

Impact of thermal processing or solvent casting upon crystallization of PLA nanocellulose and/or nanoclay composites

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Impact of thermal processing or solvent casting upon crystallization of PLA nanocellulose and/or nanoclay composites

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Abstract:

- 14 Here we present how processing (solvent casting or isothermal crystallization) impacts crystallinity of
- poly(lactic acid) (PLA) and its nanocomposites (PLA/1wt% cellulose nanofibers (CNF), PLA/1wt% nanoclay
- 16 (C30B) or PLA/1wt% CNF/1wt% C30B. Polarized optical microscopy demonstrated a heterogeneneous
- 17 nucleation process during isothermal crystallization leading to smaller homogeneously distributed spherulites.
- With solvent casting, no effect on morphology was observed with respect to the nanoparticles, but an increased
- 19 spherulite size was observed at higher temperatures. This fact raises significant concerns regarding the
- suitability of solvent casting as a lab-scale procedure to investigate materials. Additionally, combining the
- 21 reinforcing agents, CNF and C30B, did not increase nucleation rate, in contrast with the general tendency,
- 22 where the incorporation of both particles led to improved properties (e.g., thermomechanical and barrier
- properties). However, a combination of C30B and CNF did lead to an overall increase in the rigid amorphous
- 24 fraction (RAF) and a reduced mobile amorphous fraction (MAF).

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1. INTRODUCTION

- 27 The extensive use of non-renewable resources is a well-known and serious global issue. Petroleum reserves are
- 28 continually being depleted and since most plastics made from these reserves are non-biodegradable, their
- disposal is a problem. In this context, substituting petroleum-based plastics with bio-based and biodegradable
- 30 alternatives is an attractive proposition for sustainable development. Nevertheless, bio-based polymers such as
- 31 poly (lactic acid) (PLA) still suffer from practical drawbacks such as brittleness, poor thermomechanical
- properties, and slow crystallization leading to longer processing times and modest gas barrier properties ^{1,2} when
- 33 compared to currently used petrochemical-derived plastics. Consequently, considerable efforts have been
- 34 focused towards improving the properties of bio-based polymers in general, and PLA in particular. These
- include the reinforcement of PLA with different types of nanoparticles such as nanocellulose ³, nanoclay ⁴, or a
- 36 combination of both ^{5,6}.

- 38 Briefly, PLA is a biodegradable, thermoplastic aliphatic polyester obtained from the ring-opening
- 39 polymerization of lactide ⁷, which is produced from the dehydration of lactic acid obtained from different

renewable resources. Nanoclays are composed of several layers of inorganic platelets stacked on top of each other, with platelet diameters in the range of 100 to 1000 nm and thickness <1 nm. In this study, commercially available, organically modified clay (Cloisite® 30B abbreviated to C30B) was used. In this clay the platelets are surface modified with hydrophobic bis (2-hydroxy-ethyl)-methyl tallow alkyl ammonium cations ⁸. Cellulose nanofibers (CNF) have lengths close to or in the microscale and diameters in the nanoscale. CNF typically exhibit hydroxyl (or carboxylate ⁹) groups on the nanofiber surfaces, but the CNF used in this work was partially acetylated during the CNF extraction procedure, presenting a small amount of acetyl groups on the surface (degree of substitution or DS ~ 10%) and slightly decreasing the hydrophilic character of the CNF ¹⁰.

In our previous studies², it was found that the incorporation of 1% CNF in solvent-cast PLA led to a reduction of 63% in Oxygen Transmission Rate (OTR), whereas with the equivalent composite containing 1% C30B only a 26% decrease was observed. Nanoclay has a higher surface-to-volume ratio than CNF, where a fully exfoliated platelet of dimensions 400 x 300 x 1 nm ¹¹ has an approximate surface to volume ratio of 2x10⁹ m⁻¹, while fibers of 25 nm diameter and 650 nm length exhibit only a surface to volume ratio of 1.6x10⁸ m⁻¹. Platelet-shaped morphologies therefore have 12.5 times higher surface-to-volume ratio, and would therefore be expected to improve the barrier properties more efficiently than the CNF. However, the CNF-based composites were showing better barrier properties than C30B. Considering this factor, it would be reasonable to suggest that part of the improvement in barrier properties for CNF composites, could be due to crystallinity effects originating from the fibers that is not happening on the C30B. Crystallinity is well known to have a positive impact on properties of materials such as gas barrier ^{12,13} or mechanical properties ^{14–18}. The crystallization properties of PLA 14,19,20 and PLA-based nanocomposites, such as PLA/CNF 18, PLA/C30B 13, and even PLA/based composites with banana fibers and clay 21 have been the subject of earlier studies. Differential scanning calorimetry (DSC) has revealed that both CNF- and C30B-containing PLA composites show a similar degree of crystallinity, while still exhibiting significantly different barrier properties. Therefore, this study was conducted to investigate the differences in crystallinity and morphology induced by the different types of reinforcing agents.

 Crystallinity is a broad topic that, especially in composite literature, has typically been described using only the degree of crystallinity, albeit other crystallinity-related parameters, such as polymorphism and the rigid amorphous fraction (RAF) could affect polymer properties. Crystalline PLA exhibits multiple polymorphic phases, namely α , β and γ , (and η stereocomplex 22) and it has been found that the prevailing α form exists as two different polymorphs (α = ordered and α' = disordered) which have different chain packing 23 . In addition, it has been widely accepted that the amorphous region of semi-crystalline polymers is itself composed of two fractions—the mobile amorphous fraction (MAF), which shows chain mobility, and the rigid amorphous fraction (RAF), an intermediate confined nanophase 24 . Classically, it has been considered that the RAF is present at the interface between the crystals and the surrounding amorphous phase; however, nanoparticles can also induce a confined nanophase wherein conformational rearrangements may occur, the so-called "cooperative rearrangement region" (CRR) 25 , for this reason some authors distinguish the RAF generated by crystallinity, understanding the critical parameters that affect materials properties can prove helpful towards achieving an

optimal material performance.

One of the major potential applications of bio-based polymers is in bio-based packaging materials. There are three critical parameters for such applications to be realized that can be affected by the crystallinity of the materials. The first parameter, mass transport/barrier properties, controls the quality of the contained food and the impact of crystalline morphology on water vapor transport is currently under investigation²⁶. The second parameter, transparency, is evaluated in the present work and is highly relevant in films for food packaging applications ²⁷ since customers may want to clearly see the food before purchasing. Generally, an increased crystallinity can improve certain properties, but it can also decrease optical transparency ² as a result of scattering of light due to the different densities between crystalline and amorphous domains. The third parameter, thermal transitions (i.e. $T_{\rm g}$ and $T_{\rm m}$), is also evaluated herein and can be influenced by crystallinity, which significantly affects material processing.

Here we investigate the differences in crystallinity induced by nanocellulose and nanoclay as well as the influence of combining both types of particles, while providing an insight into differences in crystallinity induced by solvent casting and isothermal crystallization. Solvent casting is widely used to investigate the impact of nanoparticles on polymer properties. However, traditionally, except for some recent techniques such as electrospinning ²⁸, or the use of 3D printed sacrificial molds ²⁹, industrially relevant techniques usually relies on higher processing temperatures. Depending on processing and crystallization behavior, different nanoparticles can have a different impact on crystallization, and solvent casting might therefore not accurately predict the performance of nanocomposites processed in more conventional processes at high temperature.

2. EXPERIMENTAL

2.1 Materials and methods

L-PLA (Ingeo 2003D) was supplied by Natureworks (Minnesota, USA). The clay used for this study was Cloisite[®] C30B and was supplied by Southern Clay Products (Texas, USA). C30B is a commercially available clay comprehensively described in the literature ^{30–32}. The extraction of nanocellulose CNF ¹⁰ and the preparation of nanocomposites have been described in more detail elsewhere ^{2,5} though a short summary is presented below.

2.2 Nanocomposite preparation

112 2.2.1 CNF extraction ¹⁰

The CNF extraction procedure as well as its characterization has been already pushlished ¹⁰. Briefly, 50 g of sisal fibers were cleaned overnight with 1.5 L of aqueous NaOH solution (2 wt%) at room temperature, and after filtration the fibers were alkali-treated three times with 1.5 L of aqueous NaOH solution (10 wt%) at boiling point over 1.5 h. The mercerized fibers were bleached with 1.25 mL of water at 70°C, 8 mL of acetic acid and 40 mL of NaClO₂ added every hour for 7 hours. Subsequently, the fibers were acetylated using 900 mL of a solution of HNO₃/acetic acid (1:6 v/v) at boiling point for 90 minutes. After that, the pulp was solvent exchanged in dimethylformamide (DMF). A 1 wt% solution of acetylated pulp in DMF was then dispersed for

72 hours with vigorous magnetic stirring followed by centrifugation at 2500 rpm for 10 mins to remove any remaining aggregates, the supernatant was used to prepare the nanocomposites.

2.2.2 Nanocomposite preparation via solvent casting

Briefly, PLA and nanoparticles were dissolved/dispersed separately in a solvent, and subsequently the solution of PLA and the suspension of nanoparticles were mixed and cast in a Teflon mold, and the solvent was removed by evaporation. Due to the different nature of the particles, an optimized protocol was used for each

128 combination.

2.2.2.1 PLA and PLA/C30B nanocomposites

Neat PLA and PLA/C30B (1wt% of clay) nanocomposites were prepared using dichloromethane (DCM) as a solvent. In total, 10 g of PLA was dissolved in 200 mL of DCM, and the mixture was kept under magnetic stirring in a sealed flask overnight. Separately, 3 g of C30B was mixed with 300 mL of DCM and kept under magnetic stirring for 24 hours. Subsequently, the clay suspension was ultrasonicated for 3 hours at 200W and then homogenized for 90 minutes with an Ultra-Turrax homogenizer (Jonke & Kunnel IKA Ultra-Turrax T25) at 20500 rpm. The PLA solution and nanoclay suspension were mixed to obtain the desired concentration of C30B in PLA and a final volume of 250 mL obtained by dilution with DCM. Thereafter the mixture was magnetically stirred, ultrasonicated for 90 minutes, homogenized for 30 minutes and finally degassed by ultrasonication for 5 minutes. Next, 80 mL of the suspension was poured slowly into a Teflon mold covered by a 5-13 µm filter paper into a Climacell climatic chamber, which was kept at 23°C for 16 h. Finally, the films were removed from the Teflon mold and further dried at 50°C under vacuum for at least 24 hours to remove the remaining traces of DCM.

2.2.2.2 PLA/CNF and PLA/CNF/C30B nanocomposites

The PLA/CNF and PLA/CNF/C30B nanocomposites (1wt% of each nanoparticle) were prepared using dimethylformamide (DMF) as a solvent. A total of 3.3 g of PLA was dissolved in 66 mL of DMF, whilst kept for 2 h at 70°C under vigorous magnetic stirring. Separately, 2 g of C30B was mixed with 200 mL of DMF and the mixture was kept under strong magnetic stirring for 24 h at room temperature. Next, the nanoclay suspension was ultrasonicated for 3 hours at 200W and thereafter homogenized for 90 min at 20500 rpm using an Ultra-Turrax homogenizer. Finally, the required amounts of the PLA, CNF, and C30B solutions or suspensions were mixed by magnetic stirring and poured slowly into a Teflon mold, where they were dried for 15 h at 80°C and subsequently for 24 h at 50°C under vacuum.

2.2.2.3 Thermal treatments

Solvent-cast materials were treated to obtain amorphous and isothermally crystallized products. In order to obtain fully amorphous specimens for UV-Vis spectroscopy and room temperature X-ray diffraction (XRD) measurements, solvent-cast products were placed between two aluminum foils and then subsequently hot pressed for 5 mins at 170°C, followed by fast cooling with water (at 10°C) (quenching). Thereafter, the fully

amorphous materials were isothermally crystallized for two hours at the corresponding crystallization temperature in an oven to achieve crystallized materials.

For other measurements including dynamic differential scanning calorimetry (DSC), temperature-modulated differential scanning calorimetry (MDSC), polarized optical microscopy (POM) and X-ray diffraction (XRD), the formation of fully amorphous materials and their isothermal crystallization at specified temperatures was performed in the instruments themselves as described in the corresponding sections.

2.3 Characterization

2.3.1 Polarized Optical Microscopy

Isothermal crystallization of the PLA and its nanocomposites was evaluated by polarized optical microscopy (POM) using a Nikon Eclipse E100 microscope with a Mettler Toledo FP82HT hot-stage at 140°C, 120°C, and 100°C. Fully amorphous samples were obtained from solvent-cast materials by inserting them between two microscope slides and placing them on the microscope hot stage, which was preheated to 200°C. After 2 minutes the samples were removed and cooled as quickly as possible with a tissue impregnated with ethanol. The sample was replaced on the hot stage after it reached the desired isothermal crystallization temperature and photographs were taken at regular intervals.

2.3.2 DSC

Isothermal crystallization kinetics were evaluated using a TA Instruments DSC Q1000 and the protocol illustrated in Figure 1. First, any crystallinity in the solvent cast materials dictated by the thermal history of the nanocomposites was erased by heating the samples at 10° C/min up to 200° C (1), maintaining the sample for two mins at 200° C (2), and then cooling at 20° C/min to 0° C (3). Thereafter, the samples were raised to the desired isothermal crystallization temperature (140° C, 120° C, 100° C or 80° C) at 10° C/min (4), and kept for 2 hours at that temperature (5). Finally, the samples were cooled to 0° C at 20° C/min (6) and then heated to 200° C at 10° C/min (7). The glass transition, $T_{\rm g}$, and melting temperature, $T_{\rm m}$ (from the maximum of the melting peak), were determined during this final heating run. No crystallization peaks were observed during any of the cooling cycles indicating that no significant crystallization occurred during this part of the treatment.

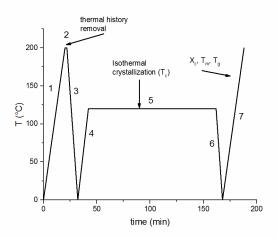


Figure 1 Schematic of the procedure used for the X_c (degree of crystallinity), T_m (melting temperature), T_g (glass transition) determination as well as for the evaluation of the crystallization kinetics.

The areas under the crystallization peaks obtained during the isothermal crystallization cycles (5) were integrated using TA Instruments Universal Analysis Software. The baseline was extrapolated from the heat flow signal after crystallization of the material was complete. The resulting area was integrated and the half crystallization time was considered as the time when 50% of maximum crystallinity was reached.

The heat capacity variation (Δ Cp) values of PLA and its nanocomposites when in a fully amorphous state at their corresponding $T_{\rm g}$ was determined in triplicate using a TA Instruments Discovery DSC. The samples were submitted to a thermal treatment similar to stages (1-4) described in Figure 1, but cycle 4 heating was done until 200°C. This was made to erase all of the thermal story of the samples and therefore measure the heat capacity variation (Δ Cp) when fully amorphous.

2.3.3 MDSC

The advantage of utilizing MDSC over DSC is that heat flow due to crystallization (termed reversible enthalpy) can be separated from that due to melting (termed non-reversible enthalpy), enabling a more accurate determination of the degree of crystallinity. MDSC was performed using a TA Instruments DSC Q1000 and a cycle similar to the protocol described in Figure 1, albeit with a modulation cycle (Amplitude = ± 0.50 °C, period = 30 s) during the final heating stage (stage 7).

To determine the degree of crystallinity (X_c), Eq 1 was used:

$$Xc = \frac{\Delta H_{\text{nonrev}} - \Delta H_{\text{rev}}}{\Delta H_0} \text{ (Eq 1)}$$

where X_c is the degree of crystallinity of the composite, ΔH_{nonrev} is the non-reversible enthalpy, and ΔH_{rev} is the reversible enthalpy. A melting enthalpy, ΔH_0 , of 106 J g⁻¹ for 100% crystalline α –poly (L-lactide) was used as reported ³³, while an enthalpy 25 J g⁻¹ lower (81 J g⁻¹) was considered for the α -phase, as suggested in the literature ³⁴. Again, no crystallization peaks were observed during the cooling cycles.

The mobile amorphous fraction (MAF) and rigid amorphous fraction (RAF) in the nanocomposites were determined by adapting an existing protocol for PLA ³⁵. Instead of only comparing the heat capacity of a specimen to the heat capacity of neat amorphous PLA (therefore different specimens), accuracy was improved by using the fully amorphous specimen (PLA or its nanocomposites) as reference to evaluate the relative impact of each crystalline morphology in the same treated material. Thereafter, these values were normalized using the heat capacity of PLA and nanocomposites. The reason for this was that PLA and its nanocomposites when in their fully amorphous phase showed different heat capacities due to the presence of nanoparticles affecting the amount of RAF.

The MAF was therefore determined by means of Eq 2.

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% MAF=
$$\frac{\Delta Cp\Delta Cp_{MAT}}{\Delta Cp'\Delta Cp_{PLA}} * 100(Eq 2)$$

where ΔCp_{PLA} is the heat capacity variation of fully amorphous PLA, while ΔCp_{MAT} is the heat capacity variation of the fully amorphous tested material (which could be PLA or any of its nanocomposites). These values were obtained as described above in Section 2.3.2 by DSC. $\Delta Cp'$ is the specific heat change of the specimen (PLA or any of its composites) in a completely amorphous state at its particular T_g , while ΔCp is the specific heat change of the same specimen under test conditions (solvent-cast or isothermal crystallization) at its corresponding T_g . In order to acquire an accurate value for Cp, a representative point and a representative slope were considered before and after the T_g . From these values two equations were obtained, one that extrapolates the value of Cp before the glass transition and the other, which extrapolates the value after the glass transition. The ΔCp was calculated as the difference between both values (using the corresponding T_g for each crystalline morphology).

The RAF was calculated by means of Eq 3:

$$\% RAF = 100 - \% MAF - \%X_c - X_{nano}$$
 (Eq 3)

- 238 where RAF is the rigid amorphous fraction, MAF the mobile amorphous fraction, X_c the degree of crystallinity,
- and X_{nano} , nanoparticle content (wt%).
- Finally, the RAF was separated between the RAF_{NANO} (induced by nanoparticles) and RAF_{CRYST} (induced by
- crystallinity, as has also been done for PLA/nanoclay nanocomposites³⁶. First, the RAF_{NANO} was calculated by
- means of Eq 4 (the heat capacity variation among fully amorphous PLA and fully amorphous composites is due
- 243 to RAF and nanoparticles) and afterwards the value of RAF_{CRYST} was calculated by means of Eq 5.

%
$$RAF_{NANO} = \left(1 - \frac{\Delta Cp_{MAT}}{\Delta Cp_{PLA}} - X_{nano}\right) * 100 \text{ (Eq 4)}$$

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$$\% RAF = \% RAF_{NANO} + \% RAF_{CRYST}$$
 (Eq 5)

- In Eq 5, ΔCp_{PLA} is the heat capacity variation of fully amorphous PLA, while ΔCp_{MAT} is the heat capacity variation of the fully amorphous tested material.
- Data from isothermal crystallization experiments within the range 10-70% relative crystallinity were fitted to the
- 249 Avrami kinetic model ³⁷ (Eq 6):

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$$\ln(-\ln(1-X_c)) = \ln k + n \times \ln t \text{ (Eq 6)}$$

In Eq 6, X_c is the relative degree of crystallinity, k is the overall kinetic constant, n is the Avrami index, and t is crystallization time. The start time (t_0) was considered the time at which crystallization was noticeable (therefore right after t_{delay}). The Avrami indeces are based on two factors (Eq 7), namely the growth directions of the spherulites (n_D), which is a value ranging from 1-3 that is dependent on the growth directions of the spherulites, and the time-dependent crystallization (n_N), which has a value between 0 for instantaneous nucleation and 1 for sporadic nucleation 37 .

sporadic nucleation ³⁷.

$$n = n_D + n_N (Eq 7)$$

2.3.4 XRD

Isothermal crystallization was also measured by XRD using a Philips X'Pert Pro diffraction system fitted with an Anton Paar HTK 1200N oven chamber and utilizing a Cu-tube (λ = 1.542 Å) operating at 40 kV and 40 mA. A heating/cooling profile similar to that described in Figure 1 for DSC was used; however, due to cooling restrictions, the samples were only cooled to 50°C instead of 0°C. During the isothermal crystallization stage, diffraction patterns were acquired with a scan range of 10-30 °20, step size of 0.067° and acquisition time of 1 min. After completion of the isothermal crystallization procedure the samples were cooled to 50°C, at which point an XRD pattern was acquired over the same scan range, but with a smaller step size of 0.017 and longer acquisition time of 10 min to enhance the signal/noise ratio.

The solvent-cast materials, the amorphous materials (after hot pressing/quenching) and isothermally crystallized materials (hot pressed and crystallized in an oven) were analyzed by the same XRD instrument at room temperature, but without the oven chamber and using scan range of 10-30 °20, step size 0.04° and 4 s/step.

2.3.5 Optical properties by UV-Vis spectroscopy

Optical properties were measured from at least three different points within the same sample under investigation using a UV-Vis spectrometer (Polar Star Omega) in the range of 200-1000 nm. An average of the measurements is presented.

3. RESULTS AND DISCUSSION

3.1 **Discussion on material preparation**

One of the key parameters for the successful improvement of properties in nanocomposites is to achieve good nanoparticle dispersion. In the present work, PLA was reinforced with two different nanoparticles of different nature (one hydrophilic, CNF, and one hydrophobic, C30B) and thus each behaves differently in the same solvent. It was not possible to find a common solvent/procedure, which led to both particles being well-dispersed and possessing suitable film properties. Therefore, to ensure a good dispersion of nanoparticles in the composites and thus allow a fair comparison, the best solvent and processing procedure (the ones that they were leasing to better nanoparticle dispersion) for each nanoparticle was used in each case. For C30B it was found that use of DCM as solvent followed by drying at room temperature led to well-dispersed composites with good film quality, whereas the same procedure applied to CNF led to poorly dispersed composites. After evaluation of different solvents, it was found that DMF was the most suitable solvent for this particular CNF, and that 80°C

was the best drying temperature. As summarized in Table 1, all composites were prepared with 1 wt% of nanoparticles, in order to strike a balance between a good dispersion and a significant increase in material performance, while minimizing the chance of clay platelet/nanofiber aggregates being present.

Table 1 Composition of the samples; PLA and nanocomposites in wt%.

	PLA	CNF	C30B
PLA	100%	-	-
PLA/C30B	99%	-	1%
PLA/CNF	99%	1%	-
PLA/CNF/C30B	98%	1%	1%

The CNF shows a diameter of 27 +/-13 nm and a length of 658 +/- 290 nm and is well dispersed in the nanocomposites as reported elsewhere. 10,2 The montmorionite-based C30B in the PLA/C30B and hybrid composites is also well dispersed, near to full-exfoliation⁵ and is therefore approximated to have individual layers of 400 x 300 x 1 nm¹¹.

3.2 Spherulite morphology and distribution by POM

The spherulite morphology and distribution in PLA and PLA nanocomposites prepared by solvent casting, followed by complete isothermal crystallization at 100°C, 120°C and 140°C, were evaluated by POM (see **Error! Reference source not found.**). First, the differences between solvent casting and isothermal crystallization were investigated. Solvent-cast samples (Figure 2, first row) of PLA/CNF and PLA/CNF/C30B show micron-sized (around 40 µm) spherulites, while any spherulites present in PLA and PLA/C30B are too small to be observed by POM, though DSC shows a crystallinity of 7 and 32% respectively in these samples. Furthermore, the presence of C30B does not influence the spherulite nature when combined with CNF. Though crystallization has occurred in the CNF-containing samples (34 and 35%, respectively, according to DSC) the spherulites do not cover the whole area.

It is clear that spherulite size is not only a result of the type of reinforcing agent, but is also highly dependent on the processing conditions, illustrating that processing temperature is a key factor for spherulite size and distribution.

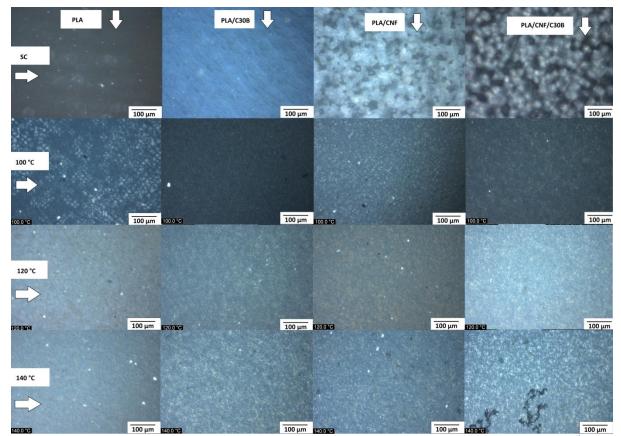
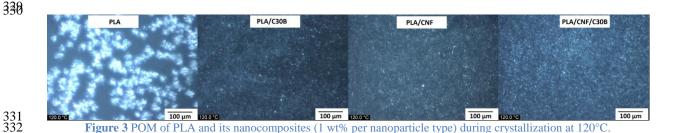


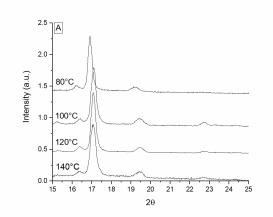
Figure 2 POM of PLA and nanocomposites (1wt% per nanoparticle type) with different crystalline morphologies. 1st row) Solvent cast, 2nd row) crystallized at 100°C, 3rd row) crystallized at 120°C) and 4th row) crystallized at 140°C.

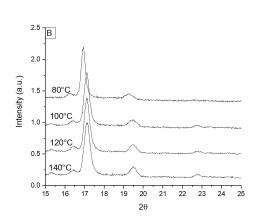
When comparing the fully crystallized morphologies between the isothermally crystallized nanocomposites at different crystallization temperatures (Figure 2, rows 2-4 and columns 3-4) no clear differences are observed, but there is a large difference when comparing these with the respective PLA samples (Figure 2, rows 2-4, column 1, inclusively). The nanocomposites, at all crystallization temperatures, show a greater amount of much smaller and more evenly distributed spherulites resulting from nucleation caused by the CNF and C30B that are homogeneously distributed, whereas the PLA contains larger spherulite sizes (up to ~65 µm) that are heterogeneously distributed. Evaluating the crystalline morphology of the fully crystallized samples is complicated due to the high amount and close packing of spherulites. But POM photographs of PLA and its nanocomposites taken at an earlier stage of the isothermal crystallization (approximately 20-30% of the total crystallization at 120°C, Figure 3) allows some differentiation. Here, it can again be seen that PLA contains much larger spherulites, whereas all of the nanocomposites contain substantially smaller homogeneously distributed spherulites because of the nucleating properties of the nanoparticles.



3.3 XRD studies

In order to elucidate which crystalline phase is generated by different crystallization procedures, and whether the nanoparticles could induce the formation of one phase over another, XRD patterns were collected. There are two thermally induced phases, α (ordered) and α' (disordered) and it has already been reported that lower processing temperatures tend to favor the creation of the disordered phase 23 . To aid investigation and for comparison, XRD patterns were also collected at 80°C, since this was likely to be a relevant temperature to observe the formation of the α' phase. The α and α' phases can be distinguished, since the latter does not exhibit any characteristic peaks, such as those corresponding to reflection plane 210, which is located at 20 ~ 22.5°, while the peaks that are present in both phases, such as 200/110 and 203/113, are shifted to lower 20 angles in the α' phase 23,34 .





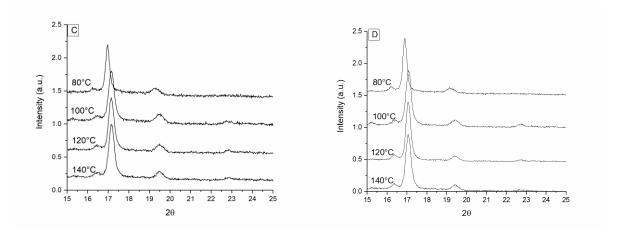
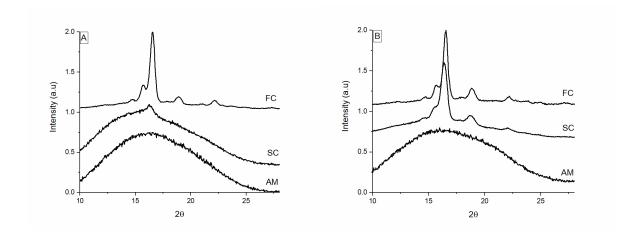
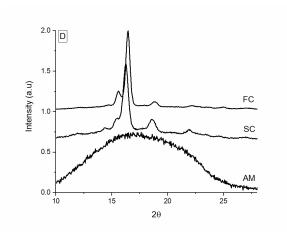


Figure 4 XRD patterns of PLA and nanocomposites crystallized at different temperatures. A) PLA, B) PLA/C30B, C) PLA/CNF, D) PLA/CNF/C30B. All of the composites have a 1wt% of each nanoparticle type.

Figure 4 presents the XRD patterns collected from isothermally crystallized PLA and its nanocomposites. In the left column are the two main crystallinity peaks of PLA at $2\theta \sim 17^\circ$, which corresponds to the reflection planes 200/110, and $2\theta \sim 19.5^\circ$, which corresponds to plane 203/113. While no significant variations in the relative positions of these peaks were observed in the solvent-cast nanocomposites due to the addition of different nanoparticles (Figure 4B-C), it was found that the crystallization temperature was clearly affecting peak position. There is a shift to lower 2θ (~0.2°) when comparing samples crystallized at >100°C with samples crystallized at 80°C, this shift, as mentioned above, has been associated to α ′ phase. It can be also seen that the peak at $2\theta \sim 22.5^\circ$, corresponding to reflection plane 201, and which is associated with the α phase, is present in the PLA and nanocomposites crystallized at 140° C, 120° C, and 100° C, while it is completely absent in the PLA and nanocomposites crystallized at 80° C. This supports the conclusion that PLA and nanocomposites crystallized at 80° C contain predominantly the α ′ phase, while nanocomposites crystallized at higher temperatures predominantly contain the α phase.

In order to evaluate whether the solvent casting procedure also induces the α' phase, the XRD patterns (Figure 5) of the solvent-cast (SC) PLA and nanocomposites were compared with those of the respective fully amorphous (AM - obtained from hot pressing at 170°C followed by fast quenching) and fully crystallized (FC (120°C)) - fully amorphous composites that were thereafter crystallized for 120 mins at 120°C in an oven) samples. Note that the XRD patterns in Figures 4 and 5 are not directly comparable because the former were collected during a crystallization monitoring experiment at 50°C (due to cooling restrictions) while the patterns in Figure 5 were collected at room temperature. Although the intensities may differ, the peak positions remain comparable.





2θ

0.10 PLA/C30B
PLA/CNF

0.00
PLA/CNF/C30B

PLA/CNF/C30B

Figure 5 XRD patterns of solvent cast, amorphous and fully crystallized materials. From A) to D) same material under different crystalline morphologies; A) PLA, B) PLA/C30B, C) PLA/CNF, D) PLA/CNF/C30B. E) Zoom-in of all of the solvent cast materials in the range of $2\theta = 21-24$. All of the composites have a 1wt% of each nanoparticle type.

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It is noticed that there is also the same shift to lower 2θ for all of the two main crystallinity peaks for the solvent-cast samples when compared with those crystallized at 120° C which contained mainly the α phase; therefore, it can also be concluded that the solvent-cast samples contained mainly the α' phase. However, in Figure 5E it can be seen that all of the diffraction traces from the solvent-cast nanocomposite samples, especially the PLA/CNF and PLA/CNF/C30B, also showed a small peak at $2\theta \sim 22^{\circ}$, which is ascribed to the α

phase. In fact, other researchers 38 have discussed the formation of the α -phase in solvent-cast samples even at low temperature, due to an increase on chain mobility arising from the solvent. However, in the present work there is apparently a coexistence of both phases. The α -phase is attributed to the solvent casting itself, while the α '-phase is attributed to the drying of the materials after solvent casting, at temperatures below the α -phase formation temperature (< 80°C).

It is reassuring to note that no crystalline peaks were found for the fully amorphous (AM) quenched composites, but only a broad characteristic amorphous halo, thereby proving that the procedure used to prepare hot-pressed amorphous samples (hot pressing at 170°C for 5 minutes) followed by fast cooling was successful.

3.4 Evaluation of the impact of nanoparticles on isothermal crystallization kinetics

The isothermal crystallization kinetics of PLA and its nanocomposites were monitored at 140°C, 120°C, 100°C and 80°C, the results are presented in Table 1 except for PLA at 140°C, since crystallization was not complete, and for all of the samples at 80°C since the rate was too slow to determine.

Table 2 Half-crystallization and crystallization detection times of PLA and composites.

		PLA	P	PLA/C30B		
T (°C)	t_{delay}^{a}	t_{delay}^{a} $t_{1/2}(exp)^{b}$		$t_{1/2}(exp)^b$		
140			0.5	11.5		
120	2.4	26	0.4	2		
100	4.9	52.1	1.8	3.7		
	PI	LA/CNF	PLA/CNF 1%/C30B			
T (°C)	t_{delay}^{a}	$t_{1/2}(exp)^b$	t_{delay}^{a}	$t_{1/2}(exp)^b$		
140	2.7	30.8	2.2	25.2		
120	1.8	10.3	0.8	4.8		
100	2.9	24.5	3.4	15.2		

a) t_{delay} (delay from arrival to the crystallization temperature and the start of the peak in DSC,

The crystallization rate reach a maximum at 120° C for all samples, and it is evident that the nanocomposites crystallize faster than neat PLA at the investigated temperatures. Among the nanocomposites, PLA/C30B showed faster nucleation than PLA/CNF or PLA/CNF/C30B, which was even more pronounced at 140° C. The better performance of C30B as a nucleating agent compared with CNF could be explained by the fact that clay is more likely to have a higher specific surface area, resulting in an increasing number of nucleation sites. In general, it was also found that t_{delay} (the time between the material reaching the crystallization temperature and onset of the crystallization peak) was proportional to the half-crystallization time.

In order to retrieve more information regarding crystallization kinetics, data from isothermal crystallization experiments within the range of 10-70% relative crystallinity were fitted to the Avrami kinetic model as described in materials and methods, resulting in the Avrami indeces shown in Table 3.

b) $t_{1/2}$ half-crystallization time (since the sample reached crystallization temperature)

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T (°C)	PLA	PLA/C30B	PLA/CNF	PLA/CNF/C30B
140		1.52	1.94	2.12
120	1.97	1.73	1.91	2.43
100	2.27	2.36	1.99	2.49

PLA/C30B nanocomposite showed a strong tendency to decrease the Avrami indeces, in line with increased crystallization temperature reflecting decreased growing directions. A similar trend has also been reported by other authors for PLA³⁹, and PLA with 10% and 15% of C30B ⁴⁰ and PLA with other organically modified clays at 1% and 3% loading 41. There are also other reports claiming a more moderate trend 42, which might be attributed to differences in clay dispersion. Notwithstanding this point, the PLA/CNF nanocomposite had constant values regardless of crystallization temperature, which is in agreement with some reports in the literature for low bacterial cellulose content in PLA 43 and for non-modified nanocrystalline cellulose in PLA 44. Interestingly, it was found that the hybrid nanocomposite PLA/CNF 1%/C30B 1% showed moderate variation in Avrami indices in line with increasing temperature between that of CNF and C30B, thereby suggesting the simultaneous growth of both clay- and nanocellulose-nucleated spherulites. In any case, all of the composites showed no major dissimilarities in values of n suggesting that there is no strong effect from the nanoparticles on the spherulite growing direction. Avrami indeces for the neat PLA (n=1.97 for crystallization at 120°C and n=2.27 for crystallization at 100°C) were not considered because, as can be seen in Error! Reference source not found., after complete crystallization at 120°C, the PLA spherulites reached a diameter of approximately 65 μm, while PLA film showed a thickness of 75 μm. Consequently, a spherulite growing in PLA could be affected by the physical dimensions of the film.

3.5 Influence of crystallization temperature and nanoparticles on thermal transitions

The effect of the crystallization temperature and the presence of nanoparticles on $T_{\rm g}$ and $T_{\rm m}$ was studied by DSC, and the results are shown in Table 4. PLA is known to have a very low $T_{\rm g}$, which limits it performance in some areas such as packaging of microwave-heated food or hot tea-coffee cups among others. Additionally, a large variation on $T_{\rm m}$ will certainly affect the optimal PLA processing temperature in an extruder during thermoforming. This is relevant for PLA, but it is critical for PLA/CNF composites since cellulose and CNF suffer from degradation at high temperature. Therefore, an evaluation of the impact of the nanoparticles and nanoparticle- induced crystallization is fundamental to optimize the performance of the composites.

Table 4 Thermal properties ($T_{\rm g}$ and $T_{\rm m}$) (°C) of the PLA and nanocomposites after full crystallization at 140°C, 120°C, and 100°C, solvent-cast and in an amorphous state.

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	PI	LA	PLA/C	C30B	PLA/	CNF	PLA/CN	NF/C30B
Crystallization	$T_{ m g}$	$T_{ m m}$						
140°Ca	58.8	162.3	57.6	161.9	56.5	163.2	57.9	162.6
$120^{\circ}\mathrm{C^a}$	61.7	154.9	58.8	154.4	60.0	155.3	59.6	154.4
$100^{\circ}\text{C}^{\text{a}}$	60.5	149.4	61.9	149.3	61.2	150.6	62.0	150.3

Amorphous ^c	55.5	-	56.2	-	54.9	-	55.2	-
SC^b	60.4	155.0	59.8	154.5	61.7	151.1	61.4	153.7

a) Isothermal crystallization at the corresponding crystallization temperature.

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- b) Solvent-cast nanocomposites: PLA and PLA/C30B at 23°C; PLA/CNF and PLA/CNF/C30B at 80°C.
 - c) Amorphous nanocomposites obtained from a fast melt-quenching.

In general, the incorporation of CNF and/or C30B did not have a significant impact on the $T_{\rm g}$ or $T_{\rm m}$ of PLA within the respective isothermally crystallized samples; however, the $T_{\rm m}$ of all of the PLA and nanocomposite samples did increase in line with increased crystallization temperature. For example, when increasing the isothermal crystallization temperature of PLA from 100 to 140°C, the $T_{\rm m}$ increased from 149.4 to 162.3°C, whereas for PLA/CNF 1% it increased from 150.6 to 163.2°C. The reason of this increased melting temperature with increases crystallization temperature is that at high temperatures larger, more stable, lamellae are formed within the spherulites which melt at higher temperatures It can also be seen that all of the isothermally crystallized materials showed higher T_o values when compared with the respective amorphous materials, which is attributed to a constriction of the MAF occurring after the material is crystallized. However, this might not be a direct effect of the crystallinity, but is probably due to induced changes on the amorphous region by the growing spherulites. The MAF trapped between spherulites has also been shown to have different relaxation values when compared with the amorphous matrix ³⁶. In this context, the presence of nanoparticles, unlike crystallization, does not constrain the amorphous phase as much as the presence of spherulites otherwise a larger variation would be observed between the T_g values of neat PLA and PLA nanocomposites. Finally, it was found that the T_m values of the solvent-cast PLA/CNF (151.1°C) and PLA/CNF/C30B (153.7°C) were slightly below the values of solvent-cast PLA (155.0°C) and PLA/C30B (154.5°C), suggesting that the different crystalline morphology for these two groups of samples, as observed in **Error! Reference source not found.**, have a small impact on $T_{\rm m}$; however, variations among the materials are close to the accuracy of the DSC.

3.6 Crystallinity and mobile/rigid amorphous fraction

It is widely accepted that crystallinity plays a very important role in materials properties, which makes crystallinity analysis (usually by DSC) essential for evaluation of the properties of materials and composites. Recently, evaluation of the so-called Rigid Amorphous Fraction (RAF) and its impact on material properties has been receiving additional attention. Apart from reducing the Mobile Amorphous Fraction, (MAF), which are the only "mobile" domains, and therefore essential for the extensibility of the material, it has been speculated that the RAF could be linked to specific material properties. Among other factors, the RAF is suspected of having a larger free volume than the MAF, which would have a significant impact on the sorption properties of the material. Therefore, understanding how crystallization affects those properties could be key to understanding, foreseeing and optimizing material properties.

The melting enthalpy of 100% α -crystalline PLA was considered to be 106 J g⁻¹, while that of 100% α -crystalline PLA was considered to be 25 J g⁻¹ lower at 81 J g⁻¹ ³⁴, while for solvent-cast materials an intermediate value of 93 J g⁻¹ was used (average of the enthalpy of the α and α ' phases). The heat capacity change at the T_g of fully amorphous PLA was found in this study to be 0.55 J g⁻¹ K⁻¹, which is similar to what

has been found by others, between 0.48 and 0.628 J g⁻¹ K⁻¹ ^{34,35,45,46}. As expected, The heat capacity variation at

the glass transition temperature of the fully amorphous nanocomposites are slightly lower than the neat PLA and are shown in Error! Reference source not found.. Additionally, in the same Table, the values of RAF induced by nanoparticles (RAF $_{NANO}$) are presented as calculated by means of Eq 4. The values of the heat capacity of PLA and nanocomposites at the T_g can be found in the supplementary information (Table S1).

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Furthermore, the MAF and RAF values of the PLA and its nanocomposites alongside their degrees of crystallinity are summarized in Table 5. RAF values in Table 4 have been split according to RAF induced by the crystalline morphology (RAF_{CRYS}) and the total RAF (i.e. $RAF_{CRYS} + RAF_{NANO}$) by means of Eq 4. The completely amorphous PLA/C30B 1% sample has a RAF of 4%, which therefore defines the RAF_{NANO} as 4%, since there is no impact from crystallinity. The solvent-cast PLA/C30B 1% sample has a RAF (i.e. total CRYS + NANO) of 16%, while 4% of this is the RAF_{NANO} (same as the amorphous sample) and the remaining 12% is attributed to RAF_{CRYS}.

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 $\begin{tabular}{ll} \textbf{Table 5} Degree of crystallinity (X_c), mobile amorphous fraction (MAF), and rigid amorphous fraction (RAF) of PLA and nanocomposites under different crystalline morphologies. \\ \end{tabular}$

Isothermal	PLA			PLA/C30B			
Crystallization	X_{c}	MAF	RAF/RAF _{CRYS} /RAF _{NANO} d	$X_{\rm c}$ MAF		RAF/RAF _{CRYS} /RAF _{NANO} d	
140°C ^a				36%	43%	20%/16%/4%	
120°C	35%	42%	22%	39%	36%	24%/20%/4%	
100°C	33%	45%	23%	36%	36%	27%/23%/4%	
Amorphous ^c	0%	100%	0%	0%	95%	4%/0%/4%	
SC ^b	6%	90%	4%	29%	54%	16%/12%/4%	
Isothermal		Р	LA/CNF	NF		PLA/CNF/C30B	
Crystallization	X_c	MAF	RAF/RAF _{CRYS} /RAF _{NANO} d	X_c	MAF	RAF/RAF _{CRYS} /RAF _{NANO} d	
140°C	36%	43%	20%/16%/4%	37%	37%	24%/15%/9%	
120°C	37%	38%	24%/20%/4%	40%	32%	25%/16%/9%	
100°C	36%	37%	26%/22%/4%	37%	33%	28%/19%/9%	
Amorphous ^c	0%	95%	4%/0%/4%	0%	89%	9%/0%/9%	
SC ^b	34%	41%	29%/25%/4%	35%	35%	32%/23%/9%	

a) The data for PLA at 140°C are not presented, due to incomplete crystallization.

b) Solvent-cast nanocomposites: PLA and PLA/C30B at 23°C; PLA/CNF and PLA/CNF/C30B at 80°C.

c) The amorphous nanocomposites were obtained from a fast melt-quenching.

d) Rigid amorphous fraction: Overall RAF%/% /RAF $_{CRY}$ /RAF $_{NANO}$).

Regarding the presence of nanoparticles, seemingly both CNF and C30B showed a similar impact on the formation of RAF_{NANO} in amorphous samples (each at 4%), despite the fact that C30B is likely to show a higher specific area than CNF. This is attributed to the presence of the long chain hydrophobic modifier present on the C30B surfaces apparently minimizing the creation of RAF_{NANO} by enhancing compatibility between polymer matrix and nanoparticles. Hybrid CNF/C30B showed an RAF_{NANO} (9%) close to the combination of the RAF_{NANO} induced by the two types of particles individually. A corresponding decrease in MAF is observed when C30B or CNF is added and suggests the nanoparticles are well dispersed and do not interact with each other, since interaction among nanoparticles is likely to decrease the overall surface area of nanoparticles in the polymer matrix and lead to a decreased RAF.

The RAF of neat PLA isothermally crystallized at 100°C (23%) and 120°C (22%) is in the higher range of values presented in the literature (12%-22%) ^{35,36,47}. When evaluating the effect of isothermal crystallization temperature on the RAF values for all samples it can be noted that higher crystallization temperature leads to slightly reduced RAF, which is a trend reported in the literature ⁴⁸.

It is shown that all of the isothermally crystallized and solvent-cast nanocomposites exhibit increased crystallinity and a reduced MAF when compared with the respective neat isothermally crystallized PLA samples. This is considered a result of the smaller spherulite sizes induced in nanocomposites (Figure 2), allowing for a better packing of the different spherulites within the matrix, which subsequently allowed the formation of more crystalline domains, thus decreasing the MAF. The isothermally crystallized nanocomposites showed an increased RAF_{CRYS+NANO}, compared to neat PLA, which was due to the presence of nanoparticles. When comparing the values of RAF_{CRYS} it can be seen that the nanocomposites have lower values. Furthermore, it can be observed that solvent-cast PLA/C30B 1% shows a much lower amount of RAF (13%) than solvent-cast PLA/CNF 1% (25%) and solvent-cast PLA/CNF 1% (28%). This combined with the fact that the former has a much smaller spherulite size (as shown in Figure 2 - top row) and the extent of crystallinity for all three samples is approximately the same, suggests that spherulite size and RAF are closely related.

3.7 Evaluation of the influence of crystalline morphology and nanoparticles on optical transparency

The impact of nanoparticles and crystalline morphology on the transparency of films was investigated, and the results are summarized in Figure 6. Transparency is a key property in plastics for food packaging applications, and while nanoparticles are smaller than the wavelength of the visible light and therefore should not influence the transmission of visible light, their impact on crystallinity might affect transparency.

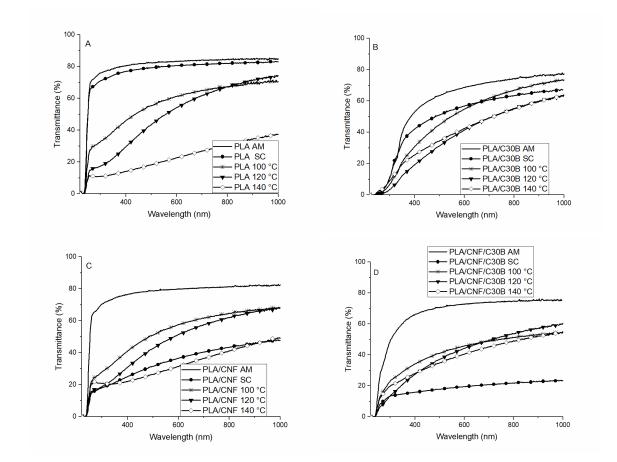


Figure 6 UV-VIS spectra of neat PLA and its nanocomposites with different crystalline morphologies after isothermal crystallization at different temperatures, and for amorphous- and solvent casting-induced crystallinity.

When evaluating the impact of crystallization temperature on the transparency of films, it is evident that crystallization at 100°C leads to more transparent materials, although the difference in materials crystallized at 120°C is generally small. Surprisingly, crystallization at 140°C dramatically affects the transparency of PLA and CNF-containing nanocomposites, whilst not having such a significant influence on nanocomposites with C30B. Assuming that there is no noticeable change in crystalline morphology among PLA/CNF, PLA/C30B and PLA/CNF/C30B crystallized at 140°C, and also that PLA shows incomplete crystallization at this temperature, this effect is mostly attributed to a temperature-induced internal deformation (i.e. bubbles or irregularities), which can cause light scattering.

This observation is interesting, assuming that the decrease in transparency is due to thermal deformation, it is anticipated that composites showing better thermomechanical properties would provide better transparency. Higher thermomechanical resistance leads to less deformed material. However it could be argued that there is an inconsistency with PLA/CNF crystallized at 140°C, material that in our previous work ² showed better thermomechanical properties than PLA/C30B but still showed reduced transparency without any clear difference in crystalline morphology. However, this can be explained based on the different reinforcing mechanisms of both nanoparticles. Previously we have observed better reinforcing performance of CNF, which was attributed to the establishment of a percolated network of the CNF, which can uphold any stress of the polymer chains. Meanwhile, the higher specific area and higher compatibility of C30B should lead to stronger interfacial bonding between the polymer matrix and the clay (including the aliphatic chains at its surface) and

thus allows a better stress transfer. This anchoring mechanism of the chains by the nanoclays, also reported elsewhere ³⁶, prevents any shape degradation during the higher temperature processing and reduces any thermal deformation as observed with CNF. In the case of CNF, care should therefore be taken during processing, since too high a processing temperature could lead to reduced performance. Presumably, in this scenario the reduced surface area of CNF and lower compatibility with the polymer matrix leads to deformations at higher processing temperatures due to a lack of anchorage between polymer chains and nanoparticles.

When comparing respective amorphous samples with nanocomposites isothermally crystallized at 120°C and 100°C, it is evident that, for all of the cases, increased crystallinity leads to reduced transparency in the visible region of the spectra (>400 nm). This can be explained by the fact that crystalline domains have higher density than amorphous domains, which leads to light scattering as the light passes between each of the domains. It is also noteworthy that the presence of nanoparticles does not significantly affect the transparency of films within the isothermally crystallized samples, which is presumably due to the dispersion of the nanoparticles on a nanometer scale. A similar observation can be seen for the respective amorphous nanocomposites, although in this case the PLA/C30B does show a slight decrease in transparency. When evaluating the transparency of solvent-cast films, it can be seen that solvent-cast PLA/C30B shows increased transparency when compared to the other nanocomposites, while PLA/CNF/C30B shows a significantly reduced transparency. This is attributed to smaller or larger spherulite sizes observed in the solvent-casted PLA/C30B or PLA/CNF/C30B nanocomposites as shown in Figure 2 (row 1). In addition to this, also the amount of RAF could affect the transparency of the samples. RAF has been reported to have a larger free volume than the MAF, which ultimately could cause light scattering and effectively the free volume regions of RAF could act as "bubbles" in a polymer matrix.

A UV-blocking effect (reduction of transmittance below 400nm) can be seen for PLA/C30B 1%, which is not observed for PLA/CNF 1% which shows behavior similar to PLA. Surprisingly, PLA/CNF 1%/C30B 1% shows less of a UV-blocking behavior when compared with PLA/C30B 1%, even though the same amount of C30B is present. A better dispersion of clay (i.e. exfoliation) will lead to increased nanoparticle surface area that can block UV light ⁵⁰ suggesting this effect may be attributed to small differences in clay dispersion between C30B-reinforced composites caused by the presence of CNF. It is remarkable that, after full crystallization, at any of the temperatures studied, the hybrid nanocomposites containing 1% CNF and 1% C30B shows good transparency, which is often a desirable feature for food packaging films.

4. CONCLUSIONS

In the present work, the influence of processing conditions on the crystallinity of solvent-cast and isothermally crystallized PLA, PLA/CNF 1%, PLA/C30B 1%, and PLA/CNF 1%/C30B 1% was evaluated by DSC, MDSC, POM, and XRD. It was found that solvent casting at room temperature induces a different crystallinity compared to isothermal crystallization and therefore leads to materials with different performance compared to high temperature processed materials. Similarly, composites prepared at high temperature, might not accurately be used to assess material properties, when the material ultimately is intended to be processed via solvent-based electrospinning at lower temperatures. However, different solvent casting methods were shown to induce

different crystallinity. The combination of both CNF and C30B did not show significant variations in spherulite size or distribution when compared with single nanoparticle-filled composites.

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The thermal transitions were not significantly influenced by the nanoparticles, but the increasing isothermal crystallization temperatures did result in decreasing glass transition temperature and increasing melting points when assessing nanoparticles either individually or in combination. The kinetic investigation of crystallization demonstrated that combining both types of nanoparticles did not lead to a sum of both crystallization rates but to an average. A similar effect was also observed with spherulite growth directions. PLA/C30B 1% showed a clear tendency towards decreased growing directions with increased crystallization temperature, whereas PLA/CNF 1% showed no significant variations and a combination with PLA/CNF 1%/C30B 1% showed only a moderate intermediate decrease in growing direction. The combination of both nanoparticles within the amorphous matrix effectively led to a doubling of the RAF_{NANO}, which was also due to the sum of each individual nanoparticle; however, no further variations in RAF_{NANO} due to the effect of each nanoparticle was apparent after full isothermal crystallization. Within the isothermally crystallized samples, the main difference in the hybrid composites was a reduced MAF, which was compensated by an increase in extent of crystallinity, probably due to better spherulite packaging.

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Transparency of the nanocomposites generally depended on the spherulite size, which was clearly seen for the solvent casted samples. For isothermally crystallized samples, a similar degree of crystallinity and spherulite size were determined, though higher crystallization temperatures resulted in lower transparency, which was attributed to defects in the materials rather than crystallization phenomena.

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 - 6. Data availability
- The raw and processed data required to reproduce these findings cannot be shared at this time due to technical or time limitations

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7. REFERENCES

- 625 1. Madhavan Nampoothiri, K.; Nair, N. R.; John, R. P. Bioresour. Technol. 2010, 101, 8493.
- Trifol, J.; Plackett, D.; Sillard, C.; Hassager, O.; Daugaard, A. E.; Bras, J.; Szabo, P. *J. Appl. Polym. Sci.* **2016**, *133*, 1.
- 628 3. Khalil, H. A.; Bhat, A. H.; Yusra, A. I. Carbohydr. Polym. 2012, 87, 963.
- 4. Krishnamachari, P.; Zhang, J.; Lou, J.; Yan, J.; Uitenham, L. *Int. J. Polym. Anal. Charact.* 2009, *14*,
 336.
- 631 5. Trifol, J.; Plackett, D.; Sillard, C.; Szabo, P.; Bras, J.; Daugaard, A. E. *Polym. Int.* **2016**, *65*, 988.
- 632 6. Wu, C. N.; Saito, T.; Yang, Q.; Fukuzumi, H.; Isogai, A. ACS Appl. Mater. Interfaces 2014, 6, 12707.
- 633 7. Jamshidian, M.; Tehrany, E. A.; Imran, M.; Jacquot, M.; Desobry, S. Compr. Rev. Food Sci. Food Saf.

- **2010**, *9*, 552.
- 8. Bitinis, N.; Verdejo, R.; Maya, E. M.; Espuche, E.; Cassagnau, P.; Lopez-Manchado, M. A. Compos.
- 636 Sci. Technol. **2012**, 72, 305.
- 637 9. Fukuzumi, H.; Saito, T.; Isogai, A. Carbohydr. Polym. **2013**, 93, 172.
- 638 10. Trifol, J.; Sillard, C.; Plackett, D.; Szabo, P.; Bras, J.; Daugaard, A. E. Cellulose 2016.
- 639 11. Ploehn, H. J.; Liu, C. Ind. Eng. Chem. Res. 2006, 45, 7025.
- 640 12. Gorrasi, G.; Anastasio, R.; Bassi, L.; Pantani, R. *Macromol. Res.* **2013**, *21*, 1110.
- 641 13. Picard, E.; Espuche, E.; Fulchiron, R. Appl. Clay Sci. 2011, 53, 58.
- 642 14. Sarasua, J. R.; Arraiza, A. L.; Balerdi, P.; Maiza, I. *Polym. Eng. Sci.* **2005**, *45*, 745.
- 643 15. Garlotta, D. J. Polym. Environ. 2001, 9, 63.
- 644 16. Guinault, A.; Sollogoub, C.; Domenek, S.; Grandmontagne, A.; Ducruet, V. Int. J. Mater. Form. 2010,
- 645 *3*, 603.
- 646 17. Perego, G.; Cella, G. D.; Bastioli, C. J. Appl. Polym. Sci. 1996, 59, 37.
- 647 18. Suryanegara, L.; Nakagaito, A. N.; Yano, H. Compos. Sci. Technol. 2009, 69, 1187.
- 648 19. Naga, N.; Yoshida, Y.; Noguchi, K.; Murase, S. Open J. Polym. Chem. 2013, 03, 29.
- 649 20. Miyata, T.; Masuko, T. Polymer. 1998, 39, 5515.
- 650 21. Jandas, P. J.; Mohanty, S.; Nayak, S. K. J. Therm. Anal. Calorim. 2013, 114, 1265.
- 651 22. Sarasua, J. R.; Rodriguez, N. L.; Arraiza, A. L.; Meaurio, E. Macromolecules 2005, 38, 8362.
- 652 23. Zhang, J.; Tashiro, K.; Tsuji, H.; Domb, A. J. Macromolecules 2008, 41, 1352.
- 653 24. Wunderlich, B. Prog. Polym. Sci. 2003, 28, 383.
- 654 25. Adam, G.; Gibbs, J. H. J. Chem. Phys. 1965, 43, 139.
- Trifol, J.; Mericer, C.; Plackett, D.; Sillard, C.; Minelli, M.; Hassager, O.; Daugaard, a E.; Bras, J.;
- 656 Giacinti, M.; Szabo, P. 20th Int. Conf. Compos. Mater. Copenhagen 2015, 19.
- 657 27. López-Rubio, A.; Lagarón, J. M.; Hernández-Muñoz, P.; Almenar, E.; Catalá, R.; Gavara, R.; Pascall,
- 658 M. A. Innov. Food Sci. Emerg. Technol. **2005**, 6, 51.
- 659 28. Martínez-Sanz, M.; Olsson, R. T.; Lopez-Rubio, A.; Lagaron, J. M. J. Appl. Polym. Sci. 2012, 124,
- 660 1398.
- 661 29. Mohanty, S.; Larsen, L. B.; Trifol, J.; Szabo, P.; Burri, H. V. R.; Canali, C.; Dufva, M.; Emnéus, J.;
- 662 Wolff, A. Mater. Sci. Eng. C 2015, 55, 569.
- 663 30. Mohapatra, A. K.; Mohanty, S.; Nayak, S. K. Polym. Compos. 2012, 33, 2095.
- 664 31. Katiyar, V.; Gerds, N.; Koch, C. B.; Risbo, J.; Hansen, H. C. B.; Plackett, D. J. Appl. Polym. Sci. 2011,
- 665 122, 112.
- 666 32. Rhim, J. W.; Hong, S. I.; Ha, C. S. LWT Food Sci. Technol. 2009, 42, 612.
- 667 33. López-Rodríguez, N.; Martínez De Arenaza, I.; Meaurio, E.; Sarasua, J. R. RSC Adv. 2015, 5, 34525.
- 668 34. Righetti, M. C.; Gazzano, M.; Di Lorenzo, M. L.; Androsch, R. Enthalpy of melting of α'- and α-crystals
- of poly(L-lactic acid). Eur. Polym. J. **2015**, 70, 215–220.
- 35. Zuza, E.; Ugartemendia, J. M.; Lopez, A.; Meaurio, E.; Lejardi, A.; Sarasua, J. R. Polymer. 2008, 49,
- 671 4427.
- 672 36. Saiter, A.; Delpouve, N.; Dargent, E.; Oberhauser, W.; Conzatti, L.; Cicogna, F.; Passaglia, E. Eur.
- 673 *Polym. J.* **2016**, 78, 274.

- 674 37. Lorenzo, A. T.; Arnal, M. L.; Albuerne, J.; Müller, A. J. Polym. Test. 2007, 26, 222.
- 675 38. Pan, P.; Han, L.; Shan, G.; Bao, Y. Macromolecules 2014, 47, 8126.
- 676 39. Lohmeijer, P. J. A.; Goossens, J. G. P.; Peters, G. W. M. J. Appl. Polym. Sci. 2017, 134, 2.
- 677 40. Krikorian, V.; Pochan, D. J. *Macromolecules* **2004**, *37*, 6480.
- 678 41. Li, X.; Yin, J.; Yu, Z.; Yan, S.; Lu, X.; Wang, Y.; Cao, B.; Chen, X. Polym. Compos. 2009, 30, 1338.
- 679 42. Lee, S.-H.; Wang, S.; Teramoto, Y. J. Appl. Polym. Sci. 2008, 108, 870.
- 680 43. Ambrosio-Martín, J.; Lopez-Rubio, A.; Fabra, M. J.; Gorrasi, G.; Pantani, R.; Lagaron, J. M. J. Appl.
- 681 *Polym. Sci.* **2015**, *132*, 1.
- 682 44. Pei, A.; Zhou, Q.; Berglund, L. A. Compos. Sci. Technol. 2010, 70, 815.
- 683 45. Arnoult, M.; Dargent, E.; Mano, J. F. *Polymer.* **2007**, *48*, 1012.
- 684 46. Henricks, J.; Boyum, M.; Zheng, W. J. Therm. Anal. Calorim. 2015, 120, 1765.
- 685 47. Magoń, A.; Pyda, M. Polymer. 2009, 50, 3967.
- 686 48. Righetti, M. C.; Tombari, E. *Thermochim. Acta* **2011**, *522*, 118.
- 687 49. Lin, J.; Shenogin, S.; Nazarenko, S. Polymer. 2002, 43, 4733.
- 688 50. Gao, F. Mater. Today 2004, 7, 50.