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Continuous Process Performance Enhancements for 50-500 L S.U.B.s

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Continuous Process Performance Enhancements for 50-500 L S.U.B.s

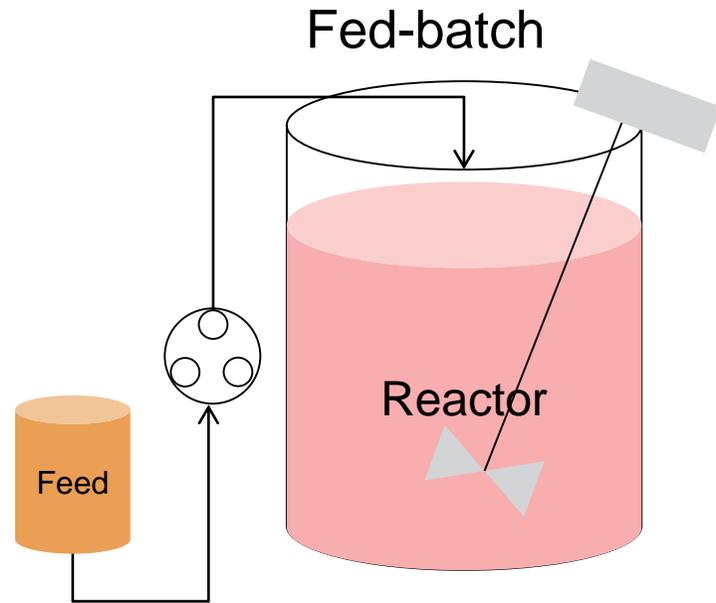
September 25, 2018

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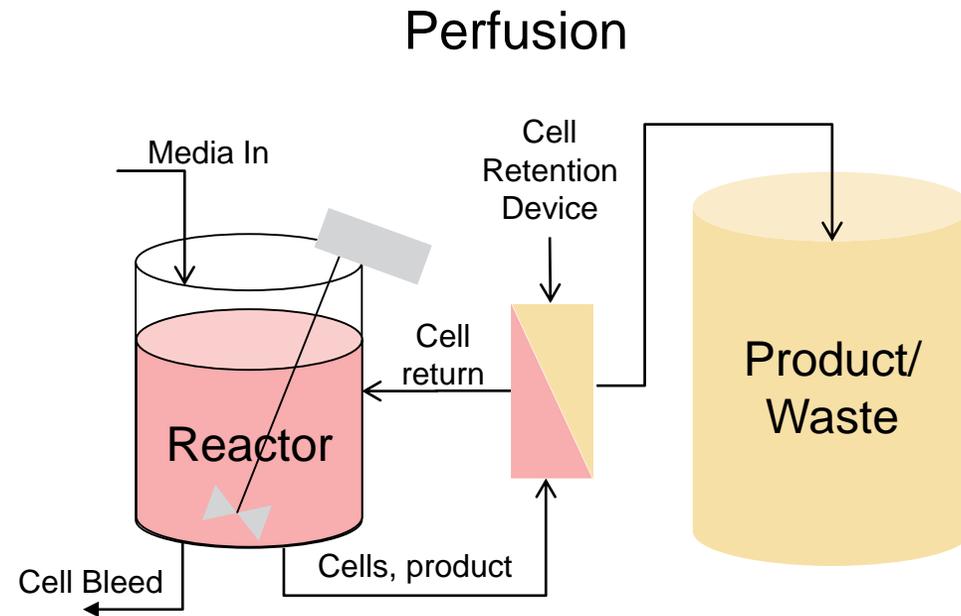
- Perfusion Overview and Workflow
 - Mass transfer limitations
 - Mixing limitations
- S.U.B. Enhancements
- Results
 - Mass transfer performance
 - Cell culture case study
 - Cell culture mass transfer models



Perfusion vs. Fed-batch



- Feed addition from D3-end
- Volume change in reactor
- High titers achievable
- Large production vessels ($\geq 2000\text{L}$)



- Continuous filtration for ≥ 21 days
- Cell retention usually via filtration (0.2-0.65 μm)
 - Concentrated Fed-batch uses 30-50 kDa
- Used for:
 - Unstable products
 - Intensified seed train
 - Cell banking

Perfusion Advantages/Challenges

- Advantages

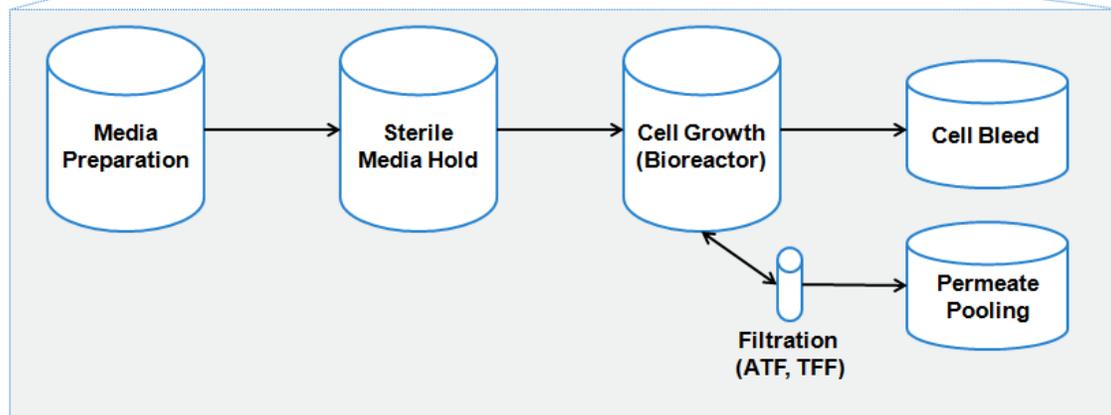
- Smaller reactors
- Healthier culture with less waste = predictable product quality
- Higher cell densities
- Consistency from steady state production
- Less frequent bioreactor turnaround
- Clean harvest stream for DSP
- Continual harvest ensures some success despite late-stage contamination
- Cost savings

- Challenges

- What is steady state?
- Process control and integration
- More complex setup (Regulatory)
- High validation costs
- Filter fouling leads to culture shutdown
- Higher gas usage = foaming risk
- Sensor stability



Perfusion Work Flow



- Thermo Fisher Scientific Offerings:

- Cell line development
- Media optimization
- Media hydration
- Sterile media hold
- **Bioreactor production vessels**
- Product pooling
- Waste containment
- Chromatography resins
- Bulk storage and final fill



Overcoming Legacy S.U.B. System Limitations

- Custom 500 L S.U.B. configuration
 - Standard impeller (25.1 cm diameter)
 - Standard laser DHS (980 pores, 0.368 mm Ø)
 - 2 ea frit (1 standard, 1 additional)

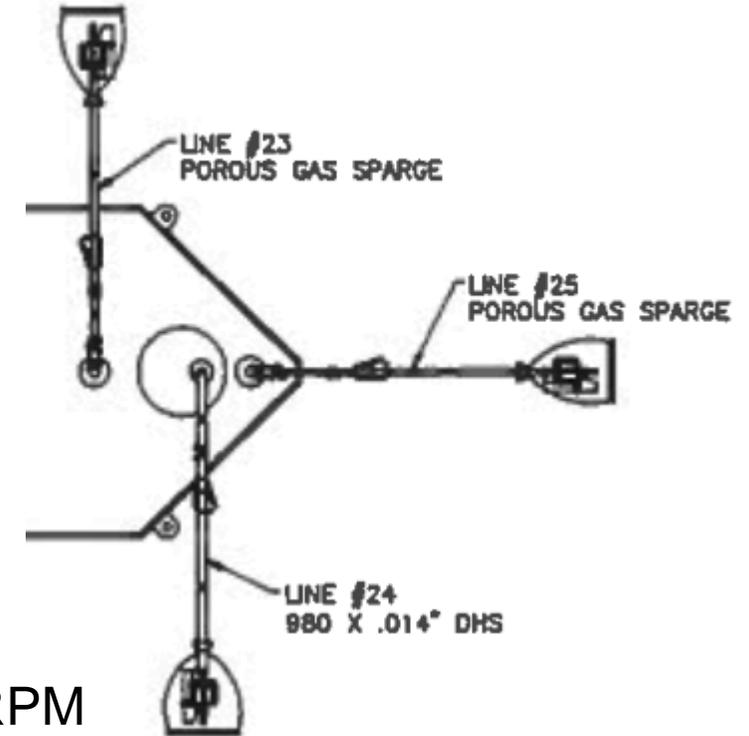
- Standard Dynamic $k_L a$ testing

- 1 g/L pluronic
- 3.5 g/L HEPES
- DHS = **15 slpm**
- Agitation = **150 RPM** (65 W/m^3)

		Additional Frit (slpm)		
		10	20	40
Standard Frit (slpm)	10	36.5	37.6	38.1
	20	37.6	40.5	42.6
	40	39.6	40.2	41.9

- Limited benefit from running frits at extreme flow rates even at max RPM

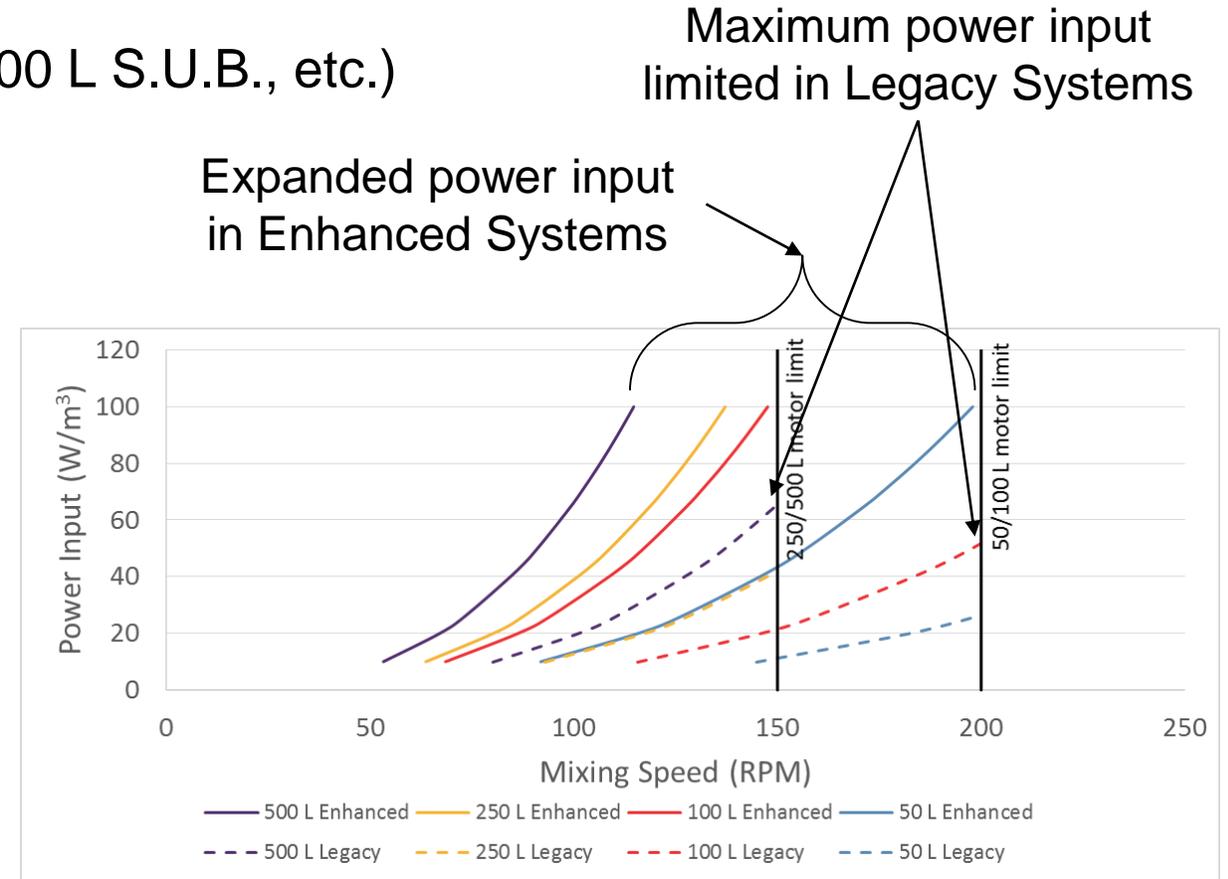
- Combined air sparge of 95 slpm (0.19 VVM) = ~42/hr
- Second option would be to increase DHS sparging rate



S.U.B. Mixing Enhancements

- Implement upsized impeller (1000 L impeller in 500 L S.U.B., etc.)

S.U.B. Size		50	100	250	500
Max Motor RPM		200	200	150	150
Standard Impeller	Diameter (cm)	11.11	14.6	20	25.1
	Speed at 20 W/m ³ (RPM)	182.5	145.8	117.1	101.1
	Max PIV at max RPM (W/m ³)	26.3	51.6	42.0	65.4
Upsized Impeller	Diameter (cm)	14.6	20	25.1	32.1
	Speed at 20 W/m ³ (RPM)	115.7	86.3	80.2	67.1
	Max PIV at max RPM (W/m ³)	103.2	248.9	130.8	223.7

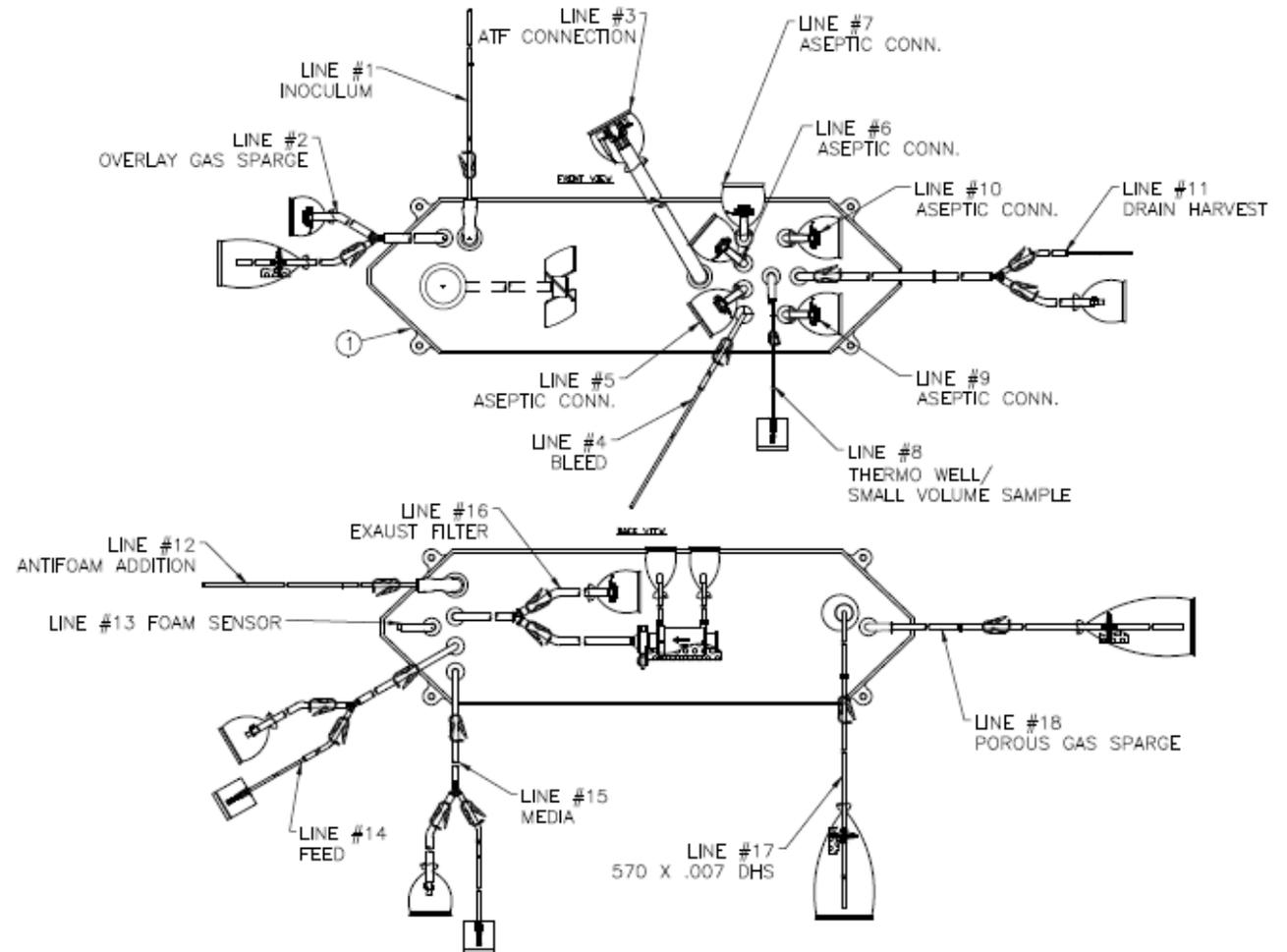


All systems meet objective of 100 W/m³

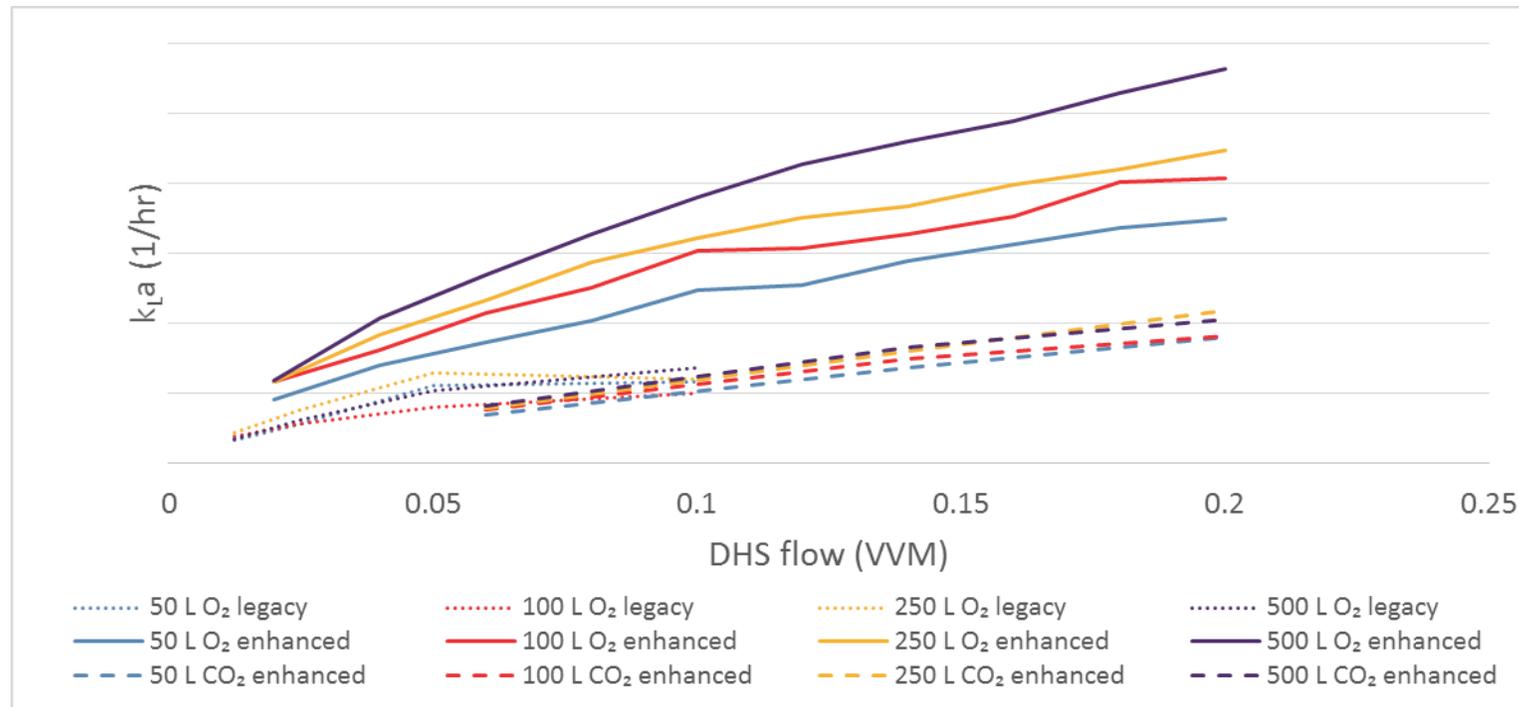
Note: Safely within the qualified design space of the 1000L/2000L S.U.M. (rated up to 350 RPM).

S.U.B. BPC Perfusion Enhancements

1. Enhanced DHS for each S.U.B. size
 - Increased DHS efficiency (smaller pore/bubble)
 - Boost capacity (0.2 VVM @ <15m/s GEV)
 - Frit optional in all S.U.B. designs
2. Upsized impeller in each S.U.B. size (n+1)
3. SU foam sensor for automated antifoam dispensing
4. Port for cell bleed – maintain cell density in perfusion cultures
5. 1" ID ATF/TFF connections available



Characterization Results with Enhanced Sparging and Mixing



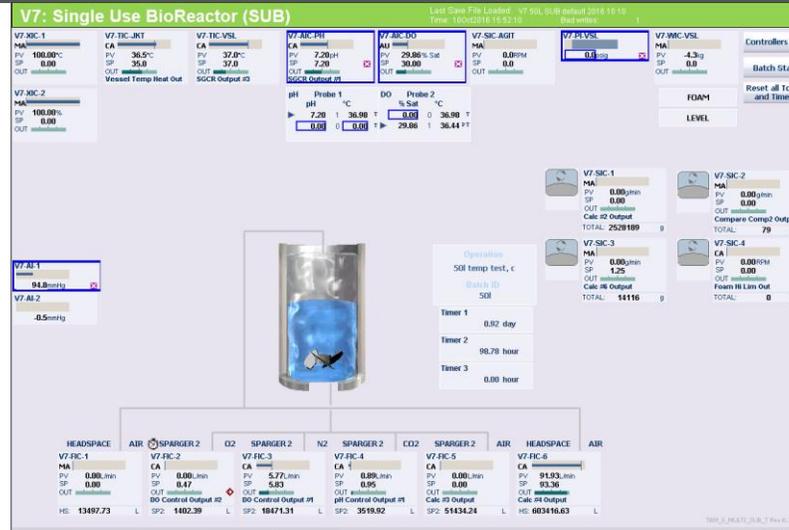
50L Perfusion S.U.B. Case Study Setup

	Components/Conditions	Setting
Cells/Media	Cell Line	CHO-DP12 (Supplied by Repligen)
	Seed Density	0.4×10^6 cells/mL
	Target Cell Density	Various up to maximum
	Media Composition	CD OptiCHO media + 100 ng/mL LR3 + 4 mM Glutamax
	Base	N/A
	Antifoam	Antifoam C (10,000 ppm simethicone stock)
	Glucose	450 g/L stock
Bioreactor	Bioreactor W.V.	40 L
	Temp	37°C
	DO Setpoint	30% (O_2 /air through DHS)
	pH	7.0 ± 0.2 (CO_2)
	Air	Headspace sweep at 2 slpm
	Agitation	107-184 RPM 20-100 W/m^3
	Antifoam dosing	Sensor-based antifoam addition
	Glucose Feed	Maintain 1-3 g/L with constant feed
Cell Bleed	Sensor-based cell bleed (ABER)	
ATF	ATF System	ATF6SU
	ATF Filter	F6:RF02PES 0.2 micron PES HF
	Filter SA	2.53 m^2
	Perfusion rate	Day 0-3: None
		Day 3-26: variable depending on cell density/nutrient demands, 1-4 VVD (40-160 L/day)
	Flux	0.67-2.67 LMH
	ATF Rate	19.2 LPM
	Shear Rate	2264 s^{-1}



Perfusion Process Automation

- Standard
 - DO (TruFluor DO)
 - pH
 - RTD
- Foam sensor linked to antifoam pump
- Cell density sensor linked to cell bleed pump
- S.U.B. load cells linked to media pump (Heaviside equation)



$$\text{Feed} = 2 \cdot \text{Target} \cdot \left(\frac{1}{1 + \exp^{-2 \cdot k \cdot x}} \right)$$



Cell density balance (probe-less)

$$V_R \cdot \frac{dX_R}{dt} = V_R \cdot \mu \cdot X_R - Q_B \cdot X_R$$
$$\mu = \frac{\ln(X_2) - \ln(X_1)}{t_2 - t_1} + \frac{Q_B}{V_R}$$
$$Q_B = \left(\mu - \frac{\ln(X_2/X_1)}{t_2 - t_1} \right) \cdot V_R$$

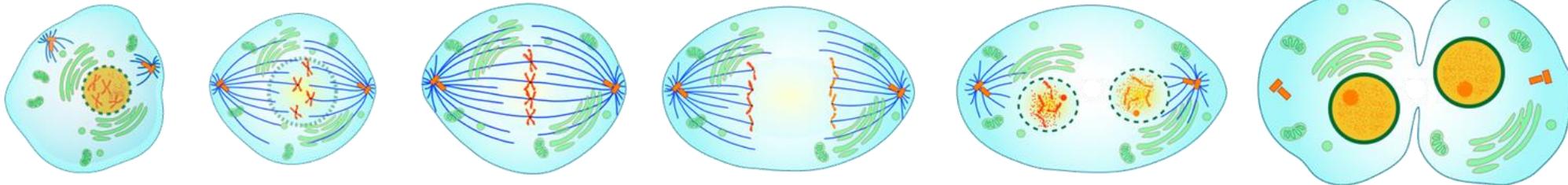


Nomenclature

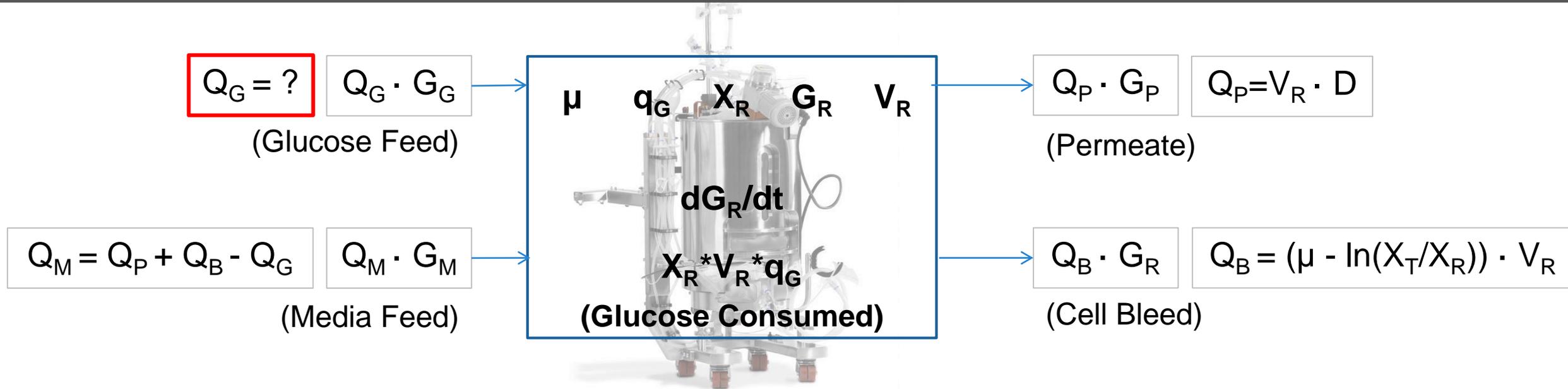
Equation

- Change in cell density = effective growth – cell bleed
- Rearrange, integrate, solve for Q_B to obtain bleed rate
- Best to average growth rates over multiple days

- V_R = reactor working volume
- X_R = cell density
- dX_R/dt = cell density change over time
- μ = cell growth rate
- Q_B = reactor bleed rate



Glucose Mass Balance Equations



Cell Growth:

$$V_R \frac{dX_R}{dt} = V_R \cdot \mu \cdot X_R - Q_B \cdot X_R$$

Overall Glucose Consumption:

$$\frac{dG_R}{dt} = Q_M \cdot G_M + Q_G \cdot G_G - Q_P \cdot G_P - Q_B \cdot G_R - X_R \cdot V_R \cdot q_G$$

If

$$\frac{dG_R}{dt} = 0 \quad \text{and} \quad \frac{dX_R}{dt} = 0$$

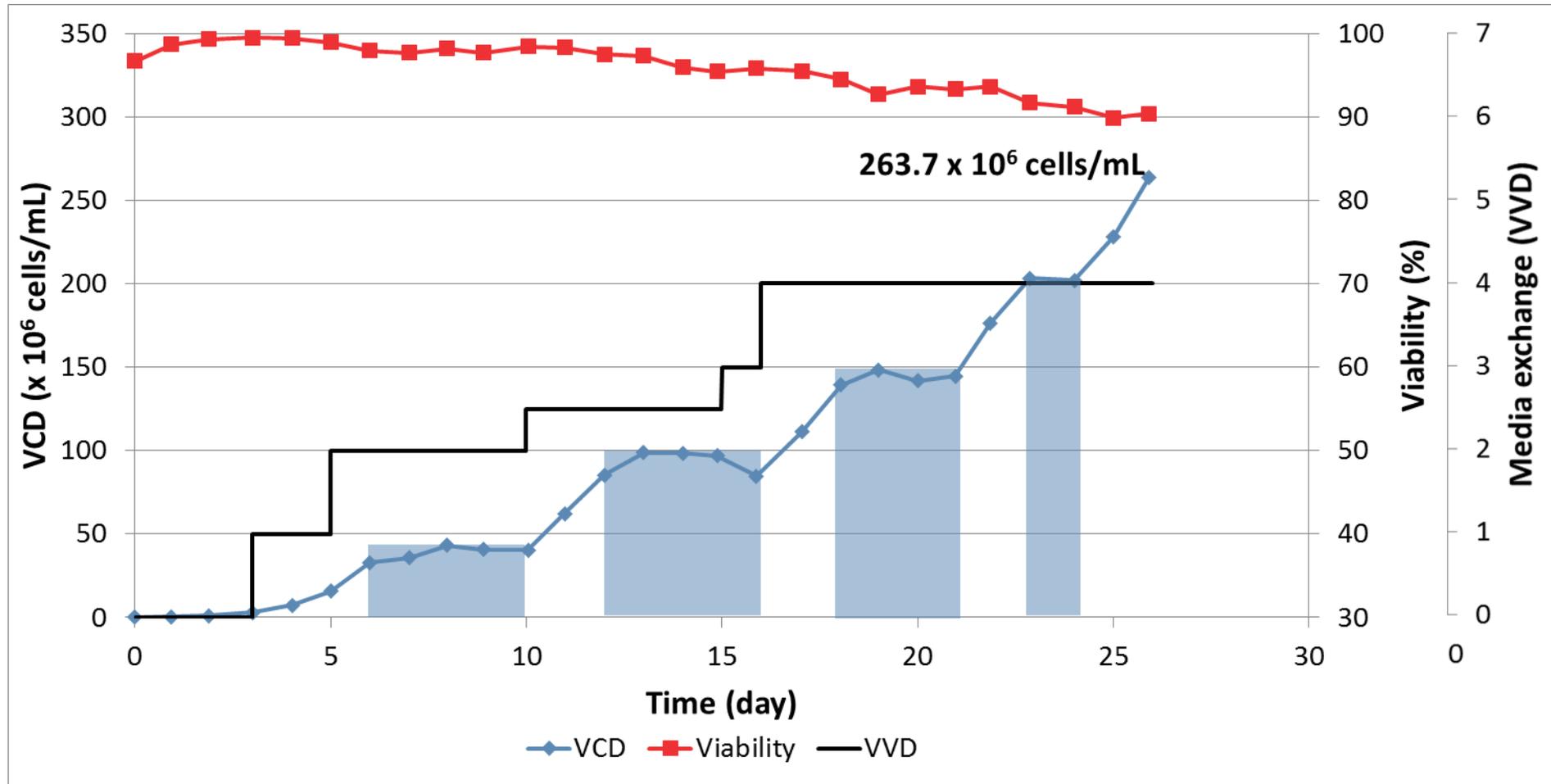
Then

$$Q_G = \frac{[D \cdot G_P + \mu \cdot G_R + X_R \cdot q_G - (D + \mu) \cdot G_M] \cdot V_R}{(G_G - G_M)}$$

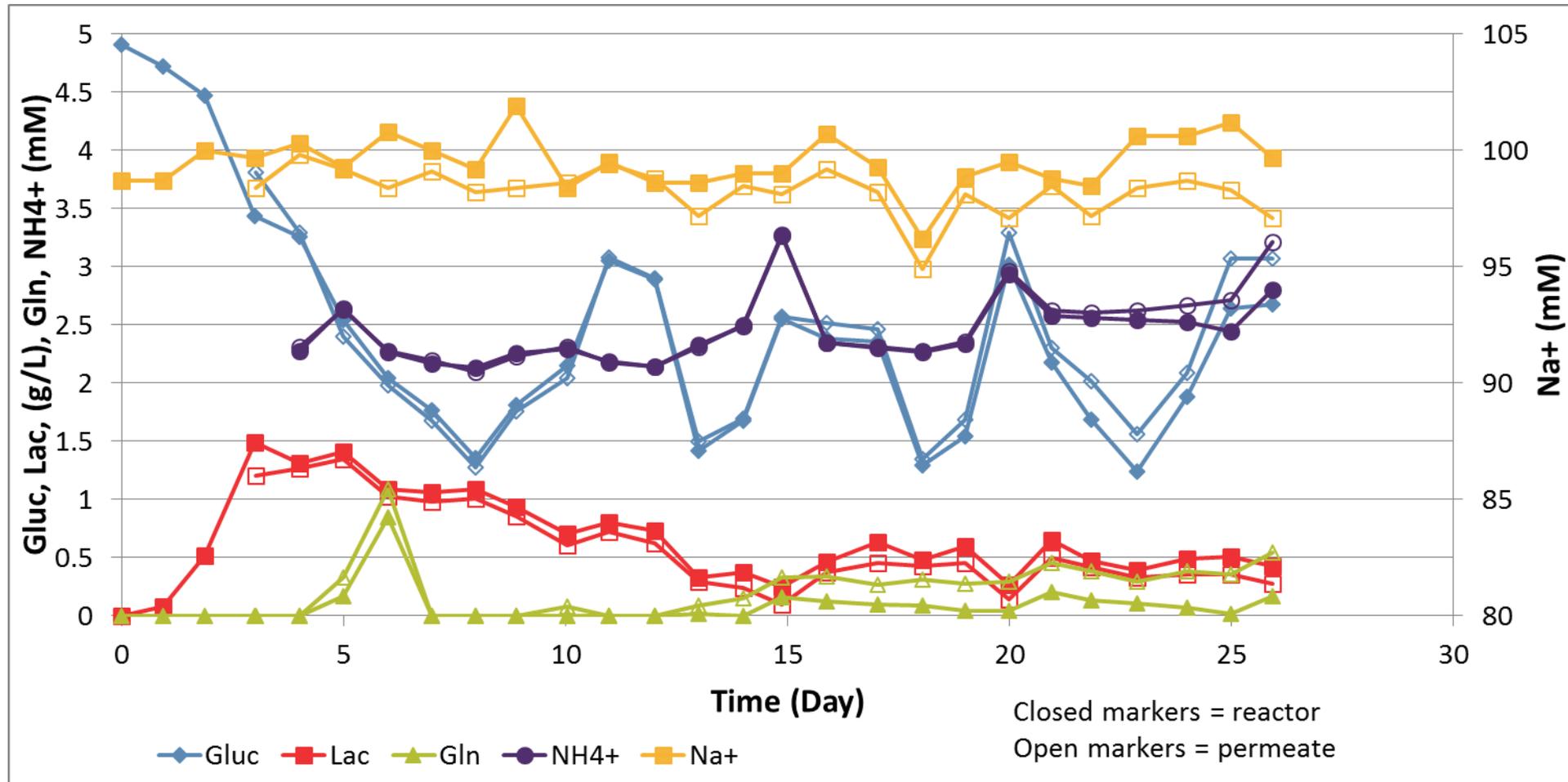
Nomenclature

- Q = flow
- G = [glucose]
- μ = growth
- q_G = gluc consumption
- V = volume
- X = [cells]
- D = perfusion rate

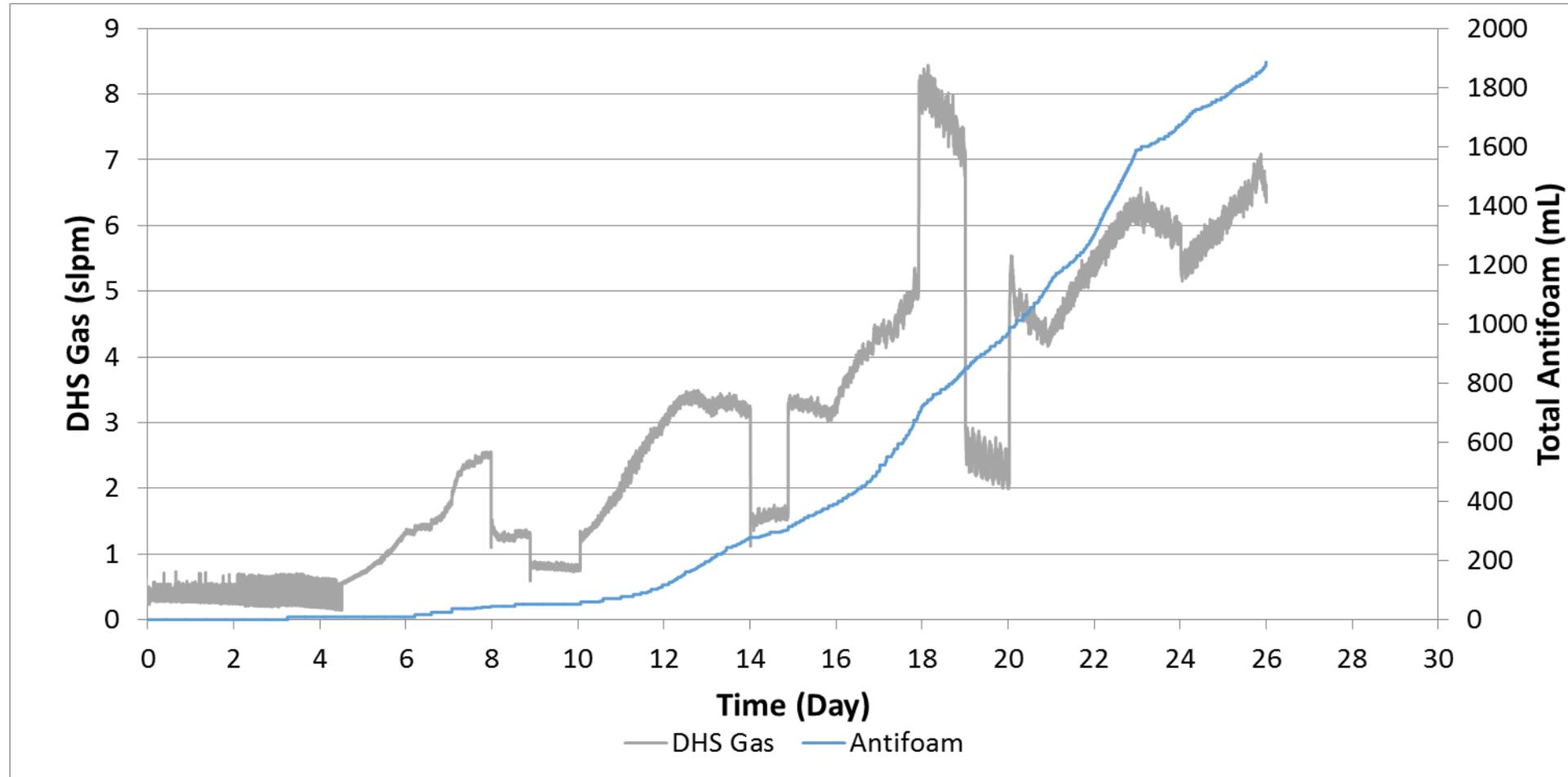
Cell Culture Results – 50 L S.U.B. Cells



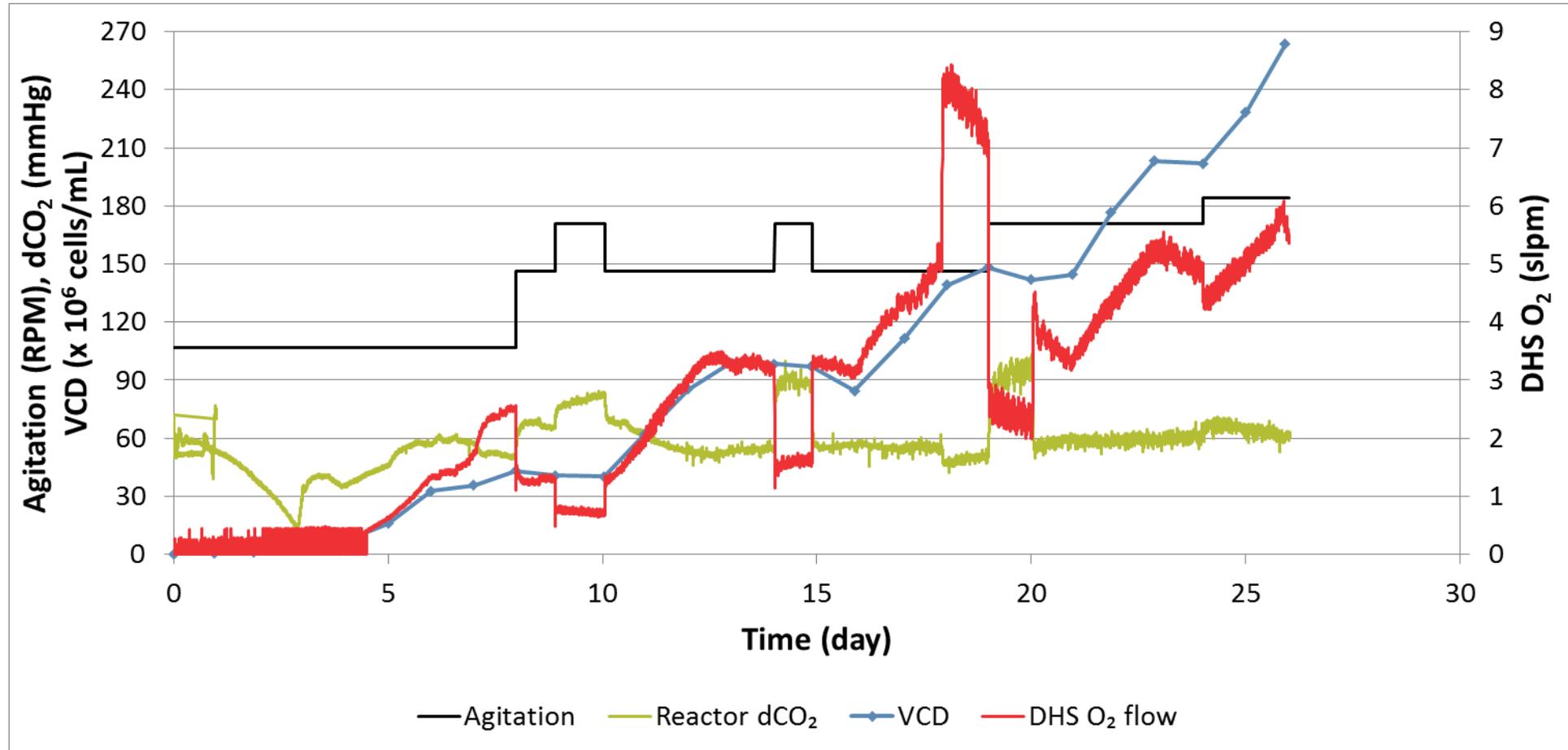
Cell Culture Results – 50 L S.U.B. Culture Parameters



Cell Culture Results – 50 L S.U.B. with Antifoam Control Loop



Cell Culture Results – 50 L S.U.B. Gassing, Agitation



Mass Balance Models – Cells = f(gassing, mixing)

- Can we build an equation to model sustainable cell concentration based on mixing and gassing?

- $OUR = q_{O_2} \cdot C_X$

- $OTR = k_L a \cdot (C_{O_2}^* - C_{O_2})$

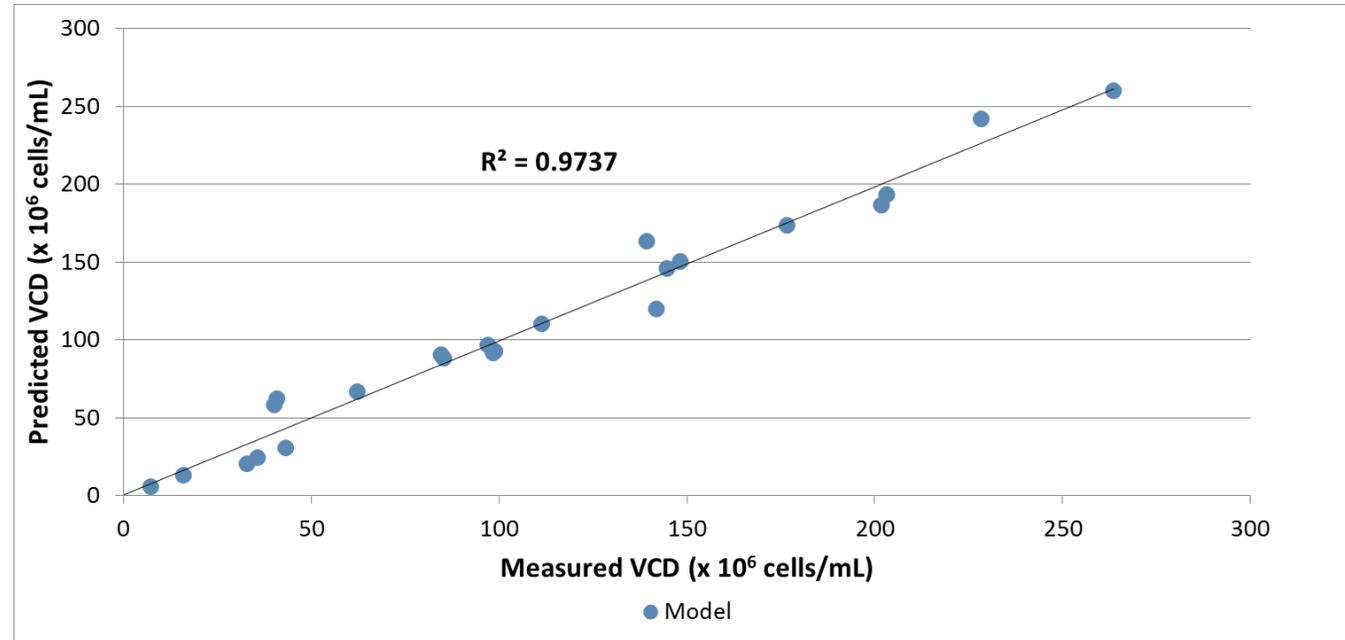
$$C_{O_2} = pp_{O_2,air} \cdot SP$$

$$C_{O_2}^* = \left(\frac{F_{O_2} \cdot pp_{O_2} + F_{air} \cdot pp_{O_2,air}}{F_{TOT}} \right)$$

$$k_L a = \alpha \cdot PIV^\beta \cdot vvm^\gamma$$

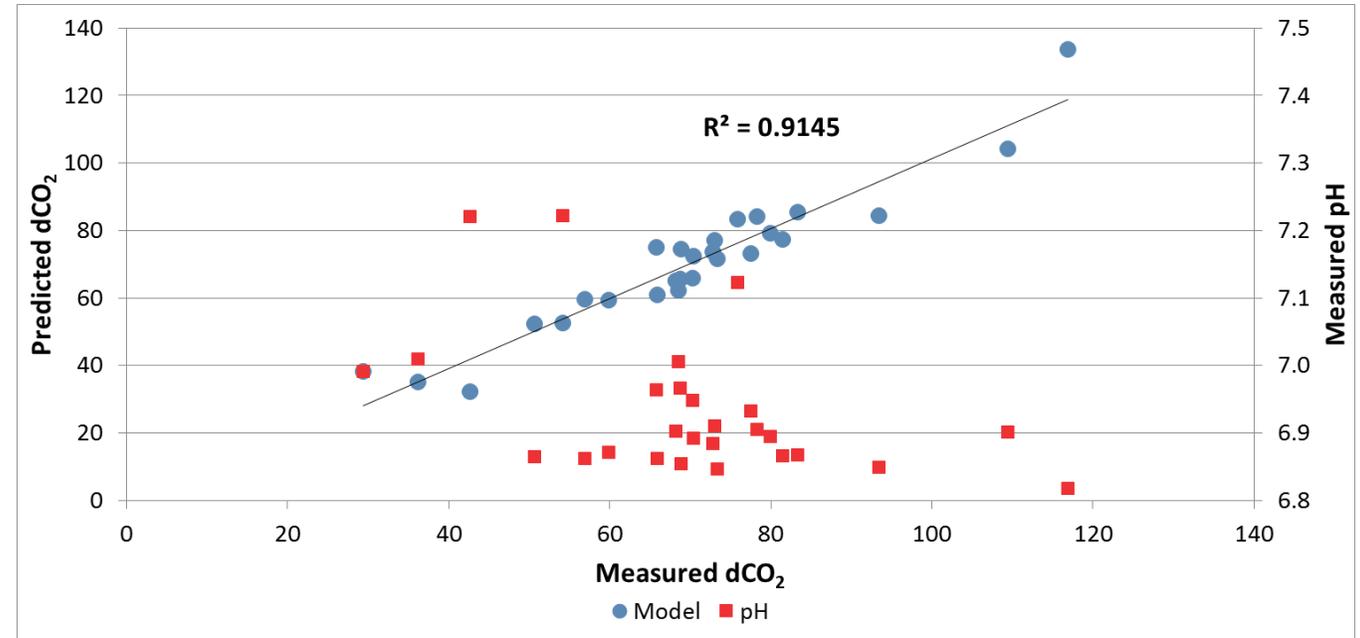
- If $OUR = OTR$

- $\therefore q_{O_2} \cdot C_X = \alpha \cdot PIV^\beta \cdot vvm^\gamma \left(\frac{F_{O_2} \cdot pp_{O_2} + F_{air} \cdot pp_{O_2,air}}{F_{TOT}} - pp_{O_2,air} \cdot SP \right)$



Mass Balance Models – $\text{CO}_2 = f(\text{acids, base})$

- pH = baseline pH – acid buildup + base buildup
- Acid/base accumulations
 - CO_2 concentration – controllable ($k_L a_{\text{CO}_2}$)
 - Lactate
 - Ammonium
 - Ammonia
- $k_L a_{\text{CO}_2} = \alpha \cdot PIV^\beta \cdot vvm^\gamma$
- $\therefore \text{CO}_2 = \frac{\text{pH}}{k_L a_{\text{CO}_2} \cdot (\text{acid buildup}) \cdot (\text{base buildup})}$



Conclusions

- S.U.B. enhancements lead to 3-4 fold increases in oxygen mass transfer from legacy vessels
- Scalability of S.U.B.s
- High degree of automation vital to perfusion success
- Achieved $>260 \times 10^6$ cells/mL in cell culture
 - Room for more oxygen mass transfer at all scales
- Highly automated process controlling DO, pH, dCO_2
- Predictive mass transfer models based on culture data
- Further work to be done optimizing media and exchange rates