coupled with
247 significantly higher densities at W5 and W6 than those observed at P_1 (Fig. 8).

248 A general view of the P -induced changes involving the extra-framework population is shown in Fig.
249 7.

250

251 4.3.2 Ca and K1-K2 sites

252 As reported in Table 5, the distance Ca-O7 increases with pressure, whereas the distances Ca-O4 and
253 Ca-O3 decrease. This trend leads the Ca site toward the mirror plane located at $y = \frac{1}{4}$. This behavior might

254 be correlated to the tilting of the TO_4 tetrahedra and, in particular, to the closure of the O4-O7-O3 angle in
255 the 8-mRs[100]-1.

256 The structural data show also a correlation between the distances K1/K2-O1 and K1/K2-O8 and the
257 inter-tetrahedral angles T3-O1-T4 and T2-O8-T2, respectively. As explained in the previous section, the
258 principal effect of the hydrostatic compression on the 8-mRs(001) is the tilting of the TO_4 tetrahedra, which
259 leads to a reduction of the T3-O1-T4 and T2-O8-T2 angles with pressure. The decrease of the
260 aforementioned angles leads to a shortening of the K1/K2-O1 and K1/K2-O8 distances (Table 5).

261

262 5. Discussion and conclusions

263 This is the first experiment in which the high- P behavior of a natural phillipsite is described on the basis
264 of single-crystal X-ray diffraction data (collected up to 9.4 GPa). The previous experiment on phillipsite was
265 conducted on a polycrystalline sample up to 3.6 GPa (Gatta and Lee 2007). Gatta and Lee (2007) described
266 the elastic behavior of phillipsite on the basis of powder data. However, the low quality of the powder data
267 themselves, along with the modest P -range investigated (*i.e.*, $P_{\text{max}} = 3.6$ GPa), did not allow the authors to
268 have a clear picture of the high- P behavior of this zeolite, and only one BM-EoS was used to model its
269 compressibility. A potential change of the compressional behavior was already reported by Gatta and Lee
270 (2007) at $P > 2$ GPa. In this study, we used the same natural sample previously used by Gatta and Lee
271 (2007). In this light, this work can be considered as an extension of the first study. Also in this case, we
272 observe a change of the compressional behavior of phillipsite between 2.0-2.5 GPa, which is not due by a
273 potential penetration of the P -fluid molecules. The inversion of β -trend is likely the most evident effect of
274 such a change. The diffraction patterns and the structure refinements confirmed that the $P2_1/m$ is preserved
275 within the entire P -range investigated (*i.e.*, 0 – 9.4 GPa). Therefore, the change of the elastic behavior does
276 not reflect a phase transition, but rather a change of the deformation mechanisms at the atomic scale.

277 More specifically, phillipsite experiences a “softening” at $P > 2$ -2.5 GPa, and the bulk modulus **in** the
278 low- P regime is drastically higher than that of the high- P regime (*i.e.*, 89(8) vs. 18.8(7) GPa, Table 10). A
279 similar behavior was previously observed in other open-framework materials (*e.g.*, Gatta et al. 2006, 2008,
280 **2009b**, 2012). As the tetrahedra behave as rigid units (at least at a first approximation), the structure
281 deformation is basically governed by tetrahedral tilting and by the rearrangement of the extra-framework

282 population, as usually observed in zeolites (*e.g.*, Gatta 2008, Gatta and Lee 2014, Gatta et al. 2014, Lotti et
283 al. 2016).

284 The elastic anisotropic scheme of phillipsite is preserved within the P -range investigated, with
285 $K_a > K_c > K_b$. The structure is, therefore, more compressible along [010]. From the low- to the high- P regime,
286 the linearized bulk modulus K_b decreases from 50(5) to 12(1) GPa. Such a behavior might be somehow
287 influenced by a change of the extra-framework population and, more specifically, by the disappearance of
288 the W4 site. W4 (along with W5 and W6) lies almost in the center of the 8-mRs[010] channel, in such a way
289 that a helicoidally H₂O-chain occurs. The lack of W4 implies a reduced “pillar effect” of the H₂O-chain (Fig.
290 7 and 8). As the H₂O-chain is perpendicular to (010), its weakening does not affect significantly the
291 compressibility along [100] or [001]. However, if the ratio O7-O7/O3-O3 is plotted vs. P , where O3-O3 and
292 O7-O7 are two independent diameters of the 8-mRs[010] channel, we observe an almost horizontal trend up
293 to $P7$ and then a drastic increase at $P > P7$ (Fig. 5). Therefore, one of the reasons of the softening along [100]
294 and [001] can be ascribed to the tilting of the 8-mRs[010]-tetrahedra, in response to the disappearance of
295 W4. The tilting causes the deformation of the 8-mRs[010] channel and, in turn, the β -inversion (as described
296 in the section 4.2).

297 An additional cause of the elastic anisotropy may be correlated to the migration of W1. The lack of W1
298 at high- P , in the 8-mRs[100]-1, leads to a significant shortening of the O8-O9 diameter, which is
299 perpendicular to [001]. Therefore, the migration of W1 cannot affect K_a or K_b but only K_c .

300 There is not a unique explanation about the H₂O sites migration at high pressure and the occurrence of
301 subsites, *e.g.* W1', W2', W2'' (Table 3), as described in the section 4.3.1. The lack of the proton positions
302 does not allow a clear view of the H-bonding network. However, it appears that the framework deformation
303 leads to energetically most favorable H-bonding connection with H₂O molecules located in a slightly
304 different positions than the parent ones (at room conditions), promoting split and, in general, H₂O sites
305 migration.

306

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314 7. References

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Table 1. Unit-cell parameters of the zeolite phillipsite with P . P_{19-21} in decompression.

P_n	$P(\text{GPa})$	$V(\text{\AA}^3)$	$a(\text{\AA})$	$b(\text{\AA})$	$c(\text{\AA})$	$\beta(^{\circ})$
P_1	0.20(5)	1001.6(3)	9.8934(4)	14.184(2)	8.6998(3)	124.874(6)
P_2	0.60(5)	1000.2(3)	9.8982(4)	14.153(2)	8.6941(4)	124.792(7)
P_3	0.94(5)	993.8(3)	9.8780(4)	14.105(2)	8.6790(4)	124.733(7)
P_4	1.22(5)	991.1(3)	9.8675(4)	14.082(2)	8.6739(4)	124.683(7)
P_{4b}	1.22(5)	991.6(3)	9.8689(4)	14.085(2)	8.6756(4)	124.685(6)
P_5	1.60(5)	988.8(3)	9.8546(5)	14.068(2)	8.6681(5)	124.631(8)
P_6	1.82(5)	985.3(3)	9.8402(4)	14.051(2)	8.6585(4)	124.612(7)
P_7	2.14(5)	973.4(3)	9.7930(4)	13.995(2)	8.6242(4)	124.560(6)
P_8	2.57(5)	965.2(3)	9.7643(4)	13.952(2)	8.6013(4)	124.539(7)
P_9	3.13(5)	956.9(3)	9.7536(5)	13.886(3)	8.5839(5)	124.610(8)
P_{10}	3.92(5)	941.8(3)	9.7283(7)	13.782(4)	8.5434(8)	124.70(1)
P_{11}	4.85(5)	913.0(3)	9.6822(9)	13.569(4)	8.468(1)	124.85(2)
P_{12}	5.26(5)	900.4(5)	9.6498(9)	13.490(4)	8.432(1)	124.88(2)
P_{13}	6.14(5)	881.0(3)	9.5903(7)	13.379(4)	8.3692(8)	124.88(1)
P_{14}	6.71(5)	864.6(3)	9.5410(9)	13.279(4)	8.323(1)	124.93(2)
P_{15}	7.48(5)	853.8(3)	9.514(1)	13.203(5)	8.300(1)	125.02(2)
P_{16}	8.20(5)	841.7(3)	9.477(1)	13.137(6)	8.264(1)	125.11(2)
P_{17}	8.73(5)	829.6(4)	9.435(2)	13.092(7)	8.220(2)	125.20(3)
P_{18}	9.44(5)	821.1(4)	9.393(2)	13.084(8)	8.187(2)	125.31(3)
P_{19}	1.93(5)	989.8(3)	9.8283(7)	14.103(3)	8.6691(5)	124.539(9)
P_{20}	1.93(5)	971.9(3)	9.7718(5)	14.008(2)	8.6196(4)	124.537(7)
P_{21}	0.50(5)	1007.9(4)	9.925(1)	14.181(5)	8.730(1)	124.88(2)

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398 **Table 2 (deposited).** Details pertaining to the structure refinements of phillipsite at different pressures.
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	P_1 0.20 GPa	P_2 0.60 GPa	P_3 0.94 GPa	P_4 1.22 GPa	P_5 1.60 GPa	P_6 1.82 GPa	P_7 2.14 GPa
$\min \leq h \leq \max$	-16; 16	-15; 15	-16; 15	-16; 15	-16; 15	-16; 15	-15; 15
$\min \leq k \leq \max$	-10; 10	-10; 12	-10; 11	-11; 11	-11; 11	-10; 11	-11; 11
$\min \leq l \leq \max$	-13; 12	-14; 14	-14; 14	-13; 14	-13; 14	-13; 14	-13; 14
Unique reflections	1934	1999	1860	1841	1839	1812	1823
Observed reflections $I > 3\sigma(I)$	1181	1500	1395	1360	1356	1312	1349
Number of refined parameters	82	84	84	84	84	83	84
Number of restraints	2	1	1	1	1	1	1
R_{int} (obs)	0.067	0.078	0.078	0.084	0.081	0.083	0.089
R_{int} (all)	0.080	0.088	0.087	0.092	0.091	0.093	0.097
R_1 (obs)	0.0224	0.0232	0.0250	0.0269	0.0253	0.0278	0.0229
R_1 (all)	0.0255	0.0244	0.0261	0.0279	0.0262	0.0289	0.0240
wR_1 (obs)	0.0803	0.0928	0.0907	0.0974	0.0955	0.0980	0.1063
wR_1 (all)	0.0809	0.0945	0.0911	0.0978	0.0960	0.0985	0.1067
Residuals ($e/\text{\AA}^3$)	+0.23; -0.17	+0.22; -0.24	+0.25; -0.26	+0.24; -0.28	+0.19; -0.19	+0.22; -0.23	+0.20; -0.23

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	P_8 2.57 GPa	P_9 3.13 GPa	P_{10} 3.92 GPa	P_{11} 4.85 GPa	P_{21} 0.50 GPa
$\min \leq h \leq \max$	-15; 16	-15; 15	-15; 15	-15; 14	-13; 10
$\min \leq k \leq \max$	-10; 11	-10; 11	-9; 10	-9; 10	-11; 8
$\min \leq l \leq \max$	-13; 14	-12; 14	-11; 13	-11; 13	-8; 14
Unique reflections	1803	1762	1888	1559	1884
Observed reflections $I > 3\sigma(I)$	1297	1232	1022	813	1154
Number of refined parameters	83	84	83	83	80
Number of restraints	1	2	2	2	1
R_{int} (obs)	0.102	0.114	0.130	0.162	0.090
R_{int} (all)	0.110	0.126	0.153	0.192	0.010
R_1 (obs)	0.0718	0.0444	0.0392	0.0570	0.0826
R_1 (all)	0.0729	0.0457	0.0440	0.0612	0.0862
wR_1 (obs)	0.1167	0.1297	0.1458	0.1673	0.1027
wR_1 (all)	0.1174	0.1303	0.1469	0.1685	0.1033
Residuals ($e/\text{\AA}^3$)	+0.26; -0.27	+0.29; -0.25	+0.21; -0.23	+0.34; -0.33	+0.29; -0.23

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404 **Table 3 (deposited).** Refined positional and displacement parameters of phillipsite at different pressures. (*)
 405 fixed value ;(**) value refined with a restrain.
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Site	<i>P</i> (GPa)	<i>s.o.f.</i>	<i>x</i>	<i>y</i>	<i>z</i>	<i>U</i> _{iso} (Å ²)	
Ca	<i>P</i> ₁ (0.20)	0.31(1)	0.6672(9)	0.372(1)	0.562(1)	0.041(4)	407
	<i>P</i> ₂ (0.60)	0.308*	0.674(1)	0.370(1)	0.572(1)	0.048(2)	408
	<i>P</i> ₃ (0.94)	0.308*	0.678(1)	0.367(1)	0.574(1)	0.048(2)	409
	<i>P</i> ₄ (1.22)	0.308*	0.681(1)	0.365(1)	0.575(1)	0.049(2)	410
	<i>P</i> ₅ (1.60)	0.308*	0.684(1)	0.362(1)	0.577(1)	0.049(2)	411
	<i>P</i> ₆ (1.82)	0.308*	0.685(1)	0.362(1)	0.577(1)	0.050(2)	412
	<i>P</i> ₇ (2.14)	0.308*	0.687(1)	0.360(1)	0.578(1)	0.047(2)	413
	<i>P</i> ₈ (2.57)	0.308*	0.687(1)	0.359(1)	0.577(1)	0.042(2)	414
	<i>P</i> ₉ (3.13)	0.308*	0.690(2)	0.356(2)	0.577(2)	0.055(3)	415
	<i>P</i> ₁₀ (3.92)	0.308*	0.682(2)	0.357(3)	0.576(3)	0.075(5)	416
	<i>P</i> ₁₁ (4.85)	0.308*	0.684(4)	0.361(5)	0.580(5)	0.12(1)	417
T1(Si)	<i>P</i> ₁ (0.20)	1.00	0.7264(3)	0.0073(3)	0.2855(3)	0.0139(6)	418
	<i>P</i> ₂ (0.60)	1.00	0.7256(2)	0.0068(3)	0.2861(3)	0.0113(6)	419
	<i>P</i> ₃ (0.94)	1.00	0.7254(2)	0.0073(3)	0.2863(3)	0.0112(6)	420
	<i>P</i> ₄ (1.22)	1.00	0.7250(3)	0.0074(3)	0.2865(3)	0.0114(6)	421
	<i>P</i> ₅ (1.60)	1.00	0.7249(2)	0.0073(3)	0.2870(3)	0.0127(6)	422
	<i>P</i> ₆ (1.82)	1.00	0.7246(3)	0.0071(3)	0.2867(3)	0.0127(6)	423
	<i>P</i> ₇ (2.14)	1.00	0.7241(3)	0.0071(3)	0.2869(3)	0.0142(7)	424
	<i>P</i> ₈ (2.57)	1.00	0.7234(3)	0.0063(4)	0.2871(4)	0.0144(8)	425
	<i>P</i> ₉ (3.13)	1.00	0.7231(4)	0.0042(4)	0.2883 (4)	0.0178(9)	426
	<i>P</i> ₁₀ (3.92)	1.00	0.7212(5)	0.0003(6)	0.2891(6)	0.024(1)	427
	<i>P</i> ₁₁ (4.85)	1.00	0.7213(6)	-0.0050(8)	0.2923(7)	0.031(1)	428
T2(Si)	<i>P</i> ₁ (0.20)	1.00	0.4207(2)	0.1390(3)	0.0435(3)	0.0147(6)	429
	<i>P</i> ₂ (0.60)	1.00	0.4210(2)	0.1384(3)	0.0454(3)	0.0135(6)	430
	<i>P</i> ₃ (0.94)	1.00	0.4211(2)	0.1383(3)	0.0458(3)	0.0140(6)	431
	<i>P</i> ₄ (1.22)	1.00	0.4213(3)	0.1377(3)	0.0461(3)	0.0145(6)	432
	<i>P</i> ₅ (1.60)	1.00	0.4214(3)	0.1376(3)	0.0461(3)	0.0162(6)	433
	<i>P</i> ₆ (1.82)	1.00	0.4213(3)	0.1375(3)	0.0458(3)	0.0166(6)	434
	<i>P</i> ₇ (2.14)	1.00	0.4213(3)	0.1374(3)	0.0459(4)	0.0187(7)	435
	<i>P</i> ₈ (2.57)	1.00	0.4221(4)	0.1371(4)	0.0488(4)	0.0181(8)	436
	<i>P</i> ₉ (3.13)	1.00	0.4209(4)	0.1361(5)	0.0532(5)	0.0250(9)	437
	<i>P</i> ₁₀ (3.92)	1.00	0.4193(5)	0.1342(6)	0.0618(6)	0.032(1)	438
	<i>P</i> ₁₁ (4.85)	1.00	0.4167(7)	0.1308(9)	0.0725(8)	0.040(2)	439
	<i>P</i> ₂₁ (0.50)	1.00	0.4214(3)	0.1384(3)	0.0453(4)	0.0206(7)	440

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Site	P (GPa)	$s.o.f.$	x	y	z	$U_{iso}(\text{\AA}^2)$	
							448
T3(Si)	$P_1(0.20)$	1.00	0.0434(3)	0.0251(3)	0.2807(3)	0.0140(6)	449
	$P_2(0.60)$	1.00	0.0430(2)	0.0271(3)	0.2803(3)	0.0105(6)	450
	$P_3(0.94)$	1.00	0.0432(2)	0.0275(3)	0.2804(3)	0.0114(6)	451
	$P_4(1.22)$	1.00	0.0435(3)	0.0279(3)	0.2806(3)	0.0116(6)	452
	$P_5(1.60)$	1.00	0.0441(2)	0.0286(3)	0.2810(3)	0.0126(6)	453
	$P_6(1.82)$	1.00	0.0441(3)	0.0288(3)	0.2810(3)	0.0128(6)	454
	$P_7(2.14)$	1.00	0.0442(3)	0.0297(3)	0.2810(3)	0.0152(7)	455
	$P_8(2.57)$	1.00	0.0436(3)	0.0307(4)	0.2807(4)	0.0140(7)	456
	$P_9(3.13)$	1.00	0.0426(4)	0.0332(4)	0.2814(4)	0.0190(9)	457
	$P_{10}(3.92)$	1.00	0.0389(4)	0.0348(6)	0.2813(5)	0.023(1)	458
	$P_{11}(4.85)$	1.00	0.0352(6)	0.0396(8)	0.2816(8)	0.033(1)	459
	$P_{21}(0.50)$	1.00	0.0438(3)	0.0270(3)	0.2809(3)	0.0183(7)	460
T4(Si)	$P_1(0.20)$	1.00	0.0855(3)	0.1408(3)	0.0053(3)	0.0155(6)	461
	$P_2(0.60)$	1.00	0.0838(2)	0.1406(3)	0.0039(3)	0.0122(6)	462
	$P_3(0.94)$	1.00	0.0832(2)	0.1401(3)	0.0027(3)	0.0122(6)	463
	$P_4(1.22)$	1.00	0.0826(3)	0.1400(3)	0.0022(3)	0.0119(6)	464
	$P_5(1.60)$	1.00	0.0816(3)	0.1401(3)	0.0014(3)	0.0134(6)	465
	$P_6(1.82)$	1.00	0.0815(3)	0.1403(3)	0.0013(3)	0.0131(6)	466
	$P_7(2.14)$	1.00	0.0803(3)	0.1399(3)	0.0003(3)	0.0146(7)	467
	$P_8(2.57)$	1.00	0.0785(3)	0.1399(4)	-0.0014(4)	0.0140(8)	468
	$P_9(3.13)$	1.00	0.0750(4)	0.1398(4)	-0.0042(4)	0.0185(9)	469
	$P_{10}(3.92)$	1.00	0.0702(4)	0.1387(6)	-0.0090(5)	0.023(1)	470
	$P_{11}(4.85)$	1.00	0.0624(6)	0.1378(8)	-0.0176(7)	0.030(1)	471
	$P_{21}(0.50)$	1.00	0.0842(3)	0.1403(3)	0.0044(4)	0.0194(7)	472
O1	$P_1(0.20)$	1.00	0.0637(7)	0.1122(9)	0.1739(8)	0.027(2)	473
	$P_2(0.60)$	1.00	0.0625(7)	0.1160(8)	0.1738(8)	0.021(1)	474
	$P_3(0.94)$	1.00	0.0616(7)	0.1178(8)	0.1747(8)	0.020(1)	475
	$P_4(1.22)$	1.00	0.0628(7)	0.1187(8)	0.1763(9)	0.021(2)	476
	$P_5(1.60)$	1.00	0.0625(7)	0.1199(8)	0.1765(8)	0.023(1)	477
	$P_6(1.82)$	1.00	0.0633(7)	0.1197(8)	0.1772(9)	0.022(2)	478
	$P_7(2.14)$	1.00	0.0620(8)	0.1232(9)	0.1782(9)	0.024(2)	479
	$P_8(2.57)$	1.00	0.0598(9)	0.123(1)	0.175(1)	0.025(2)	480
	$P_9(3.13)$	1.00	0.051(1)	0.124(1)	0.170(1)	0.033(2)	481
	$P_{10}(3.92)$	1.00	0.036(1)	0.124(2)	0.155(2)	0.042(3)	482
	$P_{11}(4.85)$	1.00	0.024(2)	0.124(2)	0.149(2)	0.046(4)	483
	$P_{21}(0.50)$	1.00	0.0654(8)	0.1145(9)	0.1769(9)	0.028(2)	484
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Site	P (GPa)	$s.o.f.$	x	y	z	$U_{iso}(\text{Å}^2)$	
O2	$P_1(0.20)$	1.00	0.6325(8)	0.5868(9)	0.1517(9)	0.027(2)	491
	$P_2(0.60)$	1.00	0.6276(7)	0.5864(8)	0.1470(8)	0.025(1)	492
	$P_3(0.94)$	1.00	0.6262(7)	0.5844(9)	0.1470(8)	0.026(1)	493
	$P_4(1.22)$	1.00	0.6230(8)	0.585(1)	0.1441(9)	0.027(2)	494
	$P_5(1.60)$	1.00	0.6226(8)	0.5847(9)	0.1445(9)	0.027(2)	495
	$P_6(1.82)$	1.00	0.6215(8)	0.585(1)	0.144(1)	0.029(2)	496
	$P_7(2.14)$	1.00	0.6194(9)	0.584(1)	0.142(1)	0.030(2)	497
	$P_8(2.57)$	1.00	0.618(1)	0.583(1)	0.141(1)	0.030(2)	498
	$P_9(3.13)$	1.00	0.614(1)	0.585(1)	0.139(1)	0.036(2)	499
	$P_{10}(3.92)$	1.00	0.615(2)	0.588(2)	0.135(2)	0.054(3)	500
	$P_{11}(4.85)$	1.00	0.620(2)	0.585(3)	0.128(2)	0.069(5)	501
	$P_{21}(0.50)$	1.00	0.6272(9)	0.5849(9)	0.148(1)	0.033(2)	502
O3	$P_1(0.20)$	1.00	0.5951(8)	0.0981(9)	0.2257(9)	0.028(2)	503
	$P_2(0.60)$	1.00	0.5940(7)	0.0975(8)	0.2282(9)	0.027(2)	504
	$P_3(0.94)$	1.00	0.5952(7)	0.0971(8)	0.2305(8)	0.026(1)	505
	$P_4(1.22)$	1.00	0.5952(8)	0.0978(9)	0.2319(9)	0.026(2)	506
	$P_5(1.60)$	1.00	0.5962(8)	0.0989(9)	0.2333(9)	0.027(2)	507
	$P_6(1.82)$	1.00	0.5959(8)	0.0988(9)	0.233(1)	0.028(2)	508
	$P_7(2.14)$	1.00	0.5964(9)	0.099(1)	0.235(1)	0.030(2)	509
	$P_8(2.57)$	1.00	0.595(1)	0.099(1)	0.237(1)	0.031(2)	510
	$P_9(3.13)$	1.00	0.597(1)	0.094(1)	0.245(1)	0.038(2)	511
	$P_{10}(3.92)$	1.00	0.592(1)	0.086(2)	0.250(2)	0.044(3)	512
	$P_{11}(4.85)$	1.00	0.587(2)	0.080(2)	0.256(2)	0.042(4)	513
	$P_{21}(0.50)$	1.00	0.5964(9)	0.0962(9)	0.230(1)	0.036(2)	514
O4	$P_1(0.20)$	1.00	0.0371(8)	0.922(1)	0.1834(9)	0.029(2)	515
	$P_2(0.60)$	1.00	0.0359(7)	0.9267(9)	0.1792(9)	0.028(2)	516
	$P_3(0.94)$	1.00	0.0386(7)	0.9281(9)	0.1807(8)	0.026(1)	517
	$P_4(1.22)$	1.00	0.0404(8)	0.929(1)	0.181(1)	0.027(2)	518
	$P_5(1.60)$	1.00	0.0408(8)	0.930(1)	0.1798(9)	0.029(2)	519
	$P_6(1.82)$	1.00	0.0413(8)	0.929(1)	0.180(1)	0.029(2)	520
	$P_7(2.14)$	1.00	0.0439(9)	0.931(1)	0.181(1)	0.030(2)	521
	$P_8(2.57)$	1.00	0.045(1)	0.930(1)	0.182(1)	0.034(2)	522
	$P_9(3.13)$	1.00	0.047(1)	0.928(1)	0.185(1)	0.039(3)	523
	$P_{10}(3.92)$	1.00	0.054(2)	0.934(2)	0.191(2)	0.056(4)	524
	$P_{11}(4.85)$	1.00	0.061(2)	0.928(2)	0.212(2)	0.057(4)	525
	$P_{21}(0.50)$	1.00	0.0360(9)	0.925(1)	0.180(1)	0.037(2)	526
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Site	P (GPa)	$s.o.f.$	x	y	z	$U_{iso}(\text{\AA}^2)$	
O5	$P_1(0.20)$	1.00	0.8765(7)	0.0448(8)	0.2738(8)	0.026(2)	532
	$P_2(0.60)$	1.00	0.8756(7)	0.0441(8)	0.2719(8)	0.023(1)	533
	$P_3(0.94)$	1.00	0.8762(7)	0.0451(8)	0.2734(8)	0.026(1)	534
	$P_4(1.22)$	1.00	0.8768(8)	0.0454(9)	0.2744(9)	0.026(2)	535
	$P_5(1.60)$	1.00	0.8749(8)	0.0456(9)	0.2723(9)	0.029(2)	536
	$P_6(1.82)$	1.00	0.8755(8)	0.0461(9)	0.273(1)	0.029(2)	537
	$P_7(2.14)$	1.00	0.8732(9)	0.045(1)	0.270(1)	0.034(2)	538
	$P_8(2.57)$	1.00	0.873(1)	0.046(1)	0.272(1)	0.032(2)	539
	$P_9(3.13)$	1.00	0.872(1)	0.045(1)	0.274(1)	0.043(3)	540
	$P_{10}(3.92)$	1.00	0.871(1)	0.048(2)	0.278(2)	0.047(3)	541
	$P_{11}(4.85)$	1.00	0.871(2)	0.046(2)	0.289(2)	0.053(4)	542
	$P_2(0.50)$	1.00	0.8756(8)	0.0470(9)	0.2730(9)	0.030(2)	543
O6	$P_1(0.20)$	1.00	0.2804(8)	0.3763(9)	0.0861(8)	0.028(1)	544
	$P_2(0.60)$	1.00	0.2804(7)	0.3778(8)	0.0876(9)	0.024(1)	545
	$P_3(0.94)$	1.00	0.2790(7)	0.3784(8)	0.0855(9)	0.024(1)	546
	$P_4(1.22)$	1.00	0.2785(8)	0.3793(9)	0.084(1)	0.026(2)	547
	$P_5(1.60)$	1.00	0.2766(8)	0.3789(9)	0.0824(9)	0.028(2)	548
	$P_6(1.82)$	1.00	0.2775(8)	0.3794(9)	0.084(1)	0.028(2)	549
	$P_7(2.14)$	1.00	0.2749(9)	0.380(1)	0.081(1)	0.030(1)	550
	$P_8(2.57)$	1.00	0.272(1)	0.381(1)	0.078(1)	0.030(2)	551
	$P_9(3.13)$	1.00	0.271(1)	0.383(1)	0.082(1)	0.040(3)	552
	$P_{10}(3.92)$	1.00	0.266(1)	0.388(2)	0.086(2)	0.045(3)	553
	$P_{11}(4.85)$	1.00	0.262(2)	0.393(2)	0.093(2)	0.049(4)	554
	$P_2(0.50)$	1.00	0.2808(9)	0.3764(9)	0.087(1)	0.036(2)	555
O7	$P_1(0.20)$	1.00	0.7934(7)	0.5203(8)	0.5026(7)	0.022(1)	556
	$P_2(0.60)$	1.00	0.7937(7)	0.5216(8)	0.5014(8)	0.022(1)	557
	$P_3(0.94)$	1.00	0.7938(7)	0.5224(8)	0.5021(8)	0.023(1)	558
	$P_4(1.22)$	1.00	0.7925(8)	0.5227(9)	0.5012(9)	0.024(2)	559
	$P_5(1.60)$	1.00	0.7925(8)	0.5243(9)	0.5013(9)	0.027(2)	560
	$P_6(1.82)$	1.00	0.7917(8)	0.5241(9)	0.501(1)	0.027(2)	561
	$P_7(2.14)$	1.00	0.7931(9)	0.526(1)	0.503(1)	0.032(2)	562
	$P_8(2.57)$	1.00	0.794(1)	0.529(1)	0.504(1)	0.033(2)	563
	$P_9(3.13)$	1.00	0.792(1)	0.535(1)	0.505(1)	0.040(2)	564
	$P_{10}(3.92)$	1.00	0.790(1)	0.543(2)	0.500(2)	0.042(3)	565
	$P_{11}(4.85)$	1.00	0.788(2)	0.554(2)	0.498(2)	0.049(4)	566
	$P_2(0.50)$	1.00	0.7941(8)	0.5229(9)	0.5024(9)	0.028(2)	567

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Site	P (GPa)	$s.o.f.$	x	y	z	$U_{iso}(\text{\AA}^2)$	
O8	$P_1(0.20)$	0.50	0.550(1)	3/4	-0.019(1)	0.033(2)	574
	$P_2(0.60)$	0.50	0.551(1)	3/4	-0.019(1)	0.030(2)	575
	$P_3(0.94)$	0.50	0.552(1)	3/4	-0.018(1)	0.036(2)	576
	$P_4(1.22)$	0.50	0.554(1)	3/4	-0.017(1)	0.033(3)	577
	$P_5(1.60)$	0.50	0.557(1)	3/4	-0.014(2)	0.040(3)	578
	$P_6(1.82)$	0.50	0.556(1)	3/4	-0.014(2)	0.038(3)	579
	$P_7(2.14)$	0.50	0.558(2)	3/4	-0.011(2)	0.044(3)	580
	$P_8(2.57)$	0.50	0.554(2)	3/4	-0.017(2)	0.047(4)	581
	$P_9(3.13)$	0.50	0.552(2)	3/4	-0.029(2)	0.059(5)	582
	$P_{10}(3.92)$	0.50	0.545(3)	3/4	-0.050(3)	0.080(7)	583
	$P_{11}(4.85)$	0.50	0.546(4)	3/4	-0.069(5)	0.10(1)	584
O9	$P_1(0.20)$	0.50	0.026(1)	1/4	-0.061(1)	0.029(2)	585
	$P_2(0.60)$	0.50	0.028(1)	1/4	-0.063(1)	0.026(2)	586
	$P_3(0.94)$	0.50	0.028(1)	1/4	-0.067(1)	0.027(2)	587
	$P_4(1.22)$	0.50	0.028(1)	1/4	-0.068(1)	0.025(2)	588
	$P_5(1.60)$	0.50	0.027(1)	1/4	-0.071(1)	0.028(2)	589
	$P_6(1.82)$	0.50	0.026(1)	1/4	0.071(1)	0.028(2)	590
	$P_7(2.14)$	0.50	0.026(1)	1/4	-0.073(1)	0.032(2)	591
	$P_8(2.57)$	0.50	0.023(1)	1/4	-0.079(2)	0.033(3)	592
	$P_9(3.13)$	0.50	0.022(2)	1/4	-0.084(2)	0.040(3)	593
	$P_{10}(3.92)$	0.50	0.017(2)	1/4	-0.097(3)	0.050(5)	594
	$P_{11}(4.85)$	0.50	0.022(3)	1/4	-0.097(4)	0.069(7)	595
K1	$P_1(0.20)$	0.59(2)	0.862(1)	1/4	0.226(2)	0.048(2)	596
	$P_2(0.60)$	0.49(2)	0.854(1)	1/4	0.220(1)	0.041(2)	597
	$P_3(0.94)$	0.46(2)	0.848(1)	1/4	0.215(2)	0.039(1)	598
	$P_4(1.22)$	0.44(2)	0.845(1)	1/4	0.212(3)	0.038(2)	599
	$P_5(1.60)$	0.42(3)	0.842(2)	1/4	0.209(3)	0.041(2)	600
	$P_6(1.82)$	0.42(3)	0.841(2)	1/4	0.208(3)	0.039(2)	601
	$P_7(2.14)$	0.50(4)	0.836(2)	1/4	0.199(3)	0.040(2)	602
	$P_8(2.57)$	0.51(4)	0.833(2)	1/4	0.199(3)	0.037(2)	603
	$P_9(3.13)$	0.50(4)	0.827(2)	1/4	0.197(4)	0.041(2)	604
	$P_{10}(3.92)$	0.48(4)	0.825(3)	1/4	0.208(5)	0.059(3)	605
	$P_{11}(4.85)$	0.53(7)	0.819(5)	1/4	0.211(8)	0.106(6)	606
	$P_{21}(0.50)$	0.51(2)	0.853(1)	1/4	0.217(2)	0.048(2)	607
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Site	P (GPa)	$s.o.f.$	x	y	z	$U_{iso}(\text{\AA}^2)$	
K2	$P_1(0.20)$	0.33**	0.823(2)	1/4	0.152(3)	0.048(2)**	617
	$P_2(0.60)$	0.43**	0.817(1)	1/4	0.147(2)	0.041(2)**	618
	$P_3(0.94)$	0.46**	0.817(1)	1/4	0.147(2)	0.039(1)**	619
	$P_4(1.22)$	0.48**	0.816(1)	1/4	0.147(2)	0.038(2)**	620
	$P_5(1.60)$	0.50**	0.815(2)	1/4	0.148(3)	0.041(2)**	621
	$P_6(1.82)$	0.50**	0.811(2)	1/4	0.142(4)	0.040(2)**	622
	$P_7(2.14)$	0.42**	0.808(2)	1/4	0.139(4)	0.037(2)**	623
	$P_8(2.57)$	0.41**	0.808(2)	1/4	0.139(4)	0.037(2)**	624
	$P_9(3.13)$	0.42**	0.803(2)	1/4	0.137(4)	0.041(2)**	625
	$P_{10}(3.92)$	0.44**	0.797(3)	1/4	0.136(5)	0.059(3)**	626
	$P_{11}(4.85)$	0.39**	0.787*	1/4	0.135*	0.106(6)*	627
W1	$P_1(0.20)$	0.41**	0.814(2)	1/4	0.141(3)	0.048(2)**	628
	$P_2(0.60)$	0.62(4)	0.787(3)	1/4	0.530(3)	0.079(4)	629
	$P_3(0.94)$	0.32(4)	0.787(6)	1/4	0.531(7)	0.075*	630
	$P_4(1.22)$	0.21(4)	0.782(8)	1/4	0.54(1)	0.075*	631
	$P_5(1.60)$	0.17(4)	0.77(1)	1/4	0.56(1)	0.075*	632
	$P_6(1.82)$	0.20(4)	0.72(1)	1/4	0.56(1)	0.075*	633
	$P_7(2.14)$	0.16(4)	0.73(1)	1/4	0.56(1)	0.075*	634
	$P_8(2.57)$	0.19(4)	0.72(1)	1/4	0.55(1)	0.075*	635
	$P_9(3.13)$	0.30(5)	0.712(8)	1/4	0.559(9)	0.075*	636
	$P_{10}(3.92)$	0.46(5)	0.699(9)	1/4	0.550(7)	0.075*	637
	$P_{11}(4.85)$	0.35(5)	0.709(9)	1/4	0.568(9)	0.075*	638
W2	$P_1(0.20)$	0.36(6)	0.72(1)	1/4	0.57(1)	0.075*	639
	$P_2(0.60)$	0.42(3)	0.761(4)	1/4	0.582(5)	0.075*	640
	$P_3(0.94)$	0.60(4)	0.779(3)	3/4	0.430(3)	0.079(4)**	641
	$P_4(1.22)$	0.40(4)	0.791(5)	3/4	0.429(6)	0.075*	642
	$P_5(1.60)$	0.33(4)	0.792(7)	3/4	0.426(7)	0.075*	643
	$P_6(1.82)$	0.28(4)	0.798(8)	3/4	0.427(9)	0.075*	644
	$P_7(2.14)$	0.29(4)	0.791(8)	3/4	0.424(9)	0.075*	645
	$P_8(2.57)$	0.29(4)	0.788(8)	3/4	0.421(9)	0.075*	646
	$P_9(3.13)$	0.32(4)	0.791(7)	3/4	0.422(8)	0.075*	647
	$P_{10}(3.92)$	0.30(6)	0.72(1)	3/4	0.39(1)	0.075*	648
	$P_{11}(4.85)$	0.51(4)	0.670(5)	3/4	0.357(6)	0.075*	649
W2	$P_1(0.20)$	0.78(5)	0.659(4)	3/4	0.344(4)	0.075*	650
	$P_2(0.60)$	0.44(6)	0.65(1)	3/4	0.33(1)	0.075*	651
	$P_3(0.94)$	0.47(4)	0.761(4)	3/4	0.418(5)	0.075*	652
	$P_4(1.22)$	0.47(4)	0.761(4)	3/4	0.418(5)	0.075*	653
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Site	P (GPa)	$s.o.f.$	x	y	z	$U_{iso}(\text{\AA}^2)$	659
W3	$P_1(0.20)$	0.96(4)	0.342(1)	0.642(1)	0.158(1)	0.079(4)**	660
	$P_2(0.60)$	0.98(3)	0.342(1)	0.635(1)	0.156(2)	0.075*	661
	$P_3(0.94)$	0.98(3)	0.341(1)	0.632(1)	0.153(2)	0.075*	662
	$P_4(1.22)$	0.99(3)	0.341(1)	0.632(1)	0.154(2)	0.075*	663
	$P_5(1.60)$	0.99(3)	0.340(1)	0.631(1)	0.151(2)	0.075*	664
	$P_6(1.82)$	1.00*	0.340(1)	0.632(1)	0.153(2)	0.075*	665
	$P_7(2.14)$	1.00(3)	0.339(1)	0.630(2)	0.152(2)	0.075*	666
	$P_8(2.57)$	1.00*	0.342(2)	0.633(2)	0.158(2)	0.075*	667
	$P_9(3.13)$	0.98(3)	0.343(2)	0.636(2)	0.163(2)	0.075*	668
	$P_{10}(3.92)$	0.80(3)	0.343(2)	0.632(3)	0.162(3)	0.075*	669
W4	$P_1(0.20)$	0.55(4)	0.427(3)	1/4	0.437(3)	0.079(4)**	670
	$P_2(0.60)$	0.47(4)	0.426(4)	1/4	0.432(5)	0.075*	671
	$P_3(0.94)$	0.43(4)	0.421(4)	1/4	0.427(5)	0.075*	672
	$P_4(1.22)$	0.42(5)	0.422(5)	1/4	0.429(6)	0.075*	673
	$P_5(1.60)$	0.36(5)	0.419(6)	1/4	0.425(7)	0.075*	674
	$P_6(1.82)$	0.38(5)	0.418(5)	1/4	0.424(7)	0.075*	675
	$P_7(2.14)$	0.32(5)	0.419(7)	1/4	0.426(8)	0.075*	676
	$P_8(2.57)$	0.45(6)	0.417(6)	1/4	0.417(6)	0.075*	677
	$P_9(3.13)$	0.25(5)	0.41(1)	1/4	0.41(1)	0.075*	678
	$P_{21}(0.50)$	0.57(4)	0.423(3)	1/4	0.431(4)	0.075*	679
W5	$P_1(0.20)$	0.55(3)	0.526(3)	0.987(3)	0.545(3)	0.079(4)**	680
	$P_2(0.60)$	0.61(3)	0.534(2)	0.973(3)	0.545(3)	0.075*	681
	$P_3(0.94)$	0.60(3)	0.533(2)	0.975(3)	0.547(3)	0.075*	682
	$P_4(1.22)$	0.60(3)	0.536(2)	0.975(3)	0.547(3)	0.075*	683
	$P_5(1.60)$	0.60(3)	0.538(2)	0.976(3)	0.551(3)	0.075*	684
	$P_6(1.82)$	0.59(3)	0.536(2)	0.974(3)	0.547(3)	0.075*	685
	$P_7(2.14)$	0.62(3)	0.539(2)	0.977(3)	0.554(3)	0.075*	686
	$P_8(2.57)$	0.58(3)	0.538(3)	0.974(4)	0.552(4)	0.075*	687
	$P_9(3.13)$	0.51(3)	0.534(4)	0.977(4)	0.544(4)	0.075*	688
	$P_{10}(3.92)$	0.67(3)	0.533(3)	0.982(5)	0.536(4)	0.075*	689
	$P_{11}(4.85)$	0.68(4)	0.534(3)	1.021(5)	0.543(4)	0.075*	690
	$P_{21}(0.50)$	0.62(2)	0.531(2)	0.973(3)	0.542(3)	0.075*	691

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Site	P (GPa)	$s.o.f.$	x	y	z	$U_{iso}(\text{\AA}^2)$	
							701
W6	$P_1(0.20)$	0.29(2)	0.590(5)	0.870(6)	0.552(5)	0.079(4)**	702
	$P_2(0.60)$	0.41(3)	0.590(3)	0.856(4)	0.549(4)	0.075*	703
	$P_3(0.94)$	0.50(3)	0.589(3)	0.857(4)	0.544(3)	0.075*	704
	$P_4(1.22)$	0.56(3)	0.587(3)	0.856(4)	0.545(3)	0.075*	705
	$P_5(1.60)$	0.56(3)	0.590(3)	0.855(3)	0.546(3)	0.075*	706
	$P_6(1.82)$	0.59(3)	0.590(2)	0.856(3)	0.547(3)	0.075*	707
	$P_7(2.14)$	0.57(3)	0.591(3)	0.852(4)	0.547(3)	0.075*	708
	$P_8(2.57)$	0.56(3)	0.591(3)	0.857(4)	0.555(4)	0.075*	709
	$P_9(3.13)$	0.51**	0.593(4)	0.851(5)	0.545(4)	0.075*	710
	$P_{10}(3.92)$	0.52**	0.595(4)	0.844(4)	0.554(5)	0.075*	711
	$P_{11}(4.85)$	0.47**	0.609(5)	0.848(5)	0.566(6)	0.075*	712
	$P_{12}(0.50)$	0.46**	0.591(3)	0.863(4)	0.547(4)	0.075*	713
							714
W2'	$P_2(0.60)$	0.29(3)	0.668(7)	3/4	0.369(8)	0.075*	715
	$P_3(0.94)$	0.34(7)	0.676(6)	3/4	0.376(7)	0.075*	716
	$P_4(1.22)$	0.36(4)	0.673(6)	3/4	0.374(8)	0.075*	717
	$P_5(1.60)$	0.33(4)	0.673(7)	3/4	0.376(8)	0.075*	718
	$P_6(1.82)$	0.34(4)	0.665(6)	3/4	0.370(8)	0.075*	719
	$P_7(2.14)$	0.37(4)	0.671(7)	3/4	0.368(8)	0.075*	720
	$P_8(2.57)$	0.40(6)	0.624(9)	3/4	0.346(8)	0.075*	721
							722
W1'	$P_9(3.13)$	0.36(4)	0.005(7)	1/4	0.550(8)	0.075*	723
	$P_{10}(3.92)$	0.20(5)	0.02(1)	1/4	0.57(2)	0.075*	724
	$P_{11}(4.85)$	0.36(6)	0.051(9)	1/4	0.58(1)	0.075*	725
							726
W2''	$P_{10}(3.92)$	0.27(5)	0.46(1)	1/4	0.77(1)	0.075*	727
	$P_{11}(4.85)$	0.58(0)	0.446(8)	1/4	0.755(8)	0.075*	728

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741 **Table 4 (deposited).** Refined T-O distances (Å) at different pressures.

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P_n	$P(\text{GPa})$	T1-O5	T1-O7	T1-O2	T1-O3	T2-O8	T2-O2	T2-O6	T2-O3
P_1	0.20(5)	1.635(1)	1.652(1)	1.661(2)	1.685(1)	1.634(2)	1.638(1)	1.644(1)	1.645(2)
P_2	0.60(5)	1.645(1)	1.637(1)	1.675 (2)	1.688(1)	1.642(2)	1.628(1)	1.645(1)	1.640(2)
P_3	0.94(5)	1.646(1)	1.643(1)	1.657(2)	1.668(1)	1.636(2)	1.645(1)	1.641(1)	1.650(2)
P_4	1.22(5)	1.647(1)	1.636(1)	1.679(2)	1.669(1)	1.641(2)	1.633(1)	1.637(1)	1.646(2)
P_5	1.60(5)	1.645(1)	1.639(1)	1.674(2)	1.678(1)	1.640(2)	1.630(1)	1.643(1)	1.650(2)
P_6	1.82(5)	1.649(1)	1.633(1)	1.673(2)	1.676(1)	1.641(2)	1.625(1)	1.641(1)	1.647(2)
P_7	2.14(5)	1.636(1)	1.647(1)	1.666(2)	1.666(1)	1.637(2)	1.618(1)	1.642(1)	1.651(2)
P_8	2.57(5)	1.633(1)	1.652(1)	1.656(2)	1.676(1)	1.637(2)	1.632(1)	1.638(1)	1.630(2)
P_9	3.13(5)	1.626(1)	1.662(1)	1.655(2)	1.643(1)	1.632(2)	1.641(1)	1.629(1)	1.665(2)
P_{10}	3.92(5)	1.655(1)	1.635(1)	1.651(1)	1.619(1)	1.650(2)	1.647(1)	1.645(1)	1.664(2)
P_{11}	4.85(5)	1.632(1)	1.628(1)	1.605(1)	1.639(1)	1.681(2)	1.657(1)	1.643(1)	1.654(1)
P_{21}	0.50(5)	1.647(1)	1.652(1)	1.668(2)	1.652(1)	1.643(2)	1.643(1)	1.638(1)	1.660(2)

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P_n	$P(\text{GPa})$	T3-O1	T3-O7	T3-O5	T3-O4	T4-O9	T4-O4	T4-O1	T4-O6
P_1	0.20(5)	1.622(1)	1.641(2)	1.642(1)	1.669(2)	1.637(2)	1.638(1)	1.650(1)	1.651(1)
P_2	0.60(5)	1.637(1)	1.650(1)	1.635(1)	1.651(2)	1.636(2)	1.641(1)	1.644(1)	1.664(1)
P_3	0.94(5)	1.639(1)	1.642(2)	1.635(1)	1.635(2)	1.641(2)	1.650(1)	1.653(1)	1.657(1)
P_4	1.22(5)	1.638(1)	1.650(2)	1.633(1)	1.631(2)	1.638(2)	1.655(2)	1.654(1)	1.657(1)
P_5	1.60(5)	1.640(1)	1.644(2)	1.643(1)	1.632(2)	1.638(2)	1.656(1)	1.657(1)	1.650(1)
P_6	1.82(5)	1.634(1)	1.649(2)	1.640(1)	1.644(2)	1.636(2)	1.649(1)	1.657(1)	1.657(1)
P_7	2.14(5)	1.644(2)	1.628(2)	1.639(1)	1.630(2)	1.636(2)	1.657(1)	1.659(1)	1.638(1)
P_8	2.57(5)	1.637(1)	1.619(2)	1.637(1)	1.651(2)	1.640(2)	1.637(1)	1.648(1)	1.634(1)
P_9	3.13(5)	1.611(1)	1.612(2)	1.633(1)	1.682(2)	1.634(2)	1.620(1)	1.655(1)	1.642(2)
P_{10}	3.92(5)	1.656(1)	1.656(2)	1.625(1)	1.634(2)	1.657(2)	1.657(1)	1.632(1)	1.633(1)
P_{11}	4.85(5)	1.576(1)	1.687(2)	1.633(1)	1.718(2)	1.643(2)	1.652(1)	1.672(1)	1.654(1)
P_{21}	0.50(5)	1.618(1)	1.637(2)	1.651(1)	1.666(2)	1.645(2)	1.633(1)	1.654(1)	1.662(1)

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758 **Table 5 (deposited).** Refined distances (Å) at different pressures.

P_n	P (GPa)	K1-O1(x2)	K1-O8	K2-O1(x2)	K2-O8	Ca-O4	Ca-O7
P_1	0.20(5)	3.004(2)	3.391(3)	2.995(2)	3.181(2)	2.564(3)	2.642(2)
P_2	0.60(5)	2.995(2)	3.337(3)	2.981(2)	3.148(2)	2.541(3)	2.678(2)
P_3	0.94(5)	2.978(2)	3.300(3)	2.953(2)	3.148(2)	2.517(3)	2.707(3)
P_4	1.22(5)	2.976(2)	3.282(3)	2.948(2)	3.143(2)	2.493(3)	2.712(3)
P_5	1.60(5)	2.972(2)	3.283(3)	2.946(2)	3.153(2)	2.489(2)	2.747(3)
P_6	1.82(5)	2.981(2)	3.260(3)	2.941(2)	3.151(2)	2.474(2)	2.740(3)
P_7	2.14(5)	2.924(2)	3.226(2)	2.901(2)	3.118(2)	2.458(2)	2.771(3)
P_8	2.57(5)	2.927(2)	3.170(2)	2.894(2)	3.070(2)	2.440(2)	2.793(3)
P_9	3.13(5)	2.897(2)	3.109(2)	2.856(2)	3.027(2)	2.407(2)	2.867(3)
P_{10}	3.92(5)	2.908(2)	3.038(2)	2.827(2)	2.965(2)	2.419(2)	2.974(3)
P_{11}	4.85(5)	2.907(2)	3.025(2)	2.831(2)	2.952(1)	2.261(2)	3.048(3)
P_{21}	0.50(5)	3.008(2)	3.320(3)	3.016(2)	3.117(2)	2.591(3)	2.732(3)

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P_n	P (GPa)	W1-Ca	W1-W6	W2-W6	W2-O8	W1-O9	W1-O3(x2)
P_1	0.20(5)	2.202(2)	3.790(2)	3.123(2)	3.207(3)	2.940(3)	3.081(3)
P_2	0.60(5)	2.174(2)	3.700(2)	3.104(1)	3.205(3)	2.923(3)	3.081(3)
P_3	0.94(5)	2.039(2)	3.613(2)	3.120(1)	3.175(3)	2.821(3)	3.121(3)
P_4	1.22(5)	1.879(2)	3.435(2)	3.164(1)	3.174(4)	2.753(4)	3.167(3)
P_5	1.60(5)	1.658(2)	3.059(2)	3.104(1)	3.129(3)	2.896(3)	3.161(2)
P_6	1.82(5)	1.653(1)	3.088(3)	3.096(1)	3.104(3)	2.842(3)	3.187(2)
P_7	2.14(5)	1.612(2)	2.980(2)	3.068(1)	3.085(3)	2.944(4)	3.092(2)
P_8	2.57(5)	1.565(2)	2.939(2)	2.809(3)	2.880(2)	2.860(3)	3.137(2)
P_9	3.13(5)	1.496(2)	2.844(2)	2.544(1)	2.826(2)	2.919(4)	3.087(2)
P_{10}	3.92(5)	1.512(2)	2.827(2)	2.563(1)	2.878(2)	2.720(3)	3.197(3)
P_{11}	4.85(5)	1.562(2)	2.986(2)	2.641(1)	2.938(2)	2.690(3)	3.229(3)
P_{21}	0.50(5)	2.114(2)	3.698(2)	2.958(2)	3.129(3)	2.957(3)	3.053(3)

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774 **Table 6.** High-pressure evolution of the 8-mRs(001): relevant interatomic distances (Å), angles (°), and the
 775 ellipticity ratio $\varepsilon_{8\text{-mRs}(001)}$ (calculated as O5-O5/O9-O8, with O5-O5>O9-O8).
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P_n	$P(\text{GPa})$	O5-O5	O9-O8	O1-O1	O3-O3	O1-O3	$\varepsilon_{8\text{-mRs}(001)}$
P_1	0.20(5)	5.810(8)	6.121(2)	3.901(6)	4.299(6)	4.913(2)	0.948(2)
P_2	0.60(5)	5.828(8)	6.166(2)	3.794(5)	4.318(6)	4.929(2)	0.945(2)
P_3	0.94(5)	5.780(8)	6.180(2)	3.730(5)	4.314(6)	4.908(2)	0.935(2)
P_4	1.22(5)	5.756(8)	6.181(2)	3.693(5)	4.284(6)	4.907(2)	0.932(2)
P_5	1.60(5)	5.752(8)	6.203(2)	3.661(5)	4.252(6)	4.901(2)	0.927(2)
P_6	1.82(5)	5.731(8)	6.179(2)	3.661(5)	4.249(6)	4.899(2)	0.928(2)
P_7	2.14(5)	5.724(8)	6.161(2)	3.550(5)	4.233(6)	4.869(2)	0.929(2)
P_8	2.57(5)	5.706(8)	6.141(2)	3.532(5)	4.218(6)	4.869(2)	0.929(2)
P_9	3.13(5)	5.673(8)	6.194(2)	3.483(5)	4.316(6)	4.826(2)	0.915(2)
P_{10}	3.92(5)	5.555(8)	6.261(3)	3.465(5)	4.507(7)	4.849(2)	0.887(2)
P_{11}	4.85(5)	5.596(8)	6.431(3)	3.465(5)	4.678(7)	4.866(2)	0.870(2)
P_{21}	0.50(5)	5.747(8)	6.145(2)	3.836(5)	4.354(6)	4.924(2)	0.935(2)

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P_n	$P(\text{GPa})$	O1-O9-O1	O1-O5-O3	O5-O3-O8	O3-O8-O3
P_1	0.20(5)	92.90(5)	135.32(2)	116.62(3)	108.97(6)
P_2	0.60(5)	90.37(5)	134.76(2)	115.86(3)	108.84(7)
P_3	0.94(5)	88.20(5)	134.80(2)	115.62(3)	107.99(7)
P_4	1.22(5)	87.02(6)	134.71(2)	115.60(3)	106.92(7)
P_5	1.60(5)	85.93(5)	134.61(2)	115.84(2)	105.24(6)
P_6	1.82(5)	85.92(5)	134.89(2)	115.62(2)	105.40(7)
P_7	2.14(5)	83.56(5)	134.20(2)	115.17(2)	104.29(6)
P_8	2.57(5)	82.66(5)	133.92(2)	114.67(2)	105.55(6)
P_9	3.13(5)	81.13(5)	134.44(2)	113.40(3)	107.78(6)
P_{10}	3.92(5)	80.21(5)	136.65(3)	109.59(3)	114.45(7)
P_{11}	4.85(5)	79.23(4)	135.53(3)	109.20(3)	119.58(7)
P_{21}	0.50(5)	133.73(2)	137.03(3)	115.07(6)	109.09(6)

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791 **Table 7.** High-pressure evolution of the 8-mRs[010]: relevant interatomic distances (Å), angles (°), and the
 792 ellipticity ratio $\varepsilon_{8\text{-mRs}[010]}$ (calculated as O3-O3/O1-O1, with O1-O1 > O3-O3).

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P_n	$P(\text{GPa})$	$\varepsilon_{8\text{-mRs}[010]}$	O6-O6	O7-O7	O1-O1	O3-O3
P_1	0.20(5)	0.852(5)	6.874(6)	5.810(2)	7.807(7)	6.652(3)
P_2	0.60(5)	0.838(5)	6.834(6)	5.833(2)	7.868(7)	6.592(3)
P_3	0.94(5)	0.831(5)	6.842(6)	5.818(2)	7.888(7)	6.553(3)
P_4	1.22(5)	0.829(5)	6.837(6)	5.789(2)	7.870(8)	6.528(3)
P_5	1.60(5)	0.828(5)	6.869(6)	5.793(2)	7.888(7)	6.532(3)
P_6	1.82(5)	0.829(5)	6.838(6)	5.775(2)	7.865(7)	6.522(3)
P_7	2.14(5)	0.820(5)	6.850(6)	5.762(2)	7.890(7)	6.466(3)
P_8	2.57(5)	0.811(5)	6.846(6)	5.758(2)	7.905(7)	6.409(3)
P_9	3.13(5)	0.777(5)	6.743(6)	5.725(2)	8.014(7)	6.230(3)
P_{10}	3.92(5)	0.729(5)	6.606(6)	5.762(2)	8.216(7)	5.986(3)
P_{11}	4.85(5)	0.687(5)	6.452(6)	5.801(2)	8.356(7)	5.737(2)
P_{21}	0.50(5)	0.844(5)	6.866(6)	5.833(2)	7.805(7)	6.590(3)

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P_n	$P(\text{GPa})$	O3-O7-O1	O7-O1-O6	O1-O6-O3	O6-O3-O7
P_1	0.20(5)	159.93(2)	107.69(2)	142.31(2)	124.73(2)
P_2	0.60(5)	159.38(2)	106.53(2)	142.82(2)	125.41(2)
P_3	0.94(5)	159.78(2)	106.10(2)	142.02(2)	125.74(2)
P_4	1.22(5)	159.75(3)	106.04(2)	141.39(2)	125.61(2)
P_5	1.60(5)	159.49(2)	106.15(2)	140.69(2)	125.42(2)
P_6	1.82(5)	159.51(2)	106.02(2)	140.98(2)	125.18(2)
P_7	2.14(5)	159.71(2)	105.57(2)	139.96(2)	125.63(2)
P_8	2.57(5)	158.78(2)	105.26(2)	139.31(2)	125.87(2)
P_9	3.13(5)	158.15(3)	101.97(2)	140.30(2)	126.64(2)
P_{10}	3.92(5)	154.43(3)	97.617(2)	143.43(3)	128.75(3)
P_{11}	4.85(5)	150.49(3)	93.749(2)	145.67(3)	130.10(3)
P_{21}	0.50(5)	159.19(2)	107.91(2)	141.50(2)	125.72(2)

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808 **Table 8.** High-pressure evolution of the 8-mRs[100]-1: relevant interatomic distances (Å), angles (°), and the
 809 ellipticity ratio $\varepsilon_{8\text{-mRs}[100]-1}$ (calculated as O9-O8/O7-O7, with O7-O7 > O9-O8).

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P_n	$P(\text{GPa})$	O7-O7	O9-O8	O3-O3	O3-O4	O3-O8-O3	O4-O7-O3	$\varepsilon_{8\text{-mRs}[001]-1}$
P_1	0.20(5)	7.650(5)	6.669(7)	4.299(6)	4.288(5)	108.97(6)	38.50(2)	0.872(2)
P_2	0.60(5)	7.688(5)	6.657(7)	4.318(6)	4.306(5)	108.84(7)	38.27(2)	0.866(2)
P_3	0.94(5)	7.686(5)	6.635(7)	4.314(6)	4.274(5)	107.99(7)	37.98(2)	0.863(2)
P_4	1.22(5)	7.673(5)	6.638(8)	4.284(6)	4.262(5)	106.92(7)	37.93(2)	0.865(2)
P_5	1.60(5)	7.717(5)	6.650(7)	4.252(6)	4.261(5)	105.24(6)	37.76(2)	0.862(2)
P_6	1.82(5)	7.704(5)	6.637(7)	4.249(6)	4.258(5)	105.40(7)	37.82(2)	0.862(2)
P_7	2.14(5)	7.733(5)	6.621(7)	4.233(6)	4.219(5)	104.29(6)	37.39(2)	0.856(2)
P_8	2.57(5)	7.775(5)	6.515(7)	4.218(6)	4.192(5)	105.55(6)	37.16(2)	0.838(2)
P_9	3.13(5)	7.896(5)	6.385(7)	4.316(6)	4.089(4)	107.78(6)	35.97(2)	0.809(2)
P_{10}	3.92(5)	8.079(5)	6.133(7)	4.507(7)	3.999(4)	114.45(7)	34.35(2)	0.759(2)
P_{11}	4.85(5)	8.338(5)	6.007(7)	4.678(7)	3.817(4)	119.58(7)	32.38(2)	0.720(2)
P_{21}	0.50(5)	7.726(5)	6.640(7)	4.354(6)	4.285(5)	109.09(6)	38.03(2)	0.859(2)

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814 **Table 9.** High-pressure evolution of the 8-mRs[100]-1: relevant interatomic distances (Å), angles (°), and the
 815 ellipticity ratio $\varepsilon_{8\text{-mRs}[100]-1}$ (calculated as O7-O7/O9-O8, with O9-O8 > O7-O7).

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P_n	$P(\text{GPa})$	O7-O7	O9-O8	O1-O9-O1	O7-O1-O9	O1-O7-O2	O2-O8-O2	$\varepsilon_{8\text{-mRs}[001]-1}$
P_1	0.20(5)	6.503(5)	7.794(6)	92.90(5)	156.53(2)	130.09(2)	124.44(8)	0.834(2)
P_2	0.60(5)	6.495(5)	7.820(6)	90.37(5)	157.16(2)	130.20(2)	125.64(8)	0.831(2)
P_3	0.94(5)	6.414(5)	7.835(6)	88.20(5)	157.57(1)	130.76(2)	126.30(8)	0.819(2)
P_4	1.22(5)	6.395(5)	7.837(7)	87.02(6)	158.06(3)	130.59(2)	127.12(9)	0.816(2)
P_5	1.60(5)	6.351(5)	7.832(6)	85.93(5)	158.13(2)	131.21(2)	127.92(8)	0.811(2)
P_6	1.82(5)	6.347(5)	7.827(6)	85.92(5)	158.44(2)	131.19(2)	128.07(9)	0.811(2)
P_7	2.14(5)	6.262(5)	7.798(6)	83.56(5)	158.89(2)	131.72(2)	129.45(8)	0.803(2)
P_8	2.57(5)	6.177(5)	7.866(6)	82.66(5)	158.66(2)	133.25(2)	127.98(8)	0.785(2)
P_9	3.13(5)	5.974(5)	7.955(6)	81.14(5)	154.94(2)	136.44(2)	124.53(7)	0.751(2)
P_{10}	3.92(5)	5.703(4)	8.163(7)	80.21(5)	149.88(3)	141.67(2)	119.02(7)	0.699(2)
P_{11}	4.85(5)	5.386(4)	8.318(7)	79.23(4)	143.77(3)	148.71(2)	116.21(7)	0.648(2)
P_{21}	0.50(5)	6.427(5)	7.831(6)	90.46(5)	157.60(2)	131.44(2)	125.70(8)	0.821(2)

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824 **Table 10.** Refined elastic parameters of phillipsite for the first and the second compressional regime (see text
 825 for further details), based on II-BM equations of state fits. (*) fixed parameter; $K_0 = (1/\beta_{V,x})_{P_0,T_0} = -$
 826 $V(\partial P/\partial V)_{P_0,T_0}$; $K' = (\partial K/\partial P)_{T_0}$

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Elastic parameters of phillipsite in the first compressional regime (P1-P6)				
	V_0, l_0 ($\text{\AA}^3, \text{\AA}$)	K_0 (GPa)	K'	$\beta_{V,l}$ (GPa^{-1})
V	1005(1)	89(8)	4*	0.011(1)
a	9.914(7)	81(12)	4*	0.012(2)
b	14.201(9)	50(5)	4*	0.020(2)
c	8.707(2)	107(8)	4*	0.0093(7)
Elastic parameters of phillipsite in the second compressional regime (P9-P20)				
	V_0, x_0 ($\text{\AA}^3, \text{\AA}$)	K_0 (GPa)	K'	$\beta_{V,l}$ (GPa^{-1})
V	1098(2)	18.8(7)	4*	0.053(2)
a	10.07	30(2)	4*	0.033(2)
b	14.8(1)	11(1)	4*	0.091(8)
c	8.94(2)	21(1)	4*	0.048(2)

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848 **Table 11.** Evolution of some selected T-O-T angles (°) with P .

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P_n	P (GPa)	T4-O1-T3	T2-O8-T2	T1-O7-T3	T4-O6-T2
P_1	0.20(5)	144.74(4)	147.99(5)	144.38(3)	144.79(4)
P_2	0.60(5)	141.95(4)	148.39(5)	145.22(3)	143.87(4)
P_3	0.94(5)	139.95(4)	148.61(5)	144.95(3)	144.45(4)
P_4	1.22(5)	139.06(4)	148.76(9)	144.68(3)	144.53(4)
P_5	1.60(5)	138.28(4)	148.99(5)	144.39(3)	145.45(4)
P_6	1.82(5)	138.48(4)	148.79(9)	144.34(3)	144.59(4)
P_7	2.14(5)	135.34(4)	148.46(5)	144.18(3)	145.63(4)
P_8	2.57(5)	135.83(4)	148.46(5)	143.89(3)	146.20(4)
P_9	3.13(5)	135.58(4)	150.71(5)	140.88(3)	144.28(4)
P_{10}	3.92(5)	136.57(4)	150.65(5)	137.30(4)	141.34(4)
P_{11}	4.85(5)	137.37(4)	153.79(5)	132.80(4)	137.37(4)
P_{21}	0.50(5)	142.66(4)	148.03(5)	144.51(3)	145.10(4)

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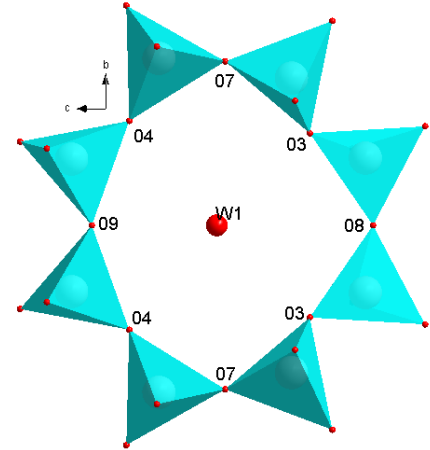
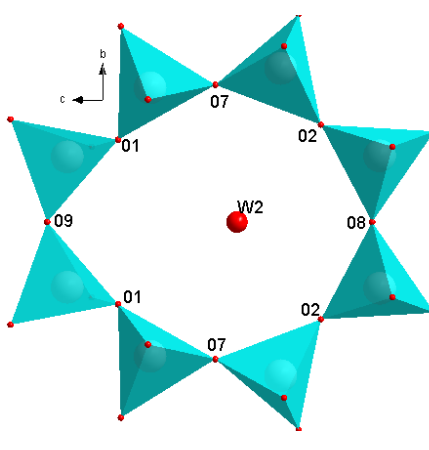
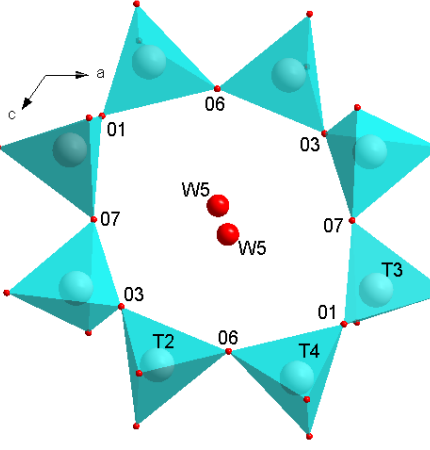
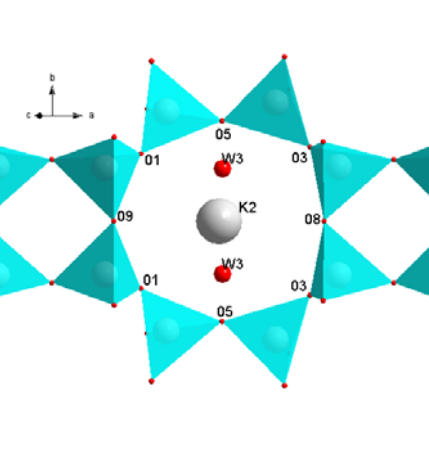
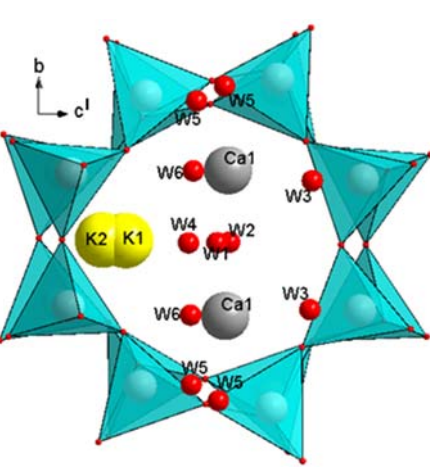
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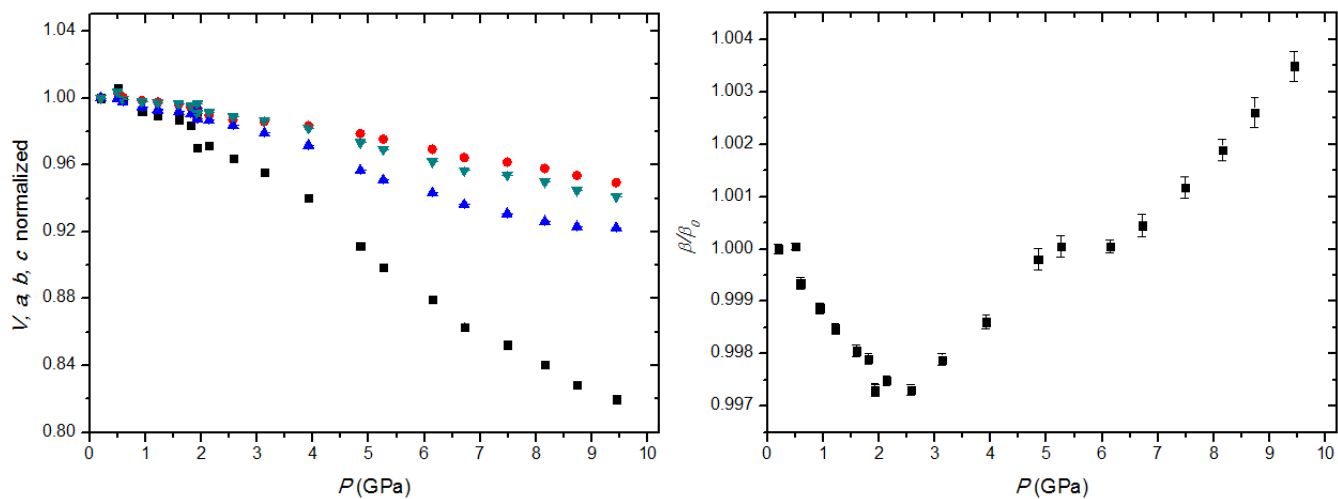
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869 **Figure 1.** Configuration of the 8-mR[100]-1, 8mR[100]-2, 8-mR[010] and 8-mR(001) and of the **extra-**
 870 **framework** population in phillipsite (as viewed down [100]), based on the structural refinements at 0.20 GPa
 871 (P1).

		872 73 74 75 76 77 78 879
8-mRs[100]-1	8-mRs[100]-2	880
		881 887
8-mRs[010]	8-mRs(001)	888
		889 890 891 892 893 894 895 896
Configuration of the extra-framework population.		897 898

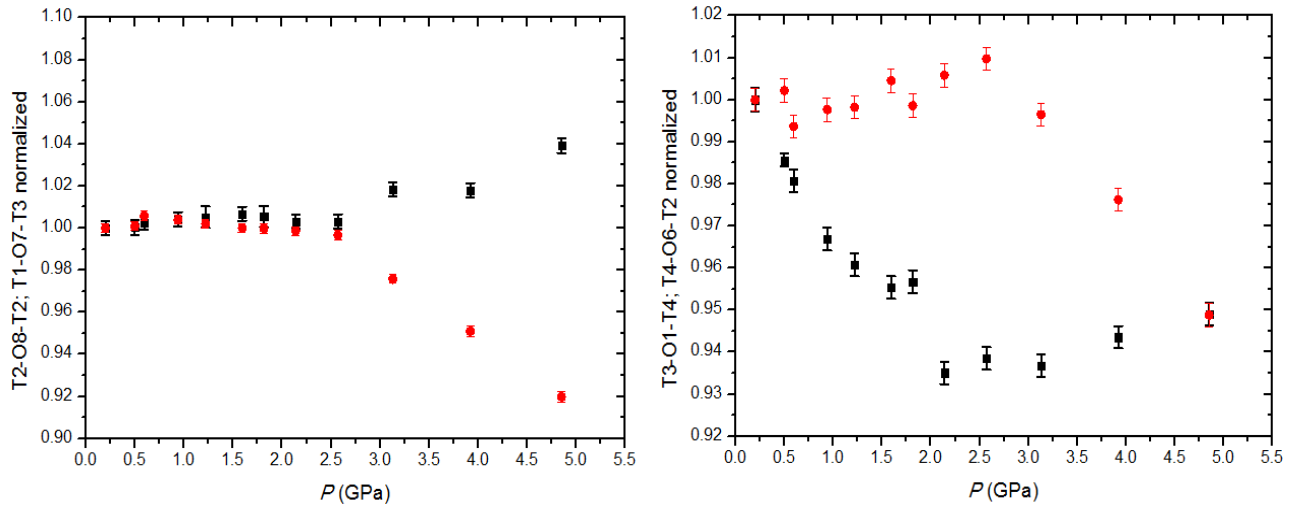
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Figure 2. High-pressure evolution of the normalized (to $P1$) unit-cell volume and axial parameters of phillipsite compressed in *m.e.w.* V/V_0 in black squares, a/a_0 red circles, b/b_0 blue triangles, c/c_0 cyan triangles.



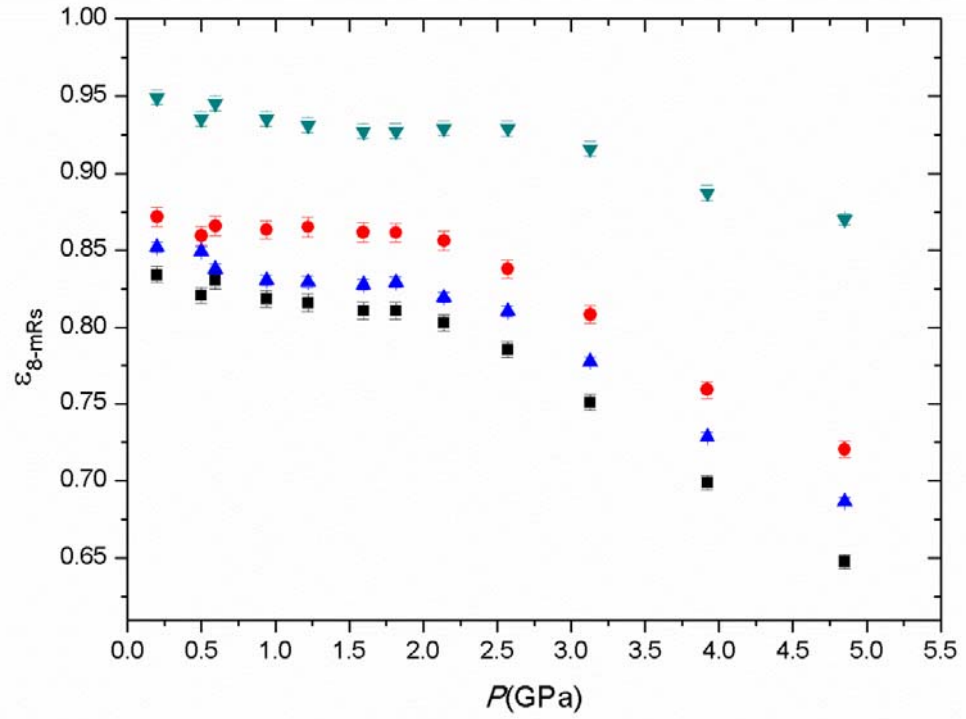
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Figure 3. High-pressure evolution of some selected T-O-T angles. T2-O8-T2 in black squares, T1-O7-T3 red circles; T4-O1-T3 in black squares, T4-O6-T2 red circles.

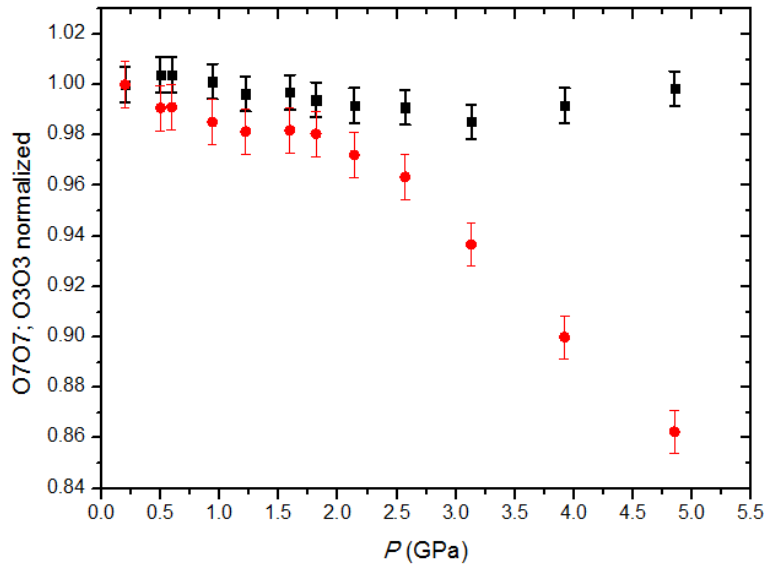


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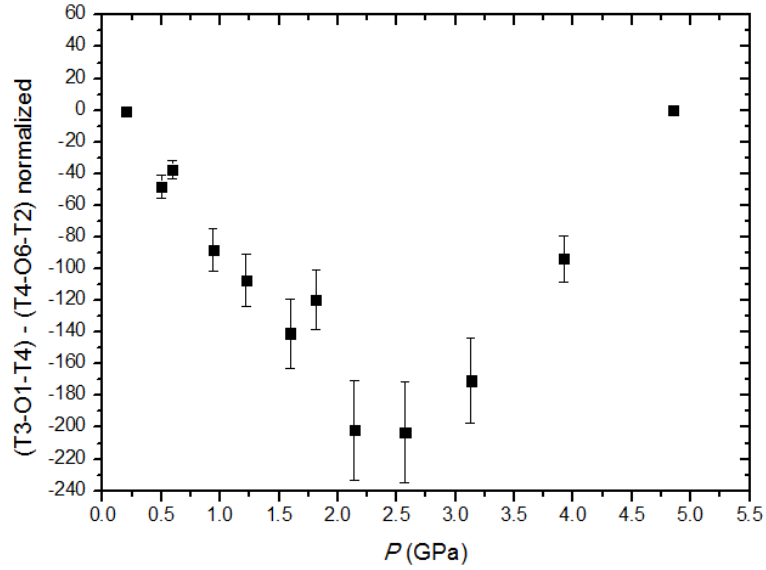
982 **Figure 4.** High-pressure evolution of the ϵ_{8-mRs} parameters; $\epsilon_{8-mRs}[100]-1$ in black squares, $\epsilon_{8-mRs}[100]-2$ red
 983 circles, $\epsilon_{8-mRs}[010]$ blue triangle, and $\epsilon_{8-mRs}(001)$ cyan triangles.



1028 **Figure 5.** Evolution of the 8-mRs[010] diameters vs. pressure. O7-O7 in black squares, O3-O3 in red circles.

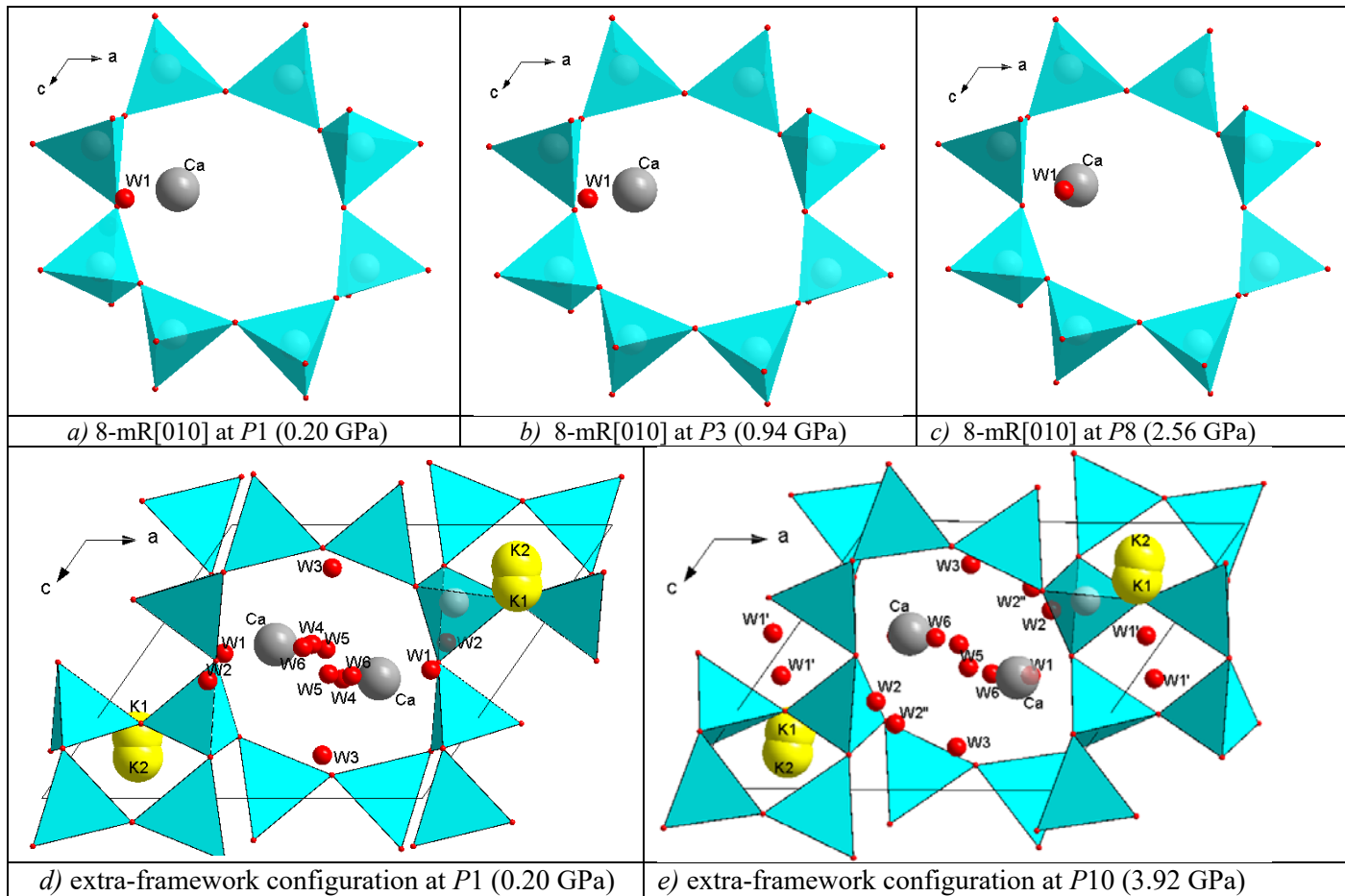


1075 **Figure 6.** High-pressure evolution of the (normalized) difference between the inter-tetrahedral angles T3-
1076 O1-T4 and T4-O6-T2.
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Figure 7. Migration of W1 with P viewed down $[010]$ (a,b,c) and general view of the P -induced changes into the structure (d,e). H_2O molecules in small red spheres, K cations in yellow and Ca in dark grey.



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1147 **Figure 8.** Clinographic view with the helicoidal configuration of the H₂O molecule-chain in the low (*left*)
1148 and high (*right*) compressional regime.
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