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Raman Sharma Department of Chemical Engineering, Birla Institute of Technology and Science Pilani, Rajasthan, India., ramansharma_env@yahoo.com

Mines ParisTech 60 Boulevard Saint-Michel, 75006 Paris, France.

Arnaud Delebarre 60 Boulevard Saint-Michel, 75006 Paris, France.

Babu Alappat Department of Civil Engineering, Indian Institute of Technology Delhi, Hauz Khas, New Delhi, India.

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RECIRCULATING FLUIDIZED BED REACTOR FOR CHEMICAL-LOOPING

RAMAN SHARMA¹, ARNAUD DELEBARRE², BABU ALAPPAT³/

¹Department of Chemical Engineering, Birla Institute of Technology and Science Pilani-Køjasthan, India. ²Mines ParisTech, 60 Boulevard Saint-Michel, 75006 Paris, France

³Department of Civil Engineering, Indian Institute of Technology Delhi, Hauz Khas, Mew Delhi – 110016, India.

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OUTLINE OF PRESENTATION

- Chemical-Looping Combustion (CLC)
- Existing reactor arrangements for CLC
 - Single reactor arrangement
 - Interconnected reactor arrangement
- Issues related to the existing reactor arrangements
- > Re-Circulating Fluidized Bed (RCFB) Reactor design for CLC
- > How RCFB overcomes the issues related to the existing reactor designs?
- Conclusions

CHEMICAL LOOPING COMBUSTION (CLC)



Reaction Equations in CLC

Air Reactor

 $Me + \frac{1}{2}O_2 \rightarrow MeO$

Fuel Reactor

 $(2n+m)MeO + C_nH_{2m} \rightarrow (2n+m)Me + mH_2O + nCO_2$

REQUIREMENTS FOR CLC

- Split the combustion in oxidation and reduction cycles by introducing metal oxides
- Air reactor is a high velocity reactor for the transfer of bed material within the reactors
- Fuel reactor is a low velocity reactor for higher residence of bed material
- Wear and tear resistant metal oxide and reactors
- Reactive metal oxide for higher fuel conversion
- Good solid circulation rate for proper transfer of heat and reactants within the reactors

REQUIREMENTS FOR CLC

- Reactor system with low gas by passing required for the purity of the CO_2 capture
- Low particle agglomeration required for proper particle flow and uniform temperature in the reactors
- Regimes of fluidizations

VARIOUS REACTOR CONFIGURATIONS

• Single reactor configuration

• Interconnected reactor configuration



SINGLE REACTOR ARRANGEMENT

SINGLE REACTOR CONFIGURATION



Externally heated low velocity batch fluidized bed reactor of quartz. (Leion, H.; Mattisson, T.; Lyngfelt, A. The use of petroleum coke as fuel in chemical-looping combustion, *Fuel*. 2007, 86, 1947-1958)



Batch fluidized bed reactor of stainless steel working in the low velocity and high velocity cycles.

(Hoteit, A.; Chandel, M.K.; Durécu, S.; Delebarre, A. Biogas combustion in chemical looping fluidized bed reactor, International Journal of Greenhouse Gas Control. 2009, 3, 561-567)

INTERCONNECTED REACTORS ARRANGEMENT (CONTINUOUS MODE)

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<u>Circulating Fluidized Bed</u>



•The setup involves two separate reactors and of course a cyclone.

•Particles from the riser escape out on increasing the fluidization velocity.

•Cyclone collects the particles.

•Collected particles are diverted into the standpipe.

•Standpipe is also fluidized to make the particles to flow back into the riser.

•To avoid the gas bypassing from the riser into the standpipe, a certain bed height is maintained in the standpipe.

•Bed in the standpipe add on to the overall pressure drop.



TWO COMPARTMENT FLUIDIZED BED REACTOR (1 AIR REACTOR /2 / DOWNCOMER, 3 FUEL REACTOR, 4 SLOT, 5 GAS DISTRIBUTOR, AND 6 WIND BOX).

(KRONBERGER, B.; JOHANSSON, E.; LÖFFLER, G.; MATTISSON, T.; LYNGFELT, A.; HOFBAUER, H. A/TWO COMPARTMENT FLUIDIZED BED REACTOR FOR CO₂ CAPTURE BY CHEMICAL-LOOPING COMBUSTION, CHEMICAL ENGINEERING 2ND TECHNOLOGY. 2004. 27(12), 1318-1326.



DUAL CIRCULATING FLUIDIZED BED REACTOR ARRANGEMENT.

(KOLBITSCH, P.; PRÖLL, T.; BOLHÀR-NORDENKAMPF, J.; HOFBAUER, H. DESIGN OF A CHEMICAL LOOPING COMBUSTOR USING A DUAL CIRCULATING FLUIDIZED BED REACTOR SYSTEM, CHEMICAL ENGINEERING AND TECHNOLOGY. 2009, 32(3), 398-403.)

SOME OF THE ISSUES THAT CAN CROP-UP IN THE CLC

► Low residence time of bed material in the air reactor.

- ► High attrition of bed material in the cyclone.
- Cluster formation in the air reactor.
- Complex operation involving loop-seals.
- High heat losses as bed material leaves the air reactor and moves to cyclone.
- ► Gas bypassing.





/closing valve

RE-CIRCULATING FLUIDIZED BED REACTOR



ADVANTAGES OF RCFB REACTOR

- > Cyclone separator is not present in RCFB reactor.
- Bed particles do not leave the reaction site hence less heat losses.
- > RCFB is an excellent mixing device.
- No complex loop seal in case of a single reactor operated in reduction and oxidation cycles.

CLC REACTOR CONFIGURATION USING RCFB REACTOR(S)

► Two interconnected RCFB reactors

 A single RCFB reactor alternatively working in oxidation and reduction cycles.

A single RCFB reactor where central draft tube act as air reactor and the downcomer act as fuel reactor.

VARIABLES DURING THE COLD MODEL EXPERIMENTS

- ▶ Bed Inventory (4 kg, 6 kg, 8 kg, 9 kg, 10 kg).
- ▶ Particle size (Sand Grade I, II, III).
- ▶ Spacer section (3 cm, 8 cm, 15 cm).
- ▶ Jet tube diameter (2.5 cm and 3 cm).

| Sr. No. | Sand Grade | Geldart's Classification | Average Particle Size (mm) |
|---------|---------------------------|--------------------------|----------------------------|
| | | | |
| 1. | Grade I | D | 1.3 |
| | (2mm – 1mm) | | |
| 2. | Grade II | В | 0.5 |
| | (1 mm – 0.5 mm) | | |
| 3. | Grade III | В | 0.35 |
| | (0.5mm – 0.09mm) | | |

SCHEME OF COLD MODEL EXPERIMENTS

| Test | Jet tube diameter (m) | Spacer section (m) | Sand Grade | Inventory (kg) |
|--------|-----------------------|--------------------|------------|----------------|
| Series | | | | |
| 1 | 0.025 | 0.03 | Ι | 4, 6, 8, 9 |
| 2 | 0.025 | 0.08 | Ι | 6, 8, 9 |
| 3 | 0.025 | 0.15 | | 8, 9, 10 |
| 4 | 0.025 | 0.03 | II | 4, 6, 8, 9 |
| 5 | 0.025 | 0.08 | II | 5,8,9 |
| 6 | 0.025 | 0.15 | П | 8, 9, 10 |
| 7 | 0.025 | 0.03 | ш | 4, 6, 8, 9 |
| 8 | 0.025 | 0.08 | | 6, 8, 9 |

SCHEME OF COLD MODEL EXPERIMENTS

| 9 | 0.025 | 0.15 | III | 8, 9, 10 |
|----|-------|------|-----|------------|
| 10 | 0.03 | 0.03 | Ι | 4, 6, 8, 9 |
| | | | | |
| 11 | 0.03 | 0.08 | Ι | 6, 8, 9 |
| 12 | 0.03 | 0.15 | Ι | 8, 9, 10 |
| 13 | 0.03 | 0.03 | II | 4, 6, 8, 9 |
| | | | | |
| 14 | 0.03 | 0.08 | II | 6, 8, 8 |
| 15 | 0.03 | 0.15 | II | 8,9,10 |
| 16 | 0.03 | 0.03 | III | 4, 6, 8, 9 |
| | | | | |
| 17 | 0.03 | 0.08 | III | 6, 8, 9 |
| 18 | 0.03 | 0.15 | III | 8, 9, 10 |

IMPORTANT PARAMETERS FOR CLC

- Regime of Fluidization for air reactor and fuel reactor
 affect the residence time.
- Operating Voidage heat transfer
- ► Residence time fuel conversion
- ► Particle Size conversion
- Solid circulation rate uniform bed temperature



OPERATING VOIDAGE VARIATION IN THE RISER



OPERATING VOIDAGE VARIATION IN THE RISER

2.5 cm jet tube section

3 cm jet tube section

Sand Grade III



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OPERATING VOIDAGE VARIATION IN THE DOWNCOMER



OPERATING VOIDAGE VARIATION IN THE DOWNCOMER

2.5 cm jet tube section

3 cm jet tube section

Sand Grade III



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SOLID CIRCULATION RATE VARIATION



SOLID CIRCULATION RATE VARIATION

2.5 cm jet tube section

3 cm jet tube section

28

15 cm spacer section



SUSPENSION DENSITY VARIATION IN THE DOWNCOMER/FUEL REACTOR



SUSPENSION DENSITY VARIATION IN THE FUEL REACTOR/DOWNCOMER

2.5 cm jet tube section

3 cm jet tube section

Sand Grade III



CONCLUSIONS

- Existing interconnected reactor arrangements for CLC have some issues
- ► To overcome some of these issues, RCFB reactor has been proposed
- ► RCFB can be used as
- 1. An interconnected reactor arrangement
 - Single reactor working in cycles of air reactor cycle and fuel reactor cycle with N₂ bubbled in between the cycles
- 2. A single RCFB where the riser is acting as air reactor and downcomer as fuel reactor
 - In this configuration a permanent seal is required on the top downcomer section



- The draft tube in the RCFB ensures good solid mixing & solid circulation, longer residence time which results in maintaining uniform temperature throughout the reactor and better distribution of bed inventory and fuels
- The construction of the RCFB reactor is not complex as it does not have cyclone separator and complex loop seals, which makes it less expensive with flexible operating conditions.
- ▶ Further experimental studies are needed to verify the claims made.



THANK YOU

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