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Microstructure and Creep Resistance of Ti-rich Mo_{ss} + Mo_5Si_3 + Mo_5SiB_2 Alloys

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Background: Mo-Si-B Phase Diagram

Mo_{ss} + A15 + T₂

good creep/oxidation resistance
acceptable ductility

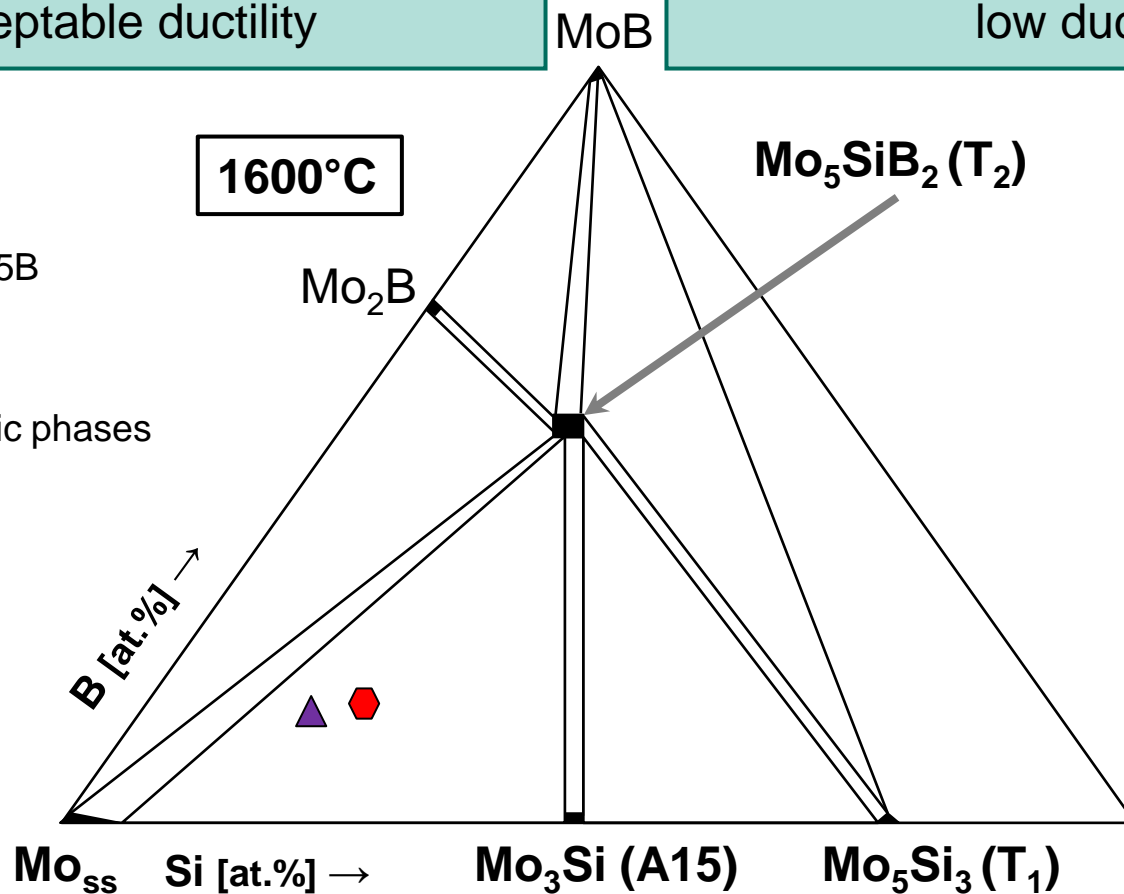
A15 + T₁ + T₂

very good creep/oxidation resistance
low ductility

Typical alloys:

- ◆ Mo-12.5Si-8.5B
- ▲ Mo-9Si-8B

50-60% intermetallic phases
T_m ≥ 2000°C



Schematic according to
Nowotny et al.,
Monatshefte für Chemie
(1957)
Nunes et al., *Structural Intermetallics* (1997)

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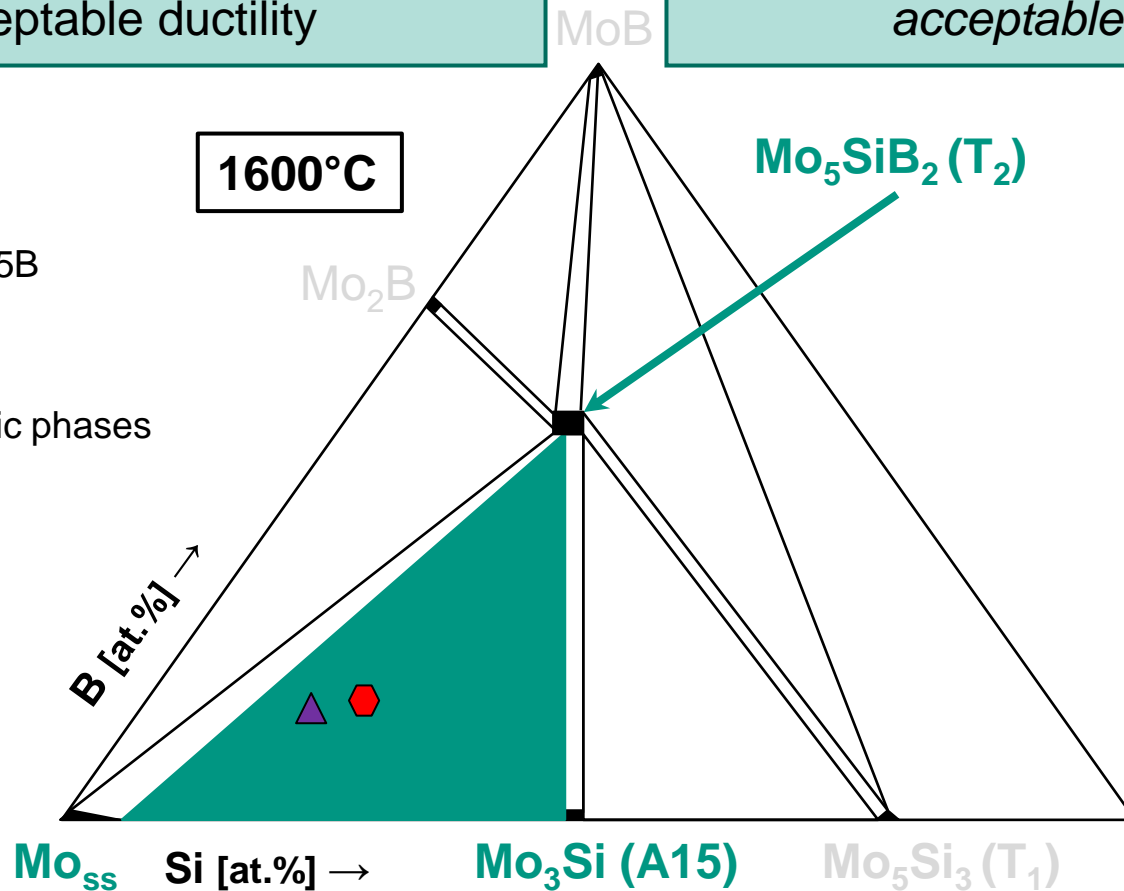
Optimal Mo_{ss} + T₁ + T₂

very good creep/oxidation resistance
acceptable Ductility

Typical alloys:

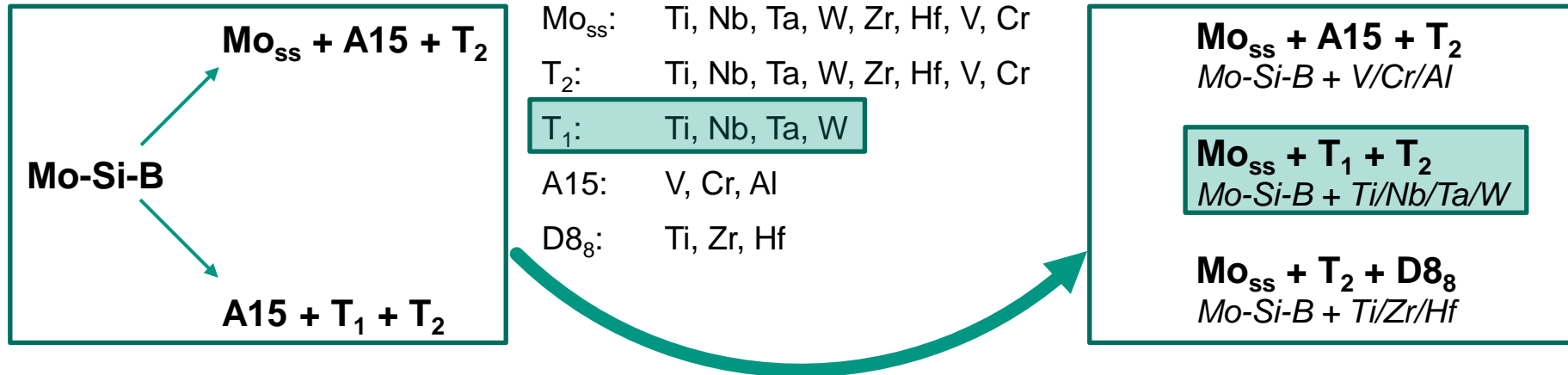
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Alloying Concept in Mo-Si-B Alloys

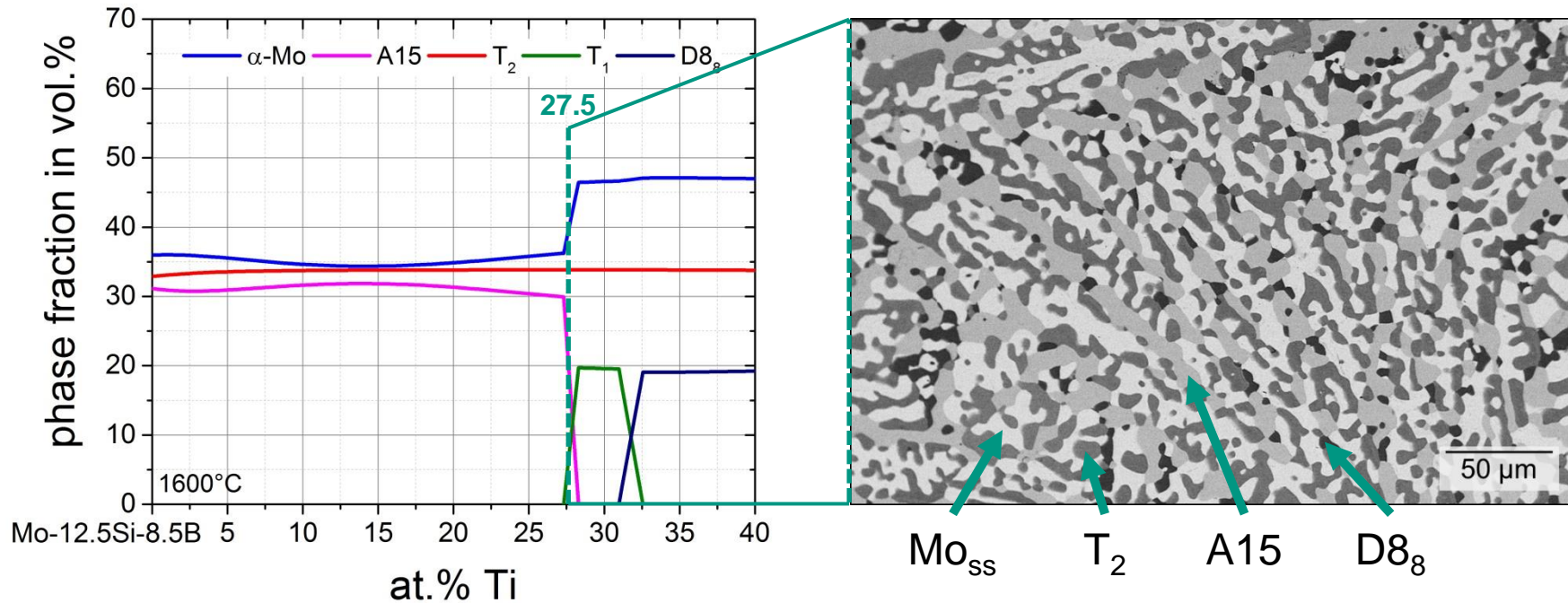


Schematic according to
 Sakidja et al., *Acta Mater.* **56** (2008)
 Yang et al., *Acta Mater.* **58** (2010)

- Some elements can stabilize additional phase equilibria
- Mo_{SS} + T₁ + T₂ by alloying with **Ti**, Nb, Ta, W

Thermodynamic calculation of Mo-Si-B-xTi alloys

Mo-12.5Si-8.5B-27.5Ti 1600 °C 150 h



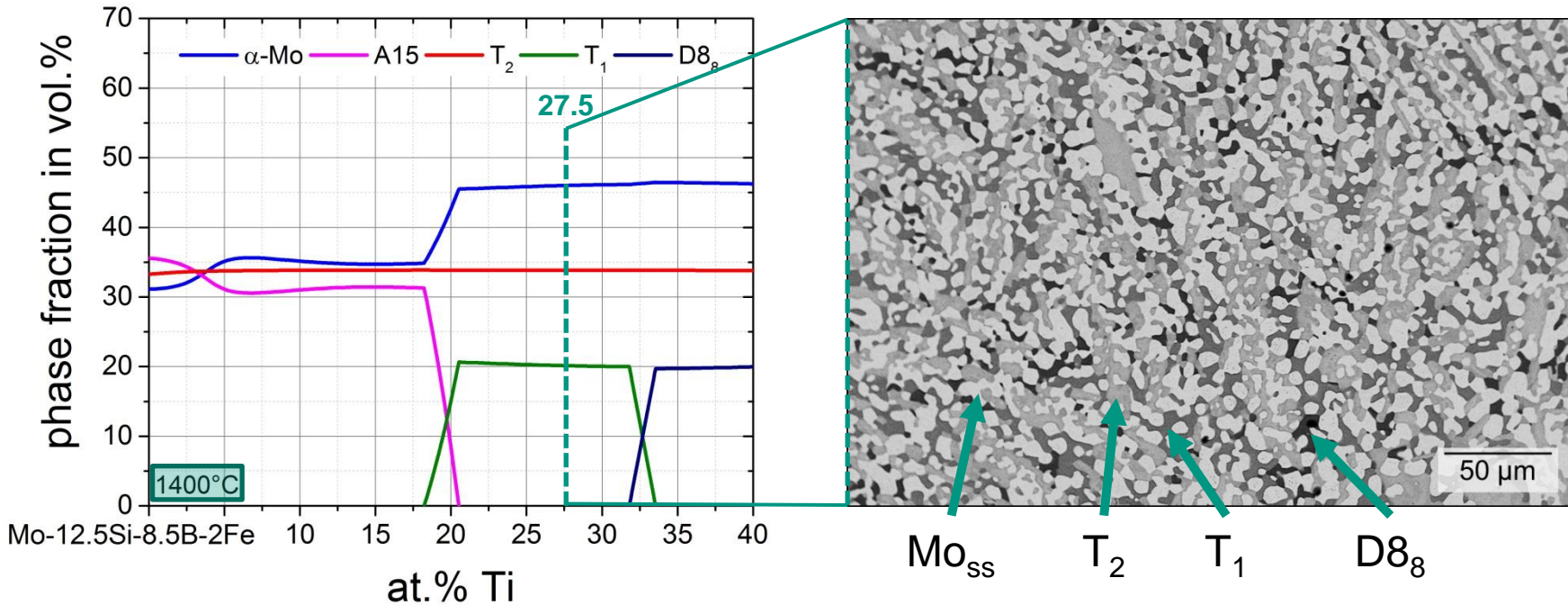
- Formation of T_1 instead of A15 phase and increase of Mo_{ss} phase fraction at 27 at.% Ti
- Yang et al. [1] found $Mo_{ss} + T_1 + T_2 + A15$ phase equilibria at 1600°C
- Could not be reproduced in this work

➔ How can T_1 be stabilized?

[1] Yang et al., *Acta Mater.* **58** (2010)

Effect of Fe on stability of $Mo_{ss} + T_1 + T_2$ phase equilibria

Mo-12.5Si-8.5B-27.5Ti-2Fe 1400 °C 100 h

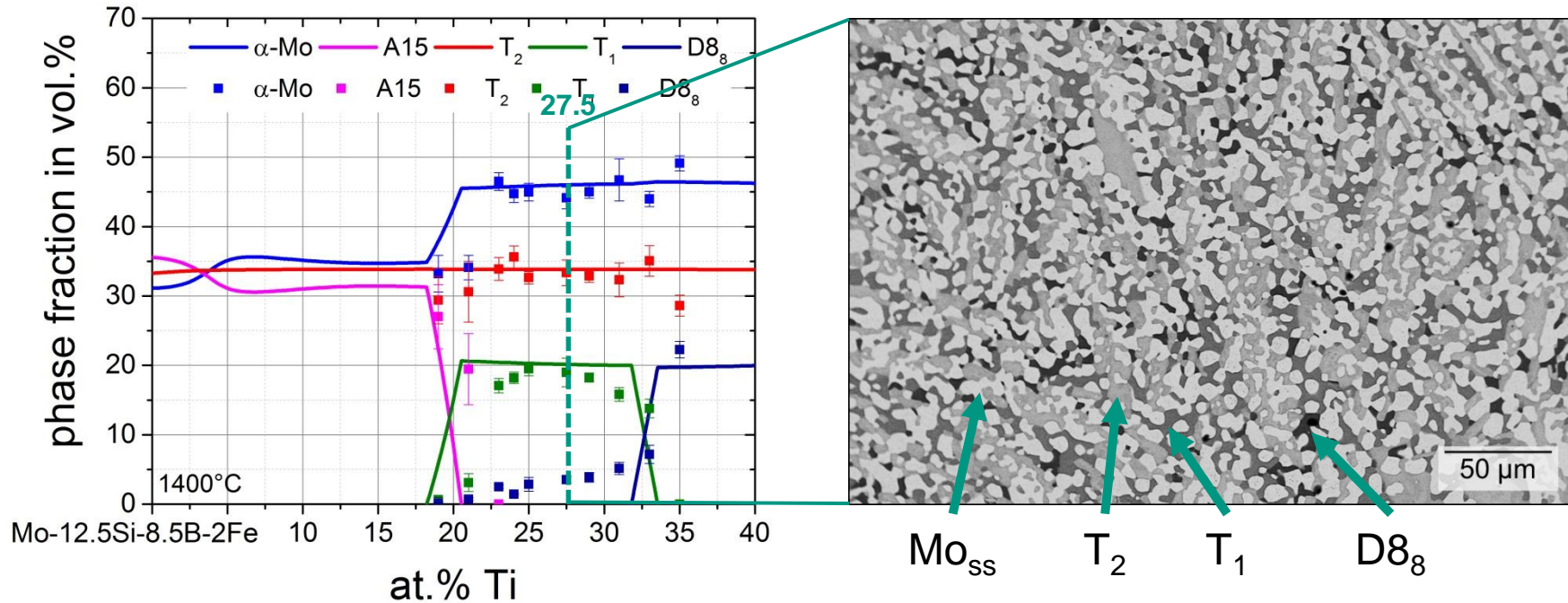


- Ti-concentration for $Mo_{ss} + T_1 + T_2$ phase equilibrium is expanded by 2 at.% Fe
- Heat treatment at lower Temperature increase possible Ti-concentration
- $D8_8$ as a residual phase below 3 vol.%

➔ Validation for Mo-12.5Si-8.5B-xTi-2Fe at 1400°C

Experimental results for Mo-12.5Si-8.5B-xTi-2Fe

Mo-12.5Si-8.5B-27.5Ti-2Fe 1400 °C 100 h

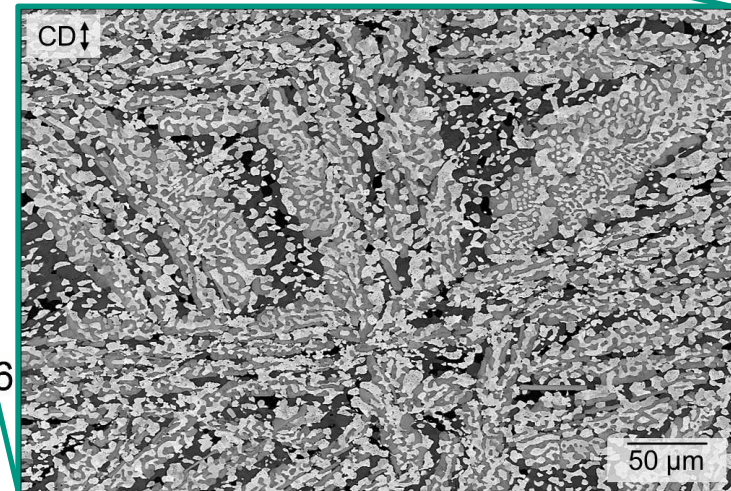
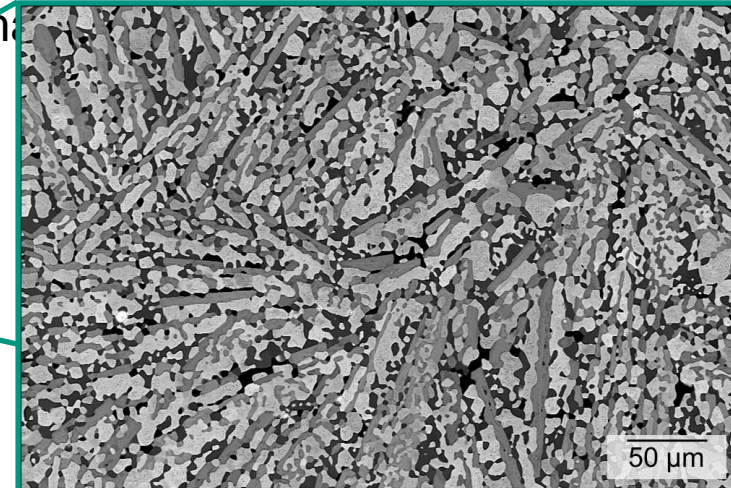
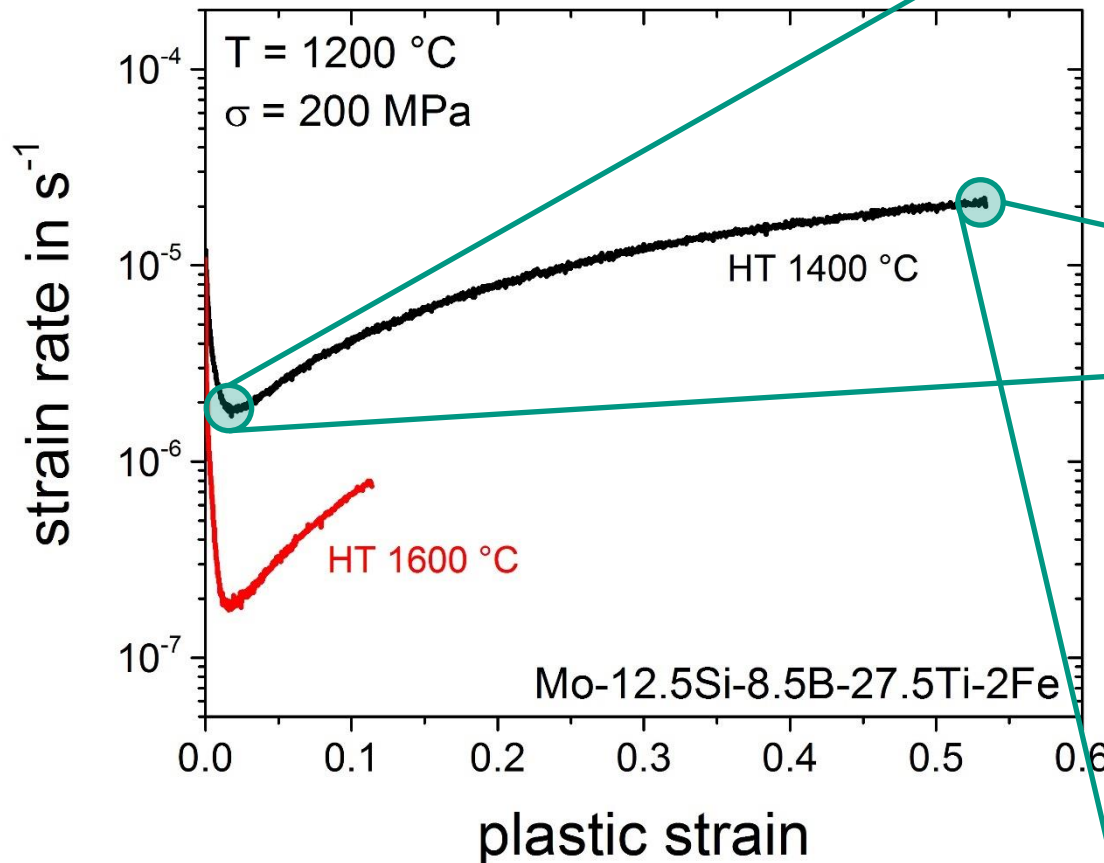


- Results and simulation are in good agreement, slight shift to higher Ti
- T_1 stable for wide range of Ti after heat treatment at 1400°C

➔ How is the creep behavior of $Mo_{ss} + T_1 + T_2$ alloys?

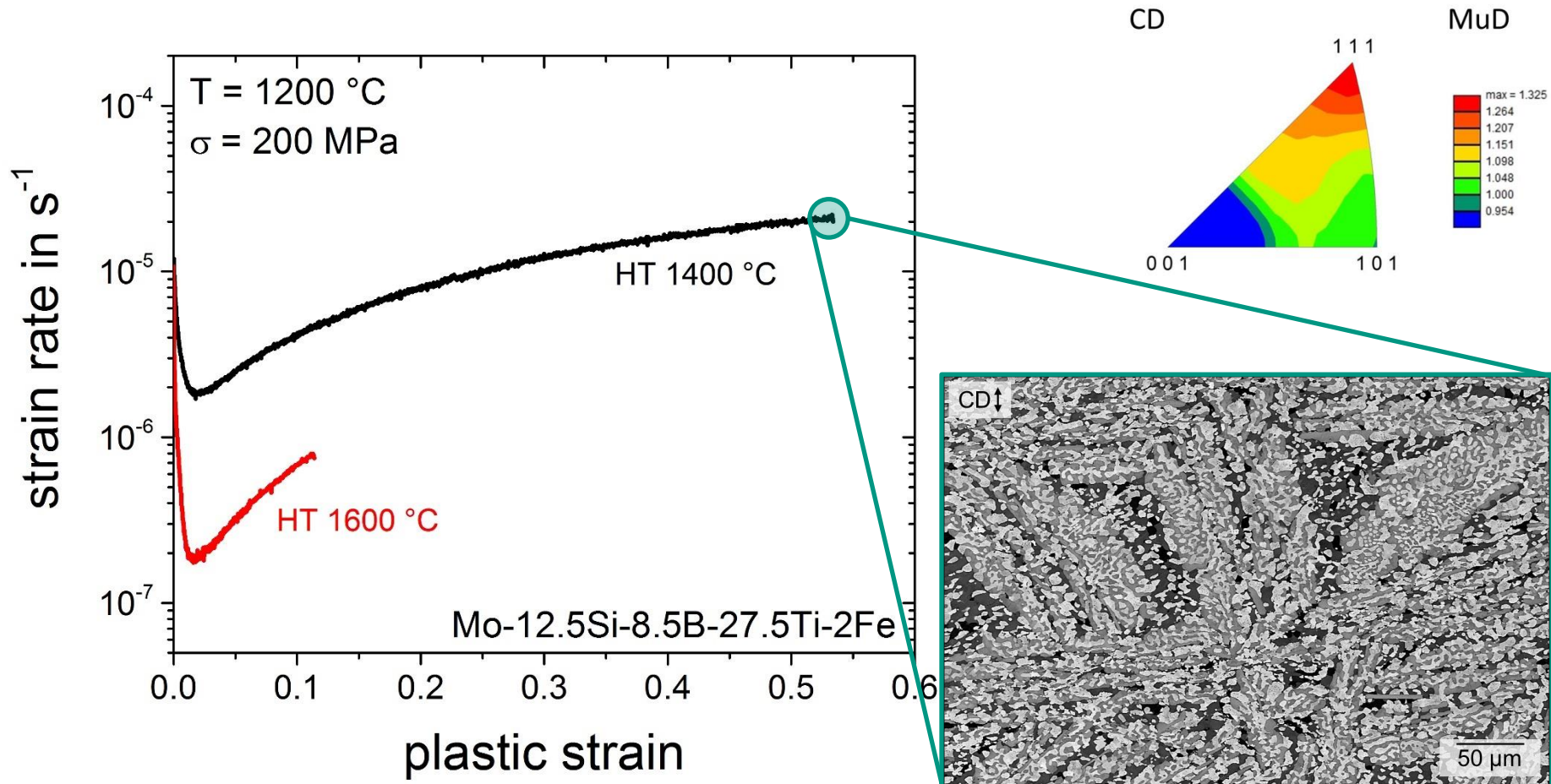
Creep behavior of $\text{Mo}_{\text{ss}} + \text{T}_1 + \text{T}_2$ alloys

- Compression creep behavior was examined in vacuum
- Formation of slight $\langle 111 \rangle$ texture during deformation



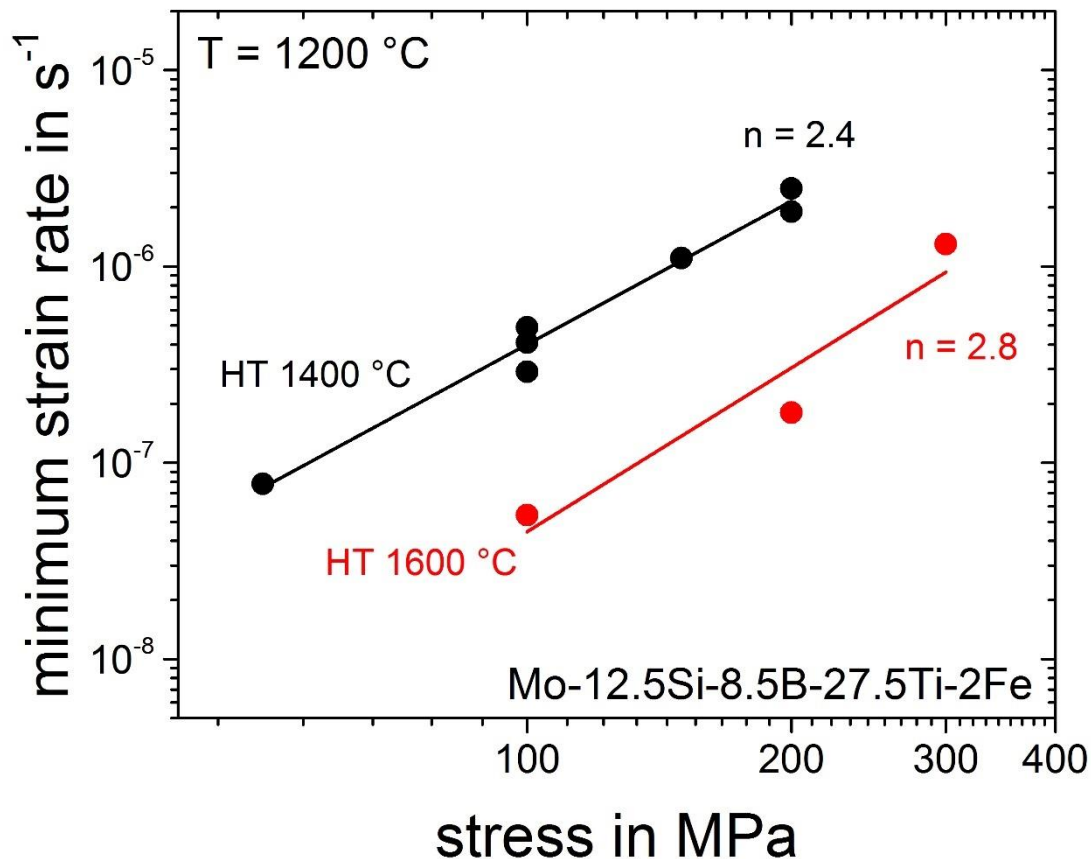
Creep behavior of $\text{Mo}_{\text{ss}} + \text{T}_1 + \text{T}_2$ alloys

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- Formation of slight $\langle 111 \rangle$ texture during deformation of Mo_{ss}



Creep behavior of $\text{Mo}_{\text{ss}} + \text{T}_1 + \text{T}_2$ alloys

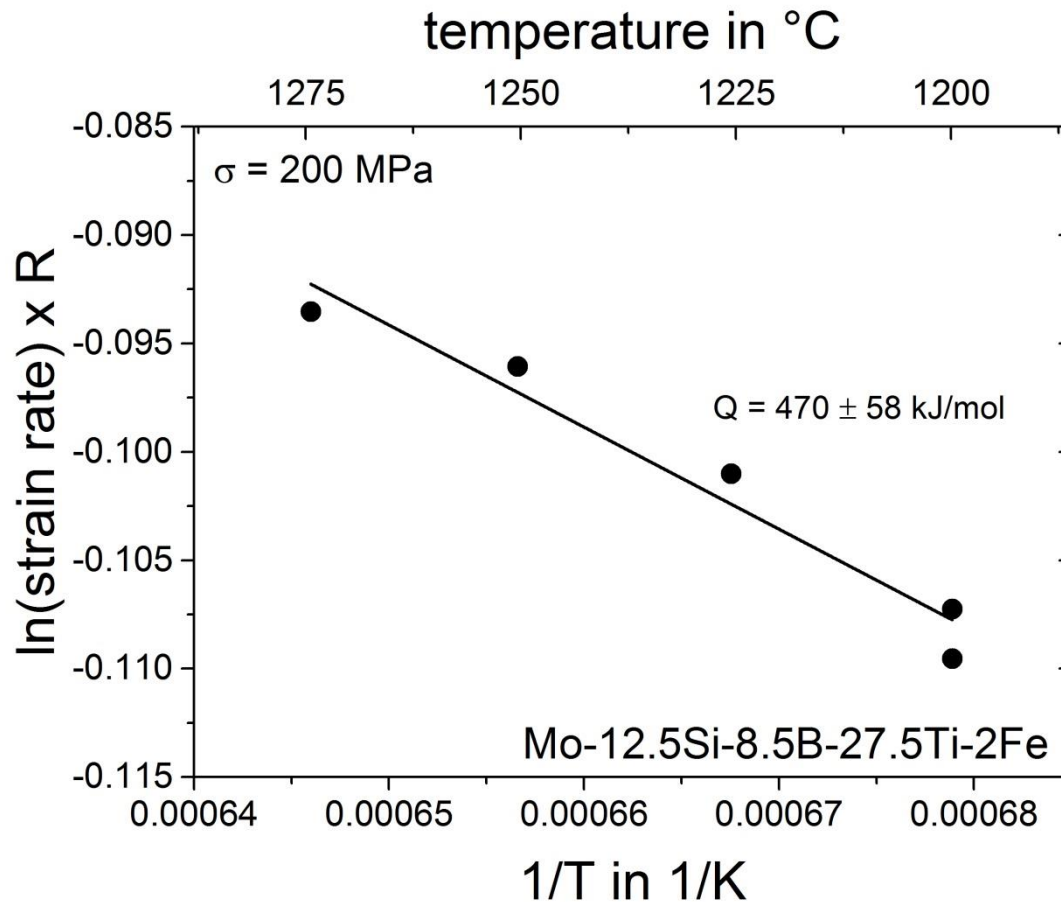
Norton Plot



- Value of n is close to 3
- suggests dislocation climbed controlled creep in Mo_{ss} as dominate mechanism

Creep behavior of $\text{Mo}_{\text{ss}} + \text{T}_1 + \text{T}_2$ alloys

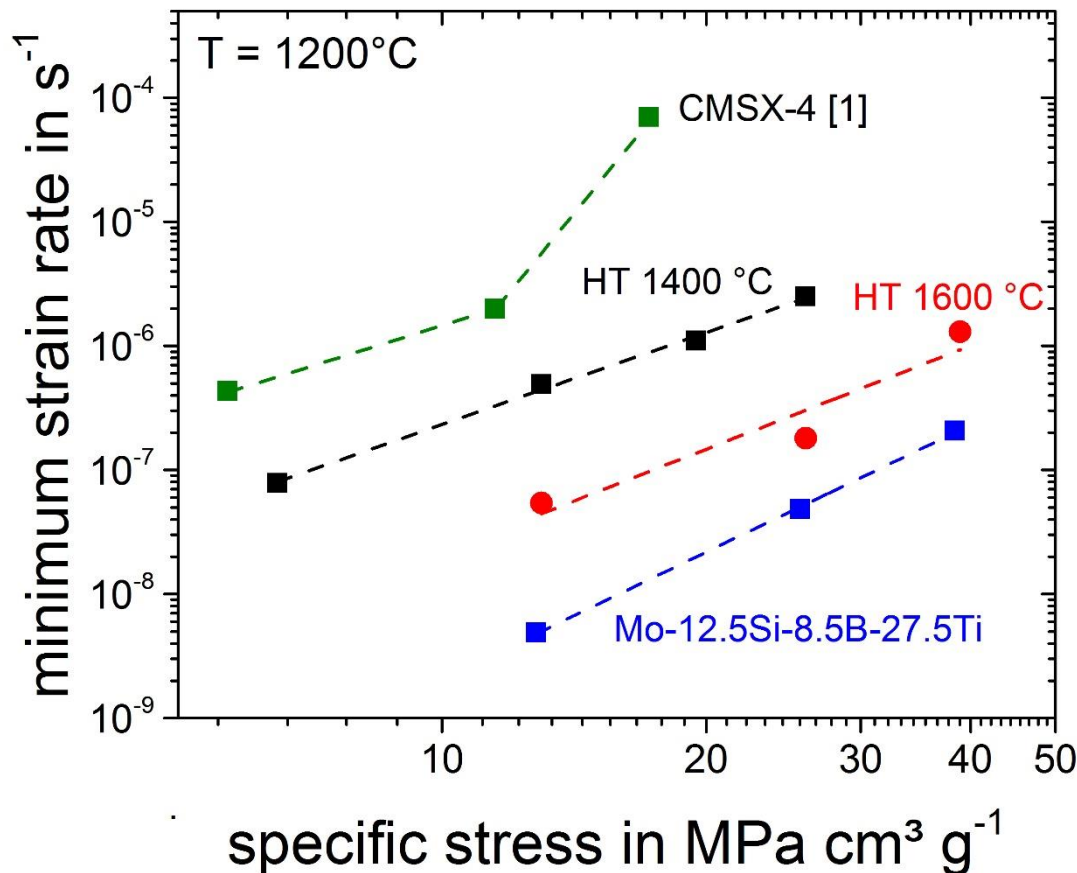
Arrhenius Plot



- Activation energy only slightly larger than for pure Mo self diffusion (405 kJ/mol)
- suggests dislocation climbed controlled creep in Mo_{ss} as dominate mechanism
- higher value probably by interdiffusion of Ti in Mo

Creep behavior of $\text{Mo}_{\text{ss}} + \text{T}_1 + \text{T}_2$ alloys

Literature comparison



- $\text{Mo}_{\text{ss}} + \text{T}_1 + \text{T}_2$ alloys have better creep resistance than CMSX-4 at 1200°C
- Mo-12.5Si-8.5B-27.5Ti have lowest minimum strain rates

[1] Heilmaier et al., *JOM* 61 (2009)

Summary and Conclusion

- $\text{Mo}_{\text{ss}} + \text{T}_1 + \text{T}_2$ phase equilibria is stable in Ti-rich Mo-Si-B alloys while Fe is present
- T_1 is stabilized for wide range of Ti
- Necessary Ti-concentration depends also on HT temperature
- Simulation and Experiment are in good agreement

- Creep is controlled by dislocation climb in Mo_{ss} at 1200 °C
 - Refinement of microstructure during creep deformation
 - Slight $\langle 111 \rangle$ texture in compression direction
 - Stress exponent n is close to 3
 - Activation energy of 470 kJ/mol slightly higher than Mo self diffusion (405 kJ/mol) → Interdiffusion coefficient?
- Creep resistance higher than for CMSX-4

Thank you for your Attention!

Acknowledgement

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DFG Deutsche
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