

# GH-3PAD – a new numerical solver for multiphase transport in porous media - new insights on gas hydrate and free gas co-existence

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H51L-1369



### Pre-processing

**Setting up depositional history of the basin**

- Time of the first deposition
- Fluctuating sedimentation rates
- Varying lithology (initial porosity and compaction length scale)
- Varying productivity (degradable organic matter input)
- Potential fluxes of fluids and/or gas phases

**Setting up modeling parameters**

- Water depth
- Salinity
- Initial temperature profile
- Initial pressure (incl. compressible fluids and gas phases)
- Initial concentration of chemical species (CH<sub>4</sub>, SO<sub>4</sub>, DIC, POC)

**Adjusting parameters**

- Initial box definition
- Time-step limited to the flux of fluid or gas phase (Courant number)
- Vertical resolution of the basin

Variables obtained:  
 $P_{ini}$ ,  $Temp_{ini}$ ,  $\rho_f$ ,  $\rho_g$ ,  $\rho_h$ ,  $\rho_s$ ,  $\mu_f$ ,  $\mu_g$ ,  $\lambda_f$ ,  $\lambda_g$ ,  $\lambda_h$ ,  $\lambda_s$ ,  $C_{pf}$ ,  $C_{pg}$ ,  $C_{ph}$ ,  $C_{ps}$

### Simulation

**Deposition of a new sedimentary layer**

**Compaction of the sediment package**

- Solid velocity calculation due to the mesh movement
- Intrinsic and relative permeability calculation for 3-phase system

Variables obtained:  
 new modeling box size, new  $\phi$ ,  $k$ ,  $k_f$ ,  $k_g$ ,  $V_s$

**Pressure update**

- 3-phase compressible solver
- Darcy' velocity update (2-phase)

**Temperature update**

- Bulk thermal conductivity
- Bulk heat capacity
- Temperature advection
- Temperature diffusion

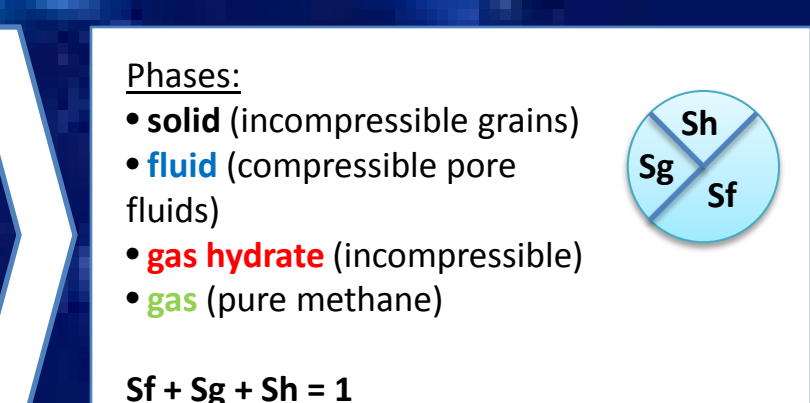
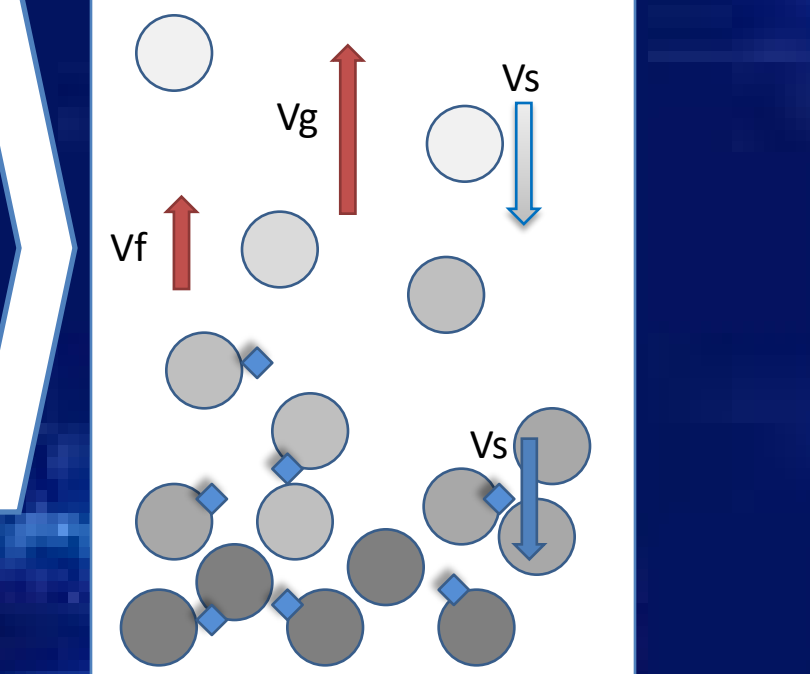
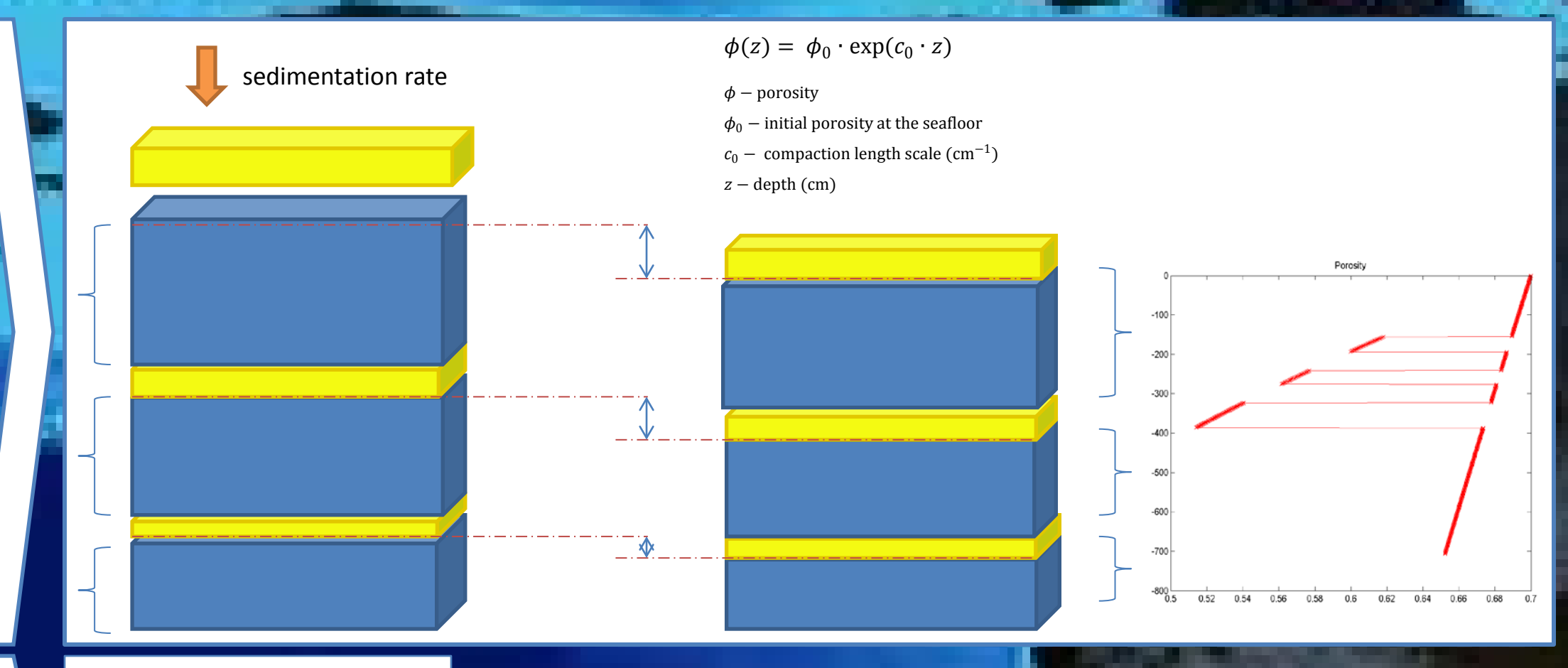
**Advection**

- Advection of chemical species in the pore fluids
- Advection of gas phase

**Diffusion**

- Diffusion of chemical species in the pore fluids
- Tortuosity calculation
- Diffusion coefficients of CH<sub>4</sub>, SO<sub>4</sub>, and DIC in marine sediments

Variables obtained:  
 $P$ ,  $Temp$ ,  $V_s$ ,  $U_f$ ,  $U_g$



$$(\rho C_p)_{bulk} \frac{\partial T}{\partial t} = -(\rho C_p)_{bulk} \vec{v}_i \cdot \nabla T - \rho_f C_{pf} \vec{v}_f \cdot \nabla T - \rho_g C_{pg} \vec{v}_g \cdot \nabla T + \nabla \cdot (\lambda_{bulk} \nabla T) + Q$$

Bulk heat capacity  
 $(\rho C_p)_{bulk} = (1-\phi)\rho_s C_{ps} + \phi S_f \rho_f C_{pf} + \phi S_g \rho_g C_{pg} + \phi S_h \rho_h C_{ph}$

Bulk thermal conductivity  
 $\lambda_{bulk} = \lambda_s^{(1-\phi)} \lambda_f^{S_f \phi} \lambda_g^{S_g \phi} \lambda_h^{S_h \phi}$

$$\frac{\partial((1-\phi)\rho_s)}{\partial t} = -\nabla \cdot ((1-\phi)\rho_s \vec{v}_s) \quad \text{Mass balance for solids}$$

$$\phi S_f (\vec{v}_f - \vec{v}_s) = -\frac{k k_f}{\mu_f} (\nabla P + \rho_f \vec{g}) \quad \text{Mass balance for solutes}$$

$$\phi S_g (\vec{v}_g - \vec{v}_s) = -\frac{k k_g}{\mu_g} (\nabla P + \rho_g \vec{g}) \quad \text{Mass balance for gas phase}$$

$$\frac{\partial((1-\phi)\rho_f)}{\partial t} = -\nabla \cdot ((1-\phi)\rho_f \vec{v}_f) \quad \text{Mass balance for hydrates}$$

$$\frac{\partial(\phi S_f C)}{\partial t} = \nabla \cdot (\phi S_f D \nabla C) - \nabla \cdot (\phi S_f C \vec{v}_f) + Q \quad \text{Mass balance for chemical species dissolved in fluids}$$

Rate	Kinetic rate law
Anaerobic Oxidation of Methane (mmol · yr <sup>-1</sup> )	$R_{AOM} = K_{AOM} \cdot C(SO_4) \cdot C(CH_4)$
Methanogenesis (mmol · yr <sup>-1</sup> )	$R_M = 0.5 \cdot \frac{K_{SO_4} \cdot C(SO_4) + K_{SO_4} \cdot R_{POC} \cdot \tau_c}{C(SO_4) + K_{SO_4} + R_{POC} \cdot \tau_c}$
Sulfate reduction (mmol · yr <sup>-1</sup> )	$R_{SR} = 0.5 \cdot \frac{C(SO_4)}{C(SO_4) + K_{SO_4}} \cdot R_{POC} \cdot \tau_c$
Constant	Value
$K_{AOM}$ (dm <sup>3</sup> · mmol <sup>-1</sup> · yr <sup>-1</sup> )	10 <sup>-10</sup>
$K_{SO_4}$ (mM)	1
Conversion factor	Formulation
$\tau_c$ from (wt.%) into (mM)	$\tau_c = \frac{\phi \cdot MW_C}{(1-\phi) \cdot d_s \cdot 10^3}$

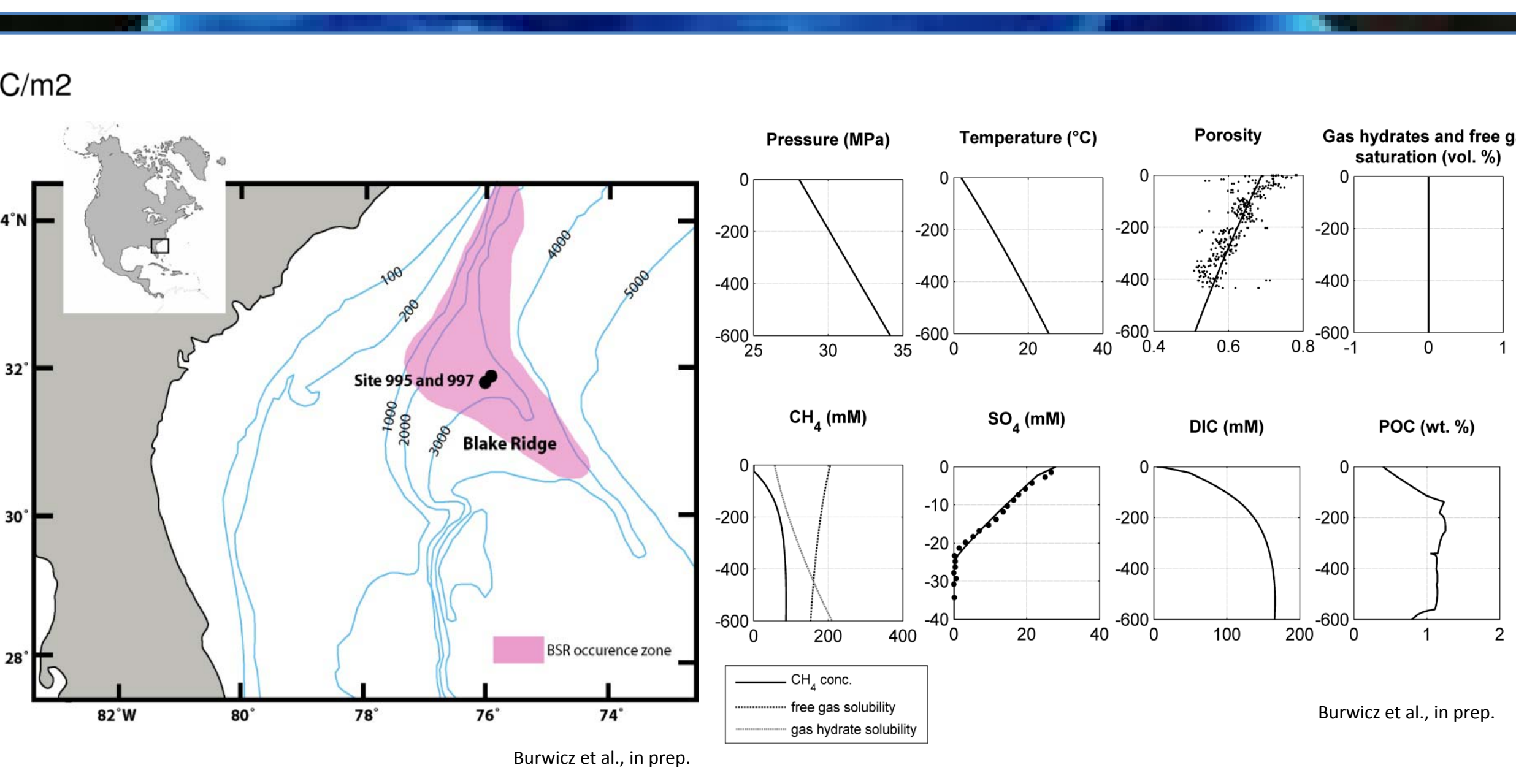
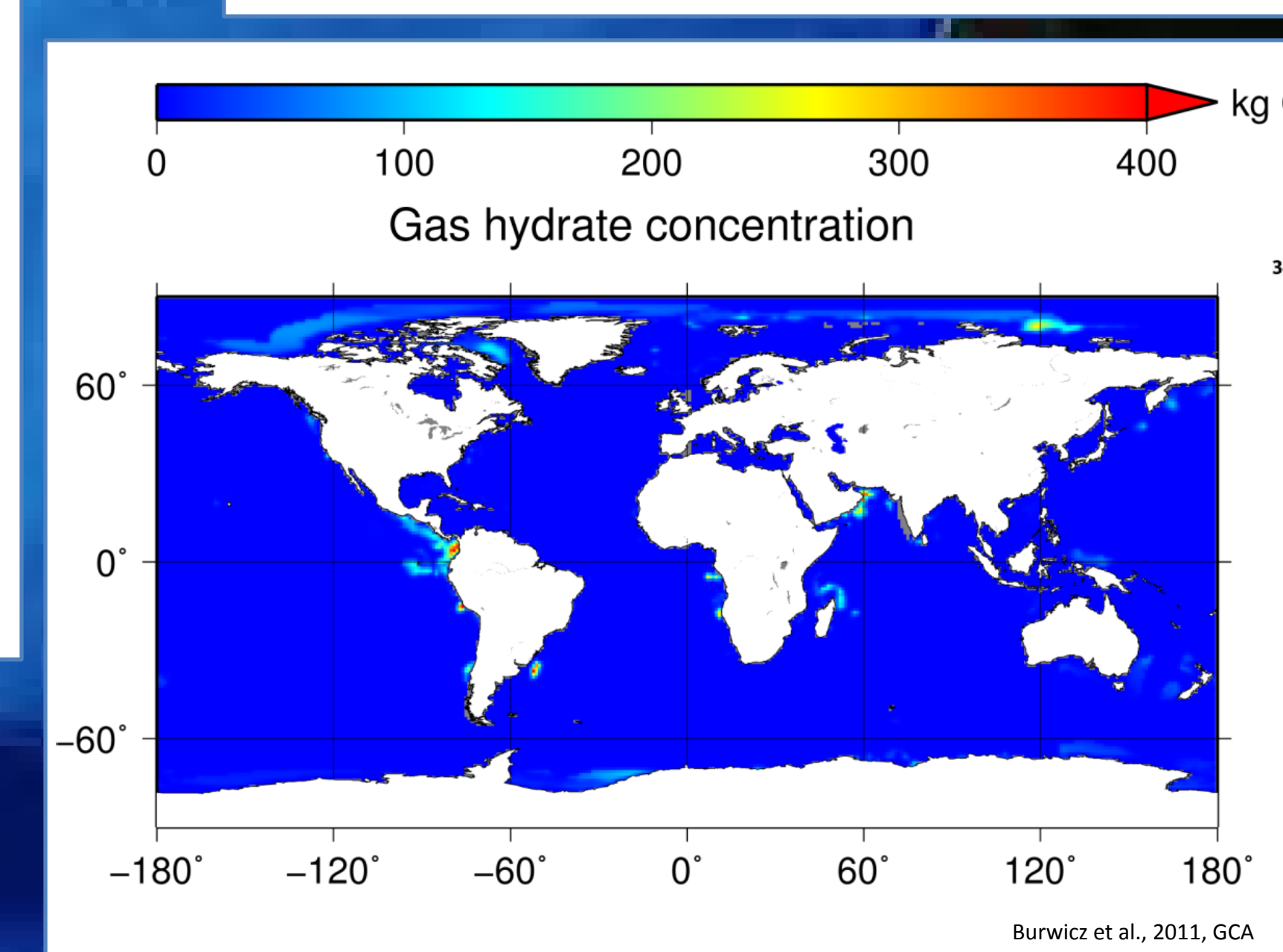
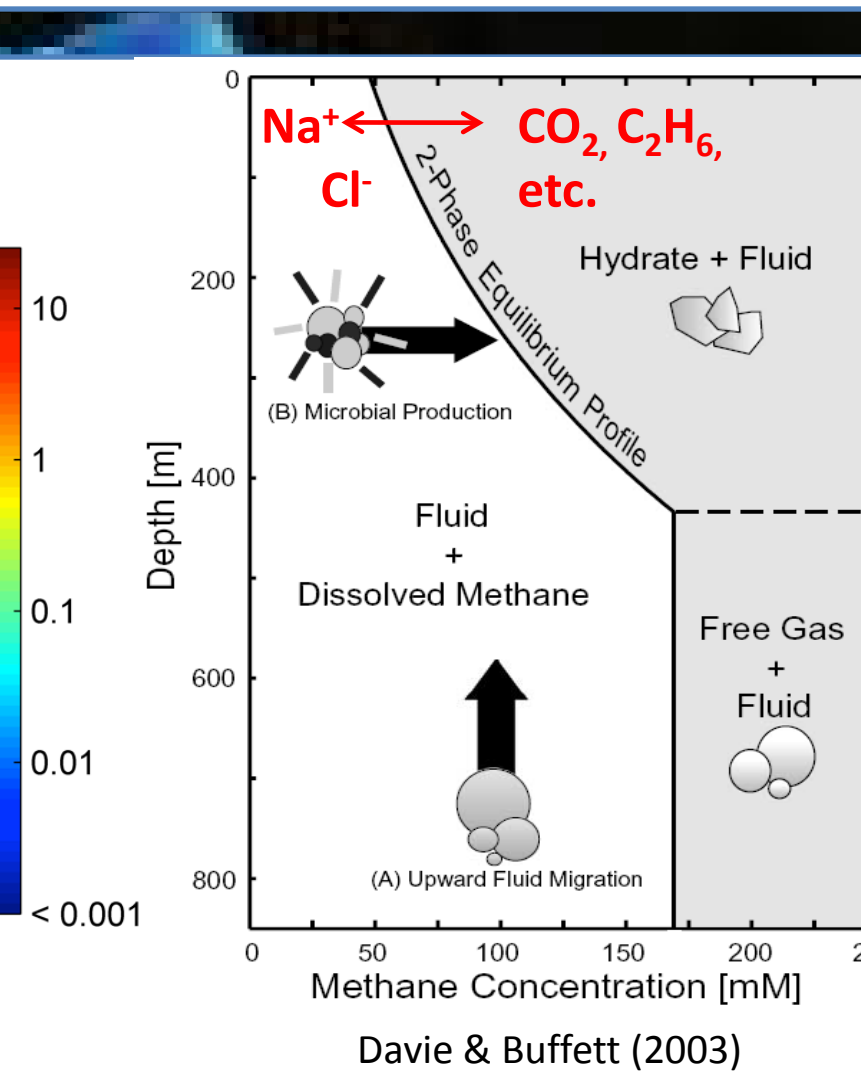
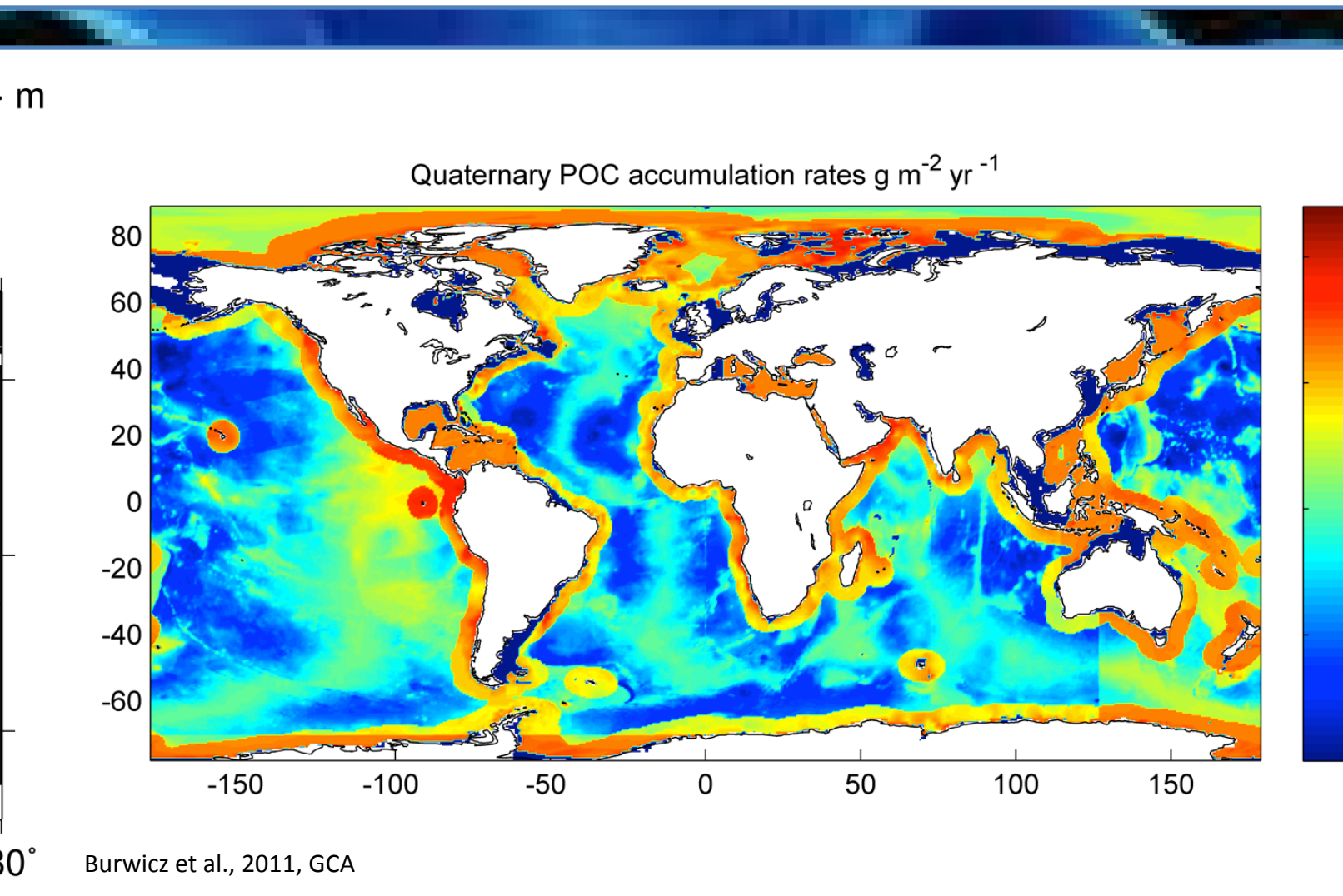
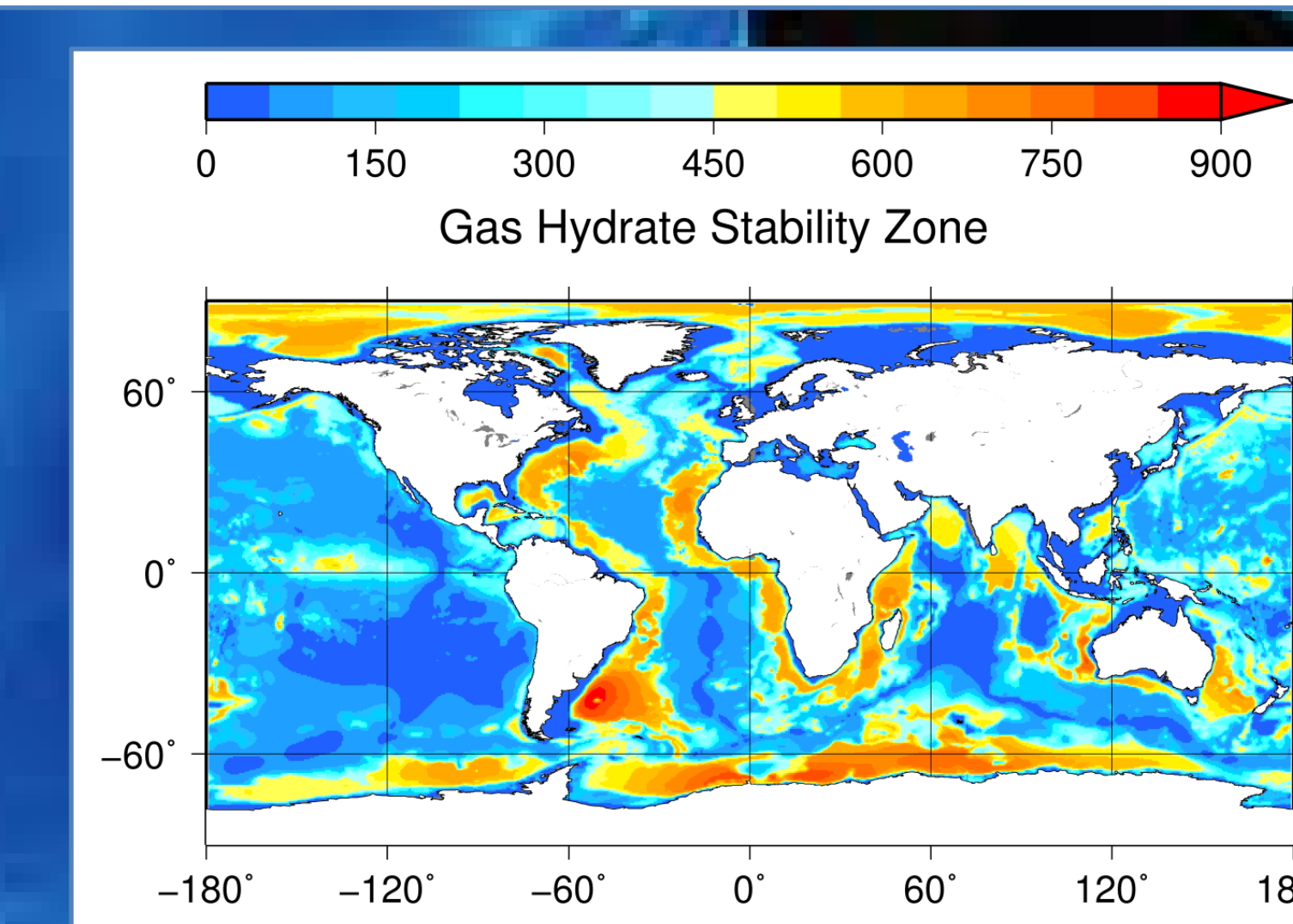
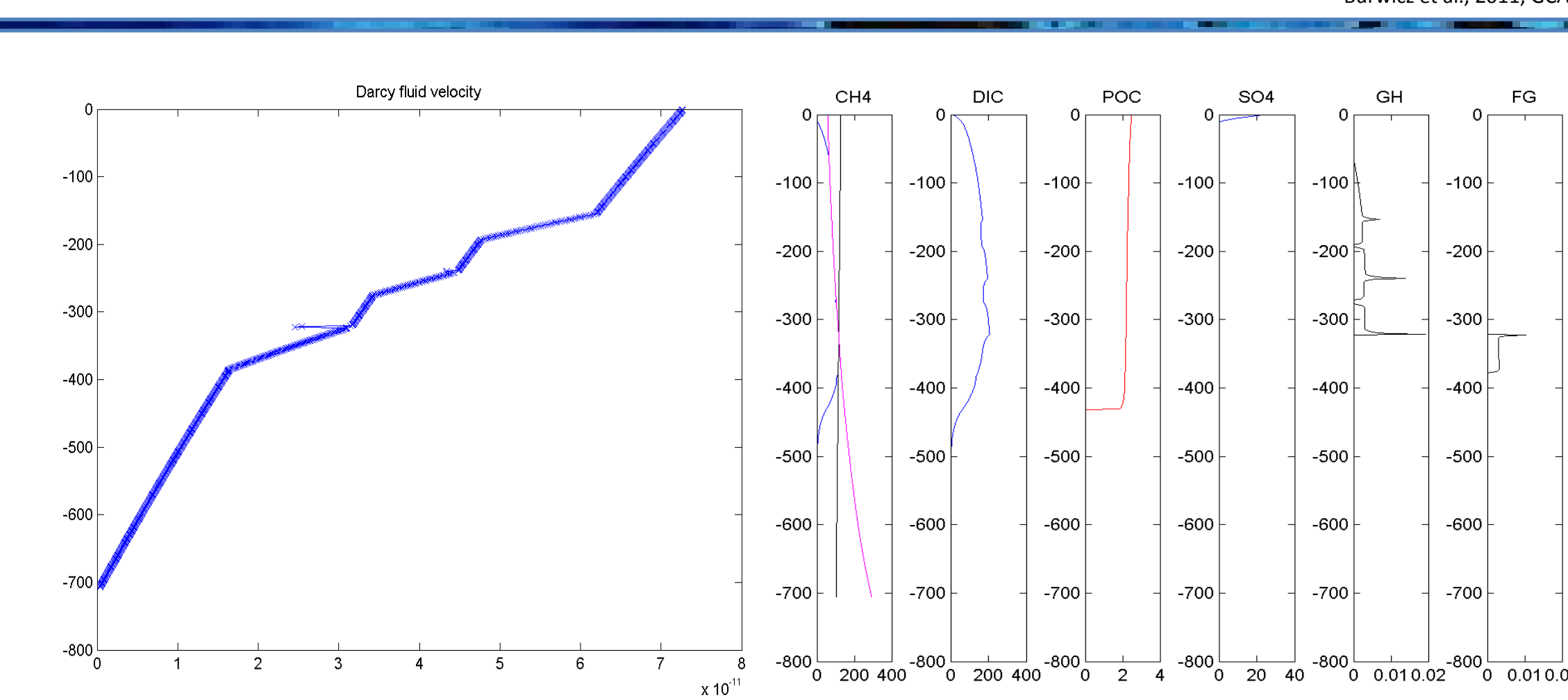
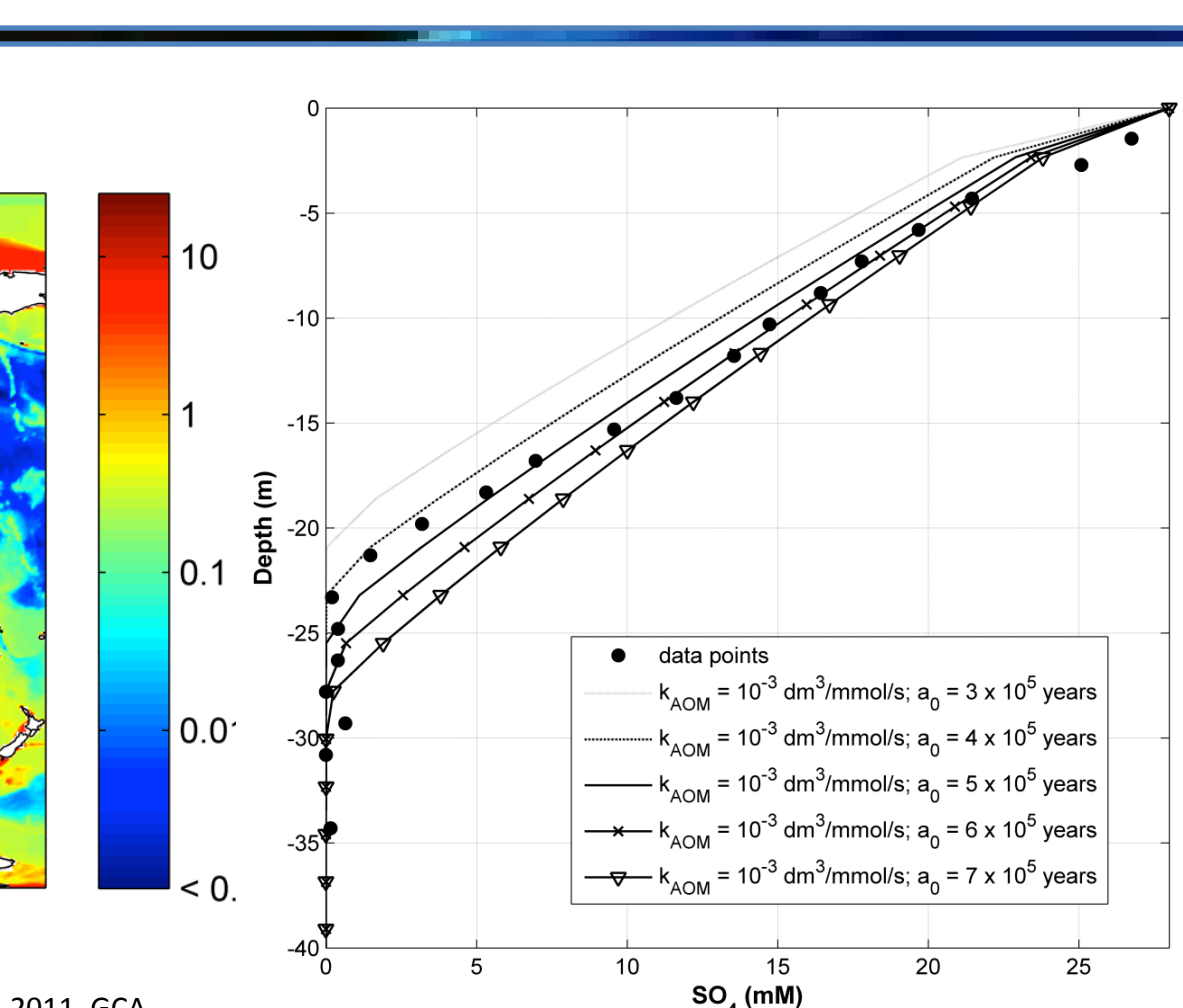
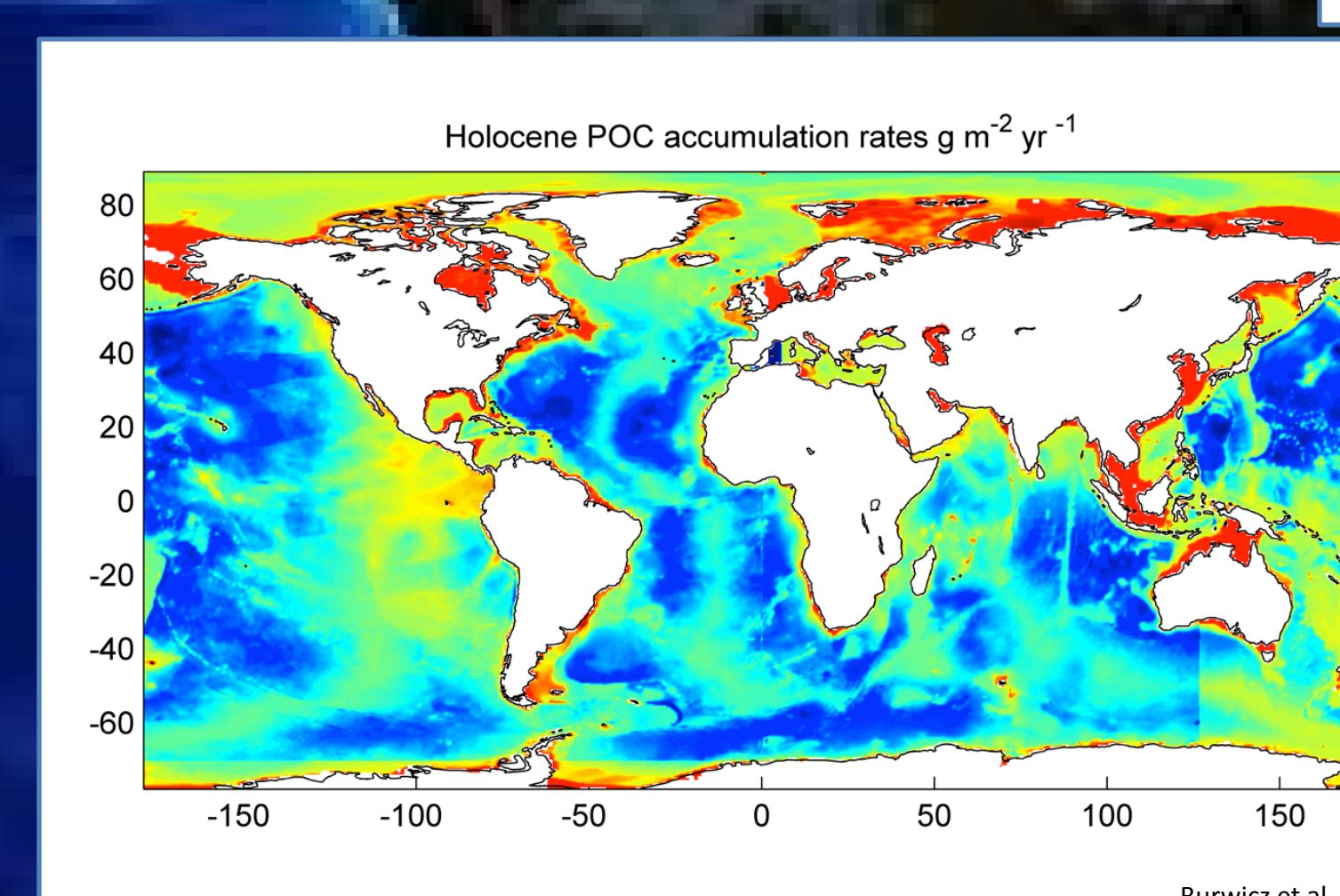
A kinetic rate law of organic matter decomposition (based on Middelburg J., 1989; modified by Wallmann K., 2006)

$$R_{POC} = \frac{K_c}{C(DIC) + C(CH_4) + K_c} \cdot k_x \cdot G(POC)$$

$$k_x = 0.16 \cdot \left(a_0 + \frac{z}{10}\right)^{-0.95}$$

assumes a depth-decreasing reactivity of metabolites

$R_{POC}$  – rate of POC degradation (wt. % · yr<sup>-1</sup>)  
 $K_c$  – Monod inhibition constant (mM)  
 $k_x$  – age-dependent kinetic constant (yr<sup>-1</sup>)  
 $C$ ,  $G$  – concentration of dissolved (mM) and solid (wt. %) species, respectively  
 $a_0$  – initial age of organic matter decomposition (yr)  
 $z$  – depth (cm)  
 $w$  – burial velocity of solid species (cm · yr<sup>-1</sup>)



### Simulation

**Chemical reactions solver**

- In-situ POC degradation kinetics
- Kinetically-controlled biochemical reactions of methanogenesis, sulfate reduction and anaerobic oxidation of methane (AOM)
- Calculation of gas hydrate and free gas solubility in brine
- Gas hydrate and free gas formation (kinetics vs. thermodynamics)

Variables obtained:  
 new concentrations of dissolved chemical species

### Post-processing

**Equation-of-state for 3-phase system H<sub>2</sub>O-NaCl-CH<sub>4</sub> + GH**

Variables obtained:  
 volumes and masses of phases, new  $\rho_f$ ,  $\rho_g$ ,  $S_f$ ,  $S_g$ ,  $S_h$

### Results

- P,T profiles
- Depth-resolved profiles of chemical species concentrations, gas hydrate and free gas saturations
- Full compaction history
- Local/global gas hydrate estimates

